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(54) Title: A WRAPPER TUBE FOR A FUEL SUBASSEMBLY OF A NUCLEAR REACTOR CORE AND METHOD FOR PROTECTING FUEL AGAINST OVERHEATING IN CASE OF COOLANT BOILING

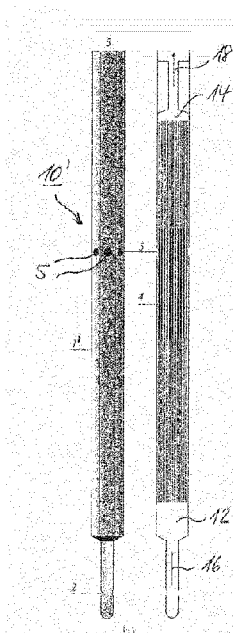


Fig. 1. Schematic view of a sodium-cooled fast reactor fuel subassembly with traditional (a) and modified (b) design of the wrapper tube

(57) Abstract: The present invention discloses an innovative design of the sodium-cooled fast reactor subassembly wrapper tube (Figure 1 (b)) and a method for protecting the sodium-cooled fast reactor core against overheating and melting in case of the accidents accompanied by a sodium boiling. More generally, the invention is considered to be valuable in any field of technology where a heat generating fuel, heater or the like need to be cooled sufficiently to prevent the resources involved from damage caused by overheating and/or melting. The innovation of the wrapper tube design compared to the traditional wrapper tube design of a sodium-cooled fast reactor fuel subassembly (Figure 1 (a)) consists in an introduction of openings (5). The openings are made in all faces of the wrapper tubes of all fuel subassemblies at the same axial location. The goal of the openings (5) is to provide the sodium flow bypass between the neighbouring subassemblies, in the case when the sodium vapour obstructs or fully blocks the liquid sodium flow at the top of the fuel subassembly (i.e. above the axial level of the openings). Due to this bypass, the sodium flow rate at the inlet of the subassembly, where the boiling occurs, does not significantly drop (Figure 2 (b)). As a result, the sodium vapour does not propagate downwards to the core centre, where the void reactivity coefficient is positive, but rather in radial direction from one channel to another, being always kept in the region of low or even negative void reactivity coefficient. Moreover, the availability of the sodium flow rate through the subassembly, where boiling occurs, is beneficial for preventing the cladding dryout, because a part of sodium will flow through the boiling region in the form of a liquid film on the surface of the claddings.

A wrapper tube for a fuel subassembly of a nuclear reactor core and method for protecting fuel against overheating in case of coolant boiling

5 The invention relates to a wrapper tube for a fuel subassembly of a nuclear reactor core, preferably used in a sodium-cooled fast reactor. Further, the present invention relates to a method for protecting fuel against overheating and melting in case of an accidental coolant boiling in a nuclear reactor,
10 such as a sodium-cooled fast reactor. Furthermore, the present invention relates to a reactor core assembled from a number of fuel subassemblies comprising in the wrapper tubes.

The present invention is aimed at improving the response of a
15 nuclear reactor core to the accidental situations with onset of the coolant boiling, such as sodium boiling, in the fuel rod bundle. More generally, the invention is considered to be valuable in any field of technology where a heat generating fuel, heater or the like need to be cooled sufficiently to
20 prevent the resources involved from damage caused by overheating and/or melting due to a boiling of a coolant.

Considering a reference example, the sodium-cooled fast reactor is an innovative nuclear reactor system which - due to
25 the fast neutron spectrum - has a potential to operate with only natural uranium as a feed fuel and to have only products of fission as a waste. Provided that the corresponding fuel cycle is developed, the already available resources of the natural uranium can make such a reactor a sustainable and safe
30 source of energy for centuries, producing a waste in a compact and controllable form.

The core of the sodium-cooled fast reactor is a device where the nuclear fission and heat generation occur. The core -
35 depending on the reactor power - can be assembled from several hundreds of fuel subassemblies oriented vertically. A typical fuel subassembly 10 as shown in Figure 1(a) of a not shown sodium-cooled fast reactor typically comprises a bundle of a

few hundreds of fuel rods 4 arranged in a triangular (hexagonal) lattice and enclosed in a wrapper tube 1 of a hexagonal cross-sectional area with openings 2 and 3 at the bottom and the top of the fuel subassembly 10 to allow sodium
5 flowing according to arrows 16, 18 in and out, respectively. Every fuel rod 4 in the bundle is a column of the fuel pellets enclosed in a hermetical stainless steel tube (cladding). To accommodate gases, released from the fuel during reactor operation, empty spaces are foreseen inside the cladding tube,
10 such as upper and lower fission gas plenums 12 and 14. The subassembly includes also the upper and lower reflectors, not shown in Figure 1.

Due to the design of the wrapper tube, every subassembly of a
15 typical sodium-cooled fast reactor is isolated from each other and has its own sodium flow rate. The cold sodium from the reactor lower plenum enters the subassembly from the bottom, heats up inside and flows out from the subassembly top into the reactor upper plenum. In normal operation the sodium
20 always remains liquid.

The liquid sodium was selected as a cooling medium for the fast nuclear reactors because of its neutronic characteristics (favourable for the fast neutron energy spectrum) as well as
25 due to its thermal-hydraulic characteristics (favourable for efficient removal of heat). However, in accidental cases (e.g. in case of a failure of the pumps combined with a failure of the protection system) there is a probability that sodium at the top of the fuel bundle reaches its saturation point and
30 starts to boil. The response of the sodium-cooled fast reactor to the sodium boiling is one of the most serious challenges to be addressed while designing the core and demonstrating the reactor safety. The key phenomena challenging the integrity of the fuel rods (and, therefore, prevention of the radioactivity
35 release in the coolant) in case of sodium boiling are:
1) reactor power evolution caused by the feedback between sodium density and the neutron multiplication factor (reactivity); and

2) deterioration of the heat transfer from fuel rods to sodium due to reduction of the sodium flow rate, followed, in a worst case, by dryout of the fuel rod claddings.

5 The reactivity evolution (and, therefore, the power evolution) caused by the sodium density change is determined by a spatial distribution of the void reactivity coefficient. The void reactivity coefficient in the given core region is the change of the reactivity caused by removal of one kilogram of the sodium from this region. This coefficient in a typical sodium-cooled fast reactor core is strongly positive at the core centre and less positive or even negative at the core periphery .

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15 The sodium boiling pattern in a typical sodium-cooled fast reactor core is characterised by a fast formation of large vapour bubbles in the top part of the fuel subassembly (where the sodium is the hottest and where the void reactivity coefficient is close to zero or even negative) . These bubbles are rapidly expanding radially and, as a result, may block the flow area of the channel. This blockage leads to an abrupt stop of the coolant flow at the subassembly inlet. As a result, the stagnant sodium inside the fuel subassembly continues to boil off and the vapour propagates down towards the core centre, where the void reactivity coefficient is strongly positive, leading, therefore, to reactivity and power escalation. This process is schematically illustrated in Figure 2 (a) . The quick power escalation can lead to dryout of the fuel rod claddings and finally to the cladding and fuel melting and relocation with subsequent release of radioactivity in the coolant. This tremendous drawback can not be avoided by the disclosure of prior documents typically dealing with the design of the arrangement of the fuel rods because the designs disclosed in US-PS 4,138,318, DT 23 45 338 Al and WO 2011/045390 are not enabled to prevent a boiling front to propagate downwards (against the flow direction of the coolant) through the hot fissile zone of the fuel rods.

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It is, therefore, an objective of the present invention to provide a wrapper tube for a heat-generating fuel pin bundle, preferably for use in a sodium-cooled fast reactor fuel subassembly described above. The invention aims at reducing the impact of the coolant boiling occurring in emergency situations on the core power evolution and on the fuel cooling ability .

This objective is achieved according to the present invention by design of a wrapper tube for a heat-generating fuel pin bundle, preferably used in a sodium-cooled fast reactor, comprising :

- a) a wrapper tube having a cross-sectional area, preferably a hexagonal cross-sectional area;
- b) a number of fuel rods arranged in a regular lattice, preferably a triangular or a hexagonal lattice; a space between the fuel rods allowing a flow path for a coolant in order to remove heat generated in the fuel;
- c) a number of openings in the wrapper tube being provided as a coolant flow bypass between neighbouring subassemblies in case of a partial or total blockage of the internal flow path by a coolant vapour in one or several subassemblies, wherein said openings are provided at a level where a fuel rod fission zone is located.

This wrapper tube design, therefore, enables for a significant improvement in the operation safety of fuel rod comprising heat generating fuels. The goal of the openings is to provide the coolant flow bypath between neighbouring subassemblies in a region where the heat critical fuel rod fission zone is located, in the case when the coolant vapour obstructs or fully blocks the liquid coolant flow at the top of the fuel subassembly (i.e. above the axial level of the openings) . Due to this bypath, the coolant flow rate at the inlet of the subassemblies, in which the boiling occurs, does not significantly drop. As a result, the coolant vapour does not propagate downwards (as seen in the flow direction of the coolant) to the core centre, where the void reactivity

coefficient is positive, but rather in radial direction from one channel to another, being always kept in the region of low or even negative void reactivity coefficient.

5 The high power density required for the economic performance of the fast reactor core makes it advantageous when the fuel rods are arranged in a compact triangular (hexagonal) lattice and, therefore, the wrapper tube has a hexagonal cross-sectional area. This geometry allows forming the core from the
10 fuel subassemblies arranged in a honeycomb pattern offering six neighbours and herewith six neighbouring bypass channels for the coolant in case of a cooling problem due to "blocking" of the flow path by the coolant vapour in one or several subassemblies .

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In order to enable an easy alignment of the openings when assembling the subassemblies to the core, a preferred embodiment of the present invention may provide a solution where the openings are disposed along a circumferential ring;
20 all openings belonging to one circumferential ring being disposed substantially at the same longitudinal height.

In a further preferred embodiment with the aim to prevent the coolant vapour propagating downwards (as seen in the flow
25 direction of the coolant) to the core centre, where the void reactivity coefficient is positive, the longitudinal height of the opening may correspond to the upper half of the fuel region as seen in the flow direction of the coolant.

30 It is further advantageously when the hydraulic diameter of the six openings (one per face of the wrapper tube) accumulates to less than 50% of the total perimeter of the wrapper tube.

35 With respect to the method of protecting a nuclear reactor core against overheating and melting in case of an accidental coolant boiling, it consists, according to the present invention, in establishing the flow connections between the

neighbouring subassemblies implemented in the form of the above-described openings in the subassembly wrapper tubes, which allows achieving the above-mentioned objective.

5 With respect to the reactor core, the above-mentioned objective is achieved according to the present invention by a localizing the vapour region in the upper part of the reactor core due to liquid coolant flow in radial direction through the openings in the subassembly wrapper tubes as described
10 above.

Preferred embodiments of the present invention are hereinafter explained with reference to the attach drawings which depict in:

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Figure 1 a schematic view of a sodium-cooled fast reactor fuel subassembly with a wrapper tube according to the prior art (a) and the modified design of the wrapper tube (b) ; and

20 Figure 2 a schematic illustration of the flow pattern in case of a sodium boiling in a sodium-cooled fast reactor fuel subassembly with traditional (a) and modified (b) design of the wrapper tube. The figure shows not all subassemblies of the core, but only three neighbouring subassemblies in the
25 case when the coolant boiling starts only in one subassembly.

The innovation of the design of a modified wrapper tube subassembly 10' compared to the traditional wrapper tube subassembly 10 of a sodium-cooled fast reactor fuel
30 subassembly consists in an introduction of additional openings 5 in all faces of a modified wrapper tube 1'. Preferably, the openings 5 are made at the same axial position in the modified wrapper tubes 1' of all fuel subassemblies 10' in the core. The axial location of the openings 5 corresponds to the upper
35 half of the fuel region 6 (see Figure 1(b)) what is considered be within the region of the fuel rod fissile zone. It is very important to arrange the openings 5 in this region because of the heat generated in the fuel rods by nuclear fission. The

exact position, shape and dimension of the openings have to be determined, of course, for a specific core design by experimental investigation and numerical modelling.

- 5 As shown in Figure 2(a), in emergency situations the sodium boiling starts at the top of the fuel column, where the sodium is the hottest and where the void reactivity coefficient is close to zero or even negative, and then propagates in the direction of arrows 22 and 24 (see a boiling region 20 in
- 10 Figure 2(a)). The boiling region propagation towards the core centre, i.e. in the direction of arrow 24 in Figure 2(a), is not desirable, because the core centre is the region of highly positive void reactivity coefficient which is considered the most critical part of the fuel rod fissile zone which, of
- 15 course, extends along the total length of the fuel rods. The bubbles rapidly expanding radially block the flow area of the channel, leading to an abrupt stop of the coolant flow 33 at the subassembly inlet.
- 20 The goal of the openings 5 in the modified wrapper tube 1' is to provide a liquid sodium flow bypath (see arrows 26 and 28) between not further shown neighbouring subassemblies 10', in the case when the sodium vapour obstructs or fully blocks the liquid sodium flow at the top of the fuel subassembly (i.e.
- 25 above the axial level of the openings). Due to this bypath, the sodium flow rate 30' at the inlet of the modified fuel subassembly 10', where the boiling occurs, does not significantly drop (see Figure 2(b)). As a result, the sodium vapour does not propagate downwards (as along arrow 24 in
- 30 Figure 2(a)) to the core centre, where the void reactivity coefficient is positive, but rather in radial direction from one channel to another, being always kept in the region of low or even negative void reactivity coefficient. Moreover, the availability of the sodium flow rate 30' through the modified
- 35 fuel subassembly 10', where boiling occurs, is beneficial for preventing the cladding dryout, because a part of sodium will flow through the boiling region in the form of a liquid film on the surface of the claddings.

Therefore, the invention provides a significant improvement of the sodium-cooled fast reactor core behaviour under sodium boiling conditions through keeping the vapour generation
5 region 20 in the upper part of the core, where the void reactivity effect is close to zero or even negative. The cross-flows between neighbouring fuel assemblies 10' in normal operation have been identified to be negligible.

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Patent Claims

1. A fuel subassembly (10') of a nuclear reactor core, preferably used in a sodium-cooled fast reactor, comprising:
- 10 a) a wrapper tube having a hexagonal cross-sectional area;
b) a number of fuel rods (4) arranged in a triangular (hexagonal) lattice; a space between the fuel rods allowing a flow path for a coolant in order to remove heat generated in the fuel;
- 15 c) a number of openings in the wrapper tube being provided as a coolant flow bypass between neighbouring subassemblies in case of a partial or total blockage of the internal flow path by a coolant vapour in one or several subassemblies, wherein said openings are provided at a level where a fuel rod fission
- 20 zone is located.
2. The fuel subassembly (10') according to claim 1, characterized in that the wrapper tube (1') has a hexagonal cross-sectional area.
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3. The fuel subassembly (10') according to any of the preceding claims, characterized in that the openings (5) are disposed along a circumferential path; all openings (5) being disposed substantially at the same
- 30 longitudinal height or axial position.
4. The fuel subassembly (10') according to claim 3, characterized in that the longitudinal height of the openings (5) corresponds to the
- 35 upper half of the fuel region (6) as seen in the flow direction of the coolant.

5. The fuel subassembly (10') according to any of the preceding claims, characterized in that the hydraulic diameter of the six openings 5 (one per face of the wrapper tube) accumulates to less than 50% of the total perimeter of the wrapper tube.

6. A method for protecting a sodium-cooled fast reactor core against overheating and melting in case of an accident accompanied by sodium boiling, based on the use of the fuel subassembly (10') according to any of the preceding claims 1 to 5.

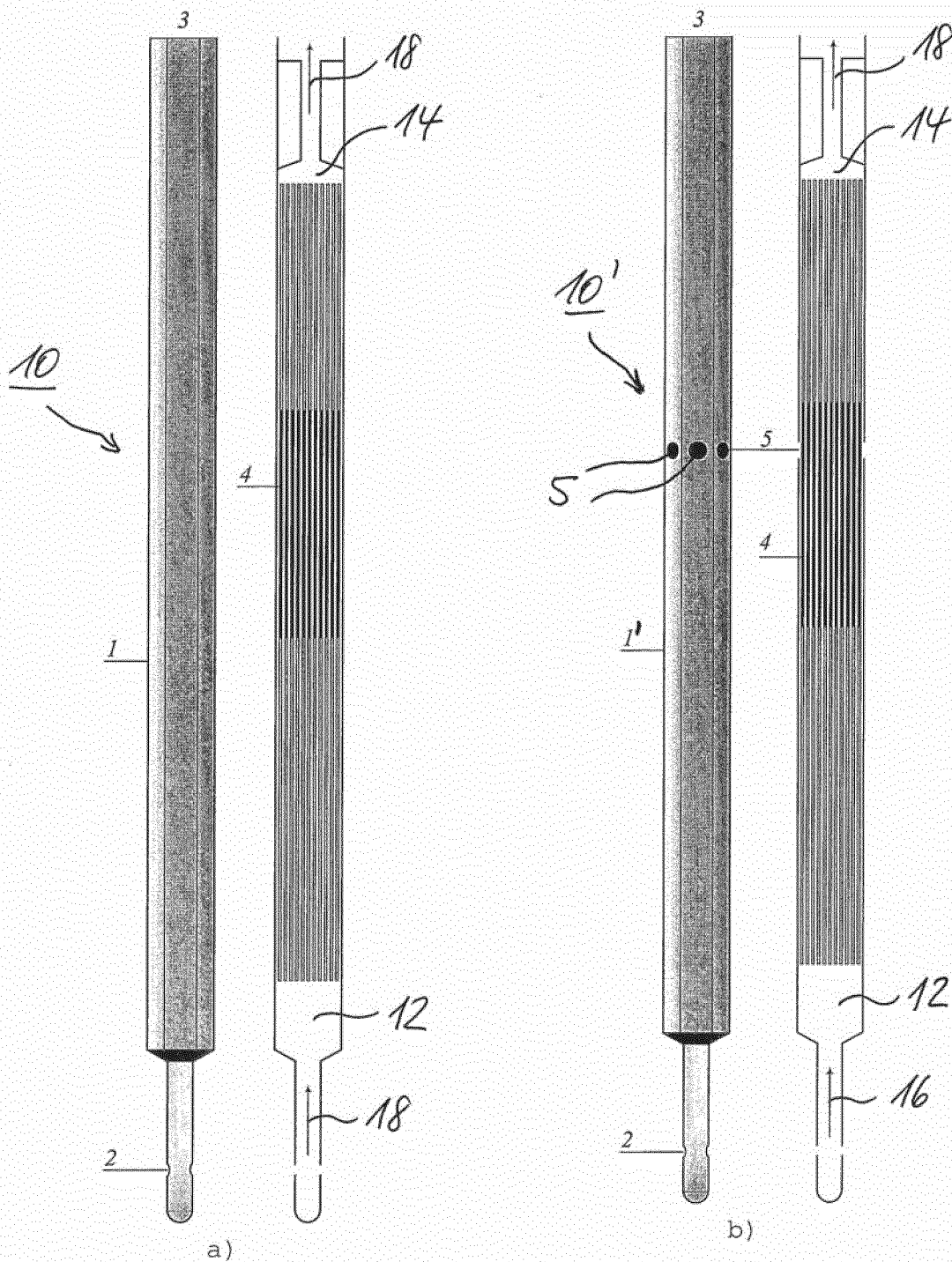


Fig. 1. Schematic view of a sodium-cooled fast reactor fuel subassembly with traditional (a) and modified (b) design of the wrapper tube

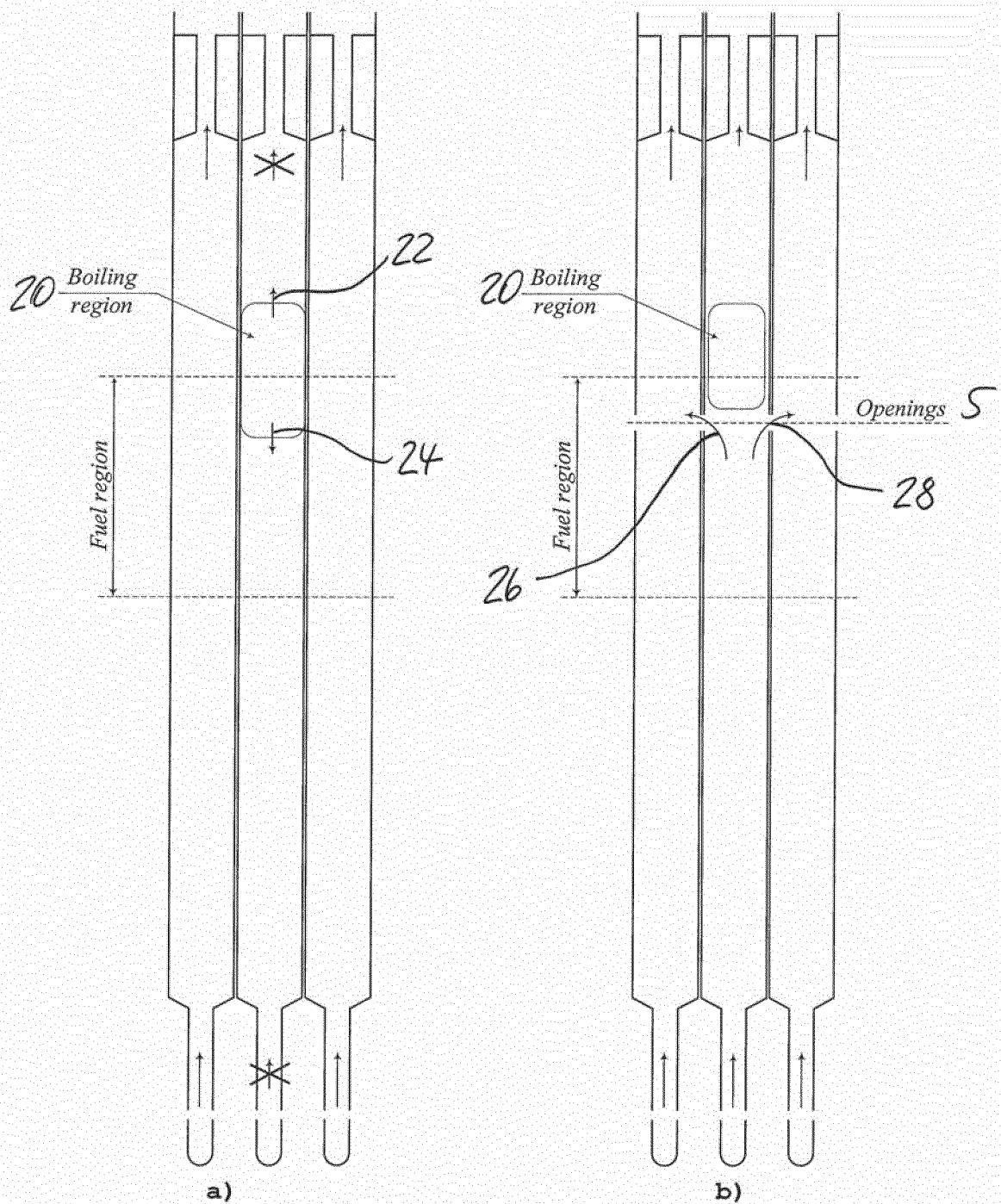


Fig. 2. Schematic illustration of the flow pattern in case of a sodium boiling in a sodium-cooled fast reactor fuel subassembly with traditional (a) and modified (b) design of the wrapper tube

INTERNATIONAL SEARCH REPORT

International application No
PCT/EP2012/075292

A. CLASSIFICATION OF SUBJECT MATTER
INV. G21C3/322 G21C3/324
ADD. G21C1/02

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
G21C

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal , COMPENDEX, INSPEC, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 4 138 318 A (SPEELMAN JAN E) 6 February 1979 (1979-02-06) abstract; figures 1,2 column 1, lines 5-14 column 2, line 44 - column 3, line 17 column 3, lines 51-60 -----	1-6
X	DE 23 45 338 Al (ILJUNIN WLADIMIR GRIGORIEWITSC; MUROGOW WIKTOR MICHAELOWITSCH; OBNINSK) 20 March 1975 (1975-03-20) figures 1-3 page 9, line 1 - page 10, line 20 ----- -/-	1-6



Further documents are listed in the continuation of Box C.



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INTERNATIONAL SEARCH REPORT

International application No
PCT/EP2012/075292

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	wo 2011/045390 AI (COMMISSARIAT ENERGIE ATOMIQUE [FR] ; JEANNE THIERRY [FR]) 21 April 2011 (2011-04-21) abstract; figure 1 page 1, lines 6-11 page 15, line 15 - page 16, line 7 page 16, lines 25-30 page 17, line 19 - page 18, line 20 -----	1, 2, 4
A	US 2011/261921 AI (KOGA TOMONARI [JP] ET AL) 27 October 2011 (2011-10-27) abstract; figures 1-5 paragraphs [0002] , [0055] - [0059] -----	1-6

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/EP2012/075292

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 4138318	A	06-02-1979	NONE
DE 2345338	AI	20- 03-1975	NONE
wo 2011045390	AI	21- 04-2011	CN 102576571 A 11-07-2012
			EP 2489043 AI 22-08-2012
			FR 2951578 AI 22-04-2011
			KR 20120092636 A 21-08-2012
			US 2012201342 AI 09-08-2012
			wo 2011045390 AI 21-04-2011
US 2011261921	AI	27-10-2011	JP 4559965 B2 13-10-2010
			JP 2007178177 A 12-07-2007
			US 8040998 BI 18-10-2011