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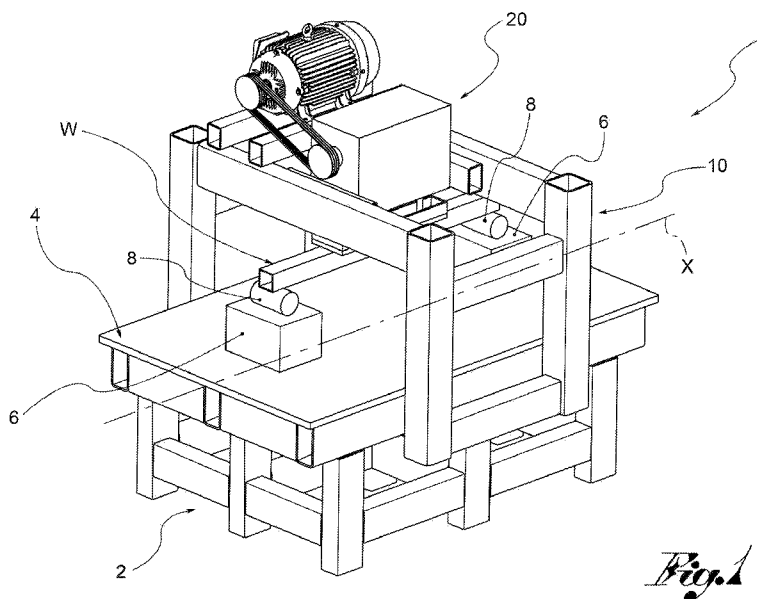
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- (54) Title: DISPLACEMENT-IMPOSED FATIGUE TEST BENCH FOR A MANUFACTURED ITEM



- (57) Abstract: Displacement-imposed fatigue test bench 1 for a manufactured item W in metallic material, comprises a base 2, means of constraint for the constraint of the manufactured item W to a table 4 according to a predefined constraint simulation and a drive group 20. Such drive group 20 comprises a characterisation device 14, moved by drive means, and a pressure element 16, moved by the characterisation device 14 to impose a deformation on the manufactured item W. In addition, the characterization device 14 comprises a shaft 26 fitted with at least one cam element 28 which operates the pressure element 16 impressing a vertical oscillation on it.



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DESCRIPTION**"DISPLACEMENT-IMPOSED FATIGUE TEST BENCH FOR A
MANUFACTURED ITEM"**Sphere of application

5 [0001] The present invention relates to a fatigue test bench for manufactured items, in particular made from metallic material and specifically from aluminium.

State of the art

10 [0002] It is known that the fatigue design of manufactured item is as important as it is difficult, on account of the fact that the fatigue breakpoint phenomenon manifests itself in actual fact depending on the material which the manufactured item is made from, on the geometry of such manufactured item, on the stress characteristics it is
15 subjected to, and on innumerable other factors.

[0003] A number of studies exist which have highlighted the characteristics of the fatigue breakpoint and proposed different design methods. However, almost all such studies take into consideration the behaviour of a
20 specific sample and then propose a design method based on the assumption of extending the observed behaviour to a real manufactured item.

[0004] Such situation leads to a situation of uncertainty of the fatigue design which translates into the need to
25 use elevated safety factors, which translates into a

waste of material and non-optimal geometries of the manufactured item.

Purpose of the invention

[0005] The purpose of the present invention is to make a
5 fatigue test bench suitable for conducting experimental tests on manufactured items, in particular made from metallic material and specifically from aluminium.

[0006] Such purpose is achieved by a fatigue test bench made according to claim 1.

10 Brief description of the drawings

[0007] Figure 1 shows a fatigue test bench according to the present invention, according to one embodiment.

[0008] Figure 2 shows a drive group of the bench in figure 1.

15 [0009] Figure 3 shows a characterisation device of the drive group in figure 2.

[0010] Figures 4 and 5 show an example of application of strain gauges.

[0011] Figure 6 shows a fatigue test bench according to the
20 present invention, according to a further embodiment.

[0012] Figure 7 shows a detail of the bench in figure 6.

Description of an embodiment

[0013] With reference to the appended drawings, reference numeral 1 globally denotes a fatigue test bench for
25 manufactured items, in particular for manufactured items

made from metallic material, specifically from aluminium and the alloys thereof.

[0014] The bench 1 comprises a base 2 preferably made from a frame composed of girders, preferably welded to each other, to assure a high degree of rigidity.

[0015] The bench 1 further comprises a table 4 for the support of the manufactured item to be tested, preferably having its main extension along a table axis X.

[0016] The bench 1 is further provided with means of constraint for the constraint and attachment if necessary of the manufactured item to the table. For example, the means of constraint comprise a pair of blocks 6, for example distanced along the table axis 4, and respective cylinders 8, supported by the blocks 6, which the manufactured item W may be rested on.

[0017] The configuration and the structure of the means of constraint varies according to the type of stress which the manufactured item is to be subjected to. For example, the means of constraint formed by the two blocks 6 and the two cylinders 8 simulate a "joint" type constraint for the manufactured item.

[0018] The bench 1 comprises in addition a frame 10 which surmounts the table 4 and is supported at the two sides of the table by the base 2.

[0019] Preferably, the frame 10 is also composed of a

structure formed of girders, for example welded to each other.

[0020] In addition, the bench 1 comprises a drive group 20, at least partially supported by the frame 10, suitable
5 for impressing upon the manufactured item W a variable stress over time by means of an imposed displacement.

[0021] The drive group 20 comprises drive means, for example comprising an electric motor 22, for example supported by the frame 10.

10 [0022] The group 20 further comprises a characterisation device 14, connected to the drive means, for example by means of a belt connection 24, and a pressure element 16, connected to the characterisation device, suitable for coming into contact with the manufactured item W to
15 impose a deformation on it.

[0023] Preferably, the pressure element 16 is a plate, preferably reinforced and stiffened by ribs 16a, having a main extension along the table axis X, that is in the direction of extension of the manufactured item.

20 [0024] Advantageously, such pressure element permits a distribution of the action on the manufactured item, so as to prevent concentrated actions which could lead to scoring of the manufactured item.

[0025] The characterisation device 14 comprises a shaft 26
25 rotating by virtue of its connection to the drive means

around a rotation axis Z fitted with at least one cam element 28, provided with an outer eccentric surface 28a, which operates the pressure element 16 impressing a vertical oscillation on it.

5 [0026] According to a preferred embodiment, at least two cam elements 28 are provided, distanced along the rotation axis Z of the shaft.

[0027] Preferably, the cam element 28 is made in one piece with the remaining part of the shaft 26.

10 [0028] The shaft 26 also has support surfaces 30 and the device 14 comprises at least one bearing 32 for the support in rotation of the shaft, positioned at the support surfaces 30.

[0029] Preferably, the outer surfaces 28a of said cam
15 elements 28 are lowered in relation to the support surfaces 30 of the bearings.

[0030] This makes it possible, in a preferred embodiment, to position a bearing 32 in an intermediate position between two cam elements 28, increasing the rigidity of
20 the support of the shaft.

[0031] The characterization device 14 further comprises transmission elements 40, firmly connected to the pressure element 16, each engaged and moved in oscillation by the relative cam element 28.

25 [0032] Preferably, said transmission elements 40 comprise

rollers in contact with the respective cam elements, to improve the contact conditions with said cam elements.

[0033] According to a preferred embodiment, the characterisation device 14 is modifiable or replaceable
5 to vary the characteristics of the deformation imposed on the manufactured item.

[0034] For example, a first shaft 26 is replaceable with a different shaft having differently shaped cam elements, so as to vary the characteristics of the displacement
10 imposed on the pressure element and thus the characteristics of the deformation imposed on the manufactured item.

[0035] According to a further example, the cam elements are replaceable.

15 [0036] According to yet a further variant, the transmission elements present cam-shaped contact surfaces with the shaft and are replaceable.

[0037] Moreover, the drive group 20 comprises return means, such as spiral springs 50 suitable for permanently
20 pressing the pressure plate to ensure contact with the shaft 26.

[0038] The drive group 20 further comprises a box 60, inside which the characterisation device 14 is housed, made so as to be oil or liquid proof.

25 [0039] Preferably, in fact, the characterisation device is

in a bath of oil or of a coolant liquid, for adequate heat dissipation.

[0040] Preferably, moreover, the bench 1 comprises recirculation means operatively connected to the box 60
5 for the recirculation and the conditioning of the oil or of the coolant liquid.

[0041] According to a preferred embodiment, the bench 1 further comprises a derivation accessory, connectable to the pressure element, for the transformation of the
10 vertical oscillatory movement of the same into a different desired movement (such as a horizontal oscillatory movement or circular oscillatory movement) or to apply the action to the manufactured item in a particular point in space, for example to adapt to the
15 geometry of the manufactured item

[0042] According to a further embodiment, the bench 1 comprises a plurality of strain gauges, connectable to the manufactured product to detect the real deformation and stress, and a data management device, connected to
20 said strain gauges, for the visualisation and management of the experimental data acquired.

[0043] In particular, the purpose of the strain gauges is to verify the real stress to which the manufactured item is subjected during the fatigue test. Moreover, the use
25 of strain gauges, located in the areas subject to scoring

or changes in cross-section, makes it possible to detect the real coefficient of overstress induced by the geometrical discontinuity.

[0044] In one variant, the strain gauges are connected to the structure of the fatigue test bench 1, for example positioned on the columns of the frame 10 or base 2.

[0045] In a further variant, accelerometers are provided to measure the vibrations acting on the manufactured item W or on the fatigue test bench 1.

10 Examples of experimental tests

[0046] A) In a first experimental test, the manufactured item consisted of a tubular extrudate in aluminium alloy of square cross-section having a side = 150 mm, thickness = 5 mm, length between the supports = 2000 mm, loaded at the centreline with load surface = 500 mm, supported at the two ends with joints and resulting load = 30000 N.

[0047] The manufactured item was tested with 12 Hz frequency up to $5 \cdot 10^6$ cycles Operating without stop times, the test lasts about 5 days.

[0048] B) In a further experimental test, the manufactured item is composed of a riveted joint between two sheets in aluminium alloy with thickness = 3 mm, blind rivets having a diameter of = 4.8 mm. One of the two ends of the joint is held in a vice and blocked to the bench, the

other is subjected to pulling at the free end equal to the load needed to cause a displacement in said point of application of the action (arrow) equal to =1 mm. The displacement is imposed by a derivation accessory
5 connected to the pressure plate for the simulation of the desired displacement.

[0049] At an imposed frequency of 15 Hz, the test continues until failure of one of the connection elements (rivet or flap of sheet), reaching a duration limited to several
10 days.

Example of application of strain gauges

[0050] One example of application of strain gauges is shown in Figures 4 and 5.

[0051] In the case shown, the manufactured item is a
15 prismatic extrudate, resting on two jointed supports, loaded on the centreline with an extensive load surface.

[0052] The strain gauges 1 and 4, permit the detection of the maximum value of flexural stress (both of compression and of traction) and any asymmetries in the
20 distribution of the stresses.

[0053] The strain gauges 2 and 6, placed on the neutral axis of the cross-section, permit assessment of any axial loads due to load or constraint imprecision (and permit, together with the values supplied by the strain gauges 1
25 and 4, an assessment of any stress asymmetries).

[0054] The strain gauges 3 and 5 permit assessment of any "corner stress" and the calculation of the consequent overstress coefficient, for example to determine the best connection radius between the edges as regards fatigue.

5 [0055] According to an embodiment variant, shown in figures 6 and 7, the characterisation device 14 comprises a shaft 26 rotating around the rotation axis Z, fitted with at least one cam element 28 of a truncated cone shape, even with non-circular bases.

10 [0056] The cam element 28 is provided with a smaller base b_m and a larger base B_M which respectively represent the minimum and maximum cam lift profile able to ensure contact with the transmission elements 40. In one embodiment, the minimum cam lift profile is equal to 1 mm
15 and the maximum cam lift profile is equal to 10 mm.

[0057] As shown in figure 6, each cam element 28 has a truncated cone shape defined, along the rotation axis Z, by:

[0058] - a first truncated-cone cross-section 281, defined
20 between the first minimum lift profile and the first maximum lift profile;

[0059] - a possible cylindrical intermediate cross-section 282, defined between the first maximum lift profile and the second maximum lift profile;

25 [0060] - a second truncated-cone cross-section 283, defined

between the second maximum lift profile and the second minimum lift profile.

[0061] According to a preferred embodiment, at least two cam elements 28 of a truncated-cone shape are provided, 5 distanced along the rotation axis Z of the shaft.

[0062] As shown in figure 6, the characterisation device 14 comprises, for each cam element 28, a pair of transmission elements 40, firmly connected to the pressure element 16.

10 [0063] Each transmission element 40 is translatable in the direction of the rotation axis Z, along the truncated cone profile of the cam element 28. In particular, a first transmission element 40 translatable along the profile of the first truncated cone cross-section 281, 15 and a second transmission element 40 translatable along the profile of the second truncated cone cross-section 283 are provided. Preferably, the first and the second transmission elements translate in opposite directions.

[0064] Each transmission element 40 is therefore 20 translatable between the first minimum lift profile and the maximum lift profile of each truncated cone cross-section. Such translation permits a precise adjustment of the displacement assigned to the pressure element 16 by acting on the position of the transmission elements 40.

25 [0065] The characterisation device 14 is thus adjustable to

vary the characteristics of the deformation imposed on the manufactured item W by means of the translation of the transmission element 40 along the truncated cone profile of the cam element 28'. This way, it is possible
5 to vary the characteristics of the displacement imposed on the pressure element 16 without having to replace the shaft 26 with a different shaft having differently shaped cam elements.

[0066] The transmission elements 40 comprise rollers 401 in
10 contact with the respective cam elements 28. To improve the contact conditions between the transmission element 40, and in particular the roller 401, and the truncated cone profile of the cam element 28, the rotation axis Z' of the rollers 401 is inclined in relation to the
15 rotation axis Z of the shaft 26.

[0067] In the embodiment shown in figure 6, the characterisation device 14 comprises for each truncated cone cam element 28, a pair of transmission elements 40 in the form of rollers 401 with rotation axes Z' inclined
20 in relation to the rotation axis Z, according to the inclination of the respective truncated cone cross-section 281, 283. The presence of rollers 401 with inclined rotation axis Z' ensures contact between the cam element 28 and the transmission element 40, gradually as
25 the latter is moved by translation in the direction of

the rotation axis Z of the shaft 26 to perform an adjustment of the characterisation device 14.

[0068] The translation of the transmission elements 40 during the adjustment of the displacement imposed on the manufactured item W for the relative test, takes place thanks to the mounting of said transmission elements 40 on special supports 402 connected to guides 403 positioned in the direction Z. In particular, each support 402 slides along two linear, substantially parallel guides 403.

[0069] The translation of the transmission elements 40 along the guides 403 is performed by means of a control system comprising:

[0070] - a control shaft 404; the rotation of which determines a displacement of the supports 402 along the guides 403;

[0071] - a vertical shaft 407, fitted with a control handwheel 408;

[0072] - a transmission mechanism 406, comprising toothed wheels for the transmission of movement between the vertical shaft 407 and the control shaft 404.

[0073] In particular, the control shaft 404 is provided with a mated threading (right hand and left-hand) for each pair of transmission elements 40. Each support 402 is coupled to the control shaft 403 by means of a

threaded hole (lead screw) according to criteria typical of control screws. The rotation of the control shaft 404 permits each pair of supports 402 to reduce or increase the distance D between the transmission elements 40 so as to ensure the contact of the rollers 401 with the cam element 28 (and in particular with the respective truncated cone cross-section 281, 283) for each value chosen in the range comprised between the minimal lift profile and the maximum lift profile.

10 [0074] The control shaft 404 is supported at the ends and in the centreline by supports 405 and is blocked in position by attachment elements, such as for example blocking rings , connected to said supports 405.

[0075] The rotation of the control shaft 404 is controlled from outside the box using the handwheel 408, engaged on the vertical shaft 407 integral with the transmission mechanism 406. Such transmission mechanism 406, attached (for example by screws or welded,) to the upper plate 161 of the pressure element 16, comprises conical toothed wheels for the transmission of the movement between axes orthogonal to each other. The connection between these two shafts is made for example by means of a spanner screw type connection with recessed head upstream of the first support 405 at the end of the control shaft.

25 [0076] The drive group 20 comprises return means, such as

spiral springs 50 mounted for example along the columns 162 of the pressure element 16, suitable for permanently pressing the pressure plate to ensure contact with the shaft 26.

5 [0077] The pressure element 16 can thus translate vertically between the first minimum lift profile and the maximum lift profile of the truncated cone cam element 28, thus permitting the adjustment of the displacement imposed on the manufactured item W depending on the test
10 in question. The possible vertical displacement of the pressure element 16 makes it necessary to correctly equilibrate the sum of the forces, (in particular the elastic reaction provided by the sample W subject to the imposed displacement, the forces of inertia of the
15 oscillating masses, the elastic reaction provided by the spiral spring 50 at any moment of functioning, to ensure continuity of contact between the cam elements 28 and the respective rollers 401.

[0078] To ensure such continuity of contact, the preloading
20 of the spiral springs 50 is acted on. The pressure element 16 is then fitted with internally threaded sleeves 501, fitted along the columns 162, also threaded, of the pressure element 16. Each sleeve 501 can translate vertically along the columns 162 by screwing, by means of
25 a connection typical of a ring nut. The sleeve 501 is then

fixed in the desired position by means of an attachment counter-nut 502. The variation of the preloading of the spiral spring 50 is then obtained by the vertical shifting of the sleeves 501, on the upper rim of which a lower end of said spring rests.

[0079] Graduated indexes are provided so as to facilitate the measurement of the imposed displacement on the sample W tested and the preloading assigned to the spiral spring 50, preferably combined with cursors, positioned on the box 60.

[0080] To improve the adjustment of the characterisation device 14, the following are also provided:

[0081] - position sensors, to measure the location of the supports 402 in relation to the cam elements 28, or the effective preloading of each of the spiral springs 50;

[0082] - force sensors, for the compensation by means of the automatic control unit or manually, of any errors or discrepancies compared to the ideal situation.

[0083] Innovatively, the fatigue test bench according to the present invention, makes it possible to perform experimental fatigue tests on real manufactured items, in a reasonable time and simulating real load conditions.

[0084] In particular, advantageously, the test bench makes it possible to modify the characteristics of the imposed displacement on the manufactured item according to the

test to be performed or, for example, to simulate the real working conditions of the manufactured item.

[0085] According to a further advantageous aspect, the test bench permits a considerable reduction of test times, even for tests performed for very high numbers of cycles, to the order of millions of cycles.

[0086] According to a further advantageous aspect, the characterization device is adjustable to vary the characteristics of the deformation by means of the translation of the transmission element along the truncated cone profile of the cam element.

[0087] According to a further advantageous aspect, the characterisation device is adjustable without the need to replace the shaft.

[0088] According to a further advantageous aspect, the fatigue test bench proves more versatile and free of the need to build new shafts fitted with cam elements the profiles of which reproduce the different displacement, speed and acceleration values to impose at the physical point of the sample W tested each time

[0089] According to a further advantageous aspect, the fatigue test bench permits a reduction of the costs and times for making new parts.

[0090] It is clear that a person skilled in the art may make modifications to the bench described above so as to

satisfy contingent requirements, while remaining within the scope of protection as defined by the following claims.

Claims

1. Displacement-imposed fatigue test bench (1) for a manufactured item (W), in metallic material, comprising:
- a base (2);
 - 5 - a table (4) supported by the base (2), for the support of the manufactured item (W);
 - means of constraint for the constraint of the manufactured item (W) to the table (4) according to a predefined constraint simulation;
 - 10 - a drive group (20) comprising:
 - a) drive means;
 - b) a characterisation device (14), moved by the drive means;
 - c) a pressure element (16), moved by the characterization
 - 15 device (14) and suitable for coming into contact with the manufactured item (W) to impose a deformation on it;
- characterised in that the characterization device (14) comprises a shaft (26) fitted with at least one cam element (28), which operates the pressure element (16)
- 20 impressing a vertical oscillation on it.
2. Bench according to claim 1, wherein the cam element (28) is provided with an outer eccentric surface (28a).
3. Bench according to claim 1 or 2, wherein the cam element (28) is made in one piece with the remaining part
- 25 of the shaft (26).

4. Bench according to any of the previous claims, wherein at least two cam elements (28) are provided, distanced along the rotation axis (Z) of the shaft (26).

5. Bench according to any of the previous claims, comprising transmission elements (40), firmly connected to the pressure element (16) each engaged and moved in oscillation by the relative cam element (28).

6. Bench according to claim 5, wherein said transmission elements (40) comprise rollers in contact with the respective cam elements (28).

7. Bench according to claim 5, wherein the transmission elements (40) present cam-shaped contact surfaces with the shaft (26) and are replaceable.

8. Bench according to any of the previous claims, wherein the shaft (26) has support surfaces (30) for bearings (32) and the outer surfaces (28a) of said cam elements (28) are lowered in relation to the support surfaces (30) of the bearings (32).

9. Bench according to claim 8, wherein a bearing (32) is positioned in an intermediate position between two cam elements (28).

10. Bench according to any of the previous claims, wherein the cam elements (28) are replaceable.

11. Bench according to any of the claims from 1 to 7, wherein the cam element (28) is a truncated cone shape,

even with non-circular bases.

12. Bench according to claim 11 when dependent on claim 5, wherein each transmission element (40) is translatable in the direction of the rotation axis (Z), along the truncated cone profile of the cam element (28).

13. Bench according to claim 11 or 12, wherein the truncated cone shape is defined, along the rotation axis (Z) of the shaft (26), by:

- a first truncated-cone cross-section (281), defined between the first minimum lift profile and a first maximum lift profile;

- a second truncated-cone cross-section (283), defined between a second maximum lift profile and a second minimum lift profile.

14. Bench according to claim 13, comprising a first transmission element (40) translatable along the profile of the first truncated cone cross-section (281), and a second transmission element (40) translatable along the profile of the second truncated cone cross-section (283).

15. Bench according to any of the claims from 12 to 14, wherein each transmission element (40) is a roller (401) having a rotation axis (Z') inclined in relation to the rotation axis (Z) of the shaft (26).

16. Bench according to any of the claims from 12 to 15, wherein each transmission element (40) is mounted on a

support (402) connected to guides (403) positioned in the direction of the axis (Z).

17. Bench according to claim 16, wherein the translation of the transmission elements (40) is performed by means
5 of a control system comprising.

- a control shaft (404), the rotation of which determines a displacement of the supports (402) along the guides (403);

- a vertical shaft (407), fitted with a control handwheel
10 (408);

- a transmission mechanism (406), comprising toothed wheels for the transmission of movement between the vertical shaft (407) and the control shaft (404).

18. Bench according to any of the claims from 11 to 17,
15 wherein the drive group (20) comprises preloaded spiral springs (50) joined to the pressure element (16) to ensure contact between the transmission elements (40) and the respective cam element (28).

19. Bench according to any of the claims from 11 to 18,
20 comprising graduated indexes fitted with a cursor to measure the entity of the displacement imposed on the sample tested (W), and/or position sensors to measure the location of the transmission elements (40) in relation to the cam element (28), and /or force sensors.

25 20. Bench according to any of the claims from 1 to 10,

wherein the characterisation device (14) is replaceable to vary the characteristics of the deformation imposed on the manufactured item (W).

21. Bench according to any of the claims from 12 to 19,
5 wherein the characterisation device (14) is adjustable to vary the characteristics of the deformation imposed on the manufactured item (W) by means of the translation of the transmission element (40) along the truncated cone profile of the cam element (28').

10 22. Bench according to any of the previous claims, wherein the pressure element (16) is a plate.

23. Bench according to any of the previous claims, comprising a box (60), inside which the characterization device (14) is housed, made so as to be oil or liquid
15 proof, said characterization device being in a bath of oil or of a coolant liquid.

24. Bench according to claim 23, comprising recirculation means operatively connected to the box (60) for the recirculation and the conditioning of the oil or of the
20 coolant liquid.

25. Bench according to any of the previous claims, comprising a derivation accessory, connectable to the pressure element (16), for the transformation of the vertical oscillatory movement thereof into a different
25 movement or to apply the action to the manufactured item

(W) in a particular point in space.

26. Bench according to any of the previous claims, comprising a plurality of strain gauges, connectable to the manufactured product (W) and/or to the frame of said
5 bench (1), to detect the real deformation and stress, and a data management device, connected to said strain gauges, for the visualisation and management of the experimental data acquired.

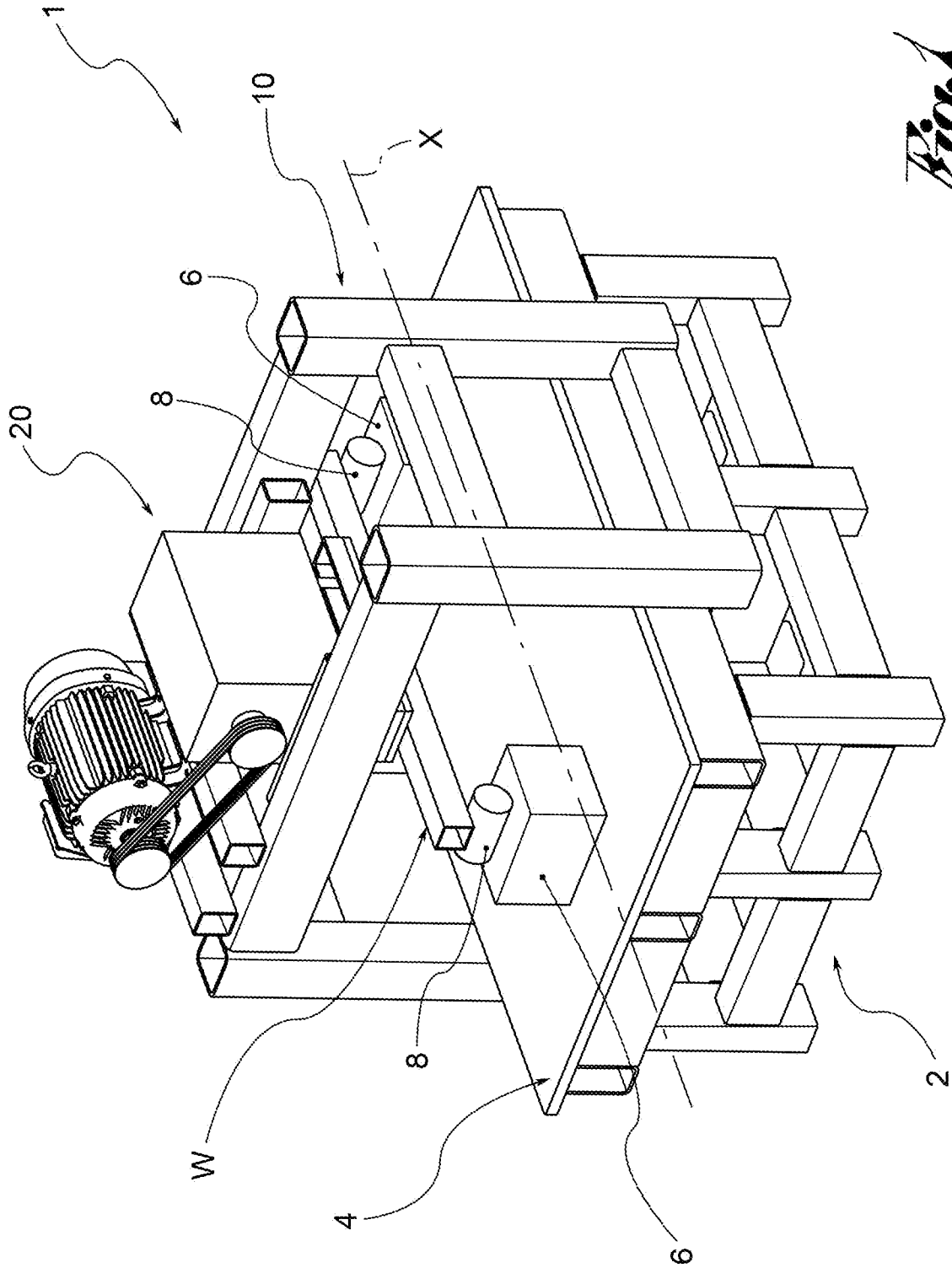


Fig. 1

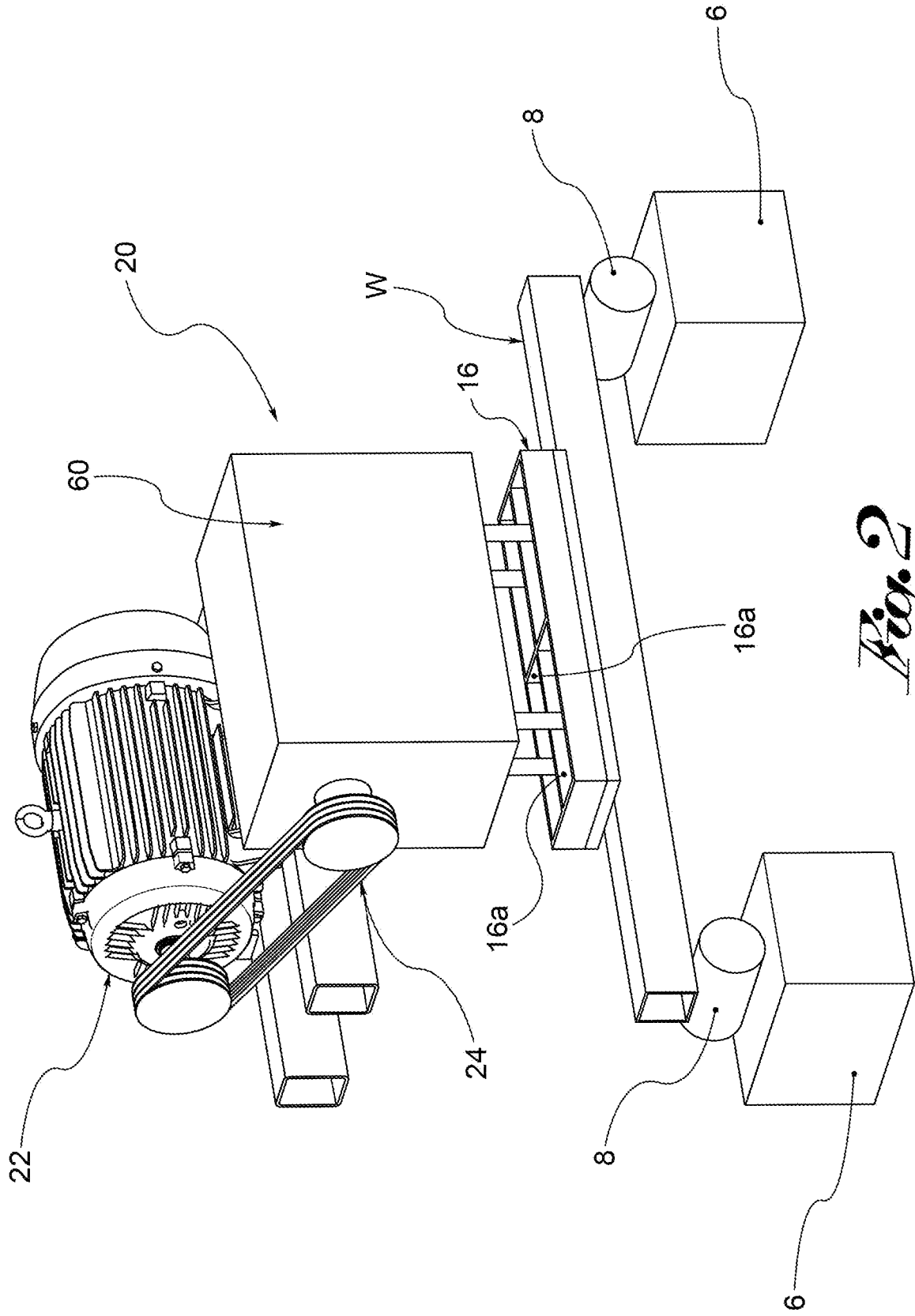


Fig. 2

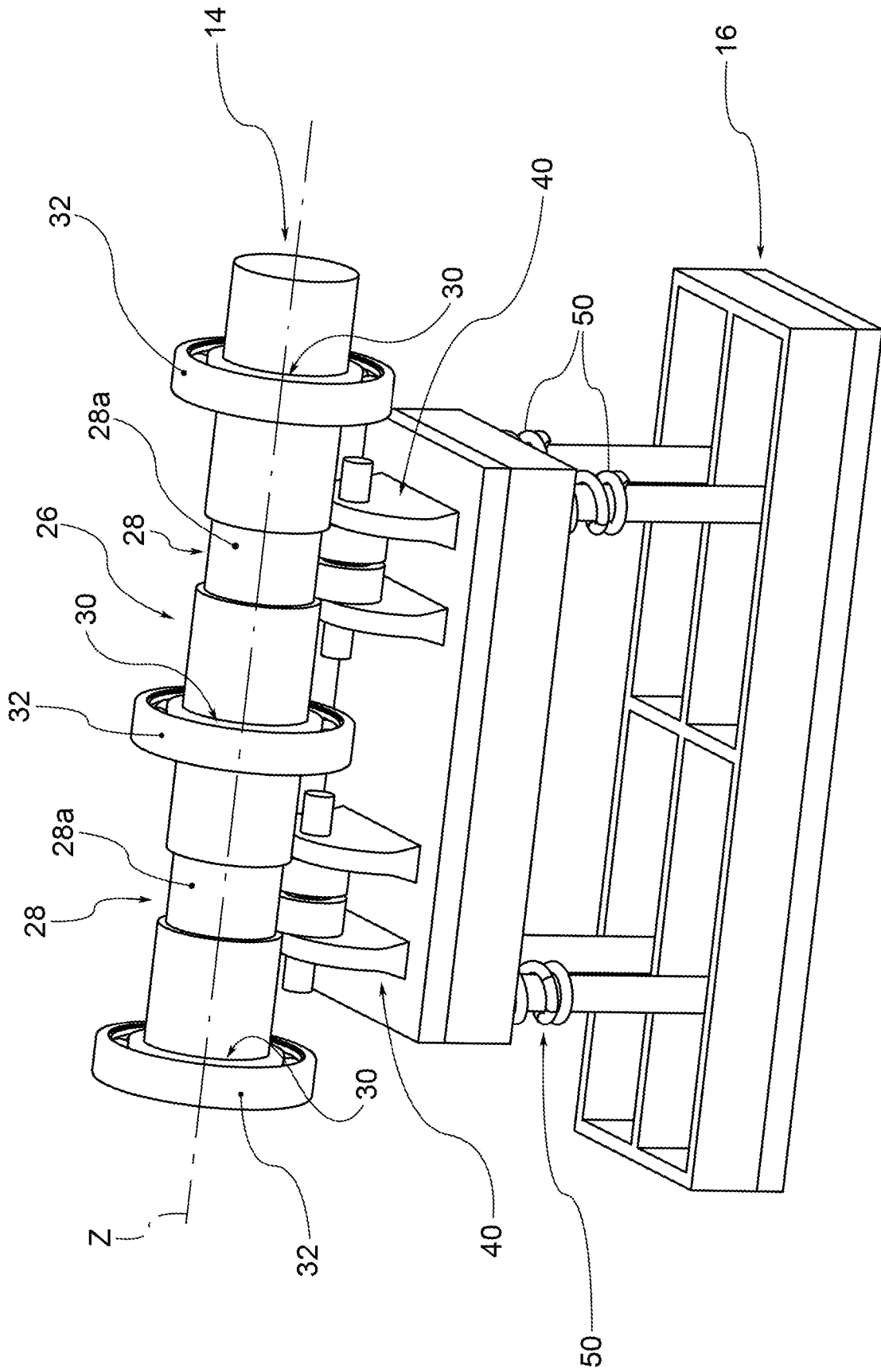
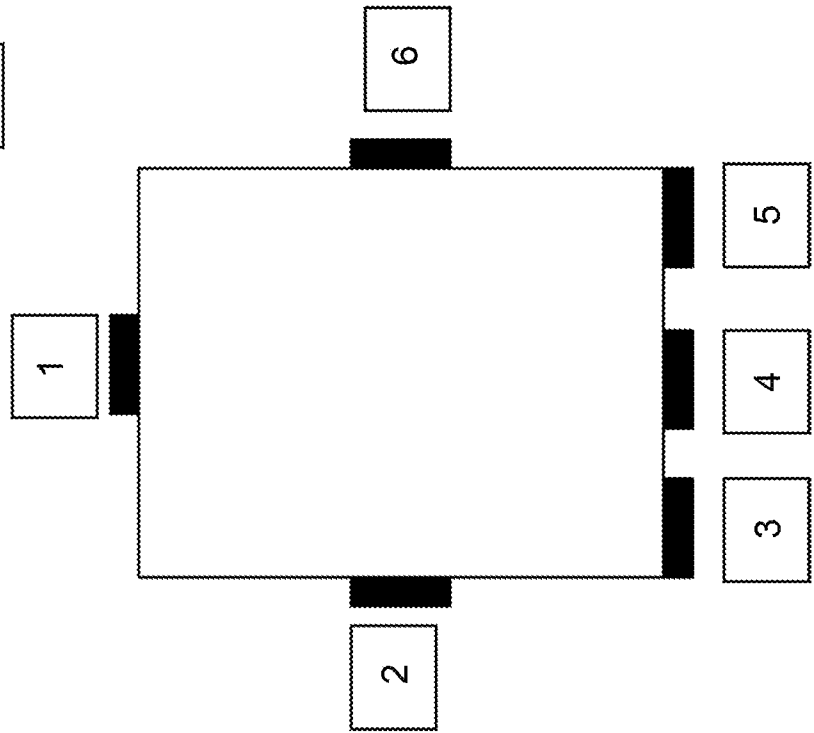
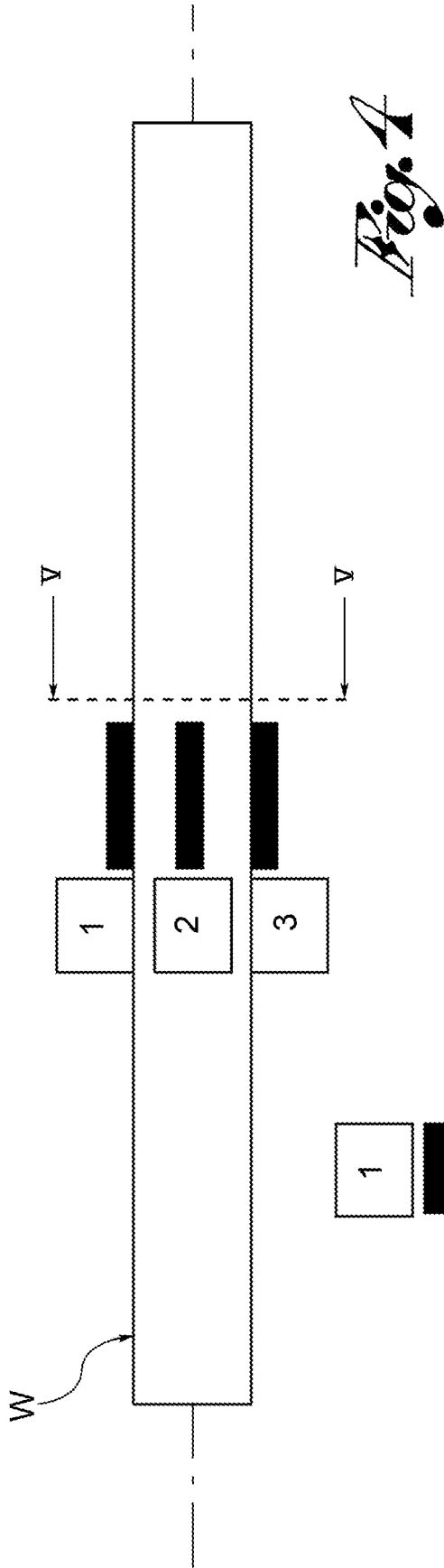


Fig. 3



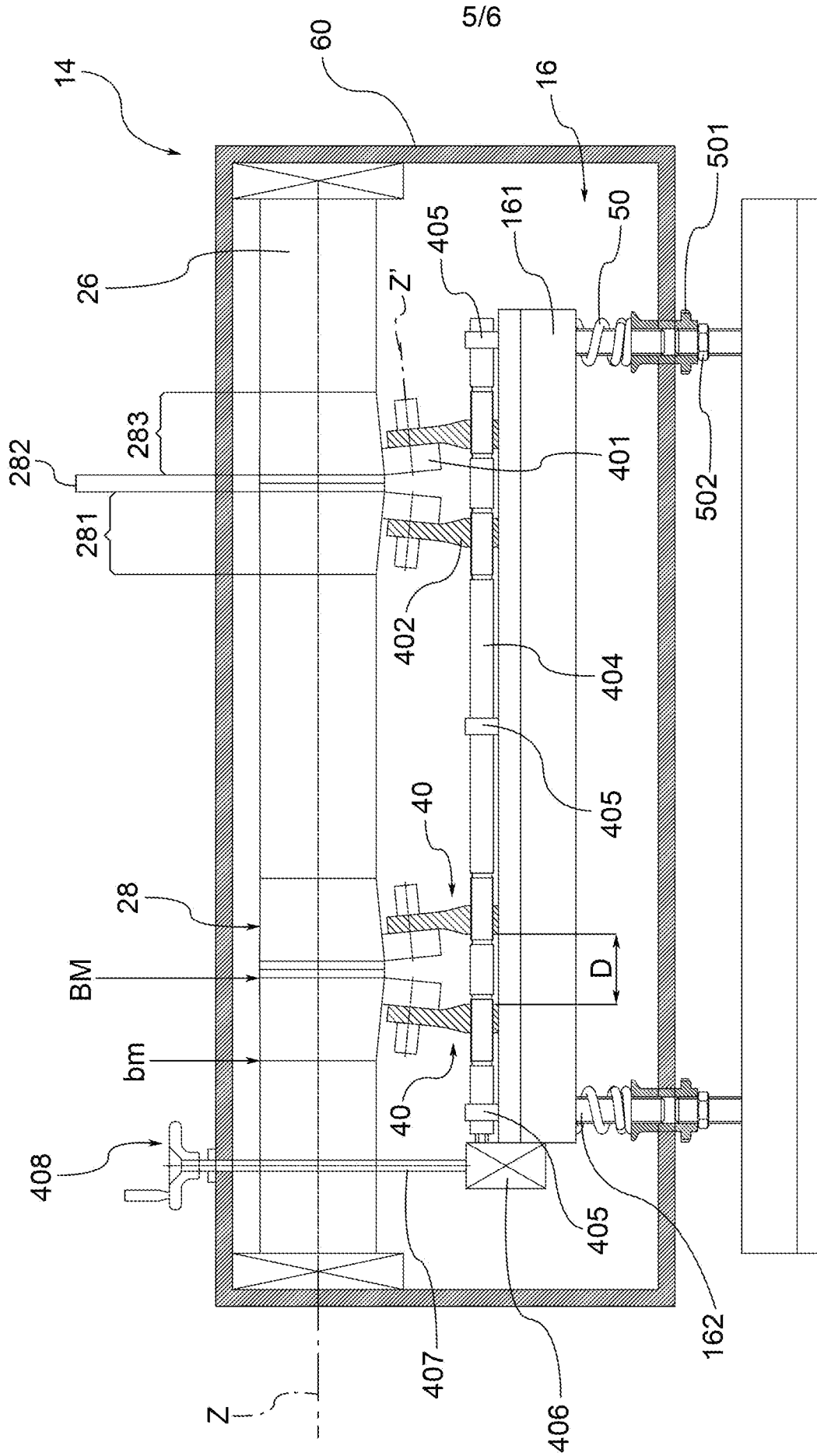


Fig. 6

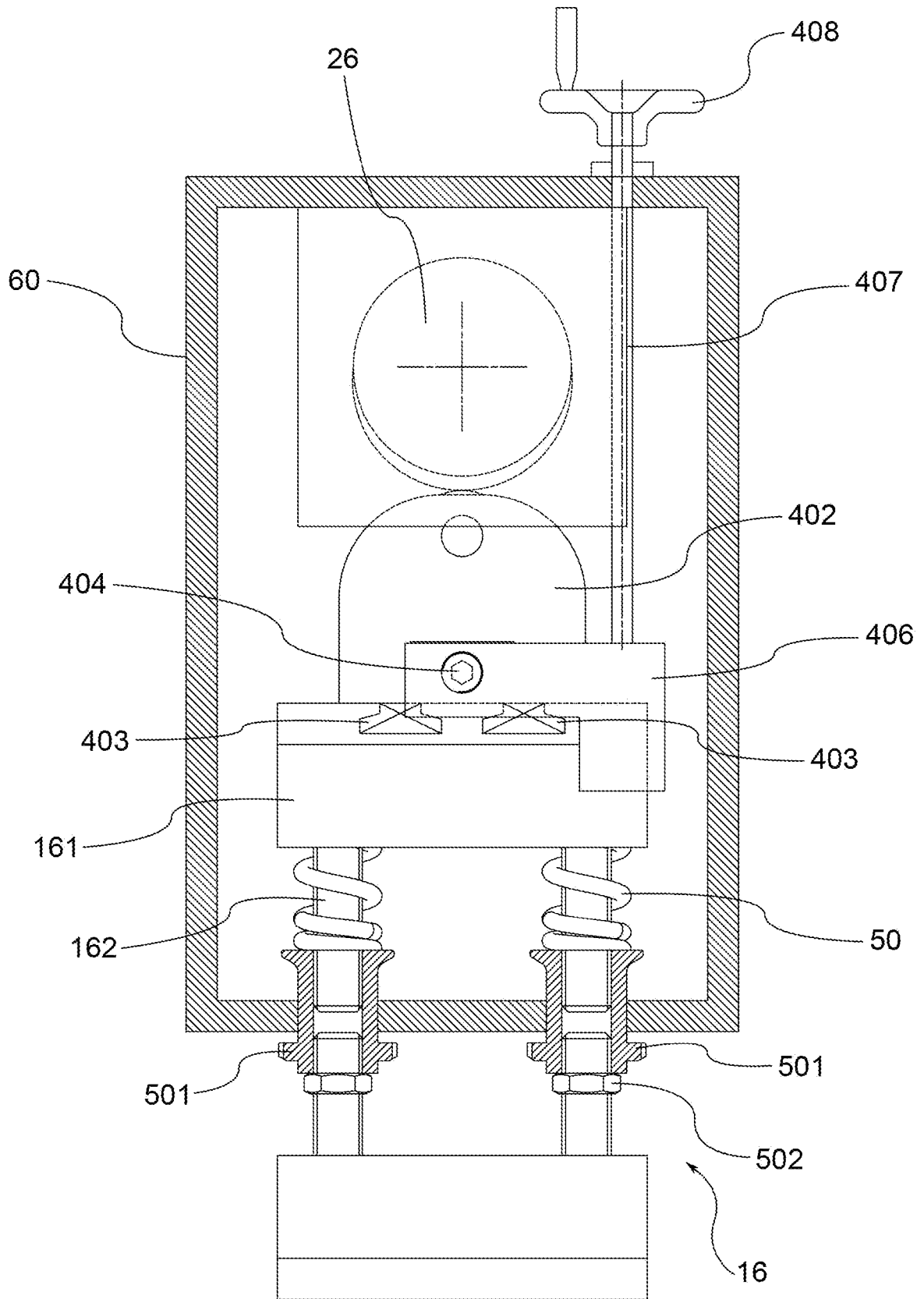


Fig. 7

INTERNATIONAL SEARCH REPORT

International application No
PCT/IB2013/051067

A. CLASSIFICATION OF SUBJECT MATTER
INV. G01N3/34
ADD.
According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED
Minimum documentation searched (classification system followed by classification symbols)
G01N

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)
EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	JP 2006 258454 A (TORAY INDUSTRIES) 28 September 2006 (2006-09-28) paragraph [0006] paragraph [0010] paragraph [0013] paragraph [0014] paragraph [0023] paragraph [0022] paragraph [0026] figures 3-6	1-26
A	EP 0 603 029 A1 (COLAS SA [FR]) 22 June 1994 (1994-06-22) column 6, lines 8-17 figure 1	1-26
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Further documents are listed in the continuation of Box C.

See patent family annex.

* Special categories of cited documents :

- "A" document defining the general state of the art which is not considered to be of particular relevance
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Date of the actual completion of the international search 11 June 2013	Date of mailing of the international search report 18/06/2013
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INTERNATIONAL SEARCH REPORT

International application No
PCT/IB2013/051067

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
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Information on patent family members

International application No

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