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(54) **Crash resistant aluminium alloy sheet products and method of making same**

(57) Aluminum sheet products having high strengths and favorable crashworthiness are disclosed. The aluminum alloys include Si, Mg and Mn in controlled amounts which provide high yield strengths while retaining formability and crash resistant properties. The sheet

products undergo heat treatment and slow quenching. The sheet products are particularly suitable for use as auto body sheet products.

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Description

Cross-Reference to Related Application

[0001] This application claims priority to Provisional Application Serial No. 60/436,123, filed December 23, 2002.

Field of the Invention

[0002] The present invention relates to aluminum alloys, and more particularly relates to aluminum sheet products in which alloy compositions and processing methods are controlled in order to produce improved crash resistance properties.

Background of the Invention

[0003] The use of aluminum sheet in automotive applications has generally been limited to Aluminum Association 6xxx alloys (Al-Mg-Si) for outer panels and 5xxx alloys (Al-Mg) for inner panels and structural members. In order to maximize the weight savings potential of aluminum, it is desirable to replace relatively low strength 5xxx alloys in the structure with higher strength 6xxx alloys. However, a shortcoming of existing 6xxx auto body sheet (ABS) alloys is their ability to absorb energy during crash situations. This is generally termed crashworthiness.

[0004] Autobody sheet requires a combination of good forming properties along with good strength after paint baking operations. The forming properties require good stretch forming and good bending. This traditionally has been achieved with rapid water quenching from solution heat treat temperatures. However, rapid water quenching often results in distortion, surface irregularities and water staining that are unacceptable for outer auto body applications. Air quenching offers many advantages over water quenching with respect to eliminating quench distortion problems, but air quenching can lead to poor bending performance.

[0005] The present invention has been developed in view of the foregoing and to address other deficiencies of the prior art.

Summary of the Invention

[0006] The present invention controls alloy compositions and quench rates to produce aluminum alloy sheet products exhibiting good as-processed formability and shape, and good crashworthiness and strength in the artificially aged condition.

[0007] An aspect of the invention is to provide a 6xxx alloy with a desired combination of strength and crashworthiness.

[0008] Another aspect of the present invention is to provide a heat treated and slow quenched aluminum alloy sheet comprising from about 0.5 to about 0.7 wt. % Si, from about 0.5 to about 0.7 wt. % Mg, from about 0.1 to about 0.3 wt. % Mn, and the balance Al and incidental impurities.

[0009] A further aspect of the present invention is to provide a method of treating an aluminum alloy sheet, the method comprising providing a heat treated aluminum alloy sheet comprising Si, Mg, Mn, and the balance aluminum and incidental impurities, and slow quenching the heat treated aluminum sheet at a rate of less than about 200°F/second.

[0010] These and other aspects of the present invention will be more apparent from the following description.

Brief Description of the Drawings

[0011] Fig. 1 is a schematic diagram illustrating an aluminum sheet heat treating and slow quenching process in accordance with an embodiment of the present invention.

[0012] Fig. 2 is a graph of temperature versus time for a paint bake treatment.

[0013] Fig. 3 is a graph of yield strength versus line speed of a continuous heat treat furnace, illustrating strength properties for two different 6xxx alloys without a slow quench and with a slow quench in accordance with embodiments of the present invention.

[0014] Figs. 4a and 4b are graphs of tensile properties versus paint bake time at 185°C for two different alloys.

[0015] Figs. 5a-5c are computer generated illustrations taken from different views of a sample crash box made of alloy 6060 sheet without a slow quench.

[0016] Figs. 6a-6c are computer generated illustrations taken from different views of a sample crash box made of alloy 6xxx sheet with a slow quench.

[0017] Figs. 7a-7c are computer generated illustrations taken from different views of a sample crash box made of

alloy 6060 sheet with a slow quench.

[0018] Figs. 8a-8c are computer generated illustrations taken from different views of a sample crash box made of alloy 6xxxA sheet without a slow quench.

Detailed Description of Preferred Embodiments

[0019] The present invention provides aluminum alloy sheet products having favorable crash resistant properties. As used herein, the term "sheet" refers to aluminum alloy products having thicknesses from 0.2 to 6.3 mm. For auto body sheet products, thicknesses of from 0.7 to 3.5 mm are preferred. The aluminum alloy sheet products exhibit favorable crash resistance or crashworthiness properties. For the purpose of this invention, crashworthiness is defined as the ability of a material to absorb energy by plastic deformation without appreciable cracking. The crashworthiness of the sheet products can be quantified by critical fracture strain (CFS).

[0020] A preferred process path includes the following steps: casting of an aluminum alloy ingot by conventional or continuous methods; hot rolling; intermediate annealing; cold rolling; solution heat treating; and slow quenching, e.g., air quench or minimum distortion water quench. The steps of solution heat treating and slow quenching preferably occur on a continuous heat treater or temper line. After slow quenching, the sheet may optionally be reheated and coil cooled. The optional cooling step may be performed as an off-line batch process. The steps of solution heat treating and slow quenching, in addition to an optional reheating step, are schematically illustrated in Fig. 1.

[0021] In the solution heat treatment step, the aluminum alloy sheet may be run through a continuous heat treater to substantially dissolve soluble phases formed during upstream processing. This process typically involves furnace temperatures of 800 to 1,100°F at speeds from 20 to 150 feet per minute. The temperature and dwell time in the furnace may be adjusted based upon alloy composition and gauge.

[0022] In the slow quenching step, upon exit from the furnace zone of the continuous heat treater, the sheet is quenched at a controlled rate to retain the solute in solid solution. This can be accomplished, for example, with air or minimum distortion water. An aspect of this invention is the use of relatively slow quench rates that minimize sheet distortion while still developing favorable physical properties. As used herein, the term "slow quench" means quenching at a rate of less than about 200°F/second, preferably less than about 100°F/second. Quench rates for air type processes preferably range from about 20 to about 100°F/second, more preferably from about 40 to about 70°F/second. Water quench rates preferably range from 50 to 1,000°F/sec, more preferably from 100 to 200°F/second.

[0023] In the optional reheating step, a heating unit may follow the quench unit and any coil handling equipment, preferably just ahead of the coiling equipment on the exit end of the line. The heating unit raises the temperature of the sheet such that an elevated coiling temperature can be achieved. A preferred range of coiling temperatures is from about 130 to about 190°F. In the coil cooling step, the warm coil is allowed to cool slowly, typically as a 5,000 to 50,000 lb. mass of metal. This typically results in cooling rates of from about 0.1 to about 5°F/hour.

[0024] In accordance with an embodiment of the present invention, the composition of the aluminum alloy sheet is controlled in order to provide favorable crash resistance properties. The Si and Mg levels are controlled in order to provide high strengths. The Mn level is sufficient to control the grain size of the sheet, particularly during heat treating. Suitable alloys include 6xxx alloys such as 6009, 6060, 6063 and 6005. Typical, preferred and more preferred alloy composition ranges are listed in Table 1.

Table 1

Alloy Compositions (Wt.%)						
	Si	Mg	Mn	Fe	Cu	Al
Typical	0.5-0.7	0.5-0.7	0.1-0.3	0.35 max	0.20 max	balance
Preferred	0.56-0.68	0.54-0.66	0.12-0.18	0.15-0.30	0.10 max	balance
More Preferred	0.58-0.66	0.56-0.64	0.12-0.18	0.15-0.25	0.10 max	balance

[0025] A particularly preferred Al-Mg-Si-Mn alloy is listed in Table 2. Table 2 lists the preferred 6xxxA alloy compositions and a 6060 alloy composition in wt.percentages, with the balance comprising aluminum and incidental impurities.

Table 2

Aluminum Alloy Sheet Compositions						
Alloy		Si %	Fe %	Cu %	Mn %	Mg %
6xxxA	target	0.62	0.20	-	0.15	0.60
	min.	0.58	0.15	-	0.12	0.56
	max.	0.66	0.25	0.10	0.18	0.64
6060	target	0.56	0.20	0.075	-	0.55
	min.	0.53	0.15	0.05	-	0.52
	max.	0.58	0.25	0.10	0.10	0.57

[0026] An advantage of the present invention is the improvement in the crashworthiness of the aluminum alloy sheet product, which may be measured by critical fracture strain (CFS) and axial crush tests. Using the typical engineering stress-strain output from a standard tension test, a critical fracture strain can be determined:

$$\text{CFS} = -\ln(\epsilon_{t,\text{eng}})$$

in which $\epsilon_{t,\text{eng}}$ represents the total engineering thinning strain. The total engineering thinning strain is a function of e_m , Φ_m and Φ_f :

$$\epsilon_{t,\text{eng}} = f(e_m, \Phi_m, \Phi_f)$$

where e_m is the engineering strain at the maximum load; Φ_m is the engineering stress at the maximum load; and Φ_f is the engineering stress at the fracture load.

[0027] The following engineering assumptions are made in the development of the CFS: strains in the thickness and width directions are the same before the maximum load (P_{max}); the true stress after P_{max} is a constant; and the width strain is constant after P_{max} . The total thinning strain at fracture may therefore be determined. In accordance with the present invention, a minimum CFS crashworthiness value of about 15 is preferred, with a value of at least 18 being more preferred.

[0028] A typical property comparison for alloys is shown in Table 3.

Table 3

Alloy	Yield Strength	Crush Results	CFS
5083	145 MPa	Good with some cracking on tight folds	18
6060	216 MPa	Good with some cracking at geometric constraints	21
6xxxA	244 MPa	Good with some cracking at tight folds	18

[0029] Twelve lots of materials 2.0 mm thick were fabricated. Details of the fabrication are given in Table 4. Prior to hot rolling, each of the cast samples was scalped and preheated at 590°C for 8 hours followed by 560°C for 9 hours. The main variables were alloy composition, use of a slow spray quench at an approximate cooling rate of 150°F/second following hot rolling, and the line speed of the continuous heat treat furnace (CHT). The compositions of the two 6xxxA and 6060 alloys studied are shown above in Table 2.

Table 4

STEP	Coil 1 6xxxA	Coil 2 6xxxA	Coil 3 6060	Coil 4 6060
Hot Rolling	1080 x 10 mm	1080 x 8 mm	1080 x 10 mm	1080 x 8 mm
Hot Rolling exit t. °C	>450°C	>450°C	>450°C	>450°C

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Table 4 (continued)

STEP	Coil 1 6xxA	Coil 2 6xxA	Coil 3 6060	Coil 4 6060
Slow Quench after hot rolling	YES	NO	YES	NO
SHT Cont. Furnace	550-570-570 °C spray bar	550-570-570 °C spray bar	550-570-570 °C spray bar	550-570-570 °C spray bar
Speed 1	7 mt/min	5 mt/min	7 mt/min	5 mt/min
Speed 2	11 mt/min	8 mt/min	11 mt/min	8 mt/min
Speed 3	15 mt/min	12 mt/min	15 mt/min	12 mt/min

[0030] The sheet was evaluated in the as received T4 temper and also after a simulative paint bake treatment at 180°C (365°F). Fig. 2 is a temperature-time plot of a thermocoupled sheet sample during the paint bake treatment.

Table 5

Tensile Properties for Sheet Products in T4 Temper									
Alloy	Slow Quench	Speed	Test	Rm	ASTM Test Rp0.2	A	Uniform A	r	n
Coil		(m/min)	direction	(MPa)	(MPa)	(%)	(%)		
6060	No	12	L	164	95	29	24	0.43	0.225
			X	155	94	22	21	0.518	0.221
			T	152	88	30	25	0.749	0.215
		8	L	184	108	28	23	0.634	0.23
			X	182	106	23	22	0.634	0.222
			T	178	104	25	19	0.749	0.227
		5	L	192	116	26	21	0.749	0.223
			X	189	115	27	19	0.518	0.216
			T	191	116	26	21	0.685	0.22
6060	Yes	15	L	183	113	28	25	0.595	0.216
			X	187	110	25	21	0.518	0.24
			T	185	108	25	20	0.749	0.232
		11	L	180	111	30	24	0.411	0.219
			X	183	109	27	22	0.277	0.216
			T	183	112	27	22	0.214	0.216
		7	L	187	115	27	21	0.427	0.223
			X	186	113	26	21	0.346	0.223
			T	188	112	26	20	0.267	0.224
6xxA	No	12	L	163	94	28	24	0.629	0.231
			X	167	90	23	21	0.634	0.243
			T	159	91	25	20	0.629	0.222
		8	L	196	109	28	22	0.629	0.246
			X	192	109	25	21	0.518	0.24
			T	189	105	25	21	0.629	0.247

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Table 5 (continued)

Tensile Properties for Sheet Products in T4 Temper									
Alloy	Slow Quench	Speed	Test	Rm	ASTM Test Rp0.2	A	Uniform A	r	n
Coil		(m/min)	direction	(MPa)	(MPa)	(%)	(%)		
		5	L	209	116	27	22	0.634	0.246
			X	204	119	24	20	0.518	0.238
			T	200	113	25	18	0.629	0.233
6xxA	Yes	15	L	196	118	28	20	0.518	0.228
			X	194	118	28	21	0.343	0.224
			T	188	114	25	21	0.429	0.215
		11	L	210	128	28	22	0.477	0.229
			X	209	129	26	22	0.477	0.225
			T	203	125	23	18	0.524	0.218
		7	L	208	125	26	21	0.682	0.232
			X	209	124	26	21	0.687	0.234
			T	207	124	24	20	0.525	0.233

[0031] The tensile properties of the sheet in the T4 temper are presented in Table 5. There was a slight tendency for the T4 yield strength to decrease with increasing CHT line speed, which is probably indicative of incomplete dissolution of Mg₂Si at the faster line speed. Minor variations in other T4 properties were found.

[0032] Guided bend tests using T4 sheet pre-strained 10% show that the slow quench is beneficial to bending of both alloys. Both alloys fabricated using the slow quench withstood the maximum sharp bend. Downflange and hemming tests illustrate that both alloys are flat hem capable.

[0033] The sheet r&n tensile properties after the paint bake were measured using 2 inch gage length specimens. Table 6 lists the r&n tensile data.

Table 6

Tensile Properties for Sheet Products after Paint Bake									
Alloy	Slow Quench	CHT LineSpeed meters/ min	r&n test data (L - direction after PB)						
			YS (MPa)	UTS (MPa)	YS/UTS	Uniform Elong. (%)	Total Elong. (%)	r (avg)	n
6060	No	5 avg	237	247	0.96	10.3	15.2	1.0064	0.0850
			239	249		10.4	16.1	0.9614	0.0845
			238	248		10.4	15.7	0.9839	0.0848
6060	No	8 avg	230	238	0.97	10.1	15.5	0.9403	0.0906
			230	239		11.0	15.4	0.9982	0.0910
			230	238		10.6	15.5	0.9693	0.0908
6060	No	12 avg	197	206	0.95	9.3	15.3	0.9267	0.0958
			192	201		9.7	15.0	0.9657	0.0976
			194	204		9.5	15.2	0.9462	0.0967

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Table 6 (continued)

Tensile Properties for Sheet Products after Paint Bake									
Alloy	Slow Quench	CHT LineSpeed meters/min	r&n test data (L - direction after PB)						
			YS (MPa)	UTS (MPa)	YS/UTS	Uniform Elong. (%)	Total Elong. (%)	r (avg)	n
6xxA	Yes	7 avg	236	243	0.97	10.2	17.1	0.7234	0.0897
			235	243		10.9	16.2	0.7301	0.0912
			236	243		10.6	16.7	0.7268	0.0905
6xxA	Yes	11 avg	237	245	0.97	10.3	17.0	0.7626	0.0919
			237	244		10.7	18.0	0.7448	0.0913
			237	244		10.5	17.5	0.7537	0.0916
6xxA	Yes	15 avg	228	235	0.97	10.1	15.6	0.8057	0.0917
			228	234		10.5	16.4	0.8491	0.0923
			228	234		10.3	16.0	0.8274	0.0920
6060	Yes	7 avg	237	245	0.96	10.0	16.4	0.7026	0.0831
			237	246		9.9	14.7	0.7120	0.0830
			237	246		10.0	15.6	0.7073	0.0831
6060	Yes	11 avg	239	247	0.97	10.4	15.6	0.6590	0.0822
			236	245		10.3	16.9	0.6609	0.0839
			238	246		10.4	16.3	0.6600	0.0831
6060	Yes	15 avg	236	245	0.97	10.0	15.2	0.6953	0.0804
			237	245		10.1	16.5	0.6594	0.0815
			237	245		10.1	15.9	0.6774	0.0810
6xxA	No	5 avg	249	257	0.97	9.8	14.8	1.0046	0.0832
			248	256		9.9	16.4	0.9965	0.0831
			249	256		9.9	15.6	1.0006	0.0832
6xxA	No	8 avg	232	241	0.97	10.3	16.3	1.0856	0.0904
			231	239		10.3	16.0	1.0917	0.0896
			232	240		10.3	16.2	1.0887	0.0900
6xxA	No	12 avg	165	176	0.94	10.1	16.4	1.0024	0.1137
			172	18		10.3	16.1	0.9479	0.1060
			169	2179		10.2	16.3	0.9752	0.1099

[0034] Fig. 3 plots yield strength of the alloys as a function of the processing variables. The yield strength has the tendency to decrease at the fastest CHT line speeds due to incomplete dissolution of Mg_2Si . Guinier x-ray data showed the presence of Mg_2Si in the materials processed at the faster line speeds. The influence of line speed on yield strength is most pronounced in the sheet which was processed without using the slow quench.

[0035] Fig. 4a is a graph of R_m , $R_{p0.2}$ and A values versus paint bake time at 185°C for the 6060 sample listed in Table 6 which was subjected to the slow quench and a CHT speed of 11 meters/minute. Fig. 4b is a similar graph for the 6xxA sample which was likewise subjected to the slow quench and CHT speed of 11 meters/minute.

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[0036] Crash boxes were assembled having a rectangular cross section measuring 63 mm by 133 mm. Welds or rivets may be used at approximately 1 inch on center with the first and last weld approximately ½ inch from the end. The number of spot welds or rivets specified were 20 per flange. An adhesive sold under the designation Betamate 1494 by Gurit Essex is a one-component toughened epoxy that is applied warm along the side seams of the crash boxes, followed by riveting. A pneumatic heated cartridge gun is used to dispense the adhesive at approximately 40 to 50°C (104 to 122°F). The metal components to be joined were also heated to approximately the same temperature to assist in application of the adhesive and improve flow and wettability. The adhesive was applied to warm metal on the flanges just prior to spot welding or riveting. Rivets were installed at the same locations specified for welding. End caps are then welded in place. After assembly, the boxes were paint baked. The paint baked boxes were tested in axial crush. The crush loads and energy absorbed at displacements of 100, 150, and 200 mm is given in Table 7.

Table 7

Axial Crush Test Results of Paint Baked Samples								
Sample No.	Alloy	Slow Quench	CHT Line Speed meters/min	Crush (after PB)				
				Max Load	Mean Load	Energy Absorbed @ (J)		
				(kN)	(J/mm)	100 mm	150 mm	200 mm
1	6060	No	8 avg	144.7	55.7	5941	8472	11039
				144.4	56.5	6011	8470	11184
				144.9	52.8	5935	8746	10470
				144.7	55.0	5962	8563	10898
2	6xxA	Yes	11 avg	156.3	54.9	6380	8364	10877
				152.8	58.6	6323	8955	11602
				157.0	53.4	6171	8496	10571
				155.4	55.6	6291	8605	11017
	6xxA	Yes	11 avg	162.2	58.4	5932	9146	11563
				162.2	51.1	5505	8000	10119
				156.9	57.3	6690	9149	11361
				160.4	55.6	6042	8765	11014
3	6060	Yes	11 avg	154.6	50.4	6076	7924	9983
				141.4	53.8	6205	8449	10670
				140.6	51.9	5554	8028	10278
				145.5	52.0	5945	8134	10310
	6060	Yes	11 avg	149.1	56.4	5771	8977	11170
				148.1	55.7	6081	8644	11045
				153.1	52.3	6437	8175	10364
				150.1	54.8	6096	8599	10860
4	6xxA	No	8 avg	140.0	51.3	5752	8257	10156
				147.8	55.6	5724	8469	11020
				143.8	52.8	5992	8461	10455
				143.9	53.2	5823	8396	10544

[0037] Computer generated illustrations of the crushed appearance of the boxes are shown in Figs. 5-8. Figs. 5a-c

are computer generated illustrations from different view of Sample No. 1 listed in Table 7. Figs. 6a-c are computer generated illustrations of Sample No. 2. Figs. 7a-c are computer generated illustrations of Sample No. 3. Figs. 8a-c are computer generated illustrations of Sample No. 4. There were no significant differences among the quantifiable crush parameters for the samples tested.

[0038] The performance of the materials met the goals of a sheet alloy product for use in crash critical applications. The paint baked sheet had yield strengths of about 235 MPa, total elongation of 15% and good static crush performance. The T4 properties indicate acceptable formability.

[0039] Whereas particular embodiments of this invention have been described above for purposes of illustration, it will be evident to those skilled in the art that numerous variations of the details of the present invention may be made without departing from the invention as defined in the appended claims.

Claims

1. A heat treated and slow quenched aluminum alloy sheet comprising from about 0.5 to about 0.7 wt.% Si, from about 0.5 to about 0.7 wt.% Mg, from about 0.1 to about 0.3 wt.% Mn, and the balance Al and incidental impurities.
2. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the Si comprises from about 0.58 to about 0.68 wt.%.
3. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the Si comprises from about 0.60 to about 0.66 wt.%.
4. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the Mg comprises from about 0.56 to about 0.66 wt.%.
5. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the Mg comprises from about 0.58 to about 0.64 wt.%.
6. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the Mn comprises from about 0.12 to about 0.18 wt.%.
7. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the aluminum alloy comprises a maximum of 0.35 wt.% Fe.
8. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the aluminum alloy comprises from about 0.15 to about 0.30 wt.% Fe.
9. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the aluminum alloy comprises from about 0.15 to about 0.25 wt.% Fe.
10. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the aluminum alloy comprises a maximum of 0.20 wt.% Cu.
11. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the aluminum alloy comprises a maximum of 0.10 wt.% Cu.
12. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the Si comprises from about 0.58 to about 0.68 wt.%, the Mg comprises from about 0.56 to about 0.66 wt.%, and the Mn comprises from about 0.12 to about 0.18 wt.%.
13. The heat treated and slow quenched aluminum alloy sheet of claim 12 wherein the aluminum alloy comprises from about 0.15 to about 0.30 wt.% Fe, and a maximum of 0.10 wt.% Cu.
14. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the Si comprises from about 0.60 to about 0.66 wt.%, the Mg comprises from about 0.58 to about 0.64 wt.%, and the Mn comprises from about 0.12 to about 0.18 wt.%.

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15. The heat treated and slow quenched aluminum alloy sheet of claim 14 wherein the aluminum alloy comprises from about 0.15 to about 0.25 wt.% Fe, and a maximum of 0.10 wt.% Cu.
- 5 16. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the Si comprises about 0.62 wt.%, the Mg comprises 0.60 wt.%, and the Mn comprises about 0.15 wt.%.
17. The heat treated and slow quenched aluminum alloy sheet of claim 16 wherein the aluminum alloy comprises about 0.20 wt.% Fe.
- 10 18. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has a critical fracture strain of at least 15.
19. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has a critical fracture strain of at least 18.
- 15 20. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has a yield strength of at least 220 MPa.
21. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has a yield strength of at least 230 MPa.
- 20 22. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has a yield strength of at least 240 MPa.
- 25 23. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has a critical fracture strain of at least 15, and a yield strength of at least 220 MPa.
24. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has a critical fracture strain of at least 15, and a yield strength of at least 230 MPa.
- 30 25. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has a critical fracture strain of at least 15, and a yield strength of at least 240 MPa.
26. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has a critical fracture strain of at least 18, and a yield strength of at least 220 MPa.
- 35 27. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has a critical fracture strain of at least 18, and a yield strength of at least 230 MPa.
- 40 28. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has a critical fracture strain of at least 18, and a yield strength of at least 240 MPa.
29. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has a thickness of from about 0.7 to about 3.5 mm.
- 45 30. The heat treated and slow quenched aluminum alloy sheet of claim 29 wherein the sheet comprises an auto body sheet.
31. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has been slow quenched at a rate of less than 200°F/second.
- 50 32. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has been slow quenched at a rate of from about 20 to about 100°F/second.
- 55 33. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has been slow quenched at a rate of from about 40 to about 70°F/second.
34. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has been slow quenched

at a rate of about 150°F/second.

35. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has been air quenched.

36. The heat treated and slow quenched aluminum alloy sheet of claim 1 wherein the sheet has further been coil cooled.

37. The heat treated and slow quenched aluminum alloy sheet of claim 36 wherein the sheet has been coil cooled at a cooling rate of from about 0.1 to about 5°F/hour.

38. The heat treated and slow quenched aluminum alloy sheet of claim 36 wherein the sheet has been coil cooled from an initial coiling temperature of from about 130 to about 190°F.

39. A method of treating an aluminum alloy sheet, the method comprising:

providing a heat treated aluminum alloy sheet comprising Si, Mg, Mn, and the balance aluminum and incidental impurities; and
slow quenching the heat treated aluminum sheet.

40. The method of claim 39 wherein the sheet is slow quenched at a rate of less than 200°F/second.

41. The method of claim 39 wherein the sheet is slow quenched at a rate of from about 20 to about 100°F/second.

42. The method of claim 39 wherein the sheet is slow quenched at a rate of from about 40 to about 70°F/second.

43. The method of claim 39 wherein the sheet is air quenched.

44. The method of claim 39 wherein the sheet is coil cooled.

45. The method of claim 44 wherein the sheet is coil cooled at a cooling rate of from about 0.1 to about 5°F/hour.

46. The method of claim 44 wherein the sheet is coil cooled from an initial coiling temperature of from about 130 to about 190°F.

47. The method of claim 39 wherein the aluminum alloy comprises from about 0.5 to about 0.7 wt.% Si, from about 0.5 to about 0.7 wt.% Mg, from about 0.1 to about 0.3 wt.% Mn, and the balance Al and incidental impurities.

48. The method of claim 47 wherein the Si comprises from about 0.58 to about 0.68 wt.%, the Mg comprises from about 0.56 to about 0.66 wt.%, and the Mn comprises from about 0.12 to about 0.18 wt.%.

49. The method of claim 48 wherein the aluminum alloy comprises from about 0.15 to about 0.30 wt.% Fe, and a maximum of 0.10 wt.% Cu.

50. The method of claim 47 wherein the Si comprises from about 0.60 to about 0.66 wt.%, the Mg comprises from about 0.58 to about 0.64 wt.%, and the Mn comprises from about 0.12 to about 0.18 wt.%.

51. The method of claim 50 wherein the aluminum alloy comprises from about 0.15 to about 0.25 wt.% Fe, and a maximum of 0.10 wt.% Cu.

52. The method of claim 47 wherein the Si comprises about 0.62 wt.%, the Mg comprises 0.60 wt.%, and the Mn comprises about 0.15 wt.%.

53. The method of claim 39 wherein the sheet has a critical fracture strain of at least 15, and a yield strength of at least 220 MPa.

54. The method of claim 39 wherein the sheet has a critical fracture strain of at least 15, and a yield strength of at least 230 MPa.

55. The method of claim 39 wherein the sheet has a critical fracture strain of at least 15, and a yield strength of at

least 240 MPa.

56. The method of claim 39 wherein the sheet has a critical fracture strain of at least 18, and a yield strength of at least 220 MPa.

5 57. The method of claim 39 wherein the sheet has a critical fracture strain of at least 18, and a yield strength of at least 230 MPa.

10 58. The method of claim 39 wherein the sheet has a critical fracture strain of at least 18, and a yield strength of at least 240 MPa.

59. The method of claim 39 wherein the sheet has a thickness of from about 0.7 to about 3.5 mm.

15 60. The method of claim 59 wherein the sheet comprises an auto body sheet.

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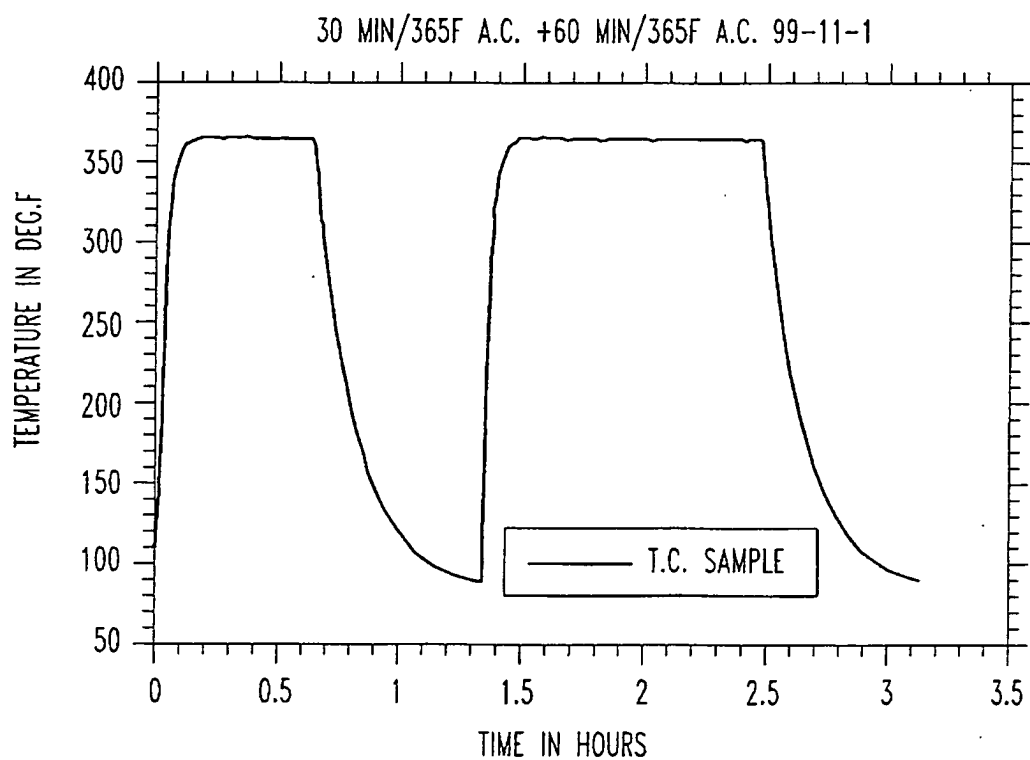
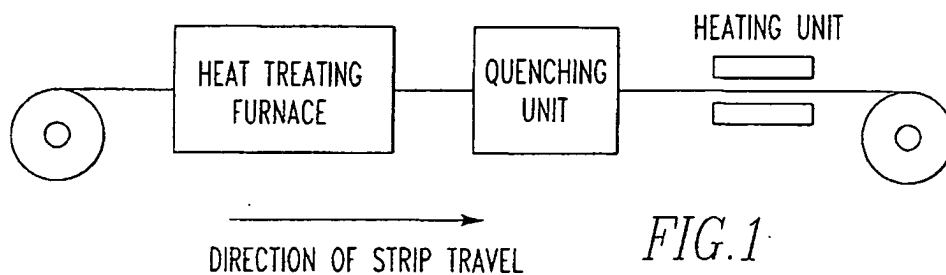
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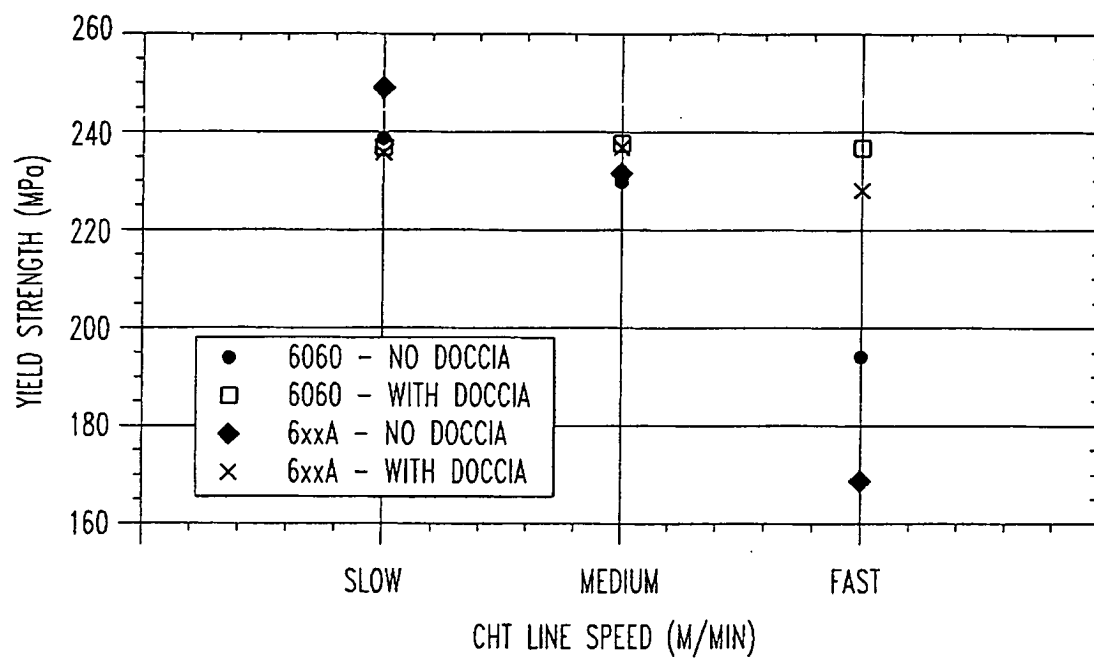
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*FIG.3*

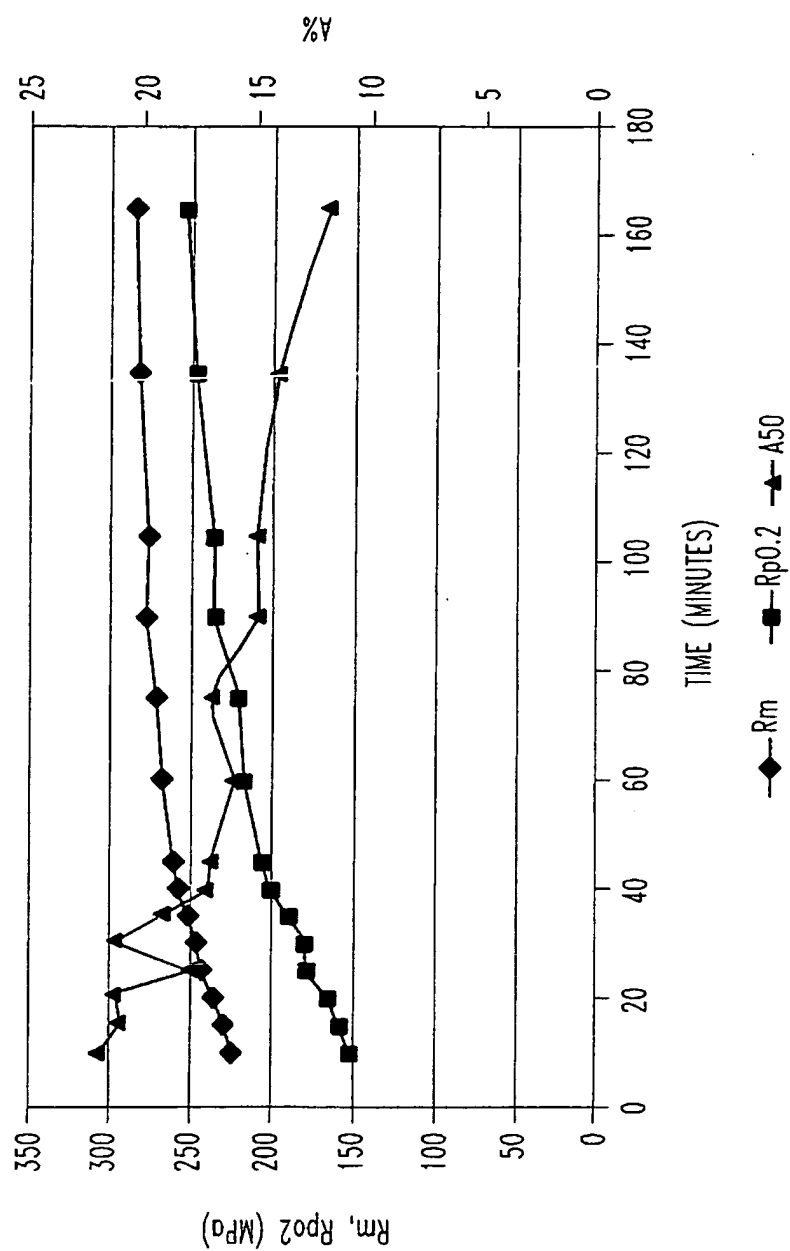


FIG. 4(a)

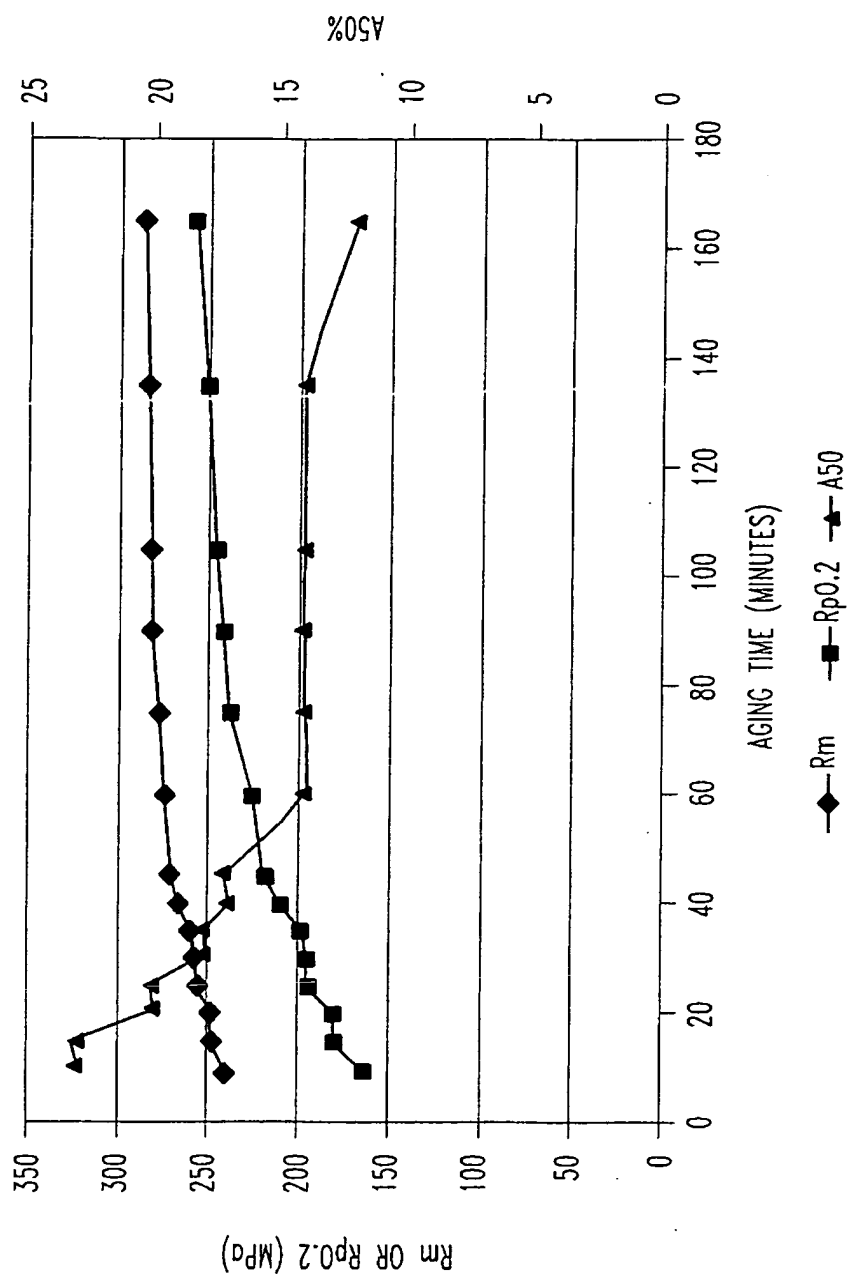


FIG. 4(b)

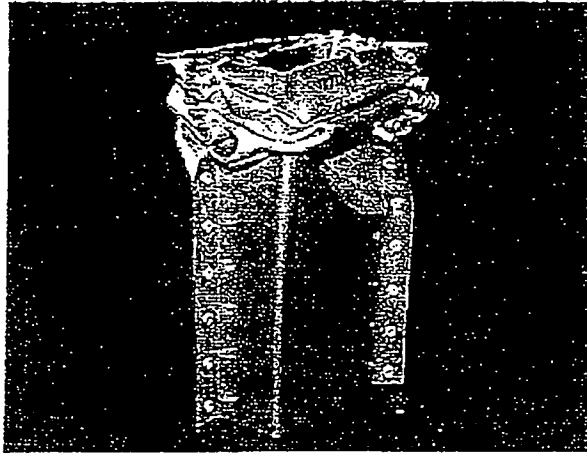


Fig. 5b

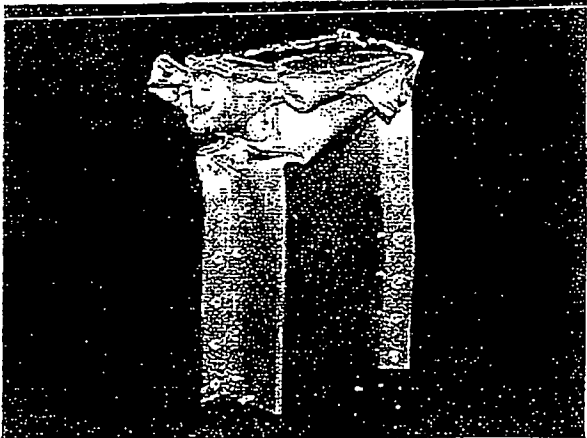


Fig. 5b

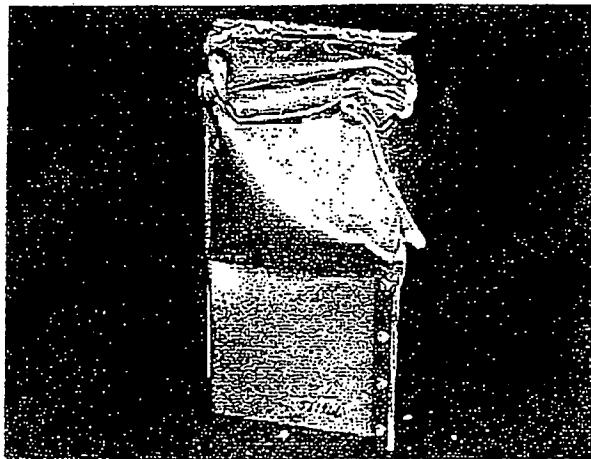


Fig. 5c

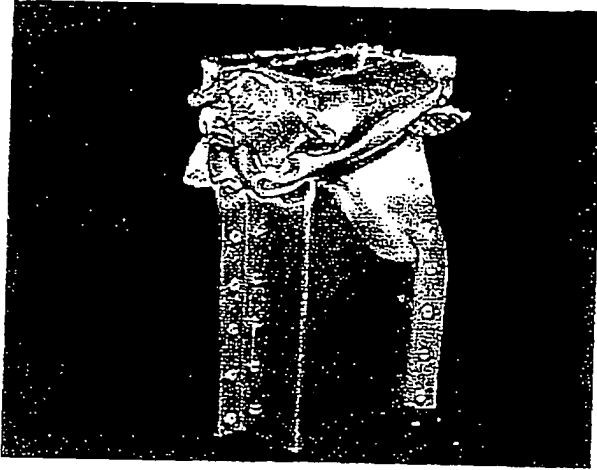


Fig. 6a

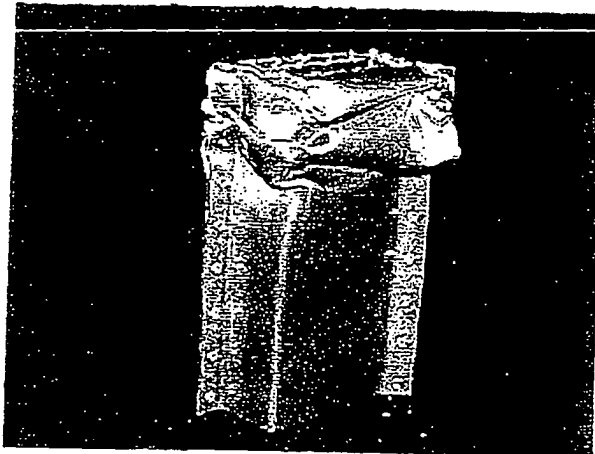


Fig. 6b

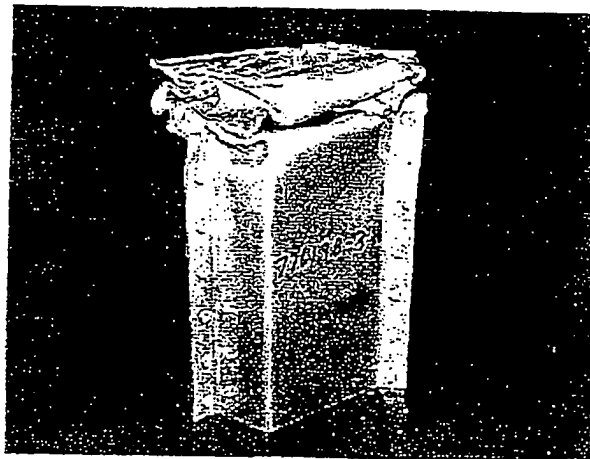


Fig. 6c

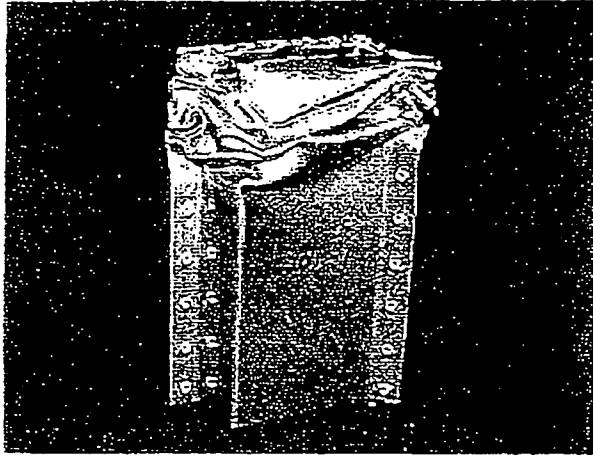


Fig. 7a

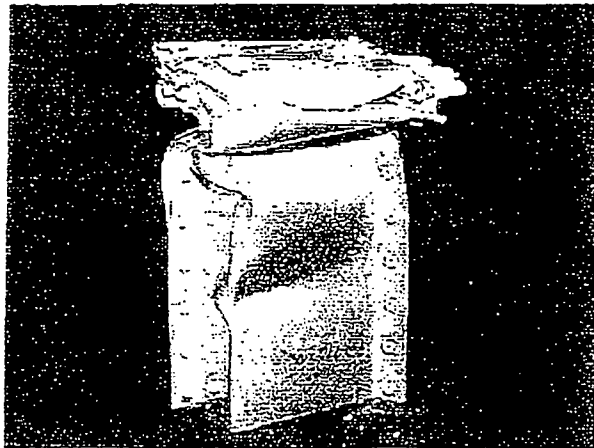


Fig. 7b

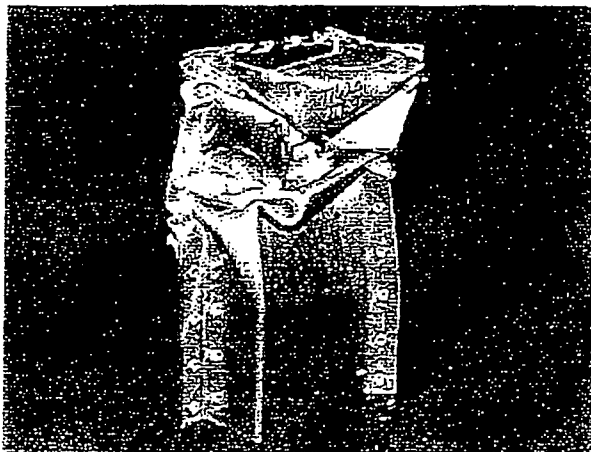


Fig. 7c

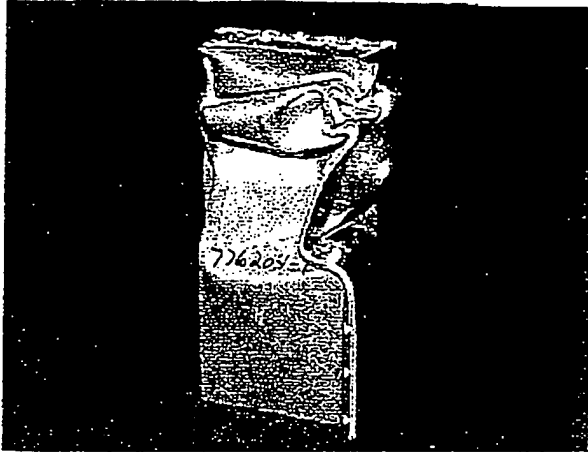


Fig. 8a

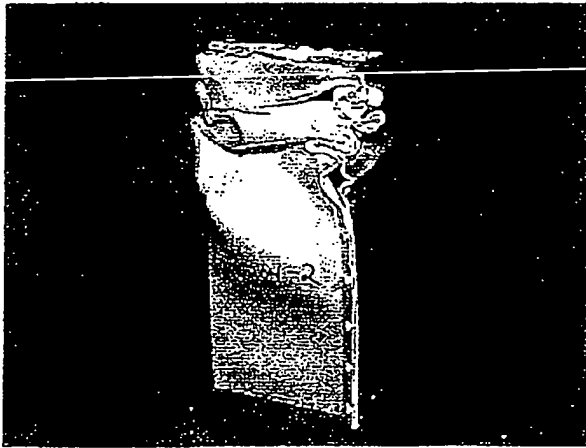


Fig. 8b

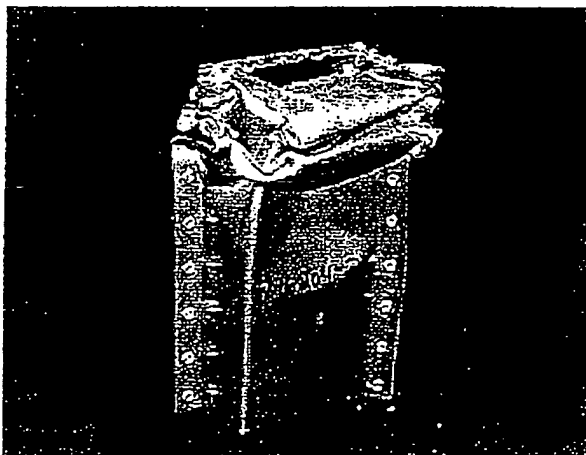


Fig. 8c