

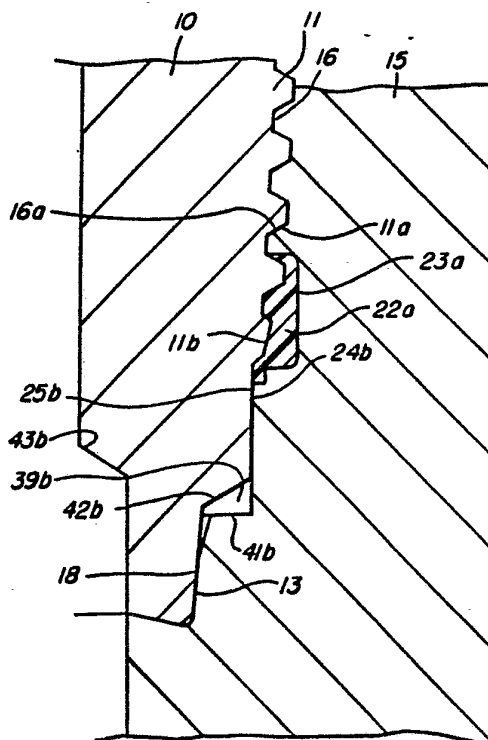
INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

<p>(51) International Patent Classification³ : F16L 19/00, 25/00, 15/00</p>	<p>A1</p>	<p>(11) International Publication Number: WO 85/ 03757</p> <p>(43) International Publication Date: 29 August 1985 (29.08.85)</p>
<p>(21) International Application Number: PCT/US84/02062</p> <p>(22) International Filing Date: 12 December 1984 (12.12.84)</p> <p>(31) Priority Application Number: 583,176</p> <p>(32) Priority Date: 24 February 1984 (24.02.84)</p> <p>(33) Priority Country: US</p> <p>(71)(72) Applicants and Inventors: RAULINS, George, M. [US/US]; 12408 Veronica, Farmers Branch, TX 75234 (US). GRIMMER, George, G. [US/US]; 3040 Eric Lane, Farmers Branch, TX 75234 (US). PETERSON, James, Lee [US/US]; 852 Lamar, Gretna, LA 70053 (US).</p> <p>(74) Agent: GAY, M., H.; Vinson & Elkins, 2900 First City Tower, Houston, TX 77002-6760 (US).</p>		<p>(81) Designated States: AT, AT (European patent), AU, DE, DE (European patent), FR (European patent), GB, GB (European patent), JP, NO.</p> <p>Published <i>With international search report.</i></p>

(54) Title: PIPE JOINT

(57) Abstract

A pipe joint in which a metal-to-metal seal (13, 18) is provided on the exterior of the pipe, a torque shoulder provides a further metal-to-metal seal (14, 19) and a still further seal is provided by a resilient ring (22). The box is protected against ballooning which might result in jump out of the threads by proportioning the thickness of the box at the point of seal at the maximum diameter of seal (t_b) to the outer diameter of the box (D_b) as compared to the full wall thickness of the pipe (t_p) related to the outer diameter of the pipe (D_p).



FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	GA	Gabon	MR	Mauritania
AU	Australia	GB	United Kingdom	MW	Malawi
BB	Barbados	HU	Hungary	NL	Netherlands
BE	Belgium	IT	Italy	NO	Norway
BG	Bulgaria	JP	Japan	RO	Romania
BR	Brazil	KP	Democratic People's Republic of Korea	SD	Sudan
CF	Central African Republic	KR	Republic of Korea	SE	Sweden
CG	Congo	LI	Liechtenstein	SN	Senegal
CH	Switzerland	LK	Sri Lanka	SU	Soviet Union
CM	Cameroon	LU	Luxembourg	TD	Chad
DE	Germany, Federal Republic of	MC	Monaco	TG	Togo
DK	Denmark	MG	Madagascar	US	United States of America
FI	Finland	ML	Mali		
FR	France				

-1-

Description

Pipe Joint

05 This application is a continuation-in-part of our
copending application Serial No. 06/367,952, filed
April 13, 1982 and our copending application 06/456,526,
filed January 7, 1983.

10 Technical Field

This invention relates to pipe joints and more particularly to joints to be used downhole in a producing well.

15 The invention may be used with drill pipe, tubing or
a casing, all of which are referred to herein as "pipe".

Background Art

20 The trend towards deeper and deeper wells, along with
higher pressures and more severe environments found at
these depths, has created a requirement for heavy wall
tubular goods. The depths and pressures require high
strength pipe; on the other hand, the severe H₂S condi-
tions require that the material be of low hardness. Low
hardness inherently demands softer, and therefore, lower
25 strength materials. Hence "ultra heavy walls" are re-
quired to develop the strengths needed.

To utilize the full pipe strength of these ultra
heavy wall materials, connections must be developed that
utilize as many of the required features of the pipe,
30 while sacrificing as few features as possible. The
desired features are that the connections develop full
pipe strength and tensile strength, internal pressure
rating, and collapse rating. The connection should also
be able to withstand high temperatures and/or bending.

35

Disclosure of the Invention

In accordance with this invention, the pipe joint is
designed such that the box of the joint will have

-2-

approximately the same internal pressure rating at the point of maximum metal-to-metal seal, that is, resistance to ballooning, as does the full wall thickness of the pipe between a pair of connectors. The thread system may be
05 designed without regard to the seal surfaces between pipe and box and a step surface may joint the metal-to-metal seal system and the thread system.

It is frequently desirable to include in addition to the metal-to-metal seal in a pipe joint a secondary seal
10 of plastic or resilient material.

In accordance with this invention, the pipe joint is designed such that a resilient or plastic seal may be utilized. Where a plastic material inert to well fluids is utilized which must be compressed to be effective, the
15 invention provides for maintaining such material under compression without the plastic seal interfering with the normal engagement and sealing function of the metal-to-metal seal.

It is an object of this invention to provide a pipe
20 joint in which the box is designed to have a resistance to ballooning equal to or greater than the pipe connected together by the pipe joint.

Another object is to provide a pipe joint in which the resistance to ballooning of the box at the maximum
25 diameter of the metal-to-metal seal is at least equal to the resistance to ballooning of the pipe being connected together and the thread system may be designed for optimum strength without regard to the metal-to-metal seal.

Another object is to provide a pipe joint of the type
30 having a metal-to-metal seal between the box and an external surface on the pipe in conjunction with a back-up seal of plastic material.

Another object is to provide a pipe joint having a metal-to-metal seal with a back-up seal of compressible
35 material in which the material is placed under compression without interfering with the normal engagement and sealing of the metal-to-metal seal surfaces.

-3-

Another object is to provide a pipe joint having a metal-to-metal seal in conjunction with a back-up seal of compressible material in which, as the joint is made up, excess compressible material is extruded from the zone of the back-up seal until just before final make-up of the joint at which time the compressible material is confined and placed in compression during final make-up and in which means are provided for receiving the extruded material so that it will not reach the primary metal-to-metal sealing surfaces and possible interfere with their normal engagement and sealing functions.

Another object is to provide a pipe joint having primary and secondary metallic seal surfaces with each of a cooperating pair of seal surfaces extending at complementary tapers and a resilient seal entrapped between the secondary seal surfaces and the thread system of the joint.

Another object is to provided a pipe joint as in the preceding object in which interference between the seal surfaces and the roots and crests of the thread of the joint are such that the thread interference does not affect the sealing characteristics of the metallic seals and the secondary seal likewise does not interfere with the primary seal.

Another object is to provide a pipe joint coated with a malleable anodic metal such as cadmium.

Another object is to provide a pipe joint of the type having a primary metal-to-metal seal with a back-up seal of compressible material in which, as the joint is made up, excess compressible material is extruded from the back-up seal area after which a secondary metal-to-metal seal becomes effective to act as a secondary metal-to-metal seal for the joint and to confine the compressible material against further extrusion so that as the joint is finally made up, the material may be placed under substantial compression.

Another object is to provide a pipe joint as in the preceding object in which means are provided for receiving

-4-

the extruded seal material so that it will not reach the area of the primary metal-to-metal seal and possibly interfere with full make-up and sealing of the metal-to-metal seal.

- 05 A pipe joint constructed in accordance with this invention will have a wall thickness at the greatest diameter section of the metal-to-metal seal such that this thickness relative to the diameter of the box is equal to or slightly greater than the ratio of the full wall
10 thickness of the pipe to the diameter of the pipe.

Thus, the pipe will be constructed according to the relationship $\frac{t_b}{D_b} = \frac{t_p}{D_p}$ wherein: t_b is the thickness of the box wall at the largest diameter point of sealing engagement between the sealing surfaces in the box and on the
15 outer diameter surface of the pipe, D_b is the outer diameter of the box at the point where t_b is measured, t_p is the full wall thickness of the pipe, and D_p is the diameter of the pipe at the full wall thickness.

20 Brief Description of the Drawings

Other objects, features and advantages of the invention will be apparent from the drawing, the specification and the claims.

In the drawings wherein like reference numerals
25 indicate like parts and illustrative embodiments of this invention are shown:

Figure 1 is a quarter-section view of a pipe joint including a coupling between two pipes;

Figure 2 is a fragmentary view on an enlarged scale
30 of a modified form of pipe joint;

Figures 3, 4 and 5 are fragmentary quarter-section views showing sequentially the make-up of the pipe joint of Figure 1;

Figures 6 and 7 are fragmentary quarter-section views
35 showing sequentially the make-up of the pipe joint of Figure 2 and illustrating a slightly modified form of joint;

-5-

Figures 8, 9 and 10 are sectional views of the modified pipe joint of Figures 8a and 10a, showing in Figure 8, the condition of the seal system prior to engagement of the compressible material by the pin thread, and in Figure 9, the seal material being extruded past the secondary seal during make-up, and in Figure 10, the fully made-up joint with extruded material contained within the excess seal groove.

Figure 8A is a fragmentary sectional view on an enlarged scale of a modified form of pipe joint of Figures 8, 9 and 10 in which a compressible member provides a back-up seal; prior to the pin threads engaging the compressible material;

Figure 10A is a view similar to Figure 8a showing the pipe joint in fully made-up position with the seal material under compression and with excess seal material which was extruded during make-up contained within an excess seal groove and the primary and secondary metal seals in sealing engagement;

Figures 8AA and 10AA are views similar to Figures 8A and 10A illustrating a modified form of joint.

Best Mode for Carrying Out the Invention

The pipe 10 is provided with an external tapered thread 11 thereon. Preferably, this thread is of the buttress type having its load bearing surface extending substantially normal to the center line of the pipe. In some instances, the taper of the threads may be that normally used, that is on the order of three-quarters of an inch per foot. In many instances, where very heavy wall pipe is used, it will be preferred to use a larger taper such as one and one-quarter inch per foot. The use of the steeper taper permits a shorter threaded section of the pipe and box of the coupling. The shorter threaded section in turn reduces the overall length of the coupling and permits greater control and accuracy in cutting threads and other surfaces.

-6-

Adjacent the smaller diameter end of thread 11, the outer diameter of the pipe steps down at 12 to a smaller diameter surface 13 which may be smaller than the diameter of the smallest box thread. This surface 13 is a sealing
05 surface and extends annually about the pipe and longitudinally for a short distance adjacent the end of the pipe. This surface 13 should be contoured to result in a firm sealing contact with the box of the coupling when the joint is made up. For instance, the surface may be on a
10 slight taper or it may be on a radius to provide the sealing contact.

Preferably, the pipe is stressed radially outwardly to ensure the sealing characteristics of the surface 13 and for this purpose, the end of the pipe 14 forms an
15 acute angle with the surface 13. By way of example, the sealing surface 13 may be formed on an angle slightly less than 3° and the abutment surface 14 on an angle of approximately 15° .

The box 15 of the coupling will have an internal
20 thread 16 complementary to and mating with the thread 11 on the pipe.

The box will step down at 17 to a smaller diameter sealing surface 18 which sealingly engages with the sealing surface 13 on the pipe.

25 The box is provided with a torque shoulder 19 extending inwardly from the seal surface 18 to the bore 21 through the coupling. The shoulder 19 should have a matching taper with the shoulder 14 on the end of the pipe which when the pipe is bottomed in the box, limits make-up
30 of the pipe and box and preferably, due to its inclined surface, urges the pipe toward sealing position between the surfaces 13 and 18 which provide the primary seal. Also, the torque shoulder 19 and the end of the pipe 14 may provide a seal, particularly against external pressure.
35

In the illustrated embodiments of Figures 1 and 2, the surfaces 13 and 18 should seal along their entire engaged length. Due to the slight taper of the surfaces,

-7-

the maximum diameter point of sealing engagement is their point of engagement remote from the abutment shoulder 19. This is the point of last metal-to-metal sealing engagement against pressure within the tubing.

05 In accordance with this invention, the box is designed such that its strength at this point of maximum sealing diameter resistant to ballooning is equal to or greater than the strength of the pipe to resist ballooning.

10 In accordance with this invention, the wall thickness (tb) of the box at the point of maximum diameter of the engaged and sealing surfaces 13 and 18 relative to the outer diameter (Db) of the coupling is approximately equal to or greater than the ratio of the full wall thickness of
15 the pipe (tp) relative to the outer diameter of the pipe (Dp) so that the box will be as resistant to ballooning under internal pressure as will the pipe. This will prevent ballooning of the coupling and the possible resultant disengagement of the threads 11 and 16. Thus,
20 so long as the seal provided by surfaces 13 and 18 remains effective, there should be no danger of the threads disengaging due to ballooning of the coupling.

In the form shown in Figure 1 the internal diameter flange 20 results in a larger tb measured at the flange.
25 As the flange is adjacent the point of maximum sealing of surfaces 13 and 18, the flange supports the sealing surfaces against ballooning, resulting in the coupling having a greater $\frac{t}{D}$ ratio than the pipe.

Preferably, a resilient seal is provided by a plastic
30 ring 22 in the groove 23 in the box. This ring is preferably of a plastic material such as tetrafluoroethylene. The groove 23 is positioned such that as the pipe is rotated to full make-up position, the small diameter end of thread of thread 11 enters the area of groove 22 and
35 places the ring under substantial compression. The pipe has an annular surface 24 below thread 11 which overlies the seal 22 before the thread 11 begins to compress the seal 22. Preferably, the surface 24 on the pipe is spaced

-8-

a slight distance from the complementary surface 25 in the box so that the plastic material would be permitted to flow under pressure into the space thus provided. Thus, the seal material forced into the space between surfaces 05 24 and 25 provides a primary plastic seal backed up by seal material in the thread 11 and groove 23. This plastic seal provides a back-up for the metal-to-metal seals.

It may be desirable to avoid any chance of pressure 10 fluid from within the pipe joint reaching threads 11 and 16. In the make-up of the threads, dope is utilized which might result in a seal between the threads. If the other seals permitted fluid to flow into the threaded area, and a seal inadvertently occurred somewhere along the thread 15 system, then the pressure from within the joint would be acting outwardly on the threaded section of the box and might result in disengagement of the threads due to ballooning of the threaded section of the box. To avoid this possibility, a bleed port 26 may be provided in the 20 box, preferably immediately adjacent the resilient seal 22 so that any leakage of fluid past the seals would be vented to the exterior of the joint and would not cause ballooning of the threaded section of the box.

If desired, the surfaces 18 could be extended away 25 from the torque shoulder 19 and a groove provided in this extended surface for the plastic seal. If the step 17 was of substantial dimension, this would position the plastic seal immediately adjacent the metal-to-metal seal and the value of t_b would be approximately the same for the 30 metal-to-metal seal and for the plastic seal.

The relative area of the torque shoulder 19 and the make-up torque should be such that the induced pressure on the shoulder 19 is substantially greater than the internal pressure to be sealed against. For deep high pressure 35 wells, this induced pressure might be on the order of 30,000 to 50,000 psi.

Figures 3, 4 and 5 show the make-up of the pipe and box of Figure 1. In Figure 3 the pipe 10 has been

-9-

threaded into the box 15 to the point where the surface 24 overlies the seal 22 to hold it in its groove during final make-up. In Figure 4 the pipe 10 is shown to be inserted into the box 15 to the extent that the seal 22 has been
05 extruded into the space between the surfaces 24 and 25 and the sealing surfaces 13 and 18 are beginning their make-up. In Figure 5 the pipe 10 is shown to be in the final fully sealed position in the box with the nose of the pipe in firm engagement with the torque shoulder 18 and the
10 pipe made-up preferably to exert a pressure per square inch against the torque shoulder greater than the pressure within the tubing.

Only the upper portion of pipe 27 is shown in the lower end of the coupling. It will be understood that the
15 pipe 27 is identical to pipe 10 and that the coupling is symmetrical and is identical below the flange 20 to the portion of coupling shown above flange 20.

Modified forms of the invention are shown in Figures 2, 6 and 7. In the form of the invention of Figure 2 the
20 pipe 28 is formed with the seal surface 13 and an additional seal surface 29 which cooperates with the end surface 31 of the pipe to form a V-shaped annular member. The surfaces 31 and 29 mate with complementary torque shoulders 32 and seal surface 33 in the box 34. In this
25 form of the invention seals occur at the torque shoulder 31-32, at the seal surface 29 and 33, and at the seal surface 13 and 18. The box is provided with a groove 35 adjacent the upper end of seal surface 18 and again a seal of plastic material 36 is provided in the this groove.

30 The pipe 28 and box 34 are shown in position with the seal surfaces disengaged in Figure 6 and it is noted that the seal 36 projects beyond the groove 35. As best shown in Figure 7, as the nose of the pipe moves into the final sealing position the seal material 36 is compressed and
35 expanded and will flow into the juncture between the seal surfaces 13 and 18. As shown in Figure 7, if a slight spacing is left between the surfaces 13 and 18 on the side of the seal adjacent the threads, as indicated at 37 in

-10-

Figure 7, space will be provided for the seal material to flow into on the side of the plastic seal 36 remote from the torque shoulder 31. Thus, if an excess of seal material is present, as suggested in Figure 7, it will
05 flow into the space 37 and will not interfere with the metal-to-metal seal of surfaces 13 and 18.

In this form of the invention t_b would be measured in the coupling immediately adjacent the groove 35 on the side of the seal groove adjacent to the torque shoulder 31
10 as the largest point of metal-to-metal seal occurs at this point. In the event of failure of all of the metal-to-metal seals, and energizing of the plastic seal 36, the value of t_b at the point of seal of the plastic seal would be only slightly smaller than the value of t_b at the
15 metal-to-metal seal; thus the coupling at the plastic seal would be as resistant to ballooning as would be the pipe 28, and the coupling would not balloon at the point of the plastic seal to any appreciable extent. This is particularly true in view of the fact that the flange 20 is again
20 supporting the seals and the resistance of the coupling to ballooning in view of the support of the flange would actually be greater than the resistance of the tubing to ballooning.

The $\frac{t}{D}$ of the coupling is preferably equal to that of
25 the pipe. However, it will be appreciated that the $\frac{t}{D}$ ratio of the coupling need only approximate that of the pipe. Where the torque shoulder and associated flange is employed, the $\frac{t}{D}$ ratio of the coupling may be slightly less than that of the pipe at the point of maximum sealing
30 diameter because of the support of the flange for the sealing surface which would make the coupling stronger than the pipe if the $\frac{t}{D}$ ratio of the coupling were equal to that of the pipe. Obviously, the $\frac{t}{D}$ ratio may be slightly greater in the coupling relative to the pipe as this
35 provides additional strength and might be preferred where the torque shoulder and its associated flange are not utilized. Also, in some designs it might be acceptable to have a coupling which had a $\frac{t}{D}$ ratio approaching that of

-11-

the pipe, but which was slightly less. Therefore, the invention encompasses a provision of a $\frac{t}{D}$ ratio in the coupling which is approximately the $\frac{t}{D}$ ratio of the pipe.

To provide the coupling with tensile strength equal
05 to the pipe, the amount of metal in the coupling measured at the last full thread or at the plastic seal groove when the groove overlies the threads of the pin is preferably at least equal to the area or amount of metal in the pipe measured at the full wall thickness of the pipe and in
10 planes normal to the joint axis.

In Figures 8 through 10, 8a and 10a, a modified form of joint is shown which employs a compressible back-up seal. In this form of the invention, the box 15 is provided at the last thread with a seal receiving groove
15 23a and a seal member 22a of compressible material. In some services, the well fluids being produced are such that they can be sealed against only by special materials which are not subject to attack by the well fluids. For instance, it may be desirable to use a seal material
20 primarily or entirely of tetrafluoroethylene, commonly known by its trademark Teflon. Teflon will withstand fluids found in many wells and is a desirable seal material. To function properly, Teflon and like materials should be placed under substantial compression and the
25 design of the joint of Figures 8 through 10 provide for using a compressible material which may be placed under substantial compression.

To prevent any substantial extrusion of the compressed material between the threads, they should be carefully
30 formed and the joint should be made up as is customary with lubricant which will fill and seal between the pin and box threads. Preferably, the relationship is such that when the joint is made up, the roots and crests, as well as load flanks of the threads 11 and 16 are in
35 substantial engagement with each other. The stabbing flanks 11a on the pin and the complementary flanks 16a on the box will have a few thousandths of an inch clearance. With this relationship and the lubricants normally

-12-

employed in making up threaded joints for use in petroleum wells, the thread system will not provide an avenue for escape of the seal material 22a when placed in substantial compression and no substantial amount of seal material
05 will be extruded into the thread system during final make-up when the seal material is placed under a substantial compression.

The seal material 22a is slightly larger in volume than the volume of the groove 23a as defined by the pipe and threads extending into the groove 23a when the joint
10 is fully made-up. This excess amount of material is extruded between the surface 24a on the pin and the surface 25a on the box as the pin moves towards final sealing engagement as shown in Figure 9.

15 These secondary seal surfaces 24a and 25a are formed on slightly different tapers so that they may engage and seal with each other in a non-critical manner as the pin moves to its final made-up position shown in Figures 10 and 10a. Prior to reaching this position, the seal
20 material 22a will have been placed under compression and extruded through the space between the two secondary seal surfaces 24a and 25a as the pin threads move into and reduce the volume within the groove 23a. The excess seal material will extrude between the two secondary seal
25 surfaces and as the pin is rotating relative to the box, the extruded material will also be torn, usually at a number of places.

As the thread system moves toward the final make-up position shown in Figure 10 and 10a, the secondary seal
30 surfaces 24a and 25a will have come into sealing engagement slightly before final make-up of the pin and box and, as additional area of the groove 23a is occupied by the pin thread 11, the seal material 22a will be placed in substantial compression so that it will function with
35 maximum performance as a seal. Also, the surfaces 24a and 25a will now provide not only a seal for confining the compressible material 22a in the groove 23a but will also

-13-

provide an additional metal-to-metal seal against loss of the fluid being conveyed through the joint.

To guard against the extruded seal material reaching the primary seal provided by the primary seal surface 18 in the box and the primary seal 13 on the pin, means are provided for receiving at least a part of this excess seal material. Preferably, this means is a groove 38 positioned between the secondary sealing surfaces 24a and 25a and the primary sealing surfaces 13 and 18. Thus, as the material is extruded past the secondary sealing surfaces 24a and 25a, it will gather in the excess seal material groove 38 and be prevented from reaching and interfering with the primary seal surfaces 13 and 18. No particular form of groove 38 is required. Preferably it will receive all extruded material. It is preferably spaced as far as possible from the primary seal surfaces 13 and 18 and more preferably immediately adjacent to the secondary seal surfaces 24a and 25a as shown in the drawings. While a special groove 38 is illustrated, it will be appreciated that this function could be provided by enlarging the space 39 between the pin and box. It has been found that a small groove 38 positioned immediately adjacent the secondary surfaces 24a and 25a will adequately receive the extruded material. It is preferable to leave the space indicated at 39 small so that extruded material will tend to collect in the groove 38 instead of passing into the space 39.

In the pipe joint of Figures 8 through 10 and 8a and 10a, excess seal material may be used so that the amount of material and the presence of pipe dope is not critical and the seal material as well as any pipe dope which may be trapped within the groove 23a may be placed under substantial compression after the secondary seal surfaces 24a and 25a are in engagement. These surfaces provide a means for entrapping the seal material to permit it to be placed under compression as well as providing a secondary metal-to-metal seal against loss of fluid being conveyed through the joint. The excess seal groove 38 will trap

-14-

the extruded seal material and prevent it from reaching the primary seal surfaces 13 and 18. It will be appreciated with this type of seal that a triple seal is provided, that is, the primary seal of surfaces 13 and 18, the
05 secondary seal of surfaces 24a and 25a and the compressed material of seal 22a.

A bleed port such as port 26 (Figure 1) may be utilized if desired.

Referring now to Figure 8AA and Figure 10AA, there is
10 shown a further modified form of joint. The joint is similar to that shown in Figures 8A and 10A and the description of these Figures and the reference numerals referring to the description of Figures 8A and 10A have been repeated in Figure 8AA and Figure 10AA with the
15 changed structure indicated by the suffix (b).

In the box the secondary seal surface 25b cooperates with a secondary surface 24b on the pin which surfaces are on identical tapers. The relative diameter of the surfaces are such as to provide interference therebetween
20 during make-up and for engagement of the lower end of the pin surface 24b with the upper end of the box surface 25b as viewed in Figure 10AA during make-up and before the threads 11 exert any significant pressure on the seal 22a which would cause the seal to be significantly extruded
25 into the space between the secondary seal surfaces 24b and 25b.

To lessen the tendency of the threads 11 to tend to urge the seal 22a axially toward the secondary seal surfaces, the last thread 11b is truncated, as shown, to
30 reduce its height, and thus the tendency of the threads to urge the resilient seal toward the secondary seal surfaces.

Between the secondary seal surfaces 24b and 25b and the primary seal surfaces 13 and 18, the box is provided
35 with a step 41b which cooperates with a complementary step 42b on the pin to provide therebetween a space 39b. This space is provided so that in the event there is any of the resilient seal 22a extruded past the secondary seal

-15-

surfaces 24b and 25b, such extruded material will be received within the annular space 39b and not driven into the space between the primary seals 13 and 18. Also, it is customary in making up threaded joints to apply thread
05 dope to the threads and some of this dope might also be driven past the secondary seal surfaces. If so, the thread dope which passes the secondary seal surfaces would be accumulated in the space 39b and not interfere with make-up of the primary seal surfaces 13 and 18.

10 The step 41b and 42b also facilitates a primary objective of this invention to have at the seal surfaces 13 and 18 a $\frac{t}{D}$ ratio in the box which is at least as great as the $\frac{t}{D}$ ratio of the pipe so that the coupling at the
15 point of primary seal will be as strong as the pipe. In conjunction with this desired ratio, it is also desirable to have a thread system which is not too steeply tapered and does not extend over an excessive length. If the thread system is too long this results in a long coupling and difficulties in maintaining tolerances when cutting
20 the seal surfaces. With the present invention the desired degree of taper of the threads may be employed and the step permits the increase of wall thickness of the coupling at the primary seal permitting the length of the thread system to be limited to that needed for the desired
25 strength in the joint.

With the use of a torque shoulder which drives the primary seal surfaces into tighter engagement, it is advantageous to have the end of the pipe thin walled, as shown. At the area of the secondary seal, however, it is
30 desirable that the pipe wall be thickened as the effect of the torque shoulder on the secondary seal is minimal if it effects the secondary seal at all. For this purpose the ID of the pipe is maintained down to the step 43b where it is increased slightly, as is conventional.

35 It might be noted that while in Figures 8AA and 10AA the primary seal is shown on the periphery of the pin, such seal might be provided by a chamfer on the end of the pin member, such as shown at 29 on Figure 2. In

-16-

accordance with one pipe joint commercially available, the primary seal is provided at the chamfer 29, as shown in Figure 2, and the pin and box are spaced apart slightly immediately above this chamfer, as viewed in Figure 2.

- 05 This invention, and particularly in the form shown in Figures 8AA and 10AA, could be utilized with the primary seal provided by such a chamfer.

The interference between the thread system and the surfaces of the primary and secondary seals should be
10 carefully controlled. Interference is desired between the roots and crest of the buttress-type teeth shown in the thread system so that they will resist backing out of the joint. It is preferred, however, that this interference not tend to balloon the coupling to an extent that would
15 interfere with sealing of the secondary seal surfaces 24b and 25b. In like manner the interference between the surfaces 24b and 25b should not be sufficient to interfere with the sealing characteristics of the primary seal surfaces 13 and 18. For this purpose, with the form of
20 coupling shown in Figures 8AA and 10AA, it is preferred that the interference between the secondary seal surfaces be less than the interference between the primary seal surfaces and that the interference between the roots and crest of the thread system be less than the interference
25 between the secondary seal surfaces. Where the chamfer-type primary seal surface, such as shown in Figure 2, is utilized, it would continue to be preferred that the interference between the secondary seal surfaces be less than that between the primary seal surfaces, but the
30 interference may be substantially equal because the primary seal surfaces are energized by axial movement of the pin into the box to engage the torque shoulders which tend to spread the pin radially outwardly to tighten the primary seal surfaces against each other.

- 35 The primary and secondary seal surfaces are preferably provided by complementary conical surfaces. To protect the primary seal surfaces during make-up of the joint, it is preferred that the primary seal surfaces

-17-

extend at a greater taper than the secondary seal surfaces. This will result in the secondary seal surfaces engaging first and tend to prevent damage of the primary seal surfaces during stabbing of the pin into the box and
05 during the initial thread make-up.

Preferably, at least one of the primary and one of the secondary seal surfaces are coated with a malleable metal which provides an anode in the joint. The malleable metal will assist in filling minute voids, scratches,
10 etc., on the seal surfaces to provide a better seal. Use of a metal which acts as an anode will provide cathodic protection for the joint against corrosive fluids, such as sulphur containing compounds. Preferably, the coating material is cadmium, but other suitable materials may be
15 utilized.

By providing the frusto-conical primary and secondary seal surfaces with the surfaces of each system extending at the same taper, a seal at both the primary and secondary area is assured.

20 The seal at the secondary area being provided before any significant extrusion of the resilient seal member 22a traps this seal member between the secondary seal and the thread system.

The resilient seal element 22a should be sized such
25 that it will not be significantly extruded prior to the time that the secondary seal surfaces come into engagement with each other. The sizing should further be such that as the joint is finally made up the resilient seal member is trapped and the thread 11 exerts a substantial force on
30 the resilient seal member to maintain it under a high internal pressure.

The foregoing disclosure and description of the invention are illustrative and explanatory thereof and various changes in the size, shape and materials, as well
35 as in the details of the illustrated construction, may be made within the scope of the appended claims without departing from the spirit of the invention.

-18-

Claims

1. A pipe joint comprising, a box having a tapered thread and an annular primary seal surface, an annular seal groove in the box at the last thread, an annular seal member of compressible material in said seal groove, a step between said primary seal surface and said seal groove, an annular secondary seal surface between said step and seal groove, a pipe having a tapered thread and an annular primary seal surface for sealing engagement with the primary seal surface of the box, said pipe thread extending into said seal groove when the pipe joint is fully made up, an annular secondary seal surface on said pipe between the thread and primary seal surface for engaging said secondary seal surface in the box, a step between said primary and secondary seal surfaces on said pipe and spaced from said step in the box when the joint is fully made up to provide a space for receiving any seal material extruded past said secondary seal surfaces, said box and pipe having the following approximate relationship:
- $$\frac{t_b}{D_b} = \frac{t_p}{D_p}$$
 wherein, t_b is the thickness of the box wall at the largest diameter point of sealing engagement between said primary sealing surfaces, D_b is the outer diameter of the box at the point where t_b is measured, t_p is the full wall thickness of the pipe, and D_p is the diameter of the pipe at the full wall thickness, said primary seal surfaces provided by frusto-conical surfaces extending at a first identical taper, said secondary seal surfaces provided by frusto-conical surfaces extending at a second identical taper which is less than said first taper, said secondary seal surfaces engaging during make-up of the joint prior to the engagement of said primary seal surfaces and prior to any significant extrusion of said resilient seal.
2. The pipe joint of Claim 1 wherein said threads are buttress-type and wherein said primary seal surfaces

-19-

have greater interference than said secondary seal surfaces and said secondary seal surfaces have greater interference than the roots and crest of said threads.

- 05 3. The pipe joint of Claim 1 wherein said threads are buttress-type and the roots and crest of said threads have less interference than the interference of said primary or said secondary seal surfaces.
- 10 4. The pipe joint of Claims 1, 2 or 3 wherein a torque shoulder is provided in the box engaging the end of the pipe at full make-up of the joint.
- 15 5. The pipe joint of Claim 1 wherein at least one of the pin and box surfaces of said primary and secondary seal surfaces are plated with an anode-type malleable metal.
6. The joint of Claim 1 wherein at least one of the pin and box surfaces of said primary and secondary seal surfaces are plated with cadmium.
- 20 7. The joint of Claim 1 wherein the pipe wall is substantially thicker in the area of the secondary seal than in the area of the primary seal.

25

30

35

1/5

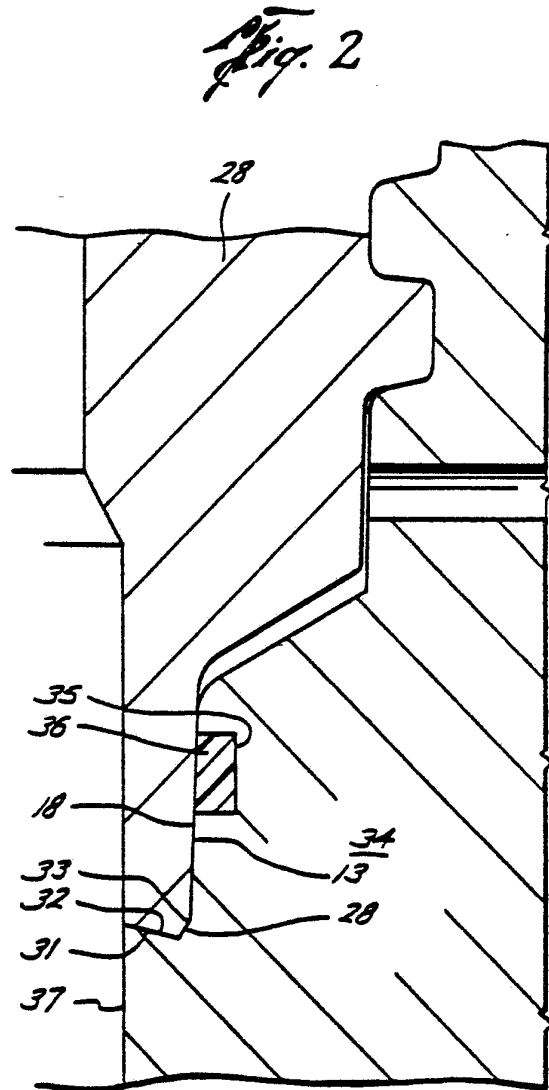
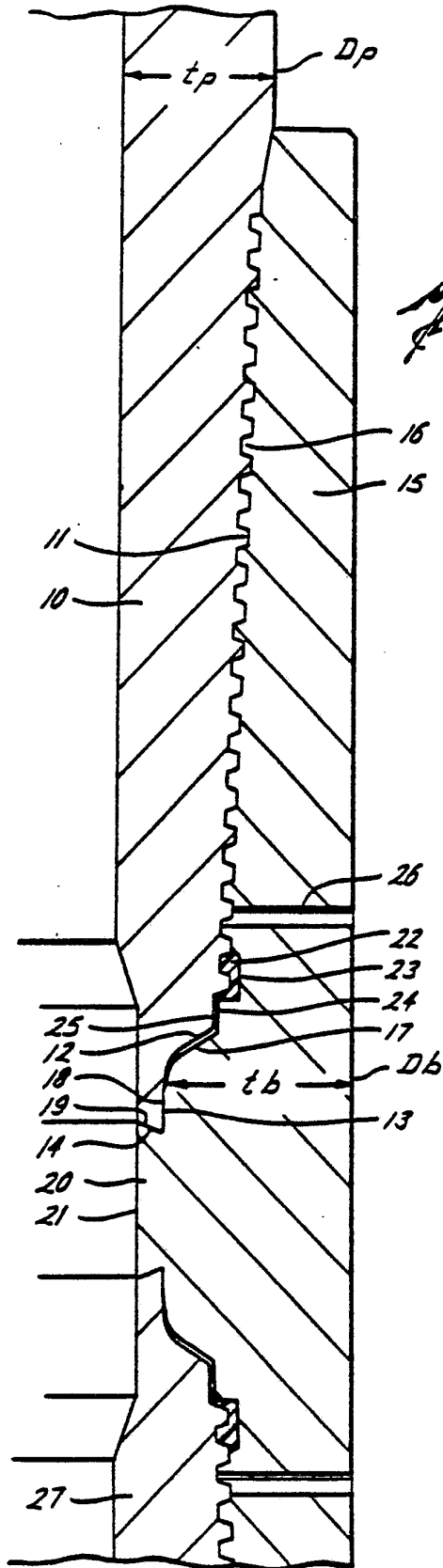


Fig. 3

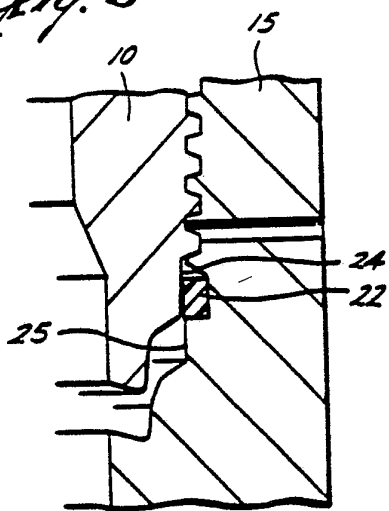


Fig. 6

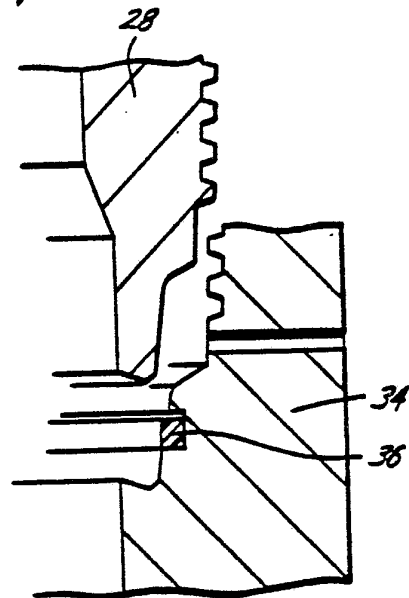


Fig. 4

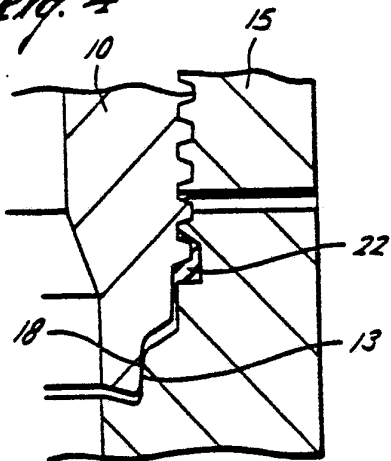


Fig. 7

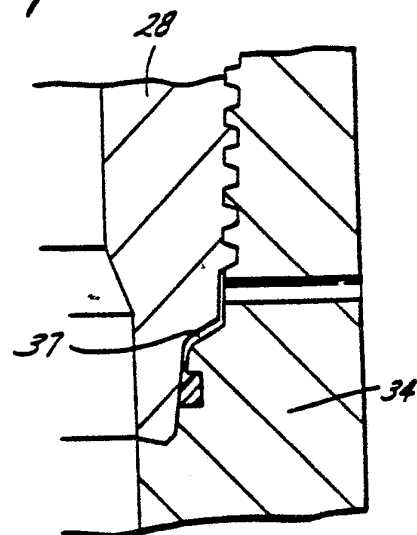
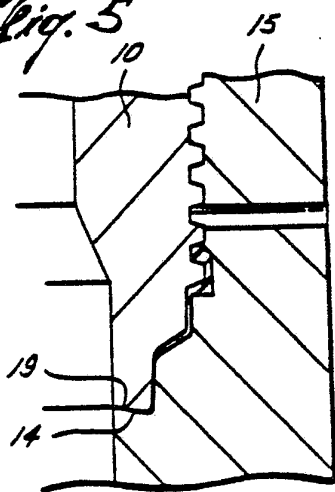


Fig. 5



3/5

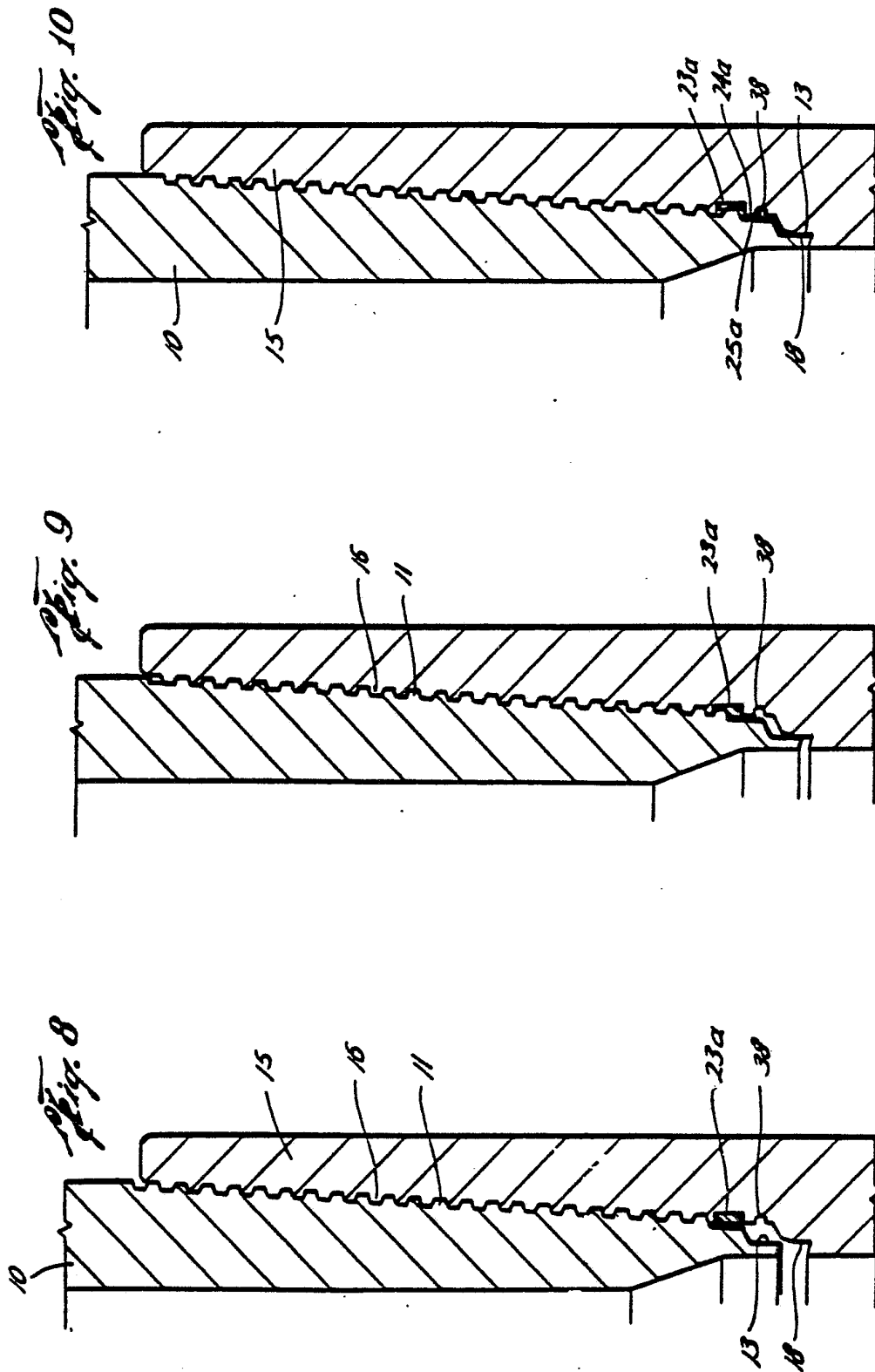


Fig. 10A

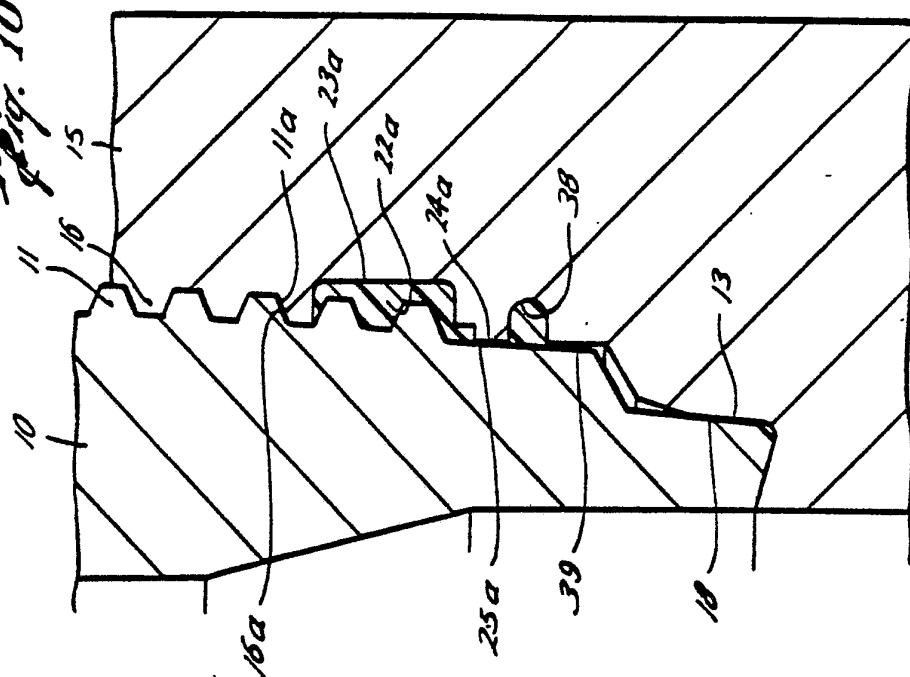
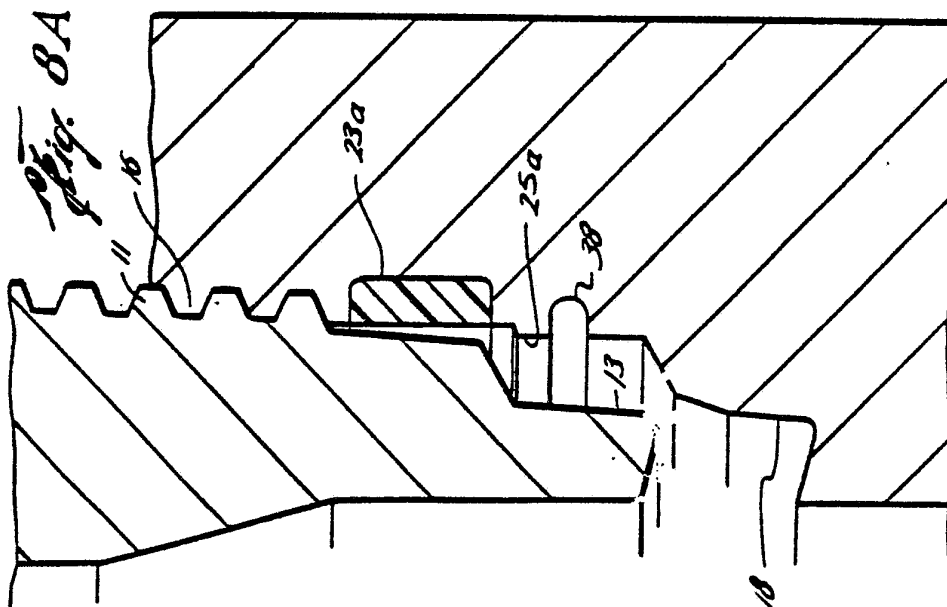
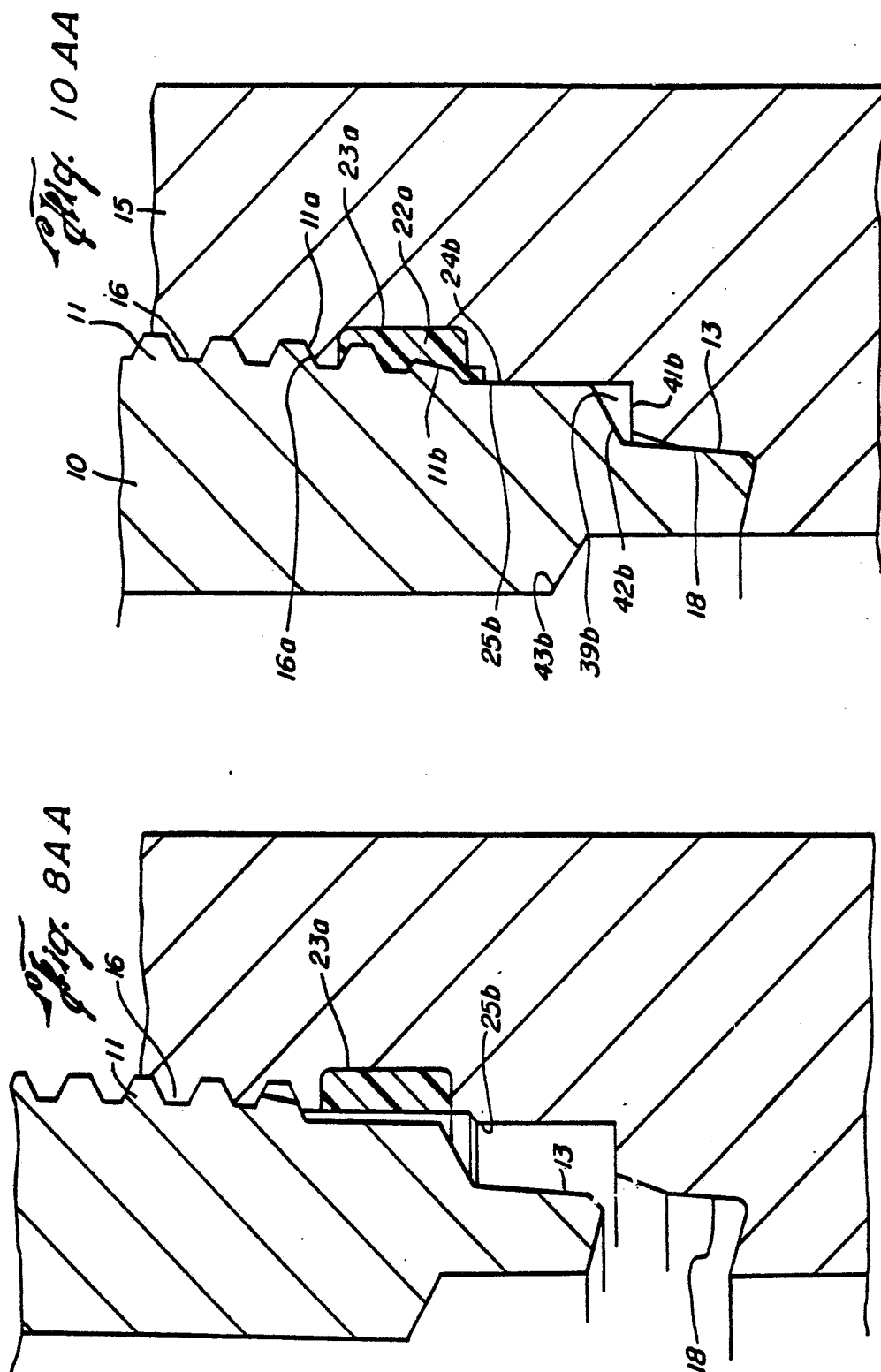


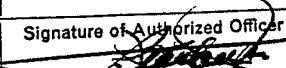
Fig. 8A





INTERNATIONAL SEARCH REPORT

International Application No PCT/US 84/02062

I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) ³		
According to International Patent Classification (IPC) or to both National Classification and IPC Int. Cl. ³ F16L 19/00, 25/00, 15/00 U.S. Cl. 285/350, 334, 332.3, 383, 351, 390		
II. FIELDS SEARCHED		
Minimum Documentation Searched ⁴		
Classification System	Classification Symbols	
U.S.	285/332.2, 332.3, 333, 334, 350, 351, 355, 383, 390	
Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched ⁵		
III. DOCUMENTS CONSIDERED TO BE RELEVANT ¹⁴		
Category *	Citation of Document, ¹⁶ with indication, where appropriate, of the relevant passages ¹⁷	Relevant to Claim No. ¹⁸
A	US, A, 4,398,756, (Duret et al) 16 August 1983	1-7
A	US, A, 4,004,832, (Connelly) 25 January 1977	1-7
A	US, A, 3,850,461, (Fujioka et al) 26 November 1974	1-7
A	US, A, 3,658,368, (Hokanson) 25 April 1972	1-7
A	US, A, 3,508,771, (Duret) 28 April 1970	1-7
A	US, A, 3,497,246, (Weiner) 24 February 1970	1-7
A	US, A, 3,489,438, (McClure) 13 January 1970	1-7
A	US, A, 3,489,437, (Duret) 13 January 1970	1-7
A	US, A, 3,467,413, (Madrelle) 16 September 1969	1-7
A	US, A, 3,100,656, (MacArthur) 13 August 1963	1-7
A	US, A, 3,047,316, (Wehring et al) 31 July 1962	1-7
A	US, A, 2,980,451, (Taylor et al) 18 April 1961	1-7
<div style="display: flex; justify-content: space-between;"> <div style="width: 45%;"> <p>* Special categories of cited documents: ¹⁵</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> </div> <div style="width: 45%;"> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"&" document member of the same patent family</p> </div> </div>		
IV. CERTIFICATION		
Date of the Actual Completion of the International Search ² 21 February 1985	Date of Mailing of this International Search Report ² <div style="font-size: 1.2em; font-weight: bold;">01 MAR 1985</div>	
International Searching Authority ¹ ISA/US	Signature of Authorized Officer ²⁰  Richard J. Scanlan, Jr.	

FURTHER INFORMATION CONTINUED FROM THE SECOND SHEET

A	US, A, 2,932,531, (Briechele) 12 April 1960	1-7
A	US, A, 2,907,589, (Knox) 06 October 1959	1-7
A	US, A, 2,610,028, (Smith) 09 September 1952	1-7
A	CA, A, 635,412, (Pezzotta) 30 January 1962	1-7
A	GB, A, 478,477, (Deutsche) 19 January 1938	1-7

V. ☐ OBSERVATIONS WHERE CERTAIN CLAIMS WERE FOUND UNSEARCHABLE ¹⁰

This international search report has not been established in respect of certain claims under Article 17(2) (a) for the following reasons:

1. ☐ Claim numbers because they relate to subject matter ¹² not required to be searched by this Authority, namely:

2. ☐ Claim numbers because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out ¹³, specifically:

VI. ☐ OBSERVATIONS WHERE UNITY OF INVENTION IS LACKING ¹¹

This International Searching Authority found multiple inventions in this international application as follows:

1. ☐ As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims of the international application.

2. ☐ As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims of the international application for which fees were paid, specifically claims:

3. ☐ No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claim numbers:

4. ☐ As all searchable claims could be searched without effort justifying an additional fee, the International Searching Authority did not invite payment of any additional fee.

Remark on Protest

☐ The additional search fees were accompanied by applicant's protest.

☐ No protest accompanied the payment of additional search fees.