



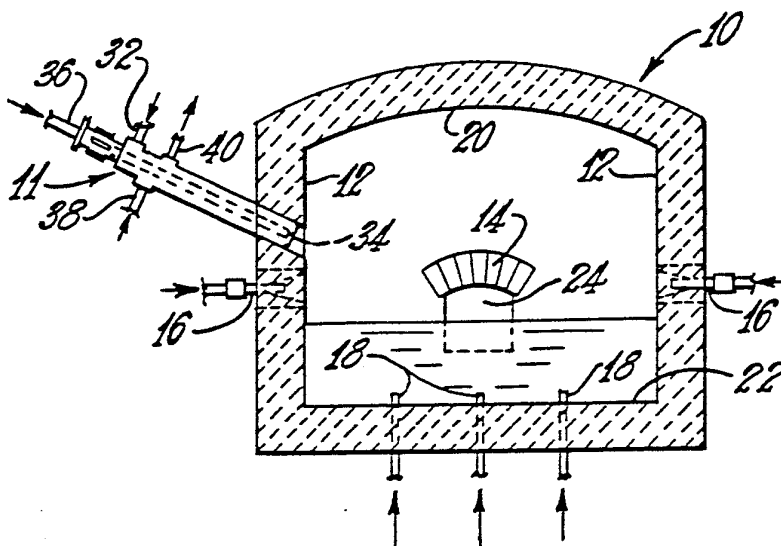
INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification ³ : C03B 5/225, 5/235	A1	(11) International Publication Number: WO 82/ 04246 (43) International Publication Date: 9 December 1982 (09.12.82)
(21) International Application Number: PCT/US81/01464 (22) International Filing Date: 29 October 1981 (29.10.81) (31) Priority Application Number: 269,226 (32) Priority Date: 1 June 1981 (01.06.81) (33) Priority Country: US (71) Applicant: OWENS-CORNING FIBERGLAS CORPORATION [US/US]; Law Department - 26, Fiberglass Tower, Toledo, OH 43659 (US). (72) Inventors: ERICKSON, Thomas, David ; 649 Canterbury Court, Newark, OH 43055 (US). MINNEN, Pol, Alexandre ; Rue Florikosse, Number 42, B-Verviers (BE). (74) Agents: PACELLA, Patrick, P. et al.; Law Department - 26, Fiberglass Tower, Toledo, OH 43659 (US).		(81) Designated States: AU, DE, FI, GB, JP, NL, NO, SE. Published <i>With international search report.</i> <i>With amended claims.</i>

(54) Title: PROCESS FOR PRODUCING MOLTEN GLASS

(57) Abstract

Method and apparatus for producing heat-softenable mineral into materials such as glass. The process and apparatus carry on processing of mineral material from a batch stage through melting in a furnace (10), delivering streams of the material and attenuating them to filaments and packaging the filaments. By impinging the surface of molten glass with a flame of high energy heat from a burner (11), production is substantially increased and the amount of energy employed per ton of molten glass is reduced.



FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	GA	Gabon	MR	Mauritania
AU	Australia	GB	United Kingdom	MW	Malawi
BB	Barbados	HU	Hungary	NL	Netherlands
BE	Belgium	IT	Italy	NO	Norway
BG	Bulgaria	JP	Japan	RO	Romania
BR	Brazil	KP	Democratic People's Republic of Korea	SD	Sudan
CF	Central African Republic	KR	Republic of Korea	SE	Sweden
CG	Congo	LI	Liechtenstein	SN	Senegal
CH	Switzerland	LK	Sri Lanka	SU	Soviet Union
CM	Cameroon	LU	Luxembourg	TD	Chad
DE	Germany; Federal Republic of	MC	Monaco	TG	Togo
DK	Denmark	MG	Madagascar	US	United States of America
FI	Finland	ML	Mali		
FR	France				

-1-

1

5

D E S C R I P T I O N

10

PROCESS FOR PRODUCING MOLTEN GLASS

TECHNICAL FIELD

This invention relates to the melting of inorganic materials to produce molten glass.

15

BACKGROUND ART

Conventional glass furnaces include a melting zone into which the raw batch material is charged. Air fuel burner flames are projected into the melting zone to melt the raw material which then flows through a throat in the front wall. Conventionally, glass melting furnaces burn either natural gas or oil.

U.S. Patent 3,856,496, issued December 24, 1974, discloses one modification to the conventional glass melting furnace. Pairs of adjacent burners are mounted in the rear wall of the furnace for melting raw batch material. The angle between the adjacent burners of each pair can be adjusted to increase mixing of fuel and air to ensure complete combustion. The burners also may be adjusted to maximize the area of raw batch covered by the burner flames. The burners produce a flame and create a circulation of hot effluent gases in the interior of the glass tank in a clockwise or counter clockwise pattern.

30

DISCLOSURE OF INVENTION

We have discovered that by providing a flame of high energy heat and impinging it directly upon the surface of molten glass, production may be substantially increased and a reduction in the amount of energy employed per ton of

35

BAD ORIGINAL



-2-

1 finished glass may be achieved. This invention is readily
adaptable for use with oxygen-enriched burners. The
burners actually in service use oxygen and natural gas. In
one embodiment the flame is directed at the surface of
5 molten glass open to exposure at the rows of bubbles in the
glass melting furnace. In another embodiment, opposed
oxygen-enriched burners are located in opposite furnace
sidewalls facing each other. The burners are adjusted to
maximize the area of molten glass covered by the burner
10 flames. Creating a localized hot spot on the surface of
the molten glass is believed to be the critical feature of
this process.

The very strong and very localized heat brought
to the surface of the molten glass at a given location
15 increases the temperature of the molten glass to such an
extent that the throughput of the furnace can be increased
with a reduction in the amount of fuel per ton used. This
invention satisfies the time/temperature relationship
required in melting batch. The high temperature burner is
20 preferred because it increases the temperature of the
molten glass without increasing the temperature of the
whole melting tank. Merely increasing the energy in
conventional burners may not be satisfactory as this tends
to make the temperature of the furnaces too high.

25 Also, increasing glass throughput by conventional
methods is not always possible without abnormally
increasing total fuel usage. This is uneconomical and
often harmful to refractory structure. Conventional heat
input would produce so much volume of combustion products
30 that the flames would impinge the refractory and cause its
rapid destruction.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a side view of a glass melting furnace
employed to carry out this invention.

35 FIG. 2 is a rear view of a glass melting furnace
employed to carry out this invention.



-3-

1 FIG. 3 shows a water cooled nozzle which feeds oxygen directly into the fuel jets.

BEST MODE OF CARRYING OUT INVENTION

5 This invention may be used to produce conventional wool glass for insulation and ceiling board and to produce conventional textiles and reinforcements such as those made from E glass.

10 Preferably, this invention relates to a method and apparatus for processing heat-softenable minerals into materials such as glass and, more especially, to a method and apparatus for carrying on processing of mineral or inorganic materials from a batch stage through melting and delivering streams of the material, attenuating the streams to filaments and packaging the filaments. Textile
15 filaments have been produced by attenuating streams of glass from a feeder to filaments by winding the filaments upon a collector or tube in package form.

20 While only a single oxygen-enriched burner or a pair of such burners is employed in the disclosed embodiment, multiple oxygen-enriched burners are well within the scope of this invention.

FIG. 1 is a side view of a glass melting furnace employed to carry out this invention. Furnace 10 is formed of sidewall 12 and another sidewall, rear wall, front wall,
25 roof and bottom structures (not shown). The front wall 14 contains a port or throat which permits the molten glass to leave the furnace. A row of conventional burners 16 is shown. A number of conventional bubblers 18 also is shown. Water cooled, oxygen gas burner 11 also is shown in
30 position.

The chamber of melting furnace 10 is adapted to be fired or heated by fuel gas or other suitable fuel mixed with air which is preheated in the recuperator to a
35 temperature not exceeding that at which the air may be safely mixed with the fuel gas at the regions of delivery of the fuel gas and air into the fuel chamber at lengthwise spaced regions above the level of the glass in the chamber.

BAD ORIGINAL



-4-

1 As shown in FIG. 1, a row or battery of combustion burners
16 mounted in burner blocks is arranged at each side of the
furnace.

Arranged at opposite sides of furnace 10 adjacent
5 the stack or rear end of furnace 10 are batch charging
stations including batch feed openings provided with batch
chargers or batch feeders not shown. Disposed above each
of the batch chargers is a hopper, each hopper being
provided with a control valve for regulating the delivery
10 of raw batch into each charger.

The raw materials usually consist of sand,
limestone, soda ash, and a borate such as colemanite or
ulexite. The batch make-up depends on the type of glass
being made and need not contain all of the above materials.
15 Various other materials may be present in small amounts.
The glass also may be flux free glasses, i.e., glasses that
contain little or no fluxing agents such as boron or
fluorine.

The heat necessary for melting the raw materials
20 and for maintaining the molten batch at a desired
temperature is provided by two rows of conventional burners
16. The burners are designed to burn a suitable liquid
fuel such as oil, or a fuel gas such as natural gas. The
type of fuel used depends on what is available
25 commercially, the economy of the fuel, and its suitability
for glass melting. The burner pairs are positioned in the
sidewall 12 and the opposite sidewall not shown. As
previously discussed, FIG. 1 shows oxygen-enriched burner
11 positioned at the rear row of bubblers 18.

30 FIG. 2 is a rear view of furnace 10 showing one
example of the angle at which burners 11 are extended into
the furnace. In addition, FIG. 2 shows roof 20 and bottom
floor 22. FIG. 2 also shows throat 24 extending through
front wall 14.

35 FIG. 3 shows the detailed features of burner 11.
A burner construction wherein the oxygen is injected
directly into the fuel at the nozzle is shown in FIG. 3.

BAD ORIGINAL



-5-

1 Burner 11 includes a cylindrical pipe 30 having a fuel
inlet 32 which feeds the fuel to the burner. Pipe 30
terminates in a nozzle tip 34 from which the fuel jets are
emitted. Oxygen is fed to tube 30 by means 36 so that the
5 oxygen and fuel are emitted together from the nozzle tip
34. To prevent burner 11 from overheating, water a cooled
jacket is employed. FIG. 3 shows water inlet 38 and water
outlet 40. Burner 11 usually employs bronze rear casting
42 and oxygen quick-disconnect fitting 44.

10 The temperature of the flame may vary widely.
Properly speaking, there is no preferred temperature range
for the flame. The temperature generally depends upon the
quality of the natural gas and the oxygen/gas ratio. In
the following embodiment, the temperature of the oxygen
15 flame is about 2780°C. This figure is substantially higher
than the temperature of a conventional burner with air
which is about 1950°C.

In one embodiment, the temperature of the flame
should be at least 2500°C. The oxygen/gas ratio is
20 adjusted close to stoichiometric, which is a ratio of
1.75:1. Actually, a ratio of 2:1 preferably is chosen for
safety. It is extremely important not to fire a reducing
gas flame as gas cracking occurs immediately.

In the conventional process of the following
25 embodiment, the surface temperature of the molten glass in
the absence of the oxygen flame of this invention usually
is 1560 to 1600°C. Accordingly, the temperature of the
oxygen flame is at least 1000-1100°C higher than the
surface temperature of the molten glass, compared to only a
30 350°C difference with regard to air flames of conventional
burners.

The preferred burners to be employed in this
invention use only natural gas and pure oxygen. That is,
the burners do not employ an air/oxygen mixture with the
fuel. It is within the scope of this invention, however,
35 to employ burners where the use of an air/oxygen mixture
may be possible as long as the temperature of the heat

BAD ORIGINAL



-6-

- 1 source is sufficiently high to (1) increase the throughput
of the furnace and (2) reduce the amount of fuel employed
per ton of glass.

Example

- 5 To demonstrate that this invention achieves
increased pull without increasing total fuel per ton usage,
the following comparison was made. A conventional glass
melting furnace was used as a standard. The fuel usage for
the furnace is 17.2 million BTUs per ton of glass. The
10 furnace had a front wall temperature of 1540°C.

- With this invention, throughput increased about
26% and the gas consumed by the conventional burners and
the oxygen burners equaled 14.4 million BTUs per ton of
glass. Oxygen usage was 70 SCFM (standard cubic feet per
15 minute) and the front wall temperature was 1555°C. The
improvement in fuel usage was a reduction of about 18% of
fuel for the same glass tonnage in the conventional
furnace.

- Exposed molten material can be found in many
20 regions of the melting chamber. Frequently, the floor of
the chamber may be provided with orifices for delivering
jets of gas into and upwardly through the molten material.
Often, the orifices are arranged in rows transversely of
the chamber. In one embodiment, the high intensity heat
25 may be directed at exposed molten material in the region of
the chamber near these orifices. In another embodiment,
the high intensity heat may be directed at exposed molten
material in the region near the row of orifices nearest the
batch charging end of the chamber. Still other areas of
30 exposed molten glass may occur in regions near electrodes
if electric heating is employed to melt the batch. In
still another embodiment the oxygen burners may be
installed at the front end of the melter above front
bubblers.

35 INDUSTRIAL APPLICABILITY

This invention can be used with a method and
apparatus for processing heat-softenable mineral materials

BAD ORIGINAL



-7-

- 1 such as glass and, more especially, to a method and
apparatus for carrying on processing of mineral or
inorganic material from a batch stage through melting,
delivering streams of the material, attenuating the streams
5 to filaments and packaging the filaments.

Textile filaments have been produced by
attenuating streams of glass from a feeder to filaments by
winding the filaments upon a collector or tube in package
form.

- 10 The invention can be used with a method wherein a
series of glass melting and processing facilities or units
are employed, each unit provided with a plurality of
forehearth sections oriented or arranged in aligned rows
and the forehearth sections provided with large numbers of
15 orificed feeders in combination with filament-attenuating
and packaging units individual to each feeder or plurality
of feeders arranged in an enclosure or chamber wherein the
packaging units or devices are disposed in rows along each
side of an aisle to facilitate supervision of the
20 operations by a minimum number of operators.

- The invention uses a melting and conditioning
facility or unit for processing raw batch filament-forming
material and conditioning the same suitable for forming
textile filaments wherein a plurality of forehearths or
25 forehearth sections are supplied with the material from the
unit, the unit being of a size and character to promote a
repeated circulation or recycling of the molten material in
paths by agitation and convection whereby the material is
fined and refined during its circulatory movements in the
30 melting and conditioning unit so that the material is
maintained in the unit for a period of time to assure
substantially complete degasification of the material and
the promotion of homogeneity thereof.

- The invention uses a plurality of melting and
35 furnaces or units wherein each unit is provided with a
plurality of forehearths or forehearth sections each
provided with a plurality of stream feeders or bushings

BAD ORIGINAL



-6-

1 arranged to discharge streams of glass wherein the feeders
are aligned in rectilinear rows and the groups of streams
are processed to strands of filaments by winding machines
disposed in rows beneath the feeders facilitating operation
5 with a minimum number of operators.

The melting units are particularly adaptable for
conditioning glass or other mineral material for forming
textile filaments wherein the amount of glass processed per
unit of time is greatly increased and advantage taken of
10 high melting rates and volume production of filaments to
reduce the cost of textile filaments.

15

20

25

30

35

BAD ORIGINAL



-9-

1

5

C L A I M S

10 1. The method of processing heat-softenable material including feeding batch material into a chamber near one end of the chamber, applying heat to the chamber to melt the batch material, impinging a source of high energy heat upon a portion of the surface of molten
15 material, and flowing molten material through a passage near the other end of the chamber.

2. A method according to claim 1 wherein the source of high energy heat impinges essentially all of the surface of exposed molten glass in the chamber.

20 3. A method according to claim 1 wherein the source of high energy heat impinges a portion of the surface of the molten glass essentially across the width of the chamber transverse to the flow of molten material in the chamber.

25 4. A method according to claim 1, including the steps of agitating the molten material at a region and impinging the source of high energy heat on the surface of the molten material at that region.

30 5. A method according to claim 1 including the step of projecting streams of gas through the molten material at a region and impinging the source of high energy heat on the surface of the molten material at that region.

35 6. A method according to claim 4 wherein the source of high energy heat impinges at the region of agitating nearest the batch feeding end of the chamber.

BAD ORIGINAL



-10-

1 7. A method according to claim 5 wherein the source of high energy heat impinges at the point of projecting streams of gas nearest the batch feeding end of the chamber.

5 8. A method according to claim 1 wherein the source of high energy heat is substantially higher than the temperature of the surface of the molten material.

 9. A method according to claim 1 wherein the source of high energy heat has a temperature at least
10 1000°C higher than the temperature of the surface of the molten material.

 10. A method according to claim 1 wherein the source of high energy heat has a temperature of at least 2500°C.

15 11. A method according to claim 1 wherein the source of high energy heat has a temperature of 2780°C.

 12. Apparatus for processing heat-softenable material including, in combination, a furnace formed with a melting chamber, means for feeding batch material into the
20 chamber near one end of the chamber, a plurality of heating means associated with the chamber for melting the batch material, means for impinging high energy heat upon a portion of the surface of the molten material, a passage near the other end of the chamber, and means for flowing
25 molten material away from the chamber through the passage.

 13. Apparatus according to claim 12 wherein the means for impinging high energy heat is a flame.

 14. Apparatus according to claim 12 wherein the chamber has a pair of sidewalls and wherein the means for
30 impinging high energy heat is a high intensity burner associated with each sidewall of the furnace.

 15. Apparatus according to claim 12 wherein the chamber has a floor which is provided with orifices arranged in rows transversely of the chamber, said orifices
35 being arranged to deliver jets of gas into and upwardly through the body of molten material in the chamber and wherein the means for impinging high energy heat is

BAD ORIGINAL



-11-

1. directed at the area of the chamber provided with the orifices.

16. Apparatus according to claim 15 wherein the means for impinging high energy heat is directed at the area of the chamber near the row of orifices nearest the means for feeding batch material to the chamber.

17. Apparatus according to claim 12 wherein the means for impinging high energy heat is directed at an area of the chamber which extends essentially transversely across the width of the chamber.

18. Apparatus according to claim 12 wherein the means for impinging high energy heat is a burner with a non-reducing flame and a temperature substantially higher than the temperature of the molten material.

19. Apparatus according to claim 18 wherein the flame has a temperature of at least 1000°C higher than the temperature of the surface of the molten material.

20. Apparatus according to claim 18 wherein the flame has a temperature of at least 2500°C.

21. Apparatus according to claim 18 wherein the flame has a temperature of 2780°C.

22. Apparatus according to claim 18 wherein the burner uses only natural gas and oxygen.

23. Apparatus according to claim 22 wherein the oxygen and natural gas have an oxygen/gas ratio close to stoichiometric.

24. Apparatus according to claim 22 wherein the oxygen and natural gas have an oxygen/gas ratio ranging from 1.75:1 to 2:1.



BAD ORIGINAL

1

AMENDED CLAIMS

5

(received by the International Bureau on 29 March 1982 (29.03.82))

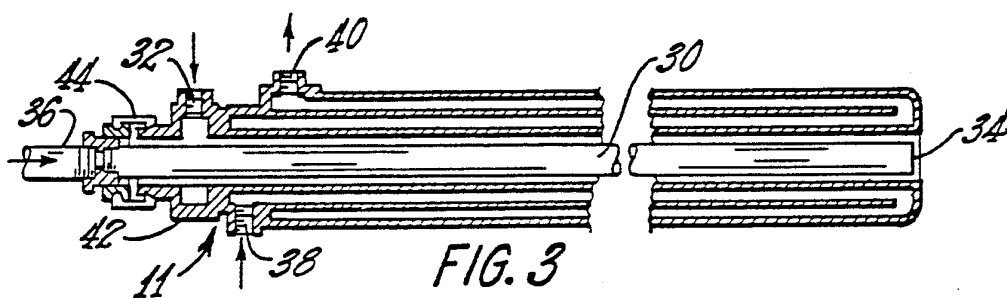
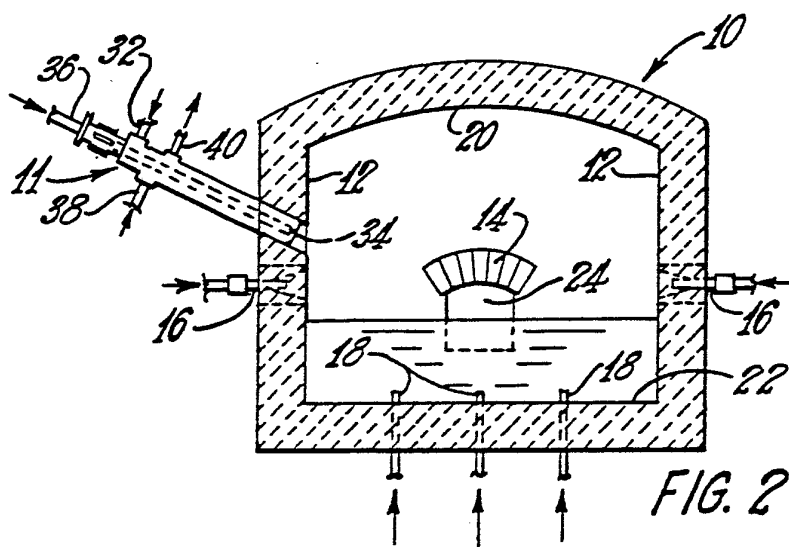
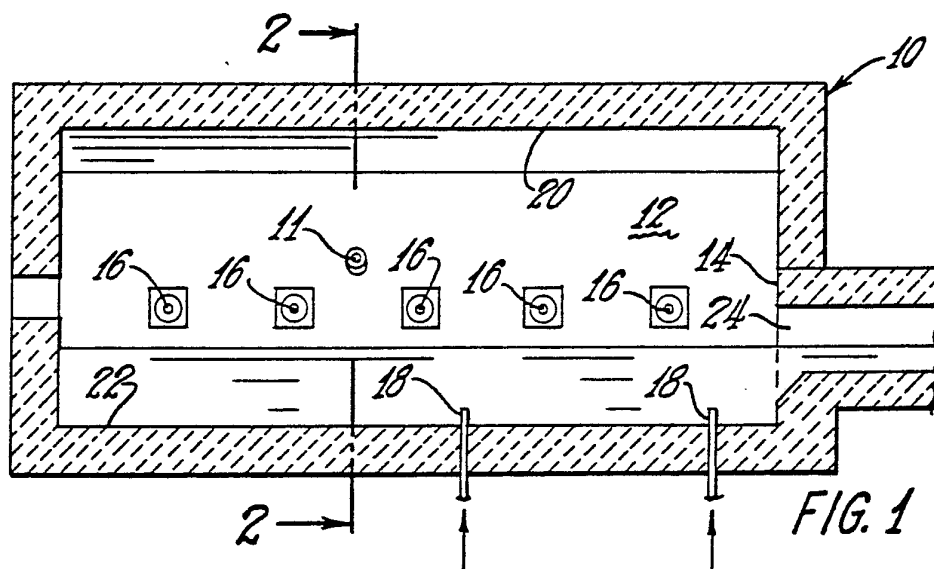
1 to 24 cancelled

25. (New) A method for producing glass
10 including the steps of:
 feeding glass batch into a melting furnace near
 one end of the furnace;
 heating the furnace to melt the glass batch;
 impinging the surface of the molten glass with a
15 flame of high energy heat from at least one oxy-fuel
 burner; and
 withdrawing molten glass near the other end of
 the furnace.
26. (New) A method according to claim 25
20 wherein the flame creates a localized hot spot on the
 surface of the molten glass.
27. (New) A method according to claims 25 or 26
 wherein the flame impinges the surface of the molten glass
 essentially across the width of the furnace transverse to
25 the flow of molten glass in the furnace.

30

35

1 / 1



INTERNATIONAL SEARCH REPORT

International Application No PCT/US81/01464

I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) ³		
According to International Patent Classification (IPC) or to both National Classification and IPC INT. CL. ³ C03B 5/225, C03B 5/235 U.S. CL. 65/136,347		
II. FIELDS SEARCHED		
Minimum Documentation Searched ⁴		
Classification System	Classification Symbols	
U.S.	65/134,135,136,337,346,347; 432/13,19,20,195	
Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched ⁵		
III. DOCUMENTS CONSIDERED TO BE RELEVANT ¹⁴		
Category ⁶	Citation of Document, ¹⁵ with indication, where appropriate, of the relevant passages ¹⁷	Relevant to Claim No. ¹⁸
X	US,A, 3,015,190, PUBLISHED 02 JANUARY 1962, ARBEIT.	-5,12-14,17
A	US,A, 3,337,324,PUBLISHED 22 AUGUST 1967, CABLE, JR., ET AL.	8-11,18-24
A	US,A, 3,592,622, PUBLISHED 13 JULY 1971, SHEPHERD.	8-11,18-24
A	US,A, 3,592,623, PUBLISHED 13 JULY 1971, SHEPHERD.	8-11,18-24
A	US,A, 2,254,079, PUBLISHED 26 AUGUST 1941, McALPINE.	6,7,15,16
A	US,A, 3,856,496, PUBLISHED 24 DECEMBER 1974, NESBITT ET AL.	1-24
A	US,A, 3,249,417, PUBLISHED 03 MAY 1966, VAN ZONNEVELD.	1-24
A	US,A, 3,332,758, PUBLISHED 25 JULY 1967, FIRNHABER.	1-24
A	US,A, 3,523,781, PUBLISHED 11 AUGUST 1970, LEVEQUE.	1-24
<p>* Special categories of cited documents: ¹⁵</p> <div style="display: flex; justify-content: space-between;"> <div style="width: 45%;"> <p>"A" document defining the general state of the art</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document cited for special reason other than those referred to in the other categories</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> </div> <div style="width: 45%;"> <p>"P" document published prior to the international filing date but on or after the priority date claimed</p> <p>"T" later document published on or after the international filing date or priority date and not in conflict with the application, but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance</p> </div> </div>		
IV. CERTIFICATION		
Date of the Actual Completion of the International Search ²	Date of Mailing of this International Search Report ²	
31 DECEMBER 1981	<div style="font-size: 1.5em; font-weight: bold;">03 FEB 1982</div>	
International Searching Authority ¹	Signature of Authorized Officer ²⁰	
ISA/US	RICHARD V. FISHER	