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(54) Title: MULTI-COMPONENT INORGANIC ANCHORING SYSTEM BASED ON FINE ALUMINOUS CEMENT

(57) **Abrégé/Abstract:**

The present invention describes a multi-component inorganic anchoring system for a chemical fastening of anchors and post-installed reinforcing bars in mineral substrates, comprising a curable powdery aluminous cement component A and an initiator component B in aqueous-phase for initiating the curing process, wherein the powdery aluminous cement component A is an aluminous cement component based on powdery calcium aluminate cement, and wherein component B comprises an accelerator constituent and water, characterized in that at least part of the calcium aluminate cement comprised in component A has an average particle size in the range of from 0.5 to 15 µm. Moreover, the present invention pertains to a use of calcium aluminate cement having an average particle size in the range of from 0.5 to 15 µm in a multi-component inorganic anchoring system to increase load values as well as to a method for a chemical fastening of anchoring means, preferably of metal anchors and post-installed reinforcing bars, in mineral substrates, such as structures made of brickwork, concrete, pervious concrete or natural stone.

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(54) **Title:** MULTI-COMPONENT INORGANIC ANCHORING SYSTEM BASED ON FINE ALUMINOUS CEMENT

(57) **Abstract:** The present invention describes a multi-component inorganic anchoring system for a chemical fastening of anchors and post-installed reinforcing bars in mineral substrates, comprising a curable powdery aluminous cement component A and an initiator component B in aqueous-phase for initiating the curing process, wherein the powdery aluminous cement component A is an aluminous cement component based on powdery calcium aluminate cement, and wherein component B comprises an accelerator constituent and water, characterized in that at least part of the calcium aluminate cement comprised in component A has an average particle size in the range of from 0.5 to 15 μm . Moreover, the present invention pertains to a use of calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm in a multi-component inorganic anchoring system to increase load values as well as to a method for a chemical fastening of anchoring means, preferably of metal anchors and post-installed reinforcing bars, in mineral substrates, such as structures made of brickwork, concrete, pervious concrete or natural stone.



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Multi-component inorganic anchoring system based on fine aluminous cement

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FIELD OF THE INVENTION

10 The present invention pertains to a multi-component inorganic anchoring system for a chemical fastening of anchors and post-installed reinforcing bars in mineral substrates, comprising a curable powdery aluminous cement component A and an initiator component B in aqueous-phase for initiating the curing process, wherein the powdery aluminous cement component A is an aluminous cement component based on powdery calcium aluminate cement, and wherein component B comprises an accelerator constituent and water, characterized in that at least part of the calcium aluminate cement comprised in component A has an average particle size in the range of from 0.5 to 15 μm . Moreover, the present invention pertains to a use of calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm in a multi-component inorganic anchoring system to increase load values as well as to a method for a chemical fastening of anchoring means, preferably of metal anchors and post-installed reinforcing bars, in mineral substrates, such as structures made of brickwork, concrete, pervious concrete or natural stone.

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BACKGROUND OF THE INVENTION

Many mortar systems exist which provide a good chemical fastening of anchors and post-installed reinforcing bars in mineral substrates or surfaces. Predominantly mineral systems based on aluminous cement have been developed. Aluminous cement has as its major constituent monocalcium aluminate and is widely used in the building and construction industries as the final products evidence a high level of mechanical performance over extended periods of time. Also, aluminous cement is resistant to bases and attains its maximum strength more rapidly than Portland cement and is capable of

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withstanding solutions of sulfates. Hence, aluminous cement systems are preferably employed in the field of chemical anchoring.

When it comes to chemically fastening of anchors and post-installed reinforcing bars in mineral substrates, most of the known systems lack in sufficient fluidity for most practical applications of the resultant anchoring compositions. Moreover, liquid systems or systems in slurry form exist that have to be mixed prior to the introduction into the borehole making application difficult, in particular with respect to overhead or under water applications, as liquid mortar can drop out of the borehole or can liquefy due to the surrounding water or moist. Often such prior art compositions also evidence a tendency to crack in a relatively short time or do not exhibit the required mechanical performance, in particular under certain conditions such as under the influence of elevated temperatures, in different conditioned boreholes as well as over a long period of time. Moreover, known systems tend to exhibit a large extend of shrinkage when applied in a borehole which results in an insufficient anchoring of the anchors and post-installed reinforcing bars.

Therefore, there is a need for an inorganic anchoring system, preferably a multi-component inorganic anchoring system, which is superior over the prior art systems. In particular, it is of interest to provide a system that can be used for a chemical fastening of anchors and post-installed reinforcing bars in mineral substrates without adversely affecting the handling characteristics, in particular with respect to overhead or under water applications, and the mechanical performance of the chemical anchoring system. Especially, there is a need for a system that provides increased load values when compared to the known systems. In addition, there is a need to improve load values by the addition of fillers or particles materials, such as an inorganic-based material, to lower the consumption of more expensive binder material or to improve some properties of the mixed material.

In view of the above, it is an object of the present invention to provide an inorganic anchoring system, preferably a multi-component inorganic anchoring system, in particular a two-component inorganic capsule anchoring system, which has an excellent mechanical performance, also over a long period of time, and at the same time having increased load values when compared to the known systems and which has advantages,

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in particular with regard to its direct application within the borehole, under water and overhead.

Moreover, it is an object of the present invention to provide a method for a chemical
5 fastening of anchoring means, preferably of metal anchors and post-installed reinforcing bars, in mineral substrates, such as structures made of brickwork, concrete, pervious concrete or natural stone, using this inorganic anchoring system.

These and other objectives as they will become apparent from the ensuing description
10 of the invention are solved by the present invention as described in the independent claims. The dependent claims pertain to preferred embodiments.

SUMMARY OF THE INVENTION

15 In one aspect, the present invention pertains to a multi-component inorganic anchoring system comprising a curable powdery aluminous cement component A and an initiator component B in aqueous-phase for initiating the curing process, wherein the powdery aluminous cement component A is an aluminous cement component based on powdery calcium aluminate cement, and wherein component B comprises an accelerator
20 constituent and water, which is characterized in that at least part of the calcium aluminate cement comprised in component A has an average particle size in the range of from 0.5 to 15 μm . This provided system is used for chemical fastening of anchoring means in mineral substrates.

25 In another aspect, the invention pertains to a use of calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm in a multi-component inorganic anchoring system for a chemical fastening of anchors and post-installed reinforcing bars in mineral substrates, comprising a curable powdery aluminous cement component A and an initiator component B for initiating the curing process, to increase load values.

30 Finally, in another aspect, the present invention pertains to a method for a chemical fastening of anchors and post-installed reinforcing bars in mineral substrates, which is characterized in that a multi-component inorganic anchoring system is used for fastening, which comprises a curable powdery aluminous cement component A and an
35 initiator component B for initiating the curing process, wherein the powdery aluminous

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cement component A is an aluminous cement component based on powdery calcium aluminate cement, and wherein component B comprises an accelerator constituent and water, which is characterized in that at least part of the calcium aluminate cement comprised in component A has an average particle size in the range of from 0.5 to 15
5 μm . The mineral substrates, are substrates such as structures made of brickwork, concrete, pervious concrete or natural stone.

DETAILED DESCRIPTION OF THE INVENTION

10 The following terms and definitions will be used in the context of the present invention:

As used in the context of present invention, the singular forms of “a” and “an” also include the respective plurals unless the context clearly dictates otherwise. Thus, the term “a” or “an” is intended to mean “one or more” or “at least one”, unless indicated otherwise.

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The term “aluminous cement” in the context of the present invention refers to a calcium aluminate cement that consists predominantly of hydraulic active calcium aluminates. Alternative names are “high-alumina cement” or “Ciment fondu” in French. The main active constituent of calcium aluminate cements is monocalcium aluminate (CaAl_2O_4 ,
20 $\text{CaO} \cdot \text{Al}_2\text{O}_3$, or CA in the cement chemist notation).

The term “initiator” or “initiator component” in the context of the present invention refers to a compound or composition that modifies the chemical environment to start a particular chemical reaction. In the present invention, the initiator starts the curing
25 process in the final mixture.

The term “accelerator constituent” in the context of the present invention refers to a compound or a mixture of compounds that accelerate curing of the final mixture in order to achieve faster setting times.

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It has been surprisingly found out by the inventors, that the addition of a calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm to an inorganic anchoring system for a chemical fastening of anchors and post-installed reinforcing bars in mineral substrates, comprising a curable powdery aluminous cement
35 component, results in a significant increase of load values when compared to a system

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not comprising any calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm . It has also been found out that the addition of a fine calcium aluminate cement does not adversely affecting the handling, characteristics and the mechanical performance of the chemical anchoring system, especially when applied
5 over a long period of time, under water and overhead.

Moreover, it has been found that the multi-component inorganic anchoring system of the present invention, in particular a two-component inorganic capsule anchoring system, allows for an easy application and fastening directly within the borehole without having
10 to premix the components before introducing them into the borehole and allows for easy under water and overhead applications.

Therefore, the present invention pertains to a multi-component inorganic anchoring system comprising a curable powdery aluminous cement component A and an initiator
15 component B in aqueous-phase for initiating the curing process, wherein the powdery aluminous cement component A is an aluminous cement component based on powdery calcium aluminate cement, and wherein component B comprises an accelerator constituent and water, characterized in that at least part of the calcium aluminate cement comprised in component A has an average particle size in the range of from 0.5 to 15
20 μm .

Component A as used in the present invention is based on an aluminous cement (CA) or a calcium sulfoaluminate cement (CAS). The aluminous cement component which can be used in the present invention is preferably an aluminous cement component based
25 on powdery calcium aluminate cement (CAC). The aluminous cement to be used in the present invention is characterized by rapid set and rapid hardening, rapid drying, excellent resistance to corrosion and shrinkage. Such a calcium aluminate cement suitable to be used in the present invention is for example Ternal[®] White (Kerneos, France).
30

The fine calcium aluminate cement comprised in component A that is used in the present invention has an average particle size in the range of from 0.5 to 15 μm , and is preferably milled to the corresponding particle size. In particular, Ternal[®] White (Kerneos, France) can be milled to particle sizes between 0.5 to 15 μm .
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Component A as used in the present invention comprises at least about 10 wt.-%, preferably at least about 20 wt.-%, more preferably at least about 30 wt.-%, most preferably at least about 70 wt.-%, from about 10 wt.-% to about 100 wt.-%, preferably
5 from about 40 wt.-% to about 90 wt.-%, more preferably from about 60 wt.-% to about 85 wt.-%, most preferably from about 70 wt.-% to about 80 wt.-% of aluminous cement, based on the total weight of component A, wherein at least part of the calcium aluminate cement has an average particle size in the range of from 0.5 to 15 μm . In a particular preferred embodiment, the curable powdery aluminous cement component A comprises
10 100 wt.-% calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm , based on the total weight of component A.

According to an alternative embodiment of the invention, component A as used comprises at least about 20 wt.-%, preferably at least about 30 wt.-%, more preferably
15 at least about 40 wt.-%, most preferably at least about 50 wt.-%, from about 20 wt.-% to about 80 wt.-%, preferably from about 30 wt.-% to about 70 wt.-%, more preferably from about 35 wt.-% to about 60 wt.-%, most preferably from about 40 wt.-% to about 55 wt.-% of aluminous cement, based on the total weight of component A, wherein at least part of the calcium aluminate cement has an average particle size in the range of from 0.5 to
20 15 μm , and at least about 5 wt.-%, preferably at least about 10 wt.-%, more preferably at least about 15 wt.-%, most preferably at least about 20 wt.-%, from about 1 wt.-% to about 50 wt.-%, preferably from about 5 wt.-% to about 40 wt.-%, more preferably from about 10 wt.-% to about 30 wt.-%, most preferably from about 15 wt.-% to about 25 wt.-% of calcium sulfate, preferably calcium sulfate hemihydrate, based on the total weight
25 of component A. In a preferred alternative embodiment of the multi-component inorganic anchoring system of the present invention, the ratio of CaSO_4/CAC of component A should be less or equal to 35:65.

In a particular preferred embodiment, the calcium aluminate cement used has an
30 average particle size ($d_{50\%}$) in the range of from 0.5 to 10 μm , more preferably of from 2 to 8 μm , most preferably has an average particle size in the range of from 2.8 to 3 μm . In a particular preferred embodiment, component A consists essentially of 100 wt.-% of calcium aluminate cement having an average particle size in the range of from 2.8 to 3
35 μm .

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The addition of calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm to the inorganic anchoring system, lowers the consumption of more expensive binder material and improves some properties of the mixed material, especially results in an increase of load values and eases under water or overhead applications, especially when the multi-component inorganic anchoring system is in form of a two-component inorganic capsule anchoring system.

In an advantageous embodiment, component A as used in the present invention may further comprise the following characteristics, taken alone or in combination.

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Component A may additionally comprise a mineral filler. The mineral filler comprised in component A according to the present invention is selected from the group consisting of limestone fillers, sand, crushed stones, gravels, pebbles and mixtures thereof, preferred are limestone fillers, coarse quartz, quartz powder, preferably quartz powder having an averaged grain size ($d_{50\%}$) of about 16 μm , quartz sand, clay, fly ash, fumed silica, carbonate compounds, such as various calcium carbonates, aluminas, pigments, titanium oxides, light fillers, corundum, and their mixtures. Suitable mineral fillers are commercially available products. Exemplarily mentioned is quartz powder Millisil W12 or W6 (Quarzwerke GmbH, Germany), quartz sand F32 (Quarzwerke GmbH, Germany), or Sewper Aggregates, such as SewperCoat[®] (Kerneos S.A, France). The mineral filler of component A is most preferably a calcium carbonate or a mixture of calcium carbonates. Component A comprises at least about 20 wt.-%, preferably at least about 30 wt.-%, more preferably at least about 40 wt.-%, still more preferably at least about 50 wt.-%, most preferably at least about 60 wt.-%, from about 20 wt.-% to about 95 wt.-%, preferably from about 30 wt.-% to about 90 wt.-%, more preferably from about 40 wt.-% to about 85 wt.-%, still more preferably from about 45 wt.-% to about 80 wt.-%, most preferably from about 50 wt.-% to about 75 wt.-% of mineral filler, based on the total weight of component A. The mineral filler is chosen to obtain a particle size complementary to that of the aluminous cement. It is preferred that the filler has an average particle size of not more than 500 μm , more preferably of not more than 400 μm , most preferably not more than 350 μm .

The mineral filler that can be used according to the present invention, is comprised in the powdery aluminous cement component A of the multi-component inorganic capsule anchoring system. The addition of the mineral filler, lowers the consumption of more

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expensive binder material and improves some properties of the mixed material, results in an increase of load values and eases overhead and under water applications when the multi-component inorganic capsule anchoring system is in form of a two-component inorganic capsule anchoring system.

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Component A may further comprise an antibacterial or biocidal agent in powder form. The antibacterial or biocidal agents which can be used in the present invention may be selected from the group consisting of compounds of the isothiazolinone family, such as methylisothiazolinone (MIT), octylisothiazolinone (OIT) and benzoisothiazolinone (BIT) and their mixtures.

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Component A may additionally comprise a thickening agent in powder form. The thickening agents which can be used in the present invention may be selected from the group consisting of organic products, such as xanthan gum, welan gum or DIUTAN® gum (CPKelco, USA), starched-derived ethers, guar-derived ethers, cellulose-derived ethers, polyacrylamide, carrageenan, agar agar, and mineral products, such as clay, and their mixtures. Suitable thickening agents are commercially available products. Component A comprises at least about 0.01 wt.-%, preferably at least about 0.1 wt.-%, more preferably at least about 0.2 wt.-%, most preferably at least about 0.3 wt.-%, from about 0.01 wt.-% to about 10 wt.-%, preferably from about 0.1 wt.-% to about 5 wt.-%, more preferably from about 0.2 wt.-% to about 1 wt.-%, most preferably from about 0.3 wt.-% to about 0.7 wt.-% of said thickening agent, based on the total weight of component A.

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Component A may also additionally comprise a plasticizer in powder form. The plasticizer comprised in component A may be selected from the group consisting of low molecular weight (LMW) polyacrylic acid polymers, polycondensates, like e.g. sulfonated melamine formaldehydes, lingsulfonates, caseins, superplasticizers from the family of polyphosphonate polyox and polycarbonate polyox, and superplasticizers from the polycarboxylate ether family, and mixtures thereof, for example Ethacryl™ G (Coatex, Arkema Group, France), Acumer™ 1051 (Rohm and Haas, U.K.), Sika® ViscoCrete®-2520 (Sika, Germany) or Sika® ViscoCrete®-20 HE (Sika, Germany). Suitable plasticizers are commercially available products. Component A may comprise at least about 0.2 wt.-%, preferably at least about 0.3 wt.-%, more preferably at least about 0.4 wt.-%, most preferably at least about 0.5 wt.-%, from about 0.2 wt.-% to about 20 wt.-%, preferably from about 0.3 wt.-% to about 15 wt.-%, more preferably from about 0.4 wt.-% to about

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10 wt.-%, most preferably from about 0.5 wt.-% to about 8 wt.-% of said plasticizer, based on the total weight of component A.

Also, component A may comprise dispersing agents in powder form.

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The presence of mineral fillers, antibacterial or biocidal agents, plasticizer, thickening agent and/or dispersing agents in powder form does not change the overall inorganic nature of the cementitious component A.

10 Component B as used in the present invention comprises an accelerator constituent and water.

The accelerator constituent is comprised of at least one alkali and/or earth alkaline metal salt selected from the group consisting of hydroxides, chlorides, sulfates, phosphates, 15 monohydrogen phosphates, dihydrogen phosphates, nitrates, carbonates and mixtures thereof, preferably the accelerator component is an alkali or earth alkaline metal salt, still preferably is a water-soluble alkali or earth alkaline metal salt, more preferably is a calcium metal salt, such as calcium hydroxide, calcium sulfate, calcium carbonate, calcium chloride, calcium formate or calcium phosphate, a sodium metal salt, such as 20 sodium hydroxide, sodium sulfate, sodium carbonate, sodium chloride, sodium formate or sodium phosphate, or a lithium metal salt, such as lithium hydroxide, lithium sulfate, lithium sulfate monohydrate, lithium carbonate, lithium chloride, lithium formate, lithium citrate, or lithium phosphate, most preferably is lithium sulfate or lithium sulfate monohydrate, or mixtures thereof. Component B comprises at least about 0.01 wt.-%, 25 preferably at least about 0.05 wt.-%, more preferably at least about 0.1 wt.-%, most preferably at least about 1.0 wt.-%, from about 0.01 wt.-% to about 30 wt.-%, preferably from about 0.05 wt.-% to about 20 wt.-%, more preferably from about 0.1 wt.-% to about 15 wt.-%, most preferably from about 1.0 wt.-% to about 13 wt.-% of said accelerator, based on the total weight of component B.

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Component B may further comprise a retarder, plasticizer and/or a carbonate-source in liquid form, such as lithium carbonate.

The retarder comprised in component B of the present invention is selected from the 35 group consisting of citric acid, tartaric acid, lactic acid, salicylic acid, gluconic acid and

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mixtures thereof, preferably is a mixture of citric acid and tartaric acid. Component B comprises at least about 0.1 wt.-%, preferably at least about 0.2 wt.-%, more preferably at least about 0.5 wt.-%, most preferably at least about 1.0 wt.-%, from about 0.1 wt.-% to about 25 wt.-%, preferably from about 0.2 wt.-% to about 15 wt.-%, more preferably
5 from about 0.5 wt.-% to about 15 wt.-%, most preferably from about 1.0 wt.-% to about 10 wt.-% of said retarder, based on the total weight of component B.

The plasticizer comprised in component B of the present invention is selected from the group consisting of low molecular weight (LMW) polyacrylic acid polymers, polycondensates, like e.g. sulfonated melamine formaldehydes, lingosulfonates, caseins, superplasticizers from the family of polyphosphonate polyox and polycarbonate polyox, and superplasticizers from the polycarboxylate ether family, and mixtures thereof, for example Ethacryl™ G (Coatex, Arkema Group, France), Acumer™ 1051 (Rohm and Haas, U.K.), Sika® ViscoCrete®-2520 (Sika, Germany) or Sika® ViscoCrete®-
10 20 HE (Sika, Germany). Suitable plasticizers are commercially available products. Component A comprises at least about 0.2 wt.-%, preferably at least about 0.3 wt.-%, more preferably at least about 0.4 wt.-%, most preferably at least about 0.5 wt.-%, from about 0.2 wt.-% to about 20 wt.-%, preferably from about 0.3 wt.-% to about 15 wt.-%, more preferably from about 0.4 wt.-% to about 10 wt.-%, most preferably from about 0.5
20 wt.-% to about 8 wt.-% of said plasticizer, based on the total weight of component B.

Component B may additionally comprise a thickening agent. The thickening agent to be used in the present invention may be selected from the group consisting of bentonite, silicon dioxide, quartz, thickening agents based on acrylate, such as alkali-soluble or
25 alkali-swellaible emulsions, fumed silica, clay and titanate chelating agents. Exemplarily mentioned are polyvinyl alcohol (PVA), hydrophobically modified alkali soluble emulsions (HASE), hydrophobically modified ethylene oxide urethane polymers known in the art as HEUR, and cellulosic thickeners such as hydroxymethyl cellulose (HMC), hydroxyethyl cellulose (HEC), hydrophobically-modified hydroxy ethyl cellulose (HMHEC), sodium carboxymethyl cellulose (SCMC), sodium carboxymethyl 2-hydroxyethyl cellulose, 2-
30 hydroxypropyl methyl cellulose, 2-hydroxyethyl methyl cellulose, 2-hydroxybutyl methyl cellulose, 2-hydroxyethyl ethyl cellulose, 2-hydroxypropyl cellulose, attapulgit clay, and mixtures thereof. Suitable thickening agents are commercially available products, such as Optigel WX (BYK-Chemie GmbH, Germany), Rheolate 1 (Elementis GmbH,
35 Germany) and Acrysol ASE-60 (The Dow Chemical Company). Component B comprises

at least about 0.01 wt.-%, preferably at least about 0.05 wt.-%, more preferably at least about 0.1 wt.-%, most preferably at least about 0.2 wt.-%, from about 0.01 wt.-% to about 15 wt.-%, preferably from about 0.05 wt.-% to about 10 wt.-%, more preferably from about 0.1 wt.-% to about 5 wt.-%, most preferably from about 0.2 wt.-% to about 1 wt.-%
5 of said thickening agent, based on the total weight of component B.

The presence of a retarder, plasticizer, thickening agent and/or a carbonate-source in liquid form does not change the overall inorganic nature of the component B.

10 Component B is present in aqueous phase, preferably in form of a liquid. In an alternative embodiment, component B may also be present in form of a slurry or paste.

The weight ratio between component A and component B (A/B) is preferentially comprised between 7/1 and 1/3, preferably is 3/1. Preferably, the composition of the
15 mixture comprises 75 wt.-% of component A and 25 wt.-% of component B. In an alternative embodiment, the composition of the mixture comprises 25 wt.-% of component A and 75 wt.-% of component B.

In a particular preferred embodiment, component A comprises or consists of the following
20 components:

50 wt.-% to 100 wt.-% of calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm ,
optionally 10 wt.-% to 50 wt.-% of mineral filler, such as calcium carbonate.

25 In a particular preferred embodiment, component B comprises or consists of the following components:

0.1 wt.-% to 20 wt.-% of lithium sulfate,
1 wt.-% to 10 wt.-% of plasticizer, and
70 wt.-% to 99 wt.-% of water.

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It is preferred that the multi-component inorganic anchoring system has an initial set-time of at least 5 min, preferably of at least 10 min, more preferably of at least 15 min, most preferably of at least 20 min, in particular in the range of from about 5 to 25 min, preferably in the range of about 10 to 20 min, after mixing of the two components A and

35 B.

In the multi-component inorganic anchoring system, especially the two-component inorganic capsule anchoring system, the volume ratio of cementitious component A to component B is 1:1 to 7:1, preferably is 3:1. In an alternative embodiment, the volume
5 ratio of cementitious component A to component B is 1:3 to 1:2.

The multi-component inorganic anchoring system is preferably a ready-for-use system, whereby component A and B are in a multi-chamber device, such as a multi-chamber cartridge, a multi-chamber cylinder and/or a multi-chamber capsule, preferably a two-
10 component capsule. In particular, the two-component inorganic capsule anchoring system includes two foil bags for separating curable component A and initiator component B. In an alternative embodiment, the two-component inorganic capsule is made of glass or paper. The two-component inorganic capsule can also be referred to as capsule-in-capsule, foil-in-foil or glass-in-glass. The contents of the capsule are mixed
15 together by inserting the inorganic anchoring system into the borehole, introducing the anchoring device thereby destroying the capsule and mixing component A and B directly within the borehole ready for setting and chemically fastening the anchoring means.

In particular, the multi-component inorganic anchoring system is to be considered as a
20 chemical anchor for fastening metal anchors and post-installed reinforcing bars.

The multi-component inorganic anchoring system comprising the calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm can be used for a chemical fastening of anchoring means, preferably of metal anchors and post-
25 installed reinforcing bars, such as anchor rods, in particular threaded rods, bolts, steel reinforcement bars or the like into mineral substrates, such as structures made of brickwork, concrete, pervious concrete or natural stone. In particular, the multi-component inorganic anchoring system can be used for a chemical fastening of anchoring means, such as metal anchors and post-installed reinforcing bars, in
30 boreholes. It has been found out, that the use of calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm in such a multi-component inorganic anchoring system significantly increases the load values and hence load capacity in boreholes.

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Hence, the use of calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm according to the present invention, alone or in addition to mineral fillers present in the multi-component inorganic anchoring system, is particular to increase load values. Moreover, the addition of calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm is advantageous to lower the consumption of more expensive binder material or to improve some properties of the mixed material.

The calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm comprised in the multi-component inorganic anchoring system is particularly applied in a method for a chemical fastening of anchoring means, preferably of metal anchors and post-installed reinforcing bars, in mineral substrates, such as structures made of brickwork, concrete, pervious concrete or natural stone.

Moreover, the multi-component inorganic anchoring system comprising the calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm may be used for the attachment of fibers, scrim, fabrics or composites, in particular of high-modulus fibers, preferably of carbon fibers, in particular for the reinforcement of building structures, for example walls or ceilings or floors, or further for mounting components, such as plates or blocks, e.g. made of stone, glass or plastic, on buildings or structural elements. However, in particular it is used for fastening of anchoring means, preferably metal anchors and post-installed reinforcing bars, such as anchor rods, in particular threaded rods, bolts, steel reinforcement bars or the like into recesses, such as boreholes, in mineral substrates, such as structures made of brickwork, concrete, pervious concrete or natural stone, whereby the components of the multi-component inorganic anchoring system are mixed, for example by destroying a cartridge, capsule or a plastic bag, or by mixing components of a multi-chamber pails or sets of buckets.

The inventive multi-component inorganic anchoring system preferably is contained separately in a two-chamber capsule so as to inhibit reaction and can be caused to react under use conditions. Moreover, the component A and the component B are produced separately from each other, so that the one component usually contains the curable powdery aluminous cement, wherein at least part of the calcium aluminate cement comprised in component A has an average particle size in the range of from 0.5 to 15 μm while the other component contains the initiator component B including the

accelerator constituent and water. The fillers, as well as the remaining components, may be contained in the one or also the other component. It is also possible that the accelerator constituent is contained in powder form in component A.

- 5 The two-chamber and multi-chamber systems, in which the inventive, multi-component inorganic anchoring system is present, include especially cartridges of glass, plastic, plastic sheets or ceramic, in the interior of which the curable component is kept separate from the initiator component agent by walls, which can be destroyed. Such cartridge or capsule systems are placed in the boreholes. To initiate the curing reaction, the
- 10 cartridges or capsules, including the partitions contained therein, are destroyed, for example, by driving anchoring means, such as the tie bar, into them.

The following example illustrates the invention without thereby limiting it.

15

EXAMPLES

1. Preparation of component A and component B

The powdery cementitious component A as well as the liquid initiator component B of the comparative example 1 and of inventive examples 2 to 10 are initially produced by

20 mixing the constituents specified in Tables 1 and 3, respectively. The proportions that are given are expressed in wt.-%.

Table 1: Composition of component A.

Powdery component A	Comparative Example	Examples									
		A0	A1	A2	A3	A4	A5	A6	A7	A8	A9
CAC, Ternal White®	100	-	-	-	-	-	-	-	-	-	-
Milled CAC 1	-	100	-	-	-	-	-	-	-	-	-
Milled CAC 2	-	-	100	-	-	-	-	-	-	-	-
Milled CAC 3	-	-	-	100	-	-	-	-	-	-	-
Milled CAC 4	-	-	-	-	100	-	-	-	-	-	-
Milled CAC 5	-	-	-	-	-	100	-	-	-	-	-
Milled CAC 6	-	-	-	-	-	-	100	-	-	-	-

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Milled CAC 7	-	-	-	-	-	-	-	100	-	-
Milled CAC 8	-	-	-	-	-	-	-	-	100	-
Milled CAC 9	-	-	-	-	-	-	-	-	-	100

Compounds marketed by Kerneos S.A., France

Table 2: Fineness of calcium aluminate cements in μm .

Compound	Average particle size d50 in μm
CAC, Ternal White®	21
Milled CAC 1	3.6
Milled CAC 2	3.5
Milled CAC 3	6.6
Milled CAC 4	4.4
Milled CAC 5	4.3
Milled CAC 6	5.2
Milled CAC 7	3.0
Milled CAC 8	2.9
Milled CAC 9	2.8

5

A typical mixing protocol for component B is as follows: dissolving lithium sulfate monohydrate in deionized water on a stirring plate and fully homogenizing it at 500 rpm; finally adding plasticizer whilst stirring, and continuing homogenizing at 500 rpm for 5 min.

10

Table 3: Composition of component B.

Liquid component B		Example
Compound	Function	B
Deionized Water		78.96
Visco Crete 2520	Plasticizer	7.70
Lithium sulfate monohydrate	Accelerator	13.34

Lithium sulfate monohydrate marketed by Alfa Aesar GmbH & Co. KG, Germany
Visco Crete 2520 marketed by Sika Deutschland GmbH, Germany

15

2. Determination of mechanical performance

After the preparation, 3 volume-parts of the powdery cementitious component A and 1 volume-part of the liquid initiator component B are mixed by stirring with a spatula per hand until it is homogenized. The mixture are casted into a stainless steel sleeve borehole having a diameter of 12 mm, an anchoring depth of 32 mm and ground undercuts of 0.33 mm. Immediately after filling, an M8 threaded anchor rod with a length of 100 mm is introduced into the borehole. The value loads of the cured mortar compositions are determined after a curing time of 24 hours by using a device for testing materials "Zwick Roell Z050" (Zwick GmbH & Co. KG, Ulm, Germany). The stainless steel sleeve is fastened on a plate while the threaded anchor rod is fixed to the force measuring device with a nut. With a preload of 500 N and a testing rate of 3 mm/min the failure load is determined by centrally pulling out the threaded anchor rod. Each Example consists of a mean value of three pull-outs. Ultimate failure loads are calculated as inner strengths and given in N/mm² in Table 4.

Table 4: Inner strengths in N/mm².

	Comparative Example	Inventive Examples (mixture of component A and B in a volume ratio of 3:1)								
Example No.	1	2	3	4	5	6	7	8	9	10
Sample number	A0 + B	A1 + B	A2 + B	A3 + B	A4 + B	A5 + B	A6 + B	A7 + B	A8 + B	A9 + B
Inner strength in N/mm ²	9.36	17.81	17.72	16.48	16.54	16.64	14.80	19.82	19.78	20.23

As it can be seen from Table 4, all inventive systems show considerable inner strengths after 24 hours of curing as well as increased load values and hence, improved mechanical strength means, in comparison to the comparative system with the initial product Ternal White[®], which is a calcium aluminate cement having an average particle size of 21 µm, which was not milled by the manufacturer, meaning which does not comprise any calcium aluminate cement having an average particle size in the range of from 0.5 to 15 µm.

As it has been shown above, the use of fine aluminous cement of the present invention, in particular with an average particle size in the range of from 0.5 to 15 µm, preferably

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from 2.8 to 3.0 μm provides for an increase in load values and hence mechanical strength when compared to systems not comprising any calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm .

- 5 As it has been shown above, the use of calcium aluminate cement of the present invention, in particular with an average particle size in the range of 0.5 to 15 μm as well as when added in an amount up to 100 wt.-%, provides for an increase in load values and hence mechanical strength when compared to systems not comprising any fine calcium aluminate cement. Moreover, the performance improves significantly in
10 boreholes when high load values are desired. Furthermore, it was found that the inventive systems comprising calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm do not show any micro-cracks after curing. Hence, the inventive systems provide for a dense, sealed anchoring system which is an important pre-condition for obtaining improved corrosion and freeze-thaw resistance as well as
15 provide for high load values.

The multi-component inorganic anchoring system has an excellent mechanical performance, also over a long period of time, and at the same time has increased load values when compared to the known systems and which has advantages, in particular
20 with regard to its direct application within the borehole, under water and overhead.

As it has been shown above, the addition of calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm , results in an increase of load values and at the same time lowers the consumption of more expensive binder material
25 and improves some properties of the mixed material.

CLAIMS

1. A multi-component inorganic anchoring system comprising a curable powdery aluminous cement component A and an initiator component B in aqueous-phase for
5 initiating the curing process, wherein the powdery aluminous cement component A is an aluminous cement component based on powdery calcium aluminate cement, and wherein component B comprises an accelerator constituent and water, characterized in that at least part of the calcium aluminate cement comprised in component A has an average particle size in the range of from 0.5 to 15 μm .
- 10
2. The multi-component inorganic anchoring system according to claim 1, wherein the calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm comprised in component A is present in the range of from about 10 wt.-% to 100 wt.-%, based on the total weight of component A.
- 15
3. The multi-component inorganic anchoring system according to claim 1 or 2, wherein the accelerator constituent comprised in component B is present in the range of from about 0.01 wt.-% to 30 wt.-%, based on the total weight of component B.
- 20
4. The multi-component inorganic anchoring system according to anyone of the preceding claims, wherein initiator component B further comprises a plasticizer.
5. The multi-component inorganic anchoring system according to anyone of the preceding claims, wherein component A further comprises at least one additional mineral
25 filler.
6. The multi-component inorganic anchoring system according to anyone of the preceding claims, wherein component B further comprises a carbonate-source in liquid form.
- 30
7. The multi-component inorganic anchoring system according to anyone of the preceding claims, characterized in that the multi-component inorganic anchoring system is a two-component inorganic capsule anchoring system.

8. The multi-component inorganic anchoring system according to anyone of the preceding claims, wherein the calcium aluminate cement comprised in component A has an average particle size in the range of from 2.8 to 3 μm .
- 5 9. A use of the multi-component inorganic anchoring system according to anyone of the preceding claims, for chemical fastening of anchoring means in mineral substrates.
10. Use of calcium aluminate cement having an average particle size in the range of from 0.5 to 15 μm in a multi-component inorganic anchoring system for a chemical
10 fastening of anchors and post-installed reinforcing bars in mineral substrates, comprising a curable powdery aluminous cement component A and an initiator component B for initiating the curing process, to increase load values.
11. Use according to claim 10, wherein component B further comprises an
15 accelerator constituent and water.
12. Use according to claim 10 or 11, wherein component B further comprises a plasticizer.
- 20 13. Use according to anyone of claims 10 to 12, wherein the calcium aluminate cement comprised in component A has an average particle size in the range of from 2.8 to 3 μm .
14. Method for a chemical fastening of anchors and post-installed reinforcing bars in
25 mineral substrates, characterized in that a multi-component inorganic anchoring system is used for fastening, which comprises a curable powdery aluminous cement component A and an initiator component B for initiating the curing process, wherein the powdery aluminous cement component A is an aluminous cement component based on powdery calcium aluminate cement, and wherein component B comprises an accelerator
30 constituent and water, characterized in that at least part of the calcium aluminate cement comprised in component A has an average particle size in the range of from 0.5 to 15 μm .
15. Method according to claim 14, wherein the multi-component inorganic anchoring
35 system used for fastening is a two-component inorganic capsule anchoring system.