

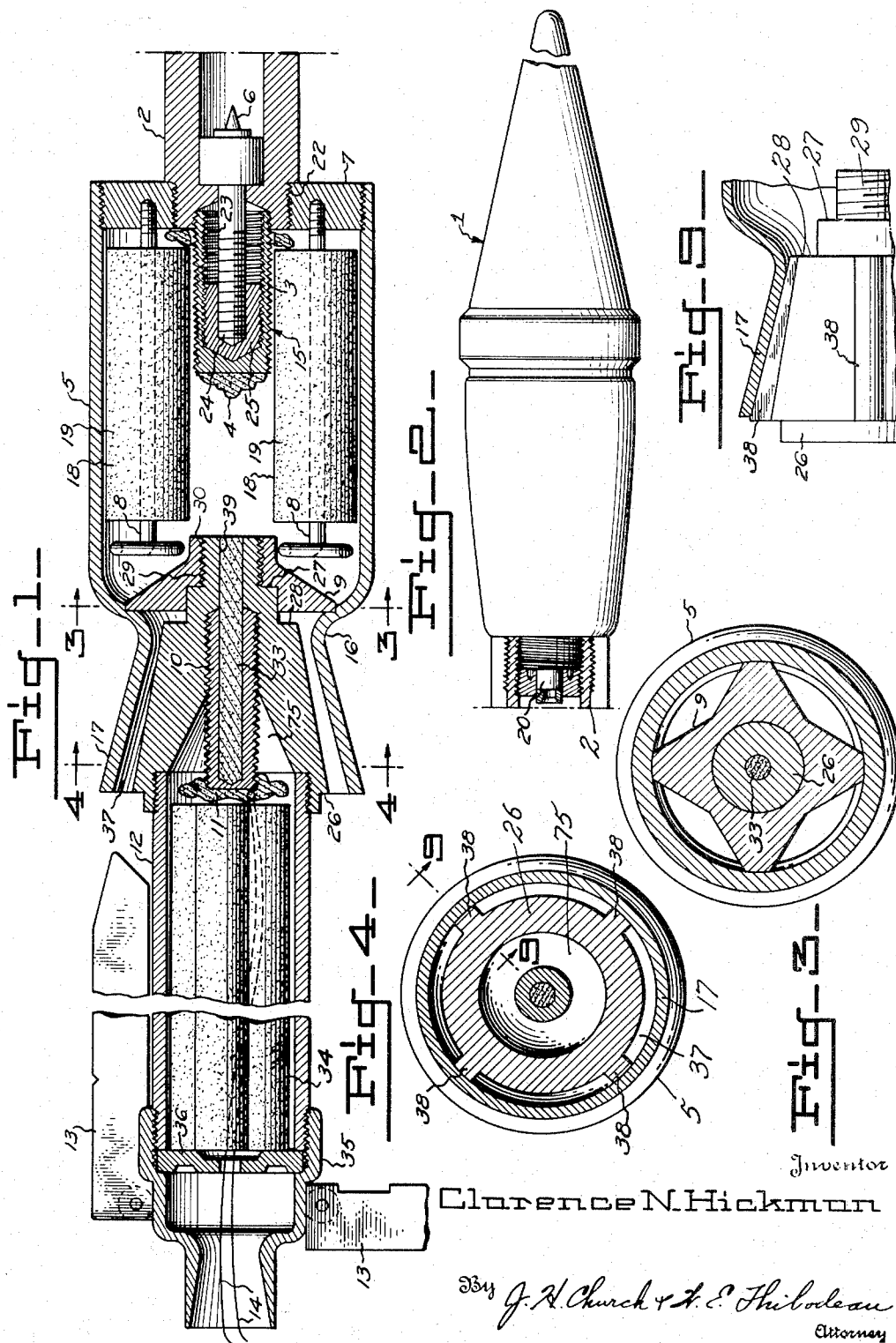
Nov. 22, 1955

C. N. HICKMAN
ROCKET PROJECTILE HAVING DISCRETE FLIGHT
INITIATING AND SUSTAINING CHAMBERS

2,724,237

Filed March 5, 1946

2 Sheets-Sheet 1



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Fig-5-

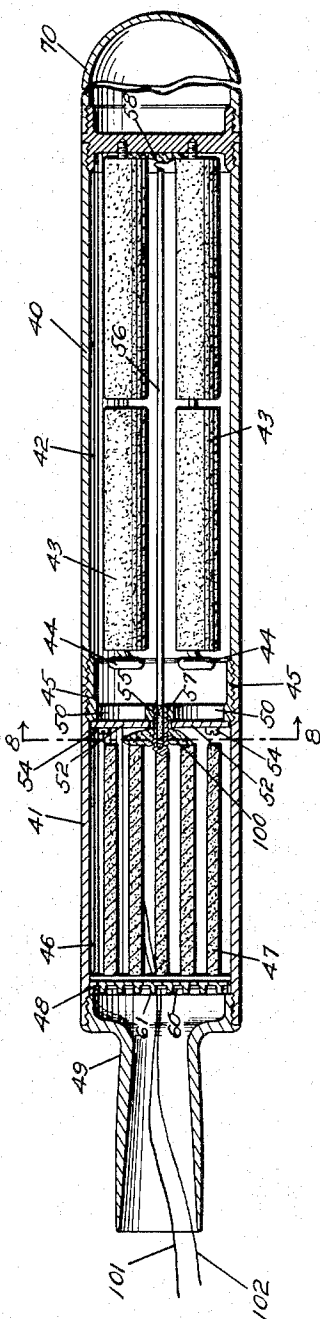


Fig-6-

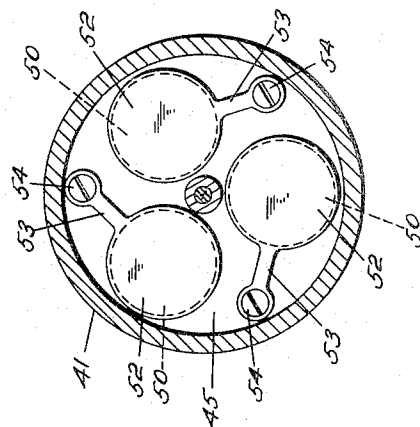


Fig-7-

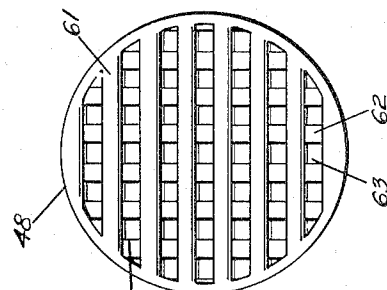
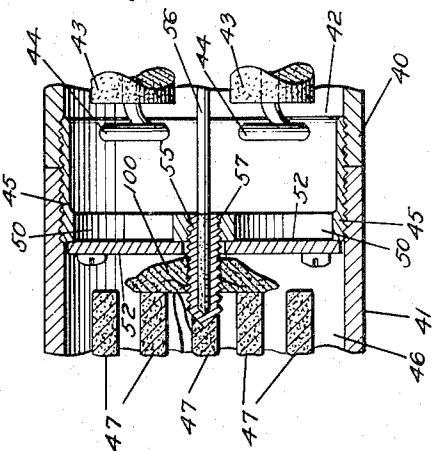


Fig-8-



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1

2,724,237

ROCKET PROJECTILE HAVING DISCRETE FLIGHT INITIATING AND SUSTAINING CHAMBERS

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Application March 5, 1946, Serial No. 652,206

2 Claims. (Cl. 60—35.6)

(Granted under Title 35, U. S. Code (1952), sec. 266)

The invention described herein may be manufactured and used by or for the Government for governmental purposes, without the payment to me of any royalty thereon.

This invention relates to rocket propelled projectiles and more particularly to rocket propelled projectiles which are adapted to be fired from projectors held in the hands of ground troops.

One of the foremost obstacles to be overcome in perfecting this type of rocket propelled projectile is that of eliminating the presence of a blast from the jet, after the rocket has left the projector, without causing a material reduction in the rocket's final velocity. The presence of this jet blast is a serious source of annoyance to the firing personnel who must be stationed, during firing, at a position to the rear of the muzzle of the projector and in the direction of the line of flight of the rocket. Attempts have been made to protect the firing personnel from the effects of the jet blast by providing a disc shaped shield at the muzzle of the projector. It was found, however, that excessive recoil forces were produced by the gases of combustion striking the shield. Consequently, use of this shield as a means for protecting the firing personnel has been largely abandoned.

The blast which occurs after the projectile has left the firing tube can be eliminated only if the burning of the propellant is completed while the rocket is within the tube. If high velocity and long range are not required the annoyance caused by the jet blast may be easily avoided by selecting a powder of web thickness (distance between burning surfaces) sufficiently thin to have the burning completed during the time it takes the rocket to travel the length of the projector. It is when the velocity and range are to be increased that difficulties arise, since in order to increase the velocity, and still have the burning completed by the time the projector has left the tube, the powder charge must be increased. But, by increasing the powder charge, the quantity of gas ejected per unit time is also increased, with the result that higher pressures will be developed in the motor chamber unless the throat area of the nozzle is increased. It must be noted also that the total time for burning the propellant is decreased with an increase in velocity, since it takes less time for the rocket to travel the length of the tube. Therefore, on obtaining a higher velocity by increasing the charge, the web thickness must be further reduced to insure that the burning will be over by the time the rocket leaves the tube. This reduction in web thickness increases the burning area of the propellant with the result that still more gas is liberated per unit time. To provide for the ejection of this increase in gas liberation, the throat area must be again enlarged, otherwise higher pressures will be developed. Obviously, there is a limit to the amount the throat may be increased. It cannot be made larger than the chamber. In fact, for practical as well as theoretical reasons, the throat diameter should not be more than one-third to one-half the inside diameter of the combustion chamber.

2

In actual practice there is a limit to the amount the web thickness may be decreased without encountering difficulties in trapping the propellant. In contrast to the burning of a propellant in a gun, the propellant in a rocket combustion chamber is not entirely consumed, i. e., unburned particles escape from the trap after the web of the powder has been reduced to a certain thickness. The smaller the original web thickness, the larger is the percentage of unburned powder that escapes, consequently, decreasing the web thickness is uneconomical and inefficient.

There are certain advantages to be obtained by allowing the pressure to increase with increase in powder charge. The higher pressures cause an increase in burning rate and a reduction in total burning time. The foremost objection to a high gas pressure in rockets is that a heavy walled combustion chamber must be provided to withstand these pressures. Obviously, the weight of the chamber cuts down the efficiency and the ultimate range of the rocket.

Accordingly, it is an object of this invention to provide a rocket projectile which can be fired from a shoulder gun projector or other such projector adapted to be held in the hands of ground troops without having the initial jet blast continued after the projectile has left the projector. Furthermore, the velocity and range of the rocket projector of this invention are not limited by the burning time of the propellant utilized to start the rocket in flight.

A particular object of this invention is to provide an improved military rocket having two separate driving charges. The first driving charge is a relatively quick burning charge, which imparts to the rocket projectile a thrust sufficient to get the projectile out of the projector tube and started in the direction of its normal trajectory. After the rocket projectile has cleared the projector by a safe, precalculated distance, dependent upon the size of the rocket and its particular application, the second driving charge is set off. This second charge need not be quick burning but must be set off a predetermined interval after the burning of the first charge has been completed.

The specific nature of the invention as well as other objects and advantages thereof will clearly appear from a description of a preferred embodiment as shown in the accompanying drawings in which:

Fig. 1 is a fragmentary longitudinal sectional view of a rocket projectile embodying this invention;

Fig. 2 is a side elevational view of the explosive head partly broken away to show the fuse;

Fig. 3 is a cross sectional view taken along the line 3—3 of Fig. 1;

Fig. 4 is a cross sectional view taken along the line 4—4 of Fig. 1;

Fig. 5 is a view similar to Fig. 1 showing a modified form of the invention;

Fig. 6 is an enlarged detail view in longitudinal section showing the thermal igniter utilized to effect discharge of the propellant charge;

Fig. 7 is an enlarged detail view showing the unitary grid utilized to trap the secondary propellant charge;

Fig. 8 is a cross sectional view taken along the line 8—8 of Fig. 5; and

Fig. 9 is a fragmentary sectional view taken along line 9—9 of Fig. 4.

Referring now to Fig. 1, the high explosive and armor-piercing head 1 of the rocket has secured thereto a cylindrical sleeve 2 which is provided with an undercut threaded portion 22 for holding the head 1 to the trap plate 7 of casing 5. The thermal arming device 15 for the impact fuze 20 is threaded into the cylindrical sleeve 2 at its forward end. A screw 3 which is provided with a tapped threaded axial opening 23 is threaded

3

into the base of the cylindrical sleeve 2 so that the closed end of the screw 3 projects into the cylindrical casing 5 when the cylindrical sleeve 2 is threaded into the trap plate 7. The firing pin 6 is provided with a cylindrical rod 24 of a diameter less than the diameter of the tapped opening 23. The end of this rod is threaded and adapted to be inserted into the opening 23. A small slug 25 of a low melting point alloy, such as Wood's metal, is placed in the opening 23 of screw 3 so that when the temperature of such screw is raised to the melting point of the metal 25 and the rod 24 is inserted into this opening, it will remain firmly in place after the metal 25 solidifies on cooling.

The cylindrical casing 5 has its forward end threaded onto the periphery of trap plate 7 and has the walls at its rear end swaged inwardly to form an inwardly flared entrance to a constricted throat portion 16 and then the walls taper outwardly in a rearward direction to provide a flared nozzle 17 for expanding the gases of combustion liberated by the propellant charge 18. This propellant charge is made up of a plurality of cylindrical grains 19 of double-base powder, each having an axial cylindrical perforation. The grains are supported in the chamber in any suitable manner, such as by means of a plurality of "wormshead" trap wires 8, similar to those described in my copending application, Serial No. 538,315 filed June 1, 1944, now abandoned, which have their forward ends threaded into trap plate 7 and upon which the propellant charges are strung.

An annular adapter 26 is provided having a generally frusto conical shape. This adapter has a plurality of radially divergent rib members 38 (Fig. 4) formed on its lateral surface which also have outer surfaces of frusto conical shape to conform to the shape of the nozzle flare 17. It should be noted that while the outer surface of the radially divergent ribs conforms to the interior configuration of the nozzle, the slope of the conical sides of the portion of the adapter shown in section is less than the slope of the nozzle surface and thus provides an annular nozzle space 37 of increasing area in the direction of the exit gases. The forward portion of the adapter is reduced in diameter to form the shoulders 27 and 28 and the extreme forward end 29 is threaded to engage in a threaded axial hole 30 in a star-shaped guide 9 which centers and supports the adapter 26 within the nozzle of the combustion chamber.

The adapter 26 has a rearwardly opening, conical bore 75 communicating with an axial hole 39 therethrough. The rear end of hole 39 is threaded to receive a threaded delay type thermal igniter 10 which is preferably constructed in a manner similar to the thermal igniter disclosed in my copending application Serial No. 538,314, filed June 1, 1944, Patent No. 2,459,163, January 18, 1949. The igniter comprises a threaded element having a forwardly opening axial powder recess 33 therein which aligns with hole 39. The powder recess 33 and hole 39 are filled with powder. A black powder primer 4 is suitably mounted within casing 5, preferably opposite the forward open end of hole 39.

The base of the adapter 26 is interiorly threaded to receive a secondary cylindrical casing 12. The cylindrical casing 12 is threaded into the rear end of adapter 26. This casing contains a relatively quick-burning propellant charge 34 and has a venturi nozzle 35 threaded on to an end thereof and supporting the flight stabilizing fins 13. The nozzle 35 also holds the grid trap 36 in place between the end surface of the cylindrical casing 12 and the venturi nozzle 35. An electrically fired squib igniter 11 is suitably mounted within secondary cylindrical casing 12 and wires 14 connect squib 11 to conventional external contacts.

It should be noted here that the rocket employs the principles of design described and claimed in my copending application, Serial No. 576,439, filed February 6, 1945, Patent No. 2,503,271, April 11, 1950, inasmuch

4

as the center of thrust, produced by the high velocity discharge of the gases of combustion through the expanding annular passage 37, is substantially coincident with the center of gravity of the rocket. If any non-uniformity occurs in the discharge of gases through the nozzle 35, no dispersion will result because the direction of its line of flight is restricted by the projector, since the burning of the propellant 34 within secondary casing 12 is completed within the projector tube.

The operation of the described rocket embodying this invention is as follows: the web thickness of the propellant 34 is selected so that, for the particular operating gas pressure within the casing 12, the burning will be completed before the rocket leaves its projector tube. The weight of propellant 34 is just sufficient to give the rocket an initial thrust to get the rocket out of the projector and on its way toward the target. The heat generated by the burning propellant 34 will cause the black powder in the thermal igniter 10 to be ignited by thermal conduction through the walls of the thermal element. The time required for ignition is about 0.1 sec. in the embodiment illustrated. Due to the thrust produced by the charge 34, the rocket will have traveled a distance of about 50 feet in such time interval. The igniter 10 thus sets off igniter 4 which in turn ignites the primary charge 18. The gases produced by combustion of primary charge 18 discharge through annular nozzle space 37 and accelerate the projectile sufficiently to insure that it will reach the target. About 0.1 sec. after the ignition of charge 18, sufficient heat is generated within casing 5 by the burning propellant to melt solder 25 contained within the opening 23 of the screw 3 to release the rod 24 and firing pin 6. On impact the pin 6 and its inertia element are free to move forward, striking and exploding the percussion primer to set off a powder train leading to the high explosive in the head. The burning of the propellant 18 may be selected to give the rocket sufficient velocity for penetration of the target armor by the specially designed armor-piercing head 1.

A modification of this invention is shown in Fig. 5. The rocket comprises an explosive head 70, a primary combustion chamber 42 defined by a hollow, cylindrical, forward body member 40 and containing the primary propellant charge 43 strung upon the worm head trap wires 44. A partition member 45 is threadably secured between forward body member 40 and a similar rear body member 41 and seals the main combustion chamber 42 from the fluid pressure developed in the secondary combustion chamber 46 by combustion of the quick burning secondary propellant 47. The secondary propellant 47 is held in the secondary combustion chamber 46 by means of a grid trap 48, which is retained against a shoulder formed at the rear end of chamber 46 by the nozzle 49 which is threadably secured thereto. The grid 48 is conveniently formed from a circular plate by milling parallel grooves 60 (Fig. 7) on one side of the plate in one direction to form the lands 61 and by milling parallel grooves 62 on the other side of the plate, in a direction at right angles to the direction of milling for the grooves 60, to form the lands 63. The result is a unitary grid member formed of cross bars having their surfaces projecting on opposite sides of a center line.

The partition member 45 is provided with a plurality of circular openings 50 for permitting the combustion gases liberated by the propellant 43 to pass rearwardly of the chamber for exit through the nozzle 49. The openings 50 are of equal diameter and are equally positioned on equally spaced radii of the partition member 45. In order to prevent ignition of the propellant 43 by the gases liberated from the quick burning propellant 47 in the combustion chamber 46, individual plate members 52 are provided to cover each of the openings 50 in the partition member 45. These plates each have a

tab 53 formed integrally therewith for receiving a bolt 54 which screws into partition member 45 to retain the plate in place over the opening on the side of the partition facing the nozzle.

A thermal ignition device 55 is threaded into an axial hole 57 in the partition member 45 so that its closed end projects into the secondary combustion chamber 46. An ignition train 56 is suitably supported within primary combustion chamber 42 extending forward along the axis of the rocket body and serves to ignite black powder igniter 58 which in turn ignites the main propellant 43. A conventional electrically fired squib 100 surrounds thermal ignition device 55 to ignite such device as well as secondary charge 47. Lead wires 101 and 102 connect squib 100 to the source of current (not shown).

In operation, the propellant charge 47, which is of a selected thin web, is consumed by burning in a time interval less than that required for the projectile to travel the length of the projector tube. The heat generated by burning the propellant charge 47 causes ignition of the black powder in the thermal element 55 a predetermined interval after the burning of the propellant 47 has ceased sufficient to insure that the projectile is a safe distance away from the projector. The powder in thermal element 55 ignites train 56 which in turn ignites the black powder primer 58 for the primary propellant 43. The gases liberated by the primary propellant build up a pressure sufficient to cause the plates 52 to be bent rearwardly of the combustion chamber at the tab portion 53 to uncover the openings and thereby permit exit of the gases into the second chamber for high velocity discharge through said nozzle.

I claim:

1. A rocket projectile comprising a body having a substantially cylindrical bore therein forming a main com-

bustion chamber and an auxiliary combustion chamber, said auxiliary chamber located rearwardly of the said main chamber and having a rearward outwardly flaring nozzle, a flight initiating propellant combustible to generate a gas under pressure supported within said auxiliary chamber, a sustained flight propellant combustible to generate a gas under pressure supported within said main chamber, means to ignite said flight initiating propellant, a plurality of valves for sealing said main chamber from the gas pressure generated in the said auxiliary combustion chamber during combustion of the said flight initiating propellant, and means to ignite said sustained flight propellant a predetermined time after the said ignition of the said flight initiating propellant, the said valves movable upon combustion of the sustained flight propellant to interconnect the said main chamber with the said auxiliary chamber, the said valves comprising a series of plates disposed in a plane at right angles to the longitudinal axis of the said body.

2. The combination defined in claim 1 characterized by the fact that the said plates are supported in the said plane by an integral and deformable tab element.

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