

(19) World Intellectual Property Organization  
International Bureau



(43) International Publication Date  
15 July 2010 (15.07.2010)

(10) International Publication Number  
**WO 2010/080659 A2**

PCT

(51) International Patent Classification:  
*B29C 67/00* (2006.01)

(21) International Application Number:  
PCT/US2009/069411

(22) International Filing Date:  
23 December 2009 (23.12.2009)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:  
12/349,204 6 January 2009 (06.01.2009) US

(71) Applicant (for all designated States except US): **THE BOEING COMPANY** [US/US]; 100 North Riverside Plaza, Chicago, Illinois 60606-2016 (US).

(72) Inventors; and

(75) Inventors/Applicants (for US only): **HUSKAMP, Christopher S.** [US/US]; 1620 Lucas Street, Unit #802, St. Louis, Missouri 63103 (US). **LYONS, Brett I.** [US/US]; 208 North 9th Street, Apartment 1107, St. Louis, Missouri 63101 (US).

(74) Agents: **HALPERIN, Brett L** et al.; The Boeing Company, P.O. Box 2515, MC 110-SD54, Seal Beach, California 90740-1515 (US).

(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KN, KP,

[Continued on next page]

(54) Title: MANUFACTURING AIRCRAFT PARTS

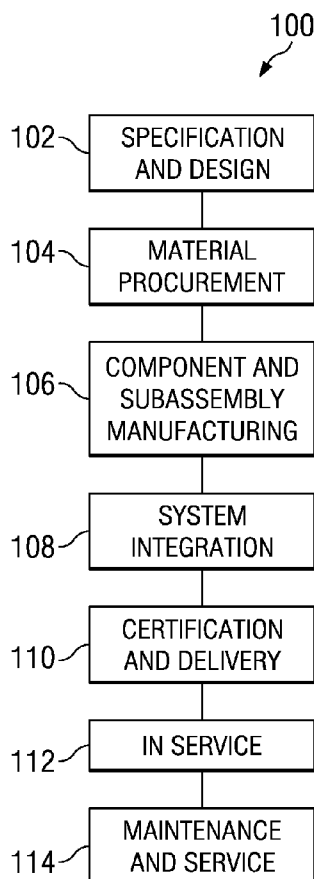


**FIG. 1**

(57) Abstract: A method and apparatus is present for manufacturing parts. A powder material is comprised of a polymer that is semi-crystalline. The powder material has an overlap between a melting temperature range and a crystallization temperature range. The powder material also has a size particular distribution that is substantially a Gaussian distribution, a particle shape that is substantially spherical, and a desired melt flow rate that is less than a temperature at which the powder material begins to chemically break down. The powder material is selected to form a selected powder material. A part is manufactured using an energy delivery system and the selected powder material.

WO 2010/080659 A2



KR, KZ, LA, LC, LK, LR, LS, LT, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PE, PG, PH, PL, PT, RO, RS, RU, SC, SD, SE, SG, SK, SL, SM, ST, SV, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

TM), European (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MK, MT, NL, NO, PL, PT, RO, SE, SI, SK, SM, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

**(84) Designated States** (*unless otherwise indicated, for every kind of regional protection available*): ARIPO (BW, GH, GM, KE, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ,

**Published:**

— *without international search report and to be republished upon receipt of that report (Rule 48.2(g))*

**MANUFACTURING AIRCRAFT PARTS****BACKGROUND INFORMATION**

The present disclosure relates generally to manufacturing parts and, in particular, to manufacturing parts using selective  
5 laser sintering.

Selective laser sintering is a manufacturing technique that fuses diffused particles into a three-dimensional object using a laser. A laser may selectively fuse small particles in the form of a powdered material by scanning cross sections on the surface  
10 of a bed of powder. These cross sections may be identified from a three-dimensional model of the part. As each cross section is scanned, the bed of powder may be lowered by a one layer thickness, and a new layer of powder may be applied on top of the scanned layer. This process may be repeated until the part  
15 is completed.

As compared to other manufacturing methods, selective laser sintering can be used to manufacture parts from a relatively wide range of materials. These materials include, for example, polymers, metals, and sand. The process may include full  
20 melting, partial melting, or liquid phase sintering.

Selective laser sintering may be used to build prototypes and production parts for use, such as in an aircraft. Selective laser sintering is capable of being used to produce parts with complex geometries within various dimensions.

25 Aircraft parts typically have stringent and/or extreme design requirements as compared to parts with other applications. These requirements may occur from operating environments that may have high loads and temperatures. Further, these parts also may be required to be capable of  
30 withstanding impact loads from maintenance, handling, and/or other types of impact loads. For example, some parts may need to survive usage in some airframe locations that have in-service

temperature ranges from around -54 degrees Celsius to around 225 degrees Celsius.

In particular, parts that exist near areas that are heated to or near engine or exhaust temperatures may need to be serviced and handled on the ground in severe winter conditions that may be present above 48 degrees north latitude or at altitude. These conditions require the material that the parts are made of to have sufficient impact resistance at the low end of the temperature range. Simultaneously, sufficient stiffness and mechanical strength must be maintained at the high end of the temperature range to prevent failure in service.

Therefore, it would be advantageous to have a method and apparatus that takes into account one or more of the different issues described above as well as possibly other issues.

#### SUMMARY

In one advantageous embodiment, a method is present for manufacturing parts. A powder material is selected. The powder material is comprised of a polymer that is a semi-crystalline. The powder material has an overlap between a melting temperature range and a crystallization temperature range. The powder material also has a size particular distribution that is substantially a Gaussian distribution, a particle shape that is substantially spherical, and a desired melt flow rate that is available at less than a temperature at which the powder material begins to chemically break down. A part is manufactured using an energy delivery system and the selected powder material.

In another advantageous embodiment, a method for manufacturing parts is present. A powder material is comprised of a polymer that is semi-crystalline. The powder material is capable of entering a liquid state and a crystalline state within an overlapping range of temperatures. The powder material has a particle size distribution capable of allowing

particles to flow through openings formed by larger particles in the particle size distribution. The powder material also has a particle shape that is substantially spherical and a desired melt flow rate that occurs at a temperature below a temperature at which the powder material begins to break down. The powder material is selected to form a selected powder material. The part is manufactured using the selected powder material and an energy delivery system.

In yet another advantageous embodiment, an apparatus has a powder material and a laser sintering machine capable of manufacturing a part using the powder material. The powder material is comprised of a polymer that is a semi-crystalline. The powder material has an overlap between a melting temperature range and a crystallization temperature range. The powder material has a size particle distribution that is substantially a Gaussian distribution, a particle shape that is substantially spherical, and a desired melt flow rate that is less than a temperature at which the powder material begins to break down.

The features, functions, and advantages can be achieved independently in various embodiments of the present disclosure or may be combined in yet other embodiments in which further details can be seen with reference to the following description and drawings.

#### **BRIEF DESCRIPTION OF THE DRAWINGS**

The novel features believed characteristic of the advantageous embodiments are set forth in the appended claims. The advantageous embodiments, however, as well as a preferred mode of use, further objectives, and advantages thereof, will best be understood by reference to the following detailed description of an advantageous embodiment of the present disclosure when read in conjunction with the accompanying drawings, wherein:

**Figure 1** is a diagram illustrating an aircraft manufacturing and service method in accordance with an advantageous embodiment;

**Figure 2** is a diagram of an aircraft in which an advantageous embodiment may be implemented;

**Figure 3** is a diagram of a manufacturing environment in accordance with an advantageous embodiment;

**Figure 4** is a block diagram illustrating characteristics for a powder material for use in manufacturing parts in accordance with an advantageous embodiment;

**Figure 5** is a diagram illustrating differential scanning calorimetry curves in accordance with an advantageous embodiment;

**Figure 6** is a diagram illustrating desirable melt flow in accordance with an advantageous embodiment;

**Figure 7** is a diagram illustrating an undesirable melt flow in accordance with an advantageous embodiment;

**Figure 8** is a diagram illustrating a table of parameters for a laser sintering machine in accordance with an advantageous embodiment;

**Figure 9** is a diagram of a table of parameters for setting a selective sintering machine in accordance with an advantageous embodiment;

**Figure 10** is a table illustrating parameters for setting a selective laser sintering system in accordance with an advantageous embodiment;

**Figure 11** is a table illustrating an illustration of mechanical properties for polymers that may be used in accordance with an advantageous embodiment;

**Figure 12** is a diagram illustrating parts that may be manufactured using polymers in accordance with an advantageous embodiment;

**Figure 13** is a flowchart of a process for manufacturing parts in accordance with an advantageous embodiment;

**Figure 14** is a flowchart of a process for processing a polymer for use as a powder material in accordance with an advantageous embodiment; and

**Figure 15** is a flowchart of a process for manufacturing a part in accordance with an advantageous embodiment.

#### DETAILED DESCRIPTION

Referring more particularly to the drawings, embodiments of the disclosure may be described in the context of aircraft manufacturing and service method **100** as shown in **Figure 1** and aircraft **200** as shown in **Figure 2**. Turning first to **Figure 1**, a diagram illustrating an aircraft manufacturing and service method is depicted in accordance with an advantageous embodiment. During pre-production, exemplary aircraft manufacturing and service method **100** may include specification and design **102** of aircraft **200** in **Figure 2** and material procurement **104**.

During production, component and subassembly manufacturing **106** and system integration **108** of aircraft **200** in **Figure 2** takes place. Thereafter, aircraft **200** in **Figure 2** may go through certification and delivery **110** in order to be placed in service **112**. While in service by a customer, aircraft **200** in **Figure 2** is scheduled for routine maintenance and service **114**, which may include modification, reconfiguration, refurbishment, and other maintenance or service.

Each of the processes of aircraft manufacturing and service method **100** may be performed or carried out by a system integrator, a third party, and/or an operator. In these examples, the operator may be a customer. For the purposes of this description, a system integrator may include, without limitation, any number of aircraft manufacturers and major-system subcontractors; a third party may include, without limitation, any number of vendors, subcontractors, and

suppliers; and an operator may be an airline, leasing company, military entity, service organization, and so on.

With reference now to **Figure 2**, a diagram of an aircraft is depicted in which an advantageous embodiment may be implemented.

5 In this example, aircraft **200** is produced by aircraft manufacturing and service method **100** in **Figure 1** and may include airframe **202** with a plurality of systems **204** and interior **206**. Examples of systems **204** include one or more of propulsion system **208**, electrical system **210**, hydraulic system **212**, and  
10 environmental system **214**. Any number of other systems may be included. Although an aerospace example is shown, different advantageous embodiments may be applied to other industries, such as the automotive industry.

Apparatus and methods embodied herein may be employed  
15 during any one or more of the stages of aircraft manufacturing and service method **100** in **Figure 1**. For example, components or subassemblies produced in component and subassembly manufacturing **106** in **Figure 1** may be fabricated or manufactured in a manner similar to components or subassemblies produced  
20 while aircraft **200** is in service **112** in **Figure 1**.

Also, one or more apparatus embodiments, method  
embodiments, or a combination thereof may be utilized during production stages, such as component and subassembly manufacturing **106** and system integration **108** in **Figure 1**, for  
25 example, without limitation, by substantially expediting the assembly of or reducing the cost of aircraft **200**. Similarly, one or more of apparatus embodiments, method embodiments, or a combination thereof may be utilized while aircraft **200** is in service **112** or during maintenance and service **114** in **Figure 1**.

30 The different advantageous embodiments provide a method for manufacturing parts. The method may include selecting a powder material that is comprised of a polymer that is a semi-crystalline polymer, has an overlap between a melting temperature range and a crystallization temperature range, has a

particle size distribution that is substantially a Gaussian distribution, has a particle shape that is substantially spherical, and has a desired melt flow rate that is less than a temperature at which the powder material begins to chemically break down. The part is manufactured using an energy delivery system and the selected powder material.

The different advantageous embodiments also provide a method for manufacturing parts in which a powder material that is semi-crystalline is selected. The powder material is capable of entering a liquid state and a crystalline state within an overlapping range of temperatures. The powder material has a particle size distribution capable of allowing particles to flow through openings formed by larger particles in the particle size distribution. The powder material also has a particle shape that is substantially spherical and a desired melt flow rate that occurs at a temperature below a temperature at which the powder material begins to chemically break down.

With reference now to **Figure 3**, a diagram of a manufacturing environment is depicted in accordance with an advantageous embodiment. In this example, manufacturing environment **300** may be used to manufacture parts for aircraft **200** in **Figure 2**. As illustrated, manufacturing environment **300** contains manufacturing apparatus **302**. Manufacturing apparatus **302** may be used to manufacture part **304**.

Manufacturing apparatus **302** may include energy delivery system **305**, chamber **306**, bed **308**, environmental control unit **310**, and powder delivery system **312**. In these examples, energy delivery system **305** may take the form of selective laser system **311**. Selective laser system **311** may be implemented using any device capable of generating laser beam **314** and directing laser beam **314**.

Powder delivery system **312** deposits powder material **316** onto bed **308**. Selective laser system **311** may direct laser beam **314** onto powder material **316** on bed **308**. Laser beam **314** may

melt and/or sinter powder material 316 in pattern 318 in a manner to form a portion of part 304.

Bed 308 may lower and another layer of powder material 316 may be deposited onto bed 308. Selective laser system 311 may then direct laser beam 314 onto powder material 316 on bed 308 to form another portion of part 304. In these different advantageous embodiments, environmental control unit 310 may control the temperature within chamber 306 and on bed 308. Further, environmental control unit 310 also may maintain a level of oxygen in chamber 306 within some selected amount. The level of oxygen in chamber 306 may be maintained within the selected amount by introducing a gas at a controlled temperature. This gas may be, for example, an inert gas.

For example, environmental control unit 310 may maintain a level of oxygen that is less than around one percent with the input gas temperature at the bed temperature plus 2 degrees Celsius. Environmental control unit 310 may introduce an inert gas, such as nitrogen, into chamber 306.

In the different advantageous embodiments, powder material 316 may be selected as a material suitable for aircraft parts. The different advantageous embodiments recognize that currently used materials for constructing parts using directed energy systems such as a selective laser sintering system may produce parts using materials having melting points that are lower than may be desired. For example, the different advantageous embodiments recognize and take into account that many currently used materials may have a melting point of around 180 to 190 degrees Celsius. In many cases, parts are desired that may be capable of withstanding temperatures of around 250 degrees Celsius and above.

The different advantageous embodiments also recognize and take into account that although many plastic materials may meet the temperature range needed for performance, these materials may be unsuitable for manufacturing parts. The different

advantageous embodiments recognize and take into account that many of these plastic materials currently cannot be used with energy delivery systems, such as selective laser sintering systems. These materials may require molds, which have higher costs and lead times.

With currently available selective laser sintering systems, mechanical parts may be made. These mechanical parts, however, may not have the desired mechanical properties at operating temperatures in which the parts may be used. For example, with selective laser sintering, the different advantageous embodiments recognize and take into account that parts may be made with mechanical properties that are suitable for temperatures around 75 degrees Celsius or less. These parts typically become soft and/or lose mechanical properties at around 100 degrees Celsius.

The different advantageous embodiments also recognize and take into account that aluminum may be used to create parts using currently available manufacturing processes. This material provides suitable properties at temperatures of around room temperature to around 120 degrees Celsius. The different advantageous embodiments, however, recognize and take into account that using aluminum increases the weight of the parts.

Thus, the different advantageous embodiments recognize and take into account that it would be desirable to have a polymer that can be used at higher temperatures than currently available materials without a weight penalty of a metal.

In these examples, manufacturing apparatus **302** may take the form of a sintering laser system machine available from 3D Systems, Inc. For example, a Sinter Station® 2500CI system may be used to implement manufacturing apparatus **302**. This system may be modified to provide the operating environment needed to process powder material **316**. For example, the machine may be modified to run at temperatures of around 330 degrees Celsius or greater. This temperature may be a temperature maintained on

the surface of bed **308**. These modifications may include ensuring seals, lubricants, and hardware are capable of operating at these temperatures. Further, the machine may be modified to provide an environment that is around one percent or less in oxygen content throughout the range of temperatures.

These modifications may include adding or using a multi-zone heater capable of operating at the desired temperatures. Further, the heating system is capable of reducing thermal gradients. These thermal gradients may be reduced to less than around 10 degrees Celsius within one inch of where a part is to be built. The reduced temperature gradient is to avoid an area in which a material does not properly liquefy, melt, and/or sinter, which may result in low mechanical properties and distortion of parts.

If the gradient results in a high-temperature area in which the temperature change is greater than desired, particles may fuse together generating a porous and hard cake from the powder material. Parts made in this type of condition may have powder material adhere to the parts making those parts dimensionally incorrect and possibly having low strength for a measured cross section.

In maintaining an oxygen level of less than one percent in these examples, nitrogen gas may be pumped into the chamber. Heating of the nitrogen gas also may be necessary to avoid degrading the energy supplied from the laser unit. Of course, any laser sintering system machine capable of processing powder material **316** may be used in addition to the example provided.

With reference now to **Figure 4**, a block diagram illustrating characteristics for a powder material for use in manufacturing parts is depicted in accordance with an advantageous embodiment. In this example, powder material **400** is an example of a powder material that may be used to implement powder material **316** in **Figure 3** to manufacture part **304**.

Powder material **400** comprises polymer **402**. Polymer **402** may have characteristics **404**. These characteristics may include, for example, without limitation, semi-crystalline **405**, melting temperature range **406**, crystallization temperature range **408**,  
5 particle size distribution **410**, particle shape **412**, and melt flow rate **414**. For example, polymer **402** has melting temperature range **406** and crystallization temperature range **408** that overlap.

In some advantageous embodiments, the overlap between  
10 melting temperature range **406** and crystallization temperature range **408** may be analyzed on differential scanning calorimetry curves. The overlap between these two ranges of temperatures may be such that the amount of heat absorbed increases when powder material **400** melts and becomes a liquid such that when  
15 powder material **400** cools and turns back into a crystallized form, an increase in heat occurs. In the different advantageous embodiments, it may be desirable to have an overlap at these increases in heat absorption and heat release at the different temperatures.

20 With reference to **Figure 5**, a diagram illustrating differential scanning calorimetry curves is depicted in accordance with an advantageous embodiment. In graph **500**, the x-axis represents temperature, while the y-axis represents heat flow. Curve **502** illustrates endothermic heat flow, while curve  
25 **504** illustrates exothermic heat curve. Curve **502** represents the heat flow for melting powder material **400** in **Figure 4**, while curve **504** illustrates heat flow for re-crystallizing powder material **400** in **Figure 4**. As can be seen, an overlap is present in section **506** in which powder material **400** in **Figure 4** may  
30 exist both in a powdered form and a melted form at the same temperature.

Turning back to **Figure 4**, particle size distribution **410**, in these examples, may be selected to increase the flow of particles. It may be desirable to allow particles to flow or

move through openings created by larger particles that may be packed or stacked against each other. Further, it may be desirable to have a particle size distribution that allows for particles to flow more easily when deposited on a bed. The  
5 increased flow of particles may be desirable to obtain a more substantially smooth surface for energy delivery.

In the different advantageous embodiments, a particle size distribution of around 20 micrometers to around 130 micrometers may be used with an average particle size between around 50  
10 micrometers and around 80 micrometers.

Particle shape **412** may be a near round and/or spherical shape. In the different advantageous embodiments, the material may be placed into a spherical shape through heat. A spherical shape may be desirable to provide better propagation of the  
15 material when powder material **400** is pushed onto a bed from a source or storage container for powder material **400**. With particles that are substantially spherical, depositing particles may allow particles to settle into openings and fill voids rather than clump or cause more uneven surfaces.

Melt flow rate **414** for polymer **402** may be selected as a melt flow rate that may occur at a temperature below the temperature at which polymer **402** begins to break down. In these examples, the melt flow rate may be selected as one in which the powder material when melting and/or in liquid form may flow but  
20 does not bead up. The flow may be in a sheet-like manner. The beading may not occur by selecting a powder material that flows with a viscosity and height and surface tension that avoids beading. This type of flow may be referred to as veining. The temperature may be such that damage or a breakdown in polymer  
25 **402** does not occur at the desired melt flow rate.

Melt flow rate **414** may be selected as one in which any gas generated and/or atmospheric gas that may be present within polymer **402** during melting may exit polymer **402**, while polymer **402** is in liquid form. Melt flow rate **414** also may be selected

to avoid balling up to avoid clumping when manufacturing the part. In the different advantageous embodiments, a melt flow rate of around 15 grams/10 minutes to around 40 grams/10 minutes at a temperature lower than the temperature at which the polymer  
5 begins to break down may be selected for melt flow rate **414**.

Turning now to **Figure 6**, a diagram illustrating desirable melt flow is depicted in accordance with an advantageous embodiment. As can be seen in this example, material **600** has a desirable melt flow in which material **600** is in a liquid form  
10 but does not form beads.

In **Figure 7**, a diagram illustrating an undesirable melt flow is depicted in accordance with an advantageous embodiment. In this example, material **700** has an undesirable melt flow in which material **600** in **Figure 6** is in a liquid form in which  
15 beading occurs.

Examples of powder materials that may be used include, for example, without limitation, nylon 66, polyphenylene sulfide, polyetherkeytinekeytone, a nylon 66 blend, a polyphenylene sulfide blend, a polyetherkeytinekeytone blend, and other  
20 suitable materials. Blends of the selected polymers may include blending the polymers with other powder materials. These powder materials may include, for example, without limitation, at least one of glass beads, hollow glass spheres, glass fibers, carbon fibers, other polymers, minerals, clays, flame-retardant  
25 additives, color additives, and/or other suitable materials.

As used herein, the phrase "at least one of", when used with a list of items, means that different combinations of one or more of the items may be used, and only one of each item in the list may be needed. For example, "at least one of item A,  
30 item B, and item C" may include, without limitation, item A or item A and item B. This example also may include item A, item B, and item C or item B and item C.

In the different advantageous embodiments, these materials may be selected to have characteristics such as, for example,

powder material **400** in **Figure 4** with a desired melting temperature range **406**. In these examples, melting temperature range **406** may be desired to be around 230 degrees Celsius and above. Of course, other melting temperature ranges may be used, depending on the particular implementation.

With reference now to **Figure 8**, a diagram illustrating a table of parameters for a laser sintering machine is depicted in accordance with an advantageous embodiment. In this example, table **800** provides an example of parameters that may be used to produce parts using nylon 66 as a powder material. Table **800** illustrates parameters that may be set in a selective sintering machine such as, for example, 3D Systems 2500CI Selective Sintering Machine. However, some modifications may be required to safely obtain and maintain the required processing temperatures.

When powder material **400** takes the form of nylon 66, the bed in the selective laser sintering machine may be heated to a temperature from around 190 degrees Celsius to around 260 degrees Celsius. The energy source should provide sufficient heat to increase the temperature above the melting point of the material from around 197 degrees Celsius to 265 degrees Celsius.

With reference now to **Figure 9**, a diagram of a table of parameters for setting a selective sintering machine is depicted in accordance with an advantageous embodiment. Table **900** provides an example of parameters for settings in a selective sintering machine such as, for example, 3D Systems SLS Machine, as previously described.

These parameters are ones that may be used when powder material **400** takes the form of polyphenylene sulfide for use in manufacturing parts. When powder material **400** takes the form of polyphenylene sulfide, the powder in the bed may be heated from around 240 degrees Celsius to around 282 degrees Celsius. The energy applied may heat the temperature of the material above

the melting point to a temperature of around 280 degrees Celsius to around 285 degrees Celsius.

With reference now to **Figure 10**, a table illustrating parameters for setting a selective laser sintering system is depicted in accordance with an advantageous embodiment. Table **1000** provides an example of parameters that may be set in a selective laser sintering machine, such as 3D Systems SLS Machine. The parameters in table **1000** may be used when powder material **400** takes the form of polyetherkeytinekeytone.

With reference now to **Figure 11**, a table illustrating mechanical properties for polymers that may be used is depicted in accordance with an advantageous embodiment. These mechanical properties are polymers that may be processed using selective laser sintering. In this example, table **1100** illustrates ultimate tensile tile strength, offset yield strength, elongation percentage, and melting point temperatures for a number of materials in comparison with some currently known materials.

In these examples, entries **1102**, **1104**, and **1106** are entries for materials selected in accordance with an advantageous embodiment. Entries **1108** and **1110** represent materials currently used for comparison purposes. Entry **1102** is for polyetherkeytinekeytone, entry **1104** is for polyphenylene sulfide, and entry **1106** is for nylon 66. Entry **1108** is for nylon 12, while entry **1110** is for nylon 11.

As can be seen, the melting points for polyetherkeytinekeytone, polyphenylene sulfide, and nylon 66 are significantly higher as compared to nylon 12 and nylon 11. Nylon 12 has a melting point temperature of around 187 degrees Celsius, while nylon 11 has a melting point temperature of around 186 degrees Celsius. Nylon 66 has a melting temperature of around 254 degrees Celsius, polyphenylene sulfide has a melting point of around 280 degrees Celsius, and polyetherkeytinekeytone has a melting point of around 310

degrees Celsius. In addition to having higher melting points, these different materials also may have the desired mechanical properties for constructing aircraft parts.

With reference now to **Figure 12**, a diagram illustrating parts that may be manufactured using polymers is depicted in accordance with an advantageous embodiment. In these examples, parts **1200** are example parts that may be manufactured using powder material **400** in **Figure 4**. Parts **1200** include duct **1202**, electrical shroud **1204**, power distribution panel **1206**, fitting **1207**, closure **1208**, conduit **1210**, and other suitable aircraft parts. Many other types of parts, other than these illustrative ones, may be manufactured using polymers and powder materials for selective laser sintering processes in accordance with an advantageous embodiment.

With reference now to **Figure 13**, a flowchart of a process for manufacturing parts is depicted in accordance with an advantageous embodiment. The process illustrated in **Figure 13** may be implemented in a manufacturing environment such as, for example, manufacturing environment **300** in **Figure 3**. In these illustrative examples, the process may begin by selecting a powder material that is comprised of a polymer that is semi-crystalline, has an overlap between a melting temperature range and a re-crystallization temperature range, has a particle size distribution that is substantially a Gaussian distribution, a particle shape that is substantially spherical, and has a desired melt flow rate that is less than a temperature at which the powder material begins to chemically break down (operation **1300**).

A polymer chemically breaks down when the polymer is heated, such that the chains in the polymer begin to fall apart. In particular, a long chain that is a high-strength chain in the polymer may fall apart into subscale chains called monomers. The chemical breakdown also may result in the polymer breaking down into constituent components and molecules. In other words,

the polymer chemically breaks down when the structure of the polymer begins to fall apart. The process then manufactures the part using an energy delivery system and the selected powder material (operation **1302**), with the process terminating

5 thereafter.

With reference now to **Figure 14**, a flowchart of a process for processing a polymer for use as a powder material is depicted in accordance with an advantageous embodiment. In these examples, the process illustrated in **Figure 14** may be used  
10 to manufacture a powder material such as, for example, powder material **316** for use in manufacturing part **304** in manufacturing environment **300** in **Figure 3**.

The process may begin by performing a cryo-grinding operation on pellets or other forms of the selected polymer  
15 (operation **1400**). In these illustrative examples, cryo-grinding may be performed by cooling the polymer stock to cryogenic temperatures to induce fracture rather than tearing of the material. The cryo-grinding operation may be performed to fracture the material in a manner that prevents heat generation  
20 and building of molecular weight within the polymer.

This polymer stock may take various forms. For example, the polymer stock may be in the form of pellets, beads, strips, or some other suitable form. The grinding operation is set to produce a general shape and size. The resulting particles may  
25 be either air or screen classified to obtain the correct particle distribution. Particles that are larger than the accepted range are removed, cooled, and reground. The particles that are too small for the specified particle range are removed and discarded.

30 The particles are then thermally shaped (operation **1402**). Operation **1402** may be performed by passing heated air through a column or a bed of powder at a temperature such that the particles may become spherodized by contact. The process terminates thereafter.

With reference now to **Figure 15**, a flowchart of a process for manufacturing a part is depicted in accordance with an advantageous embodiment. The process illustrated in **Figure 15** may be implemented in manufacturing environment 300 in **Figure 3**.

5 The process begins by preparing a powder material (operation 1500). The process loads the powder material into the laser sintering machine (operation 1502). The process then increments the part bed and the powder in feed stock to allow the powder distribution mechanism to apply powder for the next layer on the  
10 part bed (operation 1504).

The process may then warm the powder material (operation 1506). The warming of the powder material may occur prior to the powder being placed onto the bed of the laser sintering machine. The warming of the powder material may continue while  
15 the powder material is on the bed of the laser sintering machine. In other words, the powder material may be pre-warmed. In other advantageous embodiments, the powder material may not be warmed until placed onto the bed in the laser sintering machine.

20 Directed energy in the form of a laser beam may be applied in a pattern to the powder material on the bed (operation 1508). The application of the laser beam in a pattern onto the powder material may melt and/or sinter the powder material into a liquid and/or molten form. This processing of the powder  
25 material may form at least a portion of the part.

A determination may be made as to whether the part is complete (operation 1510). In some cases, the part may require a single pass of the laser beam. In other advantageous embodiments, additional passes may be required to complete the  
30 part, depending on the geometry and size of the part. If the part is not complete, the process returns to operation 1502 as described above.

If the part is complete, the process then cools the part down (operation **1512**), the part is removed (operation **1514**), with the process terminating thereafter.

The flowcharts and block diagrams in the different depicted  
5 embodiments illustrate the architecture, functionality, and operation of some possible implementations of apparatus and methods for manufacturing parts, objects, and/or products. In this regard, each block in the flowchart or block diagrams may represent a module, segment, step, operation, or a portion  
10 thereof for implementing a specified function or functions. In some alternative implementations, the function or functions noted in the block may occur out of the order noted in the figures. For example, in some cases, two blocks shown in succession may be executed substantially concurrently, or the  
15 blocks may sometimes be executed in the reverse order, depending upon the functionality involved.

Thus, the different advantageous embodiments may provide a method and apparatus for manufacturing parts. At least some of the different advantageous embodiments may provide a capability  
20 to manufacture parts having a capability to operate at higher temperatures and/or lighter weight than currently available parts manufactured using a directed energy system. In the different advantageous embodiments, polymers may be selected having one or more characteristics providing a capability to  
25 manufacture a part using a directed energy system, such as a laser beam in a laser sintering machine. Further, the part also may have the desired mechanical characteristics that may be maintained during use of the part.

The different advantageous embodiments may be especially  
30 useful with manufacturing parts for use in aircraft. As discussed above, the different advantageous embodiments may provide parts capable of operating at temperatures above around 100 degrees Celsius to around 280 degrees Celsius. Further, although the different illustrative examples may be used to

create parts for these temperatures, one or more of the different advantageous embodiments also may be used to create parts for other temperature ranges.

In this manner, by selecting polymer characteristics and manufacturing polymers with the identified characteristics, the different advantageous embodiments may use these selectively laser sintered polymers in place of metals that may normally be used for parts used at temperatures of around 200 degrees Celsius and above.

The description of the different advantageous embodiments has been presented for purposes of illustration and description, and it is not intended to be exhaustive or limited to the embodiments in the form disclosed. Many modifications and variations will be apparent to those of ordinary skill in the art. Although the different advantageous embodiments have been described with respect to parts for an aircraft, other advantageous embodiments may be applied to parts for other types of objects.

For example, without limitation, other advantageous embodiments may be applied to a mobile platform, a stationary platform, a land-based structure, an aquatic-based structure, a space-based structure, and/or some other suitable object.

More specifically, the different advantageous embodiments may be applied to, for example, without limitation, a submarine, a bus, a personnel carrier, a tank, a train, an automobile, a spacecraft, a space station, a satellite, a surface ship, a power plant, a dam, a manufacturing facility, a building, and/or some other suitable object.

Further, different advantageous embodiments may provide different advantages as compared to other advantageous embodiments. The embodiment or embodiments selected are chosen and described in order to best explain the principles of the embodiments, the practical application, and to enable others of ordinary skill in the art to understand the disclosure for

various embodiments with various modifications as are suited to the particular use contemplated.

**CLAIMS**

What is claimed is:

1. A method for manufacturing parts, the method comprising:  
selecting a powder material that is comprised of a polymer  
5 that is a semi-crystalline, has an overlap between a melting  
temperature range and a crystallization temperature range, has a  
particle size distribution that is substantially a Gaussian  
distribution, has a particle shape that is substantially  
spherical, and has a desired melt flow rate that is less than a  
10 temperature at which the powder material begins to chemically  
break down to form a selected powder material; and  
manufacturing a part using an energy delivery system and  
the selected powder material.
2. The method of claim 1, wherein the manufacturing step  
15 comprises:  
directing a laser beam to the powder material at specified  
points in space at a level sufficient to manufacture a part.
3. The method of claim 2, wherein the directing step is  
performed using a selective laser sintering process.
- 20 4. The method of claim 2, further comprising:  
heating a bed surface on which the powder material is  
heated from at least 220 degrees to around 330 degrees Celsius.
5. The method of claim 1, wherein the part is manufactured in  
an environment in which a thermal gradient of less than around  
25 10 degrees Celsius per inch is present in a location where the  
part is manufactured.
6. The method of claim 1, further comprising:  
heating a bed surface on which the powder material is  
heated from at least 220 degrees to around 330 degrees Celsius,  
30 wherein the part is manufactured in an environment in which an

oxygen level is less than around one percent, and wherein the part is manufactured in an environment in which a thermal gradient of less than around 10 degrees Celsius per inch is present on the bed surface.

5     7.     The method of claim 1, wherein the particle size distribution is from around 20 micrometers to around 130 micrometers with an average particle size between around 50 micrometers to around 80 micrometers.

8.     The method of claim 1, wherein the desired melt flow rate  
10    that can be achieved is around 15 grams/10 minutes to around 40 grams/10 minutes.

9.     The method of claim 1 further comprising:  
       grinding a polymer material to fracture the polymer  
material into the particle size distribution at a temperature  
15    that avoids heat generation that builds molecular weight.

10.    The method of claim 9, wherein the grinding step is performed using cryo-grinding.

11.    The method of claim 9, further comprising:  
       heating the polymer material after the grinding step to  
20    form the particle shape that is substantially spherical in shape.

12.    The method of claim 1, wherein the polymer is selected from one of nylon 66, a polyphenylene sulfide, a polyetherkeytinekeytone, a nylon 66 blend, a polyphenylene  
25    sulfide blend, and a polyetherkeytinekeytone blend.

13.    The method of claim 1, wherein the part is for an object selected from one of a mobile platform, a stationary platform, a land-based structure, an aquatic-based structure, a space-based structure, an aircraft, a surface ship, a tank, a personnel  
30    carrier, a train, a spacecraft, a space station, a satellite, a

submarine, an automobile, a power plant, a bridge, a dam, a manufacturing facility, and a building.

14. The method of claim 1, wherein the powder material further comprises a blend of a polymer with at least one addition of

5 glass beads, hollow glass spheres, glass fibers, carbon fibers, other polymers, minerals, clays, flame-retardant additives, and color additives.

15. An apparatus comprising:

10 a powder material that is comprised of a polymer that is semi-crystalline, has an overlap between a melting temperature range and a crystallization temperature range, has a size particle distribution that is substantially a Gaussian distribution, a particle shape that is substantially spherical, and has a desired melt flow rate that is less than a temperature  
15 at which the powder material begins to break down to form a selected powder material; and

a laser sintering machine capable of manufacturing a part using the powder material.

1/11

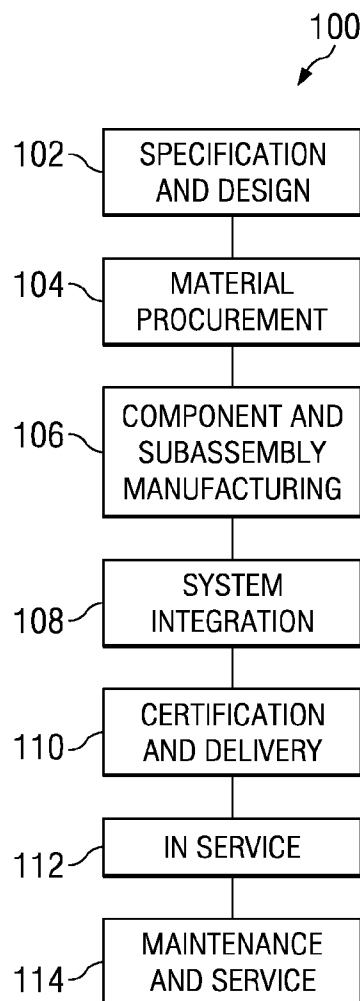


FIG. 1

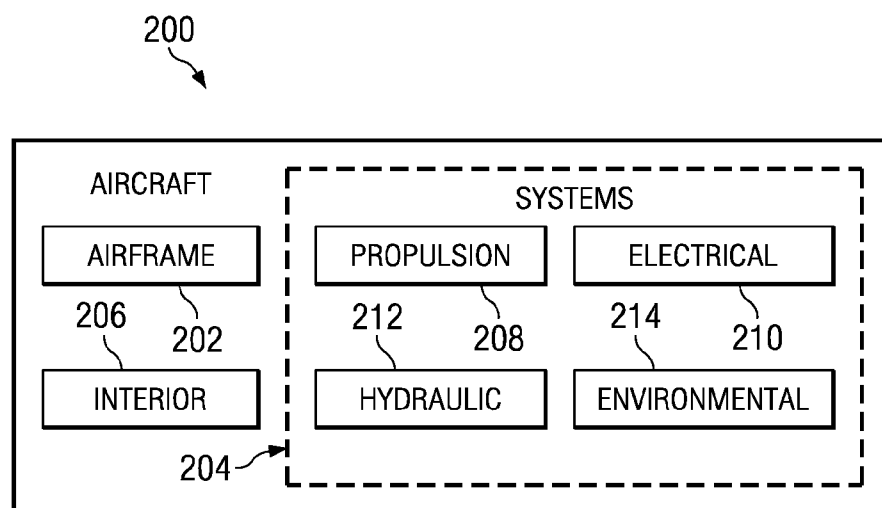


FIG. 2

2/11

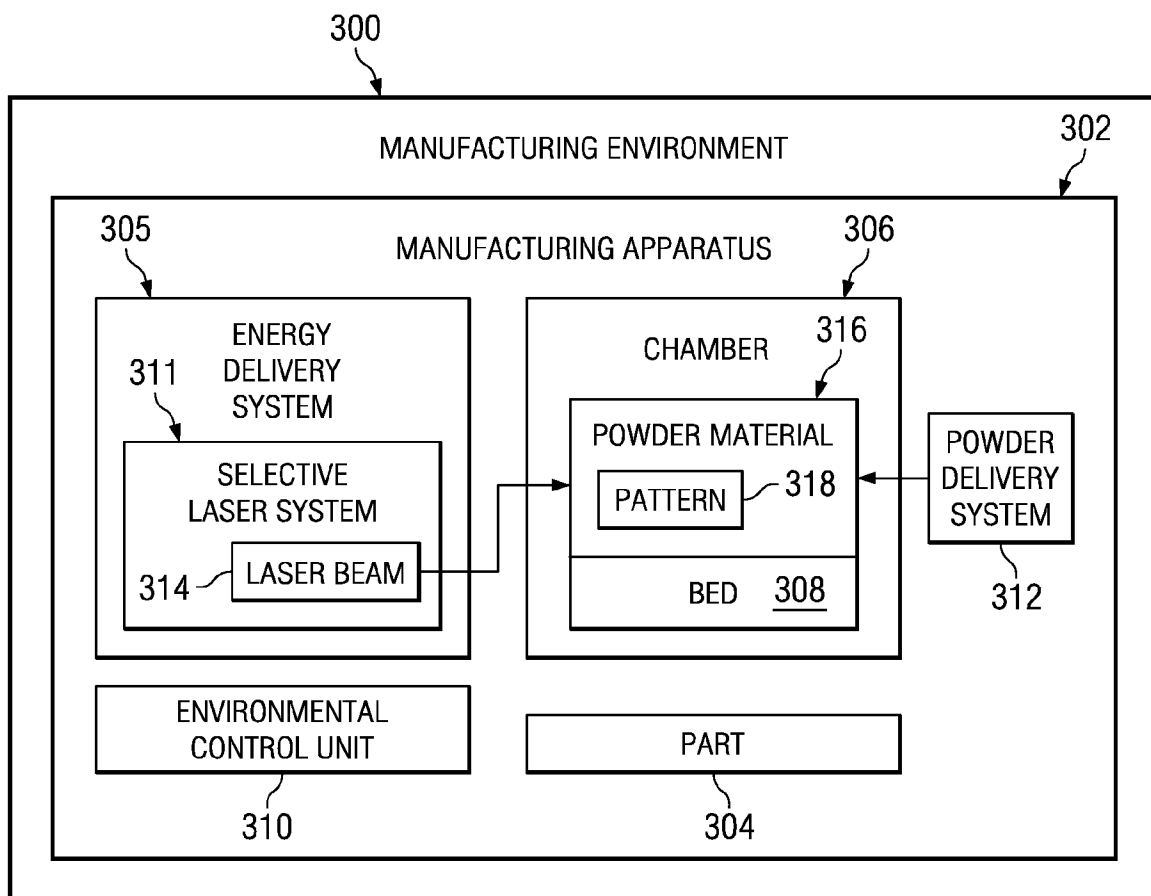


FIG. 3

3/11

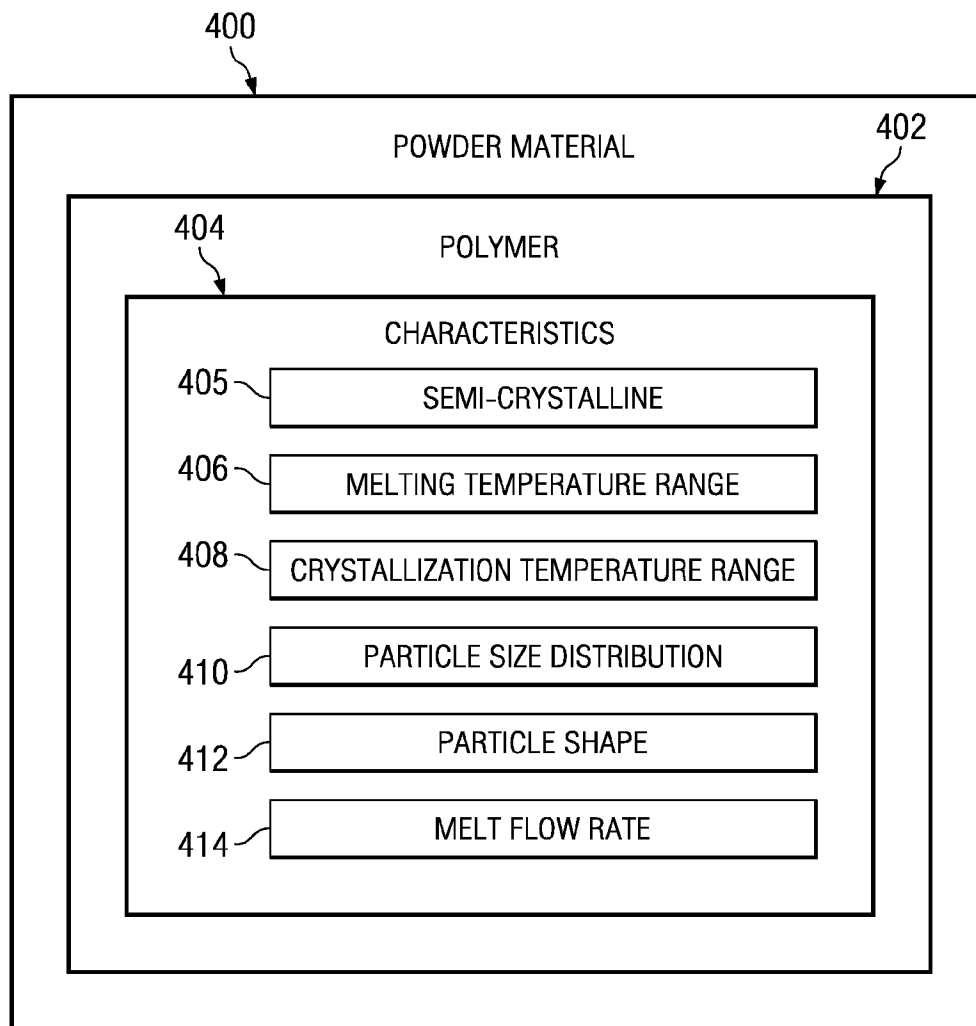


FIG. 4

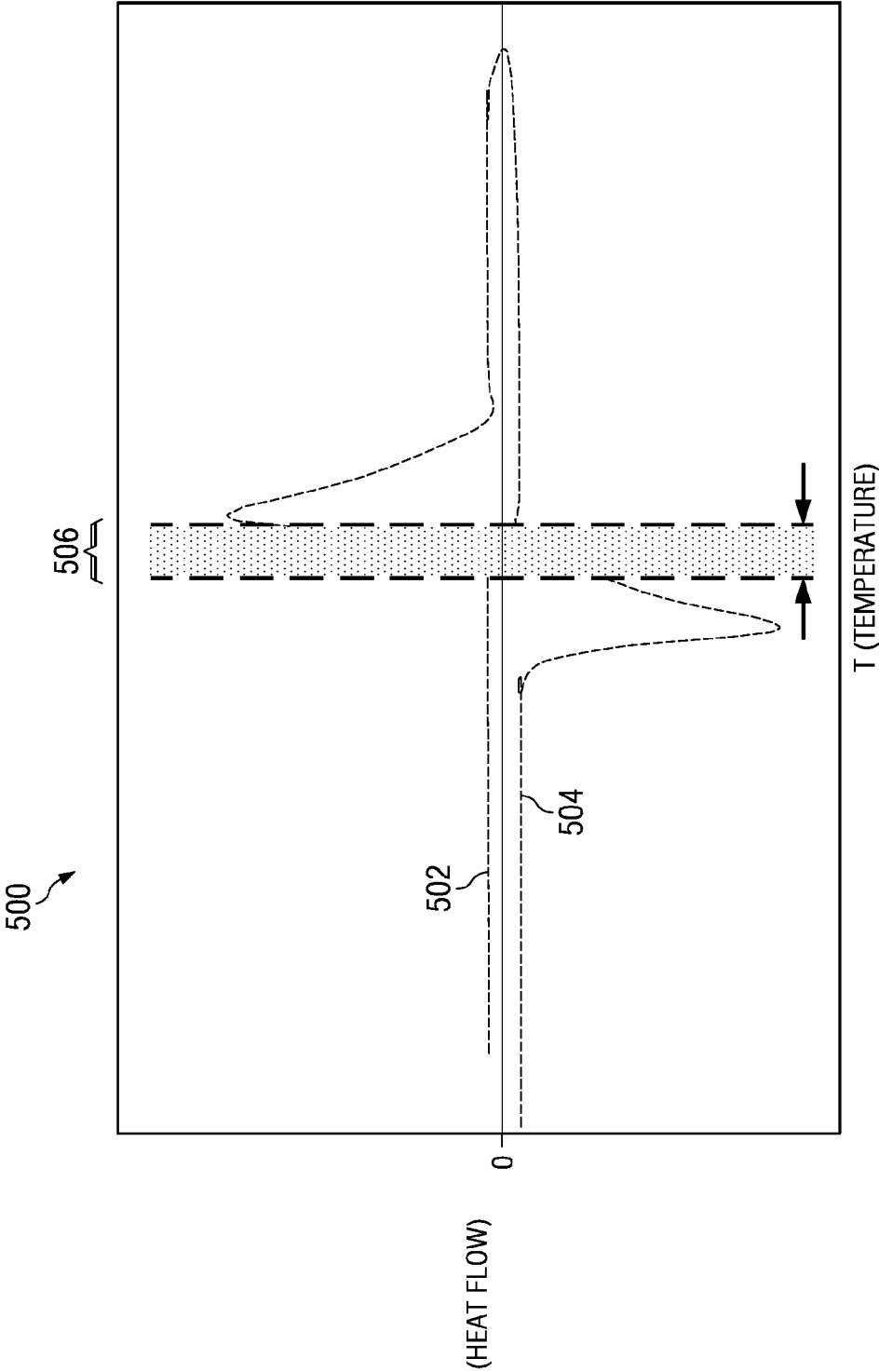


FIG. 5

5/11

600

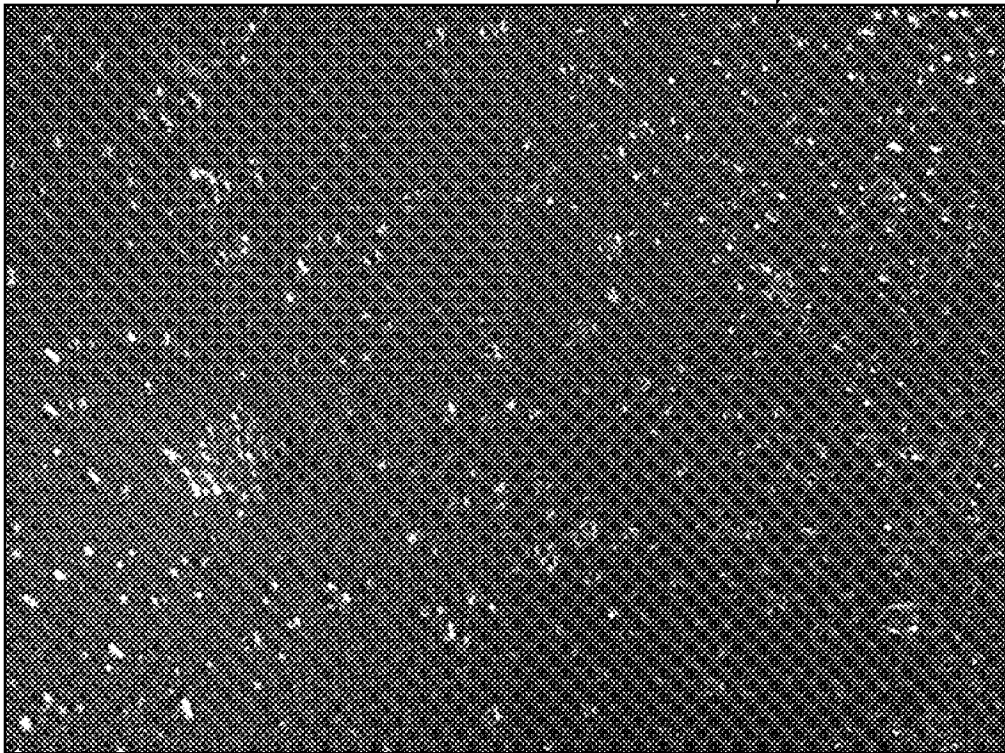


*FIG. 6*

700

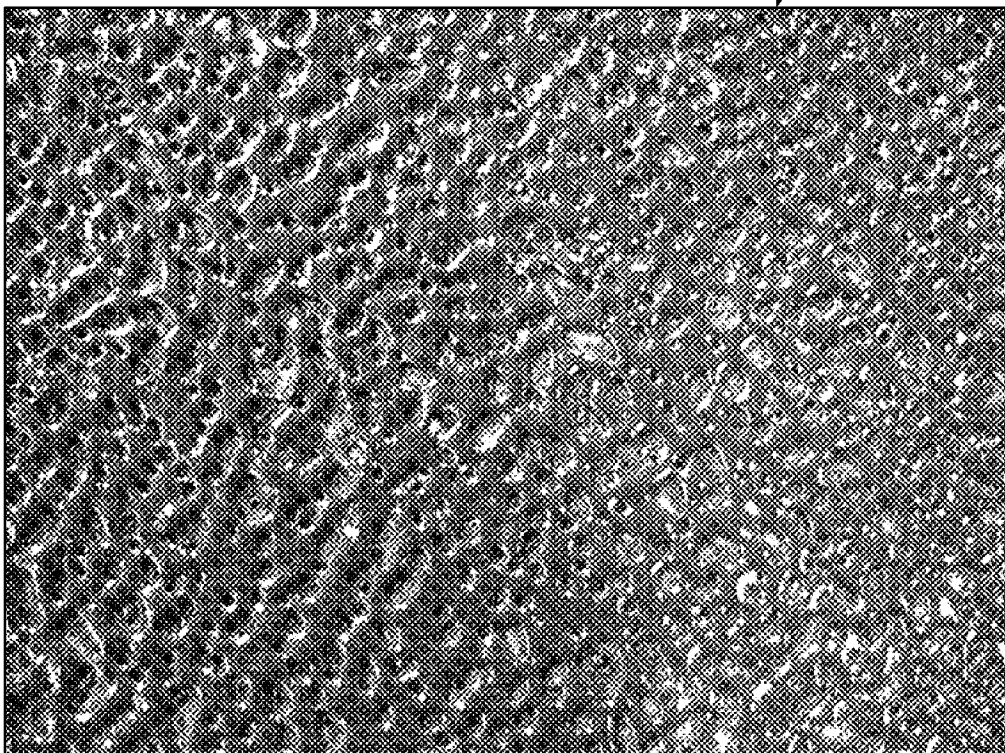


*FIG. 7*

800



6/11

FIG. 8

| PARAMETER                         | WARM-UP | BUILD  | COOL-DOWN | PARAMETER TYPE |
|-----------------------------------|---------|--------|-----------|----------------|
| CHAMBER AIRFLOW DAMPER POSITION   | 100     | 100    | 100       | BUILD          |
| DOWNDRAFT ENABLED                 | 0       | 0      | 0         | BUILD          |
| CUSTOM DOWNDRAFT ENABLED          | 0       | 0      | 0         | BUILD          |
| LEFT FEED DISTANCE                | 0.0110  | 0.0120 | 0.0110    | BUILD          |
| LEFT FEED HEATER OUTPUT LIMIT     | 60      | 60     | 60-0      | BUILD          |
| LEFT FEED HEATER SET POINT        | 91-115  | 115    | 115-15    | BUILD          |
| LEFT FEED HEATER WAIT FOR TEMP    | 1-0     | 0      | 0         | BUILD          |
| MINIMUM LAYER TIME                | 40-20   | 20     | 10        | BUILD          |
| PART CYLINDER HEATER ENABLED      | 1       | 1      | 1-0       | BUILD          |
| PART CYLINDER HEATER OUTPUT LIMIT | 100     | 100    | 100       | BUILD          |
| PART CYLINDER HEATER SET POINT    | 190     | 190    | 190-100   | BUILD          |
| PART HEATER OUTPUT LIMIT          | 35      | 35     | 35-0      | BUILD          |
| PART HEATER SET POINT             | 200-270 | 270    | 270-35    | BUILD          |
| PART HEATER WAIT FOR TEMP         | 0       | 0      | 0-1       | BUILD          |
| PART HEATER INNER/OUTER RATIO     | 1       | 1      | 1         | BUILD          |
| PISTON HEATER ENABLE              | 0       | 0      | 0         | BUILD          |
| PART HEATER OUTPUT LIMIT          | 50      | 50     | 50        | BUILD          |
| PISTON HEATER SET POINT           | 130-180 | 180    | 175-30    | BUILD          |
| POWDER LAYER DELAY                | 0       | 7      | 0         | BUILD          |
| POWDER LAYER THICKNESS            | 0.005   | 0.005  | 0.005     | BUILD          |
| RIGHT FEED DISTANCE               | 0.0110  | 0.0120 | 0.0110    | BUILD          |
| RIGHT FEED HEATER OUTPUT LIMIT    | 60      | 60     | 60-0      | BUILD          |
| RIGHT FEED HEATER SET POINT       | 91-115  | 115    | 115-15    | BUILD          |
| RIGHT FEED HEATER WAIT FOR TEMP   | 1-0     | 0      | 0         | BUILD          |
| ROLLER SPEED                      | 7.0     | 7.0    | 7.0       | BUILD          |
| ROTATE SCAN ORDER                 | 0       | 0      | 0         | BUILD          |
| VECTOR BLOOM ELIMINATION          | 1       | 1      | 1         | BUILD          |
|                                   |         |        |           |                |
| FILL LASER POWER                  | N/A     | 55.0   | N/A       | PART           |
| FILL SCAN COUNT                   | N/A     | 1      | N/A       | PART           |
| FILL BEAM OFFSET X                | N/A     | 0.0145 | N/A       | PART           |
| FILL BEAM OFFSET Y                | N/A     | 0.0150 | N/A       | PART           |
| OUTLINE LASER POWER               | N/A     | 10     | N/A       | PART           |
| OUTLINE SCAN COUNT                | N/A     | 1      | N/A       | PART           |
| OUTLINE BEAM OFFSET X             | N/A     | 0.0135 | N/A       | PART           |
| OUTLINE BEAM OFFSET Y             | N/A     | 0.0130 | N/A       | PART           |
| SLICER FILL SCAN SPACING          | N/A     | 0.010  | N/A       | PART           |
| SORTED FILL ENABLE                | N/A     | 1      | N/A       | PART           |

900  
↙

7/11

*FIG. 9*

| PARAMETER                         | WARM-UP | BUILD  | COOL-<br>DOWN | PARAMETER<br>TYPE |
|-----------------------------------|---------|--------|---------------|-------------------|
| CHAMBER AIRFLOW DAMPER POSITION   | 100     | 100    | 100           | BUILD             |
| DOWNDRAFT ENABLED                 | 0       | 0      | 0             | BUILD             |
| CUSTOM DOWNDRAFT ENABLED          | 0       | 0      | 0             | BUILD             |
| LEFT FEED DISTANCE                | 0.0110  | 0.0120 | 0.0110        | BUILD             |
| LEFT FEED HEATER OUTPUT LIMIT     | 60      | 60     | 60-0          | BUILD             |
| LEFT FEED HEATER SET POINT        | 91-119  | 119    | 119-15        | BUILD             |
| LEFT FEED HEATER WAIT FOR TEMP    | 1-0     | 0      | 0             | BUILD             |
| MINIMUM LAYER TIME                | 20-10   | 10     | 10            | BUILD             |
| PART CYLINDER HEATER ENABLED      | 1       | 1      | 1-0           | BUILD             |
| PART CYLINDER HEATER OUTPUT LIMIT | 100     | 100    | 100           | BUILD             |
| PART CYLINDER HEATER SET POINT    | 180-225 | 225    | 225-100       | BUILD             |
| PART HEATER OUTPUT LIMIT          | 35      | 35     | 35-0          | BUILD             |
| PART HEATER SET POINT             | 200-262 | 262    | 262-35        | BUILD             |
| PART HEATER WAIT FOR TEMP         | 0       | 0      | 0-1           | BUILD             |
| PART HEATER INNER/OUTER RATIO     | 1       | 1      | 1             | BUILD             |
| PISTON HEATER ENABLE              | 0       | 0      | 0             | BUILD             |
| PART HEATER OUTPUT LIMIT          | 50      | 50     | 50            | BUILD             |
| PISTON HEATER SET POINT           | 130-180 | 180    | 175-30        | BUILD             |
| POWDER LAYER DELAY                | 0       | 7      | 0             | BUILD             |
| POWDER LAYER THICKNESS            | 0.005   | 0.005  | 0.005         | BUILD             |
| RIGHT FEED DISTANCE               | 0.0110  | 0.0120 | 0.0110        | BUILD             |
| RIGHT FEED HEATER OUTPUT LIMIT    | 60      | 60     | 60-0          | BUILD             |
| RIGHT FEED HEATER SET POINT       | 91-119  | 119    | 119-15        | BUILD             |
| RIGHT FEED HEATER WAIT FOR TEMP   | 1-0     | 0      | 0             | BUILD             |
| ROLLER SPEED                      | 7.0     | 7.0    | 7.0           | BUILD             |
| ROTATE SCAN ORDER                 | 0       | 0      | 0             | BUILD             |
| VECTOR BLOOM ELIMINATION          | 1       | 1      | 1             | BUILD             |
|                                   |         |        |               |                   |
| FILL LASER POWER                  | N/A     | 28.0   | N/A           | PART              |
| FILL SCAN COUNT                   | N/A     | 1      | N/A           | PART              |
| FILL BEAM OFFSET X                | N/A     | 0.0145 | N/A           | PART              |
| FILL BEAM OFFSET Y                | N/A     | 0.0150 | N/A           | PART              |
| OUTLINE LASER POWER               | N/A     | 10     | N/A           | PART              |
| OUTLINE SCAN COUNT                | N/A     | 1      | N/A           | PART              |
| OUTLINE BEAM OFFSET X             | N/A     | 0.0135 | N/A           | PART              |
| OUTLINE BEAM OFFSET Y             | N/A     | 0.0130 | N/A           | PART              |
| SLICER FILL SCAN SPACING          | N/A     | 0.010  | N/A           | PART              |
| SORTED FILL ENABLE                | N/A     | 1      | N/A           | PART              |

1000  
↙

8/11

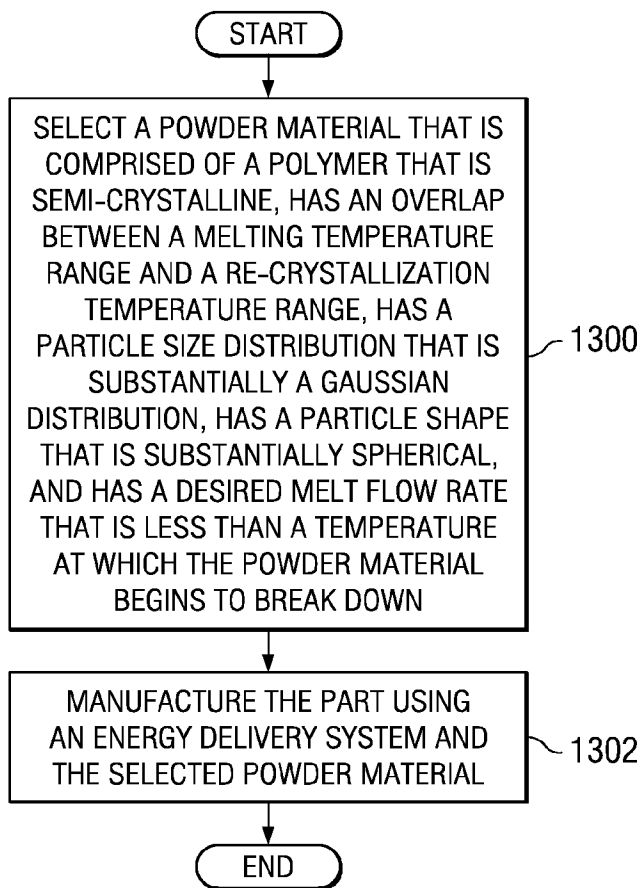
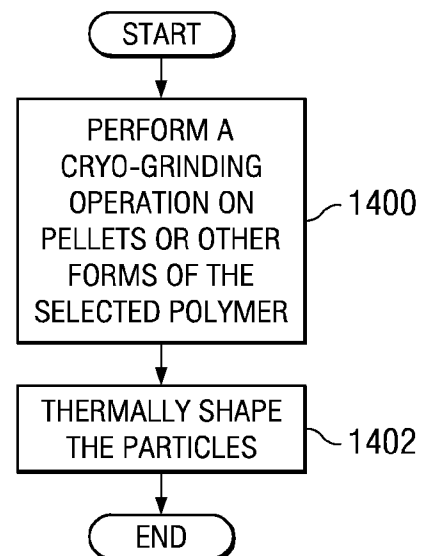
*FIG. 10*

| PARAMETER                         | WARM-UP | BUILD  | COOL-<br>DOWN | PARAMETER<br>TYPE |
|-----------------------------------|---------|--------|---------------|-------------------|
| CHAMBER AIRFLOW DAMPER POSITION   | 100     | 100    | 100           | BUILD             |
| DOWNDRAFT ENABLED                 | 0       | 0      | 0             | BUILD             |
| CUSTOM DOWNDRAFT ENABLED          | 0       | 0      | 0             | BUILD             |
| LEFT FEED DISTANCE                | 0.0110  | 0.0120 | 0.0110        | BUILD             |
| LEFT FEED HEATER OUTPUT LIMIT     | 60      | 60     | 60-0          | BUILD             |
| LEFT FEED HEATER SET POINT        | 91-119  | 119    | 119-15        | BUILD             |
| LEFT FEED HEATER WAIT FOR TEMP    | 1-0     | 0      | 0             | BUILD             |
| MINIMUM LAYER TIME                | 20-10   | 10     | 10            | BUILD             |
| PART CYLINDER HEATER ENABLED      | 1       | 1      | 1-0           | BUILD             |
| PART CYLINDER HEATER OUTPUT LIMIT | 100     | 100    | 100           | BUILD             |
| PART CYLINDER HEATER SET POINT    | 180-225 | 225    | 225-100       | BUILD             |
| PART HEATER OUTPUT LIMIT          | 35      | 35     | 35-0          | BUILD             |
| PART HEATER SET POINT             | 200-262 | 262    | 262-35        | BUILD             |
| PART HEATER WAIT FOR TEMP         | 0       | 0      | 0-1           | BUILD             |
| PART HEATER INNER/OUTER RATIO     | 1       | 1      | 1             | BUILD             |
| PISTON HEATER ENABLE              | 0       | 0      | 0             | BUILD             |
| PART HEATER OUTPUT LIMIT          | 50      | 50     | 50            | BUILD             |
| PISTON HEATER SET POINT           | 130-180 | 180    | 175-30        | BUILD             |
| POWDER LAYER DELAY                | 0       | 7      | 0             | BUILD             |
| POWDER LAYER THICKNESS            | 0.005   | 0.005  | 0.005         | BUILD             |
| RIGHT FEED DISTANCE               | 0.0110  | 0.0120 | 0.0110        | BUILD             |
| RIGHT FEED HEATER OUTPUT LIMIT    | 60      | 60     | 60-0          | BUILD             |
| RIGHT FEED HEATER SET POINT       | 91-119  | 119    | 119-15        | BUILD             |
| RIGHT FEED HEATER WAIT FOR TEMP   | 1-0     | 0      | 0             | BUILD             |
| ROLLER SPEED                      | 7.0     | 7.0    | 7.0           | BUILD             |
| ROTATE SCAN ORDER                 | 0       | 0      | 0             | BUILD             |
| VECTOR BLOOM ELIMINATION          | 1       | 1      | 1             | BUILD             |
|                                   |         |        |               |                   |
| FILL LASER POWER                  | N/A     | 28.0   | N/A           | PART              |
| FILL SCAN COUNT                   | N/A     | 1      | N/A           | PART              |
| FILL BEAM OFFSET X                | N/A     | 0.0145 | N/A           | PART              |
| FILL BEAM OFFSET Y                | N/A     | 0.0150 | N/A           | PART              |
| OUTLINE LASER POWER               | N/A     | 10     | N/A           | PART              |
| OUTLINE SCAN COUNT                | N/A     | 1      | N/A           | PART              |
| OUTLINE BEAM OFFSET X             | N/A     | 0.0135 | N/A           | PART              |
| OUTLINE BEAM OFFSET Y             | N/A     | 0.0130 | N/A           | PART              |
| SLICER FILL SCAN SPACING          | N/A     | 0.010  | N/A           | PART              |
| SORTED FILL ENABLE                | N/A     | 1      | N/A           | PART              |

9/11

1100

|      | MATERIAL | ULTIMATE<br>TENSILE<br>STRENGTH (psi) | 0.2% OFFSET YIELD<br>STRENGTH (psi) | % ELONGATION | MELT<br>POINT<br>(°C) |
|------|----------|---------------------------------------|-------------------------------------|--------------|-----------------------|
| 1102 | PEKK     | 10100                                 | 9700                                | 1.9          | 310                   |
| 1104 | PPS      | 5200                                  | 5125                                | 1.5          | 280                   |
| 1106 | NYLON 66 | 10200                                 | 7500                                | 4            | 254                   |
| 1108 | NYLON 12 | 6600                                  | 2800                                | 16           | 187                   |
| 1110 | NYLON 11 | 7000                                  | 3050                                | 22           | 186                   |

*FIG. 11**FIG. 13**FIG. 14*

10/11

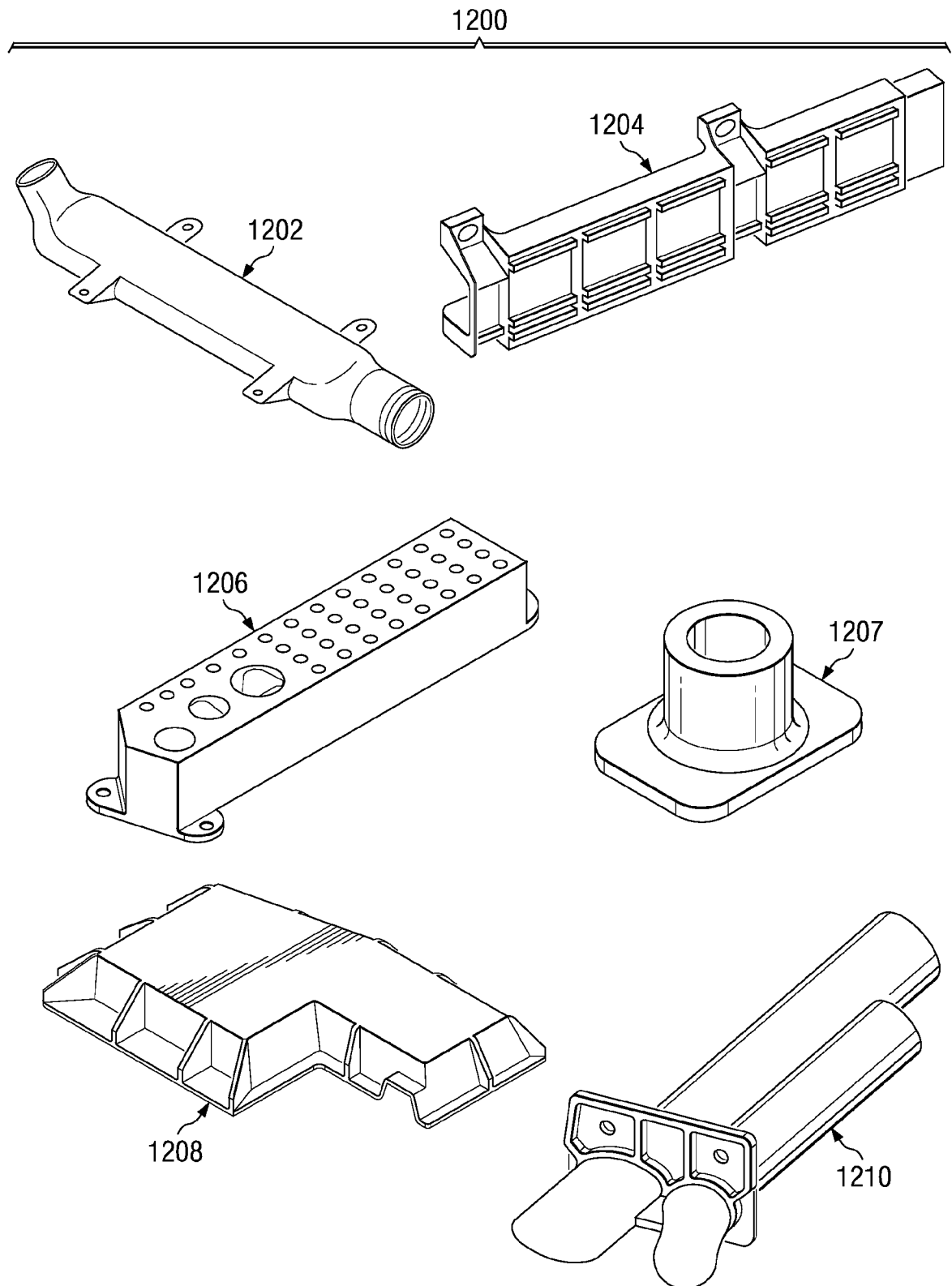


FIG. 12

11/11

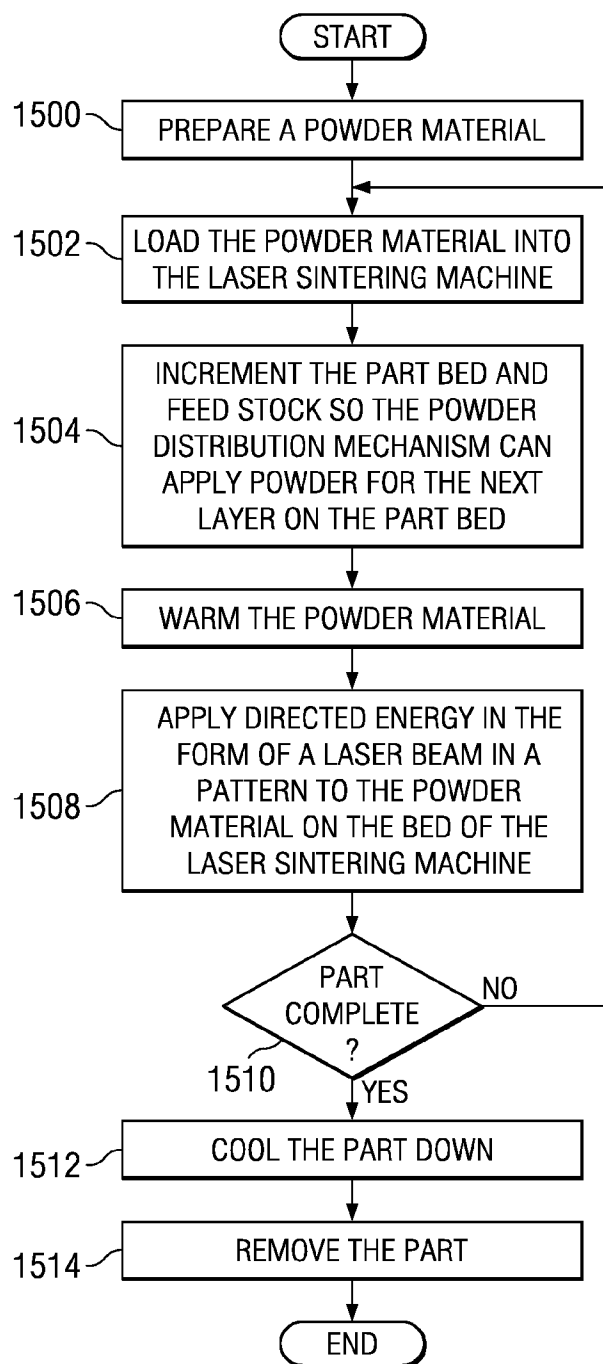


FIG. 15