Dec. 16, 1969 A. W. WILKERSON 3,484,676

FIRING CIRCUIT FOR CONTROLLED RECTIFIER MEANS

Original Filed Oct. 21, 1965 5 Sheets-Sheet 1

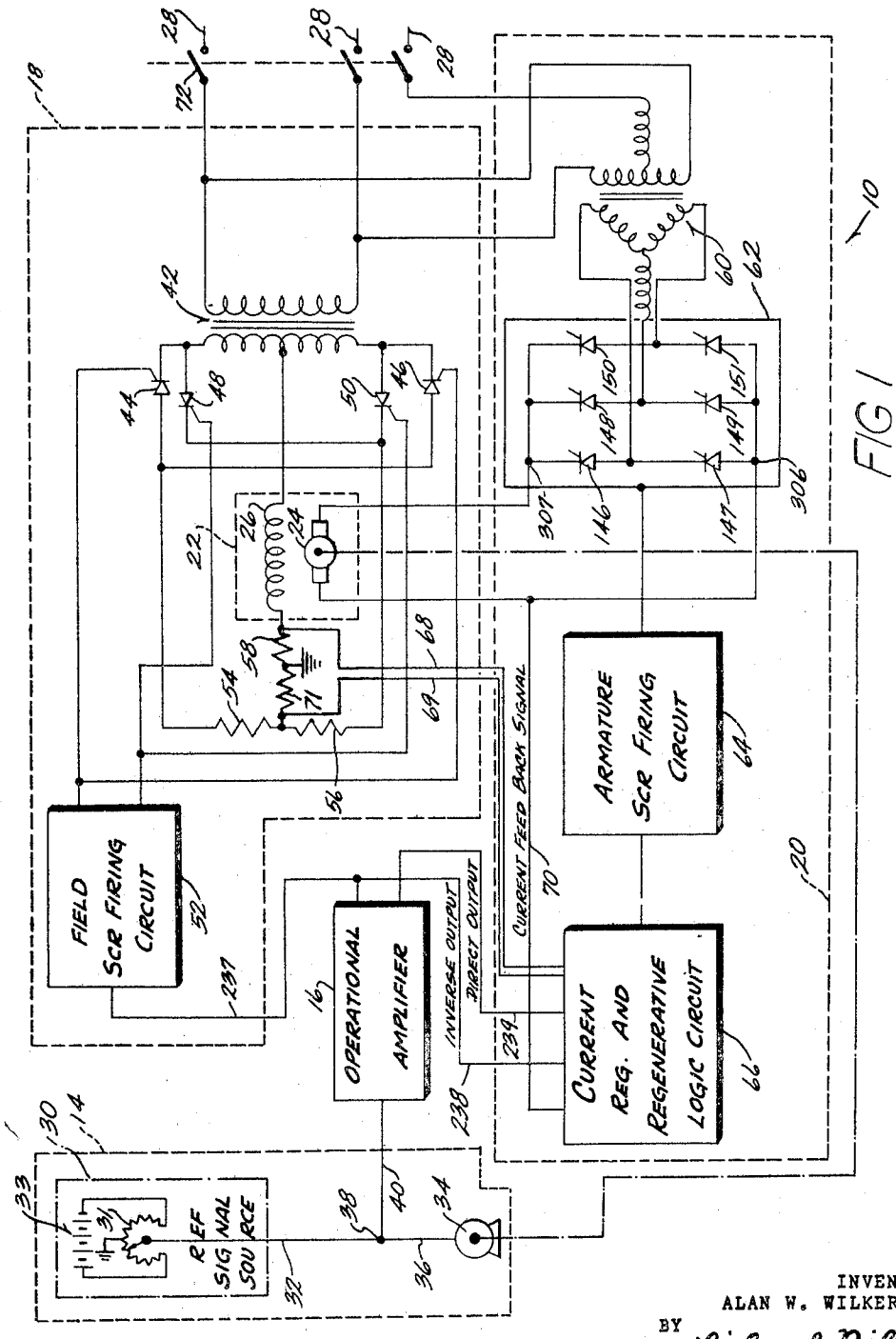


FIG 1

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FIRING CIRCUIT FOR CONTROLLED RECTIFIER MEANS

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FIG. 3

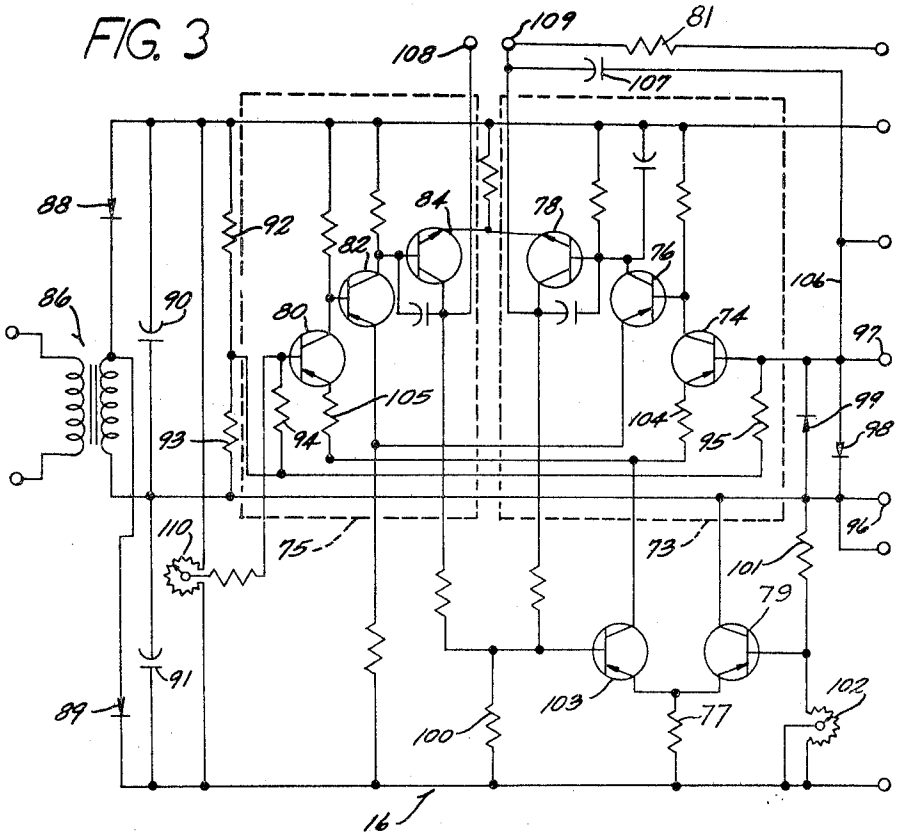


FIG. 2

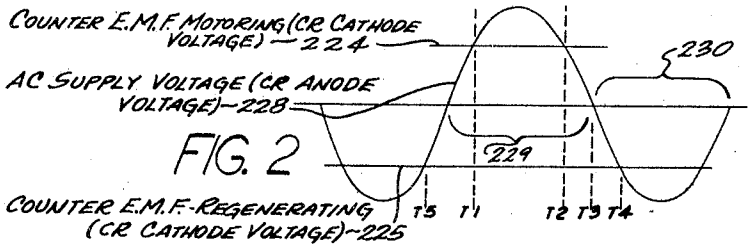


FIG. 7a

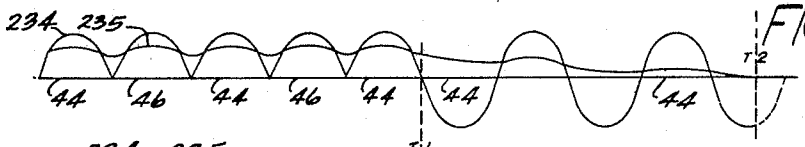
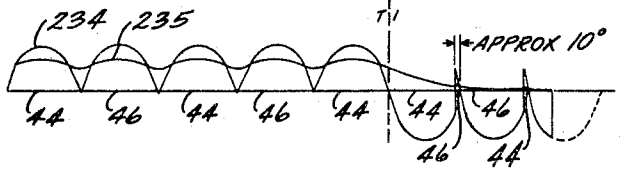


FIG. 7b



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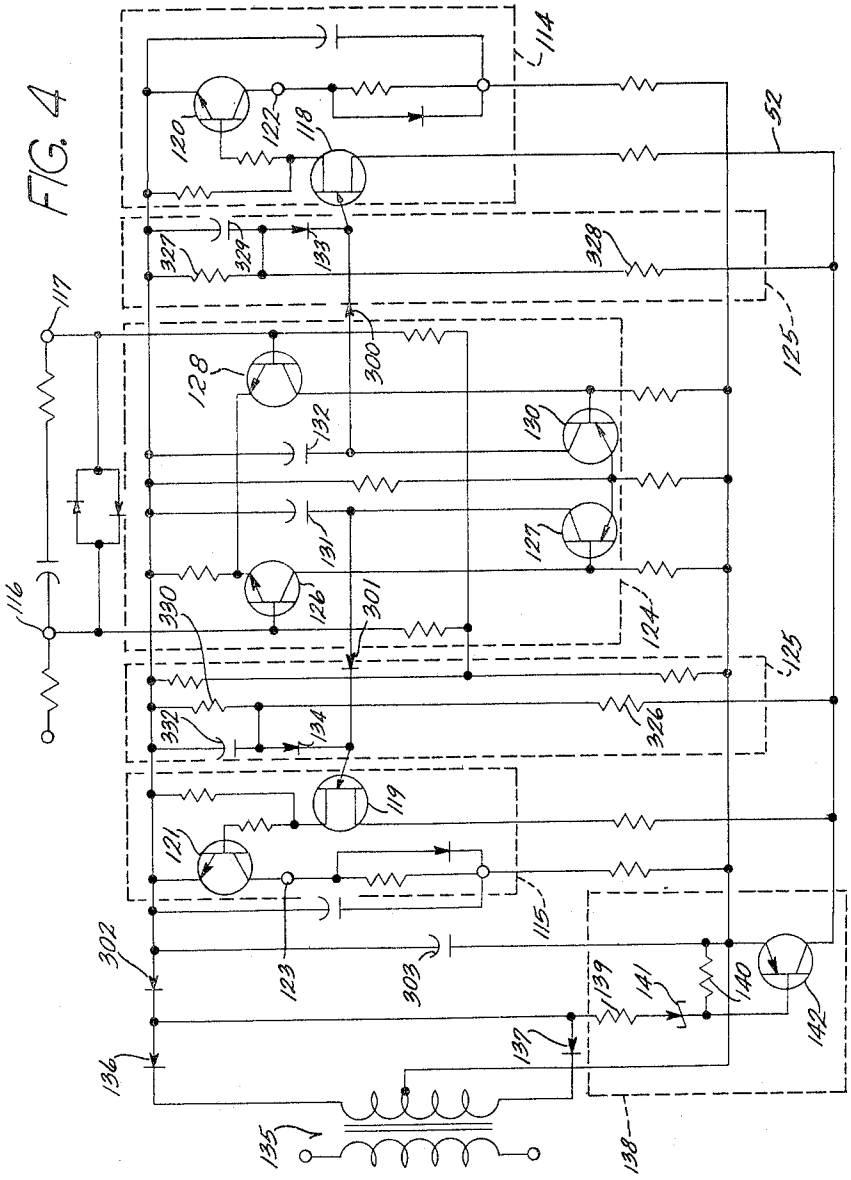
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FIG. 4



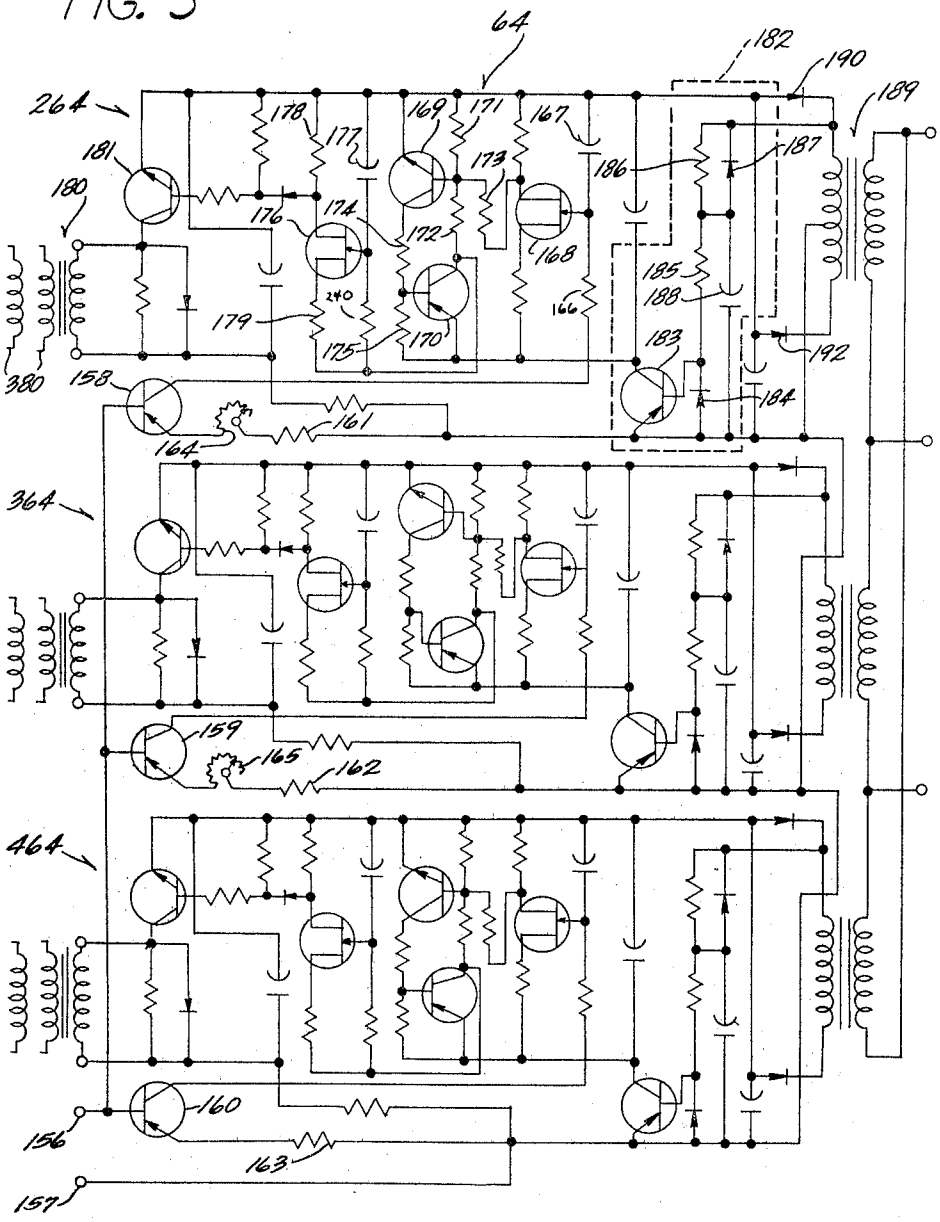
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FIRING CIRCUIT FOR CONTROLLED RECTIFIER MEANS

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FIG. 5



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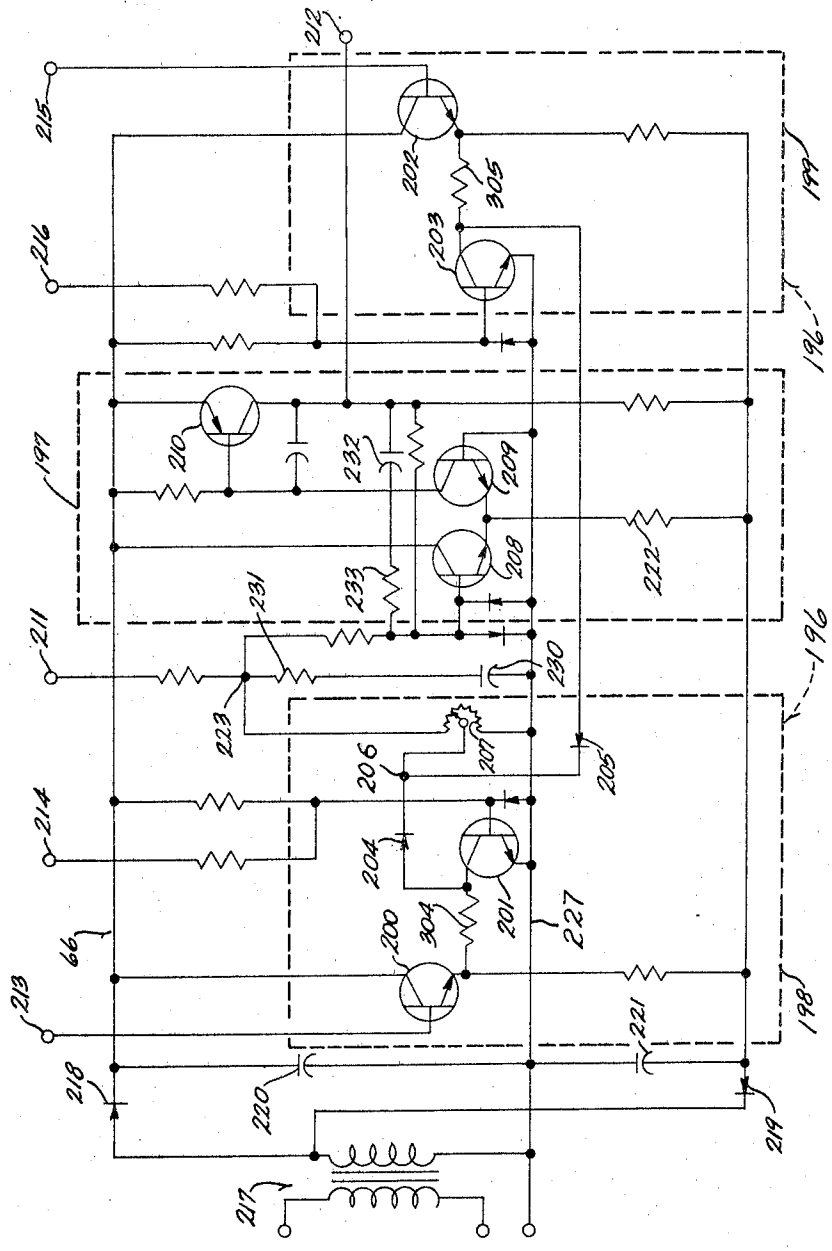


FIG. 6

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3,484,676

FIRING CIRCUIT FOR CONTROLLED RECTIFIER MEANS

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Original application Oct. 21, 1965, Ser. No. 499,409, now Patent No. 3,435,316, dated Mar. 25, 1969. Divided and this application May 13, 1968, Ser. No. 728,634
Int. Cl. H02m 7/44, 7/68
U.S. Cl. 321—47 10 Claims

ABSTRACT OF THE DISCLOSURE

A firing circuit for a controlled rectifier means interposed between an alternating current source and an inductive load supplies two firing pulses during each half cycle of the applied alternating current voltage. The first firing pulse causes the controlled rectifier bridge to energize the load responsive to an input signal. The second pulse, which occurs near the end of each half cycle, provides for a rapid reduction of the inductive energy of the load when the load is de-energized. The provision of the second pulse is independent of the input signal to the firing circuit.

CROSS-REFERENCES TO RELATED APPLICATIONS

This application is a divisional application of copending application Ser. No. 499,409, filed Oct. 21, 1965, now U.S. Patent 3,435,316 issued on Mar. 25, 1969.

BACKGROUND OF THE INVENTION

Field of the invention

The present invention relates to pulse generating circuits and more particularly to pulse generating circuits utilizable as firing circuits for controlled rectifiers.

DESCRIPTION OF THE PRIOR ART

DC motor braking—general

Many applications of DC motors require that the motor be braked during operation. For example, extremely accurate speed control may require that the motor be braked as soon as it exceeds a desired speed. Other examples include DC motors subjected to overhauling loads, as in crane, hoist, and elevator service.

The method and apparatus for controlling such braking action have presented problems for many years. A simple mechanical brake on the motor output shaft is sometimes employed. While such a device is inexpensive, its braking action is difficult to control. Maintenance of the mechanical brake also raises problems. The use of an external electro-mechanical brake, such as an eddy current brake, solves some of the foregoing problems but, on the whole, external brakes have generally proven unsatisfactory.

A DC motor may also be braked by adjusting the energization of the armature and field of the motor. One such method is termed plugging and involves reversing the motor armature voltage and current when it is desired to brake the motor. While the reduction in speed is rapid and the electrical apparatus required is little and inexpensive, the high circulating currents in the armature circuit place a large thermal strain on the motor. Repeated braking operations cannot be performed without excessive heating and damage to the motor.

In dynamic braking of a DC motor, a resistor is placed in the armature circuit. The motor in effect becomes a DC generator supplying power to the resistor load. While a

resistor limits the armature current and hence the thermal strain on the motor, it also decreases the effectiveness of the braking action, particularly at low speeds.

Regenerative braking of DC motors also employs the motor as a generator, similar to dynamic braking. However, the vital difference is that in regenerative braking the power generated by the motor is supplied back to the active power source for the motor rather than being circulated through a passive resistor load. Reduced to its essence, power may be regenerated, or supplied back to the active power source for the motor, by reversing the polarity of the armature voltage while maintaining armature current flow in the same direction or by reversing armature current flow while maintaining the polarity of the armature voltage. In either case the motor that was formerly a load becomes a power source. The advantages of such a system include the fact that braking may be done on a permanent basis, whereas plugging and dynamic braking are effective only in transient conditions or for isolated stops. Also, with proper control, the armature current may be limited, thereby eliminating the excessive motor heating experienced with other methods of braking. Braking may also be accomplished very rapidly.

Although alternating current is used as input power to a direct current motor control for many reasons, its use is particularly adapted to DC motor controls providing regenerative braking to the motor. As the voltage polarity of such an input is continually reversing on a periodic basis, voltage of either polarity may be supplied to the motor by connecting the alternating current source to the motor at the proper time.

During motoring operation, the DC motor control rectifies the alternating current input to use half cycles of one polarity of the AC power to apply a unipolarity voltage to the motor armature. The motor field is also energized with direct current to cause the motor to rotate. The rotation of the armature through the flux of the motor generates a counter E.M.F. opposing the applied voltage. The power control means, such as controlled rectifiers, in the control are arranged to be properly biased for conduction any time the counter E.M.F. is more negative than the applied voltage and to supply power from the control as a source to the motor as a load.

During regenerative operation, to cause the motor to become a source for the control, the motor field is reversed, reversing the motor flux and the polarity of the counter R.M.F. (assuming the direction of motor rotation remains instantaneously the same). The reverse counter E.M.F. again biases the controlled rectifiers to conduct current, in the same direction as during motoring, any time the counter E.M.F. is more negative than the applied alternating voltage. This includes portions of the half cycles of the other polarity, thus permitting the reversal of voltage at the control terminals necessary for regenerative operation. A regenerative DC motor control must therefore provide unidirectional current in the armature circuit any time the counter E.M.F. of the motor is more negative than the alternating voltage of the alternating current power source. This requires control during all of one half of each cycle of the alternating current input and for a portion of the other half cycle of that input.

The direction of current flow through the motor field and the motor flux generated by the current may be controlled by a controlled rectifier means which permits current to flow in either direction through the motor field.

Prior art regenerative controls have generally dissipated the energy of the motor field, during a reversal thereof to initiate regenerative operations, in to a resistive network in the field circuit. This requires some finite time for dissipation. During this time, the motor is

essentially uncontrolled being in neither the motoring nor the regenerating state, and it is highly desirable to hold such time to a minimum.

SUMMARY OF THE INVENTION

It is the object of the present invention to provide an improved firing circuit for a controlled rectifier means interposed between a source and a load, typically an inductive load such as a motor field. The firing circuit may operate the controlled rectifier means to provide variable energization to the load and it may further operate the controlled rectifier means to rapidly reduce the inductive energy of the load when it is desired to de-energize the load.

The firing circuit may operate the controlled rectifier means to provide current in either direction through the load and hence is suitable for use in the field circuit of a regenerative motor control having a controlled rectifier means to energize the motor field. Such a firing circuit reduces to a minimum the time required for reversal of the motor field.

The firing circuit supplies two firing pulses to the controlled rectifier means during each half cycle of the alternating current applied by the source to the load. The instant of applying the first pulse is proportional to the magnitude of an input signal to the firing circuit and operates the controlled recifier means to provide variable energization to the load. The application of the second pulse is independent of any input signal and occurs whether an input signal is present or not. The second pulse occurs in the latter part of each half cycle and operates the controlled rectifier means to rapidly reduce the inductive energy of the load, as by regenerating the energy back to the source.

BRIEF DESCRIPTION OF THE DRAWING

The specification includes the following drawings, forming a part thereof:

FIGURE 1 is a schematic diagram of the static, regenerative direct current motor control in which the firing circuit of the present invention may be employed;

FIGURE 2 is a graph of an alternating current wave form showing the principles of motoring and regenerative operation of the control;

FIGURE 3 is a detailed schematic drawing of an operational amplifier which may be used in the control of FIGURE 1;

FIGURE 4 is a schematic diagram of the controlled rectifier firing circuit of the present invention which may be used to operate the controlled rectifier means in the motor field circuit of the control of FIGURE 1;

FIGURE 5 is a schematic diagram of a controlled rectifier firing circuit which may be used to operate the rectifiers of the controlled rectifier bridge in the armature circuit of the control shown in FIGURE 1;

FIGURE 6 is a schematic diagram of a current regulating and regenerative logic circuit which may be used in the control shown in FIGURE 1; and

FIGURE 7*a* and *b* are wave forms illustrating the regenerative operation of the motor field.

DESCRIPTION OF PREFERRED EMBODIMENT

Brief description of static, regenerative, DC motor control

In the following specification the static, regenerative, DC motor control is described as one in which the speed of the DC motor is regulated. It is to be understood that other operative conditions of the motor, such as torque, or operative conditions in the apparatus driven by the direct current motor, as for example, web tension, may be the regulated quantity. Hence, the control is not to be construed solely as a motor speed control.

Referring now to the drawings, and specifically FIGURE 1, a block diagram of a static, regenerative, DC motor control **10** is shown therein. Control **10** includes reference and feedback circuit **14**, operational amplifier **16**, field circuit **18**, and armature circuit **20**. The control drives the DC motor **22** consisting of armature **24** and motor field **26** each of which includes or comprises an electromagnetic coil or winding. The control is provided with input power from three phase AC lines **28**.

Reference and feedback circuit **14** includes a reference signal source **30** providing a variable DC signal to conductor **32** by means of DC supply **33** and potentiometer **31**. A feedback signal is provided by tachometer **34** which is connected to armature **24** and supplies a DC signal corresponding to the speed of armature **24** to conductor **36**. Conductors **32** and **36** are joined at mixing junction **38** which provides an error signal to conductor **40**. The error signal may be of either polarity and serves as a motoring control signal in one polarity and a regenerative braking control signal in the other polarity.

The error signal in conductor **40** is fed to operational amplifier **16** which provides a high degree of amplification to the error signal. In subsequent portions of the specification or in the claims, this amplifier may be termed the "first" amplifier to distinguish it from other amplifiers in control **10**. Amplifier **16** has two output signals, both of which have abrupt saturation points. Both of the signals are proportional in magnitude to the input signal. However, the polarity of one output signal is the same as the polarity of the input error signal in conductor **40** (termed the direct output signal) while the other output signal is of the opposite polarity from the input error signal in conductor **40** (termed the inverse output signal). The graph of these output signals forms an X with the direct output signal forming one stroke, and the inverse output signal forming the other and the two signals meeting at zero output for operational amplifier **16**. One of the output signals is used to control both field circuit **18** and armature circuit **20** while the other is used to control only armature circuit **20**. While FIGURE 1 shows the inverse output signal of operational amplifier **16** as being supplied to both field circuit **18** and armature circuit **20** and the direct output signal of operational amplifier **16** as supplied through conductor **239** to armature circuit **20** only, the connection of these output signals may be reversed and the invention is not to be interpreted as limited to the connection shown in FIGURE 1. In any event, both signals are employed throughout all operational sequences of control **10**.

Field circuit **18** includes motor field **26**. The field circuit is supplied with alternating current from AC supply lines **28** through transformer **42**. The output of transformer **42** contains a controlled rectifier means comprising two groups of oppositely connected controlled rectifiers **44** and **46** and **48** and **50**. These rectifiers control the direction of current flow through motor field **26**, one group of rectifiers benig energized for each direction of current flow. A field controlled rectifier firing circuit **52**, which may be considered a push-pull proportional firing circuit, controls the operation of controlled rectifiers **44** through **50** in response to the inverse output signal from operational amplifier **16**. The control provided by field controlled rectifier firing circuit **52** determines which group of controlled rectifiers will be placed in the conductive state and may also include a determination of the magnitude of the field current. Firing circuit **52** also provides for rapid reversal of the current through motor field **26** by controlling the operation of the controlled rectifiers in a manner to regenerate the motor field current back to AC supply lines **28**.

Filed circuit **18** also contains a resistive network comprising resistors **54** and **56**. These resistors act as a limiting impedance to prevent short circuits in the motor field power circuit in the event of faulty firing of the controlled rectifiers and, as a secondary function, reduce the time constant of motor field **26**. Resistors **58** and **71** provide a means of sensing the polarity of the motor field current.

Armature circuit **20** supplies power to armature **24** during motoring operation and receives power from armature **24** during regenerative operation. Armature circuit **20** is supplied with power during motoring operation from AC supply lines **28** through transformer **60**. The amount of power provided to armature **24** is controlled by armature controlled rectified bridge **62** containing controlled rectifiers **146** through **151**. Terminals **306** and **307** constitute the output terminals of control **10**. During regenerative operation power is supplied from motor armature **24** through armature controlled rectifier bridge **62** and transformer **60** back to AC supply lines **28**.

Armature controlled recetifier firing circuit **64** controls the operation of the rectifiers in armature controlled rectifier bridge **62**. In order to provide reverse voltage capabilities, this firing circuit must be capable of controlling the operation of the controlled rectifiers through one entire half cycle of alternating current from supply lines **28** and through a portion of the other half cycle.

The current regulating and regenerative logic circuit **66** performs a dual function. The regenerative logic portion thereof determines whether a combination of conditions in control are proper for the regenerating or motoring operation and operates armature circuit **20** accordingly. In making such determination, the logic circuit utilizes a pair of AND gates operable by a field polarity signal supplied by sensing resistors **58** and **71** through conductors **68** and **69** as well as the direct and inverse output signals from operational amplifier **16** supplied through conductors **238** and **239**. The current regulating portion of circuit **66** regulates the armature current during motoring or regenerative operation and utilizes an armature current feedback signal supplied by conducto **70**.

DESCRIPTION OF OPERATION OF STATIC REGENERATIVE DC MOTOR CONTROL

The operation of control **10** may be better understood by initial reference to FIGURE 2 in which the numeral **228** indicates the alternating voltage supplied to the control through AC supply lines **28**. The supply voltage **228** includes a positive half cycle **229** and a negative half cycle **230**. Only a single phase of alternating current is shown in FIGURE 2 to simplify the explanation.

As previously mentioned, armature **24** generates a counter E.M.F. while rotating in the motoring state. This counter E.M.F. is indicated in FIGURE 2 by the graph **224** for the motoring operation of control **10**. The controlled rectifiers **146**, **148**, and **150** in armature rectifier bridge **62** may conduct any time applied voltage **228** is more positive than counter E.M.F. **224** since, as shown in FIGURE 1, the anodes of the controlled rectifiers may be considered connected to AC supply voltage **228** while the cathodes of the rectifiers are connected to the armature and counter E.M.F. **224**. The controlled rectifiers are properly biased for conduction anytime the anodes are more positive than the cathodes. This is the time interval between T_1 and T_2. The amount of power supplied to armature **24** and the speed of the motor **22** during motoring operation is determined by the point between T_1 and T_2 at which the rectifiers of rectifier bridge **62** are rendered conductive. The closer to time T_1 the rectifiers are rendered conductive, the greater the supplied power.

During regenerative operation, the energization of motor field **26** is reversed, reversing the polarity of the counter E.M.F. of the motor. The reversed counter E.M.F. is shown by the graph **225** in FIGURE 2. It will be noted that the time during which the counter E.M.F. of the motor is more negative than the applied voltage is now much greater, extending from time T_5 to time T_4. Referring to negative half cycle **230** it will also be noted that from time T_3 to time T_4 the voltage on the anodes of the controlled rectifiers **146**, **148**, and **150** in bridge **62**, that is, applied alternating voltage **228** has negative polarity with reference to the AC source.

Since the anodes of the controlled rectifier are more positive than the cathodes thereof, even though they are negative with reference to the AC source, the controlled rectifiers can conduct current in the same direction through bridge **62** if a signal is provided from armature controlled rectifier firing circuit **64**. This current will flow from armature **24** through the controlled rectifiers or armature bridge **62** and through transformer **60** in regenerative fashion to AC supply lines **28**. This is due to the fact that the polarity of the voltage on bridge **62** has reversed while the direction of current flow therethrough remains the same.

It is evident from the foregoing that armature controlled rectifier firing circuit **64** must be capable of firing the controlled rectifiers both from time T_1 to time T_2, for motoring operation, i.e., when the counter E.M.F. is more negative than the applied AC voltage, and also between time T_3 and T_4 for regenerative operation, i.e., when the applied AC voltage has reversed its polarity but before it becomes more negative than the counter E.M.F.

The operation of control **10** in the manner shown graphically in FIGURE 2 is accomplished by employing two operational loops. These may be termed the inner loop and the outer loop to indicate that the former operates within the confines of the latter. The outer operational loop is utilized to control motor speed and comprises tachometer **34**, operational amplifier **16**, current regulating regenerative logic circuit **66**, armature controlled rectifier firing circuit **64**, armature controlled rectifier bridge **62** and armature **24**. The outer loop controls the operation of control **10** as long as operational amplifier **16** is unsaturated. When operational amplifier **16** saturates, the above described outer loop becomes inoperative since further error signal changes in conductor **40** are not transmitted through operational amplifier **16**. For normal speed regulating operation, however, the operational amplifier of the outer loop is not saturated and the inner loop serves as an active part of the outer loop.

The inner operational loop is used to regulate armature current at all times in accordance with the amplified error signal from amplifier **16**. It comprises the armature current feedback signal in conductor **70**, current regulating and regenerative logic circuit **66**, armature controlled rectifier firing circuit **64**, armature controlled rectifier bridge **62**, and armature **24**. The inner loop is a complete feedback regulator employing as a reference signal one of the outputs of amplifier **16**, as selected by the logic portion of current regulating and regenerative logic circuit **66**, and as feedback, the signal in conductor **70**. The gain and response of this inner loop regulator are sufficient to cause the armature current to accurately and rapidly follow the signal from amplifier **16**, thereby causing the magnitude of armature current to be proportional to the error signal in conductor **40**. However, when the error signal becomes large enough to saturate the outputs of amplifier **16**, further increases in error signal can no longer cause an increase in armature current, since the reference signal to the inner current loop regulator cannot be larger than the saturated output of amplifier **16**. In this manner the maximum armature current is sharply limited to a value corresponding to the saturated output of amplifier **16**. One other consideration is important. Since the output of amplifier **16** may change almost instantly from a low level to its highest value the nature of response of the inner loop current regulator to an instantaneous rise in reference signal must include a complete lack of overshoot to prevet transient currents from being larger than the desired maximum value.

The field circuit **18** is operated open loop at or below the base speed of DC motor **22** except for the field polarity signal in conductor **68** and **69** to current regulating and regenerative logic circuit **66**. Above the base speed of DC motor **22**, field weakening is required.

To operate control switch **10**, switch **72** is closed to energize the circuitry of the control. Reference signal source **30** is adjusted to provide a signal corresponding to desired speed. The signal is supplied through conductor **32** to junction **38** and thence to operational amplifier **16**. Operational amplifier **16** produces a direct output signal and an inverse output signal proportional to the input signal in conductor **40**. As armature **24** is not yet rotating there will be no feedback signal supplied by tachometer **34**.

Field circuit **18** utilizes one of the output signals from operational amplifier **16** to turn on either rectifiers **44** and **46** or rectifiers **48** and **50** by means of field controlled rectifier firing circuit **52**. The desired direction of rotation of the motor is determined by which of the two groups of controlled rectifiers is turned on.

Both the inverse output signal and the direct output signal operational amplifier **16** are supplied to current regulating and regenerative logic circuit **66**. This circuit determines whether conditions in control **10** are proper for motoring or regenerative operation by means of the polarity of the output signals of operational amplifier **16** and the motor field polarity signals in conductors **68** and **69**. These signals operate the pair of AND gates in the logic portion of current regulating and regenerative logic circuit **66** and operate the armature circuit accordingly. For the present motoring operation, the logic portion of current regulating and regenerative logic circuit **66** determines that control **10** is, in fact, capable of such operation and passes the amplified error signal to the inner current regulating loop and thence to armature controlled rectifier firing circuit **64**. Armature controlled rectifier firing circuit **64** provides a firing signal to the controlled rectifier of armature controlled rectifier bridge **62** to energize armature **24** and accelerate the armature.

Acceleration of the armature **24** causes tachometer **34** to generate a feedback signal in conductor **36** which reduces the magnitude of the error signal in conductor **40**. This likewise reduces the magnitude of both outputs of operational amplifier **16** and causes armature controlled rectifier firing circuit **64** to retard the firing angle of the controlled rectifiers in armature controlled rectifier bridge **62**. Regulation of the speed of armature **24** is obtained by controlling the point of firing of the controlled rectifiers in armature controlled rectifier bridge **62** between time T_1 and time T_2, as shown in FIGURE 2, by the combined operation of the inner and outer operational loops.

Regenerative operation of control **10** may be brought on by reducing the reference signal in conductor **32** or by providing an overhauling load to armature **24**. In either case, the feedback signal generated by tachometer **34** in conductor **36** exceeds the reference signal generated by reference signal source **30** in conductor **32**. This reverses the polarity of the error signal in conductor **40** and hence the polarity of the inverse output signal and direct output signal from operational amplifier **16**. Because of the high gain of operational amplifier **16** a small reversal in the polarity of the error signal is sufficient to initiate regenerative operation.

The reversed polarity of the output signal from operational amplifier **16** to field controlled rectifier firing circuit **52** causes the latter circuit to energize the other group of controlled rectifiers in field circuit **18** reversing the current through motor field **26**. The time of reversal is short because the inductive energy stored in the winding of motor field **26** is regenerated through transformer **42** to AC supply lines **28** and because resistors **54** and **56** reduce the time constant of the field. The reversal of motor field **26** reverses the counter E.M.F. of armature **24** and the polarity of the signal in conductors **68** and **69**.

Operational amplifier **16** provides output signals of reversed polarity to the regenerative logic portion of current regulating and regenerative logic circuit **66**. In the absence of the correct motor field polarity signal from conductors **68** and **69** the logic circuit produces no output at all. The correct signal in conductor **68** or **69**, indicating motor field has completed reversal, provides a signal from current regulating and regenerative logic circuit **66** to armature controlled rectifier firing circuit **64** which controls the point of firing of the controlled rectifiers between time T_3 and T_4 as shown in FIGURE 2 depending on the magnitude of the error signal in conductor **40**. As described in connection with that figure this operation provides regenerative power to alternating current supply lines **28**.

If the error signal in conductor **40** is excessively large during either motoring or regeneration, the operational amplifier **16** becomes saturated and control over armature circuit conditions is delegated to the inner loop including current regulating portion of current regulating and regenerative logic circuit **66**. The current feedback signal is supplied from the armature circuit to the current regulating portion of current regulating and regenerative logic circuit **66**. This circuit alters the output signal to armature controlled rectifier firing circuit **64**, after comparing the feedback signal with a reference signal comprised of the saturated output of operational amplifier **16**, to retard a firing angle of the controlled rectifiers in armature controlled rectifier bridge **62** to maintain the armature current at the desired maximum value.

The following comprises the detailed description of the various components of control **10** shown in FIGURE 1. It is to be understood that the invention is not limited to the specific embodiments incorporated in this detailed description but may utilize equivalent circuits having similar functional characteristics.

DETAILED DESCRIPTION OF OPERATIONAL AMPLIFIER

As previously mentioned, this amplifier has a single input and two outputs. Both of the output signals are proportional in magnitude to the input signal. However, the polarity of one output signal is the same as the polarity of the input signal while the other output signal is opposite in polarity to the input signal. The first mentioned output signal has been termed the direct output signal while the latter signal is termed the inverse output signal. The amplifier must, of course, be capable of handling input signals from conductor **40** of either polarity.

FIGURE 3 shows a circuit suitable for use as operational amplifier **16** of control **10**. The operational amplifier contains two complementary, three-stage amplifiers. One such amplifier, **73**, is formed of transistors **74**, **76** and **78** while the other such amplifier, **75**, is formed from transistors **80**, **82** and **84**. The input transistors of each of the aforementioned amplifiers, that is, transistor **74**, and transistor **80** are closely matched for identical characteristics, so that the tendency of one such transistor to drift under operating conditions will be closely matched by the same tendency of the other transistor, thereby producing equality in the overall effect on the two amplifiers.

Amplifiers **73** and **75** are powered by a power supply consisting of transformer **86**, diodes **88**, and **89** and capacitors **90** and **91**. The power supply also includes a voltage divider consisting of resistor **92** and resistor **93**.

For reasons of overall circuit operation, it is desirable to maintain the input to input transistors **74** and **80** at zero volts. Thus, a low impedance path for the small base current required to establish the operating points of transistors **74** and **80** is provided by resistors **94** and **95** which are joined to the center of the voltage divider network. The voltage divider network provides a small voltage which is used to null the small voltage drop across resistors **94** and **95** caused by the current.

The input signal from conductor **40** is applied to operational amplifier **16** at terminals **96** and **97**. A pair of diodes **98** and **99** connected in opposite polarities across input terminals **96** and **97** limit the magnitude of the input signals to that which can be handled by the operation of the amplifier. Specifically, when the magnitude of the in-

put signal exceeds the forward conduction voltage of diodes **98** or **99**, the diodes break down and short circuit terminals **96** and **97** thereby preventing an input signal in excess of the breakdown voltage from reaching amplifiers **73** or **75**. This prevents excessive input signals from overdriving either of the amplifiers. Two diodes **98** and **99** are provided to accommodate input signals of either polarity.

The amplifier utilizes two feedback circuits. The first of these feedback circuits may be called the common mode feedback as it affects both transistor amplifier **73** and transistor amplifier **75** in an equal manner. The common mode feedback utilizes resistor **100** which measures the sum of the currents through the output of transistors **78** and **84**, that is, through the collector and emitter terminals of those transistors. The feedback signal comprising the voltage developed across resistor **100** is compared with a reference signal generated by a voltage divider consisting of resistor **101** and a rheostat **102**. The error signal between the feedback signal from resistor **100** and the reference signal from rheostat **102** is supplied through transistor **103** and resistors **104** and **105** to the emitters of transistors **74** and **80** to adjust the sum of the output of these transistors for any difference between the reference signal indicating actual total current. Transistor **79** and resistor **77** establish the operating point of transistor **103**. It will be appreciated that a high degree of amplification is obtained through transistor **103** and the three transistors constituting each transistor amplifier **73** and **75** thereby providing rapid, accurate regulation of the sum of the output of transistors **74** and **80**.

The second feedback circuit in operational amplifier **16** is termed the differential feedback as it affects differentially amplifiers **73** and **75**. This feedback may be resistive, inductive, or capacitive; the character of the feedback changing the operating characteristics of the amplifiers which the feedback serves. For example, varying the resistance of the feedback will vary the amount of gain of the amplifier, while varying the capacitance of the feedback will vary the response time of the amplifier. Specifically, in FIGURE 3 a differential feedback is shown by conductor **106** which provides a feedback signal from the emitter collector circuit of transistor **78** through capacitor **107** to input terminal **97**.

The output signals from operational amplifier **16** are supplied to terminals **108** and **109**. The direct output signal appears at terminal **108** while the inverse output signal appears at terminal **109**.

The first mode of operation, called the common mode, is one in which a given signal or phenomenon affects both transistor amplifiers **73** and **75** in an equal manner. Examples of common mode signals or phenomenon include variations in line voltage or variations in ambient temperature. As can be readily appreciated, it is necessary that such occurrences affect both transistor amplifier **73** and transistor amplifier **75** equally in order to maintain proper operation of control **10**. The second mode of operation, termed the differential mode, is one in which a given signal or phenomenon affects one of the transistor amplifiers in a different manner than it affects the other transistor amplifier. Examples of differential mode signals include an input signal to terminals **96** and **97** or unequal drift of one or the other of transistor amplifiers **73** and **75**.

As previously mentioned, the common mode feedback circuit including resistor **100** and the reference circuit including rheostat **102** insure that the total current flowing through output transistors **78** and **84** and transistor amplifiers **73** and **75** is equal to that established by the reference signal. Thus any changes in the total current due to such things as variation in line voltage or in ambient temperature are immediately corrected by the aforementioned reference and feedback signals and the high degree of amplification provided by transistor **103** and the three transistors in each of amplifiers **73** and **75**.

Operation of operational amplifier **16** in the differential mode to obtain the aforementioned direct output signal and inverse output signal is obtained by first adjusting operational amplifier **16** so that the signals at output terminals **108** and **109** are both equal to zero. Once this is accomplished, variations in the output signal at terminal **109** due to an input signal to terminals **96** and **97**, is accompanied by an equal and opposite change in the output signal at terminal **108**, as the total current through both transistor amplifiers **73** and **75** must remain the same because of the above described regulation provided by the feedback signal from resistor **100** and the reference signal from rheostat **102**.

To provide initial adjustment to operational amplifier **16**, output terminal **109** is connected through resistor **81** to input terminal **97**. Resistor **81** forms a negative feedback path which tends to reduce the output signal at terminal **109** of transistor amplifier **73** to zero potential with respect to terminal **96**. The output signal at terminal **109** is brought to exactly zero by adjusting rheostat **110** to alter the current input to transistor amplifier **75**. Assuming that the output signal at terminal **109** is greater than zero, a signal would be applied from rheostat **110** to the input of transistor amplifier **75** to cause that amplifier to conduct more heavily. This removes some of the current flowing through transistor amplifier **73** and reduces the output signal existing at terminal **109**. The reduction in current through transistor amplifier **73** occurs because the total current flowing through both transistor amplifiers **73** and **75** must remain at the value regulated by rheostat **102** and hence an increase in the current flow in one amplifier must require a decrease in current flow in the other.

After the output signal at terminal **109** has been brought into coincidence with the voltage at input terminals **96** and **97**, rheostat **102** is adjusted to alter the output signal at terminal **108** so that it is also at zero. Adjustment of rheostat **102**, of course, changes the amount of current in the output of the two transistor amplifiers **73** and **75**.

However, since the output of transistor amplifier **73** is fixed by the feedback signal between its output terminal **109** and its input terminals **96** and **97**, the output of transistor amplifier **75** is varied, thereby to alter the output signal existing at terminal **108**. The connection between output terminal **109** and input terminals **96** and **97** may then be removed and from this time on, an input signal to terminals **96** and **97** produces two equal output signals of opposite polarity.

It will be appreciated that the three stages of amplification in amplifiers **73** and **75** provide a high gain characteristic to operational amplifier **16**. This allows the amplifier to be extremely sensitive to changes in the polarity of the error signal in conductor **40** to operate control **10** in the motoring state or the regenerative state as required by that signal. The "dead band" found in prior art controls of this type, in which the control is unable to operate in the correct state, is thereby eliminated.

As a general rule, the output signal at terminal **109**, that is, the inverted output signal is connected to field control rectifier firing circuit **52** and to current regulating and regenerative logic circuit **66**. The direct output signal from terminal **108** is also connected to the current regulating and regenerative logic circuit **66**. However, it is anticipated that the connections of output terminals **109** and **108** to field control rectifier firing circuit **52** and to the current regulating and regenerative logic circuit **66** will be reversed in a considerable number of applications of control **10**.

DETAILED DESCRIPTION OF MOTOR FIELD CIRCUIT

Motor field **26** is energized by center tap transformer **42** which has the motor field **26** connected in the center tap thereof. Each end of center tap transformer has one rectifier of two complementary rectifier groups connected thereto. Specifically, controlled rectifiers **44** and **46** con-

stitute one group of rectifiers and conduct current through motor field **26** in one direction while controlled rectifiers **48** and **50** constitute the other group and conduct current through motor field **26** in the opposite direction. These rectifiers may be, and are shown in FIGURE 1 as, silicon controlled rectifiers having an anode terminal, a cathode terminal and a gate terminal. Applying a signal to the gate terminal permits the rectifier to conduct current or "fire," when the anode and cathode terminals are properly biased.

It will be appreciated that, should one rectifier of each group accidentally be turned on simultaneously, a dead short would result around a circuit comprising the two controlled rectifiers and transformer **42**. Such short circuiting has been a failing of prior art controls of this type as it disables the field circuit. To prevent excessive field current from occurring under such conditions, resistors **54** and **56** are included in the motor field circuit to provide a current limiting impedance. It will be appreciated that if other means are provided to protect the motor field circuit from controlled rectifier misfires, current limiting impedences may be eliminated. These resistors also reduce the inductive time constant of motor field **26** when it is desired to reverse the direction of current flow through the motor field.

The firing of controlled rectifiers **44** through **50** controlled by the field controlled rectifier firing circuit of the present invention which operates the aforementioned controlled rectifiers to control the amount of current in either direction through the field from zero to maximum and provides for the rapid reversal of the current through motor field **26** by regenerating the inductive energy contained therein back to AC supply line **28**. FIGURE 4 shows a field controlled rectifier firing circuit which may be used as circuit **52** of control **10** shown in FIGURE 1. Firing circuit **52** is a push-pull proportional amplifier in that it provides control to one group of rectifiers for an input signal from operational amplifier **16** of one polarity and provides control to the other group of rectifiers for an input signal from operational amplifier **16** of the opposite polarity. In instances wherein it is not desired to control the magnitude of the field current, the firing circuit **52** may have sufficient gain so that a small input signal will drive it full on.

Firing circuit **52** contains two uni-junction firing circuits **114** and **115**, each of which controls one of the groups of controlled rectifiers **44** through **50** in the motor field circuit in response to an input signal supplied to terminals **116** and **117**. Each of the uni-junction firing circuits includes a uni-junction transistor **118** and **119** which provides firing pulses through transistors **120** and **121** to output terminals **122** and **123**. For example, output terminal **122** may be connected to controlled rectifiers **44** and **46** while output terminal **123** may be connected to controlled rectifiers **48** and **50**. Transistors **120** and **121** insure that the output pulses from uni-junction transistors **118** and **119** are of sufficient magnitude and duration to fire controlled rectifiers **44** through **50**.

The aforementioned firing circuits **114** and **115** are provided with a main energization circuit, comprised of differential amplifier **124** and alternate energization circuits **125**. Differential amplifier **124** is connected to input terminals **116** and **117**. A differential amplifier is used to insure an input operating level near zero and to provide balanced push-pull operation. Each of the inputs is connected to a two stage portion of the differential amplifier **124**. Specifically, input **116** is connected to input transistor **126** which in turn is connected to output transistor **127** while input **117** is connected to input transistor **138** and to output transistor **130**. If the input levels to these terminals is zero, the output from differential amplifier **124** will be of insufficient magnitude to turn on output transistors **127** and **130**. Thus no energization signal will be supplied to uni-junction transistors **118** and **119**. If input signals in one polarity or the other are supplied to terminals **116** and **117**, either transistor **127** or transistor **130** will become conductive. Current flow through the conductive transistor will charge either capacitor **131** or capacitor **132** which will supply an input signal to the respective uni-junction transistor **118** or **119**, through diodes **300** and **301** to turn on either controlled rectifiers **44** and **46** or controlled rectifiers **48** and **50**.

In addition to the aforementioned main energization circuit for uni-junction transistors **118** and **119** there is an alternative energization circuit for each of the uni-junction transistors which is completely independent of any input signal to terminals **116** and **117**. These circuits, **125**, comprise resistor **327**, resistor **328**, and capacitor **329** and resistor **330**, resistor **326** and capacitor **332** respectively. The voltage provided by these circuits to the inputs of the uni-junction transistors through diodes **133** and **134**, respectively, is slightly less than that needed to place the uni-junction transistors in the conductive state. The operation of these circuits will be subsequently explained.

Field controlled rectifier firing circuit **52** is energized from a power supply comprised of transformer **135**, diodes **136**, **137**, and **302** and capacitor **303**.

Synchronization of field controlled rectifier firing circuit **52** with the alternating current existing in transformer **42** energizing motor field **26** is accomplished by synchronizing circuit **138**. Synchronizing circuit **138** includes resistor **139**, resistor **140**, Zener diode **141** and transistor **142**. Transistor **142** supplies power across the two base terminals of uni-junction transistors **118** and **119** and alternate energization circuits **125**. The period of each half cycle of alternating current input from supply lines **28**, during which power will be supplied across the base terminals of uni-junction transistors **118** and **119** is determined by the time interval during which current will flow through Zener diode **141** and transistor **142**. This interval initiates approximately 10° after the beginning of the half cycle and terminates approximately 10° before its end. During this time, a signal supplied from differential amplifier **124** will cause one or the other of uni-junction firing circuits **114** and **115** to turn on either one of the two groups of controlled rectifiers **44** through **50** in the motor field circuit **18**. The instant at which the firing signal is generated is determined by the magnitude of the input signal to terminal **116** or terminal **117**, an input signal of greater magnitude tending to generate a firing signal closer to the initial portions of the half cycle of alternating current, thus controlling the magnitude of the field current as well as its direction.

It is to be noted that since alternating current is applied to the controlled rectifiers, a short circuited condition in the field circuit due to stray firing can exist for only one half cycle of AC. At the end of the half cycle, the condition will automatically correct itself as the stray fired rectifier will be biased nonconductive by the applied AC.

During the time interval that power is supplied to the bases of unijunction transistors **118** and **119**, alternate energization circuits **125** will have had sufficient time to charge capacitors **329** and **332** through resistors **327** and **328** and **330** and **326** respectively. However, as previously mentioned, the voltages across capacitors **329** and **332** are insufficient to fire the uni-junction transistors when full input power is applied across the base terminals thereof. Near the end of the cycle, the voltage applied to the base terminals of uni-junction transistors **114** and **115** necessarily becomes less as the end of the half cycle of alternating current input approaches. Under these conditions of lessened voltage across the bases of uni-junction transistors **118** and **119**, the voltage existing across capacitors **329** and **332** becomes sufficient to fire the uni-junction transistors. This generates a firing pulse near the end of each half cycle of alternating current. It is to be noted that the firing signal generated in uni-junction transistors **118** and **119** by alternate energization circuits **125** is completely independent of any signal generated in uni-junction transistors **118** and **119** by dif-

ferential amplifier **124**, and occurs even though no input is applied to terminals **116** or **117**.

With no input signals to terminals **116** or **117**, the firing signals caused by alternative energization circuits **125** are supplied to all four rectifiers **44** through **50** of the two complementary groups that control the direction of current flow through motor field **26**. As the firing pulses are supplied to all the rectifiers, the positive voltage generated in two of the rectifiers is opposed by the negative voltage generated in the other two rectifiers so that the net effect of the voltage across the motor field is zero.

When an input signal is applied to terminals **116** and **117**, the firing pulse generated by alternative energization source **125** has no effect on the group of rectifiers being controlled by the main energization circuit **124** since one of these rectifiers is already conducting and the other is improperly biased for conduction. The firing pulses provided to the other group of rectifiers by alternative energization source **125** generates a current which opposes the current of the conducting rectifier. However, this condition terminates as the applied voltage reverses and the power loss to motor field **26** is of minor significance as it exists for only 10° of the half cycle.

The firing pulses generated by alternate energization circuits **125** are used to rapidly reduce the current of the motor field to zero by regenerating the inductive energy stored in the field back through transformer **42** to AC supply lines **28**.

Under normal operation of motor field circuit **18** where, for example, rectifiers **44** and **46** are alternately rendered conductive by field controlled rectifier firing circuit **52**, the graph of the voltage at the right hand terminal of the field is shown by the graph **234** in FIGURE *7a*. This is a fully rectified voltage which produces a DC current **235** through the field. The conducting rectifier is indicated below each half cycle of graph **234**.

If, at some time T_1, rectifier **46** is not turned on during the appropriate half cycle, current will continue to flow through the motor field due to its inductive characteristics. In order to maintain this current flow the motor field **26** becomes a source whose voltage exceeds the applied voltage in transformer **42** during the negative half cycle for rectifier **44**. Rectifier **44** will continue to conduct during its normal half cycle as it is then properly biased for conduction. The graph of FIGURE *7a* subsequent to time T_1 shows the field voltage under conditions where rectifier **46** is not turned on. It will be noted that, in effect, alternating voltage is applied to the field. This causes the field current to decay with a slight ripple to zero at time T_2. At this time rectifier **44** becomes nonconductive as there is no current therethrough and the voltage across the field ceases. It may be noted that the decay of inductive current in the motor field in the above circumstances is no more satisfactory than the time constant of the motor field.

It may also be noted that during the time that the motor field may be considered a source, the field is regenerating power to alternating current lines **28**, as current is maintained in the same direction through the circuit but through the polarity of the source terminals in transformer **42** has reversed. However, during the positive half cycle of rectifier **44** power is supplied to the field. This supply and regeneration of power results in little net difference and for all practical purposes may be disregarded. Thus, there is no net regeneration or power supply to the motor field and the inductive energy of the field circuit is dissipated in its resistive portion.

In the control of the present invention, rectifiers **44** and **46** are fired on approximately 10° before the end of the half cycle of applied alternating current voltage by alternate energization means **125** in controlled rectifier firing circuit **52**. The effect of this operation is shown in FIGURE *7b*. As before, a plurality of cycles may be assumed to have preceded the graph in FIGURE *7b*. Also as before, rectifier **44** is fired on but rectifier **46** is not turned on at the appropriate time to conduct current through the motor field from the AC source. This then causes rectifier **44** to continue to remain on to conduct current from the motor field, as a source, through transformer **42**. Approximately 10° before the end of the half cycle rectifier **46** is fired on. This turns off rectifier **44** as the current now has an alternative path through rectifier **46** which is preferred since it is in the direction that transformer **42** desires to provide power to motor field **26**. Rectifier **46** conducts power to the motor field for the remaining 10° of half cycle. At the end of the half cycle, the regenerative operation continues as rectifier **44** is not turned on and rectifier **46** is forced to remain on as the only path available for current flow. As the voltage of transformer **42** reverses, current is supplied to the positive terminal thereof forming the regenerative action.

For subsequent half cycles, similar operations are performed. This is, rectifier **44** is turned on in the last 10° of the half cycle to regenerate the inductive energy of the motor field back to power lines **28** when the voltage of transformer **42** again reverses. The net effect is a very large regenerative portion of the half cycle and a small power supplying portion; the power supplying portion being only the final 10° of each half cycle. This rapidly reduces the current in the motor field **26** as shown in FIGURE *7b*.

DETAILED DESCRIPTION OF ARMATURE CIRCUIT

Motor armature **24** is inserted across the output terminals of armature controlled rectifier bridge **62** of control **10**. Armature controlled rectifier bridge **62** comprises controlled rectifier **146**, **147**, **148**, **149**, **150**, and **151** arranged in complementary pairs and connected in a conventional three phase bridge configuration having output terminals **306** and **307**. The three phase secondary winding of transformer **60** is connected to the input terminals of armature controlled rectifier bridge **62**.

The control of controlled rectifiers **146** through **151**, both as to which rectifiers will conduct and for how long, is controlled by armature controlled rectifier firing circuit **64**. As previously mentioned, this firing circuit must control the operation of the controlled rectifiers of armature controlled rectifier bridge **62** throughout the entire period when the counter E.M.F. is more negative than the applied alternating current voltage.

FIGURE 5 shows a firing circuit suitable for use as armature controlled rectifier firing circuit **64**. Firing circuit **64** is, in reality, three separate firing circuits or amplifiers **264**, **364**, and **464**, each of which is connected to a complementary pair of controlled rectifiers in armature controlled rectifier bridge **62** to conduct current from transformer **60** through armature controlled rectifier bridge **62** to armature **24** and back through armature controlled rectifier bridge **62** to transformer **60**. The input signal to armature controlled rectifier firing circuit **64** is supplied to terminals **156** and **157** and input transistors **158**, **159** and **160**. These transistors are connected to the three firing amplifiers **264**, **364**, and **464**. Current feedback from the individual firing circuits to input transistors **158** through **160** is provided by resistors **161**, **162** and **163**, and by rheostat **164** and rheostat **165**. These feedbacks stabilize the input to firing circuits **264**, **364** and **464** and also, by adjustment of rheostats **164** and **165**, balance the inputs of the three individual firing amplifiers.

Firing amplifiers **264**, **364** and **464** contain identical circuitry, and for purposes of explanation only firing amplifier **264** will be explained in detail. It is to be understood that firing amplifiers **364** and **464** are identical in construction.

Referring now to firing amplifier **264**, the output of input transistor **158** is supplied through resistor **166** to capacitor **167** which supplies an input to uni-junction transistor **168**. The output from the base terminals of uni-junction transistor **168** is applied to a pair of transistors

169 and 170. These transistors form a two-transistor analogy to a silicon controlled rectifier. That is, they form a four layer semi-conductor structure similar to that found in a silicon controlled rectifier. The combined operation of transistors 169 and 170 is similar to that of a silicon controlled rectifier and it is to be understood that such a controlled rectifier may be used if desired. The two-transistor analogy to silicon controlled rectifier operation is explained more thoroughly in the second edition of the Silicon Controlled Rectifier Manual published by the General Electric Company in 1961.

Certain advantages accrue from the use of two-transistors 169 and 170 rather than a single silicon controlled rectifier in firing amplifier 264. Specifically, the firing current and the holding current may be determined by passive elements in the network. The firing current is that current necessary to place the transistor or SCR in the conductive state when applied to the base or gate terminal. The holding current is that current which must pass between the two emitters of the two transistor configuration or between the anode and cathode of the silicon controlled rectifier in order to maintain the device in the conductive state. In firing amplifier 264 these currents are determined by the resistive network comprised of resistors 171, 172, 173, 174, and 175. Additionally, an extra terminal, that is the collector terminal of transistor 170, is provided by the two-transistor configuration that is unavailable when a silicon controlled rectifier is used.

The aforementioned collector terminal of transistor 170 is supplied to a uni-junction relaxation oscillator comprised of uni-junction transistor 176, capacitor 177, resistor 178, resistor 179 and resistor 240. The rate of oscillation of this oscillator is determined by the various circuit components connected therewith and is designed to be much faster than the rate of pulse generation provided by uni-junction transistor 168. It will be appreciated that, when a pulse is generated by uni-junction transistor 168, triggering and retaining transistor 170 in the conductive state, a signal will be applied from the collector of transistor 170 to uni-junction transistor 176 and a series of rapid pulses from the base terminals of uni-junction transistor 176 will be supplied to pulse transformed 180 for the remainder of a synchronization period, hereinafter described. The pulses from uni-junction transistor 176 are amplified by transistor 181 before being supplied to pulse transformer 180. Pulse transformer 180 is connected to two controlled rectifiers in armature controlled rectifier bridge 62 by output windings 380.

The rapid pulses from uni-junction transistor 176 will be supplied to pulse transformer 180 for the remainder of the synchronization period determined by synchronizing circuit 182. Synchronizing circuit 182 includes transistor 183, rectifier 184, resistor 185, resistor 186, rectifier 187, and capacitor 188 and serves to synchronize the operation of firing amplifier 264 to the AC supply frequency. Synchronizing circuit 182 is connected between the above described pulse generating components and a power supply comprised of transformer 189 and diodes 190 and 192. The primary of transformer 189 is connected to alternating current supply lines 28.

At the beginning of each half cycle of alternating current supplied by transformer 189, transistor 183 will be turned on rapidly by means of a signal supplied through rectifier 187 and resistor 185. Current flow through rectifier 187 also charges capacitor 188 so that its lower terminal is positive. The turning on of transistor 183 provides power to the remainder of firing amplifier 264 and allows a uni-junction transistor 176 to generate rapid pulses to pulse amplifier 180 when transistor 170 has been turned on by uni-junction transistor 168. The instant at which uni-junction transistor 176 begins generating pulses is determined by the magnitude of the input signal to terminals 156 and 157, input signals of greater magnitude tending to initiate pulse generations earlier in the positive half cycle of alternating current power.

At the end of the positive half cycle of alternating current, capacitor 188 discharges through resistors 186 and 185. This provides a bias to the base of transistor 183 that allows that transistor to remain on for a portion of the negative half cycle. When capacitor 188 is discharged, transistor 183 becomes nonconductive, terminating pulse generation by uni-junction transistor 176. The portion of the negative half cycle during which transistor 183 is conductive depends upon the magnitude of capacitor 188. Thus, firing amplifier 264 will initiate pulse generation by unijunction transistor 176 in the negative half cycle of alternating current power for a small input to terminals 156 and 157, i.e., from time T_3 to T_4 in FIGURE 2. As the input signal is increased, the initiation of pulse generation by uni-junction transistor 176 will advance from the negative half cycle of alternating current power into the positive half cycle and may be moved to near the beginning of the positive half cycle of alternating current. The pulses generated by uni-junction transistor 176 and supplied to pulse transformer 180 tend to place the controlled rectifiers in armature controlled rectifier bridge 62 in the conductive state. The controlled rectifiers will actually begin conducting when they have become properly biased across the anode and the cathode terminals.

By using a plurality of rapid pulses, armature controlled rectifier firing circuit 64 insures that the controlled rectifiers of armature controlled rectifier bridge 62 will be turned on at the earliest possible time they become properly biased across the anode and cathode. If the single pulse were employed to render the controlled rectifiers conductive, such pulse might be delivered at a time when the controlled rectifier was improperly biased and, hence, the controlled rectifier would never be turned on. The controlled rectifiers could also be turned on by an AC rider or straight DC energization to the gate terminal. However, if signals of this type of sufficient magnitude to insure dependable firing are used, they cause excessive gate dissipation, shortening the life of the controlled rectifier. It will be appreciated that, with the plurality of rapid pulses of short duration provided by the armature controlled rectifier firing circuit 64, excessive gate dissipation is prevented yet reliable firing is provided, since each individual pulse may be of considerable magnitude. Additionally, as previously mentioned, armature controlled rectifier firing circuit 64 insures that the controlled rectifiers will be turned on as soon as they are properly biased across their anodes and cathodes.

Current regulating and regenerative logic circuit 66 supplies the control or input signal to armature controlled rectifier circuit 64. A circuit which may perform the functions of armature current regulation and regenerative logic is shown in FIGURE 6. As its name implies, circuit 66 includes a regenerative logic portion 196 and a current regulating portion 197. Both the regenerative logic portions 196 and the current regulating portion 197 are energized by a power suply circuit consisting of transformer 217, rectifiers 218 and 219 and filter capacitors 220 and 221.

Regenerative logic portion 196 determines whether control 10 is capable of regenerating or motoring on the basis of the polarities of the signals from operational amplifier 16 and from the motor field via conductors 68 and 69 and operates the armature circuit 20 accordingly. Regenerative logic portion 196 is comprised of two AND gates which require the correct combination of signal polarities from the aforesaid sources to produce an output from one of them.

More specifically, regenerative logic portion 196 is comprised of AND gate 198 and AND gate 199. AND gate 198 consists of transistor 200, connected in emitter follower configuration, and transistor 201, while AND

gate **199** consists of transistor **202**, also connected in emitter follower configuration, and transistor **203**. The outputs of AND gates **198** and **199** are supplied through diodes **204** and **205**, respectively, and through rheostat **207** to the input of current regulating portion **197**.

The input signals to the regenerative logic AND gate **198** consist of the inverse output signal from operational amplifier **16** applied to input terminal **213** and the field polarity signal in conductor **68** applied to input terminal **214**. The input signals to the regenerative logic AND gate **199** consist of the direct output signal from operational amplifier **16** applied to input terminal **215** and the field polarity signal in conductor **69** applied to terminal input **216**.

For either AND gate **198** or AND gate **199** to open and supply a signal to current regulating portion **197**, input signals of the correct polarity must be present at both input terminals of the AND gate. For example, during motoring operation in one direction, an input signal from operational amplifier **16** is supplied to terminal **213** which is of a polarity to bias transistor **200** into the conductive state. An input signal from conductor **68** to terminal **214**, indicating the direction of current flow in the motor field **26**, will be of a polarity to bias transistor **201** off, thereby preventing that transistor from diverting the output of transistor **200** to conductor **227**. This opens AND gate **198** and the output of transistor **200** which is proportional to the error signal in conductor **40**, amplified by operational amplifier **16**, is supplied through resistor **304** and diode **204** to potentiometer **207** to control current regulating portion **197** which in turn controls the operation of armature firing circuit **64**.

The polarity of the input signal from operational amplifier **16** to terminal **215** being of the opposite polarity of the signal applied to terminal **213** prevents transistor **202** from conducting and, hence, no signal can emanate from AND gate **199**. Further, transistor **203** is biased on tending to divert any output from transistor **202** to conductor **227**.

When control **10** undergoes regenerative operation, the polarities of the signals from operational amplifier **16** to input terminals **213** and **215** reverse as the polarity of the error signal has reversed. This turns off transistor **200**. The reversed polarity of the input signal to terminal **215**, however, turns transistor **202** on. The polarity of the input signals to terminals **214** and **216** does not reverse instantaneously when control **10** initiates regenerative operation as it takes a finite time for the motor field **26** to reverse. During this time no signal will appear from AND gate **198** as transistor **200** is biased off and no signal will appear from AND gate **199** as transistor **203** diverts the output of transistor **202** since the polarity of the signal in conductor **69** applied to terminal **216** has not yet reversed.

When the direction of current flow through the motor field **26** does reverse, indicating the motor field is now ready for regenerative operation, the polarity of the signal in conductor **69** reverses. This turns off transistor **203** and opens AND gate **199** to provide a control signal through diode **205** to junction **206** which acts as a control signal during regenerative operation of the control.

Operation in the other direction of motor rotation is the opposite of the above described operation.

Current regulating portion **197** of current regulating and regenerative logic circuit **66** consists of a two stage amplifier with the associated input, feedback, and output circuits. The first of the amplifier consists of transistors **208** and **209** and is a differential stage. The total current through both transistors **208** and **209** is determined by the supply voltage across capacitor **221** and the value of resistor **222**. A variation in the emitter collector current of transistor **208** provides an equal but opposite variation to the emitter collector current of transistor **209** in order to maintain the total current constant. This variation is applied to the base of transistor **210** forming the second stage of the amplifier. The output of the emitter collector circuit of transistor **210** is applied to output terminal **212**.

The inputs to current regulating circuit **197** consist of the signal from the regenerative logic circuit **196** applied to potentiometer **207** and a signal proportional to armature current supplied to input terminal **211**. The magnitude of the signal applied to junction **223** from regenerative logic circuit **196** is controlled by potentiometer **207** and the magnitude of the output signals of operational amplifier **16**. This signal is then mixed with the current feedback signal at junction **223** to form an error signal which is supplied to the base of transistor **208**. As the current feedback signal is a series of current pulses, the error signal is filtered through capacitor **230** and resistor **231**.

A compensating feedback is also provided in current regulating portion **196**. This is a negative feedback from the output of transistor **210** to the input of transistor **208** and is passed through capacitor **232** and resistor **233**. This feedback alters the time response of the amplifier to prevent overshoot and to insure stable, balanced firing of armature controlled rectifier bridge **62**. The compensating feedback must be of a sufficient magnitude so that there is no overshoot under the most severe input signal conditions.

The output signal is supplied to terminal **212**. This output signal is inverted with respect to the input signal. Specifically, because of the differential configuration of transistors **208** and **209**, an increase in the signal to the base of transistor **208** increases the output of that transistor while decreasing the output of transistor **209** since the total current flow through both of them must be constant. The decrease in output of transistor **209** is amplified by transistor **210** and supplied to output terminal **212**. The reason for inverting the output signal is to simplify obtaining the negative feedback signal required for the compensating feedback. The polarity of the output from circuit **66** is arranged so that an increased error results in an increased or advanced firing angle to the controlled recifiers in bridge **62**.

The operation of the current regulating portion **197** of current regulating and regenerative circuit **66** is critical to the overall operation of control **10** as portion **197** operates the previously described inner current regulating loop of the control. This inner loop is a true regulating circuit with both reference and feedback signals and is of high gain so that only a small error signal between the reference and the feedback is sufficient to produce maximum output.

Because of the true regulating action of current regulation portion **197**, the armature current is maintained at all times proportional to the reference signal from potentiometer **207**, which is in turn proportional to the output signals of operational amplifier **16**, except when the AND gates **198** and **199** of regenerative logic circuit **196** are not open.

Current limiting action of the inner current regulating loop occurs when the input signals to operational amplifier **16** are of sufficient magnitude to cause saturation of its output. When the output of operational amplifier **16** becomes saturated, a limit is reached in the magnitude of signal that can be delivered through either AND gate **198** or **199** and potentiometer **207**. Since the signal through the potentiometer **207** is the reference to current regulating portion **197**, a limit is also placed on the amount of armature current that the inner current regulating loop will allow. This action provides the aforementioned sharp current limit. It will also be noted that the current limit action is obtained without the necessity of transiently excessive armature current to trigger the limiting means.

The compensating feedback through capacitor **232** and resistor **233** around current regulating portion **197** modifies its response to prevent overshoot of armature current under the most abrupt saturation of operational amplifier **16**.

A full appreciation of the relationship and interaction

of the detailed elements of the above described components in the structure and operation of the control may be had by referral to the foregoing Description of Operation of Static Regenerative DC Motor Control and reference is hereby made to that portion of the specification.

While the present embodiment of the invention is considered preferred, it is appreciated that numerous modifications may be made to the present invention.

I claim:

1. A controlled rectifier firing circuit (52) for operating a controlled rectifier means (44, 46 or 48, 50) responsive to an input signal to the firing circuit, said controlled rectifier means being connected between an alternating current power supply (42) and an inductive load (26) for conducting successive half cycles of the alternating current through the load to provide a unidirectional load current, said firing circuit comprising: a pulse generating means (114 or 115) coupled to the controlled rectifier means and having an operative state synchronized to the half cycles of alternating current, said pulse generating means being energizable when in the operative state for generating firing pulses to the controlled rectifier means during the half cycles of alternating current; a first energization means (124) operatively connected with said pulse generating means for energizing the latter responsive to the input signal to cause said controlled rectifier means to successively conduct at least portions of the half cycles of alternating current through the load; and an alternative energization means (125) operatively connected with said pulse generating means, said alternative energization means being coupled to the alternating current power supply and responsive to the half cycles thereof for energizing said pulse generating means to generate firing pulses near the ends of the half cycles of the alternating current to provide a conduction path in the controlled rectifier means between the load and the power supply for the inductive energy of the load.

2. The controlled rectifier firing circuit of claim 1 including a synchronizing circuit (138) connected to the alternative energization means to energize the pulse generating means for biasing said pulse generating means into the operative state during the half cycles of alternating current.

3. The controlled rectifier firing circuit of claim 2 wherein said alternative energization means is coupled to the alternating current power supply through said synchronizing circuit.

4. The controlled rectifier firing circuit of claim 3 wherein said synchronizing circuit includes a Zener diode (141) interposed between the alternating current power supply and said pulse generating means and alternative energization means for biasing said pulse generating means into the operative state during periods when the voltage magnitude of the half cycles of alternating exceeds the breakover voltage of said diode and for causing said alternative energization means to energize the pulse generating means at the end of said periods.

5. The controlled rectifier firing circuit of claim 1 wherein said first energization means comprises an amplifier (126–130) having input terminals (116 and 118) responsive to the input signal and an output terminal connected to said pulse generating means and said pulse generating means includes a uni-junction transistor (118, 119) having its input connected to said amplifier output terminal and its output coupled to said controlled rectifier means.

6. The controlled rectifier firing circuit of claim 1 for operating a controlled rectifier means (44, 46, 48 and 50) responsive to a bipolarity input signal to the firing circuit, said controlled rectifier means being connected between the alternating current power source and the inductive load for conducting successive half cycles in either direction through the load, said control rectifier firing circuit including a pair of pulse generating means coupled to the controlled rectifier means, said pulse generating means each having an operative state synchronized to the half cycles of alternating current and being energizable when in the operative state for generating firing pulses, one of said pulse generating means (114) generating firing pulses to the controlled rectifier means, when energized, for causing the controlled rectifier means to conduct at least portions of the half cycles in one direction through the load, the other of the pulse generating means (115) generating firing pulses to the controlled rectifier means, when energized, for causing the controlled rectifier means to conduct at least portions of the half cycles in the other direction through the load, said first energization means (124) being responsive to the polarity of the input signal for energizing one of said pulse generating means responsive to an input signal of one polarity, said first energization means energizing the other of said pulse generating means responsive to an input signal of the other polarity, said alternative energization means (125) energizing said pulse generating circuits to produce pulses near the ends of the half cycles of the alternating current to provide a conduction path in the controlled rectifier means between the load and the power supply to regenerate the inductive energy of the load to the power supply during a decrease in the current through the load.

7. The controlled rectifier firing circuit of claim 6 wherein said first energization means comprises a differential amplifier (126–130) having input terminals (116 and 117) responsive to the input signal and output terminals connected to said pulse generating means, said pulse generating means including uni-junction transistors (118 and 119) having their inputs connected to said amplifier output terminals and their outputs coupled to said controlled rectifier means.

8. The controlled rectifier firing circuit of claim 6 wherein said alternative energization means comprises an alternative energization circuit operatively connected with each of said pulse generating means.

9. The controlled rectifier firing circuit of claim 6 including a synchronizing circuit (138) connected to the alternating current power supply and to said pulse generating means for biasing said pulse generating means into the operative state during the half cycles of the alternating current of the supply.

10. The controlled rectifier firing circuit of claim 9 wherein said alternative energization means is coupled to said alternating current power supply through said synchronizing circuit and wherein said synchronizing circuit includes a Zener diode (141) interposed between the alternating current power supply and said pulse generating means and alternative energization means for biasing said pulse generating means into the operative state during periods when the voltage magnitude of the half cycles of alternating current exceeds the breakover voltage of said diodes and for causing said alternative energization means to energize the pulse generating means at the end of said periods.

References Cited

UNITED STATES PATENTS

3,281,645	10/1966	Spink	307—252 X
3,304,486	2/1967	Michaels	307—252 X
3,319,147	5/1967	Mapham	307—252 X
3,349,312	10/1967	Bergman	321—5
3,395,334	7/1968	Stein	323—22
3,399,337	8/1968	Stone	321—5

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