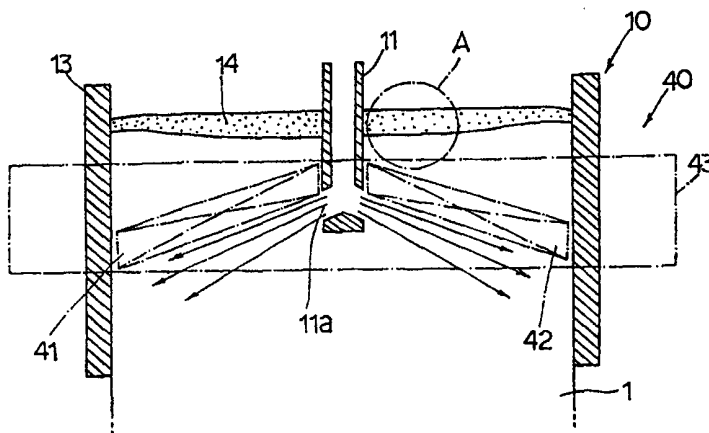




INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification ⁷ : B22D 11/10	A1	(11) International Publication Number: WO 00/07754 (43) International Publication Date: 17 February 2000 (17.02.00)
(21) International Application Number: PCT/KR99/00413 (22) International Filing Date: 30 July 1999 (30.07.99) (30) Priority Data: 1998/31788 4 August 1998 (04.08.98) KR (71) Applicants (for all designated States except US): POHANG IRON & STEEL CO., LTD. [KR/KR]; 1, Koedong-dong, Nam-ku, Pohang-si, Kyungsangbook-do 790-300 (KR). RESEARCH INSTITUTE OF INDUSTRIAL SCIENCE & TECHNOLOGY [KR/KR]; San 32, Hyoja-dong, Nam-ku, Pohang-si, Kyungsangbook-do 790-330 (KR). (72) Inventors; and (75) Inventors/Applicants (for US only): CHO, Myung, Jong [KR/KR]; Research Institute of Industrial Science & Technology, San 32, Hyoja-dong, Nam-ku, Pohang-si, Kyungsangbook-do 790-330 (KR). KIM, Sang, Joon [KR/KR]; Research Institute of Industrial Science & Technology, San 32, Hyoja-dong, Nam-ku, Pohang-si, Kyungsangbook-do 790-330 (KR). KIM, Jong, Keun [KR/KR]; Research Institute of Industrial Science & Technology, San 32, Hyoja-dong, Nam-ku, Pohang-si, Kyungsangbook-do 790-330 (KR). KIM, In, Cheol [KR/KR]; Research Institute of Industrial Science &		Technology, San 32, Hyoja-dong, Nam-ku, Pohang-si, Kyungsangbook-do 790-330 (KR). (74) Agent: CHUN, Choon, Hang; Woonam Building, 9th floor, 824-22, Yeoksam-dong, Kangnam-ku, Seoul 135-080 (KR). (81) Designated States: AU, BR, CA, CN, IN, JP, US, European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE). Published <i>With international search report.</i> <i>Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i>

(54) Title: CONTINUOUS CASTING METHOD, AND DEVICE THEREFOR



(57) Abstract

A continuous casting method, and a device for use in the casting method, are disclosed. The flow state of the discharged molten metal is properly controlled, and thus, the amounts of residual non-metallic inclusions and gas bubbles within the molten metal are decreased, so that continuously cast slabs of a good quality can be produced. The continuous casting device includes a mould (10) with a submerged nozzle (11) installed therein, the submerged nozzle having a pair of discharge holes (11a) directed toward narrow faces of the mould (10). Further, an electromagnetic brake ruler (40) is included for establishing a magnetic field within the mould (10). The electromagnetic brake ruler (40) includes a base frame (43) surrounding the mould (10), and iron cores projecting from near the wide faces of the mould, while the iron cores are wound with induction coils. It further includes a pair of electromagnetic transferring parts (41 and 42) connected to the iron cores, and disposed immediately above the discharge holes of the submerged nozzle toward narrow faces of the mould and in parallel with a discharge direction of the molten metal. With the magnetic field applied within the mould (10), the separation capability for the non-metallic inclusions and gas bubbles is increased so as to greatly reduce the internal defects of the cast products.

FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AL	Albania	ES	Spain	LS	Lesotho	SI	Slovenia
AM	Armenia	FI	Finland	LT	Lithuania	SK	Slovakia
AT	Austria	FR	France	LU	Luxembourg	SN	Senegal
AU	Australia	GA	Gabon	LV	Latvia	SZ	Swaziland
AZ	Azerbaijan	GB	United Kingdom	MC	Monaco	TD	Chad
BA	Bosnia and Herzegovina	GE	Georgia	MD	Republic of Moldova	TG	Togo
BB	Barbados	GH	Ghana	MG	Madagascar	TJ	Tajikistan
BE	Belgium	GN	Guinea	MK	The former Yugoslav Republic of Macedonia	TM	Turkmenistan
BF	Burkina Faso	GR	Greece			TR	Turkey
BG	Bulgaria	HU	Hungary	ML	Mali	TT	Trinidad and Tobago
BJ	Benin	IE	Ireland	MN	Mongolia	UA	Ukraine
BR	Brazil	IL	Israel	MR	Mauritania	UG	Uganda
BY	Belarus	IS	Iceland	MW	Malawi	US	United States of America
CA	Canada	IT	Italy	MX	Mexico	UZ	Uzbekistan
CF	Central African Republic	JP	Japan	NE	Niger	VN	Viet Nam
CG	Congo	KE	Kenya	NL	Netherlands	YU	Yugoslavia
CH	Switzerland	KG	Kyrgyzstan	NO	Norway	ZW	Zimbabwe
CI	Côte d'Ivoire	KP	Democratic People's Republic of Korea	NZ	New Zealand		
CM	Cameroon		Republic of Korea	PL	Poland		
CN	China	KR	Republic of Korea	PT	Portugal		
CU	Cuba	KZ	Kazakhstan	RO	Romania		
CZ	Czech Republic	LC	Saint Lucia	RU	Russian Federation		
DE	Germany	LI	Liechtenstein	SD	Sudan		
DK	Denmark	LK	Sri Lanka	SE	Sweden		
EE	Estonia	LR	Liberia	SG	Singapore		

CONTINUOUS CASTING METHOD, AND DEVICE THEREFOR

FIELD OF THE INVENTION

The present invention relates to a continuous casting
5 method, and a device for use in the casting method. More
specifically, the present invention relates to a
continuous casting method, and a device for use in the
casting method, in which the flow state of the discharged
molten metal is properly controlled, and thus, the
10 amounts of residual non-metallic inclusions and gas
bubbles within the molten metal are decreased, so that
continuously cast slabs of a good quality can be produced.

BACKGROUND OF THE INVENTION

15 The molten metal continuous casting method has been
adopted over the whole world since 1960s. This method has
various advantages compared with the general ingot making
method, and therefore, occupies a considerable part of
the manufactured steel.

20 The quality of a continuously cast metal is
classified into a surface quality and an internal quality,
and these qualities are closely related to the flow of
molten metal within the mould.

FIGs. 1a and 1b illustrate a mould used in the
25 general continuous casting method. Referring to these
drawings, a molten metal is supplied into a mould 10
through a submerged nozzle 11 which has two discharge
holes 11a. The molten metal which is discharged from the
two discharge holes forms jet flows toward a narrow face
30 13, and the jet flow collides with the narrow face 13 to
be divided into an ascending flow U and a descending flow

D. That is, the jet flow is divided into four recirculating streams U1, U2, D1 and D2. In FIG. 1b, reference code S indicates a turning point of the recirculating streams.

5 The molten metal which is introduced into the mold contains non-metallic inclusions (to be also called "inclusions" below) such as Al_2O_3 , MnO , SiO_2 and the like which have been formed in the pre-treating stage or have come from the refractory materials. The molten metal
10 further includes inert gas bubbles (to be also called "gas bubbles" below) which have been injected into the submerged nozzle 11, for preventing the clogging of the nozzle 11. The gas bubbles have sizes of several scores of microns to several millimeters. The inclusions and gas
15 bubbles which are contained in the upper recirculating streams have a density lower than that of the molten metal. Therefore, they are subjected to a floating force in a direction opposite from the gravity, and therefore, they move in the combined vector direction of the molten
20 metal flow and the floating force. Then they gradually move toward the meniscus of the molten metal, to be captured by the mold flux 14.

However, the inclusions and gas bubbles which are contained in the lower recirculating streams D pass
25 through the jet flow region near the nozzle discharge holes 11a before moving toward the upper recirculating streams U. The velocity of the jet flow is faster than the ascending velocity due to the floating force, and therefore, the inclusions and the gas bubbles rarely pass
30 through the jet flow. Accordingly, the inclusions and the gas bubbles which are contained in the lower

recirculating streams cannot reach the meniscus of the molten metal, but continuously circulate along with the lower recirculating streams. Therefore, they are likely to remain within the cast metal. Particularly, in the case of the continuous curved caster, the particles contained in the lower recirculating streams spirally moves due to the influence of the floating force to be ultimately adhered on the solidified layer, i.e., on the upper layer of the cast piece, thereby forming an inclusion/gas bubble accumulated region in the upper layer of the cast piece.

When the cast piece is subjected to a rolling, the residual inclusions and gas bubbles are exposed to the surface, to cause surface defects. Or they remain within the cast piece, and when an annealing is carried out, the gas bubbles expand to cause internal defects.

In order to solve this problem and to improve the quality of the cast piece, conventionally the discharge angle θ of the submerged nozzle is properly adjusted, so as to improve the quality of the cast piece. The discharge angle θ of the submerged nozzle gives a great influence to the flow of the molten metal.

If the discharge angle θ is increased, the amount of the descending flow increases, while that of the ascending flow decreases. As a result, the velocity of the molten metal on the meniscus of the melt is slowed, so that a stable surface of the melt is maintained. Therefore, the workability is improved, and the initial solidification is stably carried out, thereby upgrading the surface quality of the cast piece. However, if the discharge angle θ is increased, large amounts of

inclusions and gas bubbles are buried deeply into the cast piece, because they lose the opportunity of floating to the meniscus of the melt. Thus the internal quality of the cast piece is aggravated.

5 On the other hand, if the discharge angle θ is decreased, the amount of the descending flow decreases, and therefore, the defects due to the inclusions and the gas bubbles may decrease. However, if the discharge angle is decreased, the amount of the ascending flow
10 increases, and the velocity of the molten metal at the meniscus of the melt steeply increases. Therefore, the surface quality of the cast piece is aggravated due to the entrainment of the mould flux at the melt surface, and due to the formation of vortex. These problems become so
15 much more serious, as the casting speed becomes faster.

Thus, if only the submerged nozzle is employed, there is confronted with a limit in controlling the flow of the molten metal. Therefore, as shown in FIG. 2a, an electromagnetic brake ruler (EMBR) 20 is installed
20 immediately below the discharge hole 11a of the submerged nozzle. Thus the Lorentz force based on a magnetic field and a flow is utilized to decrease the flow velocity. (This is proposed in Swedish Patent SE 8,003,695, and US Patent 4,495,984.)

25 The method of FIG. 2a has been put to the practical use, but it is not used at present because flow distortions occur in the direction of evading the flow resistance of the magnetic field, rather than decreasing the flow velocity by the magnetic field.

30 In order to overcome this problem, the magnetic field is horizontally distributed over the entire width of

the mould as shown in FIGs. 2b and 2c. (Swedish Patent SE 9,100,184, US Patent 5,404,933, and Japanese Patent Application Laid-open No. Hei-2-284750). However, the distortion phenomenon has been observed in these methods
5 all the same.

When a dc magnetic field is not applied, the molten metal which has been discharged from the discharge holes 11a of the submerged nozzle 11 forms flow fields as shown in FIG. 3a. However, if the magnetic field is applied
10 over the entire width of the mould, the flow steams are formed as shown in FIG. 3b. That is, compared with the case where there is magnetic field, the jet flow is markedly spread in the thickness direction of the mould. Therefore, the average velocity of the jet flow directed
15 toward the mould narrow face is slowed.

As the velocity of the jet flow is slowed, the inclusions and the gas bubbles of several scores to several hundreds of microns have a long way to travel from the descending flow region to the ascending flow region,
20 compared with the case where a magnetic field is not applied.

Meanwhile, the most part of the inert gas which has been injected through the nozzle into the molten metal has sizes of several millimeters, and floats from between the
25 narrow faces to the meniscus of the melt (the floating distance depends on the molten metal injection speed and on the amount of the injected gas, and this distance corresponds from near the discharge hole to the narrow face in the case where the minimum gas amount is injected,
30 while it corresponds from immediately above the discharge hole to the narrow face in the case where the maximum gas

amount is injected). If the velocity of the main flow is fast, the direction of the main flow is not greatly affected by the floating of the inert gas bubbles. However, if the average velocity of the main flow is
5 decreased by applying a magnetic field, the direction of the main flow is greatly influenced by the floating force of the inert gas. The main flow is raised toward the surface of the melt by the floating force of the inert gas and by the flow resistance of the magnetic field which is
10 established immediately below the submerged nozzle. When the influence by the floating force of the inert gas disappears after the flow has been much proceeded, the flow is lowered in the casting direction to draw an S curve as shown in FIG. 3b (this is called "non-solidified
15 rising molten metal flow adjacent to the submerged nozzle"). Thus the flow collides with the mould narrow face with a large angle.

When the jet flow is cleaved by colliding with the narrow face of the mould, the flow amounts of the cleaved
20 flows are decided by the colliding angle. For example, if a perpendicular collision occurs, the upper and lower cleaved flows are same in their flow amounts. However, if the colliding angle is lowered, the amount of the lower flow is increased. Under this condition, the ratio
25 of the amount of the lower flow to that of the upper flow is decided by the casting speed, the nozzle discharge angle, the injected amount of the inert gas, and the magnetic field strength. However, at the general working conditions, the ratio is about 6:4, if a magnetic field
30 is not applied. If a magnetic field is applied over the entire width, the ratio becomes 8:2. Therefore, if a

magnetic field is applied like in the conventional method, the amount of the lower flow increases, while the amount of the upper flow decreases. Accordingly, the velocity of the molten metal decreases immediately below the melt
5 meniscus, and the height difference of the melt meniscus also decreases. Thus the melt face is stabilized, so as to improve the surface quality.

However, due to the increase in the amount of the lower flow, large amounts of inclusions and gas bubbles
10 are contained in the recirculating flow. Therefore, if a magnetic field is applied over the entire width, the increase of the floating opportunity owing to the decrease of the average velocity is offset. Therefore, the improvement of the internal quality cannot be expected due
15 to the fact that the inclusions and the fine inert gas bubbles are not removed.

SUMMARY OF THE INVENTION

In order to solve the above described problems, the
20 present inventors carried out theoretical studies and simulating experiments. Based on these studies and researches, the present inventors came to propose the present invention.

Therefore it is an object of the present invention to
25 provide a continuous casting method, in which an induced dc magnetic field is applied in parallel with the molten metal discharge direction, and thus, the residual amounts of inert gas bubbles and non-metallic inclusions such as Al_2O_3 , MnO and the like are minimized, thereby
30 improving the internal quality of the cast pieces.

It is another object of the present invention to

provide a continuous casting device which is used for the above continuous casting method.

In achieving the above objects, the continuous casting method according to the present invention includes
5 the steps of: feeding a molten metal through discharge holes of a submerged nozzle into a mould; and establishing a magnetic field on the incoming molten metal, characterized in that a main flux part of the magnetic field is distributed from immediately above the
10 discharge holes of the submerged nozzle in parallel with a discharge direction of the molten metal.

In another aspect of the present invention, the continuous casting device according to the present invention includes: a mould with a submerged nozzle
15 installed therein, the submerged nozzle having a pair of discharge holes directed toward narrow faces of the mould; and an electromagnetic brake ruler for establishing a magnetic field within the mould, and

the electromagnetic brake ruler includes: a base
20 frame surrounding the mould; iron cores projecting from near wide faces of the mould and with induction coils wound thereon; and a pair of electromagnetic transferring parts connected to the iron cores, keeping a certain distance from the wide faces of the mould, and disposed
25 immediately above the discharge holes of the submerged nozzle toward narrow faces of the mould and in parallel with the discharge direction of the molten metal.

Further, the device of the present invention further includes a means for controlling a non-solidified rising
30 molten metal flow near the submerged nozzle.

BRIEF DESCRIPTION OF THE DRAWINGS

The above objects and other advantages of the present invention will become more apparent by describing in detail the preferred embodiment of the present invention
5 with reference to the attached drawings in which:

FIG. 1 illustrates the flow of the molten metal within the general mould, with FIG. 1a being a plan view, and FIG. 1b being a side sectional view;

FIGs. 2a, 2b and 2c illustrate the constitutions of
10 the conventional continuous casting devices, with various electromagnetic brake rulers being installed thereon;

FIGs. 3a and 3b illustrate the molten metal flow within the mould in accordance with the presence or absence of the conventional electromagnetic brake ruler;

15 FIG. 4 illustrates the constitution of the continuous casting device according to the present invention, with FIG. 4a being a plan view, FIG. 4b being a side sectional view, and FIG. 4c being a perspective view of the critical portion;

20 FIG. 5 illustrates the constitution of another embodiment of the continuous casting device according to the present invention, with FIG. 5a being a side sectional view, and FIG. 5b being a perspective view of the critical portion;

25 FIG. 6 is a side sectional view of the continuous casting device in which the electromagnetic transferring parts of the second embodiment are added;

FIG. 7 illustrates the flow of the discharged molten metal within the mould of the present invention; and

30 FIGs. 8a and 8b comparatively illustrate the molten metal flows for different embodiments of the continuous

casting device according to the present invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Basically in the present invention, a proper
5 magnetic field is established from immediately above
discharge holes of a submerged nozzle within a mould, in
parallel with the molten metal discharge direction.

FIG. 4 illustrates the constitution of a first
embodiment of the continuous casting device according to
10 the present invention, with FIG. 4a being a plan view,
and FIG. 4b being a side sectional view.

The continuous casting device according to the
present invention includes: a submerged nozzle 11 with a
pair of discharge holes 11a formed therein; a mould 10
15 with the submerged nozzle installed therein, the
discharge holes 11a being directed toward narrow faces 13
of the mould 10; and an electromagnetic brake ruler 40
for establishing an induced magnetic field within the
mould 10.

20 The major feature of the continuous casting device
according to the present invention is the electromagnetic
brake ruler. FIG. 4c illustrates in detail the
electromagnetic brake ruler (EMBR).

As shown in FIG. 4c, the electromagnetic brake ruler
25 40 of the present invention includes: a base frame 43
surrounding the mould 10; iron cores 44 projecting from
near wide faces 12 of the mould; and a pair of
electromagnetic transferring parts 41 and 42 connected to
the iron cores 44 and keeping a certain distance from the
30 wide faces 12 of the mould 10.

The base frame 43 may be formed integrally with the

iron cores 44. Or it may be formed separately from the iron cores in such a manner that it may be moved in the direction of the wide faces. In the latter case, the induction coils 45 can be easily wound.

5 The iron cores 44 are wound with the induction coils 45, and therefore, they may induce induction currents in the mould.

Further, the pair of electromagnetic transferring parts 41 and 42 are connected to the iron cores 44,
10 keeping a certain distance from the wide faces of the mould, and thus supplies an induced dc magnetic field to the mould. The electromagnetic transferring parts 41 and 42 of the present invention are disposed starting from immediately above the discharge holes 11a of the submerged
15 nozzle toward the narrow faces 13 of the mould and in parallel with the molten metal discharge directions. That is, the electromagnetic transferring parts 41 and 42 of the electromagnetic brake ruler 40 should be disposed in parallel with the discharge directions of the molten
20 metal. The electromagnetic transferring parts 41 and 42 serve the role of changing the distribution contour of the magnetic field of the iron cores, before transferring the field to the mould. Therefore, they do not have to consist of a single piece, but may be a plurality of
25 pieces.

The electromagnetic brake ruler 40 is a means for controlling the rising flow of the non-solidified molten metal near the submerged nozzle. The structure of the ruler 40 may be made different depending on the discharge
30 angle of the molten metal. The discharge angle θ of the discharge holes may be inclined downward at angle of 1 to

90 degrees. The electromagnetic transferring parts 41 and 42 should be disposed in parallel with the discharge direction of the molten metal even in the case where the discharge angle θ is varied.

5 Meanwhile, in the electromagnetic brake ruler 40, as shown in FIG. 4b, the electromagnetic transferring parts 41 and 42 may extend up to the narrow face 13 of the mould. However, it is important that the parts 41 and 42 should cover the region immediately above the molten metal
10 jet nearest to the submerged nozzle (or the region where floating of the inert gas is brisk). In the region immediately above the molten metal jet, the floating of the inert gas is most brisk. Therefore, in this region, numerous gas bubbles can be observed, and the size of
15 this region depends on the casting speed and the injection amount of the inert gas. Under the usual conditions, the mentioned region is positioned between the submerged nozzle and the narrow face. In the case where the electromagnetic brake ruler 40 covers the area immediately
20 above the molten metal jet, the constitutions of the base frame 53, the iron core 54 and the induction coil 55 are as shown in FIG. 5b, and are similar to those of FIG. 4c. However, the transferring parts 51 and 52 become short so as to cover only the region immediately above the molten
25 metal jet.

That is, the electromagnetic brake ruler 40 should cover the region immediately above the molten metal jet nearest to the submerged nozzle at least, and should extend up to the narrow face of the mould at most.

30 Now the continuous casting method using the above described apparatus will be described.

Generally, if a conductive material moves across magnetic fluxes, then electric currents are induced in the conductive material. Owing to the interaction between the induced electric currents and the magnetic field, the Lorentz force is generated, which acts in a direction opposite to the motion of the conductive material, and is proportional to the multiplication of the moving velocity of the conductive material by the square of the applied magnetic field strength. The Lorentz force reduces the velocity of the flow, alters the direction of the flow, or cleaves the flow into a plurality of streams. Accordingly, if a magnetic field is properly applied over a flow, then the flow velocity and the flow direction can be properly altered.

The present invention is based on this principle. That is, during a continuous casting of a metal, the residual inclusions and gas bubbles are minimized, so that the internal quality problem of the cast product is improved. However, the method of the present invention has an essential difference from the conventional methods as described below.

That is, if the residual inclusions and gas bubbles within the cast product are to be minimized, the inclusions and gas bubbles should be contained in the upper layer of the recirculating stream to the maximum. That is, they have to be made to float.

For this, the following conditions have to be satisfied.

First, the velocity of the jet flows discharged from the discharge holes has to be slowed before the jet flow is divided into an ascending flow and a descending flow.

Thus, a sufficient time has to be secured so that the inclusions and gas bubbles contained in the descending flow can float toward the surface of the ascending flow.

Second, the flow direction has to be controlled so that the collision angle of the jet flow of the molten metal at the narrow face would not be lowered. Thus the amount of the ascending flow has to be made greater, so that the greater part of the inclusions and gas bubbles should be contained in the ascending flow.

10 For this purpose, in the continuous casting devices of FIGs. 4 and 5, magnetic fluxes are applied in parallel with the discharge direction of the molten metal jet.

That is, if the magnetic field is distributed in parallel with the discharge direction of the molten metal jet, then the jet flow becomes as shown in FIG. 7. Consequently, the plan view of the jet flow pattern becomes as shown in the upper portion of FIG. 3b, while its frontal view is as shown in the lower portion of FIG. 3a. Thus the overall molten metal flow is slowed.

20 Therefore, in the present invention, the flow is spread in the thickness direction of the mould as well as being slowed, so that the time for floating of the inclusions and gas bubbles can be sufficiently secured. At the same time, at the portion A of FIG. 4b where the floating

25 force acts, the rising of the flow is inhibited by the flow resistance owing to the magnetic field applied above the flow. Further, the flow direction is made not to be distorted, and the colliding angle (at the narrow face) is sufficiently secured, so that the amount of the

30 descending flow would not increase.

Thus the inclusions and gas bubbles contained in the

descending flow are minimized.

Meanwhile, the colliding angle of the molten metal becomes different depending on the discharge angle at the submerged nozzle, the length of the applied magnetic
5 field, and its field strength. If the colliding angle becomes unnecessarily upward, the flow velocity on the melt surface becomes too fast. Therefore, the floating time has to be designed such that the maximal floating can be realized with the minimal ascending flow amount.

10 The length of the electromagnetic brake ruler 40 should be such that it should extend from the molten metal discharge point to the narrow face at the maximum. The variation of the flow of the molten metal in accordance with the length of the magnetic field is illustrated in
15 FIG. 8.

That is, FIG. 8a illustrates a case where a brisk floating occurs in a region corresponding to 1/4 of the length from the discharge hole 11a to the narrow face. That is, the electromagnetic brake ruler 40 covers only
20 this region (immediately above the molten metal jet). FIG. 8b illustrates a case where the ruler 40 is extended up to the narrow face. In both of the drawings, the flow patterns of the discharged molten metal are illustrated. It is seen that in both of the cases, the flow patterns
25 are almost same to each other. This owes to the fact that most part of the inert gas floats from near the discharge hole to the melt surface, and that the floating of the inert gas slightly pushes up the molten metal flow. However, it is seen that the magnetic field cannot give
30 any great influence to the flow of the molten metal near the narrow face.

Accordingly, if the upward biasing of the flow is inhibited at the region where the floating is brisk, then the overall flow pattern of the molten metal will become same in both of the above mentioned cases. Further, near
5 the narrow face remote from the brisk floating region, the molten metal has been spread in the thickness direction of the mould, and has been slowed. Therefore, the Lorentz force become negligible in this area. Consequently, it is important that the electromagnetic
10 brake ruler 40 should cover at least the region where the floating of the inert gas is brisk. Outside this region, the distribution of the magnetic field is not much important. Therefore, a plurality of pieces of the electromagnetic transferring parts may be provided as
15 shown in FIG. 6 in such as manner that the inhibited non-solidified molten metal flow is not destroyed, and that the pieces should extend up to the narrow face outside the brisk region. In this manner, fine adjustments of the flow near the narrow face are possible. FIG. 6
20 illustrates a case where the electromagnetic transferring parts with a varied angle are disposed near the narrow face outside the brisk floating region, so that the colliding angle can be adjusted slightly upward, in a state with the non-solidified rising molten metal flow
25 inhibited. FIG. 6 also illustrates a case where the electromagnetic transferring parts are added below the flow near the narrow face so as to reduce the velocity of the descending flow. In order to carry out fine adjustments near the narrow face, the electromagnetic
30 transferring parts of various shapes may be added near the narrow face.

When carrying out the continuous casting using the above described casting device, about 35 - 40% of discharged amount of the molten metal can be made to ascend.

5 Here, the magnetic flux density of the electromagnetic brake ruler 40 should be preferably 1000 - 6000 Gausses. If the applied flux density is less than 1000 Gausses, the altering of the flow becomes insufficient, while if it exceeds 6000 Gausses, any more
10 altering of the flow cannot be expected.

Now the present invention will be described based on experimental examples.

<Comparative example 1>

15 Like in the general casting conditions, a molten metal discharge rate of 2.6 tons/min was adopted, and the downward discharge angle was adjusted to 0-25 degrees. With a magnetic field not applied, a computer-aided simulating experiment was carried out. Thus a comparison
20 was made between the upper recirculating stream and the lower recirculating stream to measure the number of the inclusions and gas bubbles.

In the case where a magnetic field was not applied, 35 - 40% of the discharged molten metal was formed into an
25 ascending flow, the rest forming a descending flow. The time for the discharged jet flow to reach the narrow face was about 0.55 - 1 second. Thus about 70% of the inclusions and gas bubbles was contained in the upper recirculating stream, while the rest is contained in the
30 lower recirculating stream.

<Comparative example 2>

At conditions same as those of the comparative example 1, a magnetic field was applied as shown in FIG. 2b to carry out a computer-aided simulating experiment.

5 Then a comparison was made between the upper recirculating stream and the lower recirculating stream to measure the inclusions and gas bubbles.

In this case, only about 10 - 20% of the discharged molten metal was formed into an ascending flow, and about
10 34% of the inclusions and gas bubbles were floated to the upper recirculating stream, while the remaining 66% was contained in the lower recirculating stream. The time for the discharge jet flow to reach the narrow face was about 1.4 - 3 seconds in average.

15 From the above results, it is seen that it was worse than the case where a magnetic field was not applied. This corresponds to the actual factory circumstance.

<Inventive example>

20 At conditions same as those of the comparative example 1, a magnetic field was applied as shown in FIG. 4b. Then a computer-aided simulating experiment was carried out, and then, a comparison was carried out between the upper recirculating stream and the lower
25 recirculating stream to measure the inclusions and gas bubbles. Here, the flux density of the applied magnetic field was varied within the range of 1000 - 6000 Gauss.

In this inventive example, about 35 - 40% of the discharged molten metal was formed into an ascending flow.
30 The time for the discharged jet flow to reach the narrow face was about 1.4 - 3 seconds in average. Further,

about 93% of the inclusions and gas bubbles was floated to the upper recirculating stream, while only 9% of them was remained in the lower recirculating stream. Thus the separation of the inclusions and gas bubbles was very much
5 superior.

According to the present invention as described above, the separation capability for the non-metallic inclusions and the gas bubbles is improved. Therefore,
10 the internal defects of the cast piece due to the non-metallic inclusions and the gas bubbles are markedly diminished.

15

20

25

30

WHAT IS CLAIMED IS:

1. A continuous casting method comprising the steps of:
5 feeding a molten metal through discharge holes of a submerged nozzle into a mould; and
establishing a magnetic field on the molten metal thus fed,
characterized in that a main flux part of the
10 magnetic field is distributed from immediately above said discharge holes of said submerged nozzle in parallel with a discharge direction of the molten metal.
2. The continuous casting method as claimed in
15 claim 1, wherein 35 - 40% of the molten metal thus discharged is made to ascend by the magnetic field.
3. The continuous casting method as claimed in
claim 1, wherein the magnetic field thus applied has a
20 flux density of 1000 - 6000 Gaussses.
4. A continuous casting device comprising:
a mould with a submerged nozzle installed therein,
said submerged nozzle having a pair of discharge holes
25 directed toward narrow faces of said mould; and
an electromagnetic brake ruler for establishing a magnetic field within said mould,
said electromagnetic brake ruler comprising:
a base frame surrounding said mould;
30 iron cores projecting from near wide faces of said mould and with induction coils wound thereon; and

a pair of electromagnetic transferring parts connected to said iron cores, keeping a certain distance from said wide faces of said mould, and disposed immediately above said discharge holes of said submerged
5 nozzle toward narrow faces of said mould and in parallel with a discharge direction of the molten metal.

5. A continuous casting device comprising:
a control means for controlling a non-solidified
10 ascending molten metal flow near said submerged nozzle.

6. The continuous casting device as claimed in claim 5, wherein said control means comprises at least a pair of electromagnetic transferring parts for applying
15 magnetic fields; said electromagnetic transferring parts are disposed in parallel with a molten metal jet flow direction (near said discharge hole of said submerged nozzle); and said electromagnetic transferring parts establish main magnetic fluxes perpendicular to a flow of
20 the molten metal and perpendicular to a drawing direction of cast strands.

7. The continuous casting device as claimed in any one of claims 5 and 6, wherein said electromagnetic
25 transferring parts cover a region immediately above the molten metal jet nearest to said submerged nozzle.

8. The continuous casting device as claimed in claim 7, wherein said electromagnetic transferring parts
30 have an arbitrary shape at a region where a floating of inert gas is not brisk (that is, outside a region

immediately above the molten metal jet nearest said submerged nozzle).

9. The continuous casting device as claimed in
5 claim 6, wherein the magnetic field has a flux density of
1000 - 6000 Gaussses.

10. The continuous casting device as claimed in
claim 6, wherein disposed angles of said electromagnetic
10 transferring parts are varied within a range of 1 to 90
degrees, so as to make them parallel with the molten
metal jet flow near said submerged nozzle.

11. The continuous casting device as claimed in
15 claim 5, wherein said control means has an operation
range falling between said discharge holes and said narrow
faces.

12. A continuous casting method for casting a molten
20 metal by using the device of claims 5 to 11.

1/10

FIG. 1a

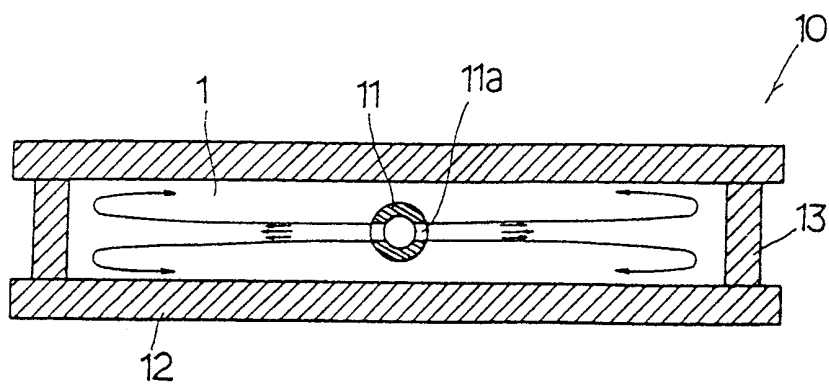
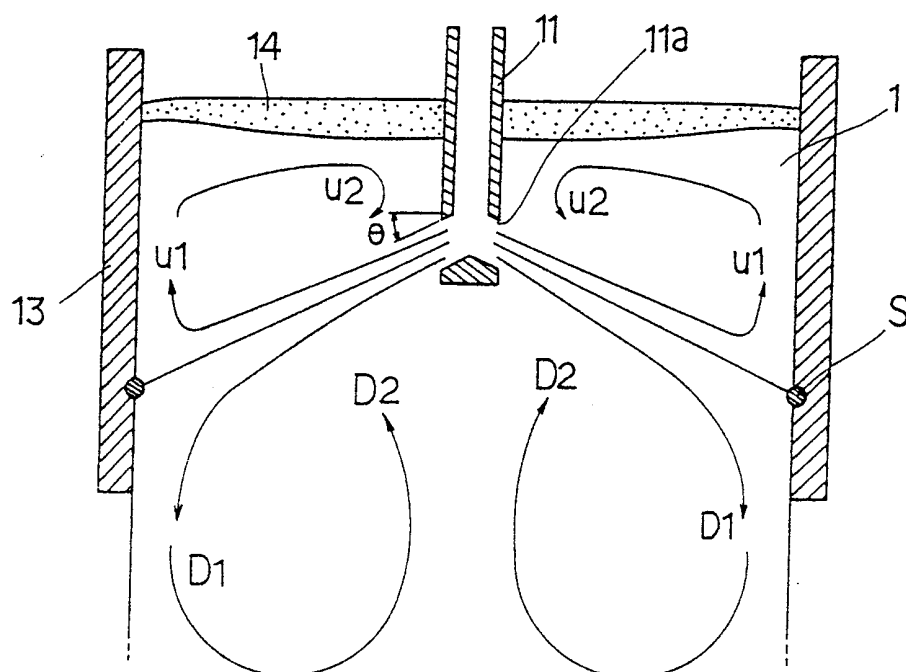


FIG. 1b



2/10

FIG. 2a

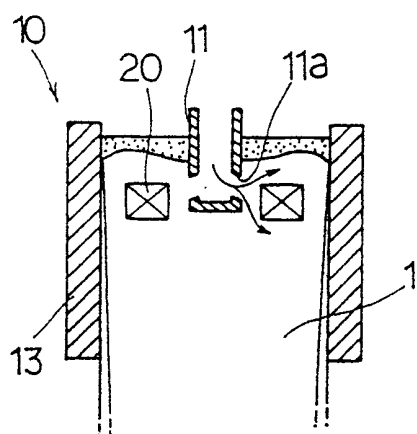


FIG. 2b

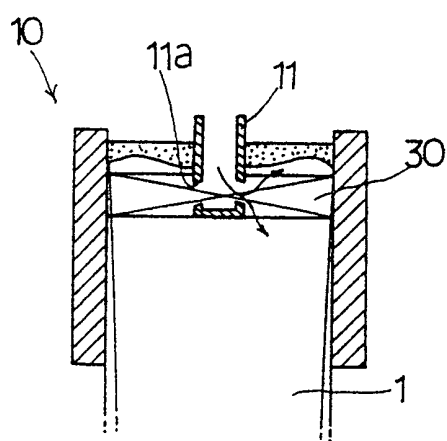
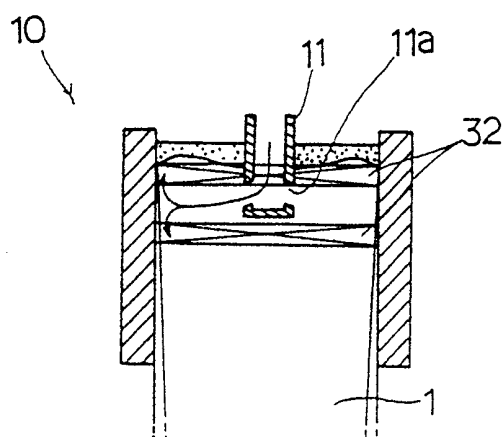
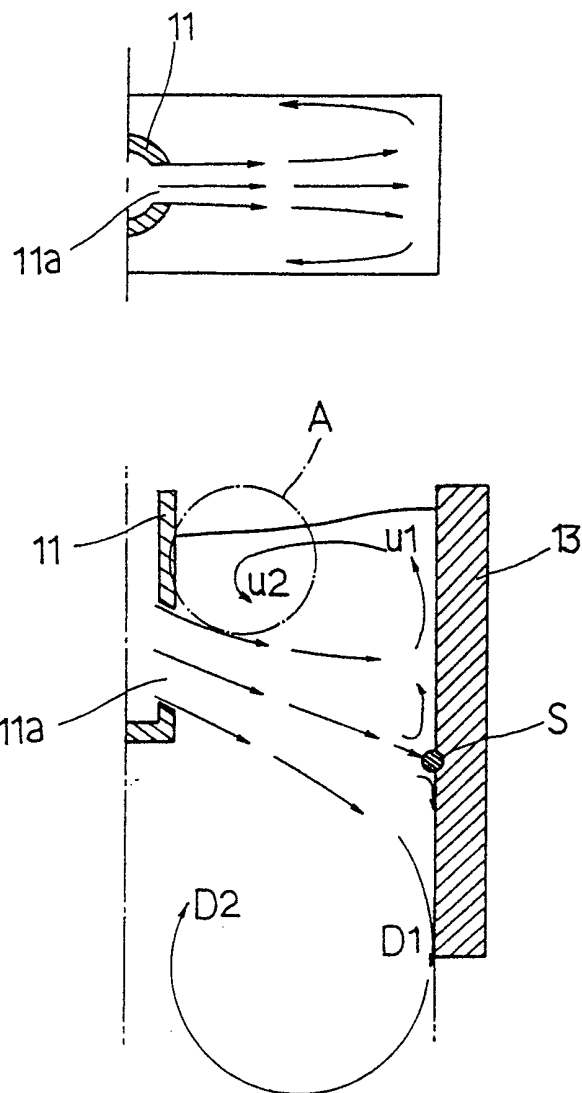


FIG. 2c



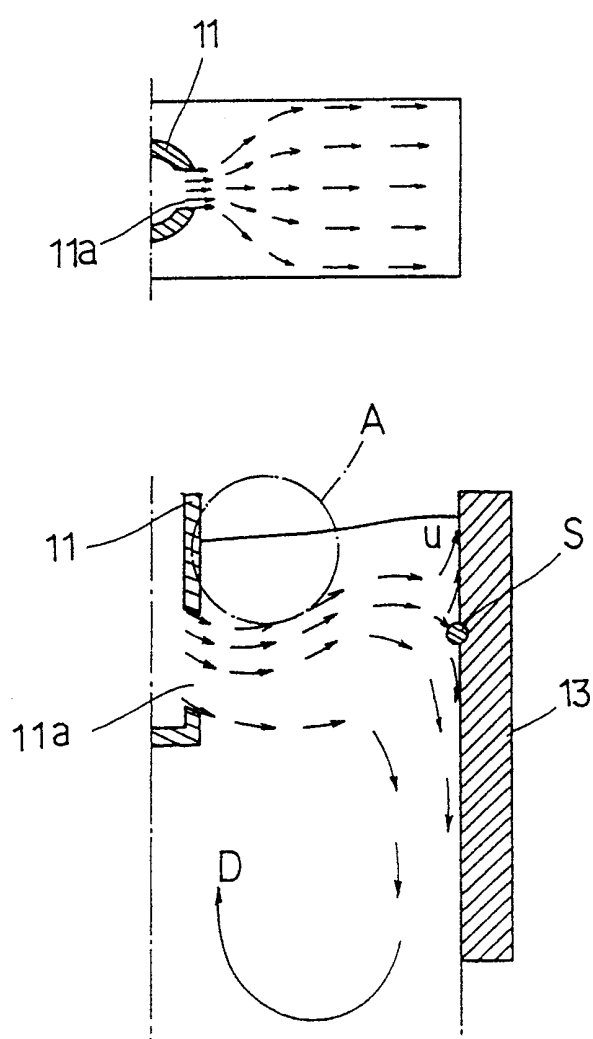
3/10

FIG. 3a



4/10

FIG. 3b



5/10

FIG. 4a

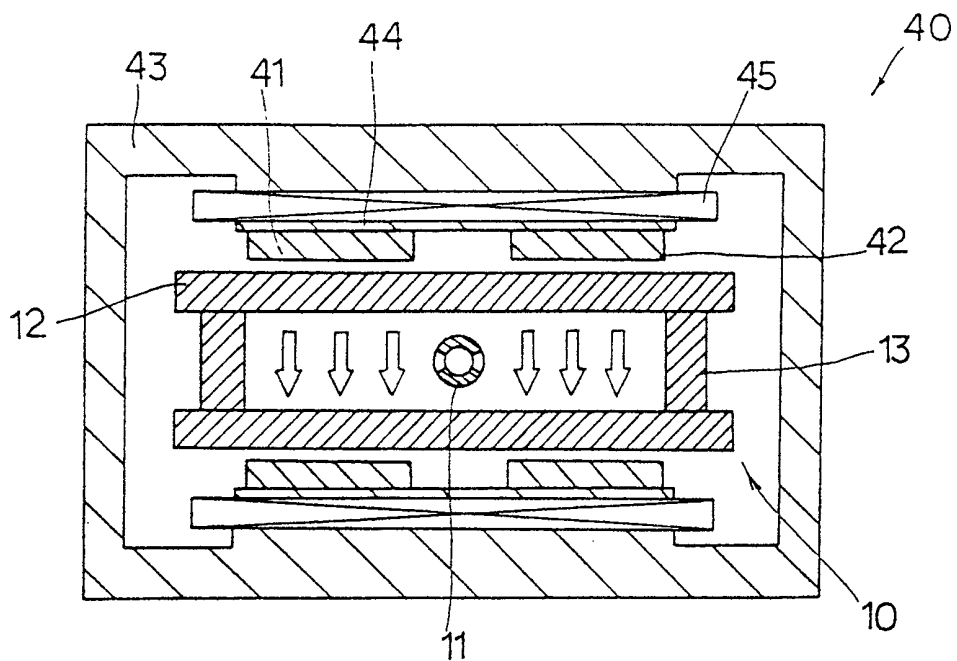
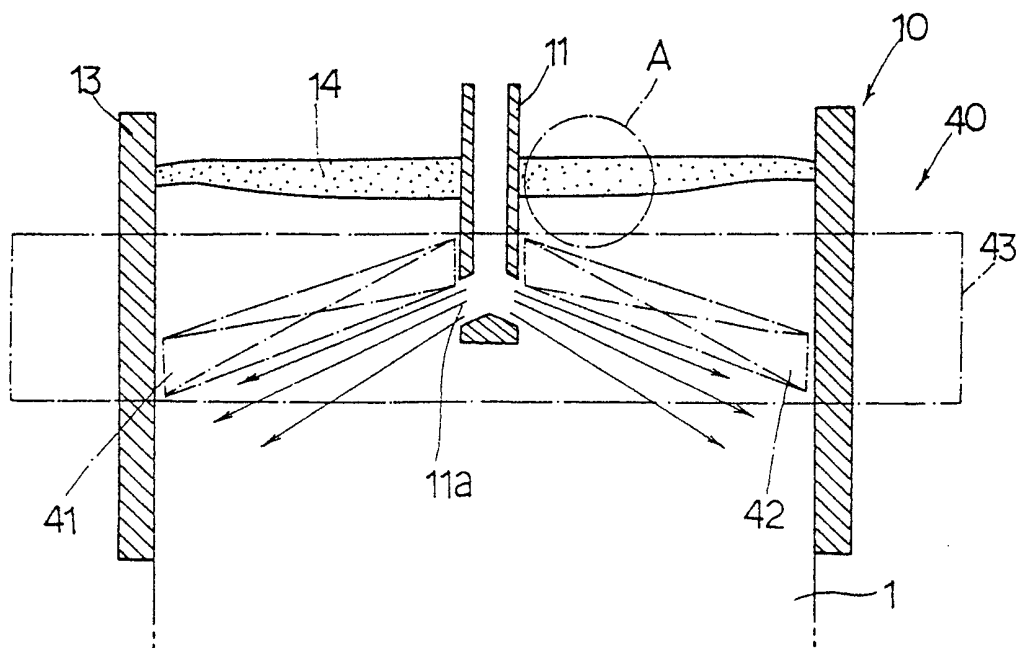


FIG. 4b



6/10

FIG. 4c

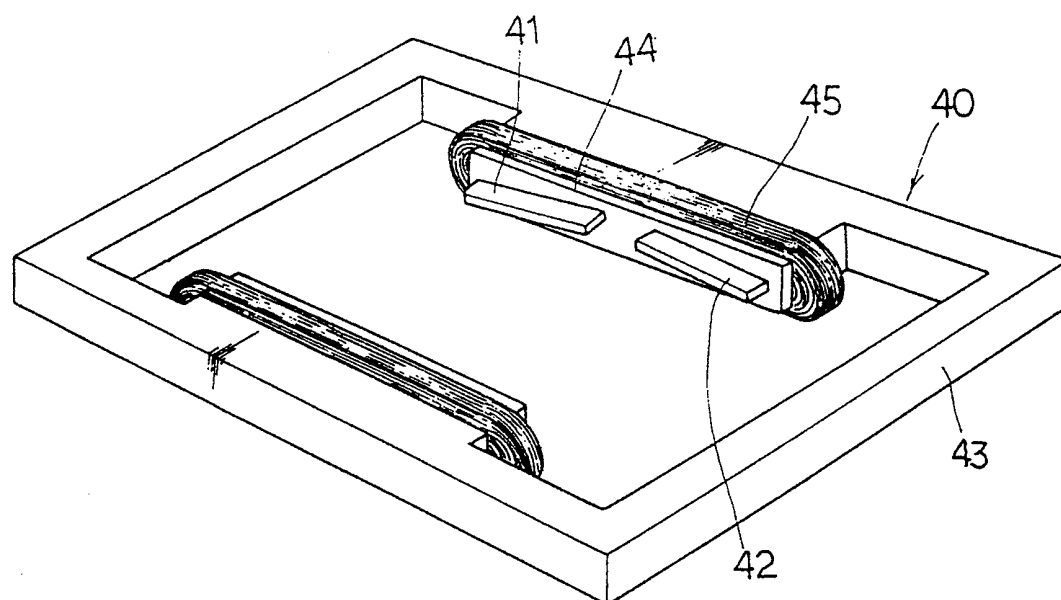
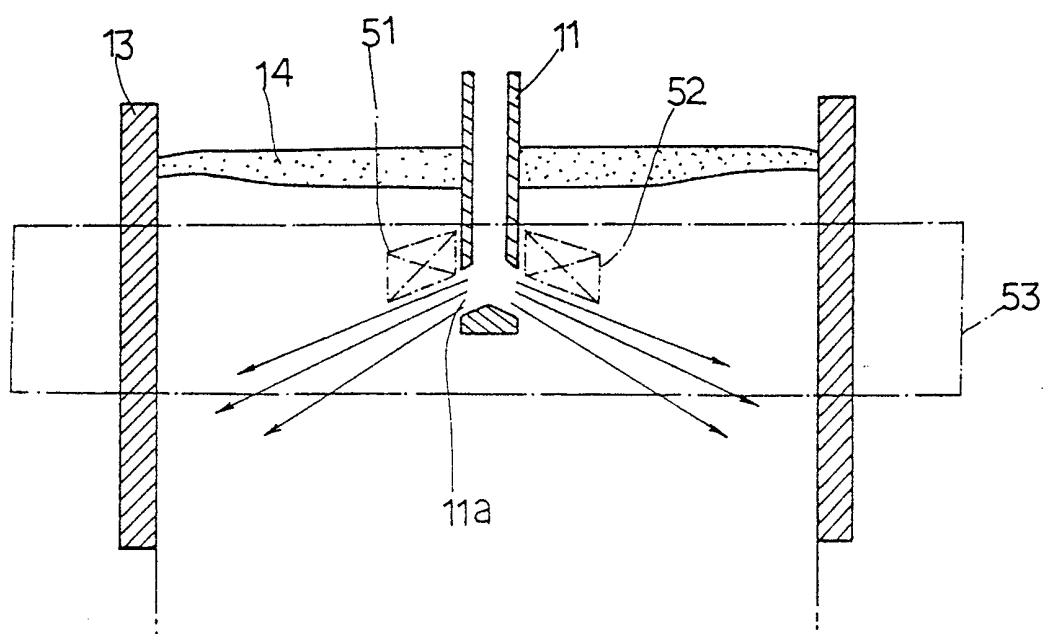
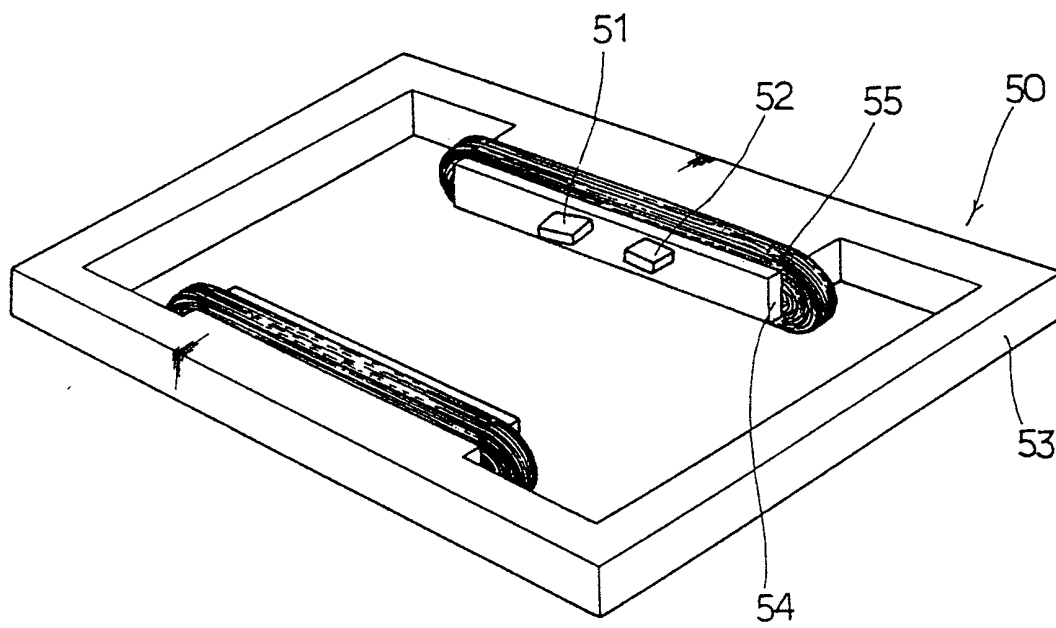


FIG. 5a



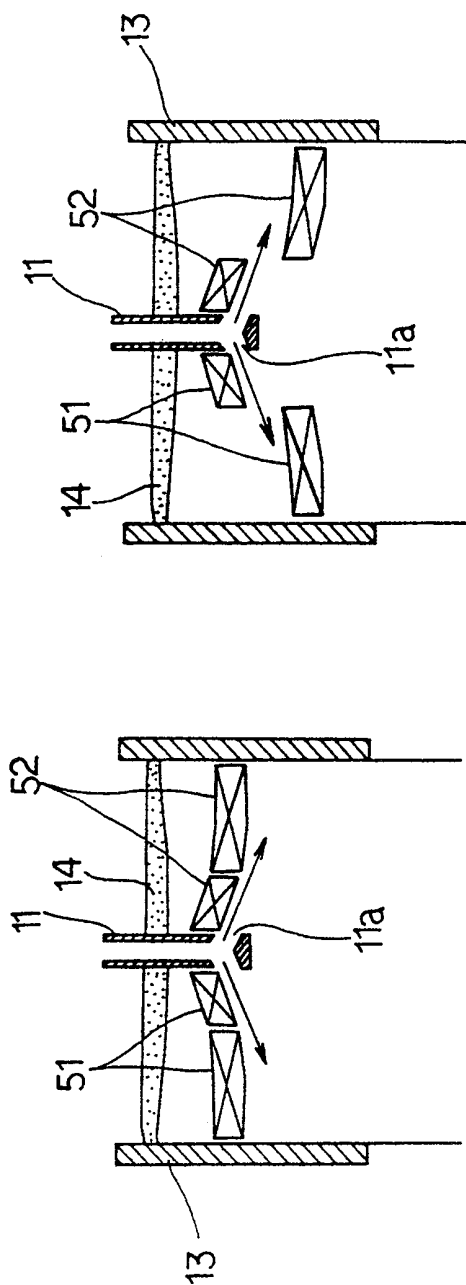
7/10

FIG. 5b



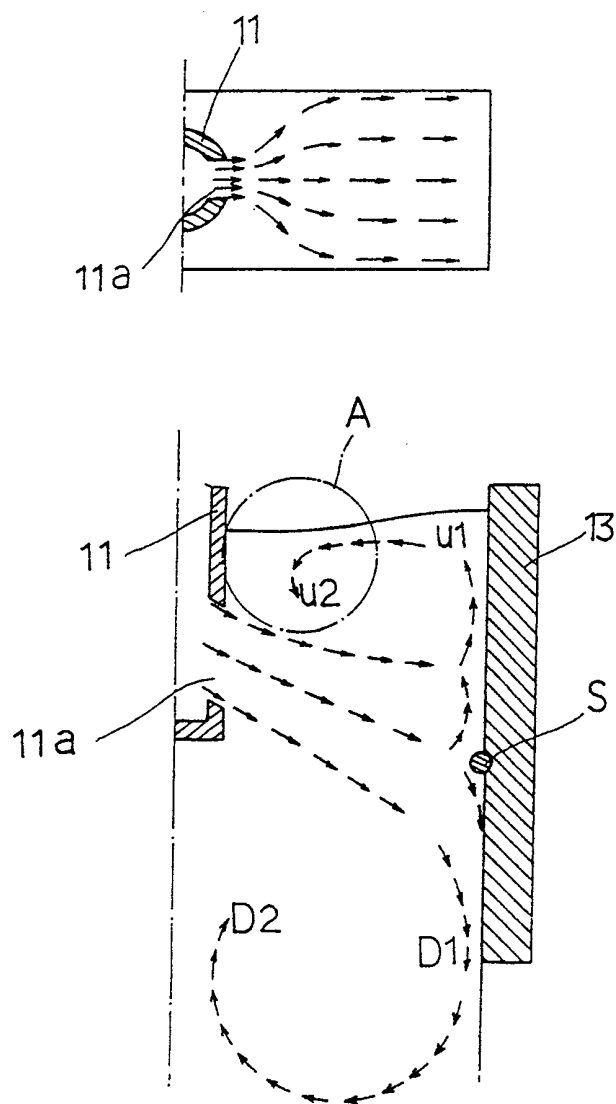
8 / 10

FIG. 6



9/10

FIG. 7



10/10

FIG. 8a

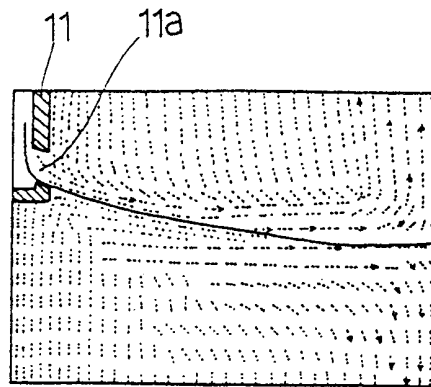
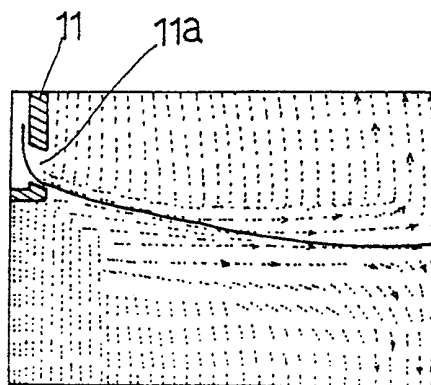


FIG. 8b



INTERNATIONAL SEARCH REPORT

International application No.
PCT/KR 99/00413

A. CLASSIFICATION OF SUBJECT MATTER		
IPC ⁷ : B 22 D 11/10		
According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED		
Minimum documentation searched (classification system followed by classification symbols)		
IPC ⁷ : B 22 D 11/10, 11/04		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)		
WPI, EPODOC		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	EP 0040383 A1 (ASEA AB) 25 November 1981 (25.11.81) claims 1-12; fig. 1-4 & US 4495984 A document cited in the application.	1,4,5,6
A	EP 0317789 A1 (ASEA BROWN BOVERI) 31 May 1989 (31.05.89) claims 1-6; fig. 1-3.	1,4,5,6
A	DE 3122155 A1 (TI LTD.) 18 March 1982 (18.03.82) fig. 4-6.	1,4

☐ Further documents are listed in the continuation of Box C. ☒ See patent family annex.		
* Special categories of cited documents: „A“ document defining the general state of the art which is not considered to be of particular relevance „E“ earlier application or patent but published on or after the international filing date „L“ document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) „O“ document referring to an oral disclosure, use, exhibition or other means „P“ document published prior to the international filing date but later than the priority date claimed „T“ later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention „X“ document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone „Y“ document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art „&“ document member of the same patent family		
Date of the actual completion of the international search		Date of mailing of the international search report
06 October 1999 (06.10.99)		09 December 1999 (09.12.99)
Name and mailing address of the ISA/AT Austrian Patent Office Kohlmarkt 8-10; A-1014 Vienna Facsimile No. 1/53424/200		Authorized officer Rieder Telephone No. 1/53424/366

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No.

PCT/KR 99/00413

Im Recherchenbericht angeführtes Patentdokument Patent document cited in search report Document de brevet cité dans le rapport de recherche	Datum der Veröffentlichung Publication date Date de publication	Mitglied(er) der Patentfamilie Patent family member(s) Membre(s) de la famille de brevets	Datum der Veröffentlichung Publication date Date de publication
EP 40383		keine - none - rien	
US A 4495984	29-01-1985	BR A 8103058 CA A1 1178779 DE C0 3161171 EP A1 40383 EP B1 40383 ES A1 511019 ES A1 8303148 JP A2 57017356 JP B4 2020349 SE A 8003695 SE B 436251 SE C 436251 ES A5 511019	09-02-1982 04-12-1984 17-11-1983 25-11-1981 12-10-1983 01-02-1983 01-05-1983 29-01-1982 09-05-1990 20-11-1981 24-11-1984 07-03-1985 01-03-1983
EP A1 317789	31-05-1989	DE C0 3873698 DE T2 3873698 EP B1 317789 JP A2 1150450 SE A0 8704259 SE A 8704259 SE B 465306 SE C 465306	17-09-1992 25-03-1992 12-08-1992 13-06-1989 02-11-1987 03-05-1989 26-08-1991 19-12-1991
DE A1 3122155	18-03-1982	AL A1 71075/81 AU A1 71076/81 BE A2 889093 BE A2 889084 CA A1 1172421 CH A 645048 DD C 159405 DD C 159859 DE A1 3122154 DE A1 3122154 DE C2 3122155 DE C2 3122154 DK A 2467/81 DK A 2468/81 ES A1 502766 ES A5 502766 ES A1 8203248 FR A1 2483817 FR A1 2483818 FR B1 2483817 FR B1 2483818 GB A1 2077161 GB A1 2079195 GB A1 2079196 GB B2 2079195 GB B2 2079196 GB B2 2077161 GR A 75273 HU B 180195 IE B 51298 IT A0 8148603 IT A 1209871 JP A2 57011755 JP A2 57011756 JP B4 60026622 JP B4 61002457 LU A 83414 LU A 83415 NL A 8102682 NL A 8102683 PL A1 231472 PL B1 130800 PT A 73133 PT B 73133 SE A 8103458 SE A 8103459 SE B 443526 SE C 443526 SI A3 1301302 US A 4470448 US A 4479531 US A 4484615 ZA A 8103647	10-12-1981 10-12-1981 01-10-1981 01-10-1981 14-08-1984 14-09-1984 09-03-1983 13-04-1983 18-03-1982 25-03-1982 27-08-1992 24-09-1992 06-12-1981 06-12-1981 01-04-1982 23-04-1982 01-07-1982 11-12-1981 11-12-1981 21-06-1985 09-08-1985 16-12-1981 20-01-1982 20-01-1982 08-08-1984 22-08-1984 06-02-1985 13-07-1984 28-02-1983 26-11-1986 02-06-1981 30-08-1989 21-01-1982 21-01-1982 25-06-1985 24-01-1986 11-09-1981 11-09-1981 04-01-1982 04-01-1982 29-03-1982 29-09-1984 01-07-1981 01-07-1982 06-12-1981 06-12-1981 03-03-1986 12-06-1986 30-03-1987 11-09-1984 30-10-1984 27-11-1984 28-07-1982