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Nakagawa et al.

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(54) **BLOWER AND OUTDOOR UNIT OF AIR
CONDITIONER COMPRISING SAME**

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(71) Applicant: **SAMSUNG ELECTRONICS CO.,
LTD.**, Suwon-si, Gyeonggi-do (KR)

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(72) Inventors: **Suguru Nakagawa**, Yokohama (JP);
Seiji Sato, Yokohama (JP)

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(73) Assignee: **SAMSUNG ELECTRONICS CO.,
LTD.**, Suwon-si (KR)

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Primary Examiner — Carlos A Rivera

Assistant Examiner — Jesse M Prager

(74) *Attorney, Agent, or Firm* — Staas & Halsey LLP

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ABSTRACT

Provided are a blower, capable of suppressing noise occurring in a stator while significantly improving blowing efficiency, and an outdoor unit using the same. The present invention comprises: a bell mouth part spaced apart at a predetermined distance in the radial direction with respect to an outer circumferential end of a propeller fan; and a diffuser part installed on the downstream side of the bell mouth part, and having a flow path area which is enlarged from the upstream side toward the downstream side with a larger magnification rate than the magnification rate of the flow path area in the downstream end of the bell mouth part; and a stator part having a plurality of stators, wherein the stator part is arranged within the diffuser part.

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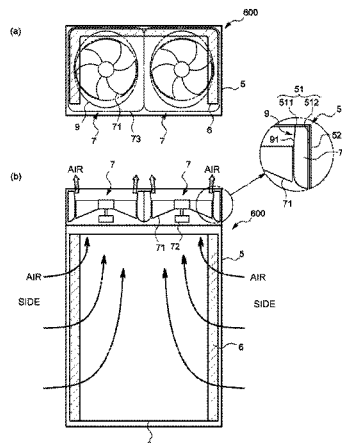
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USPC 415/207, 211.2, 220, 222–223
See application file for complete search history.

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FIG. 1

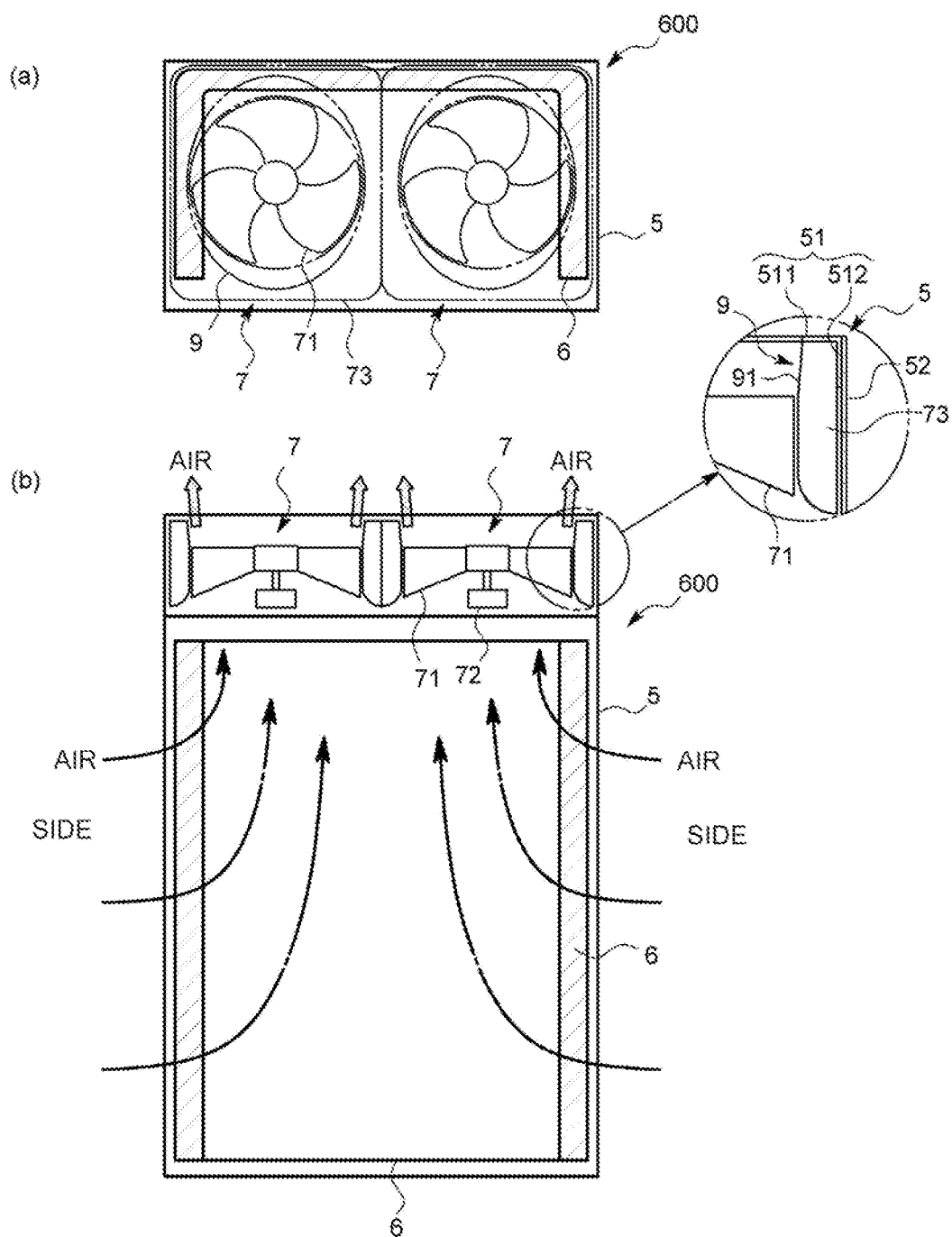


FIG.2

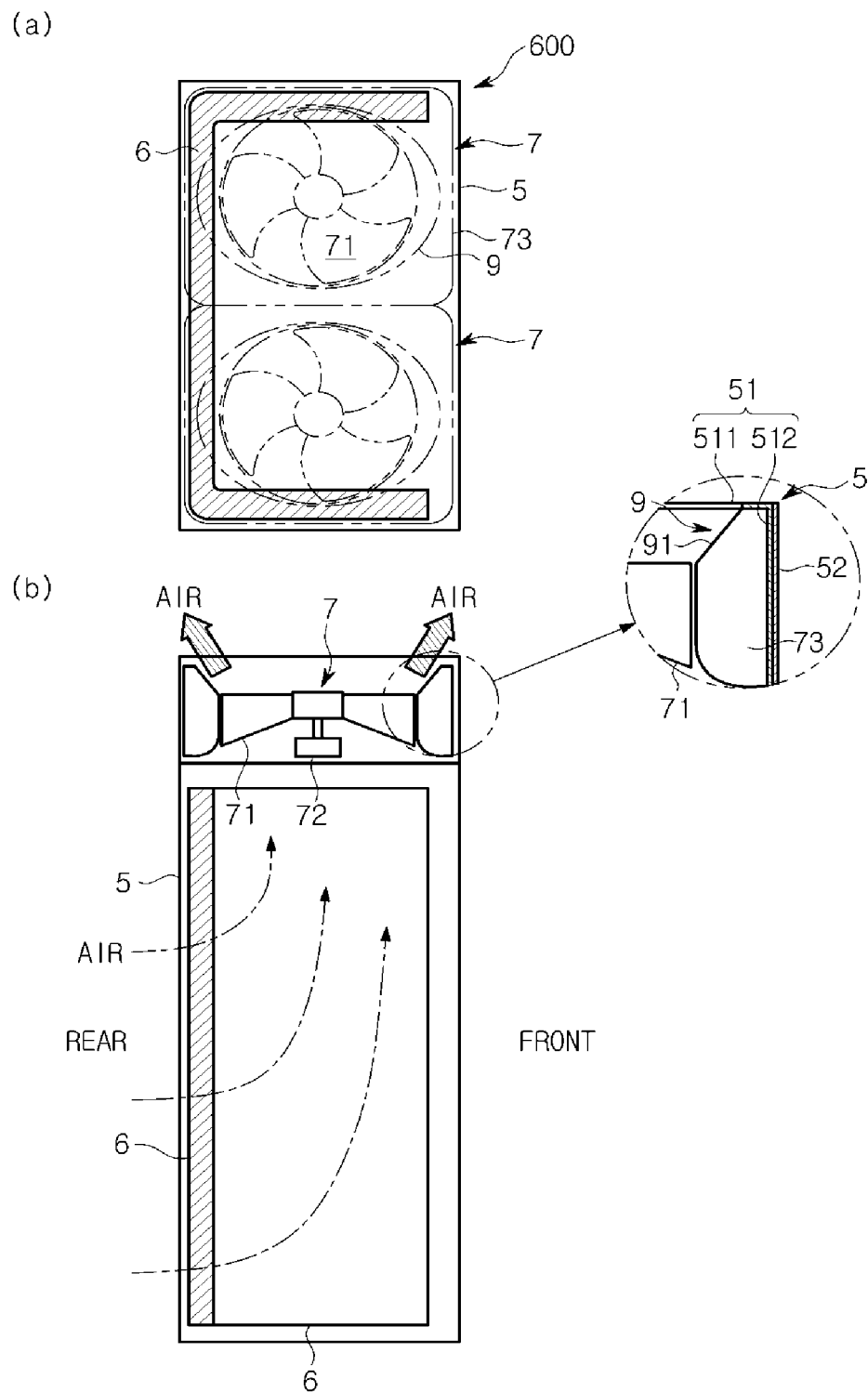


FIG. 3

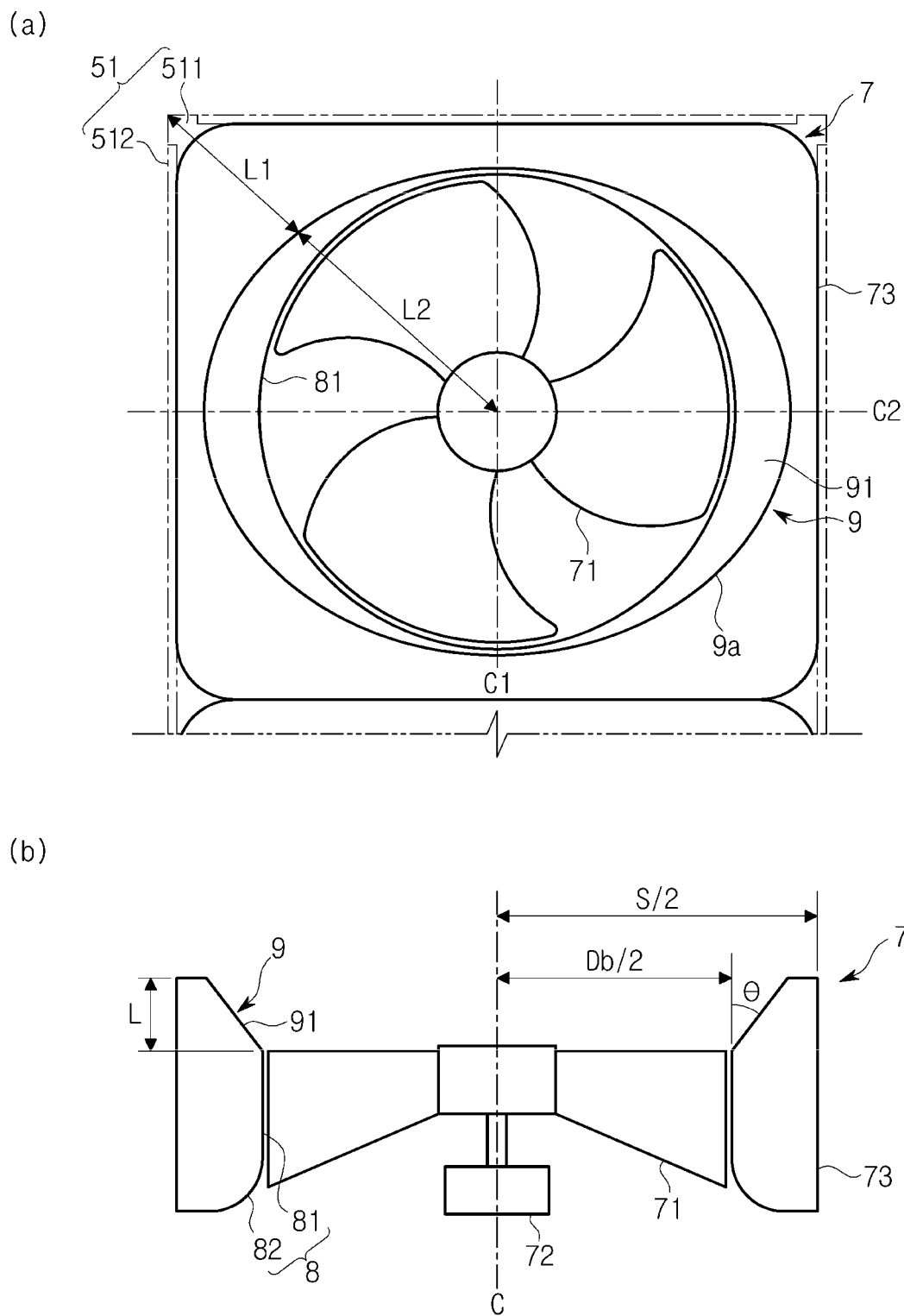


FIG. 4

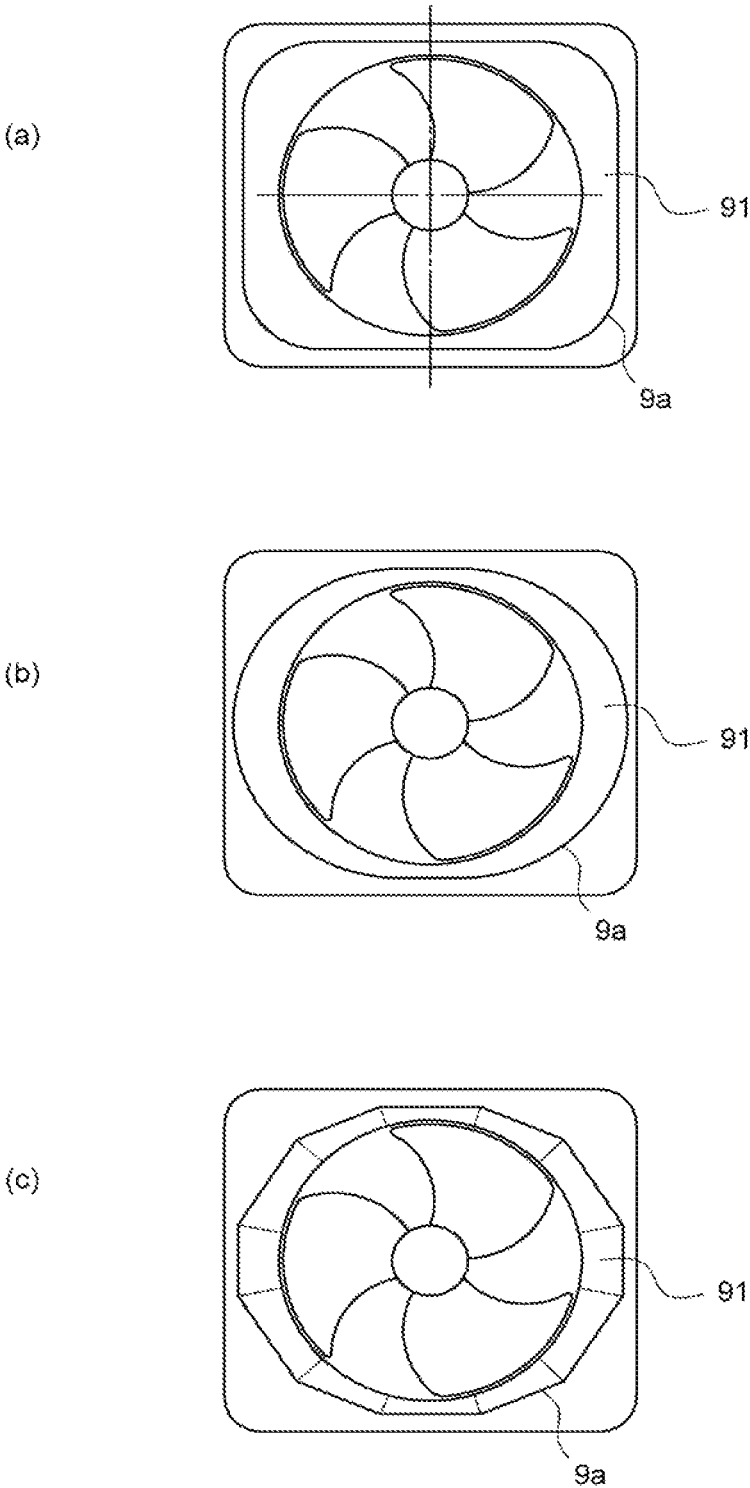


FIG.5

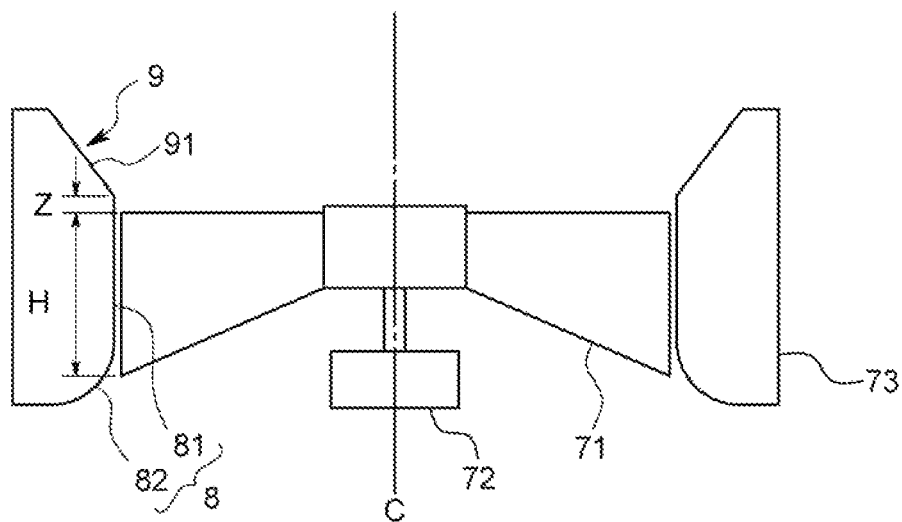


FIG.6

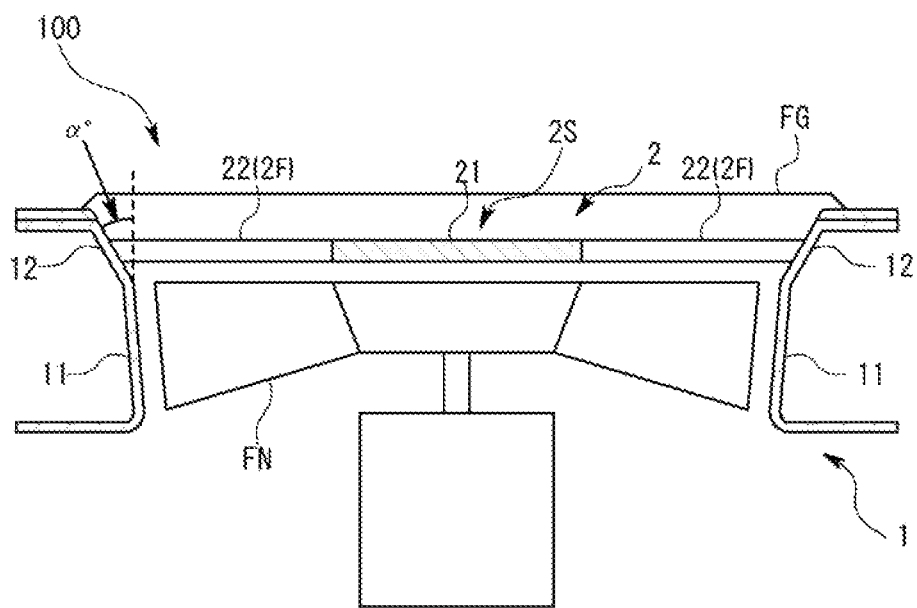
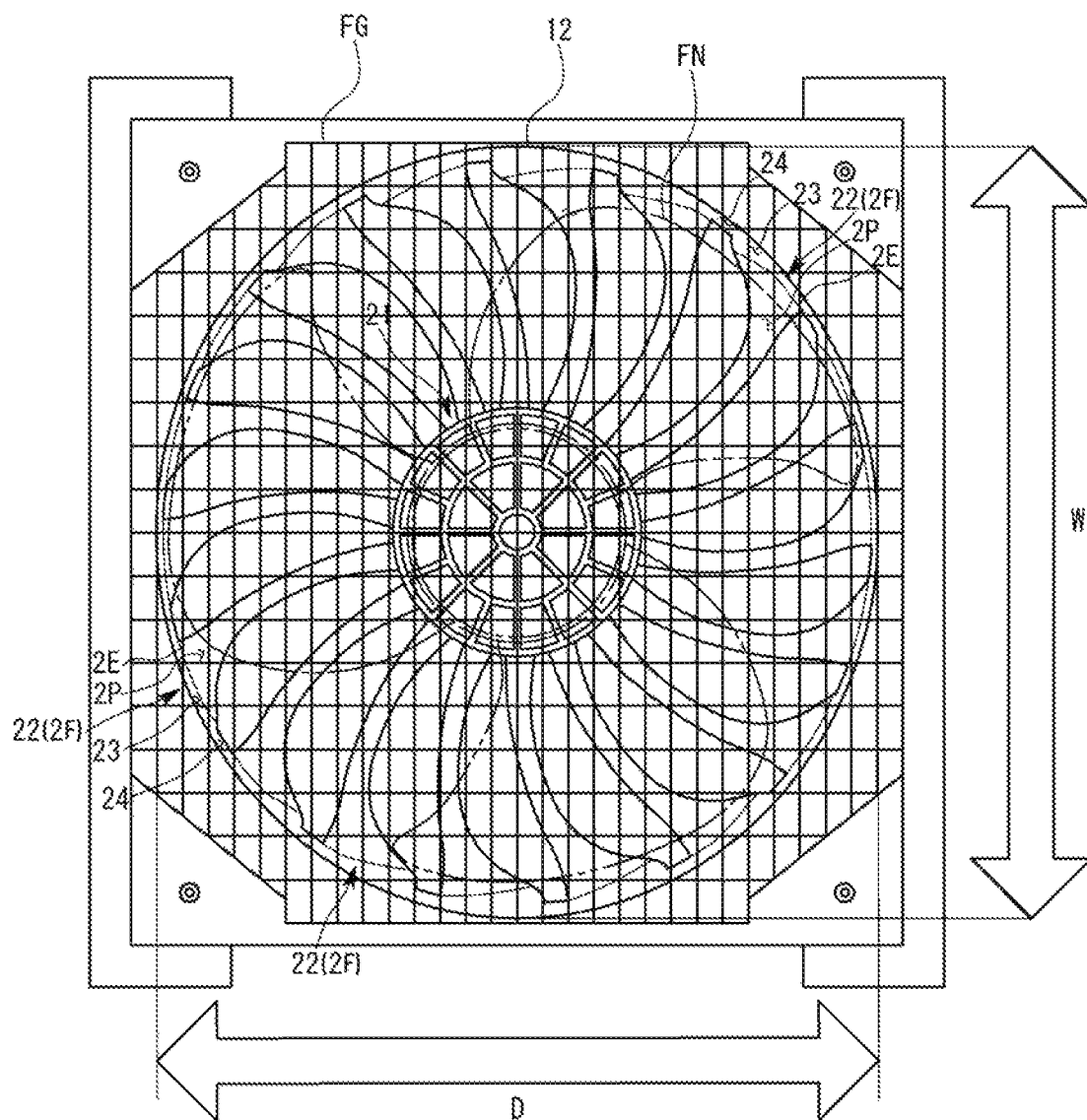


FIG. 7



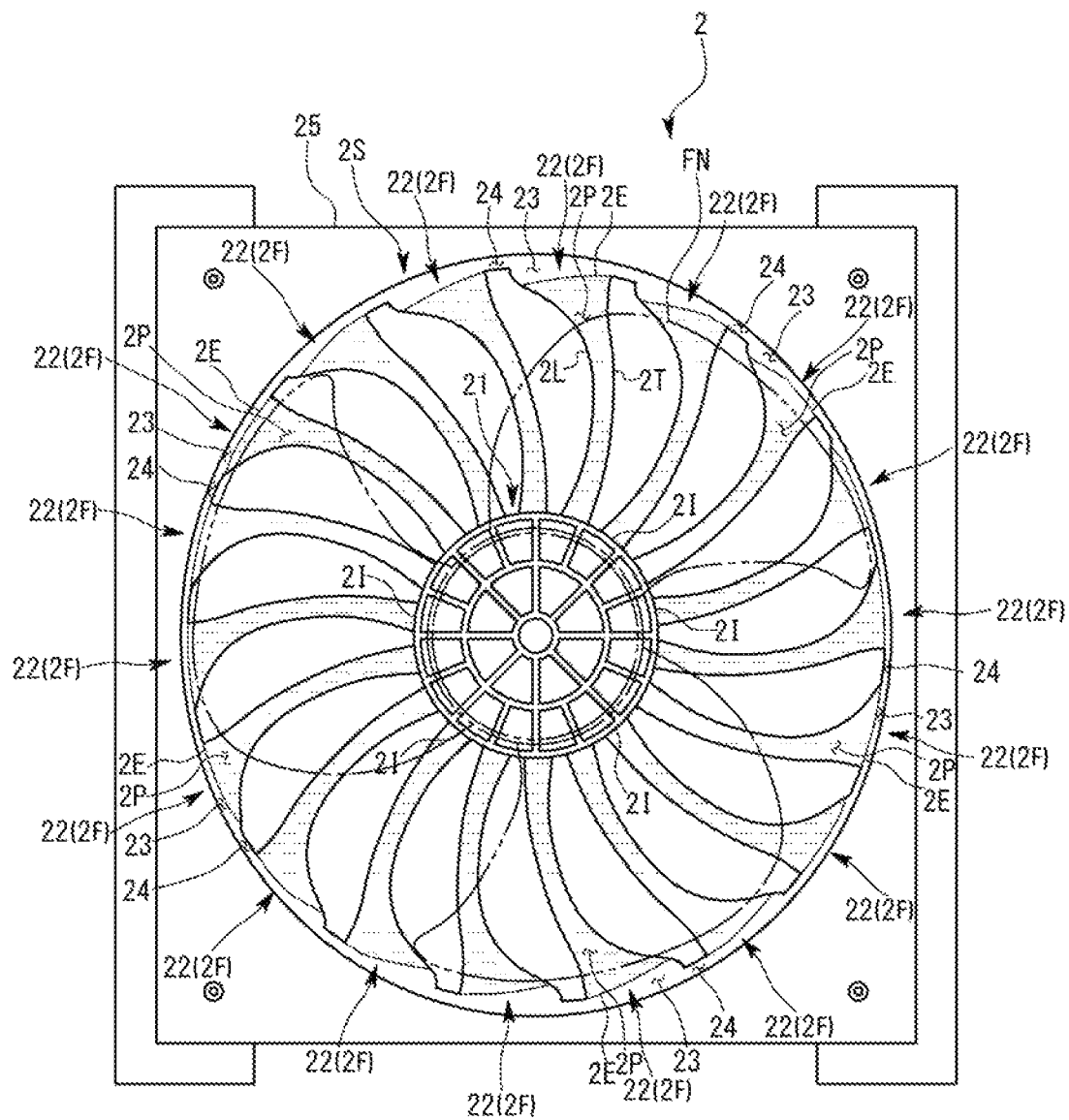


FIG. 9

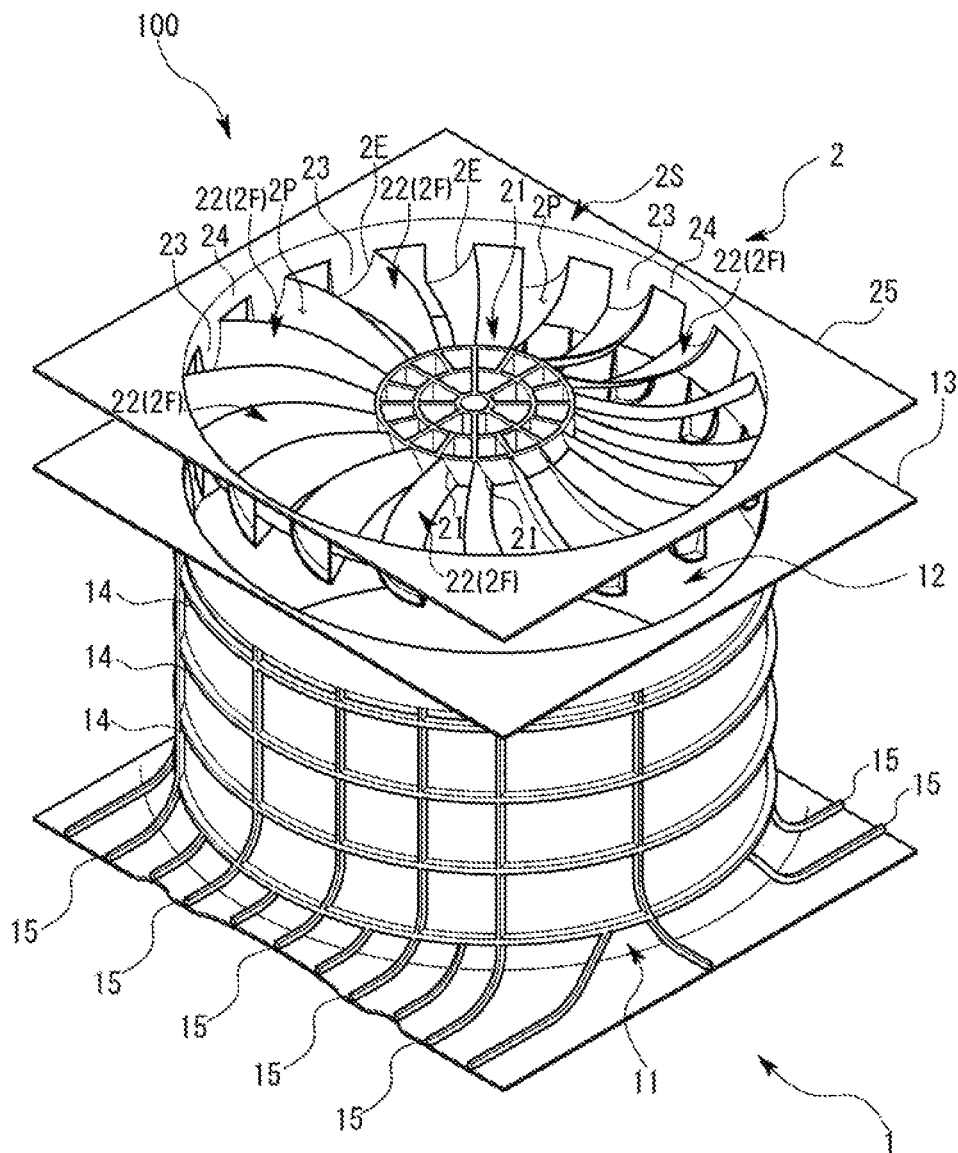


FIG.10

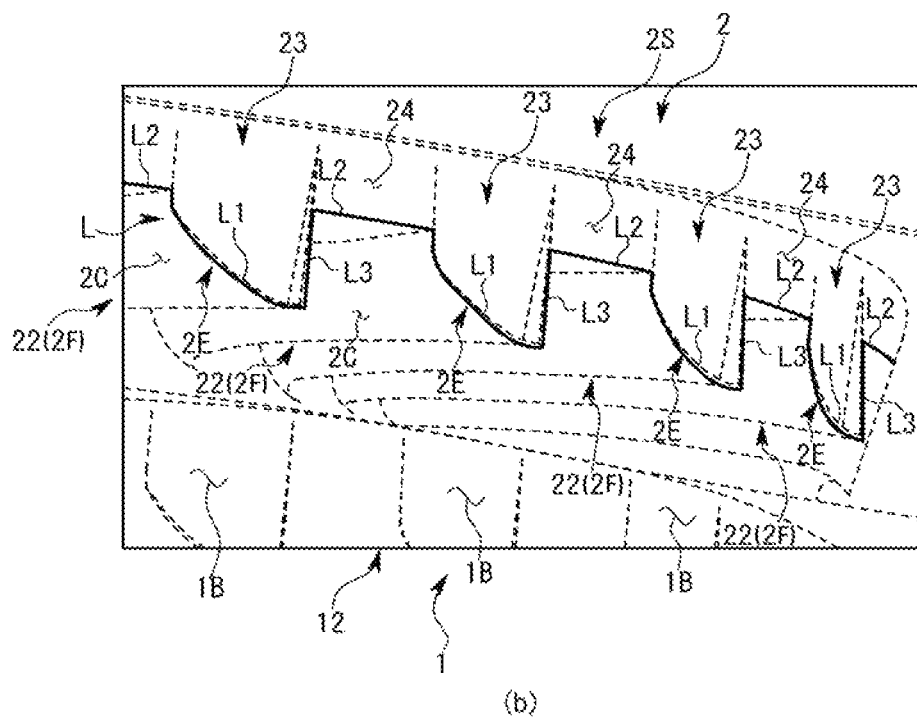
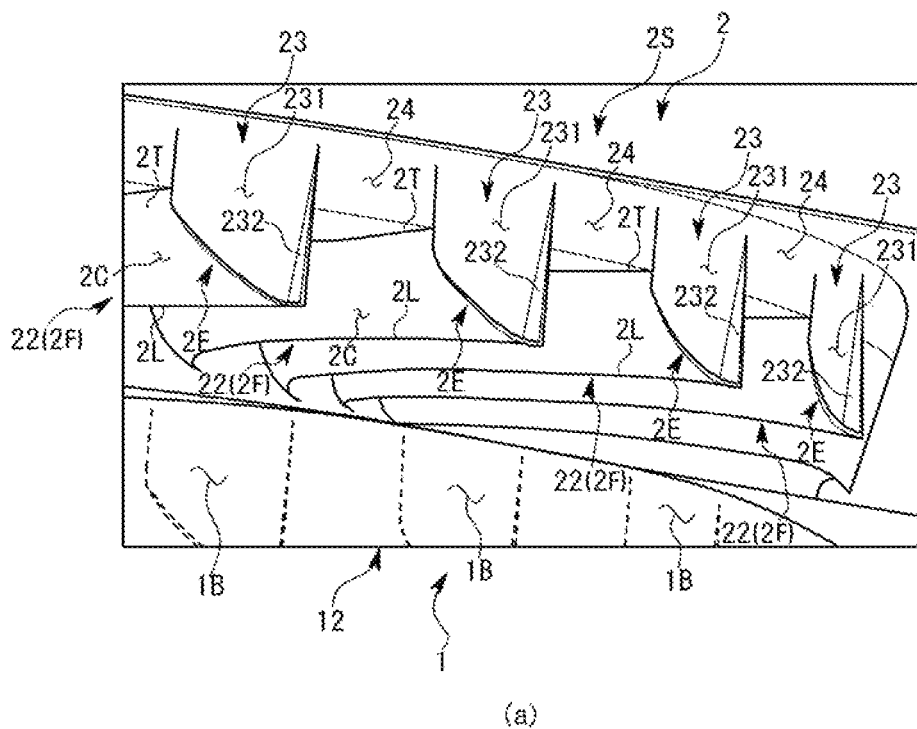


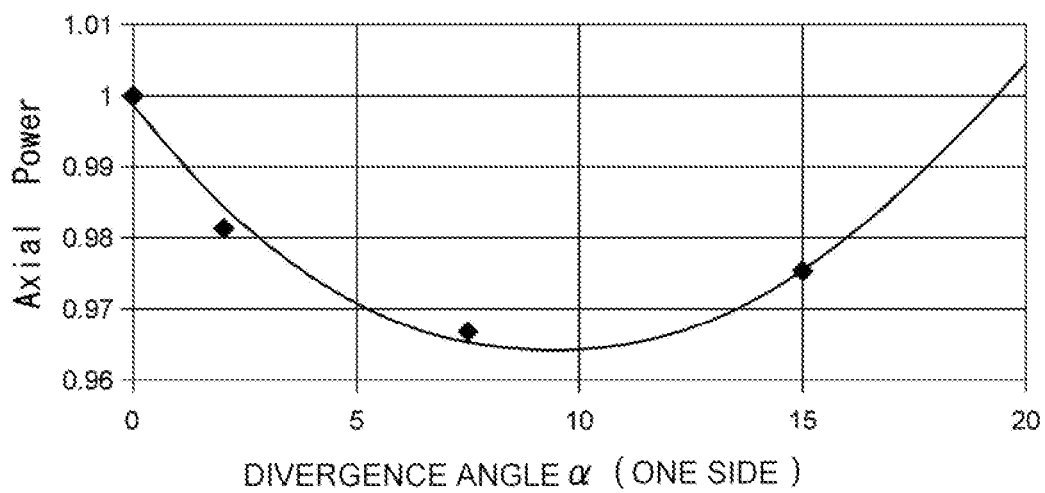
FIG.11

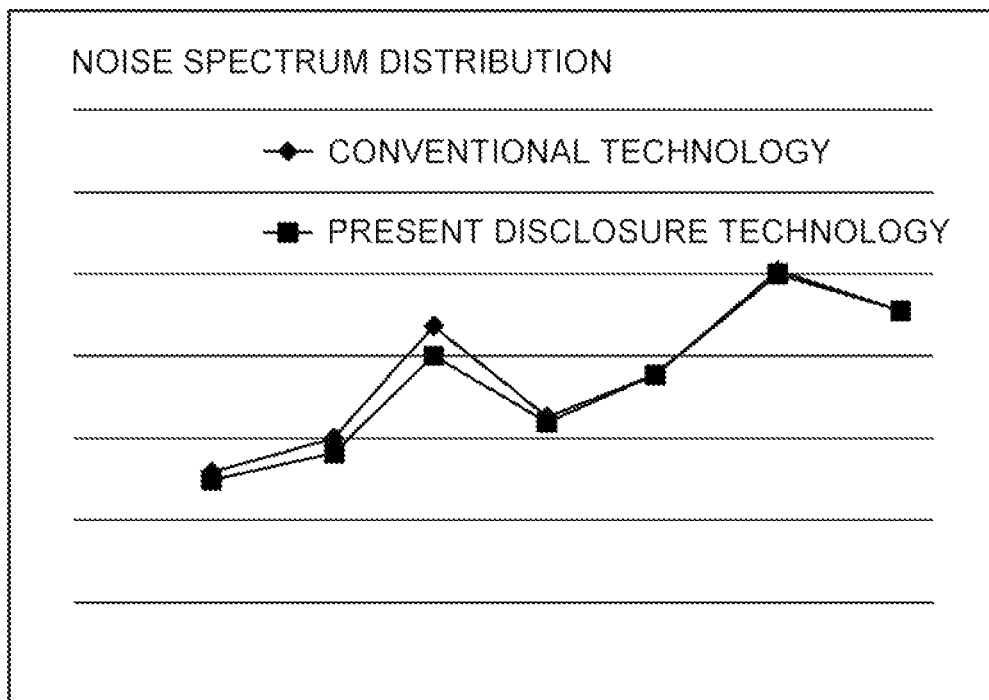
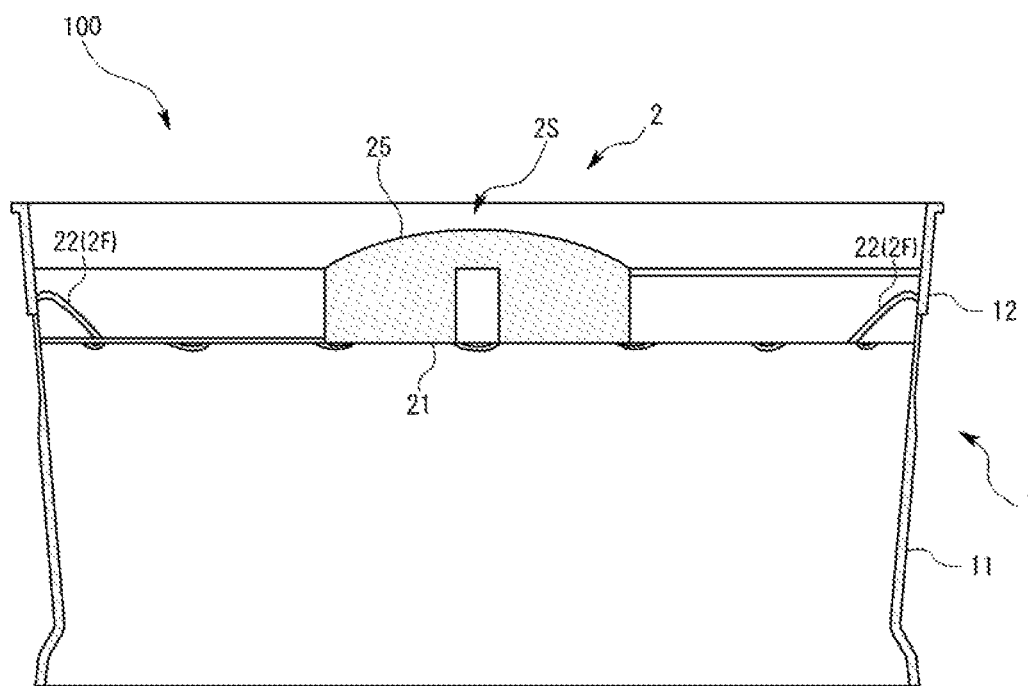
FIG.12

FIG.13



**BLOWER AND OUTDOOR UNIT OF AIR
CONDITIONER COMPRISING SAME****CROSS-REFERENCE TO RELATED
APPLICATIONS**

This application is a continuation of PCT international application PCT/KR2014/011715 filed on Dec. 2, 2014 and claims the benefit of Japanese Patent Application Nos. JP2013-249308, filed on Dec. 2, 2013, and JP2014-157177, filed on Jul. 31, 2014, and Korean Patent Application No. 10-2014-0170184, filed on Dec. 2, 2014, in the Japan Patent Office and the Korean Intellectual Property Office, respectively, the content of each of the foregoing is incorporated herein by reference.

BACKGROUND**1. Technical Field**

The present invention relates to an outdoor unit of an air conditioner and a blower used for the same.

2. Background Art

In a conventional blower, a diffuser part (a ventilation part) extends to a downstream from a cylindrical bell mouth part installed around a propeller fan, for example, as described in Japanese Unexamined Patent Application Publication No. 2013-119816.

However, an air current may not be uniformly introduced into inlet ports installed at an upstream side of the bell mouth part based on an apparatus in which the blower is installed, therefore a suction flow rate may be distributed according to region.

Because of this, blowing efficiency may not be improved more than a certain level, and there is also a problem in that when the number of revolutions of a propeller fan is increased for increasing the suction flow rate, power consumption is increased and noise is generated. Particularly, in a configuration of Patent document 1 in which a noise prevention blade (a stator blade) is installed in a diffuser part, noise generated in the noise prevention blade is also a problem.

Recently, high efficiency has been achieved by heat exchangers being installed in a plurality of parallel rows in an outdoor unit of an air conditioner, and accordingly a plurality of blowers are adjacently disposed to correspond to the heat exchangers. However, this arrangement has caused efficiency to deteriorate or noise to increase, such as air currents which flow from diffuser parts collide with each other and interfere with each other.

SUMMARY

The present invention is directed to providing a blower which significantly improves blowing efficiency and suppresses noise and an outdoor unit of an air conditioner using the same.

One aspect of the present disclosure provides a blower including a fan, a container-shaped molded object provided so that a bell mouth part provided to be spaced apart from an outer circumferential surface of the fan and a diffuser part provided to be extended from a downstream end of the bell mouth part are integrally molded, and a molded blade part including a plurality of noise prevention blades and provided at the diffuser part, wherein the diffuser part is provided to be inclined so that an area of a flow path increases toward a downstream end of the diffuser part, and an inclination angle of the diffuser part varies along a circumferential

direction of the diffuser part with respect to a rotation shaft of the fan. Another aspect of the present disclosure provides an outdoor unit of an air conditioner including a heat exchanger, the outdoor unit includes a fan having an outer circumferential end coupled to a rotation shaft; a bell mouth part including a downstream end, the bell mouth disposed to be around the outer circumferential end of the fan and spaced apart from the outer circumferential end of the fan; and a diffuser part including: an opening having an inner circumferential surface, an upstream end disposed at the downstream end of the bell mouth part, and a downstream end at which the air is discharged to outside of the outdoor unit, the diffuser part disposed to be extended from the downstream end of the bell mouth part to provide an air flow path of the fan through the opening, from the upstream end of the diffuser part toward the downstream end of the diffuser part. The inner circumferential surface of the diffuser part is inclined at a diffuser angle (Θ) with respect to an axis of a rotation of the rotation shaft so that a cross-sectional area of the air flow path increases toward the downstream end of the diffuser part, and the diffuser angle (Θ) with respect to the axis of the rotation of the rotation shaft of the fan varies along a circumferential direction of the inner circumferential surface of the diffuser part.

When an inclination angle between an inclination of the diffuser part and a rotation shaft of the fan is represented as a diffuser angle (Θ), a diffuser angle positioned at a side at which an air flow rate is great may be provided to be greater than a diffuser angle positioned at a side in which an air flow rate is small.

The plurality of noise prevention blades may be disposed to be spaced apart from each other in a radial shape around the rotation shaft of the fan, and outer circumferential ends of the plurality of noise prevention blades may be supported by an inside of the diffuser part.

The plurality of noise prevention blades may be formed to have an arc-shaped surface and provided to have convex surfaces facing the fan.

The molded blade part may be provided so that a boundary surface of a lower end of the molded blade part is provided along the convex surfaces of the plurality of noise prevention blades.

Another aspect of the present disclosure provides a blower including a fan, a diffuser part provided so that an area of a flow path is increased from a discharging surface through which the fan discharges air toward a downstream end, and a molded blade part including a hub provided in a cylindrical shape and having a hollow around a rotation shaft of the fan and a plurality of noise prevention blades provided to be extended from an outer circumferential surface of the hub toward an inclined surface of the diffuser part, wherein the plurality of noise prevention blades are disposed to be spaced apart from each other in a radial shape around the hub, and outer circumferential ends of the plurality of noise prevention blades are provided to be extended from the hub to the inclined surface of the diffuser part in an arc shape so that the outer circumferential ends of the plurality of noise prevention blades are supported by the inclined surface of the diffuser part.

An inclination angle of the diffuser part may vary along a circumferential direction of the diffuser part with respect to the rotation shaft of the fan, and a distance between an outer circumferential end of the hub and the inclined surface of the diffuser part may proportionally vary according to the varying inclination angle of the diffuser part.

That is, the blower according to an embodiment of the present disclosure is a blower provided with the bell mouth

part disposed at the outside of a propeller fan in a diameter direction and having a lateral cross-section in a circular shape, and the diffuser part installed in series at a downstream end of the bell mouth part, an inclined surface facing the outside in the diameter direction as at least a part of the inner circumferential surface of the diffuser part faces a downstream side, and simultaneously an opening of a downstream end of the diffuser part has a shape different from the circular shape.

Accordingly, since a flow path enlargement rate of the diffuser part varies according to positions by, for instance, setting the flow path enlargement rate according to a flow rate of each position of non-uniform air current having a suction flow rate deviation (a distribution) due to the position, loss of the diffuser part is may be suppressed, and a pressure restoring effect may be maximized.

As a result, blowing efficiency may be significantly increased and blowing noise may be decreased due to a flow speed decreasing effect which is an evidence of the pressure restoring effect.

An opening of a downstream end of the diffuser part, which is easy to manufacture and practical may have an oval shape (a capsule shape) or polygonal shape of which corners are rounded.

When an angle formed by the inclined surface and a rotation shaft line of the fan is represented as a diffuser angle and the diffuser angle is provided to generally vary in a circumferential direction, turbulence generation due to drastic increasing an area of a flow path of the diffuser part is suppressed as much as possible, a pressure restoring effect may be obtained, and thus efficiency improvement and a noise decrease effect may more obviously be obtained.

As a specific aspect which suppresses the turbulence generation, when the diffuser angle is represented as Θ , the diffuser angle may vary in the range of $3^\circ \leq \Theta \leq 35^\circ$.

To more obviously obtain the effect of the embodiment of the present disclosure, it is preferable that the diffuser angle of a portion at which an air flow rate which passes through the propeller fan is great be greater than that of a portion at which the air flow rate which passes through the propeller fan is small.

To obtain high efficiency and low noise while suppressing loss due to collision or interference of air currents discharged from the blowers at the blowers and other blowers disposed adjacent to the blowers, it is preferable that the diffuser angle Θ of a portion adjacent to the other blowers be set in the range of $3 \leq \Theta \leq 7^\circ$ when the diffuser angle is represented as Θ .

Meanwhile, when the bell mouth part is disposed to be spaced a predetermined distance from the outer circumferential end of the propeller fan, the diffuser part is installed at the downstream side of the bell mouth part, in which an area of a flow path is increased from an upstream side to a downstream side with an enlargement rate greater than an area enlargement rate of a flow path at the downstream end of the bell mouth part, and the stator part includes the plurality of noise prevention blades and disposed in the diffuser part, the diffuser part is formed at the downstream side of the bell mouth part, a tip clearance between the propeller fan and the bell mouth is kept to a necessary minimum, and the area enlargement rate of the flow path required for pressure restoring at the diffuser part may be obtained. Meanwhile, since the stator part is disposed in the diffuser part, the dynamic pressure of a vortex may be collected from the propeller fan compared with a conventional case. In addition, the blower according to an embodi-

ment of the present disclosure may further improve blowing efficiency due to a synergistic effect.

In addition, since the diffuser part has an enlarged magnified flow path shape and the stator part is installed therein, the vortex may be introduced into the stator part from the propeller fan in a state in which an average speed of the vortex is sufficiently lowered, and thus a noise level generated from the noise prevention blades may be lowered.

In addition, since there is no need for the diffuser part to consider a tip clearance for the propeller fan unlike the bell mouth part, and the diffuser part is installed at a downstream of the bell mouth part and the stator part is disposed in the diffuser part, blowing efficiency may be further improved due to a synergistic effect with the diffuser part and the stator part. In addition, in the above-described structure, the diffuser part has an oval shape as seen from a shaft, a direction or length of span of at least a part of the noise prevention blades of the stator part may be different, a noise level which is increased by noise generated from the noise prevention blades reaching a peak point and overlapping each other may be prevented, and thus an overall noise level may be decreased.

Further specifically, it is preferable that the downstream end of the diffuser part be formed in an oval shape as seen from the shaft, the plurality of noise prevention blades be disposed in a radial shape from the center as seen from the shaft, and an outer circumferential end be in contact with an inner circumferential surface of the diffuser part. Accordingly, the diffuser part may have a suitable shape for restoring pressure, and a length or shape along a span direction of the noise prevention members constituting the stator part may not be the same, and thus a noise peak of a blade passing frequency (BPF) may be suppressed.

To obtain a specific shape for suppressing fluid separation due to a reverse pressure gradient at the diffuser part and easily obtaining a static pressure raising effect due to the diffuser part, it is preferable that a divergence angle α which is an angle formed by an upstream end of the diffuser part with respect to a virtual line extending from the downstream end of the diffuser part toward the shaft as seen from the longitudinal cross-section be in the range of $3 \leq \alpha \leq 35^\circ$, however, when there is the noise prevention blade, the divergence angle α may be set to in the range of $0^\circ < \alpha < 18^\circ$. It may be more preferable that the divergence angle α be set to 9° . In addition, the diffuser angle Θ may be an angle of any portion of the diffuser part, the divergence angle α may be an angle of the upstream end of the diffuser part, and Θ and α may be the same.

To suppress a drastic change in a curvature at the inner circumferential surface of the diffuser part due to the divergence angles at a major axis and a minor axis of the diffuser part being greatly different, easily rectify a flow at the diffuser part, and improve a static pressure raising effect, it is preferable to be set such that $0.75 < D/W < 1$ when a length of the major axis of an oval shape of the downstream end of the diffuser part seen from the shaft is represented as W , and a length of the minor axis is represented as D .

To uniformly collect a dynamic pressure of a vortex from the propeller fan, and improve blowing efficiency, it is preferable that the central point of a circular or polygonal shape of the downstream end of the diffuser part or an intersection point of the major axis and the minor axis of an oval shape be exist on a rotation shaft line of the propeller fan as seen from the shaft.

To decrease a weight applied to the noise prevention blade and decrease necessary strength so that a thickness of the noise prevention blade is maintained and material cost is

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decreased, it is preferable that the stator part include the hub in a substantially hollow cylindrical shape in which the inner circumferential end of the noise prevention blade is connected to the outer circumferential surface and the hub include a reinforcement rib structure in a radial shape.

For example, to prevent breaking a rotational balance of the propeller fan due to snow being accumulated on a central portion of the propeller fan in the bell mouth part and being in contact with the inner circumferential surface of the bell mouth part to be destroyed, it is preferable that a cover member which is installed to cover the downstream side of the hub and has a cone-shaped surface or dome-shaped curved surface be further provided. Accordingly, since the cover member has the curved surface, snow is not accumulated on the hub, and the noise prevention blades of the stator part may also be prevented from being damaged due to a weight of snow.

It is preferable that the cover member be installed to be detachable from the hub in an area where it hardly snows so that a manufacturing cost is decreased by omitting the cover member.

To mold the diffuser part having a lateral cross-section of the downstream side in an oval shape, dispose the stator part in the diffuser part, and efficiently mold an even complex shape for improving blowing efficiency using resin injection molding, it is preferable to provide a container-shaped molded object in which the bell mouth part and the diffuser part are integrally molded and a molded blade part in which at least the stator part are molded.

According to the outdoor unit of the air conditioner using the blower according to an embodiment of the present disclosure, blowing efficiency may be significantly improved and fluid noise may also be reduced to be suitable to heat exchangers installed in a plurality of parallel rows.

As described above, a blower according to an embodiment of the present disclosure can significantly improve blowing efficiency as well as reduce blowing noise.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is front and plan schematic views illustrating an inside of a blower and an outdoor unit for an air conditioner according to a first embodiment of the present disclosure.

FIG. 2 is side and plan schematic views illustrating the inside of the blower and the outdoor unit for the air conditioner according to the first embodiment of the present disclosure.

FIG. 3 is plan and front schematic views illustrating the blower according to the first embodiment.

FIG. 4 is a schematic view illustrating a modified example of the blower according to the first embodiment.

FIG. 5 is a plan schematic view illustrating the modified example of the blower according to the first embodiment.

FIG. 6 is a schematic view illustrating a blower according to a second embodiment of the present disclosure.

FIG. 7 is a top schematic view illustrating the blower according to the second embodiment.

FIG. 8 is a top schematic view illustrating a state in which a fan guide according to the second embodiment is excluded.

FIG. 9 is an exploded schematic view illustrating the blower according to the second embodiment.

FIG. 10 is a schematic perspective view illustrating a vicinity of an outer circumferential end of a stator part according to the second embodiment.

FIG. 11 is a schematic graph which shows a relation between a divergence angle and a static pressure rising effect according to the second embodiment.

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FIG. 12 is a spectrum distribution of noise according to the second embodiment.

FIG. 13 is a schematic view illustrating a blower according to another embodiment of the present disclosure.

DETAILED DESCRIPTION OF EMBODIMENTS

One embodiment of the present disclosure will be described with reference to accompanying drawings.

<First Embodiment>

A blower 7 according to the present embodiment is a type of axial fan used for an outdoor unit 600 (hereinafter, simply referred to as the outdoor unit 600) for an air conditioner.

As illustrated in FIGS. 1 and 2, the outdoor unit 600 includes a casing 5 which is formed with a bottom plate (not shown) and side perimeter plates 52 and 51 in a substantially rectangular parallelepiped shape extending vertically, a plurality of heat exchangers 6 disposed at side and rear surfaces of the casing 5, and a plurality of (here, two) blowers 100 disposed adjacent to a top surface of the casing 5. In addition, the outdoor unit 600 has, so called, a vertical upright type in which air is introduced from a side surface of the casing 5 into an inside thereof by a vortex generated by the blower 100, comes into contact with the heat exchanger 6, and is discharged upward. In addition, the casing 5 accommodates various electric units (not shown) besides the heat exchanger 6.

Hereinafter, the blower 7 will be specifically described.

As illustrated in FIG. 3 and the like, the blower 7 includes a propeller fan 71, a motor 72 which drives and rotates the propeller fan 71, and a container-shaped molded object 73 which is disposed around the propeller fan 71 and has a container shape.

The container-shaped molded object 73 has an edge having a rectangular (including a square) outline as seen from an axis of rotation C of the propeller fan 71, and simultaneously is an integrally molded object formed by forming a through hole along a direction of the axis of rotation C, and a bell mouth part 8 and a diffuser part 9 are formed on an inner circumferential surface of the through hole. In addition, here, the container-shaped molded object 73 is disposed at an upper portion in the casing 5.

The bell mouth part 8 includes a bell mouth duct 81 which is installed having a tiny gap at a further outer side than an outer circumferential end of the propeller fan 71 in an inner circumferential surface of the container-shaped molded object 73 and has a substantially circular container-like shape, and an opening (a bell mouth) 82, which is installed to be connected to an upstream side of the bell mouth duct 81, and has a horn shape.

The diffuser part 9 is formed at the inner circumferential surface which continues from or extends from a downstream end of the bell mouth part 8 toward a side in which an upstream is generated in the inner circumferential surface of the container-shaped molded object 73, and, here, is an inclined surface 91 which is inclined toward the outside in a direction of a diameter such that a front surface of the inner circumferential surface faces a downstream side thereof.

In addition, when an angle formed between the inclined surface 91 and the axis of rotation C is defined as a diffuser angle θ , as the diffuser angle θ is provided to be smoothly changed in a circumference direction, the downstream end opening 9a in the diffuser part 9 has a shape different from a substantially circular shape, for instance, an oval shape, so that a width of the downstream end opening 9a through

which air flows from an outlet of the bell mouth duct **81** as seen from the axis of rotation C changes according to location.

Accordingly, the inclined surface **91** in which the width is minimized, that is, the diffuser angle Θ is minimized, is the inclined surface **91** positioned on a minor axis **C1** of the downstream end opening **9a** having an oval shape as seen from the axis of rotation C. Here, the diffuser angle Θ is set to 3°. In addition, a direction of the minor axis **C1** matches along a shorter side at an outer edge outline of the container-shaped molded object **73** which has a rectangular shape, and simultaneously a plurality of (two) blowers **7** are installed along the minor axis **C1** direction, in other words, longer side surfaces of the container-shaped molded objects **73** are adjacently disposed with each other.

Meanwhile, an inclined surface in which the diffuser angle Θ is maximized, is the inclined surface **91** positioned on a major axis **C2** of the downstream end opening **9a** as seen from the axis of rotation C. Here the diffuser angle Θ is set to 35°.

In addition, an inner diameter value of a downstream end of the bell mouth duct **81** is defined as D_b , a height value of the diffuser part **9** along the direction of the axis of rotation C is defined as L, an edge value of the container-shaped molded object (a width or a length as seen from the axis of rotation) is defined as S, and D_b , L, and S are set to satisfy the following equation (1).

$$S/2 \leq C(L \tan(\Theta) + D_b/2) \quad (1)$$

Here, C is a coefficient in the range of $1.03 \leq C \leq 1.5$, and more preferably in the range of $1.06 \leq C \leq 1.12$.

According to equation (1), the strength of the container-shaped molded object **73** is secured, an installation space may be maximally used, influence of an adjacent blower **7** is significantly reduced, noise due to maximizing a diameter of the propeller fan may be reduced, etc.

Meanwhile, as illustrated in FIG. 3 which is an enlarged view of FIGS. 1 and 2, a top plate **51** (Hereinafter, referred to as a top panel **51**) of the casing **5** is disposed at a top surface (a cross-section of a side of the diffuser part) of the container-shaped molded object **73** to be in contact therewith. The top panel **51** is a metal plate member provided with a surface plate part **511** having an opening approximately matching an outlet opening of the diffuser part **9** and a bent part **512** bent downward from an edge of the surface plate part **511**, and the bent part **512** is screwed to a side perimeter plate **52** of the casing **5**.

In addition, as illustrated in FIG. 3, in the present embodiment, a virtual line is drawn from the center of rotation of the propeller fan **71** to a corner of the top panel **51** as seen from the axis of rotation C, when the length of the virtual line (that is, a distance from the center of rotation of the propeller fan **71** to the corner of the top panel **51**) is defined as $L_1 + L_2$, and a distance from the center of the propeller fan **71** to an outer edge of the outlet of the diffuser part **9** on the virtual line is defined as L_2 , and also when $D_{ratio} = L_2 / (L_1 + L_2)$, equation (2) below is satisfied.

$$0.60 \leq D_{ratio} \leq 0.95 \quad (2)$$

Hereinafter, an operation and an effect of the outdoor unit **600** configured as described above will be described.

As illustrated in FIGS. 1 and 2, although the heat exchanger **6** is not disposed in the front of the casing **5**, the heat exchanger **6** is disposed at a side of the casing **5**, and thus more air is suctioned when the blower **7** is operated. In addition, since electric elements and the like disposed inside the casing **5** also have air resistance, in the present embodi-

ment, a larger amount of air is introduced through an inlet (the bell mouth **82**) of the blower **7** from front and rear portions of the bell mouth **82** where the number of elements which can serve as air resistance are few. As a result, in the diffuser part **9**, an air flow rate is maximized in the front and rear portions and the air flow rate is minimized in both side portions.

As described above, since a diffuser angle Θ at the front and rear portions of the diffuser part **9** is set to as large a value as possible in the range in which a turbulent current does not occur (here, a maximum of 35°) even though an air flow rate increases in the front and rear portions of the diffuser part **9**, a viscosity loss due to the turbulent current is suppressed and thus a pressure restoring effect at this portion may be maximized.

In addition, when the diffuser angles Θ at the front and rear portions are the same while the air flow rate at both side portions of the diffuser part **9** is decreased, because the diffuser angle Θ enlarges such that the air flow becomes unstable and a loss occurs.

In contrast, according to the present embodiment, since the diffuser angle Θ at this portion is set to a small value (a minimum of 3°), the above-described unstable air flow may be suppressed and a pressure restoring effect due to the diffuser part **9** at this portion may also be maximized.

That is, in the diffuser part **9** according to the present embodiment, since a loss due to an unstable air current such as a dispersion of the suction flow rate is suppressed as much as possible, a pressure restoring effect is maximized, and a blowing efficiency may be dramatically increased.

In addition, since the maximizing of the pressure restoring effect denotes that a flow rate in the diffuser part **9** is decreased, a blowing noise reduction may also be obtained.

In addition, in the present embodiment, since the blowers **7** are installed in series and the diffuser angles Θ at adjacent portions are set to be small values, an angle of an air current discharged therefrom becomes approximately vertical. Interference of the air currents exhausted from both of the blower **7** may be suppressed, and thus low noise blowing at high efficiency may be possible.

Because the above-described D_{ratio} is set to 0.9 or less, a bending process of the top panel **51** is certainly possible at a position at which the outlet opening of the diffuser part **9** is closest to an edge of a top panel surface plate part **511**, and thus the bent part **512** may be formed. Meanwhile, since D_{ratio} is set to 0.6 or more, an equalization of a change ratio of the outlet opening of the diffuser part outlet (a change ratio of the diffuser angle Θ along a circumferential direction) of the diffuser part defined by D_{ratio} , an equalization of a flow change by reducing the change and improvement of noise performance may be obtained. In addition, a configuration related to this may also be applied to the top panel **51** having a rectangular shape as seen from the axis of rotation C.

Next, a modified example of the first embodiment will be described.

First, it is preferable that a diffuser angle be changed and an additional shape different from a circle be formed according to a shape of a downstream end opening of the diffuser part or, for example, a distribution of a suction flow rate. Since the distribution of the suction flow rate depends on at least an arrangement of internal apparatuses, it is preferable that, for example, a diffuser angle of the inclined surface positioned at a position at which the bell mouth parts are not vertically overlapped be set to be greater than the diffuser angle of the inclined surface positioned at a portion at which the internal apparatuses and the bell mouth part are verti-

cally overlapped. Specifically, as illustrated in FIG. 4, a downstream end opening 9a of the diffuser part may have a shape such as a rectangular shape with rounded corners (see FIG. 4A), an oval shape (see FIG. 4B) or the like. In addition, for instance, when the downstream end opening 9a has the rectangular shape with rounded corners, a case in which the diffuser angle Θ is maximized at the corners may occur. As described above, the air flow rate does not need to be a maximum at a position at which the diffuser angle Θ is the maximum.

In the embodiment, although the diffuser angle Θ smoothly and continuously varies along the circumferential direction so as to suppress an occurrence of turbulence and the like as much as possible, the diffuser angle Θ may also vary discontinuously. In this case, as illustrated in FIG. 4C, the downstream end opening 9a has a shape with angles at discontinuous positions.

Although, the diffuser angle Θ is set to 35° as a maximum and 3° as a minimum in the embodiment, it is not limited thereto. For example, the maximum value may also be less than 35° , and the minimum value may also be more than 3° . Particularly, the diffuser angles Θ of a side of an adjacent blower is preferably in the range of $3^\circ \leq \Theta \leq 7^\circ$.

The diffuser angles Θ may be formed to be smoothly changed step-by-step or continuously toward a downstream side as seen from a cross-section parallel to an axis of rotation. In this case, an enlargement rate of the flow path of the diffuser part increases toward the downstream side.

In the embodiment, although a height of the downstream end of the propeller fan 71 and a height of an upstream end of the diffuser part 9 are matched when seen from a direction perpendicular to the axis of rotation C as illustrated in FIG. 3, this may also be changed. Specifically, as illustrated in FIG. 5, when H denotes a value of an outer circumferential end of the propeller fan 71 along a shaft, and Z denotes a distance between the upstream end of the diffuser part 9 and the downstream end of the propeller fan 71 along the shaft, it is preferable that Z be in the range of $H \pm 20\%$. When set as described above, since a vortex discharged from the propeller fan smoothly decreases in speed and spreads along the inclined surface 91 of the diffuser part 9, a larger pressure restoring effect may be obtained.

A shape of the bell mouth duct is not limited to a cylindrical shape, and when the outer circumferential end of the propeller fan does not have a vertical shape, for example, the shape may be a partial cone shape corresponding thereto, or a noise prevention blade may be installed at the diffuser part. Such an example will be described in detail in a second embodiment.

The blower may not be limited to the outdoor unit, and may be used for various uses. For example, the blower may also be used for a blower having a ventilation fan or a blower connected to a duct for ventilation.

In addition, the blower is not limited to air and may obtain the same effect by being applied to a gas.

<Second Embodiment>

Next, a second embodiment of the present disclosure will be described.

A blower 100 according to the present embodiment is formed by a resin injection mold, as illustrated in FIGS. 6 and 9, and includes a container-shaped molded object 1 formed in a substantially cylindrical shape and a molded blade part 2 in which a stator part 2F provided with a plurality of noise prevention blades 22 having a substantially flat rectangular parallelepiped shape is formed at a central circular portion. As illustrated in FIG. 6, the molded blade part 2 is assembled in the container-shaped molded object 1,

and then the stator part 2F may be disposed at a predetermined position in the container-shaped molded object 1. In addition, a fan guide FG is installed at a downstream side of the molded blade part 2 to cover the stator part 2F.

As illustrated in FIGS. 6 and 9, the container-shaped molded object 1 is integrally formed with a bell mouth part 11 which is disposed to be spaced a predetermined distance from an outer circumferential end of the propeller fan FN in a radius direction, and a diffuser part 12 which is installed at a downstream side of the bell mouth part 11 and wherein a flow path extends from an upstream side toward a downstream side.

As illustrated in FIG. 6, the bell mouth part 11 has portions having a circular lateral cross-section, and includes a bell mouth provided to have an open upstream side in a cone shape, and a bell mouth duct installed so that its diameter is increased from a portion facing an uppermost stream portion of the propeller fan FN. In addition, an inner circumferential surface of the bell mouth part 11 and an outer circumferential end of the propeller fan FN maintain constant tip clearance when seen from any radius directions.

As illustrated in FIG. 6, the diffuser part 12 is formed so that an upstream end connected to the bell mouth part 11 is formed to have a substantially circular lateral cross-section, and as illustrated in FIGS. 7 and 8, is formed so that an opening end of a downstream side has an oval lateral cross-section. The diffuser part 12 is also formed to have a lateral cross-section between an upstream end and a downstream end, in which a lateral cross-sectional area increases from an upstream side toward a downstream side, and simultaneously, the upstream end and the downstream end are smoothly and continuously connected. In addition, in the container-shaped molded object 1, when seen from a shaft direction from the upstream side to the downstream side, an area enlargement rate of a flow path at an upstream side end of the diffuser part 12 is greater than that of a lower downstream side end of the bell mouth part 11, and as illustrated in FIG. 6, the diffuser part 12 is connected to the bell mouth part 11 in a bent state.

As illustrated in FIG. 7, a length of a downstream end of the diffuser part 12 along a major axis direction is defined as W and a length along a minor axis direction is defined as D, each length is set to satisfy $0.75 < D/W < 1$ in the present embodiment. According to the above-described setting, a large change in a curvature of an inner circumferential surface of the diffuser part 12 due to a difference between a divergence angle α of a major axis side of the diffuser part 12 and that of a divergence angle α of a minor axis side of the diffuser part 12 does not occur, and thus it is easy to rectify a fluid flow.

In addition, an intersection point of the major and minor axes of the diffuser part 12 and center of the stator part 2F is disposed on an axis of rotation of the propeller fan FN.

In addition, as illustrated in FIGS. 9 and 10, a downstream side end of the diffuser part 12 is formed to be in contact with an outer circumferential end 2E of the stator part 2F when the molded blade part 2 is assembled at the container-shaped molded object 1, and the stator part 2F is disposed and fixed to a flow path in the diffuser part 12 after assembly. In addition, a large seating part 13, which has a flat plate shape widened in a flat surface perpendicular to a shaft, is formed at the downstream end of the diffuser part 12, and the downstream end of the diffuser part 12 is provided to be in contact with an installation flat plate part 25 which is formed at the molded blade part 2 and which will be described later.

As illustrated in FIGS. 9 and 10, the above-described structure is formed so that a plurality of concave parts 1B

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having a shape substantially the same as that of each connection part **23** of the stator part **2F**, which will be described later, are formed to be parallel to each other along a circumferential direction. The concave part **1B** causes an internal surface of the diffuser part **12** to be concave along a radius direction, and at the same time, a bottom surface thereof to be parallel to the shaft direction. Accordingly, a depth of the concave part **1B** becomes deeper from a downstream side to an upstream side.

Here, in the bell mouth part **11** and the diffuser part **12**, when a radius increase rate at a position from the upstream side to the downstream side along the shaft direction (a major axis radius and a minor axis radius) is compared, the radial increase rate of the diffuser part **12** is set to be bigger. That is, when seen in a longitudinal cross-section in FIG. 6, a surface forming the upstream side end of the diffuser part **12** is inclined with respect to a surface forming a downstream side end of the bell mouth part **11** to form a predetermined angle. In other words, as illustrated in FIG. 6, when seen in the longitudinal cross-section, a divergence angle α at a corner formed by the inner circumferential surface of the diffuser part **12** with respect to a virtual line extending from a downstream end of the bell mouth part **11** in the shaft direction is set to be in the range of $0^\circ < \alpha < 18^\circ$, which is slightly different from that of the first embodiment. As illustrated in a simulation result in FIG. 11, as the divergence angle α is set to the above-described angle, fluid separation due to a reverse pressure gradient is suppressed at an inner peripheral surface of the diffuser part **12**, and thus a static pressure rising effect may be easily obtained. It is also preferable that the angle α be in the range of $3^\circ \leq \alpha \leq 35^\circ$.

In addition, from the viewpoint of functions of the bell mouth part **11** and the diffuser part **12**, the bell mouth part **11** is for improving a fluid pressure near the propeller fan FN, and the diffuser part **12** is for increasing a pressure of a vortex from the propeller fan FN.

As illustrated in an outer peripheral surface of the container-shaped molded object **1** in FIG. 9, vertical ribs **15** extending along the shaft direction and lateral ribs **14** extending in the circumferential direction are formed to increase strength of the container-shaped molded object. A protrusion direction of the vertical rib **15** does not face a radius direction with respect to the shaft, and the protrusion direction is the same for each half thereof. That is, the container-shaped molded object **1** is provided to be molded by a mold that is divided in two as a front and a rear in a radius direction thereof, and thus the vertical rib **15** is formed in a dividing direction of the mold for each half thereof.

Next, the molded blade part **2** will be described.

As illustrated in FIGS. 7 and 9, the molded blade part **2** includes a hub **21** formed at a central portion in a substantially flat cylindrical shape, a plurality of noise prevention blades **22** disposed at an outer peripheral surface of the hub **21** in an outer radial shape, the connection parts **23** extending from the outer circumferential end **2E** of the noise prevention blade **22** to a downstream side in the shaft direction, link parts **24** which connect the connection parts **23** along the circumferential direction, and the installation flat plate part **25** in contact with the large seating part **13** having a flat plate shape. In addition, in FIG. 8, the noise prevention blade **22** is hatched to be seen easily even though it is not a cross-section.

As illustrated in FIGS. 8 and 9, the hub **21** includes three coaxial ring-shaped members each having a different diameter and a reinforcement rib structure which connects ring state members along a radial direction. That is, the hub **21**

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is formed in a hollow through which a fluid can pass, as well as formed to be capable of maintaining a predetermined strength. In addition, since the hub **21** is formed in the hollow, loads on inner circumferential ends of the plurality of noise prevention blades **22** is decreased, strength needed by the noise prevention blade **22** is decreased, and thus the thickness thereof may be formed as thinly as possible.

As illustrated in FIG. 8, the plurality of noise prevention blades **22** include the stator part **2F**, an inner circumferential end **21** of the noise prevention blade **22** is connected to the outer peripheral surface of the hub **21**, and the outer circumferential end **2E** is formed to be in contact with an inner surface of the diffuser part **12**. However, because the diffuser part **12**, except for a connection part with the bell mouth part **11**, is formed to have a lateral cross-section in an oval shape, shapes of the noise prevention blades **22** and lengths of strings of noise prevention blades are different from each other in a quarter of the oval. Accordingly, the connection part **23** also has a shape corresponding to a shape of the noise prevention blade **22**.

As described above, since a length in a span direction or a shape of the noise prevention blade **22** is repeatedly changed every quarter when the noise prevention blades **22** are seen in turn from the circumferential direction in the stator part **2F**, noise may be prevented from being generated in the noise prevention blade **22** with the same specific frequency. That is, by alternating frequencies having the highest peak in the noise prevention blades **22**, a Blade Passage Frequency (BPF) noise level may be decreased. More specifically, as illustrated in a graph in FIG. 12, a blower **100** according to the present embodiment may decrease a noise level at each frequency, particularly low frequencies, when compared with a conventional technology.

In addition, as illustrated in FIG. 9, the noise prevention blade **22** is installed so that a convex surface **2C** thereof faces an upstream side where the bell mouth part **11** and a fan motor exist, as well as a concave pressure surface **2P** faces a downstream side where the downstream end of the diffuser part **12** exists. In addition, as illustrated in the top view of FIG. 8, predetermined gaps are defined between the adjacent noise prevention blades **22** so that leading edges **2L** and following edges **2T** do not overlap each other when seen from the shaft.

As illustrated in an enlarged perspective view of FIG. 10A, the connection part **23** includes a plate-shaped part **231** extending from an outer end of the noise prevention blade **22** toward the shaft, and an outer edge rib **232** protruding from an outer edge of the plate-shaped part **231** in the radius direction. The plate-shaped part **231** has an inner circumferential surface having a shape so that the inner circumferential surface of the plate-shaped part **231** matches an inner surface of the diffuser part **12** when the connection part **23** is engaged with the concave part **1B**. In addition, the outer edge rib **232** is formed to have a height which increases from a downstream side to an upstream side.

As illustrated in FIG. 10A, the link part **24** has a partial ring state extending along a circumferential direction, and is formed to connect upstream side ends of the connection parts **23**. That is, the upstream side end of the connection part **23** and the link part **24** are alternatively disposed along the circumferential direction and formed in a ring state as a whole.

Next, division lines L between the container-shaped molded object **1** and the molded blade part **2** of the blower **100** provided as described above will be described.

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As illustrated with bold lines in FIG. 10A, each division line L of elements is formed to include at least a convex surface forming line L1 forming a convex surface 2C at the outer circumferential end 2E of the noise prevention blade 22. In the present embodiment, the division line L is defined by the convex surface forming line L1, a circumferential direction line L2 which defines a downstream end of the link part 24, and a shaft direction line L3 which is a downstream side of the outer edge rib 232 of the connection part 23 and extends from the convex surface forming line L1 to the circumferential direction line L2 along the shaft direction. In another words, as illustrated in FIG. 10B, the division line L between the container-shaped molded object 1 and the molded blade part 2 is formed in approximately a saw-toothed shape, and includes the convex surface forming line L1 forming the convex surface 2C at the outer circumferential end 2E of the noise prevention blade 22.

As described above, since the blower 100 according to the present embodiment has a complex structure in which the diffuser part 12 is formed at the downstream side of the bell mouth part 11 and the stator part 2F in which the shape of the noise prevention blade 22 is formed at an inner surface of the bell mouth part 11 is disposed in the diffuser part, a restoring pressure of fluid increases compared to a conventional technology, and thus the blowing efficiency may be significantly improved.

In addition, because the diffuser part 12 is installed at the downstream side of the bell mouth part 11, the downstream end of the diffuser part 12 is formed in the oval shape, and the noise prevention blade 22 is installed in the radial shape therein, first, speed of fluid which flows from the downstream end of the diffuser part 12 is decreased, and thus an entire noise level may be decreased. In addition, because lengths along the span direction or the shapes of the noise prevention blades are not the same and have a tiny difference between them and the vortex coming out from the propeller fan FN and the interference state of the noise prevention blade 22 are different from each other, noise intensively generated at a specific frequency may also be prevented. From that, blowing performance may be significantly improved and a noise level may also be decreased.

In addition, since the container-shaped molded object 1 is divided by the division line L, and the blower 100 includes the molded blade part 2, the noise prevention blades 22 of the diffuser part 12 and the stator part 2F are formed separately. Accordingly, the diffuser part 12 which has the complex shape for improving the blowing efficiency described above, has an enlarged flow path varying from the circular shape to the oval shape and a form in which the noise prevention blade 22 of the stator part 2F is formed up to the outer circumferential end 2E, and thus priority is given to such a complex structure while preventing manufacturability from being decreased.

More specifically, for example, when the outer circumferential end 2E of the noise prevention blade 22 is integrally injection-molded with the other members, only the outer circumferential end 2E is perpendicularly molded with respect to the shaft to be easily separated from the mold, and thus priority has been given to the manufacturability while blowing efficiency is sacrificed. In contrast to the above description, in the present embodiment, since each element is divided by the division line L, consideration of mold separation in the conventional technology may not be needed, and blowing efficiency may be improved by installing the convex surface 2C and the pressure surface 2P formed to be inclined toward the outer circumferential end 2E. In addition, since as illustrated in a top view illustrating

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the blower 100 in FIG. 9, the noise prevention blades 22 do not overlap when seen from the shaft, and as illustrated in FIG. 10A, the outer edge rib 232 is only formed at the outer edge part of the connection part 23, and because the upstream side is formed to be open, the molded blade part 2 may be easily molded by a mold divided along the shaft direction.

As described above, because molding property of the noise prevention blade 22 for the container-shaped molded object 1 is not needed, the shape of the bell mouth part 11 which expands from the substantially circular shape to the oval shape may also be molded by a simple mold. In addition, since a direction of the vertical rib 15 may be arranged by a half surface, the container-shaped molded object 1 may be molded by a mold divided into two along a radius direction, and thus manufacturability may be improved.

In addition, since the bell mouth part 11 and the diffuser part 12 are not separately formed, but are integrally formed as the container-shaped molded object 1, the blower 100 includes only two elements of the container-shaped molded object 1 and the molded blade part 2, and thus blowing efficiency is improved as well as the number of elements may also be decreased.

In addition, the other embodiments will be described.

As illustrated in FIG. 13, a cover member 25 having a top surface in a dome-shaped curved surface to cover a downstream side (a top surface side) of a hub 21 may be installed to prevent a blower 100 from being damaged by being in contact with a bell mouth part 11 when snow is accumulated on a central portion of a propeller fan FN and a rotation shaft is shaken. In addition, the cover member 25 may be provided to be separable from the hub 21 so that cost is easily decreased by omitting the present structure in areas snow does not fall.

In the above-described embodiment, although the stator part 2F is formed by installing the noise prevention blade 22 into the diffuser part 12 in a radial shape, for instance, the plurality of noise prevention blades 22 having a shape expanding straight along a long or minor axis may be installed. Such a structure may improve blowing efficiency and also suppress a noise from being intensively increased at a specific frequency by varying lengths of the noise prevention blades 22. Although the downstream end of the diffuser part 12 has an oval shape, for instance, the downstream end may have a polygonal shape close to a circle or oval. In this case, it is preferable that a central point of the downstream end of the diffuser part 12 be disposed on the rotation shaft line of the propeller fan FN.

Various modifications or embodiments except for the above-described embodiments may be combined without departing from the purposes of the present.

What is claimed is:

1. An outdoor unit of an air conditioner comprising:
 - a heat exchanger configured to exchange heat with air flowing into the outdoor unit;
 - a casing having a first surface disposed adjacent to the heat exchanger and facing the heat exchanger;
 - a fan having a rotation axis;
 - a bell mouth part configured to guide air introduced into the fan and including a downstream end, the bell mouth part disposed to be around an outer circumferential end of the fan and spaced apart from the outer circumferential end of the fan;

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and

a diffuser part extending from the downstream end of the bell mouth part to guide the air discharged from the fan, and including:

an opening, and

an inner circumferential surface inclined at diffuser angles with respect to the rotation axis, and having a first portion disposed adjacent to the first surface of the casing and a second portion disposed to be 90 degrees apart from the first portion along a circumferential direction of the inner circumferential surface of the diffuser part,

wherein:

the diffuser angles of the inner circumferential surface of the diffuser part varies along the circumferential direction of the inner circumferential surface of the diffuser part,

a diffuser angle of a first point in the first portion is larger than a diffuser angle of a second point in the second portion, the second point disposed to be 90 degrees apart from the first point along the circumferential direction of the inner circumferential surface of the diffuser part and disposed at a height from the downstream end of the bell mouth part equal to a height from the downstream end of the bell mouth part of the first point in a direction of the rotation axis, and a downstream end of the diffuser part is provided in an oval shape symmetric about a minor axis.

2. The outdoor unit of claim 1, wherein the diffuser angle of the inner circumferential surface positioned at a side of the diffuser part, in which an air flow rate for the air flow path is greater than another air flow rate in another side of the diffuser part, is provided to be greater than that of the inner circumferential surface positioned at said another side of the diffuser.

3. The outdoor unit of claim 2, wherein the diffuser angle (θ) of the inner circumferential surface with respect to the rotation axis that varies along the circumferential direction varies in a range of $3^\circ \leq \theta \leq 35^\circ$.

4. The outdoor unit of claim 2, wherein, when a plurality of fans are provided, a plurality of diffuser parts are provided to correspond to the plurality of fans, and the diffuser angle (θ) of an inner circumferential surface positioned at a side adjacent to another diffuser part varies in a range of $3^\circ \leq \theta \leq 7^\circ$.

5. The outdoor unit of claim 1, wherein:

when a length of a major axis of the opening of the downstream end of the diffuser part is represented as W, and

a length of the minor axis thereof is represented as D, the lengths of the major axis and the minor axis are set such that $0.75 < D/W < 1$.

6. The outdoor unit of claim 1, wherein a center of an opening of the downstream end of the diffuser part is provided on the rotation axis to which the fan is coupled.

7. The outdoor unit of claim 1, further comprising a panel including an opening through which air is discharged and configured to cover a side of the diffuser part, wherein, in a straight line between a corner of one side of the panel and the rotation axis of the fan, when a length of a straight line between the corner and a downstream end of the diffuser part which meets the straight line is represented as L1, and a length of a straight line between the downstream end of the diffuser part which meets the straight line and the rotation axis of the fan is represented as L2, $0.6 \leq L2/(L1+L2) \leq 0.95$ is satisfied.

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8. The outdoor unit of claim 1, wherein the heat exchanger has three sides facing the casing, and

wherein the first surface corresponds to one of the three sides of the heat exchanger which has the largest area among the three sides of the heat exchanger.

9. A blower assembly of an outdoor unit of an air conditioner including a heat exchanger configured to exchange heat with air flowing into the outdoor unit, a casing having a first surface disposed adjacent to the heat exchanger and facing the heat exchanger, wherein the blower assembly includes a fan having a rotation axis, a bell mouth part configured to guide air introduced into the fan and including a downstream end disposed around an outer circumferential end of the fan and spaced apart from the outer circumferential end of the fan, and a diffuser part extending from the downstream end of the bell mouth part to guide the air discharged from the fan, wherein the diffuser part includes:

an opening, and

an inner circumferential surface inclined at diffuser angles with respect to the rotation axis, and having a first portion disposed adjacent to the first surface of the casing and a second portion disposed to be 90 degrees apart from the first portion along a circumferential direction of the inner circumferential surface of the diffuser part,

wherein:

the diffuser angles of the inner circumferential surface of the diffuser part varies along the circumferential direction of the inner circumferential surface of the diffuser part,

a diffuser angle of a first point in the first portion is larger than a diffuser angle of a second point in the second portion, the second point disposed to be 90 degrees apart from the first point along the circumferential direction of the inner circumferential surface of the diffuser part and disposed at a height from the downstream end of the bell mouth part equal to a height from the downstream end of the bell mouth part of the first point in a direction of the rotation axis, and a downstream end of the diffuser part is provided in an oval shape symmetric about a minor axis.

10. The blower assembly of claim 9, wherein the diffuser angle of the inner circumferential surface positioned at a side of the diffuser part, in which an air flow rate for the air flow path is greater than another airflow rate in another side of the diffuser part, is provided to be greater than that of the inner circumferential surface positioned at said another side of the diffuser.

11. The blower assembly of claim 9, wherein the diffuser angle (θ) of the inner circumferential surface with respect to the rotation axis that varies along the circumferential direction continuously varies along the circumferential direction in a range of $3^\circ \leq \theta \leq 35^\circ$.

12. The blower assembly of claim 9, wherein the heat exchanger has three sides facing the casing, and wherein the first surface corresponds to one of the three sides of the heat exchanger which has the largest area among the three sides of the heat exchanger.

13. An outdoor unit of an air conditioner comprising a blower assembly configured to flow air downstream for the outdoor unit of the air conditioner, the blower assembly comprising:

a fan having a rotation axis and configured to discharge air, which has passed through a heat exchanger of the outdoor unit, from the outdoor unit;

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a bell mouth part disposed around and spaced apart from an outer circumferential end of the fan, and having an inner circumference of an upstream end, disposed along a first plane perpendicular to the rotation axis, being larger than an inner circumference of a downstream end disposed along a second plane perpendicular to the rotation axis; and

a diffuser part extended from the downstream end of the bell mouth part relative to a flow of the air through the outdoor unit, and including an opening through which the air is discharged from the outdoor unit and an inner circumferential surface which has a first portion corresponding to a minor axis of the opening and a second portion corresponding to a major axis of the opening, wherein the diffuser angles of the inner circumferential surface of the diffuser part surrounding the opening with respect to the rotation axis varies along a circumferential direction of the inner circumferential surface of the diffuser part,

a diffuser angle at a first point in the first portion is smaller than a diffuser angle of a second point in the second

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portion, the second point disposed to be 90 degrees apart from the first point along a circumferential direction of the inner circumferential surface of the diffuser part and disposed at a height from the downstream end of the bell mouth part equal to a height from the downstream end of the bell mouth part of the first point in a direction of the rotation axis, and a downstream end of the diffuser part is provided in an oval shape symmetric about the minor axis.

14. The outdoor unit of claim 13, wherein the diffuser angle of the inner circumferential surface positioned at a side of the diffuser part, in which an air flow rate for the air flow path is greater than another airflow rate in another side of the diffuser part, is provided to be greater than that of the inner circumferential surface positioned at said another side of the diffuser, wherein

the diffuser angle (Θ) of the inner circumferential surface with respect to the rotation shaft that varies along the circumferential direction continuously varies along the circumferential direction in a range of $3^\circ \leq \Theta \leq 35^\circ$.

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