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DESCRIPTION

Cross-reference to related applications

[0001] This Patent Application claims priority from Italian Patent Application No. 102019000012972 filed on July 26, 2019.

Technical field

[0002] The invention provides a system comprising a substrate and an electroless composite coating comprising a layered structure alternating a metallic NiP layer and a composite NiP layer. The invention further pertains to the method of preparation of said system and to its uses.

Background of the invention

[0003] Solid particle erosion is material removal/damage to a solid surface produced by repeated impacts of solid particles. It is to be expected whenever hard particles are entrained in a gas or liquid medium impinging on a solid at any significant velocity. The solid-liquid erosion is known as slurry erosion. Slurry erosion has become a serious problem for the performance, reliability, and service life of slurry equipment used in many industrial applications such as: mining machinery components, hydraulic transport of solids in pipelines, marine, oil gas and power generation industries.

[0004] Electroless Ni-P coatings have been well known as a hard coating for industrial applications, due to their good corrosion and wear resistance properties. They are usually obtained by co-depositing particulate materials, such as ceramics, diamond and fluoropolymers and carbides of silicon, tungsten and chromium. This valuable process can coat not only electrically conductive materials including graphite but also fabrics, insulators like plastics, rubber etc.

[0005] Examples of electroless Ni-composite plated substrates and methods of preparations thereof are found in US 2009/0011136, US 2011/0162751, US2013/0143031, and US2016/0010214.

[0006] US4358923A discloses processes and articles for composite electroless coatings comprising at least two distinct layers, the first layer comprising a metal and/or a metal alloy plus particulate matter and the second layer comprising a metal and/or a metal alloy and being substantially free of particulate matter.

[0007] US2011226144A1 discloses a doctor blade for wiping printing ink off a surface of a printing plate and/or for use as a paper doctor knife; at least the working edge region of the doctor blade is covered with a coating on the basis of a nickel-phosphorus alloy; in some embodiments, the coating comprises a composite layer of NiP, containing particles of different size and nature, and a metallic layer of NiP.

[0008] The major advantages of the electroless Ni-P plating deposition process include the formation of a uniform deposit on irregular surfaces, direct deposition on surface-activated non-conductors, and the formation of non-magnetic, low internal stress deposits. Furthermore, when accompanied by an appropriate post-heat treatment, the wear resistance of the coatings can be improved considerably. The effectiveness of using a composite electroless Ni-P-SiC coating system for cavitation erosion protection of steel has also been observed.

[0009] In the oil and gas field, the main application of the electroless Ni-P coatings is in the increase of wear resistance of parts in choke valves and in the protection of the inner/outer surface of the pipelines.

[0010] Pipelines play an important role throughout the world as a means of transporting gases and liquids over long distances from their source to the supply. According to the environment and to the fluid, abrasion and erosion phenomena can degrade rapidly the wall of the pipeline, losing integrity. Hence, in the oil and gas field, in particular for the coating of the inner surfaces of the pipelines, a very high wear (abrasive/erosive) resistance is required combined with an improved corrosion protection to harsh environment. However, the combination of these two properties is hard to achieve through the traditional and commercially available technology of composite electroless deposition.

[0011] In fact, the existing available processes are mainly intended for applications where wear resistance is needed and the corrosion protection is not a major issue. It is known that composite coatings are not able to offer a very high corrosion protection, typically less than the metal matrix alone.

[0012] Therefore, the need remains to provide an electroless composite with further improved erosion-corrosion resistance.

Summary of the invention

[0013] The present invention relates to a system comprising a substrate and an electroless composite coating in contact with the substrate as claimed by claim 1.

[0014] Preferably the composite NiP layer comprises P in amounts between 1 and 20 wt%, more preferably in an amount between 7 and 15 wt%.

[0015] Ni and P together with any other metallic element, which may be present in the metallic

and/or the composite layer form a so called metallic matrix. The amount of P is defined with respect to the total weight of the metallic matrix.

[0016] Preferably, the particles have average size between 10-5000 nm, more preferably between 50-3000 nm.

[0017] The dispersed particles are a blend comprising first and second particles different in size and nature, preferably the first particles have average size between 100-5000 nm, more preferably between 500-3000 nm and the second particles have average size between 10-2000 nm, more preferably between 50-500 nm.

[0018] Advantageously, the dispersed particles are boron carbide particles and/or silicon carbide nanoparticles.

[0019] Preferably the metallic NiP layer and the composite NiP layer comprise the same amount of P with respect to Ni.

[0020] Preferably the composite NiP layer consists essentially of Ni and P and the dispersed particles or of Ni, P, the dispersed particles and one or more further metallic element.

[0021] Preferably, the metallic NiP layer consists essentially of Ni and P or of Ni, P and one or more further metallic element.

[0022] A layer alternation is defined as any alternation between a metallic and a composite layer or a composite and a metallic layer. Conveniently, the alternation occurs from 2 to 12 times, preferably from 3 to 11 times, more preferably 5, 7 or 9 times. For example, an alternation of metallic/composite/metallic layers or composite/metallic/composite accounts for 2 times (3 layers) or an alternation of composite/metallic/composite/metallic layers for 3 times (4 layers). A coating with more than 12 alternations is still possible however it may become too expensive and time consuming to be produced.

[0023] Preferably, the layered structure consists of 3, 4, 5, 6, 7, 8, 9 or 10 layers, more preferably of 6, 8 or 10, even more preferably of 8 layers.

[0024] According to an embodiment of the invention, the electroless composite coating consists of the layered structure of alternating metallic NiP layers and composite NiP layers.

[0025] Preferably, the layer formed over and in contact with the substrate is a metallic NiP layer and or preferably the outer layer is a composite NiP layer.

[0026] The invention also provides a pipeline as claimed by claim 10, coated with the electroless composite coating as described above. Preferably the pipeline is coated with the electroless composite coating in its inner surface.

[0027] The present invention in addition provides the use of the system of the invention to improve the resistance of a pipeline to chemical and mechanical degradation as claimed by claim 12.

[0028] The present invention further provides a method to produce the system of the invention as claimed by claim 13. Said method comprises the following steps:

1. a) Substrate preparation;
2. b) Deposition of a metallic NiP layer, or of a composite NiP layer on the substrate,
3. c) Deposition of a composite NiP layer on the substrate coated with metallic NiP layer or deposition of a metallic NiP layer on the substrate coated with composite NiP layer; wherein step c) is repeated at least two times (three layers).

[0029] Preferably, the method includes a thermal treatment comprising heating the system after deposition of at least a layer at temperatures in the range 200-600 °C.

Detailed description of the invention

[0030] The present invention relates to a system comprising a substrate and an electroless composite coating in contact with the substrate; the electroless composite coating comprising a layered structure alternating a metallic NiP layer, comprising Ni and P and a composite NiP layer comprising Ni, P and particles dispersed therein, wherein the dispersed particles are a blend comprising first and second particles wherein the first and the second particles are different in size and nature.

[0031] Preferably the electroless composite coating consists of a layered structure alternating a metallic NiP layer, comprising Ni and P and a composite NiP layer comprising Ni, P and particles dispersed therein, wherein the dispersed particles are a blend comprising first and second particles wherein the first and the second particles are different in size and nature, and wherein the alternation is repeated 3 to 11 times, preferably 5, 7 or 9 times.

[0032] Preferably the electroless composite coating consists of a layered structure alternating a metallic NiP layer, comprising Ni and P and a composite NiP layer comprising Ni, P and particles dispersed therein, wherein the dispersed particles are a blend comprising first and second particles wherein the first and the second particles are different in size and nature, for a total of 4, 6, 8, 10 layers, preferably, 6, 8, even more preferably 8.

[0033] The invention pertains to an electroless composite coating comprising a layered structure alternating a metallic NiP layer comprising Ni and P; a composite NiP layer comprising Ni, P and dispersed particles; and a further NiP layer or composite NiP layer. Namely, the electroless composite coating comprises or preferably consists of a single or

repeated layered structure of metallic NiP/composite NiP/metallic NiP layers or composite NiP/metallic NiP/composite NiP layers.

[0034] The metallic NiP layer is different from the composite NiP layer. Preferably, the metallic NiP layer does not contain any particles dispersed therein.

[0035] Preferably the metallic NiP layer and/or the composite NiP layer comprises P in amounts between 1 and 20 wt%, more preferably in an amount between 7 and 15 wt%.

[0036] Ni and P together with any other metallic element, which may be present in the metallic and/or the composite layer form a so called metallic matrix. The amount of P is defined with respect to the total weight of the metallic matrix.

[0037] The metallic NiP layer comprises, preferably consists of Ni and P. The metallic NiP layer may also contain other suitable metallic elements, e.g. tungsten, cobalt, copper, etc., according to the known art on anticorrosive blends and alloys, in amounts between 0.1 wt%. and 30 wt% with respect to the total weight of the metallic matrix of the metallic NiP layer.

[0038] The composite NiP layer comprises and preferably consists of Ni, P and particles dispersed therein in amounts between 0.1% vol. and 50% vol., preferably between 10 % vol. and 40 % vol., with respect to the total volume of the layer, as measured by image analysis of the cross section of the composite layer.

[0039] The composite NiP layer may also contain other suitable metallic elements, e.g. tungsten, cobalt, copper, etc., in amounts between 0.1% wt. and 30% wt., according to the known art on anticorrosive blends and alloys, in amounts between 0.1 wt%. and 30 wt% with respect to the total weight of the metallic matrix of the composite NiP layer.

[0040] Particle content in the layer is estimated by analysing the images of the sections obtained from optical or SEM microscopy via the "Image J" software.

[0041] Preferably the metallic NiP layer and the composite NiP layer comprise the same amount of Ni and or P.

[0042] Preferably the composite NiP layer comprises and more preferably consists of the metallic matrix of the metallic NiP layer and of the dispersed particles.

[0043] The dispersed particles are a blend comprising first and second particles different in size and nature, and the blend may comprise further particles, which may be different in size and nature from first and second particles or the further particles may be different in nature but have the same size of the first or the second particles. However, the blend of dispersed particles preferably consists of the first and second dispersed particles.

[0044] Particles can be of metallic, ceramic, carbon or polymeric materials. Preferably the

particles are ceramic particles, more preferably ceramic particles with a hardness of 8 or higher in the Mohs scale. Examples of suitable ceramic particles are made of zirconia, silicon nitride, tungsten carbide, titanium nitride, silicon carbide, zirconium carbide, alumina, boron carbide, boron nitride, diamond. More preferably the particles are boron carbide and/or silicon carbide nano- and micro-particles.

[0045] Preferably the dispersed particles have an average size between 10 and 5000 nm.

[0046] Preferably the first particles have an average size between 200 and 5000 nm and more preferably between 500 and 3000 nm.

[0047] Preferably the second particles have an average size between 10 and 2000 nm, more preferably between 50 and 500 nm.

[0048] Preferably the first particles have size larger than the second particles. More preferably, first and second particles have a difference in average sizes of at least 100 nm, more preferably in the range 300-1500 nm.

[0049] More preferably the first particles are boron carbide particles and have average size between 500-3000 nm and the second particles are silicon carbide nanoparticles and have average size between 50 and 500 nm.

[0050] The average size of the particles is measured according to the standard ISO 9276-2:2001.

[0051] Preferably the first particles are dispersed in the composite layer matrix in amounts between 10% vol. and 40% vol. with respect to total volume of the composite layer, more preferably between 10% vol. and 30% vol.

[0052] Preferably the second particles are dispersed in the composite layer matrix in amounts between 0.1% vol. and 30% vol. more preferably between 1% vol. and 20% vol. with respect to the total volume of the composite layer.

[0053] Preferably the volume ratio between the first and second particles dispersed in the matrix is comprised within the range from 0.8 to 50, more preferably from 1 to 10.

[0054] The thickness of the multilayer composite coating may range from 1 to 150 μm , preferably it is in the range 50-80 μm . Preferably, the metallic NiP and composite NiP layer has a thickness in the range of 500 nm - 100 μm , more preferably in the range of 1 to 50 μm . The metallic and the composite layers may have different thickness from one another.

[0055] Conveniently, the alternation is applied from 2 to 11 times, preferably 5, 7 or 9 times.

[0056] Preferably, the layered structure consists of 3, 4, 5, 6, 7, 8, 9 or 10 layers, more

preferably of 6, 8 or 10 layers, even more preferably of 8 layers.

[0057] The multilayered composite coatings can be thermally treated after deposition to improve their mechanical properties, such as hardness. Thermal treatment can be applied for 1 to 8 hours in the range 250 - 550 °C. Programmed heating profiles may be applied, according to known methods in the art.

[0058] Preferably, the layer formed over and in contact with the substrate is a metallic NiP layer and or preferably the outer layer is a composite NiP layer.

[0059] The substrate can include metals and their alloys, carbon and ceramic materials, and polymeric ones. Preferably the substrate is metallic or is plate plated with a metallic layer for subsequent electroless nickel plating thereon. The substrate may be selected from steel, brass, aluminium, aluminium alloy, copper, titanium, titanium alloy, iron, nickel, nickel alloy, bronze, stainless steel or combination thereof. The substrate is preferably steel.

[0060] According to a preferred configuration, the first layer facing the substrate is a metallic NiP layer, while the outer one is a composite NiP layer.

[0061] The invention also provides a pipeline coated with the electroless composite coatings described above. Preferably the pipeline is coated with the electroless composite coating of the invention in its inner surface.

[0062] The invention further provides a method to produce the system of the invention comprising the electroless composite coating described above. Said method comprises the following steps:

1. a) Substrate preparation, which preferably comprises cleaning the substrate surface e.g. from organic residues and oxides. Preferably standard degreasing and etching solutions are used.
2. b) Deposition of a metallic NiP layer, or of a composite NiP layer on the substrate, said deposition preferably comprising contacting, preferably by immersion, the substrate with a NiP based solution to deposit the metallic NiP layer, or with a NiP based solution containing particles to deposit the composite NiP layer;
3. c) Deposition of a composite NiP layer on the substrate coated with metallic NiP layer or deposition of a metallic NiP layer on the substrate coated with composite NiP layer, said deposition preferably comprising contacting, preferably by immersion, the coated substrate with a NiP based solutions to deposit the metallic NiP layer or, respectively, with a NiP based solutions containing particles to deposit the composite NiP layer;

[0063] Step c) may be repeated as many time as necessary as long as the alternation metallic NiP layer/composite NiP layer or composite NiP layer/ metallic NiP layer is maintained. Step c) is repeated from 2 to 10 times, more preferably from 5 to 9 times.

[0064] According to an embodiment of the present invention, any or each step b) or c) of the method to produce the electroless coated system may be carried out by more than one coating phase in sequence, possibly in more than one batch. Coating steps carried out in multiple phases may be needed, e.g., for obtaining a thicker layer, e.g. 3000 nm.

[0065] Optionally, step a) of the method includes substrate activation, following substrate preparation. The activation may be achieved by palladium activation, electrochemical activation or by contact with less noble materials.

[0066] Preferably a washing step with water or an aqueous liquid is carried out at the end of step b) or each step c).

[0067] Optionally, the method includes a thermal treatment heating the system after deposition of at least a layer, preferably after all the layer have been deposited. The thermal treatment improves the mechanical properties of the system and of the electroless coating. Thermal treatment is preferably carried out at temperatures in the range 200-600 °C, more preferably in the range 250-550 °C.

[0068] NiP based solutions for electroless plating, suitable for carrying out either step b) or step c), are well known in the art and may be commercially available. They normally comprise compositions of at least a soluble Ni salt, e.g. a sulphate, and at least an ipophosphite salt. Several other components such as inhibitors, hydrogen absorbers, buffer systems, catalysts or other metal salts may be present.

[0069] Examples of electroless plating are described in "Glenn O. Mallory, Juan B. Hajdu, Electroless Plating: Fundamentals and Applications, AESF 1990".

[0070] In step b) or c), suitable particles in a convenient amount are suspended in the NiP solution, in order to achieve the desired amount of particles mixed with the NiP matrix in the composite layer. Preferred concentration of particles in the suspensions are in the range 1 - 10 g/L. Surfactants may also be present in order to stabilize the suspension. Suspended particles in step b) or c) have size and distribution according to the size and distribution of particles in the composite NIP layer of the desired coating of the present invention and are preferably SiC particles with an average size from 50 to 500 nm or B4C particles with an average size from 500 to 3000 nm.

[0071] Steps b) and c) are preferably carried out at a temperature from 55°C to 98 °C, more preferably from 70 to 95 °C. Preferred deposition time of each step is comprised from 1 min. to 60 min., more preferably from 5 min. to 20 min.. Different thickness of each layer may be obtained by varying time and temperature of the electroless plating step.

[0072] According to a preferred embodiment, step b) is a deposition of a metallic NiP layer and step c) is first carried out as a deposition of a composite NiP layer and then repeated an even

number of times, preferably 4, 6 or 8 times, maintaining alternation of metallic and composite layer deposition, in order to obtain a composite outer layer.

[0073] The invention further provides a pipeline coated with the electroless composite coating described above. Preferably the pipeline is coated in its inner surface.

[0074] The invention further pertains to the use of system comprising the electroless composite coating described above for increasing corrosion resistance of pipelines.

Figures

[0075]

Figure 1 shows a SEM image of sample R6 (NiP / SiC / B4C);

Figure 2 shows the eroded mass as percentage variation with respect to steel in erosion test for coatings.

Examples

[0076] Samples as described on table 1 were prepared. All samples R1-R6 have an alternating multilayer of metallic NiP layer and composite NiP layer structure. In R1, R3 and R5, the composite NiP layers contain a single type of dispersed particles. Samples R2, R4 and R6 contain a blend of first and second dispersed particles. KEL is a commercial coating, which consists of a layer of 30 μm NiP with on top a layer of 20 μm NiP/SiC with submicron SiC particles.

[0077] The total amount of co-deposited particles in the composite NiP layer is about 25% vol. (evaluated by image analysis of the cross section of the composite layer) with P content in both the metallic and composite layers of 10% wt.

Table 1

Sample name	Coating's material	Notes
R1	NiP+NiP/SiC on bare unpolished X60 steel with Pd activation	Thermally treated 1 h at 400°C
R2	NiP+NiP/SiC/B4C on bare unpolished X60 steel with Pd activation	
R3	NiP+NiP/SiC on lapped X60	
R4	NiP+NiP/SiC/B4C on lapped X60	

Sample name	Coating's material	Notes
R5	NiP+NiP/SiC	Thermally treated 1 h at 400°C
R6	NiP+NiP/SiC/B4C	Thermally treated 1 h at 400°C
KEL	Commercial coating (NiP+NiP/SiC)	Thermally treated 1 h at 400°C
X60	Carbon steel API 5L X60	Substrate

Plating electrolytes

[0078] The results presented are based on the use of Tecnoplate 3000® commercial formulation (provided by Tecnochimica SpA) with addition of SiC nanoparticles having an average size 100 nm and B4C submicron particles having an average size 800-1000 nm, with the following concentration in the bath 2 g/l and 4 g/l, respectively, when a first and second particle type is used.

[0079] Typical deposition parameters are:

pH = 4.8 and T = 90 °C;

Deposition total time = 2-4 hours;

Thickness of the entire structure for all the samples = 50 µm

Particles total concentration in the bath = 6 g/l

Post thermal treatment = 400 °C for 1 hour

Sample preparation protocol

[0080] Steel substrate was sonicated in acetone for 10 minutes, rinsed thoroughly, etched in sulphuric acid concentrated at 20% for 5 minutes and rinsed again. Tecnoplate 3000® was formulated according to the Tecnochimica guidelines; for composite plating, the selected amount of powders was added to the above cited solution and the batch was sonicated for 15-20 minutes. Activated steel was then immersed for 15 minutes in metallic plating solution at 85°C to deposit a seed layer of NiP alloy. NiP plated substrate was then rinsed with water and immersed in the composite plating bath with Silicon Carbide or a mixture of Silicon Carbide and

Boron Carbide for 2 hours at 85-90°C; the composite layer was then plated with NiP by immersing the sample in the metallic Tecnoplate solution for 10 minutes at 85°C. Composite plating and NiP plating steps have been repeated alternatively so as to obtain the final coating with 8 alternating layers (except sample KEL), the outer surface thereof being a composite layer.

[0081] At the end of the treatment, samples appeared dull and dusky; surface smoothing with abrasive paper was indeed carried out to obtain a polished surface. Final thermal heating, when applied, was carried out by holding the coated plates at 400°C in air for 1 hour as thermal treatment.

[0082] The samples were characterized according to the following procedures:

Coating characterization

[0083] Figure 1 shows a Scanning Electron Microscope (SEM) image of sample R6 (NiP / SiC / B₄C).

[0084] Morphological characterization of composite coatings shows the typical features of composite materials. Surface appearance, if not lapped, is dull and matt, while cross section observations show a two phases structure constituted by the NiP alloy metal matrix and the dispersion phase, i.e. SiC or mixture of SiC and B₄C. A multilayer structure due to NiP and composite layer alternation is also observed. The NiP matrix is obtained in a high phosphorus plating electrolyte with P content in the matrix typically, 10% by weight.

[0085] The crystalline structure evolution (XRD) with thermal treatment at various temperature between 300-500 °C for 1 hour shows the initial amorphous structure evolves into a crystalline one constituted by metallic Ni and hard Ni_xPy intermetallic compounds.

Micro-hardness

[0086] Table 2 reports the results of the micro-hardness measurements performed on sections of the samples described above. The thickness of the coatings (ranging from 50-200 µm) and the morphology of the coatings has required the use of micro-indentation (100 g weight).

Surface texture

[0087] Table 2 also reports the results 'Surface texture' (Sa) measurements obtained by optical digital microscopy.

Erosion characterization

[0088] Erosion tests have been performed in an experimental station composed of a mixing tank, a centrifugal pump and a test tank containing the nozzle and the sample, using a slurry prepared by mixing water and sand. Commercial sand was used, named "Impalpabile" from Sabbie Sataf (size < 400 μm).

[0089] The nozzle is made of tungsten carbide with a cylindrical shape and an internal diameter of 8 mm.

[0090] Previously weighed samples (6.9 x 7.5 x 0.4 cm) were subjected to a slurry highpressure perpendicular jet from the nozzle, for a variable duration time comprised between 2 and 5 minutes. The slurry is continuously circulated from the mixing tank through the centrifugal pump to the nozzle in the test tank and then back to the mixing tank. The nozzle is placed within the test tank at a distance of 20 mm from the surface of the sample to be tested, with the jet directed perpendicularly to the surface. Both the nozzle and the sample are completely sunk in the slurry so that no gas is entrained by the jet. After the test, each sample is washed, rinsed and weighed again.

[0091] The erosion factor has been calculated as $ER = \Delta M / \rho_s QCT$, wherein:

ΔM	Mass lost from the sample during the test
T	Test time
ρ_s	Density of solids in the mixture
Q	Flow rate
C	volumetric concentration of solids in the mixture
v	Jet speed
ER	Erosion Ratio

[0092] For each material the average ER is calculated from ER measured on samples tested at 2, 3 and 5 minutes duration time respectively.

[0093] Figure 2 reports the percentage erosion rate with respect to steel for erosion tests in experimental conditions (Test 2) reported below in order to highlight the behaviour of the

coating only for composite coatings from (NiP-SiC; NiP-SiC/B4C) and commercial KEL (KEL), with total thickness of the coating 50 µm and for carbon steel for comparison:

Test 2 conditions were:

$$v = 35 \text{ m/s}$$

Distance sample - nozzle: 20 mm

$$\rho_s = 1560 \text{ kg/m}^3$$

$$C = 1.2\% \text{ vol/vol}$$

[0094] These operating conditions lead to the erosion of the coating alone, with minor contribution from the substrate.

[0095] If the behaviour of the coatings only is emphasized, NiP-SiC-B4C composite coating shows an erosion resistance slightly higher than the NiP-SiC and it is able to reduce the amount of eroded material with respect to the steel substrate.

Corrosion test in 'SOUR' environment

[0096] Corrosion resistance has been evaluated through exposure tests in sour environment. The behaviour of the coatings (R5, R6, on steel API 5L X60) was compared with reference materials, i.e. bare API 5L X60. Corrosion was evaluated observing the formation of corrosion products after the test on Miller shaped samples.

[0097] Tests in sour environment were performed by contact with salt solutions, hydrogen sulfide 3% and carbon dioxide 13%.

[0098] In a pressurized chamber in Hastelloy C276 (volume 1 liter), previously weighed samples (Miller Test blocks, 2.5 x 1.3 x 0.5 cm) were immersed in 300 mL water solution containing 30 g/l of chlorides as NaCl. After closing the pressurized chamber, a gas mixture containing (by vol.): H₂S 3%, CO₂ 13%, N₂ 85% was charged under heating until the following conditions were reached:

- temperature 90 °C
- pressure 100 bar
- The samples were maintained under these conditions for a duration of 7 days.

[0099] For the bare steel X60 the test lasted only 24 hours due to the fast degradation of the materials. At the end of each test, weight losses have been evaluated and summarized in the following table 2.

The Miller test for abrasion resistance

[0100] Miller tests have been performed in a Miller Machine with four plastic trays, according to ASTM G75 (Standard), using a slurry prepared by mixing water and sand in the ratio 1/1. Commercial sand was used, named "Impalpabile" from Sabbie Sataf (size < 400 μm). The MN number of this slurry with the reference material (steel Fe-27Cr) is 156. The bottom of each tray in the machine was covered with a rubber lap of neoprene (Modified MIL-R-855C, Class 2, Grade 80). Before test, each sample (Miller metal block 2.5 x 1.3 x 0.5 cm) is washed and sonicated in water, then degreased with acetone, dried in a nitrogen stream and weighed (0.1 mg precision) and placed on the arm in the tray.

[0101] The applied load on standard Miller block samples was 22.24 N. Miller tests and SAR numbers were performed and calculated according to the standard for the coatings and a reference material (Steel Fe-27Cr). For the NiP coatings, a specific weight of 7,75 g/cm³ was used.

[0102] In order to most appropriately apply the Miller test to coated samples, suitable conditions were selected whereby erosion was essentially limited to the coating layer, without abrading the less resistant below carbon steel. Therefore, the Mille Number was calculated as the tangent slope of the interpolation at 40 minutes instead of two hours as requested by the standard procedure. It was checked that in such conditions, less than 30 % of the surface of each sample showed exposed metal substrate. In this way, only the abrasion resistance of the coating was measured. Miller test was also performed on two samples of examples R5 and R6 previously submitted to the corrosion test (examples R5C and R6C respectively).

Results

[0103] Characterization results are reported on Table 2.

Table 2

	R1	R2	R3	R4	R5	R6	R5C	R6C	X60	KEL
Average Microhardness (12 meas.)					820	750			150	
Average Roughness					2.2	2.2				
Average velocity of corrosion (2 meas.) (mm/y)					< 0.002	< 0.002			1.9	
Miller test (Slope at 40 min.)	1109	724	853	718	1326	1254	1099	904	3986	1689

[0104] On the basis of the acquired data, it can be concluded that all the tested coatings have a better abrasion resistance than steel X60 (used as substrate).

[0105] The corrosion treatment (samples R5C and R6C) does not decrease the abrasion resistance of the coatings. On the contrary, a surprising improvement was seen. According to the SAR results (t = 40 minutes for samples with abrasion of the coating lower than 30%) the best coatings appear to be NiP/SiC/B4C (R2, R4, R6 and R6C); the last two positions are for of commercial coating KEL and the substrate (X60).

[0106] As far as the corrosion test is concerned, all the coatings of the invention show an excellent corrosion resistance. The corrosion velocity is always well below 0,1 mm/year (which defines the suitability of the metallic material used in the sector Oil&Gas). This is a particularly lower value considering the thickness of the coatings (between 50-200 µm). It can be assumed that in aggressive conditions ('sour') the coating could withstand even longer period. It shall also be noted that the corrosion resistance of this sample is superior than the one of WC, widely used for *Oil & Gas applications*.

[0107] The low corrosion resistance featured by the steel substrate underline the importance of having an optimal adherence of the coating to the substrate. A detachment caused by accidental reasons would compromise the excellent corrosion resistance performances of the coating.

[0108] Morphology studies done by SEM have demonstrated that NiP / SiC and NiP /SiC / B4C have generally regular morphology.

REFERENCES CITED IN THE DESCRIPTION

Cited references

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P a t e n t k r a v

1. System, der omfatter et substrat og en strømløs kompositcoating i kontakt med substratet, hvor den strømløse kompositcoating omfatter en lagdelt struktur, som alternerer et metallisk NiP-lag omfattende Ni og P og et sammensat NiP-lag, hvilket sammensatte NiP-lag omfatter Ni, P og dispergerede partikler, hvor de dispergerede partikler er en blanding omfattende første og andre partikler, og de første og andre partikler er forskellige i størrelse og beskaffenhed, og hvor den lagdelte struktur alternerer mindst et metallisk NiP-lag, der omfatter Ni og P; mindst et sammensat NiP-lag, der omfatter Ni, P og dispergerede partikler; og mindst et yderligere NiP-lag eller sammensat NiP-lag.
2. System ifølge krav 1, hvor det metalliske NiP-lag og/eller det sammensatte NiP-lag omfatter P i en mængde på mellem 1 og 20 vægt% i forhold til den samlede vægt af den metalliske matrix i laget.
3. System ifølge krav 1 eller 2, hvor de første partikler har en gennemsnitlig størrelse mellem 500-3000 nm, og de andre partikler har en gennemsnitlig størrelse mellem 50-500 nm.
4. System ifølge et hvilket som helst af de foregående krav, hvor partiklerne er borcarbidpartikler og/eller siliciumnanopartikler.
5. System ifølge et hvilket som helst af de foregående krav, hvor det metalliske NiP-lag består af Ni og P eller af Ni, P og et eller flere yderligere metalliske grundstoffer.
6. System ifølge et hvilket som helst af de foregående krav, hvor det sammensatte NiP-lag består af Ni og P og blandingen af dispergerede partikler eller af Ni, P, blandingen af dispergerede partikler og et eller flere yderligere metalliske grundstoffer.

7. System ifølge et hvilket som helst af de foregående krav, hvor alternationen sker fra 3 til 11 gange, fortrinsvis 5, 7 eller 9 gange.
- 5 8. System ifølge et hvilket som helst af de foregående krav, hvor laget dannet over og i kontakt med substratet er et metallisk NiP-lag.
9. System ifølge et hvilket som helst af de foregående krav, hvor det ydre lag er et sammensat NiP-lag.
- 10 10. Rørledning omfattende systemet ifølge et hvilket som helst af kravene 1 til 9.
11. Rørledning ifølge krav 10, som er coatet i sin indre overflade.
- 15 12. Anvendelse af systemet ifølge et hvilket som helst af kravene 1 til 9 til at forbedre modstanden af en rørledning over for kemisk og mekanisk nedbrydning.
- 20 13. Fremgangsmåde til fremstilling af systemet ifølge et hvilket som helst af kravene 1 til 9 eller rørledningen ifølge krav 10 eller 11, omfattende følgende trin:
- a) substratforberedelse;
- b) aflejring af et metallisk NiP-lag eller af et sammensat NiP-lag på substratet,
- c) aflejring af et sammensat NiP-lag på substratet, der er coatet med metallisk NiP-lag, eller aflejring af et metallisk NiP-lag på substratet, der er coatet med komposit-NiP-lag;
- 25 hvor trin c) gentages mindst to gange (tre lag), hvor fremgangsmåden eventuelt yderligere omfatter en termisk behandling, der omfatter opvarmning af systemet efter aflejring af mindst et lag ved temperaturer i området 200-600°C.
- 30 14. Fremgangsmåde ifølge krav 13, hvor trin c) gentages så mange gange som nødvendigt, så længe det alternerende metalliske NiP-lag/komposit-NiP-

lag eller det sammensatte NiP-lag/metalliske NiP-lag opretholdes, fortrinsvis gentages op til 10 gange.

DRAWINGS

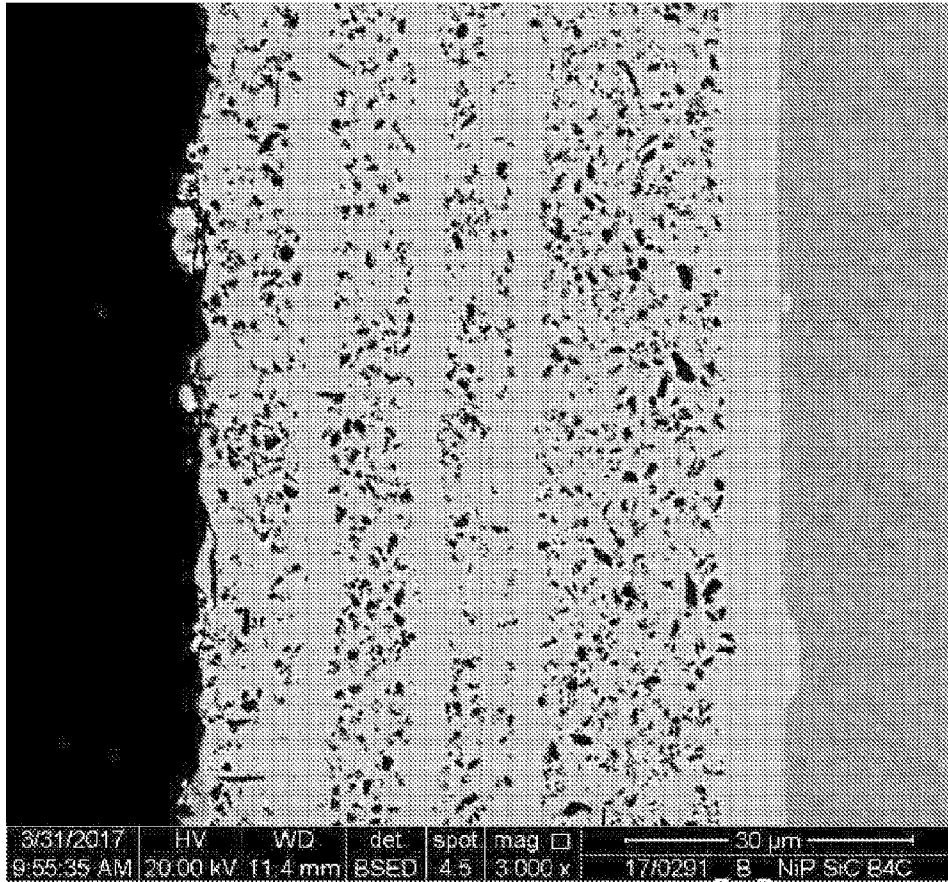


Figure 1

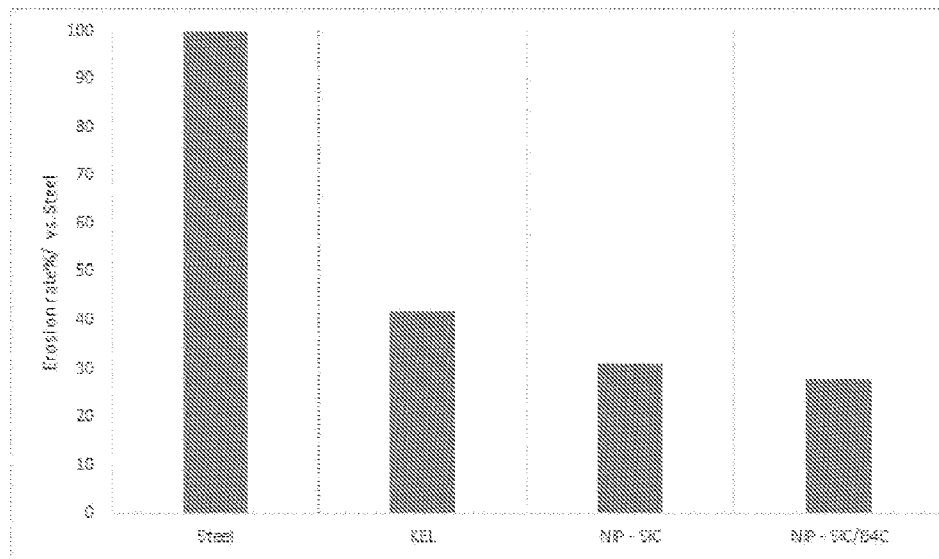


Figure 2: Erosion Test