

(19) **DANMARK**

(10) **DK/EP 3883733 T3**



Patent- og
Varemærkestyrelsen

(12) **Oversættelse af
europæisk patentskrift**

-
- (51) Int.Cl.: **B 29 C 48/275 (2019.01)** **B 29 B 7/66 (2006.01)** **B 29 B 17/00 (2006.01)**
B 29 B 17/04 (2006.01) **B 29 C 48/285 (2019.01)** **B 29 C 48/385 (2019.01)**
B 29 C 48/39 (2019.01) **B 29 C 48/525 (2019.01)** **B 29 B 9/02 (2006.01)**
- (45) Oversættelsen bekendtgjort den: **2023-03-06**
- (80) Dato for Den Europæiske Patentmyndigheds bekendtgørelse om meddelelse af patentet: **2022-12-21**
- (86) Europæisk ansøgning nr.: **20793253.4**
- (86) Europæisk indleveringsdag: **2020-10-13**
- (87) Den europæiske ansøgnings publiceringsdag: **2021-09-29**
- (86) International ansøgning nr.: **AT2020060365**
- (87) Internationalt publikationsnr.: **WO2021072465**
- (30) Prioritet: **2019-10-16 AT 508932019**
- (84) Designerede stater: **AL AT BE BG CH CY CZ DE DK EE ES FI FR GB GR HR HU IE IS IT LI LT LU LV MC MK MT NL NO PL PT RO RS SE SI SK SM TR**
- (73) Patenthaver: **PureLoop GesmbH, Unterfeldstrasse 3, 4052 Ansfelden, Østrig**
- (72) Opfinder: **GRADL-LAMI, Klaus, Mühlenweg 2a, 4274 Schönau im Mühlkreis, Østrig**
DOBERSBERGER, Manfred, Stechergasse 5, 4020 Linz, Østrig
GRUBER, Florian, Rüstdorf 60, 4690 Schwanenstadt, Østrig
FEICHTINGER, Klaus, Greinerhofgasse 13, 4040 Linz, Østrig
- (74) Fuldmægtig i Danmark: **CHAS. HUDE A/S, Langebrogade 3B, 1411 København K, Danmark**
- (54) Benævnelse: **Apparat til forarbejdning af materiale, navnlig plastmateriale**
- (56) Fremdragne publikationer:
EP-A1- 1 343 623
EP-A1- 1 918 084
WO-A1-03/076153
AT-B- 407 971
DE-A1- 19 714 944

Device for processing material, in particular plastics material**Description**

5 The invention relates to a device for processing material according to the preamble of claim 1.

Single-shaft shredders are often applied when processing materials to be shredded, especially those made of thermoplastics. Such single-shaft shredders find application in numerous fields, especially for shredding plastics material to be
10 preshredded for recycling purposes. Such material usually appears in the form of films or extrusion start-up pads, bottles and other containers, mostly in a soiled state.

There are single-shaft shredders which in one working step heat the shredded particles, partly through the cut, and transport them further into a conical
15 transition which is formed as a single-screw. These particles are further compressed in the mostly conical part and partially further heated. Part of these thermoplastic particles soften in the process. An extruder then follows on the same axis, further compressing and heating these particles and converting them to a liquid state. Such devices are known, for example, from AT 407 971 B. However,
20 above a certain size, such a design leads to very large and long systems that can no longer be operated well.

In EP 1 918 084 A1 a device is described for processing thermoplastic material with a shredding device for shredding the plastic material and an extruder, wherein the shredding device has a cylinder with a feed opening and a cutter shaft,
25 wherein the extruder has an extruder screw in a screw pipe and wherein the cylinder of the shredding device is connected to the screw pipe of the extruder via a connecting opening. The connecting opening is arranged asymmetrically with respect to a plane which lies in the axis of rotation of the cutter shaft and at right angles to the axis of rotation of the extruder screw, as seen in the direction of
30 rotation of the cutter shaft. The longitudinal axis of the screw is offset to the longitudinal axis of the extruder screw by an offset v , but here the offset v is far outside the radius of the extruder screw.

In EP 1 343 623 A1 an extrusion system for recycling non-pourable plastics is described with an extruder having an extruder screw and a feed unit which, fed
35 from a hopper, transfers the moulding compound into an extruder fill zone of the

extruder screw. However, here too, the offset v of the longitudinal axis of the screw is far outside the radius of the extruder screw.

In addition, to enable scaling to higher throughputs or sizes, it is necessary to move away from a single drive. It is possible to directly couple a separate extruder, primarily with its own drive, to the shredding unit, also primarily with its own drive.

However, the way the pretreated material is fed into the extruder is always a very critical point. Unfavourable feeding often leads to insufficient and unstable filling levels in the extrusion screw, which in turn prevents efficient or sufficient quality extrusion.

Basically, every tamping process or filling process into an extruder is critical. In many cases, a change in direction of the material and a partial closing of the intake opening by the screw flight of the extruder must also be taken into account. These are two major influencing factors.

In some devices, mixing and shredding tools rotating in a vessel succeed in creating a charging pressure, provided the material is in particulate, fluid form. This also has the advantage that excess material that cannot be taken up by the extruder is returned to the container. However, this is much more difficult with a tamping screw.

It is thus object of the present invention to create a device which, on the one hand, has a reasonable size at higher throughputs and can be operated well, and at the same time ensures advantageous filling of the extruder and efficient or high-quality extrusion.

This object is solved in such a device by the characterising features of claim 1.

It is provided here that:

- the central longitudinal axis of the screw is oriented at an angle to the central longitudinal axis of the extruder screw, in particular at an angle of 80° to 100° , preferably 90° ,
- and the longitudinal axis of the screw is offset with respect to the longitudinal axis of the extruder screw by the offset (v) in the direction of the direction of rotation of the extruder screw at or in the region of the discharge opening or the intake opening.

According to the invention it is provided that the offset (v) is in the range of $0 < v < R$, wherein R is the radius of the extruder screw (11). In this way a particularly advantageous feeding of the extruder is possible.

5 Due to the coupling of the screw being at an angle, in particular a conveying, transport or agglomerating screw, to the extruder, wherein the material is conveyed laterally into the extruder, on the one hand it is ensured that the dimensions of the device are compact even at higher throughput rates and that the system remains readily operable.

10 In addition, due to the special offset of the longitudinal axis of the screw with respect to the longitudinal axis of the extruder screw, a better and more stable filling of the extruder is ensured. The change in direction of the material caused by the arrangement at an angle in particular results in even more special requirements here.

15 On the one hand, the special offset creates a certain amount of space for the material to be deflected in the extruder intake. So if there is a slight overfeeding here, that can already be cushioned to some degree by this.

20 On the other hand, the special geometry in the coupling region must be taken into account: Thus, the "corkscrew" from the screw rotates against or in the direction of the extruder device, i.e. against the active flank of the extruder screw. A screw always has a higher density on the active flank than on the passive flank, especially when the material has not yet melted and the screw is partially filled. This more compressed material, which also partially sticks together, retains the screw shape after leaving the conveying screw and is thus pressed against the active flank of the extruder screw. In addition to more stable filling, this also causes
25 some further compression.

The longitudinal axis of the screw and the longitudinal axis of the extruder screw are just not at the same height in the process. They are oriented at an angle, advantageously substantially perpendicularly, to one another and define an x-axis and a y-axis. The offset occurs in the z-axis, thus in a direction normal to the longitudinal axis of the screw and to the longitudinal axis of the extruder screw.
30 The direction of the offset is essential in this process. The offset namely occurs in the direction in which the extruder screw rotates in the region of or directly in front of the discharge opening. In case the extruder screw rotates counterclockwise, thus for example, as viewed from behind or from the drive of the extruder, the offset
35 occurs downwards when the screw enters the extruder laterally from the left and

thus feeding occurs from the left, also as viewed from behind or from the drive. As long as the offset of the longitudinal axis of the screw in the z-axis occurs in the intended direction, it is therefore irrelevant whether the offset of the screw - depending on the direction of rotation of the extruder screw and/or the feed side into the extruder - occurs slightly upwards or downwards compared to the extruder screw.

According to a particularly advantageous embodiment, the longitudinal axis of the screw is arranged below the longitudinal axis of the extruder, i.e. with the device in the operating state, the screw is somewhat closer to the bottom than the extruder screw. The feeding of the extruder thus occurs into the region of the extruder screw that is somewhat closer to the bottom.

The screw preferably always opens out into the lateral region of the extruder, even if it is an extruder having multiple screws, in particular a twin-screw extruder. In this case, the screw advantageously opens out approximately into the plane spanned by the longitudinal axes of the extruder screws.

According to another preferred embodiment, it is provided that the intake opening of the extruder has, in the direction of the offset, a bottom surface which is inclined at an angle α with respect to the longitudinal axis and opening outwards, wherein the angle α is in the range of $0^\circ < \alpha < 20^\circ$. The bottom surface is thus sloped such that a kind of wide access ramp for the material fed to the extruder is created which then rises and steadily reduces the region of the feed as the material gets closer to the extruder screw.

It is further advantageous if the, in particular cylindrical, shredding housing has a larger inner diameter than the, in particular cylindrical, housing of the screw. This makes it easy to achieve precompression of the material. For design reasons, too, it is usually desirable to design the screw housing with a smaller diameter than the housing of the shredder in order to achieve a large holding volume for the latter and, on the other hand, to keep the effort for the screw smaller.

In this context, it is particularly advantageous when the housing is cylindrical or has a conical shape.

A favourable embodiment of the invention results when the housing of the screw is coaxially or equiaxially connected to the discharge opening of the housing of the rotor body, wherein one front side of the housing of the screw forms the intake opening for the material to be conveyed or plasticised by the screw, which then exits, in particular in the partially plasticised state, at the other front side of

this housing. This has the advantage that the heat occurring in the shredder, which is due to the cutting processes and friction, is immediately carried on without loss through the processed material into the plasticising region, where it is made effective for plasticising the material.

5 According to a most preferable embodiment, it is provided that the shredding housing, which is larger in diameter, and the housing of the screw, which is smaller in diameter, thus the shredding unit and the screw, are connected to one another by a conical transition portion. It is particularly advantageous when a conical screw is arranged in the conical transition portion for conveying and, above all, also for
10 compressing the material. Due to the compression in the conical transition, heating occurs in this region. Furthermore, partial agglomeration of the material can occur. This initially produces preheated and precompressed material in the conical transition to the tamping screw. This simplifies the change of direction and keeps the filling level of the extruder screw high. The compression of the material already
15 occurs upstream of the screw - in contrast to plant combinations in which, downstream of a single-shaft shredder, tamping screws without a special precompression device convey the largely uncompressed material into the extruder, or in which the screw only carries out compression immediately before entering the extruder. The compression of the material and the supply into the
20 extruder are therefore also separated locally. This results in sufficient and stable filling levels in the extrusion screw, thus ensuring particularly efficient and high-quality extrusion.

 According to a further preferred embodiment, it is accordingly provided that the material leaves the conical part preferably into a cylindrical or conical single-
25 screw, which subsequently conveys the material into the extruder. During this, the material is further heated or tempered and fed into the side of the extruder screw.

 The screw can advantageously be designed as a non-compressing conveying screw or a screw which at least partially compresses, plasticises and/or agglomerates the material, in particular a plasticiser screw.

30 A structurally advantageous solution for the drive results when the screw forms a support for the rotor body with an extension of its core projecting into the front end of the rotor body facing it. In this case, the screw flights abutting the inner wall of the housing of the screw form the bearing for the other end of the rotor body. There is therefore no need for a different type of bearing for the discharge end of
35 the rotor body.

In this context, it is particularly advantageous when the rotor body is coupled to the screw, and optionally also to the conical screw, in a rotationally locked manner and is driven by a common drive.

5 In the drawings, the object of the invention is shown schematically and by way of example by means of embodiment examples:

Fig. 1 shows an embodiment of the device according to the invention in a perspective overview

Fig. 2 shows the device according to the invention in a section from above.

10 Fig. 3 shows a section of the device according to the invention in a cross-section from the side.

Fig. 4 shows the same section in a cross-section from above.

In Fig. 1 and 2, the device according to the invention is shown in its entirety.
15 The device comprises, as main components, a shredding unit 1, a conveying unit 19 having a screw 7 and connected thereto downstream or in the conveying direction, and an extruder 9 connected thereto further downstream or in the conveying direction.

20 The shredding unit 1 serves for shredding and optionally heating the fed material. This is a single-shaft shredder with a shredding housing 2, in which a roller-shaped rotor body 4 is provided which is able to be driven in rotation about its longitudinal axis. The rotor body 4 bears a multiplicity of shredding tools 14 on its circumference. These blades cooperate with counter blades that are arranged stationarily on the inside of the shredding housing 2.

25 The shredding housing 2 is substantially cylindrical and encloses the rotor body 4 over most of its circumference wherein the exposed circumferential region is in the upper half of the circumference and forms the feed opening 5 for the material to be processed and shredded. The material is fed via the feed opening 5 to the rotor body 4 and is gripped by it. The material shredded in this way is
30 conveyed in the direction to an output region 6 arranged on the front side of the shredding housing 2.

Downstream or in the material conveying direction, the conveying unit 19 having a housing 15 and a screw 7, which is mounted therein and is able to be driven in rotation, for conveying and optionally compressing the material output
35 from the shredding unit 1, is arranged at the output region 6 of the shredding unit

1. The longitudinal axis of the rotor body 4 and the longitudinal axis 3 of the screw 7 are aligned coaxially or equiaxially to one another. The shredding unit 1 is designed in such a way that the material is conveyed in the axial direction of the rotor body 4 to and through the output region 6, front-sided to the screw 7. To impart this component of motion to the material in the axial direction of the rotor body 4, the inner wall of the shredding housing 2 opposite the rotor body 4 carries a multiplicity of helically extending wide grooves separated from one another by wide ribs.

The cylindrical shredding housing 2 has a larger inner diameter than the cylindrical housing 15 of the screw 7. The shredding housing 2 and the housing 15 are accordingly connected to one another by a conical transition portion 17, it being provided that a conical screw 18 is arranged in the conical transition portion 17 for conveying and optionally compressing the material.

Such single-shaft shredders, in particular the combination of a shredding unit and a conveying unit, are described, for example, in AT407971, pages 4 and 5, and are incorporated by reference into the subject matter of the present disclosure.

The extruder 9 having an extruder housing 13 and an extruder screw 11 mounted therein and able to be driven in rotation is connected to the downstream front side of the screw 7. A front-side discharge opening 8 is formed in the housing 15, via which the material is conveyed into the intake opening 16 of the extruder 9 towards the extruder screw 11.

The central longitudinal axis 3 of the screw 7 is aligned at a right angle to the central longitudinal axis 10 of the extruder screw 11.

As shown in Fig. 3 and 4, the longitudinal axis 3 of the screw 7 is offset with respect to the longitudinal axis 10 of the extruder screw 11 by the offset v , namely in a certain direction, namely in the direction of rotation 12 of the extruder screw 11, viewed at or in or in front of the region of the discharge opening 8.

The longitudinal axis 3 of the screw 7 and the longitudinal axis 10 of the extruder screw 11 are thus not at the same height, but the longitudinal axis 3 of the screw 7 is closer to the bottom or, in the device according to Fig. 1 and 2 below the longitudinal axis 10 of the extruder screw 11.

The longitudinal axis 3 of the screw 7 defines an x-axis, the longitudinal axis 10 of the extruder screw 11 defines a y-axis. The offset occurs along the z-axis, thus in a direction normal to the longitudinal axis 3 of the screw 7 and to the longitudinal axis 10 of the extruder screw 11.

Essential is the direction of the offset v . The offset v namely occurs in the direction in which the extruder screw 11 rotates in the region of or directly in front of the discharge opening 8 or the intake opening 16 of the extruder (direction of rotation 12). In the device according to the figures, the extruder screw 11 rotates anticlockwise as viewed from behind or from the drive of the extruder 9. The screw 7 opens into the extruder 9 laterally from the left, also viewed from the rear or from the drive. The offset v of the longitudinal axis 3 of the screw 7 occurs accordingly downwards, i.e. the longitudinal axis 3 of the screw 7 opens out into the region of the extruder screw 11 that is somewhat closer to the bottom.

The feed opening 16 of the extruder 9 has, in the direction of the offset v , a bottom surface 20 located in the bottom region during operation, which is inclined at an angle α of about 15° to the longitudinal axis 3 or to the horizontal.

PATENTKRAV

1. Apparat til forarbejdning af materiale, navnlig plastmateriale, omfattende

- 5 - en sønderdelingsenhed (1) til sønderdeling og i givet fald opvarmning af materialet, navnlig en enkelt-akslet sønderdeler, med et sønderdelingshus (2), i hvilket et rotorlegeme (4), navnlig i form af en valse, som kan drives i rotation omkring sin længdeakse, er tilvejebragt, og som bærer en flerhed af sønderdelingsværktøjer (14) på sin omkreds, og
- 10 med en tilførselsåbning (5), gennem hvilken materialet, der skal sønderdeles, kan tilføres til rotorlegemet (4),
- en transportørenhed (19), der slutter sig til et udløbsområde (6) for sønderdelingsenheden (1), med et hus (15) og en skrue (7), der er monteret deri og er i stand til at blive drevet i rotation, med henblik på at
- 15 transportere og eventuelt komprimere materialet, som afgives fra sønderdelingsenheden (1), hvorved sønderdelingsenheden (1) eller rotorlegemet (4) er konfigureret på en sådan måde, at materialet er i stand til at blive transporteret i den aksiale retning for rotorlegemet (4) hen imod og gennem udløbsområdet (6) på skruens (7) frontside, og hvorved rotorlegemets (4) længdeakse og skruens (7) længdeakse (3) er orienteret i det væsentlige parallelt, især koaksialt, med hinanden,
- 20 - og en ekstruder (9), som støder op til skruen (7), med et ekstruderhus (13) samt mindst én ekstruderskrue (11), der er monteret deri og i stand til at blive drevet i rotation, hvorved en frontside-afgangsåbning (8) er
- 25 dannet i huset (15), via hvilken materialet kan transporteres til ekstruderskruens (9) indløbsåbning (16) til ekstruderskruen (11),

hvorved

- 30 - skruens (7) centrale længdeakse (3) er orienteret i en vinkel i forhold til ekstruderskruens (11) centrale længdeakse (10), navnlig i en vinkel på 80° til 100°, fortrinsvis 90°,

- og skruens (7) længdeakse (3) er forskudt i forhold til ekstruderskruens (11) længdeakse (10) med forskydningen (v) i retning af ekstruderskruens (11) rotationsretning (12) på eller i området ved afgangsåbningen (8) eller indløbsåbningen (16),

5

kendetegnet ved, at forskydningen (v) ligger i intervallet $0 < v < R$, hvorved R er ekstruderskruens (11) radius.

2. Apparat ifølge et af de foregående krav,

10 **kendetegnet ved, at** skruens (7) længdeakse (3) er nærmere ved bunden end ekstruderskruens (11) længdeakse (10) med forskydningen (v), når apparatet er klargjort til drift.

3. Apparat ifølge et af de foregående krav,

15 **kendetegnet ved, at** ekstruderens (9) indløbsåbning (16), i retning af forskydningen (v), omfatter en bundflade (20), som hælder med en vinkel α i forhold til længdeaksen (3), og som åbner udad, hvorved vinklen α ligger i intervallet $0^\circ < \alpha < 20^\circ$.

20 4. Apparat ifølge et af de foregående krav,

kendetegnet ved, at det navnlig cylindriske sønderdelingshus (2) har en større indvendig diameter end det, især cylindriske, hus (15) for skruen (7).

5. Apparat ifølge et af de foregående krav,

25 **kendetegnet ved, at** huset (15) er cylindrisk eller har konisk form.

6. Apparat ifølge et af de foregående krav,

kendetegnet ved, at sønderdelingshuset (2) og huset (15) er forbundet med hinanden ved hjælp af et konisk overgangsafsnit (17), hvorved det navnlig er arrangeret, at en konisk skrue (18) er placeret i det koniske overgangsafsnit (17) med henblik på transport og eventuelt komprimering af materialet.

30

7. Apparat ifølge et af de foregående krav,

kendetegnet ved, at skruen (7) er en ikke-komprimerende transportskrue eller en skrue, som i det mindste delvist komprimerer, plastificerer og/eller agglomerer materialet, navnlig en plastificerings-skrue.

5 8. Apparat ifølge et af de foregående krav,

kendetegnet ved, at skruen (7) danner en understøtning for rotorlegemet (5), med en forlængelse af dets kerne ragende ind i rotorlegemets (5) frontende, og som vender mod skruen.

10 9. Apparat ifølge et af de foregående krav,

kendetegnet ved, at rotorlegemet (5) er koblet til skruen (7) og i givet fald også til den koniske skrue (18) på rotationslåst måde og er drevet af et fælles drev.

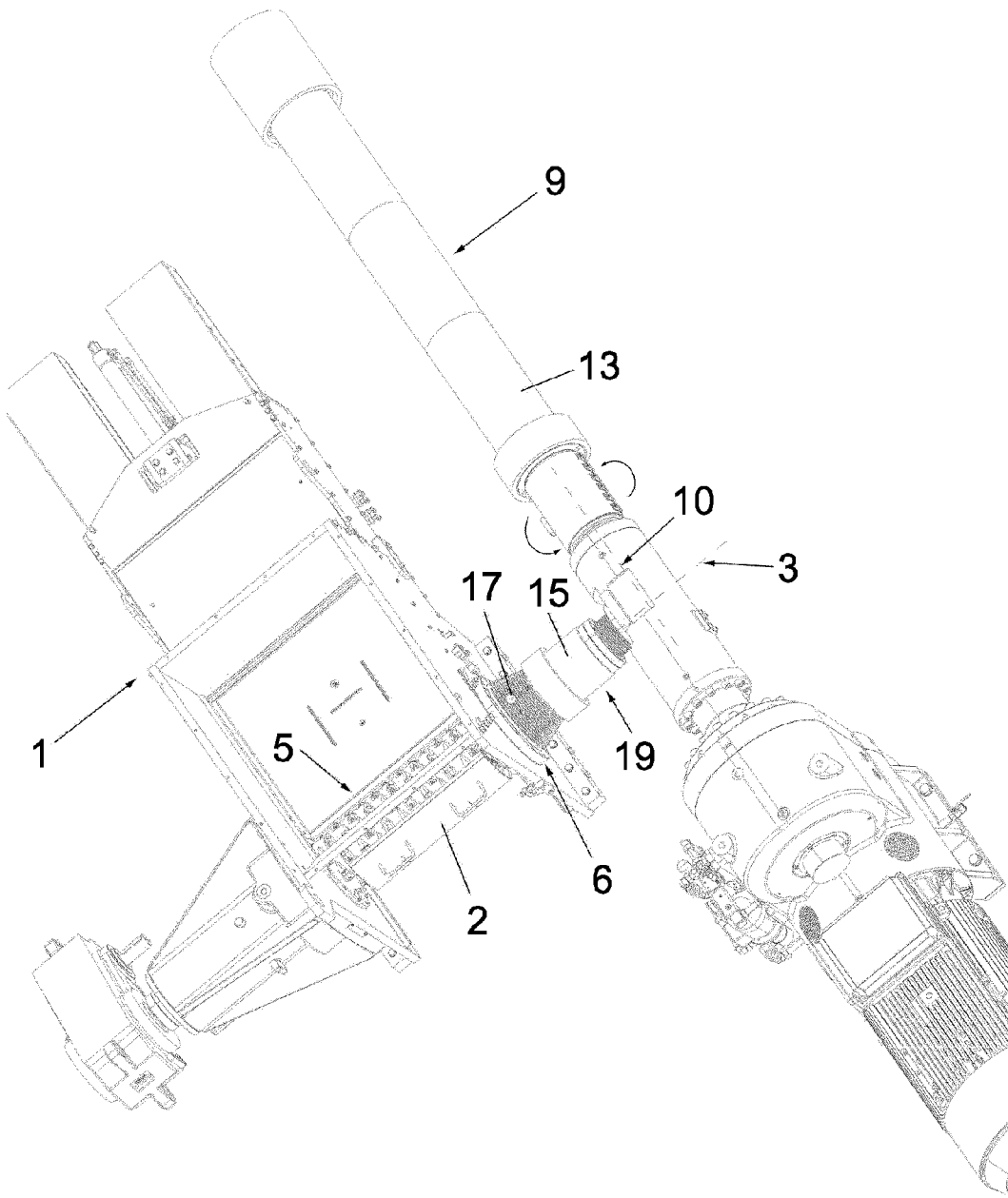


Fig. 1

Fig. 2

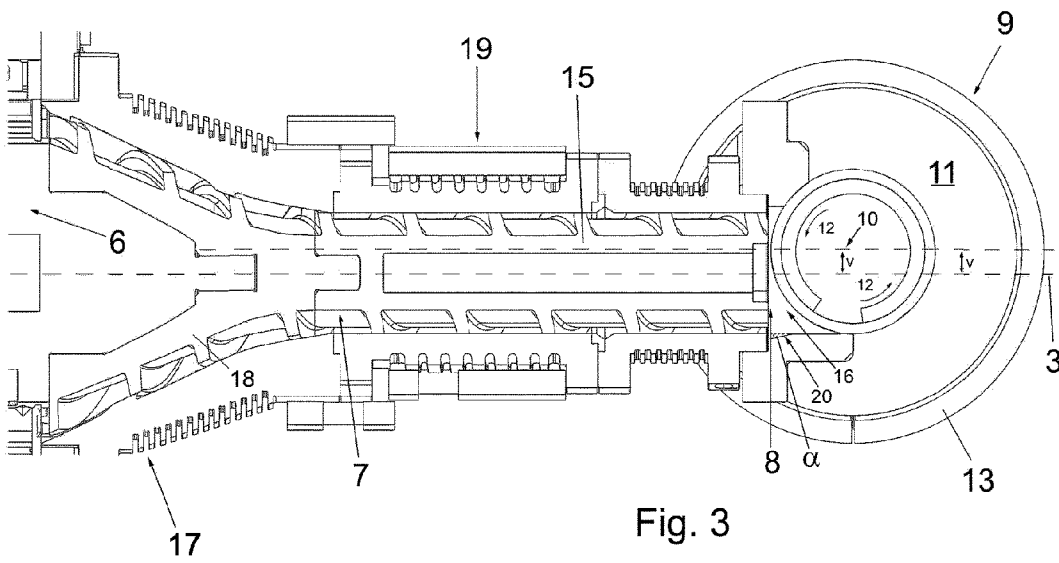
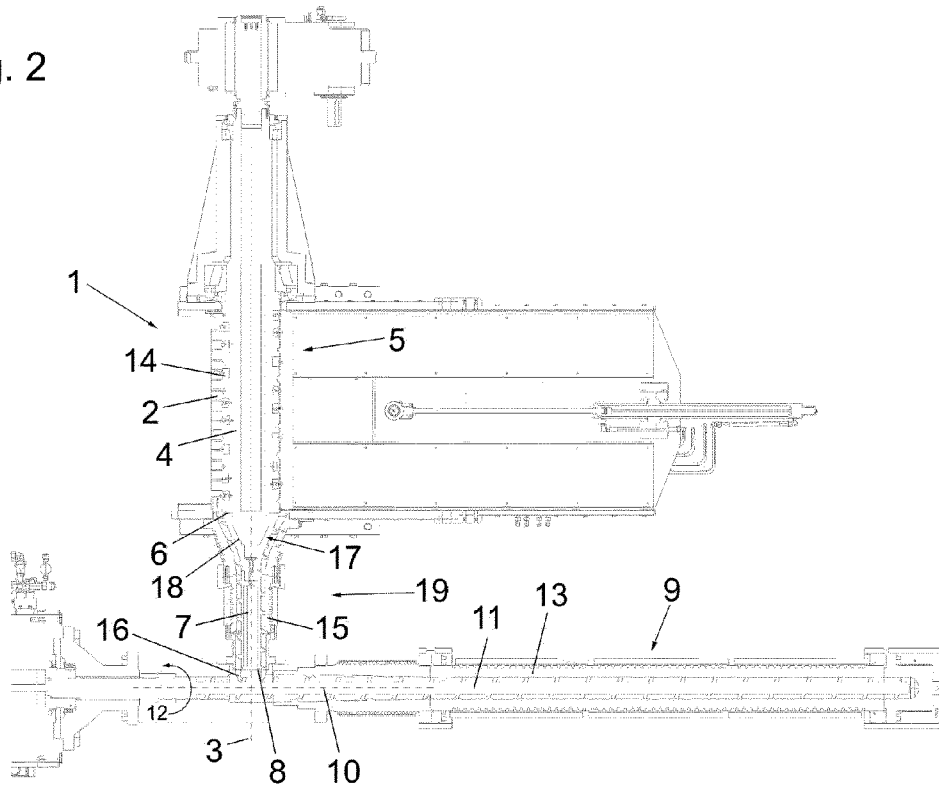


Fig. 3

