

Sept. 27, 1966

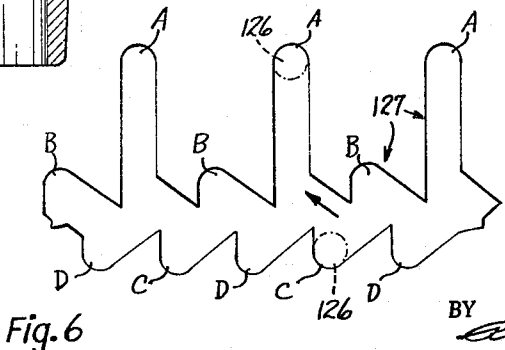
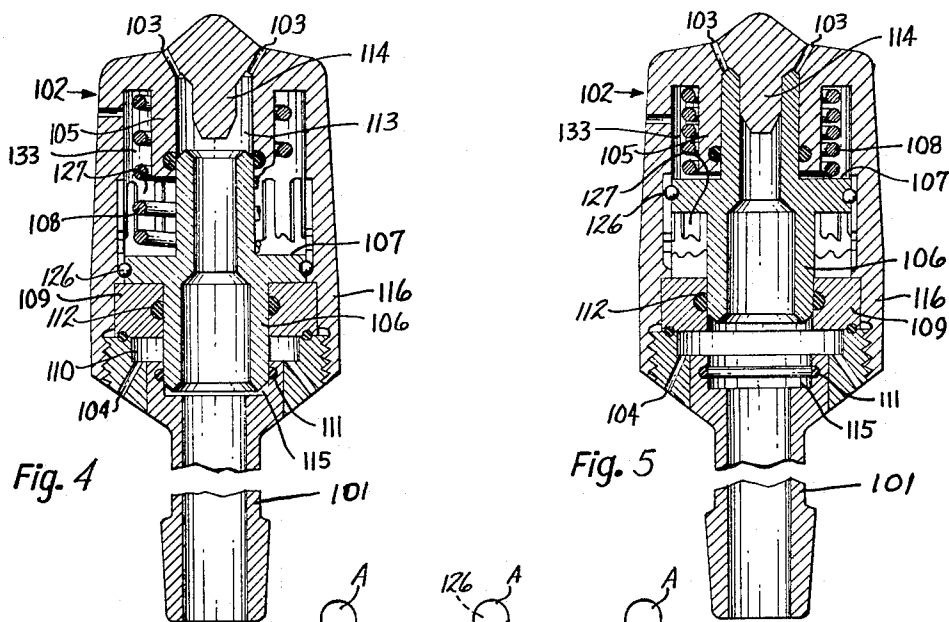
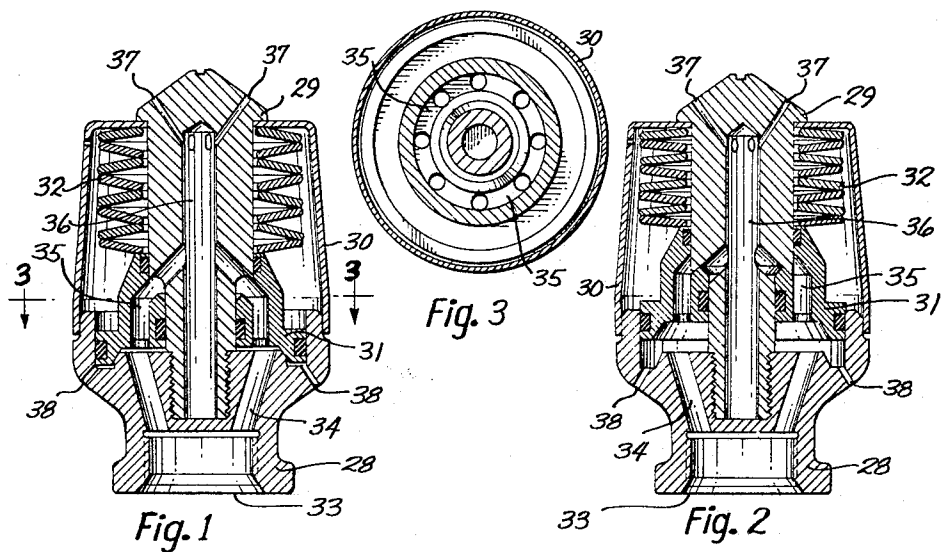
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3,275,247

CONTROLLABLE JET NOZZLE PIPE CLEANING DEVICE

Filed Jan. 11, 1965

2 Sheets-Sheet 1



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2 Sheets-Sheet 2

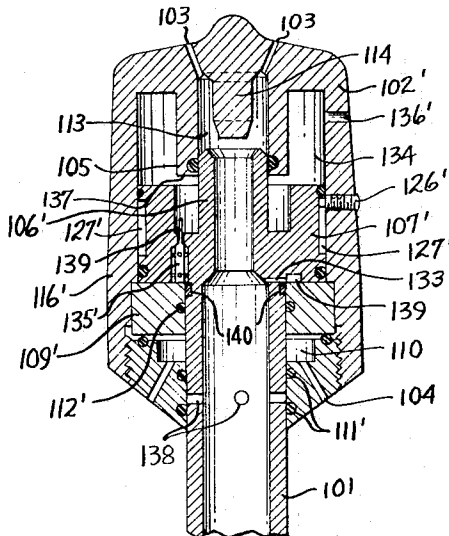


Fig. 9

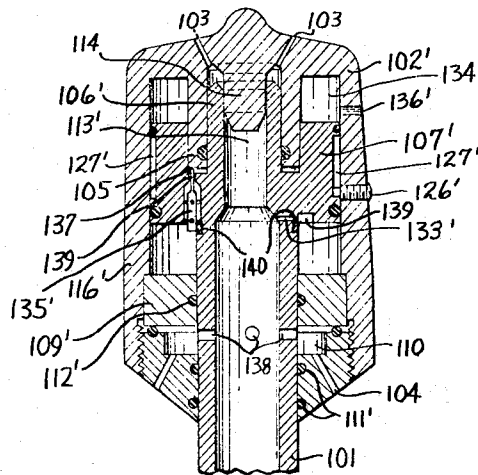


Fig. 10

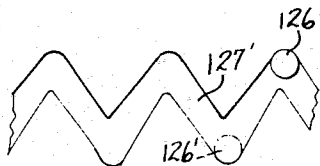


Fig. 11

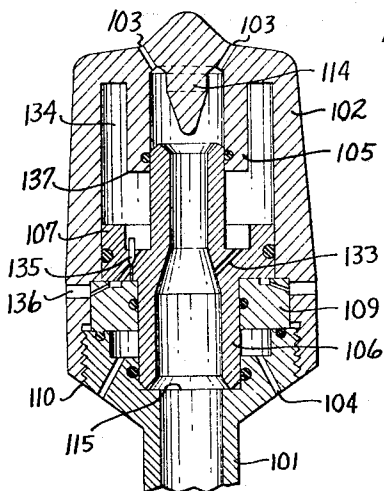


Fig. 7

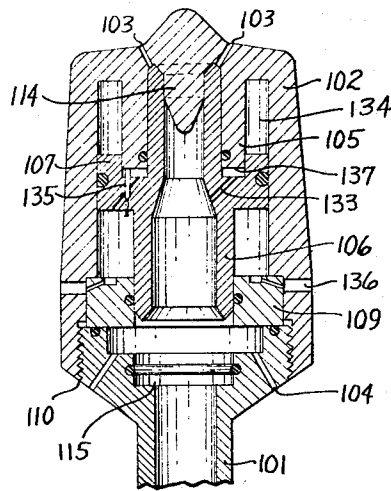


Fig. 8

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CONTROLLABLE JET NOZZLE PIPE CLEANING DEVICE

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Filed Jan. 11, 1965, Ser. No. 424,607

Claims priority, application Germany, Feb. 1, 1960,

H 38,544, Patent 1,165,945; Mar. 11, 1960, H 38,886;

Mar. 16, 1960, H 38,925

11 Claims. (Cl. 239—447)

This application is a continuation-in-part of my co-
pending applications Serial No. 86,061 filed January 31,
1961, now abandoned, for Devices for Cleaning Pipes,
Conduits, Storage Tanks and the Like and Serial No.
202,526 filed June 14, 1962, for Apparatus for the Clean-
ing of Sewer Systems now Patent No. 3,165,109 issued
January 12, 1965. This invention relates to cleansing
devices which are intended for cleansing pipes and ducts,
as well as storage and transport containers which are used
for the transport and storage of oils and oil products
and acids, as well as of milk, beer, fruit juices, and the like.

For this cleansing process, devices are known in which
the cleansing fluid is sprayed systematically by cleansing
heads with controlled nozzles, under high pressure, over
the inner wall or interior of the pipe or container to be
cleaned. The motion of the spraying head with nozzles
is frequently controlled by a preceding high-speed tur-
bine, which, whether it is operated with or without waste
water, requires a bulky, costly transmission gear for re-
ducing its speed. The nozzles then point backwards to the
direction of the principal axis of the cleanser. Through
the reaction or shock of the cleansing medium, in the
form of liquid, steam or compressed gas jets, ejected at
high pressure from the nozzles of the cleanser head carry-
ing them, a backwardly directed jet reactive force is pro-
duced and transmitted to the cleanser head and the supply
hose connected to the cleanser head. If it is desired to
impart a reverse thrust to the filling hose, the cleanser
heads must be changed.

A disadvantage of sprinkler cleansers of the aforesaid
type is that in pipelines with bends, welded places or
sluice valves, they do not always reach as far as the
inspection point or point of access, which may be re-
movable, or accessible ports or joints in the pipe system.
If the hose becomes jammed in the pipe, it is not easily
withdrawn. This disadvantage is particularly great be-
cause the pulling effect of the reaction cleansing jets can
inherently be exerted over very long stretches, for in-
stance, up to 100 meters. If excessive frictional forces
are encountered in the line to be cleansed, the line must
be broken at some not easily accessible place in order
to change the nozzles. In this connection also, it is an
essential prerequisite that the pipeline should be accessible
externally at the point where the trouble occurs. Some-
times the pipeline has to be cut in order to remove the
obstruction or change the cleansing head.

An object of the invention is to provide a device for
cleansing pipes and ducts, storage containers and the like,
with a flexible hose connection for the controllable supply
of a high-pressure liquid (30 to 80 atm.) into a head with
nozzles arranged obliquely to the wall of the pipe to be
cleansed. The reaction of jets of cleansing medium from
the nozzles draws the hose by reactive force farther into
the pipe to be cleansed, the pressure of the liquid in the
nozzle head operating a remotely controlled piston which,
according to its position, controls the supply of cleansing
liquid to nozzles directed obliquely backwards.

The invention is further based on the knowledge that
as far as possible all rapidly rotating components should
be eliminated within the drive and gear since, in addition
to the difficulties in regard to sealing or packing, the
constantly fluctuating temperatures require a simple and
rugged construction.

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The invention includes the provision of recoil or re-
action nozzles, arranged preferably circumferentially sym-
metrical to the pressure line in the nozzle head, which are
closed, with increasing liquid pressure, by means of an
auxiliary valve formed by parts of the piston and the
nozzle head, deactivating the reaction or recoil nozzles
which draw the head farther into the pipe or duct.

The invention can advantageously be embodied in a
compact form by using a cylindrical nozzle casing with an
internal valve piston formed by a hollow body, spring
loaded against the liquid pressure which, with fluctuating
pressure, slides back and forth to activate forward-dis-
charging and rearward discharging nozzles alternately.
Additionally the head or valve may be rotated progres-
sively on a sliding surface in the nozzle casing under the
action of a control cam.

A further feature of the cleansing head is that, in each
case according to the adjustment of the pressure, the hose
travels forwards or backwards in the pipe or duct to be
cleaned. A special control is provided for the feedback
water admixed with the fresh water. With automatic
feedback control of the pressure, the control valve further
moves to and fro so that the cleanser head exerts a selec-
tively controllable scrubbing action on the inside of the
pipe or duct.

The deposits in the pipe are attacked from all sides,
always at an oblique angle. The cleansing power of the
head is increased compared with devices of known type
with the same expenditure of cleansing agent. Cleansing
is completed in a shorter time. Control means for the
cleanser head can be constructed in different ways al-
though, basically, in all cases what is required is a longi-
tudinally movable, pressure-controlled, i.e. spring-loaded
valve piston, or fluid-pressure piston.

The nozzles of the cleanser head may be tilted in dif-
ferent directions, can be placed in a series of rows or in a
cross-shaped arrangement.

Notwithstanding the incorporation of an automatic
pressure control, the dimensions of the nozzle head in
length and diameter are not greater than those of the
simple nozzle head of known type for reactive motion in
one direction only. Accordingly, the advantage is gained
that pipes and ducts with sharp bends can be serviced and
the nozzle head can travel through them in each case as
desired either forwards or backwards.

Exemplary embodiments of the invention are shown
in the accompanying drawings.

In order to be able easily to compare the different forms
of embodiment, the nozzle heads are shown in longitudinal
section through the middle and on approximately the
same scale.

Referring to the drawings:

FIGURE 1 is a longitudinal central section through
one form of the cleansing device showing parts in one
position, and FIGURE 2 is a similar view showing parts
in a different position. FIGURE 3 is a transverse section
through the device taken on line 3—3 of FIGURE 1.

FIGURE 4 is a central longitudinal section through a
modified type of nozzle device showing parts in one rela-
tionship, and FIGURE 5 is a similar view through the
same device showing parts in a different relationship.
FIGURE 6 is a diagrammatic representation of structure
of the nozzle mechanism in developed representation.

FIGURE 7 is a central longitudinal section through
another modification of the nozzle construction showing
parts in one relationship, and FIGURE 8 is a similar view
showing parts in a different relationship.

FIGURE 9 is a central longitudinal section through
still another form of nozzle construction with parts in
one relationship, FIGURE 10 is a similar view of the
device with parts in a different relationship, and FIGURE

11 is a diagrammatic representation of nozzle head rotating structure in developed form.

The nozzle cleaning head can, for example, consist of a mouthpiece 28, a head piece 29 and a casing 30, as well as a longitudinally reciprocable hollow piston 31 and a Belleville spring 32.

The mouthpiece 28 is provided with a hose-connecting opening 33 and several ducts 34 branching off from such opening. Passages 35 are arranged in the piston 31 corresponding, respectively, to the ducts 34. The head piece 29 is also provided at its center with a central bore 36, one end of which is in fluid connection with the passages 35 of the piston 31 and the other end of which is in communication with nozzle openings 37 in the end of the head piece 29 opposite the hose-connecting supply opening 33.

Upon admission of the cleaning liquid under pressure, the cleaning head piston 31 is either in a position as shown in FIGURE 1, in which position the water jet can be ejected from the frontal nozzle openings 37, or the piston is pressed by greater water pressure against the action of the spring 32 in upward direction to the position of FIGURE 2, so that the fluid connection with the passage 36 is interrupted and the connection with the rearward nozzle openings 38 is opened. In this case the water jet is ejected through these nozzle openings 38 in the rearward direction.

The aggregate cross section of the frontal nozzle openings 37 is so limited that a drop in pressure cannot occur at the pump, since at a certain preset operational pressure the amount of water which can be supplied by the pump is greater than the amount of water ejected from the nozzle openings 37. Accordingly the pressure is increased in the accumulators to such a degree that the spring 32 is contracted by the piston 31 being moved toward the nozzle tip by such increased water pressure. Thus the liquid supply to the nozzle openings 37 is interrupted by movement of the piston, which simultaneously uncovers a connection to the rearward nozzle openings 38. The cross sections of these nozzle openings 38 are selected so that more liquid can be ejected than can be supplied from the pump. Consequently a maximum pulling and cleaning action is achieved by the ejection of large jets from the rear nozzle openings 38, as well as the pressure in the ducts 34 being relieved so that the pressure in the accumulator system connected to supply opening 33 and on the piston 31 drops to a value less than the force exerted on it by spring 32. Such spring therefore returns the piston 31 toward the supply opening 33 into its original position of FIGURE 1 in which it closes the annular passage leading to the rear nozzle openings 38 and opens the passages 35 and central bore 36 leading to the forward nozzle openings 37. The throttling effect on the nozzle head discharge resulting from the constriction again produced by such forward openings results in a renewed pressure increase in the accumulators causing piston 31 again to be forced forward to the position of FIGURE 2, despite the opposition of the force of spring 32, to shut off the flow through forward openings 37 and open the rear openings 38. The above-described operation whereby water is ejected alternately through the forward openings 37 and rearward openings 38 is repeated automatically until the liquid supply is shut off.

By the arrangement of several accumulators, which can be operatively connected and disconnected individually, the frequency of the reversing process can be controlled depending on whether a longer forward or rearward movement of the nozzle, corresponding to the degree of fouling of the sewer system to be cleaned, is desired. Alternatively the supply capacity of the pump can be adjusted so that such supply and the ejected liquid are in equilibrium. In this arrangement the water is ejected continuously only from the nozzle openings 38.

FIGURES 4, 5 and 6 show an exemplary alternative embodiment of the invention in which means for rotating the piston in the nozzle head are arranged in such head in rotational symmetry. In FIGURE 4 the mouth piece or spigot 101 for the attachment of the pressure hose is widened at the top to receive a cap sleeve forming the principal part of the cleanser head 102. This contains the forwardly-directed oblique nozzles 103 while the rearwardly-directed oblique nozzles 104 are arranged in the mouthpiece 101.

The upper part of the cleanser head 102 has an associated valve sleeve 105 extending downwards from the inner crown of the cleanser head to receive the hollow piston 106, the shoulder 107 of which is loaded by a coil spring 108 to bear on the sealing ring 109, on which the valve piston 106 seats in its resting position. In this position, as shown in FIGURE 4, the piston closes the antechamber 110 against the cleansing fluid, which is fed to the bore of the mouthpiece 101 at a high pressure of between 30 and 80 atmospheres.

Sealing against the pressure fluid is effected by the circular gaskets 111 and 112. When the cleansing head is set in operation and the valve piston 106 is in the resting position of FIGURE 4, the pressure fluid is first discharged through the piston's central bore into the antechamber 113 and thence is discharged through the nozzles 103.

When the pressure of the cleansing fluid builds up until the loading of the valve piston 106 by the spring 108 is overcome, the piston 106 lifts until on reaching the crown of the cleansing head it practically fills the space of the antechamber 113 and its own cavity is closed by the valve plug 114 as shown in FIGURE 5. The nozzles 103 are now also closed so that the jets directed obliquely forward stop. The bottom control end 115 of the piston 106 has meanwhile risen sufficiently to open the antechamber 110 for communication between mouthpiece 101 and the ring of rear nozzles 104. The cleansing fluid is sprayed under high pressure out of the nozzles 104 which now begin to act as reaction jets.

Being directed obliquely, jets 104 exert a particularly good cleansing and specifically a good scouring effect on the dirt lodged on the pipe or container wall, and the force of these reactive jets issuing from the nozzles pull the connecting hose forward. If the forward motion of the cleansing head is impeded, this will become apparent at the supply end of the hose by its failure to advance. It is then only necessary to reduce the fluid pressure until it acts on the valve piston 106 with less than the force of spring 108. The spring then presses the piston 106 back on its seating from the position of FIGURE 5 to the position of FIGURE 4. The forward nozzles 103 then again discharge reactive jets of the cleansing fluid which push the cleansing head and the connecting hose backwards.

By repeatedly raising and lowering the pressure, the hose can be moved to and fro until the obstruction is removed and the cleansing of the pipe under high pressure is continued, while the hose is simultaneously drawn forward.

The periphery of the shoulder 107 of the hollow piston 106 contains a semicircular recess receiving a control ball 126 simultaneously rolling on a control cam track 127 in the inner wall of the barrel 116 in the cleanser head 102, as shown in developed form in FIGURE 6. The latter figure shows the central, rising parts of the cam track 127, indicated at AA and, to right and left thereof, two reversing profiles, indicated by BB. This control cam track effects rotation of the piston 106 as a result of its axial movement influenced by the pressure variations or pressure pulses in the pipe, because of the action of the cam track on the control ball 126 in the sequence shown by the broken-line ball-representing circles 126 on the control cam curve of FIGURE 6, indicating the path taken by the control ball.

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At low pressure, as assumed for the control cam track curve shown in FIGURE 6, the ball 126 rests in an initial position indicated in that figure by CC. When the fluid pressure rises, the piston 106, shoulder 107 and the control ball 126 are pressed upwards until the ball 126 comes into the end position shown in FIGURE 6 at AA. Thereby, the piston 106 is also rotated, as clearly shown by the obliquely-ascending arrow between CC and AA in FIGURE 6.

The embodiment according to FIGURES 7 and 8 is an example of the possibility, according to the invention, of constructing a reciprocable cleansing head controlled exclusively by hydraulic means influenced by pressure variations to operate different groups of jet nozzles. The essential components are the same as in the other embodiments, except that no spring is required. The general construction of the nozzle body 102 with the water supply mouthpiece or spigot 101, the reciprocable piston 106 with its hollow end sliding in valve sleeve 105 and adapted to receive the valve plug 114 are all similar to the construction described in connection with FIGURES 4 and 5. In this instance, however, there is no bleed opening provided in the chamber of the nozzle body above the piston shoulder 107, as shown in the previously described types of cleansing head.

The particular feature of the construction shown in FIGURES 7 and 8 which differs from the cleansing heads described above is the provision of a small bleed passage 133 in the body of the piston 106 by which the central bore of such piston is placed in restricted communication with the nozzle body cavity 134 of the cleansing head 102. When the cleansing fluid is fed through the mouthpiece 101 into the central bore of the piston 106 for discharge through the forwardly-directed nozzles 103, as shown in FIGURE 7, a small amount of such liquid is bypassed through the passage 133 into the annular spray head chamber 134.

The piston shoulder 107 has a passage extending through it which is controlled by a valve 135 that is in open position when the piston is at rest in the position shown in FIGURE 7. The liquid which seeps into the body chamber 134 through the piston passage 133 is allowed, by suitable proportioning of the cross-sectional areas of the piston passage 133 and the passage controlled by valve 135 so that the valve-controlled passage is larger than the piston passage, to drain past valve 135 out through the discharge port 136 into the pipe or container to be cleansed.

When the pressure of the cleansing fluid is sufficiently high to reciprocate piston 106 upward so that the valve plug 114 fits in the piston's central bore, the forward nozzles 103 are closed in the manner previously explained and cleansing liquid is discharged through the rearwardly-directed nozzles 104 from the antechamber 110, as shown in FIGURE 8. When the pressure of liquid supplied to the mouthpiece 101 is still further increased somewhat, the end of auxiliary valve 135 is pressed against the lower edge 137 of the guiding sleeve 105. By such contact the valve is moved to closed position sealing the chamber 134 so that, as liquid under pressure is supplied gradually to this chamber through the bleed passage 133, the piston 106 is forced from the position of FIGURE 8 to that of FIGURE 7. When the piston has been returned to the position of FIGURE 7, the lower end of the control valve 135 will engage the sealing ring 109 so that such valve will be moved again into open position to enable liquid to be drained from chamber 134 faster than it is supplied to such chamber through piston passage 133. The piston will then begin to be moved from the position of FIGURE 7 toward the position of FIGURE 8 again by fluid pressure on piston 106 in accordance with the operation explained above.

The type of nozzle construction shown in FIGURES 9, 10 and 11 has features similar to the type of nozzle shown in FIGURES 4, 5 and 6 and to the type of nozzle

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shown in FIGURES 7 and 8 and has additional capabilities. In this type of construction means are provided for rotating the spray or nozzle head relative to the mouthpiece or spigot 101 to which the pressure hose can be attached. As in the two types of nozzle head shown in FIGURES 4 and 5 and in FIGURES 7 and 8, a cap sleeve forming the principal part of the cleanser head 102' contains the forwardly-directed oblique nozzles 103 while the rearwardly-directed nozzles 104 are arranged in the opposite end of the casing 116'.

In this instance the valve piston 106' is integral with the mouthpiece 101 and the shoulder 107' is integral with and projects outward from the hollow valve piston 106'. The upper end of the piston's hollow stem is engaged in the valve sleeve 105 projecting downwards from the inner crown of the cleanser head. The lower portion of the cleanser head casing 116' is sealed around the mouthpiece 101 by the seals 111' and 112', which can slide relative to the mouthpiece so as to enable the nozzle casing to move both axially and rotationally relative to such mouthpiece.

When the cleansing head is set in operation, the nozzle casing 116' may be in the relation to the mouthpiece 101 shown in FIGURE 9 in which the sealing ring 109' of the nozzle head abuts the lower side of the shoulder 107'. In this relationship fluid under high pressure, which may be between 30 and 80 atmospheres, is supplied to the antechamber 113 and thence is discharged through the forward nozzles 103. With the nozzle casing 116' in this forward position, the apertures 138 in the mouthpiece 101 are sealed between the gasket 111' so that the mouthpiece body wall serves as a control member blocking flow of water to the antechamber 110. During this operation liquid under pressure passes through the small bleed opening 133' in the side of the valve piston 106' into an annular groove in the base of the shoulder 107' which communicates with one end of a passage through the piston shoulder 107' which, under the conditions illustrated in FIGURE 9, is closed by a reciprocable valve 135'.

Fluid under pressure passing through the bleed opening 133' builds up pressure between the bottom of the valve piston shoulder 107' and the sealing ring 109' carried by the nozzle head which causes these components to separate, sliding the sealing ring down the mouthpiece 101 toward the position shown in FIGURE 10. The fluid pressure in the space between the shoulder 107' and the sealing ring 109' tends to hold the valve 135' in closed position. In addition buttons on the valve stem frictionally engage the wall of the piston passage, tending to hold the valve in any position in which it is adjusted without interfering with flow around the valve and through the piston passage when the valve is in open position.

When the nozzle head casing 116' has been slid down around the mouthpiece 101 to the position of FIGURE 10, the end 139 of the valve projecting above the piston shoulder 107' is engaged by the end 137 of the valve sleeve 105 and further movement of the casing causes the valve to be moved to the open position shown in FIGURE 10. The valve cannot fall out of the piston passage because a button projecting from the side of the valve will engage the valve-retaining ring 140 encircling the mouthpiece. The fluid under pressure in the chamber between the sealing ring 109' and the piston shoulder 107' will be released to flow through the piston passage into the valve casing chamber 134 from which it can escape from the nozzle body through the aperture 136' in its wall.

With the parts in the relationship shown in FIGURE 10 the mouthpiece body wall serves as control means by fitting tightly around the valve plug 114 to interrupt the flow from the interior of the mouthpiece 101 to the forward nozzles 103, but cleansing fluid will flow through the ports 138 in the wall of the mouthpiece into the antechamber 110 for discharge through the rearward nozzles 104. Even though the end of the mouthpiece passage is plugged by the valve plug 114, pressure will be exerted on

it tending to slide the nozzle casing 116' toward the position shown in FIGURE 9. In addition pressure fluid passing through the piston shoulder port past the valve 135' will tend to build up pressure between such piston shoulder and the end surface 137 of the valve sleeve 105, which pressure also will tend to move the nozzle casing 116' from the position of FIGURE 10 toward that of FIGURE 9. When the nozzle head casing has reached approximately the midposition of its travel, the ports 138 supplying liquid through antechamber 110 to the rear jets 104 will be closed by the lower end of the nozzle casing and the valve plug 114 will have been withdrawn from the end portion 113' of the mouthpiece bore so that cleansing fluid again will be discharged from the forward jets 103.

During the reciprocation of the nozzle casing 116' back and forth along the mouthpiece 101 as described, such casing is also rotated relative to the mouthpiece. Such rotation is accomplished by the inner end of pin 126' projecting into the interior of the casing being engaged in a cam groove 127' provided in the periphery of the shoulder 107'. Such cam groove is of undulating contour circumferentially of the piston shoulder, as shown in the developed form of such cam groove in FIGURE 11. Each time that the casing 116' moves in one direction or the other along the mouthpiece 101, the end of pin 126' engaged in the cam groove will traverse an inclined section of such groove to effect an incremental rotation of the casing 116' about its axis relative to the piston shoulder 107' and the mouthpiece 101 with which such shoulder is integral. The rotative driving action effected by interengagement of the pin 126' and the cam groove 127' is similar to the rotation effected by engagement of the ball 126 in the cam groove 127, as discussed in connection with FIGURES 4, 5 and 6.

I claim as my invention:

1. Cleaning nozzle mechanism comprising a conduit for supplying fluid under pressure, a nozzle head mounted on said conduit and having first jet means and second jet means at spaced locations in said nozzle head and directed in generally opposite directions, respectively, and further having first and second valve elements spaced apart, and control means having first and second valve elements spaced apart and cooperable with said first and second nozzle head valve elements, respectively, by reciprocation of said control means with respect to said nozzle head between a first position in which engagement of said two first valve elements blocks communication between said conduit and said first jet means while said second jet means are in communication with said conduit and a second position in which engagement of said second two valve elements blocks communication between said conduit and said second jet means while said first jet means are in communication with said conduit, and said control means further including pressure-receiving surface means upon which pressure is exerted by fluid under pressure from said conduit for creating a force effecting relative reciprocation of said control means and said nozzle head.

2. The cleaning nozzle mechanism defined in claim 1, including means engaged between the control means and the nozzle head for effecting relative rotation of the control means and the nozzle head in addition to relative reciprocation thereof.

3. The cleaning nozzle mechanism defined in claim 2, in which the means for effecting relative rotation of the control means and the nozzle head is operable to effect such rotation simultaneously with and coordinated with relative reciprocation of the control means and the nozzle head.

4. The cleaning nozzle mechanism defined in claim 2, in which means for effecting relative rotation of the control means and the nozzle head is operatively connected to the control means to effect intermittent rotation thereof relative to the nozzle head in response to reciprocation of the control means relative to the nozzle head.

5. The cleaning nozzle mechanism defined in claim 2, in which the means for effecting relative rotation of the control means and the nozzle head is operatively connected to the nozzle head to effect intermittent rotation thereof relative to the control means in response to relative reciprocation of the control means and the nozzle head.

6. The cleaning nozzle mechanism defined in claim 1, and spring means engaged between the nozzle head and the control means and acting on the control means in opposition to the action of fluid under pressure on the control means.

7. The cleaning nozzle mechanism defined in claim 1, in which the control means is a hollow piston subjected to pressure fluid, spring means engaged with said piston and urging it in a direction opposite that in which the pressure of the pressure fluid tends to move it, and rotary drive means connected to said piston and operable to effect rotation thereof in response to reciprocation of said piston.

8. The cleaning nozzle mechanism defined in claim 7, in which the pressure-receiving surface means includes a step in the bore of the hollow piston against which pressure of the fluid is exerted.

9. The cleaning nozzle mechanism defined in claim 7, in which the rotary drive means includes cam means operatively connected to the hollow piston for effecting rotation thereof.

10. The cleaning nozzle mechanism defined in claim 1, in which the jet means include two rings of orifices, the orifices in each ring being spaced apart circumferentially and diverging in the direction away from the other ring of orifices.

11. The cleaning nozzle mechanism defined in claim 1, and a longitudinally shiftable conduit for supplying the fluid under pressure, the nozzle head being mounted on and movable with said conduit, and one jet means includes a ring of orifices adjacent to and directed alongside said conduit for propelling the nozzle head and conduit in one direction and the other jet means includes a second ring of orifices in a portion of the nozzle head remote from the first ring of orifices for discharge of fluid therefrom to propel the nozzle head in the opposite direction.

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EVERETT W. KIRBY, *Primary Examiner.*