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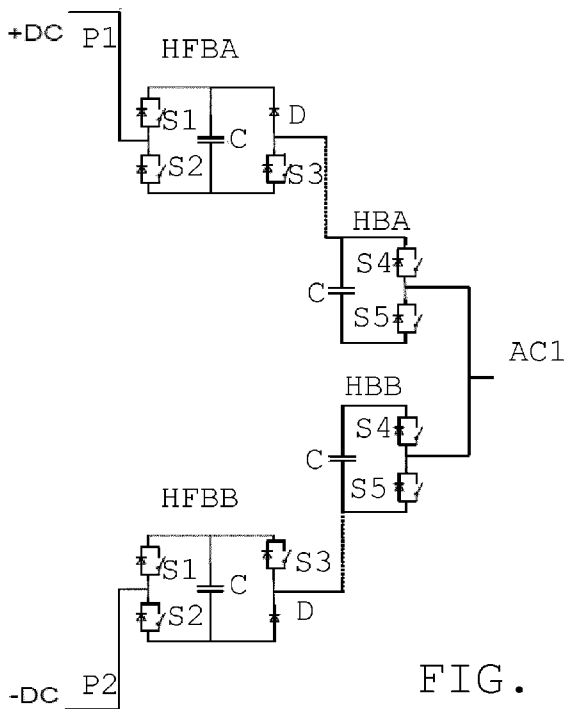


FIG. 6

(57) Abstract: A multilevel converter (10) converting between AC and DC comprises a phase arm with a number of cells between a DC pole (P1) and an AC terminal (AC1), the cells comprise at least one hybrid full bridge cell (HFBA) including a first cell connection terminal for coupling to the DC pole, a second cell connection terminal for coupling to the AC terminal, an energy storage element (C) having a positive and a negative end, a first group of series connected semiconducting units (S1, S2) in parallel with the energy storage element (C), where a junction between these forms one cell connection terminal, and a second group of series connected semiconducting units in parallel with the energy storage element (C) and comprising a third semiconducting unit (S3) and a fourth semiconducting unit consisting of a number of unidirectional conducting elements comprising at least one unidirectional conducting element (D), where a junction between these forms a further cell connection terminal.



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A MULTILEVEL CONVERTER WITH HYBRID FULL-BRIDGE CELLS

FIELD OF INVENTION

5 The present invention generally relates to multilevel converters. More particularly the present invention relates to a multilevel converter configured to convert between alternating current and direct current.

10 BACKGROUND

Multilevel converters are of interest to use in a number of different power transmission environments. They may for instance be used as voltage source
15 converters in direct current power transmission systems such as high voltage direct current (HVDC) and alternating current power transmission systems, such as flexible alternating current transmission system (FACTS). They may also be used as reactive compensation
20 circuits such as Static VAR compensators.

In order to reduce harmonic distortion in the output of power electronic converters, where the output voltages can assume several discrete levels, so called
25 multilevel converters have been proposed. In particular, converters where a number of cascaded converter cells, each comprising a number of switching units and an energy storage unit in the form of a DC capacitor have been proposed.

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Examples of such converters can be found in Marquardt, 'New Concept for high voltage-Modular

multilevel converter', IEEE 2004, A. Lesnicar, R. Marquardt, "A new modular voltage source inverter topology", EPE 2003, WO 2010/149200 and WO 2011/124260.

5 Converter elements in such a converter may for instance be of the half-bridge, full-bridge or clamped double cell type.

A half-bridge connection in upper and lower arms
10 provides unipolar cell voltage contributions and offers the simplest structure of the chain link converter. This type is described by Marquardt, 'New Concept for high voltage-Modular multilevel converter', IEEE 2004 and A. Lesnicar, R. Marquardt, "A new modular voltage
15 source inverter topology", EPE 2003.

However, there is a problem with the half-bridge topology in that the fault current blocking ability in the case of a DC fault, such as a DC pole-to-pole or a
20 DC pole-to-ground fault, is limited.

One way to address this is through the use of full-bridge cells. This is described in WO 2011/012174. Series connection of full-bridge cells offers four
25 quadrant power flows through the energy storage element of the cell capacitor as well as DC fault voltage blocking capability by imposing a reverse voltage. However, the use of full-bridge cells doubles the number of components compared with a half-bridge cell.

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One way to reduce the number of components combined with a retained fault current limiting ability is through mixing the cells of the half- and full-bridge

type. Half of the cells may then be full-bridge cells used for imposing the reverse voltage due to the rating of the cascaded converter cells. This is for instance described in WO 2011/042050. The mixing of cells
5 reduces the number of components further while retaining a good fault current limitation ability.

However there is still room for improvement with regard to component reduction combined with fault current
10 limitation.

SUMMARY OF THE INVENTION

The present invention is directed towards reducing the
15 number of components in a voltage source converter combined with providing sufficient fault current limitation.

This object is according to a first aspect achieved
20 through a multilevel converter configured to convert between alternating current and direct current and comprising
at least one phase arm with a number of cells between a DC pole and an AC terminal, the cells comprising at
25 least one hybrid full-bridge cell for fault current handling operation,
said hybrid full-bridge cell comprising
a first cell connection terminal for coupling to the DC pole,
30 a second cell connection terminal for coupling to the AC terminal,
an energy storage element having a positive and a negative end,

a first group of series connected semiconducting units, which group is connected in parallel with the energy storage element and where the semiconducting units of the first group comprises first and second switching elements with first and second anti-parallel unidirectional conducting elements, where a junction between the first and second semiconducting unit forms one cell connection terminal,

a second group of series connected semiconducting units, which group is connected in parallel with the energy storage element as well as with the first group and where the semiconducting units of the second group comprises a third semiconducting unit having a third switching element with anti-parallel unidirectional conducting element and a fourth semiconducting unit consisting of at least one unidirectional conducting element, where a junction between the first and second semiconducting unit forms a further cell connection terminal.

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The present invention has a number of advantages. It provides equal fault limiting capability as similar conventional converter structures with a reduced number of components. This is combined with a modular cell structure with low complexity and low costs. Another advantage is that the number of control signals needed for controlling the cell are reduced.

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BRIEF DESCRIPTION OF THE DRAWINGS

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The present invention will in the following be described with reference being made to the accompanying drawings, where

fig. 1 schematically shows a cell-based voltage source converter connected between two poles,
fig. 2 schematically shows the structure of a first
5 type of hybrid full-bridge cell,
fig. 3 schematically shows the structure of a first type of half-bridge cell,
fig. 4 schematically shows the structure of a second type of hybrid full-bridge cell,
10 fig. 5 schematically shows the structure of a second type of half-bridge cell,
fig. 6 schematically shows a first realization of a voltage source converter phase leg employing hybrid full-bridge cells of the first and second type and
15 half-bridge cells of the first and second type,
fig. 7 schematically shows a fault current path through an upper phase arm of the converter of fig. 6 in case of a first pole-to-ground fault occurring with a positive AC voltage,
20 fig. 8 schematically shows a fault current path through the upper phase arm of the converter of fig. 6 in case of the first pole-to-ground fault occurring with a negative AC voltage,
fig. 9 schematically shows a fault current path through
25 a lower phase arm of the converter of fig. 6 in case of a second pole-to-ground fault occurring with a negative AC voltage,
fig. 10 schematically shows a fault current path through the lower phase arm of the converter of fig. 6
30 in case of the second pole-to-ground fault occurring with a positive AC voltage,
fig. 11 schematically shows the structure of a third type of hybrid full-bridge cell, and

fig. 12 schematically shows the structure of a fourth type of hybrid full-bridge cell.

DETAILED DESCRIPTION OF THE INVENTION

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In the following, a detailed description of preferred embodiments of the invention will be given.

Fig. 1 shows one variation of a multilevel converter in the form of a cell based voltage source converter 10. The converter operates to convert between alternating current (AC) and direct current (DC). The converter 10 in fig. 1 comprises a three-phase bridge made up of a number of phase legs. There are in this case three phase legs. It should however be realized that as an alternative there may be for instance only two phase legs. There is thus a first phase leg PL1, a second phase leg PL2 and a third phase leg PL3. The phase legs are more particularly connected between two DC poles, a first DC pole P1 and a second DC pole P2 and the mid points of the phase legs are connected to corresponding alternating current terminals AC1, AC2, AC3. The midpoint of a phase leg is here connected to a corresponding AC terminal via a reactor LAC1, LAC2 and LAC3. A phase leg is thereby divided into two halves, an upper half and a lower half, where such a half is also termed a phase arm.

The first DC pole P1 furthermore has a first potential +DC that may be positive, while the second DC pole has a second potential -DC that may be negative. The first pole P1 may therefore also be termed a positive pole, while the second pole P2 may be termed negative pole.

These poles may furthermore be part of a DC power transmission system such as a High Voltage Direct Current (HVDC) power transmission system or a flexible alternating current transmission system (FACTS).

5

As mentioned above, the voltage source converter of fig. 1 is only one example of a multilevel converter where the invention may be used. It is for instance possible to provide the three phase legs in series with each other between the two poles, where these then make up a first set of phase legs. It is then possible to provide a second set of series-connected phase legs in parallel with the first set. In this case the midpoints of the phase legs of the first set forms primary AC terminals and the midpoints of the phase legs of the second set forms secondary AC terminals for the three phases.

Yet another realization of a multilevel converter is a static VAR compensator.

The phase arms of the voltage source converter 10 in the example in fig. 1 comprise cells. A cell is a unit that may be switched for providing a voltage contribution to the voltage on the corresponding AC terminal. A cell then comprises one or more energy storage elements, for instance in the form of capacitors, and the cell may be switched to provide a voltage contribution corresponding to the voltage of the energy storage element or a zero voltage contribution. If more than one energy storage element is included in a cell it is possible with even further voltage contributions.

The cells are with advantage connected in series or in cascade in a phase arm.

5 In the example given in fig. 1 there are five series-connected or cascaded cells in each phase arm. Thus the upper phase arm of the first phase leg PL1 includes five cells C1u1, C2u1, C3u1, C4u1 and C5u1, while the lower phase arm of the first phase leg PL1 includes
10 five cells C1l1, C2l1, C3l1, C4l1 and C5l1. In a similar fashion the upper phase arm of the second phase leg PL2 includes five cells C1u2, C2u2, C3u2, C4u2 and C5u2 while the lower phase arm of the second phase leg PL2 includes five cells C1l2, C2l2, C3l2, C4l2 and
15 C5l2. Finally the upper phase arm of the third phase leg PL3 includes five cells C1u3, C2u3, C3u3, C4u3 and C5u3 while the lower phase arm of the third phase leg PL3 includes five cells C1l3, C2l3, C3l3, C4l3 and C5l3. The number of cells provided in fig. 1 is only an
20 example. It therefore has to be stressed that the number of cells in a phase arm may vary. It is often favorable to have many more cells in each phase arm, especially in HVDC applications. A phase arm may for instance comprise hundreds of cells. There may however
25 also be fewer.

Control of each cell in a phase arm is normally done through providing the cell with a control signal directed towards controlling the contribution of that
30 cell to meeting a reference voltage. The reference voltage may be provided for obtaining a waveform on the AC terminal of a phase leg, for instance a sine wave.

In order to control the cells there is therefore a control unit 12.

The control unit 12 is provided for controlling all the phase arms of the converter. However, in order to simplify the figure only the control of the upper phase arm of the first phase leg PL is indicated in fig. 1.

The other phase arms are controlled in a similar manner in order to form output waveforms on the three AC terminals AC1, AC2 and AC3.

There are a number of different cell types that can be used in the converter, such as full-bridge cells, half-bridge cells and clamped double cells.

The invention is based on the use of hybrid full-bridge cells. A hybrid full-bridge cell is in the context discussed here defined as a full-bridge cell where one bridge unit comprising at least one switching element anti-parallel unidirectional conducting element pair is replaced by at least one unidirectional conducting element. A hybrid full-bridge cell in the definition used here is in one specific example thus a full-bridge where one of the switches is replaced by a diode. Thereby the cell can furthermore be termed an asymmetric full-bridge cell or an asymmetric hybrid full-bridge cell.

Fig. 2 shows a first type of hybrid full-bridge cell HFBA that is to be provided in the upper phase arm of the first phase leg.

The cell HFBA is thus a hybrid full-bridge converter cell and includes an energy storage element, here in the form of a capacitor C, which is connected in parallel with a first group of semiconducting units SU1 and SU2. The energy storage element provides a voltage U_{dm} , and therefore has a positive and negative end, where the positive end has a higher potential than the negative end. The semiconducting units SU1 and SU2 in the first group are connected in series with each other. The first group here includes two semiconducting units SU1 and SU2 (shown as dashed boxes). These two semiconducting units SU1 and SU2 are here provided as two series-connected switches S1 and S2, where each switch may be realized in the form of a switching element that may be an IGBT (Insulated Gate Bipolar Transistor) transistor together with an anti-parallel unidirectional conducting element. In fig. 2 the first semiconducting unit SU1 is therefore provided as a first switch S1 having a first transistor T1 with a first anti-parallel diode D1. The first diode D1 is connected between the emitter and collector of the transistor T1 and has a direction of conductivity from the emitter to the collector as well as towards the positive end of the energy storage element C. The second semiconducting unit SU2 is provided as a second switch S2 having a second transistor T2 with a second anti-parallel diode D2. The second diode D2 is connected in the same way in relation to the energy storage element C as the first diode D1, i.e. conducts current towards the positive end of the energy storage element C. The first semiconducting unit SU1 is furthermore connected to the positive end of the energy storage element C, while the second semiconducting unit

SU2 is connected to the negative end of the energy storage element C.

There is also a second group of series-connected
5 semiconducting units SU3 and SU4. This second group of semiconducting units is here connected in parallel with the first group as well as with the energy storage element C. The second group includes a third
10 semiconducting unit SU3 and a fourth semiconducting unit SU4. The third semiconducting unit SU3 is provided as a third switch S3, here provided through a third transistor T3 with anti-parallel third diode D3. However the fourth semiconducting unit SU4 is not a switch. It only comprises one type of semiconducting
15 element, a unidirectional conduction element, a diode D. The fourth semiconducting unit SU4 thus consists of unidirectional conducting elements, where the number of such elements is at least one. This second group of semiconducting units is thus provided in a further
20 branch in parallel with the capacitor C. The fourth semiconductor unit SU4 is furthermore connected to the positive end of the energy storage element C, while the third semiconducting unit SU3 is connected to the negative end of the energy storage element C. Both the
25 diodes D3 and D furthermore have a direction of current conduction towards the positive end of the energy storage element C.

This first type of hybrid full-bridge cell HFBA
30 comprises a first cell connection terminal TEFBA1 and a second cell connection terminal TEFBA2, each providing a connection for the cell to the upper phase arm of the first phase leg of the voltage source converter. In

this first type of hybrid full-bridge cell the first cell connection terminal TEFBA1 more particularly provides a connection from the upper phase arm to the junction between the first and the second

5 semiconducting units SU1 and SU2, while the second cell connection terminal TEFBA2 provides a connection between the upper phase arm and a connection point between the third and fourth semiconducting units SU3 and SU4. The junction between the first and second

10 semiconducting units SU1 and SU2 thus provides one cell connection terminal TEFBA1, while the junction between the third and fourth semiconducting units SU3 and SU4 provides a further cell connection terminal TEFBA2. These connection terminals TEFBA1 and TEFBA2 thus

15 provide points where the cell HFBA can be connected to the upper phase arm of the first phase leg. The first cell connection terminal TEFBA1 thereby joins the upper phase arm with the connection point or junction between two of the series-connected switches of the first

20 group, here the first and second switches, while the second cell connection terminal TEFBA2 joins the upper phase arm with a connection point between two of the series connected semiconducting units of the second group, here between the third switch and the sole diode

25 D. The first cell connection terminal TEFBA1 furthermore faces the first pole and thereby couples the cell to the first pole, while the second cell connection terminal TEFBA2 faces the AC terminal of the phase leg and thereby couples the cell to the AC

30 terminal. Thereby the further diode D also couples the second cell connection terminal TEFBA2 to the positive end of the energy storage element.

The expression couple or coupling is intended to indicate that more components, such as more cells and inductors, may be connected between the pole and the cell, while the expression connect or connecting is intended to indicate a direct connection between two components such as two cells. There is thus no component in-between two components that are connected to each other.

10 Fig. 3 schematically shows a first type of half-bridge converter cell HBA that may be used in the upper phase arm of the first phase leg. Also this cell includes an energy storage element, here in the form of a capacitor C, which is connected in parallel with a group of
15 switches. Also this energy storage element C provides a voltage U_{dm} , and thus also has a positive and negative end, where the positive end has a higher potential than the negative end. The switches in this group are connected in series with each other. The group here
20 includes a fourth and a fifth switch S4 and S5 (shown as dashed boxes), where each switch S4, S5 may be realized in the form of a switching element that may be an IGBT (Insulated Gate Bipolar Transistor) transistor together with an anti-parallel unidirectional
25 conduction element, which may be a diode. In fig. 3 there is therefore a fourth switch S4 having a fourth transistor T4 with a fourth anti-parallel diode D4, where the diode D4 has a direction of current conduction towards the positive end of the energy
30 storage element C and a fifth switch S5 connected in series with the fourth switch S4 and having a fifth transistor T5 with anti-parallel diode D5, where the diode D5 has the same direction of current conduction

as the fourth diode D4. The fourth switch S4 is connected to the positive end of the energy storage element C, while the fifth switch S5 is connected to the negative end of the energy storage element C.

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This first type of half-bridge cell HBA also comprises a first cell connection terminal TEHBA1 and a second cell connection terminal TEHBA2, each providing a connection for the cell to the upper phase arm of the first phase leg of the voltage source converter. In this first type of cell the first cell connection terminal TEHBA1 more particularly provides a connection from the upper phase arm to the junction between the fourth switch S4 and the capacitor C, while the second connection terminal TEHBA2 provides a connection from the upper phase arm to the junction between the fourth and the fifth switches S4 and S5. These cell connection terminals thus provide points where the cell can be connected to the upper phase arm. The second cell connection terminal TEHBA2 thus joins the phase arm with the connection point or junction between two of the series-connected switches of the first group, here the fourth and fifth switches S4 and S5, while the first cell connection terminal TEHBA1 joins the upper phase arm with a connection point between the fourth switch S4 and the positive end of the capacitor C. Also here the first cell connection terminal TEHBA1 faces the first pole, while the second cell connection terminal TEHBA2 faces the AC terminal of the phase leg.

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Fig. 4 shows a second type of hybrid full-bridge cell HFBB that may be provided in the second phase arm of the first phase leg.

The cell HFBB is thus a hybrid full-bridge converter cell and also includes an energy storage element, here in the form of a capacitor C, which is connected in parallel with a first group of semiconducting units.

5 Also this energy storage element C provides a voltage U_{dm} , and therefore has a positive and negative end, where the positive end has a higher potential than the negative end. The first group also here includes two series-connected semiconducting units SU1 and SU2
10 (shown as dashed boxes) in the form of switches S1 and S2. In fig. 4 there is a first switch S1 having a first transistor T1 with a first anti-parallel diode D1, where the diode D1 has a direction of current conduction towards the positive end of the energy
15 storage element C. There is also a second switch comprising a second transistor T2 with anti-parallel second diode D2 and having the same current conduction as the first diode D1. The first semiconducting unit SU1 is also here connected to the positive end of the
20 energy storage element C, while the second semiconducting unit SU2 is connected to the negative end of the energy storage element C.

There is in this case also a second group of
25 semiconducting units connected in series with each other. This second group of semiconducting units is here connected in parallel with the first group as well as with the energy storage element C. The second group also here includes a third semiconducting unit SU3 and
30 a fourth semiconducting unit SU4, where the third semiconducting unit SU3 is provided through a third switch S3 comprising a third transistor T3 with anti-parallel third diode D3 and the fourth semiconducting

unit SU4 is provided using only unidirectional conduction elements, in this example a diode D. The fourth semiconducting unit SU4 thereby consists of a number of unidirectional conducting elements,
5 comprising at least one element. The second group of semiconducting units is thus provided in a further branch in parallel with the capacitor C. The fourth semiconductor unit SU4 is in this case connected to the negative end of the energy storage element C, while the
10 third semiconducting unit SU3 is connected to the positive end of the energy storage element C. The current conducting direction of both diodes D3 and D is towards the positive end of the energy storage element C.

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This second type of hybrid full-bridge cell HFBB comprises a first cell connection terminal TEFBB1 and a second cell connection terminal TEFBB2, each providing a connection for the cell to the lower phase arm of the
20 voltage source converter, i.e. the lower phase arm of the first phase leg. Just as in the first type of hybrid full-bridge cell, the first cell connection terminal TEFBB1 provides a connection from the lower phase arm to the junction between the first and the
25 second semiconducting units SU1 and SU2, while the second cell connection terminal TEFBB2 provides a connection between the lower phase arm and the connection point between the third and fourth semiconducting units SU3 and SU4. The junction between
30 the first and the second switching units SU1 and SU2 thus provide a cell connection terminal and the junction between the third and fourth semiconducting units SU3 and SU4 provide a further cell connection

terminal. In this case the first cell connection terminal TEFBB1 furthermore faces the second pole and thereby couples the cell to the second pole, while the second cell connection terminal TEFBB2 faces the AC terminal of the phase leg. The second cell connection terminals thereby couples the cell to the AC terminal of the phase leg, while the at least one unidirectional conducting element couples the second cell connection terminal to the negative end of energy storage element C.

Fig. 5 shows a corresponding second type of half-bridge cell HBB for connection in the lower phase arm of the first phase leg. It comprises a group of switches comprising a fourth and fifth switch S4 and S5 connected in the same way as the fourth and fifth switches of the first type of half-bridge cell. However, in this second type of half-bridge cell the first cell connection terminal TEHBB1 provides a connection from the lower phase arm to the junction between the fourth and the fifth switches S4 and S5, while the second cell connection terminal TEHBB2 provides a connection from the lower phase arm to the junction between the fifth switch S5 and the negative end of the capacitor C. Also in this case the first cell connection terminal TEHBB1 faces the second pole, while the second cell connection terminal TEHBB2 faces the AC terminal of the phase leg.

Fig. 6 schematically shows a phase leg where the upper phase arm comprises the first type of hybrid full bridge cells and the first type of half-bridge cells, while the lower phase arm comprises the second type of

hybrid full bridge cells and the second type of half-bridge cells connected in the above described way.

The number of hybrid full-bridge cells in the upper
5 phase arm may be between 20 and 100% of all the cells
in the upper phase arm, may advantageously be between
20 and 50% and may as an example be 50%, while the rest
of the cells in the upper phase arm are half-bridge
cells. The same distribution may be provided in the
10 lower phase arm.

In normal operation of the converter cells, the first
type of hybrid full-bridge cell and the first type of
half-bridge cell of the upper arm of the phase leg
15 shown in fig. 6 are operated according to the switching
table below, table 1. In the table the switching states
of the first, second and third switches S1, S2 and S3
of the first type of hybrid full bridge cell are shown
together with the switching states of the fourth and
20 fifth switches S4 and S5 of the first type of half-
bridge cell. Furthermore, in the table the two cells
are considered as a pair together providing a voltage
Vout. The table therefore shows the combination of
switching states causing a voltage contribution that
25 lowers the first pole voltage +DC. There is thus a
voltage contribution $-2U_{dm}$ that lowers the pole voltage
by the voltage across both cells, a voltage
contribution $-U_{dm}$ that lowers the pole voltage by the
voltage across a single cell and a zero voltage
30 contribution. In the table also the direction of the
phase arm current I_{arm} , i.e. the current through the
upper phase arm, is indicated. As can be seen in the

table, the switching states are independent of the current direction in the phase arm.

S1	S2	S3	S4	S5	Vout	Iarm
1	0	1	0	1	-2Udm	Iarm<0 or Iarm>0
1	0	1	1	0	-Udm	
0	1	1	0	1	-Udm	
0	1	1	1	0	0	

5

TABLE 1

In a similar manner the switching states of the switches of the second type of hybrid full bridge cell and the second type of half-bridge cell of the lower phase arm of the phase leg shown in fig. 6 are operated according to the switching table below, table 2. In the table the switching states of the first, second and third switches S1, S2 and S3 of the second type of hybrid full-bridge cell are shown together with the switching states of the fourth and fifth switches S4 and S5 of the second type of half-bridge cell. Also here the two cells are considered as a pair together providing a voltage Vout. The table thus shows the combination of switching states causing a voltage contribution that raises the second pole voltage -DC. There is thus a voltage contribution +2Udm that raises the pole voltage by the voltage across both cells, a voltage contribution +Udm that raises the pole voltage by the voltage across a single cell and a zero voltage contribution. In the table also the direction of the phase arm current Iarm, i.e. the current through the lower phase arm, is indicated. As can be seen also here

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the switching states are independent of the current direction in the phase arm.

S1	S2	S3	S4	S5	Vout	Iarm
1	0	1	0	1	0	Iarm<0 or Iarm>0
1	0	1	1	0	+Udm	
0	1	1	0	1	+Udm	
0	1	1	1	0	+2Udm	

5

TABLE 2

In the hybrid full-bridge cell, the second branch of semiconducting units, i.e. the branch comprising the third and the fourth semiconducting units, here the branch with the third switch S3 and the diode D, is
 10 redundant in normal operation. This can be seen through the third switch S3 always being turned on. This means that the third switch S3 does in normal operation always provide a current path between the AC terminal of the phase leg and the corresponding pole. It can
 15 also be seen that therefore there is no needed for any switching element in parallel with the diode D of the fourth semiconducting unit of the full-bridge cells.

The reason for using full-bridge cells is ordinarily
 20 not for improving the normal operation, but to be able to limit and sometimes also block fault currents in case of a DC pole fault, such as a pole-to-pole fault or a pole-to-ground fault. When there is a pole-to-ground fault the voltage at the AC terminal of as phase
 25 leg can be considered as forming an AC voltage source VAC feeding the phase leg with an AC voltage. When such a fault occurs, the switching elements of all the

switches may be opened by the control unit of the converter. The switching element of the third switch S3 may more particularly be open, at least in the negative half period of the AC voltage for the first type of hybrid full-bridge cell HFBA and at least in the positive half period of the AC voltage for the second type of hybrid full-bridge cell HFBB.

Fig. 7 shows the fault current through the upper phase arm of fig. 6 in case of a positive pole-to-ground fault at a positive half period of the AC voltage cycle of the AC voltage source VAC and fig. 8 shows the fault current through the upper phase arm of fig. 6 in case of a positive pole-to-ground fault at a negative half period of the AC voltage cycle of the AC voltage source VAC.

As can be seen in fig. 7, the fault current will, in the positive half-period of the AC voltage source VAC, run from the AC voltage source VAC, through the fourth switch S4, through the diode D, through the hybrid cell capacitor and through the diode of the second switch S2 to the first pole. It can also be seen that since the first pole has a positive potential during normal operation, the diode D is together with the second switch S2 connected in a branch between the first and the second cell connection terminals of the hybrid cell that couples the negative end of the hybrid cell energy storage unit to the first pole. It can in this way be seen that the diode D couples an end of the hybrid cell energy storage unit to a pole, which end has a polarity that is opposite to the polarity of the pole in normal operation.

As can be seen in fig. 8, the fault current will, in the negative half-period of the AC voltage source VAC, flow from the first pole, through the first switch S1, through the hybrid cell capacitor, through the diode of the third switch S3, through the half-bridge cell capacitor and through the diode of the fifth switch S5 to the AC voltage source VAC. It can here be seen that the switching element of the third switch S3 is needed in order for the current to pass through hybrid cell capacitor in the situation depicted in fig. 7. However, there is no need for a switching element in parallel with the diode D for obtaining the same result in the situation in fig. 8.

15

As can be seen there is in both cases, i.e. for both current directions, inserted a cell voltage that limits the fault current. It can also be seen that when the fault current is positive, i.e. runs from the first pole towards the AC terminal, then the voltages of both cells are inserted in the path and thereby limit the fault current. It can also be seen that the diode D functions to couple the energy storage element of the hybrid full bridge cell HFBA between the first and the second cell connection terminals of the hybrid full bridge cell HFBA with a polarity that counteracts negative currents in the phase arm. This means that when the diode D is conducting, the negative end of the hybrid full-bridge cell capacitor faces the first pole P1 and the positive end faces the AC terminal AC1.

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A similar situation is at hand if there is a negative pole-to-ground fault.

Fig. 9 shows the fault current through the lower phase arm of fig. 6 in case of a negative pole-to-ground fault at the negative half period of the AC voltage cycle of the AC voltage source VAC and fig. 10 shows the fault current through the lower phase arm of fig. 6 in case of a negative pole-to-ground fault at the positive half period of the AC voltage cycle of the AC voltage source VAC.

10

As can be seen in fig. 9, the fault current will, in the negative half-period of the voltage source VAC, flow from the second pole, through the diode of the first switch S1, through the hybrid cell capacitor, through the diode D and through the diode of the fifth switch S5 to the AC voltage source VAC. It can also be seen that since the second pole has a negative potential during normal operation, the diode D is together with the first switch S1 provided in a branch between the first and the second cell connection terminals of the hybrid cell that couples the positive end of the hybrid cell energy storage unit to the second pole. It can in this way be seen that the diode D couples an end of the hybrid cell energy storage unit to a pole, which end has a polarity that is opposite to the polarity of the pole in normal operation.

As can be seen in fig. 10, the fault current will, in the positive half-period of the AC voltage source VAC, run from the AC voltage source VAC, through the fourth switch S4, through the half-bridge cell capacitor, through the diode of the third switch S3, through the hybrid cell capacitor and through the diode of the

30

second switch S2 to the second pole. It can also here be seen that the switching element of the third switch S3 is needed in order for the current to pass through hybrid cell capacitor in the situation depicted in fig. 9. However, there is no need for a switching element in parallel with the diode D for obtaining the same result in the situation in fig. 10.

As can be seen there is in both cases inserted a cell voltage that limits the fault current. It can also be seen that when the fault current is positive, i.e. runs from the second pole to the AC source, then the voltages of both cells are inserted in the path and thereby limit the fault current. It can also in this case be seen that the diode D functions to couple the energy storage element of the hybrid full bridge cell HFBB between the first and the second cell connection terminals of the hybrid full bridge cell HFBB with a polarity that counteracts negative currents in the phase arm. This means that when the diode D is conducting the positive end of the hybrid full-bridge cell capacitor faces the second pole P2 and the negative end faces the AC terminal AC1.

If enough such hybrid cells are provided in a phase arm, the fault current because of a pole-to-ground fault of the corresponding pole may be completely blocked.

It can thus be seen that as compared with a conventional topology that mixes half-bridge cells with conventional full-bridge cells, the same fault limiting or fault blocking ability is obtained, however using

less components. Furthermore the complexity of the structure is also kept low, which directly affects the cost, loss and modularity of the total converter design.

5

There is thus provided an alternative mixed cell configuration for DC fault current limitation or DC fault current blocking in cascaded converters used in HVDC, FACTS and other similar applications. The structure thus offers a lower number of components compared to other cell configurations with similar features (DC voltage blocking and fault blocking capability).

10

15

This structure operates in the same way as normal cascaded two level half-bridge cells (CTL) while one of the active switches, the third switch, of the hybrid cell is always ON and generate either $2U_{dm}$, U_{dm} , 0 voltage levels, according to different switching states. However, in case of a DC fault, this third switch is turned OFF to provide an opposite voltage polarity according to the fault position in upper or lower arm. This results in the DC fault being blocked or limited.

20

25

The cell structure comprises 5 transistor antiparallel diode pairs and only one extra diode which can save one active switch compared to a converter configuration where there is a mix of half-bridge cells and conventional full-bridge cells.

30

It should be realized that the hybrid cell structures used both in the upper and lower phase arms may be varied.

5 A third type of hybrid cell structure HFBC that may be used in the upper phase arm is schematically shown in fig. 11. This type differs from the structure of the first type through the fourth semiconducting unit SU4 with the diode D being connected to the negative end of
10 the cell capacitor C and the third semiconducting unit SU3 being connected to the positive end of the cell capacitor C. The first cell connection terminal TEFBC1 is further provided at the junction between the third and fourth semiconducting units SU3 and SU4, while the
15 second cell connection terminal TEFBC2 is provided between the first and second semiconducting units SU1 and SU2. In this type of cell the first cell connection terminal TEFBC1 is a further cell connection terminal coupling the cell HFBC to the first pole and the at
20 least one unidirectional conducting element couples the first cell connection terminal TEFBC1 to the negative end of the energy storage element C.

A fourth type of hybrid cell structure HFBD that may be
25 used in the lower phase arm is schematically shown in fig. 12. This differs from the structure of the second type through the fourth semiconducting unit SU4 with the diode D being connected to the positive end of the cell capacitor C and the third semiconducting unit SU3
30 being connected to the negative end of the cell capacitor C. The first cell connection terminal TEFBD1 is further provided at the junction between the third and fourth semiconducting units SU3 and SU4, while the

second cell connection terminal TEFBD2 is provided between the first and second semiconducting units SU1 and SU2. In this type of cell the first cell connection terminal TEFBD1, which is here a further cell
5 connection terminal, couples the cell to the second pole and the at least one unidirectional conducting element D couples the first cell connection terminal TEFBD1 to the positive end of the energy storage element C.

10

The third type of hybrid cell may replace the first type in the upper arm. The third type may also be combined with the first type. There may thus be cells of both the first and the third type of hybrid cell in
15 the upper phase arm.

In a similar manner, the fourth type of hybrid cell may replace the second type in the lower arm. It may also be combined with the second type. There may thus be
20 cells of both the second and the fourth type of hybrid cells in the lower phase arm.

There are a number of further variations that are possible apart from those already mentioned. It is
25 possible that only one of the phase arms comprises hybrid full-bridge cells. This may be of interest if pole-to-ground faults of one of the poles are extremely rare. This may be the case if one of the poles is an overhead line while the other is provided through a
30 cable. All cells of a phase arm may also be hybrid cells.

The distribution between the hybrid full-bridge cells and the half-bridge cells may furthermore vary. The percentage of hybrid-full bridge cells in a phase arm may for instance vary between 20 and 100%. As an
5 alternative it may vary between 20 and 50%. 50% is normally the percentage required for full fault current blocking ability. A higher percentage may be wanted if redundancy is an issue, while a lower may be used if only fault current limitation is desired. The other
10 cells, i.e. the cells that are not hybrid full-bridge cells, are furthermore not necessarily half-bridge cells. They can also be full-bridge cells or clamped double-cells. It is furthermore possible with a different distribution of hybrid full-bridge cells in
15 the two phase arms. The hybrid full-bridge cells may furthermore be provided in other types of converters than the ones shown, such is in converters that employ full bridge-cells combined with director switches, which director switches operate at a fundamental
20 frequency for selectively connecting an AC terminal to a waveform produced by cells in a phase arm.

The invention also provides the following further advantages:

- It provides a fault tolerant cell structure that can
25 be used for any kind of cascaded converter.
- It lowers the number of components compared to existing cell structures used for DC fault blocking
- On the basis of required voltage rating, the same number of devices is provided in the conduction path as
30 when there is a mix of half-bridge and conventional full-bridge cells

- The number of gate drive circuits required are reduced compared to when there is a mix of half-bridge cells and conventional full-bridge cells
- It provides a modular and easily implemented cell design structure
- It allows the possibility to form a mixture of connections of hybrid full-bridge cells and half-bridge cells and series-connection of hybrid full-bridge cells
- It provides a DC fault voltage blocking capability
- It provides a cost effective structure
- It provides a compact structure
- It provides the possibility to reduce the cost for cascaded topologies
- It provides the possibility to reduce the loss of cascaded topologies

From the foregoing discussion it is evident that the present invention can be varied in a multitude of ways. It shall consequently be realized that the present invention is only to be limited by the following claims.

CLAIMS

1. A multilevel converter (10) configured to convert between alternating current (AC) and direct current (DC) and comprising
5 at least one phase arm with a number of cells between a DC pole (P1; P2) and an AC terminal (AC1), said cells comprising at least one hybrid full bridge cell (HFBA; HFBB, HFBC; HFBD) for fault current handling operation,
10 said hybrid full-bridge cell comprising a first cell connection terminal for coupling to the DC pole,
a second cell connection terminal for coupling to the AC terminal,
15 an energy storage element (C) having a positive and a negative end
a first group of series connected semiconducting units, which group is connected in parallel with the energy storage element (C) and where the semiconducting units
20 (SU1, SU2) of the first group comprises first and second switching elements (T1, T2) with first and second anti-parallel unidirectional conducting elements (D1, D2), where a junction between the first and second semiconducting unit forms one cell connection terminal
25 (TEFBA1; TEFBB1; TEFBC2; TEFBD2),
a second group of series connected semiconducting units, which group is connected in parallel with the energy storage element (C) as well as with the first group and where the semiconducting units of the second
30 group comprises a third semiconducting unit (SU3) having a third switching element (T3) with anti-parallel unidirectional conducting element (D3) and a fourth semiconducting unit (SU4) consisting of at least

one unidirectional conducting element (D), where a junction between the first and second semiconducting unit forms a further cell connection terminal (TEFBA2; TEFBB2; TEFBC1; TEFBD1).

5

2. The multilevel converter according to claim 1, wherein the third switching element (T3) of the third semiconducting unit (SU3) in the second group is always configured to be on in normal operation of the

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converter.

3. The multilevel converter according to claim 1 or 2, wherein all switching elements of the hybrid full-bridge cell are configured to be turned off if a fault current due to a DC pole fault runs through the phase arm.

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4. The multilevel converter according to any previous claim, wherein the direction of conduction of the unidirectional conducting elements of the hybrid full-bridge cell is toward the positive end of the energy storage element.

20

5. The multilevel converter according to any previous claim, wherein the fourth semiconducting unit couples the energy storage element between the first and the second cell connection terminal with a polarity that counteracts negative currents in the phase arm.

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6. The multilevel converter according to any previous claim, wherein one hybrid full-bridge cell (HFBA; HFBC) is provided in a positive phase arm between a first pole (P1) and the AC terminal (AC1).

30

7. The multilevel converter according to claim 6,
wherein the further cell connection terminal is the
first cell connection terminal (TEFBC1) coupling the
5 hybrid full-bridge cell (HFBC) to the first pole (P1)
and the at least one unidirectional conducting element
(D) couples the further cell connection terminal
(TEFBC1) to the negative end of the energy storage
element (C).

10

8. The multilevel converter according to claim 6,
wherein the further cell connection terminal is the
second cell connection terminal (TEFBA2) coupling the
hybrid full-bridge cell (HFBA) to the AC terminal (AC1)
15 and the at least one unidirectional conducting element
(D) couples the further cell connection terminal
(TEFBA2) to the positive end of the energy storage
element (C).

20 9. The multilevel converter according to any previous
claim, wherein one hybrid full-bridge cell (HFBB; HFBD)
is provided in a negative phase arm between a second
pole (P2) and the AC terminal (AC1).

25 10. The multilevel converter according to claim 9,
wherein, in the hybrid-full bridge cell in the negative
phase arm, the further cell connection terminal is the
first cell connection terminal (TEFBD1) coupling the
hybrid full-bridge cell (HFBD) to the second pole (P2)
30 and the at least one unidirectional conducting element
(D) couples the further cell connection terminal
(TEFBD1) to the positive end of the energy storage
element.

11. The multilevel converter according to claim 9,
wherein, in the hybrid-full bridge cell in the negative
phase arm, the further cell connection terminal is the
5 second cell connection terminal (TEFBB2) coupling the
hybrid full-bridge cell (HFBB) to the AC terminal (AC1)
of the phase leg and the at least one unidirectional
conducting element (D) couples the further cell
connection terminal (TEFBB2) to the negative end of the
10 energy storage element (C).

12. The multilevel converter according to any previous
claim, wherein the percentage of hybrid full-bridge
cells in the phase arm is in the range of 20 - 100.
15

13. The multilevel converter according to claim 12,
wherein the percentage of hybrid full-bridge cells in
the phase arm is 50.

20 14. The multilevel converter according to any previous
claim, wherein the phase arm comprises at least one
half-bridge converter cell (HBA; HBB).

15. The multilevel converter according to any previous
25 claim, wherein the phase arm comprises at least one
director switch configured to selectively connect the
AC terminal (AC1) to a waveform produced by cells in
the phase arm.

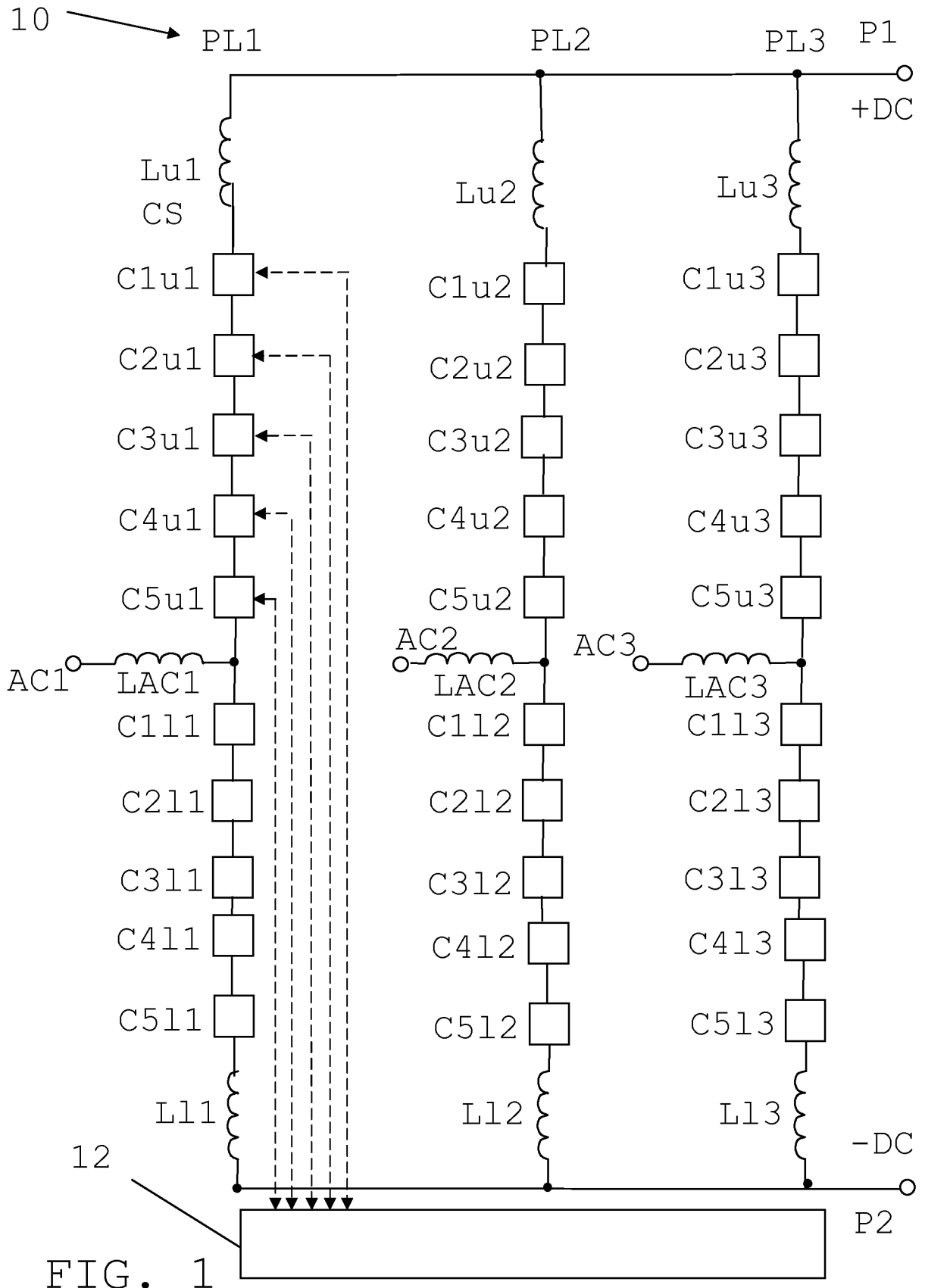
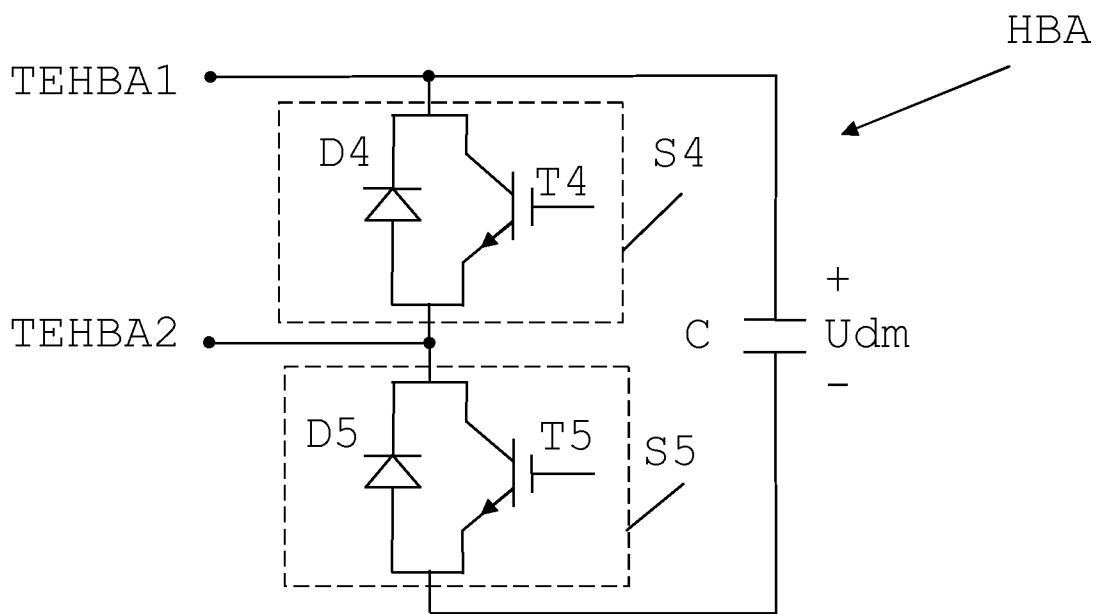
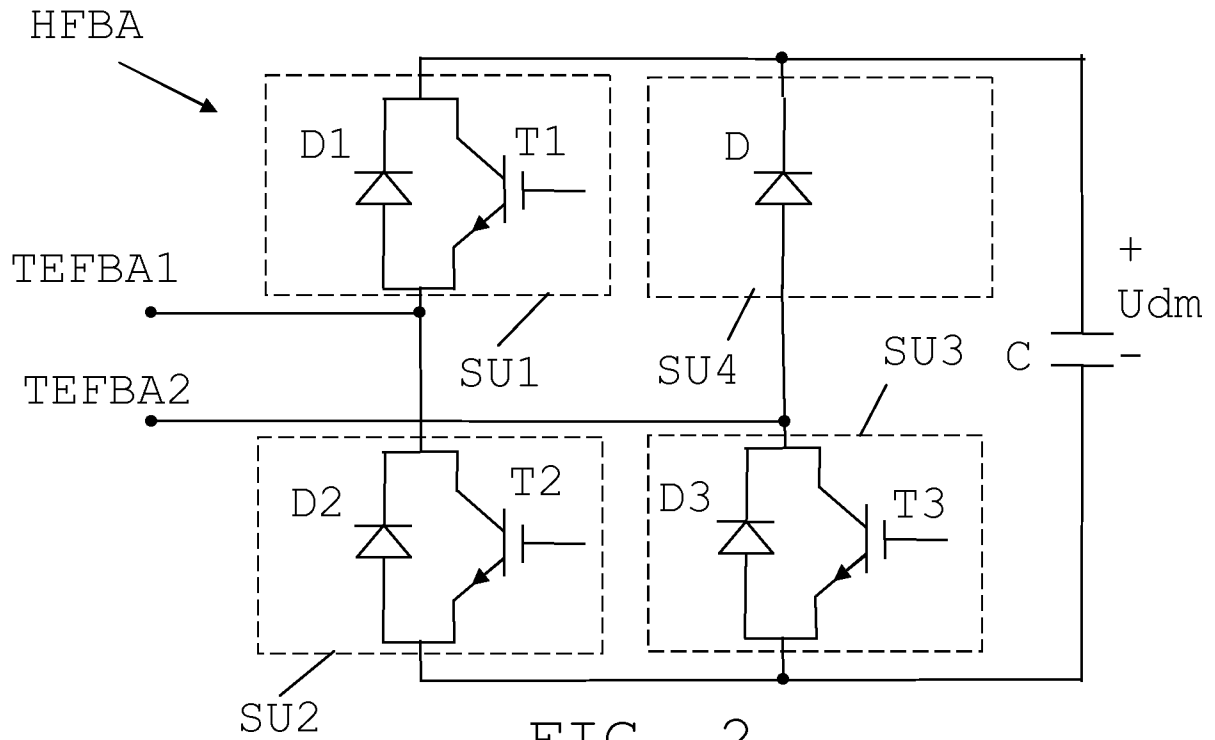


FIG. 1



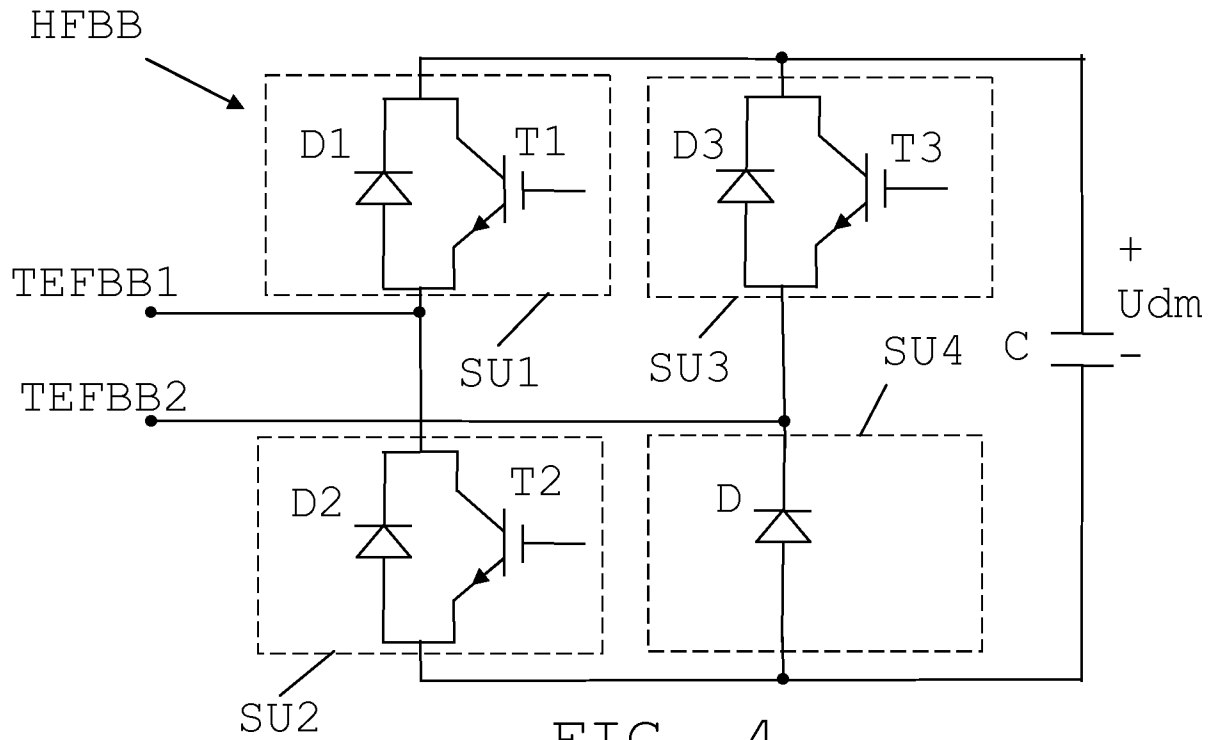


FIG. 4

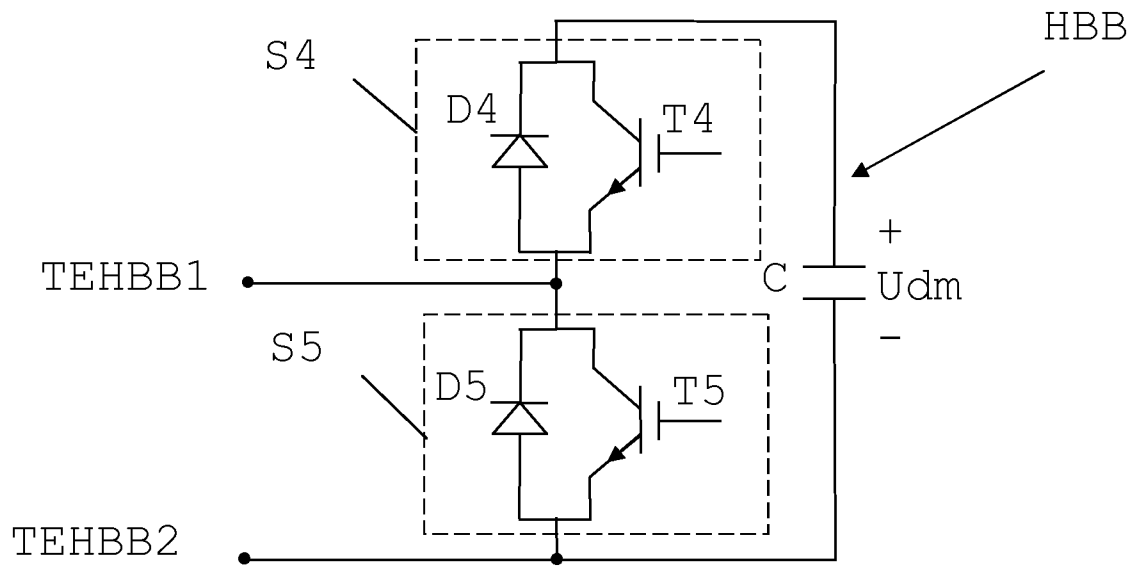


FIG. 5

4 / 7

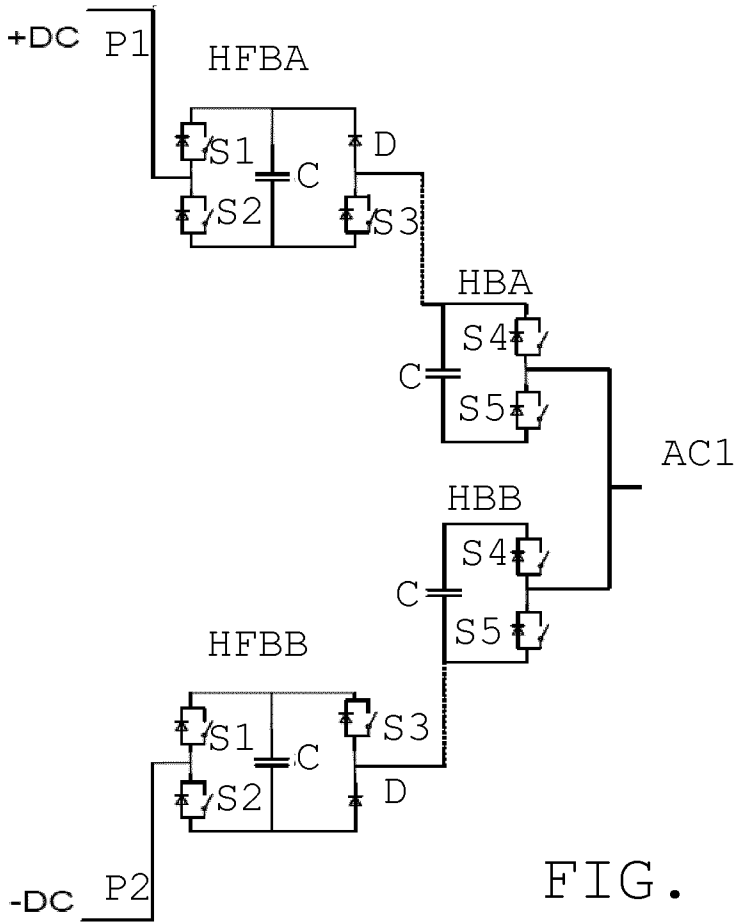


FIG. 6

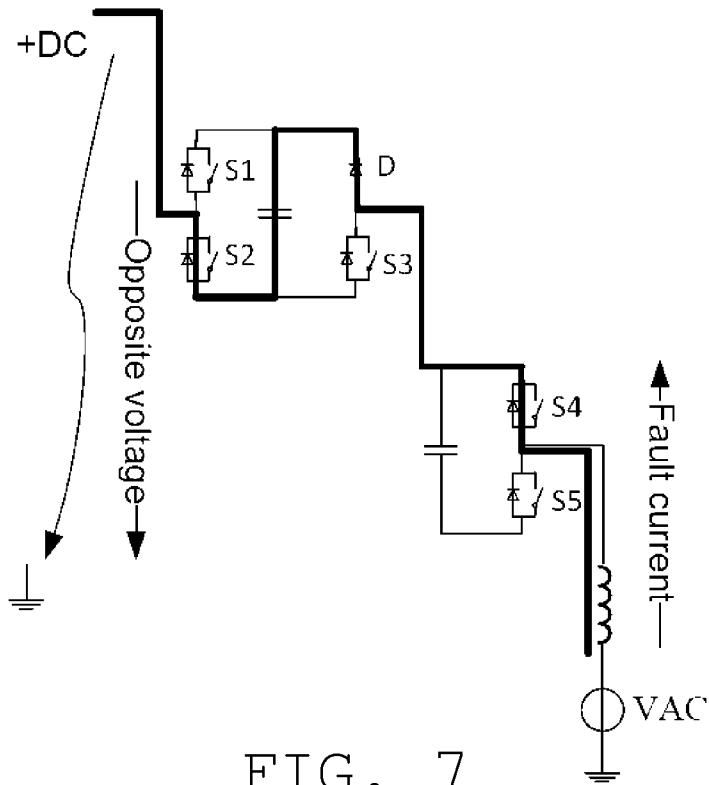


FIG. 7

5/7

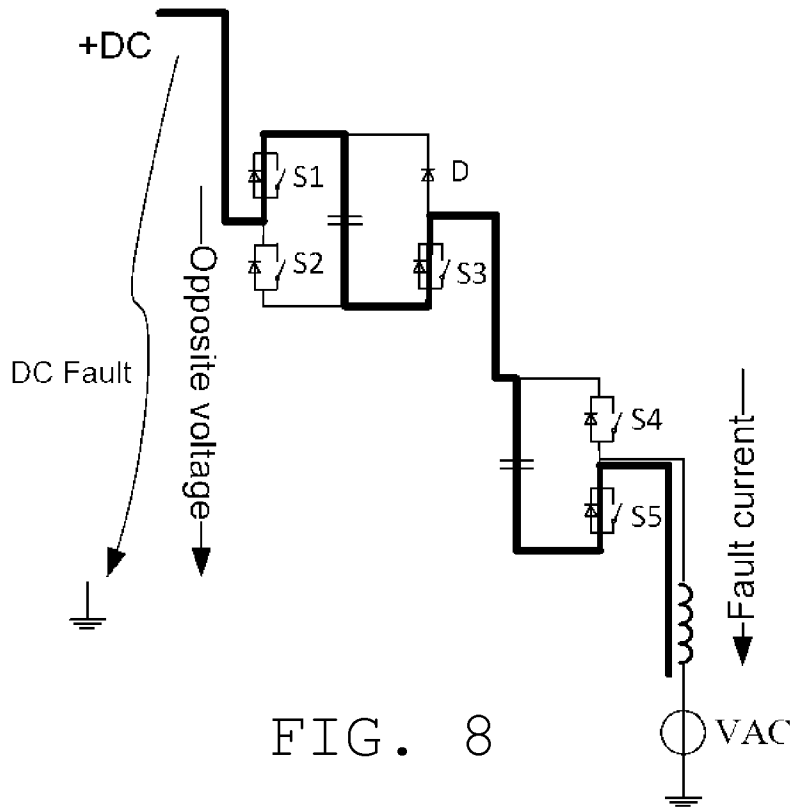


FIG. 8

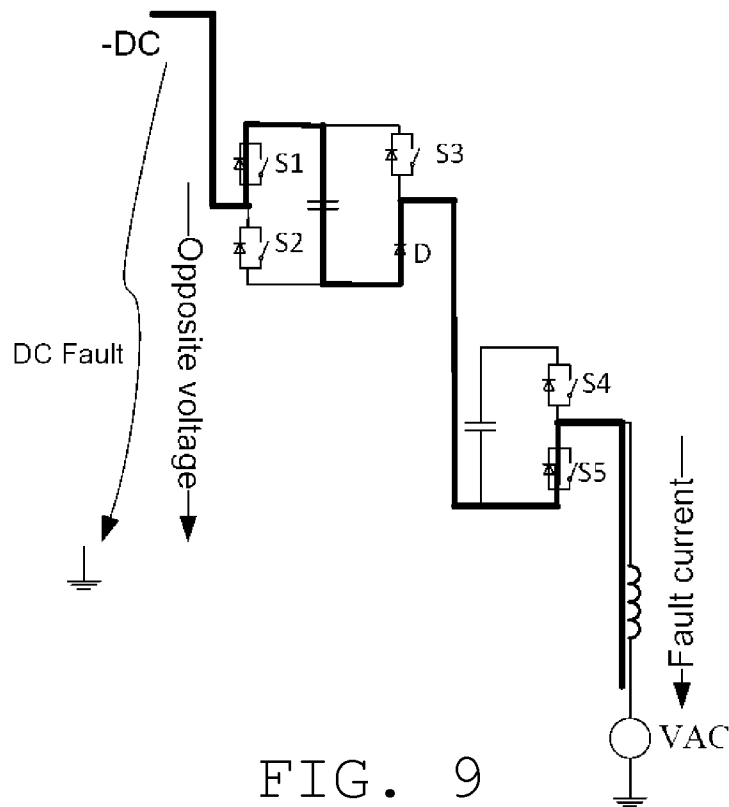


FIG. 9

6/7

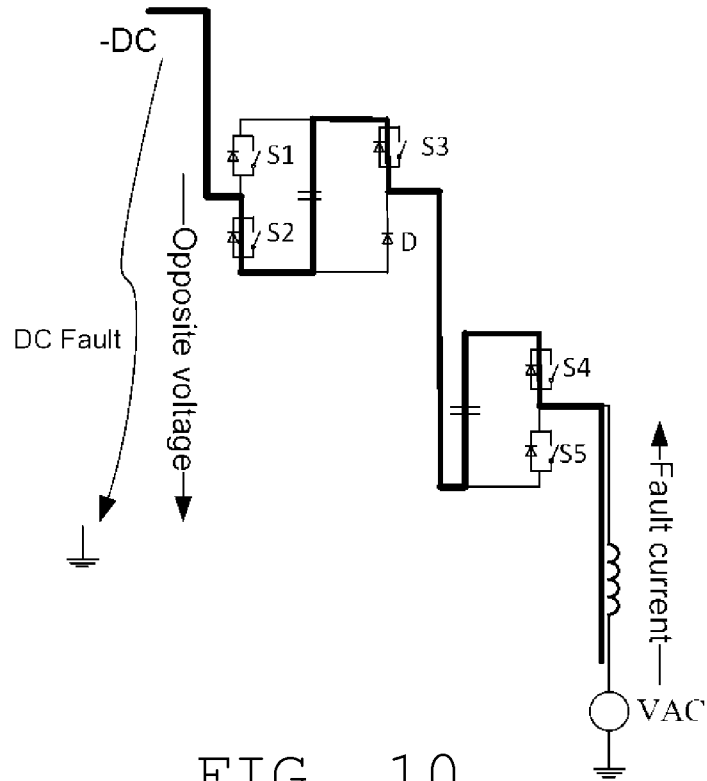


FIG. 10

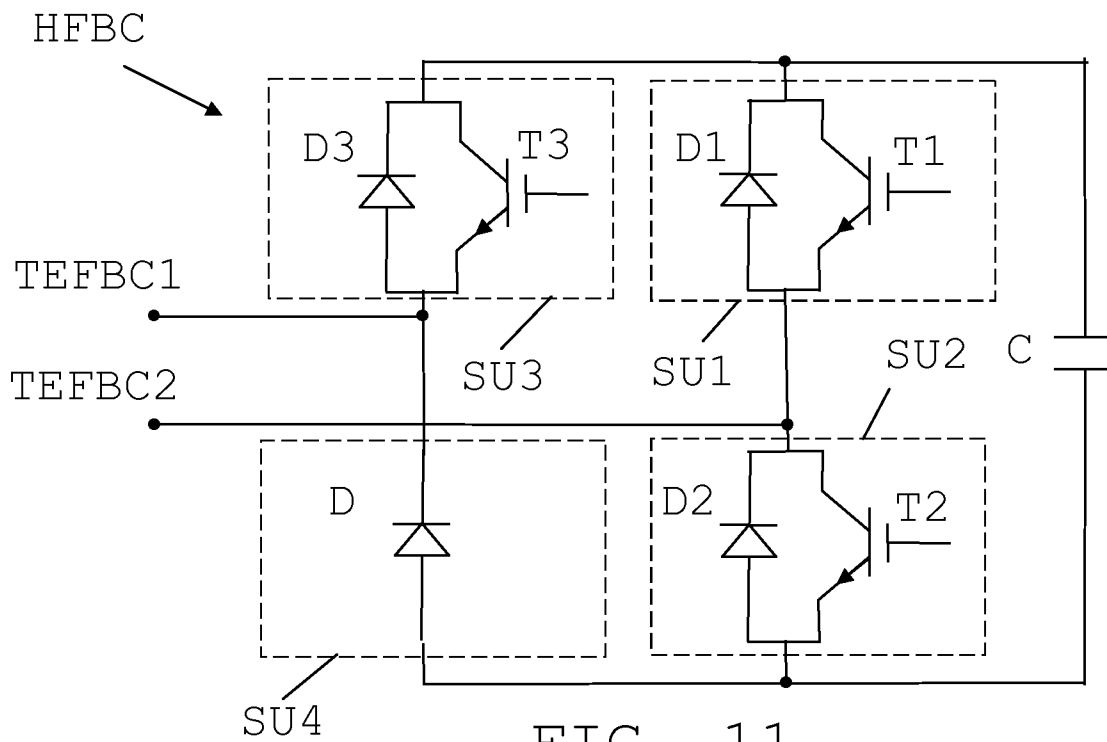


FIG. 11

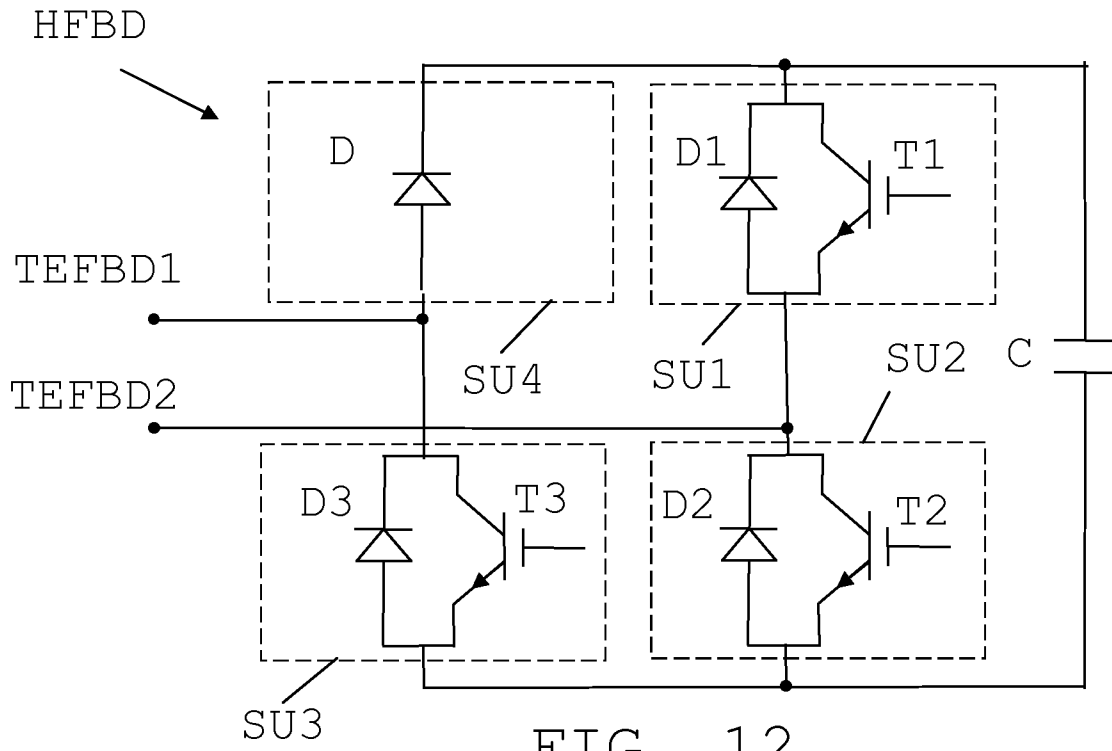


FIG. 12

INTERNATIONAL SEARCH REPORT

International application No
PCT/EP2013/051027

A. CLASSIFICATION OF SUBJECT MATTER
INV. H02M1/32 H02M7/797 H02M7/483
ADD.
According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED
Minimum documentation searched (classification system followed by classification symbols)
H02M
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)
EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	WO 2011/124258 A1 (AREVA T & D UK LTD [GB]; TRAINER DAVID [GB]; CANELHAS ANDRE PAULO [GB]) 13 October 2011 (2011-10-13) figures 2-5 figure 7 figure 12 page 2, line 20 - page 3, line 8 page 6, line 6 - line 10 page 8, line 3 - line 13 page 19, line 1 - line 20 page 21, line 30 - page 22, line 10 page 23, line 8 - page 24, line 5 page 36, line 11 - page 37, line 22 ----- -/--	1-15

Further documents are listed in the continuation of Box C.

See patent family annex.

* Special categories of cited documents :

- "A" document defining the general state of the art which is not considered to be of particular relevance
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- "O" document referring to an oral disclosure, use, exhibition or other means
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- "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
- "&" document member of the same patent family

Date of the actual completion of the international search 22 October 2013	Date of mailing of the international search report 30/10/2013
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Name and mailing address of the ISA/ European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Fax: (+31-70) 340-3016	Authorized officer Riehl, Philippe
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INTERNATIONAL SEARCH REPORT

International application No
PCT/EP2013/051027

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	<p>WO 2011/012174 A1 (AREVA T & D UK LTD [GB]; TRAINER DAVID [GB]; OATES COLIN DONALD MURRAY) 3 February 2011 (2011-02-03) cited in the application figure 5 page 6, line 16 - page 7, line 17 page 8, line 3 - line 7 page 8, line 20 - page 9, line 2 page 3, line 3 - line 7</p> <p style="text-align: center;">-----</p>	1
A	<p>EP 2 244 368 A1 (MITSUBISHI ELEC R&D CT EUROPE [NL]; MITSUBISHI ELECTRIC CORP [JP]) 27 October 2010 (2010-10-27) figure 1a</p> <p style="text-align: center;">-----</p>	1-15
A	<p>WO 2012/116738 A1 (ABB RESEARCH LTD [CH]; BERGGREN BERTIL [SE]; NORRGA STEFAN [SE]; JONSS) 7 September 2012 (2012-09-07) figures 2-3 page 22, line 29 - page 23, line 7</p> <p style="text-align: center;">-----</p>	1-15

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No PCT/EP2013/051027

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