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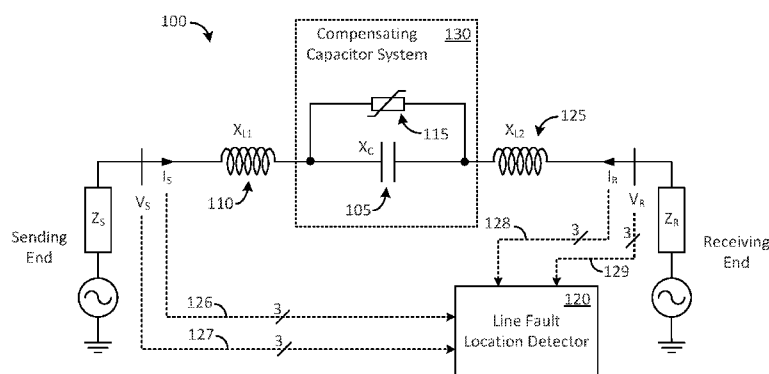


FIG. 1

(57) **Abstract:** Embodiments of the disclosure relate to systems and methods for determining a fault location in a three-phase series-compensated power transmission line system by using symmetrical components-based formulas that describe various voltage and current relationships. The voltage and current relationships can be derived using a synchronous measurement procedure that is concurrently executed at a sending end and a receiving end of the first series-compensated power transmission line system. Furthermore, determining the fault location in accordance with certain embodiments of the disclosure can eliminate one or more of a need to calculate an impedance value of any of the series capacitors or the series capacitor protection elements that are a part of the three-phase series-compensated power transmission line system, a need to monitor any of the series capacitor protection elements, and a need to measure a voltage drop across any of the series capacitors.

SYSTEMS AND METHODS FOR DETERMINING A FAULT LOCATION IN A THREE-PHASE SERIES-COMPENSATED POWER TRANSMISSION LINE

CROSS-REFERENCE TO RELATED APPLICATION

[00001] This patent application is a continuation-in-part of U.S. Patent Application No. 15/018,470, titled “Systems and Methods for Determining a Fault Location in a Three-Phase Series-Compensated Power Transmission Line,” filed February 8, 2016, the entirety of which application is hereby incorporated herein by reference.

FIELD OF THE DISCLOSURE

[00002] This disclosure relates to series-compensated power transmission lines, and more particularly, to systems and methods for determining a fault location in a three-phase series-compensated power transmission line.

BACKGROUND OF THE DISCLOSURE

[00003] A series-compensated power transmission line typically incorporates a capacitor that is coupled in series with the power transmission line to compensate for the distributed series inductance presented by the power transmission line. The capacitive compensation is directed at optimizing power transmission capacity over the power transmission line. Also typically, a protection element such as a metal-oxide varistor (MOV) is coupled in parallel with the capacitor in order to prevent damage to the capacitor when a fault, such as a short-circuit for example, occurs on the power transmission line.

[00004] Unfortunately, the overall line impedance of the series-compensated power transmission line changes in a non-linear manner when the MOV transitions from a non-conducting state to a conducting state upon the occurrence of a fault. Additionally, the overall line impedance can vary in a somewhat unpredictable manner due to various factors such as the nature of the fault (short circuit, open circuit, bridged short across lines etc.), the severity of the fault, and the conduction characteristics of the MOV. Consequently, the use of a conventional fault locating system, which may be quite effective on a non-compensated power transmission line having a substantially consistent impedance characteristic, may turn out to be inadequate for identifying a fault location in a series-compensated power transmission line.

[00005] One traditional approach for addressing this issue involves the use of a different type of fault locating system that incorporates a deterministic procedure and takes into consideration the characteristics of the protection element (the MOV, for example) and various parameters associated

with the faulty power transmission line. Such a procedure can include for example, various steps such as modeling the series compensated power transmission line, modeling the compensating capacitor, modeling the MOV, and monitoring the operational status of the MOV. Another traditional approach involves making an assumption of a faulty segment in a multi-segment power transmission system and executing a fault location procedure based on the assumption. Once a faulty segment is accurately identified, the exact location of the fault on this faulty segment has to be identified. Understandably, such traditional approaches can not only be complex and ambiguous but may also lead to imprecise results as a result of the assumptions being made.

BRIEF DESCRIPTION OF THE DISCLOSURE

[00006] Embodiments of the disclosure are directed generally to systems and methods for determining a fault location in a series-compensated power transmission line. In certain embodiments, a fault location in a three-phase series-compensated power transmission line system can be determined by using symmetrical components-based formulas to describe various voltage and current relationships present in the three-phase series-compensated power transmission line during a fault condition.

[00007] According to one exemplary embodiment of the disclosure, a three-phase series-compensated power line system includes a first series-compensated power transmission line, a second series-compensated power transmission line, a third series-compensated power transmission line, and a line fault location detector. The first series-compensated power transmission line is configured to propagate electrical power having a first phase, and includes a first compensating capacitor system that includes a first series capacitor and a first series capacitor protection element. The second series-compensated power transmission line is configured to propagate electrical power having a second phase, and includes a second compensating capacitor system that includes a second series capacitor and a second series capacitor protection element. The third series-compensated power transmission line is configured to propagate electrical power having a third phase, and includes a third compensating capacitor system that includes a third series capacitor and a third series capacitor protection element. The line fault location detector includes at least one processor that is configured to execute a first fault location procedure for identifying a location of a single-phase-to-ground fault in the three-phase series-compensated power line system. The first fault location procedure includes determining a zero sequence voltage drop based in part on a relationship between a first impedance presented by the first compensating capacitor system during the single-phase-to-ground fault, a second impedance presented by the second compensating capacitor system during the single-phase-to-ground fault, and a third impedance presented by the third compensating capacitor

system during the single-phase-to-ground fault, wherein one of the first impedance, the second impedance, or the third impedance is an undetermined impedance that is attributable to a corresponding one of the first series capacitor protection element, the second series capacitor protection element, or the third series capacitor protection element turning active during the single-phase-to-ground fault. The first fault location procedure also includes determining at least one of a positive sequence voltage drop or a negative sequence voltage drop based in part on the relationship between the first impedance, the second impedance, and the third impedance; and determining the location of the single-phase-to-ground fault at least in part, by using the zero sequence voltage drop and the at least one of the positive sequence voltage drop or the negative sequence voltage drop to eliminate determining of the undetermined impedance.

[00008] According to another exemplary embodiment of the disclosure, a line fault detector includes a plurality of input interfaces configured to receive a set of electrical current measurements and a set of voltage measurements that are obtained via a synchronous measurement procedure concurrently executed at a sending end and a receiving end of the three-phase series-compensated power transmission line system. The line fault detector further includes at least one processor configured to execute a first fault location procedure for identifying a location of a single-phase-to-ground fault in the three-phase series-compensated power line system. The first fault location procedure includes determining a zero sequence voltage drop based in part on a relationship between a first impedance presented by the first compensating capacitor system during the single-phase-to-ground fault, a second impedance presented by the second compensating capacitor system during the single-phase-to-ground fault, and a third impedance presented by the third compensating capacitor system during the single-phase-to-ground fault, wherein one of the first impedance, the second impedance, or the third impedance is an undetermined impedance that is attributable to a corresponding one of the first series capacitor protection element, the second series capacitor protection element, or the third series capacitor protection element turning active during the single-phase-to-ground fault. The first fault location procedure also includes determining at least one of a positive sequence voltage drop or a negative sequence voltage drop based in part on the relationship between the first impedance, the second impedance, and the third impedance; and determining the location of the single-phase-to-ground fault at least in part, by using the zero sequence voltage drop and the at least one of the positive sequence voltage drop or the negative sequence voltage drop to eliminate determining of the undetermined impedance.

[00009] According to yet another exemplary embodiment of the disclosure, a method includes executing a synchronous measurement procedure concurrently at a sending end and a receiving end of a three-phase series-compensated power transmission line system for obtaining a set of electrical

current measurements and a set of voltage measurements; receiving in a line fault location detector, the set of electrical current measurements and the set of voltage measurements based on the synchronous measurement procedure; and using at least one processor in the line fault location detector to execute a first fault location procedure for identifying a location of a single-phase-to-ground fault in the three-phase series-compensated power line system. The first fault location procedure includes determining a zero sequence voltage drop based in part on a relationship between a first impedance presented by the first compensating capacitor system during the single-phase-to-ground fault, a second impedance presented by the second compensating capacitor system during the single-phase-to-ground fault, and a third impedance presented by the third compensating capacitor system during the single-phase-to-ground fault, wherein one of the first impedance, the second impedance, or the third impedance is an undetermined impedance that is attributable to a corresponding one of the first series capacitor protection element, the second series capacitor protection element, or the third series capacitor protection element turning active during the single-phase-to-ground fault; determining at least one of a positive sequence voltage drop or a negative sequence voltage drop based in part on the relationship between the first impedance, the second impedance, and the third impedance; and determining the location of the single-phase-to-ground fault at least in part, by using the zero sequence voltage drop and the at least one of the positive sequence voltage drop or the negative sequence voltage drop to eliminate determining of the undetermined impedance.

[00010] Other embodiments and aspects of the disclosure will become apparent from the following description taken in conjunction with the following drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

[00011] Having thus described the disclosure in general terms, reference will now be made to the accompanying drawings, which are not necessarily drawn to scale, and wherein:

[00012] FIG. 1 illustrates a simplified representation of a three-phase series-compensated power transmission line that includes a line fault location detector in accordance with an example embodiment of the disclosure.

[00013] FIG. 2 illustrates an example circuit representation of a three-phase series-compensated power transmission line when a fault occurs between a series capacitor and a sending end of the three-phase series-compensated power transmission line according to an example embodiment of the disclosure.

[00014] FIG. 3 illustrates another example circuit representation of a three-phase series-compensated power transmission line when a fault occurs between a series capacitor and a receiving

end of the three-phase series-compensated power transmission line according to an example embodiment of the disclosure.

[00015] FIG. 4 illustrates exemplary positive, negative and zero sequences components networks associated with the example circuit representation shown in FIG. 3.

[00016] FIG. 5 illustrates a few example components contained in a line fault location detector in accordance with an exemplary embodiment of the disclosure.

DETAILED DESCRIPTION OF THE DISCLOSURE

[00017] The disclosure will be described more fully hereinafter with reference to the accompanying drawings, in which exemplary embodiments of the disclosure are shown. This disclosure may, however, be embodied in many different forms and should not be construed as limited to the exemplary embodiments set forth herein; rather, these embodiments are provided so that this disclosure will satisfy applicable legal requirements. Like numbers refer to like elements throughout. It should be understood that certain words and terms are used herein solely for convenience and such words and terms should be interpreted as referring to various objects and actions that are generally understood in various forms and equivalencies by persons of ordinary skill in the art. For example, it should be understood that the phrase “transmission line” as used herein generally refers to an electrical conductor that conducts electrical power between two points, generally referred to herein as a “sending end” and a “receiving end” of a power transmission line system. The word “link” as used herein generally refers to any one or more of an electrical conductor, a communication link, or a data link used for transporting various types of information and/or data. The word “current” as used herein generally refers to an electrical current. The word “concurrently” as used herein can be replaced in some example embodiments by alternative words and phrases such as “substantially concurrently,” and “synchronously.” Furthermore, the word “example” as used herein is intended to be non-exclusionary and non-limiting in nature. More particularly, the word “exemplary” as used herein indicates one among several examples, and it should be understood that no undue emphasis or preference is being directed to the particular example being described.

[00018] In terms of a general overview, certain embodiments of the systems and methods described herein pertain to determining a fault location in a three-phase series-compensated power transmission line system by using symmetrical components-based formulas that describe various voltage and current relationships in the three-phase series-compensated power transmission lines during a fault condition. Furthermore, the systems and methods for determining the fault location in accordance with certain embodiments of the disclosure can eliminate a need to calculate an

impedance value of any of the series capacitors or the series capacitor protection elements that are a part of the three-phase series-compensated power transmission line system; a need to monitor any of the series capacitor protection elements; and/or a need to measure a voltage drop across any of the series capacitors.

[00019] Attention is first drawn to FIG. 1, which illustrates a simplified representation of a three-phase series-compensated power transmission line system **100** that includes a line fault location detector **120** in accordance with an example embodiment of the disclosure. Even though only a single power transmission line is shown, it should be understood that the line fault location detector **120** is coupled to all three power transmission lines (two lines not shown) of the three-phase series-compensated power transmission line system **100**. Accordingly, as shown in this example embodiment, a link **126** can represent three links that are used to transport electrical current measurements from a sending end of the three power transmission lines of the three-phase series-compensated power transmission line system **100**, a link **127** can represent three links that are used to transport voltage measurements from the sending end of the three power transmission lines of the three-phase series-compensated power transmission line system **100**, a link **128** can represent three links that are used to transport electrical current measurements from a receiving end of the three power transmission lines of the three-phase series-compensated power transmission line system **100**, and a link **129** can represent three links that are used to transport voltage measurements from the receiving end of the three power transmission lines of the three-phase series-compensated power transmission line system **100**.

[00020] In this exemplary embodiment, the line fault location detector **120** is coupled to all three power transmission lines closer towards the receiving end of the three-phase series-compensated power transmission line system **100** than the sending end. Consequently, the link **126** can be a first communication link that transports the electrical current measurements to the line fault location detector **120** in a digital communications format, for example. The link **127** can be a second communication link that transports the voltage measurements to the line fault location detector **120** in a digital communications format as well. Each or both of the links **128** and **129** can also be implemented in the form of communication links or as a result of the shorter transportation distance can be implemented in other ways, such as via analog links.

[00021] The simplified representation of the series-compensated power transmission line system **100** includes a series capacitor **105** that provides a compensating capacitance (X_C) to a distributed series inductance X_L that is a part of an overall line impedance Z_L of a power transmission line (where $Z_L = Z_{L1} + Z_{L2}$). The series capacitor **105** is typically implemented using a number of capacitors that are coupled together to form a capacitor bank. The distributed series

inductance X_L is schematically shown in FIG. 1 in the form of two series inductances X_{L1} and X_{L2} , corresponding to Z_{L1} and Z_{L2} respectively. Specifically, the distributed series inductance X_{L1} is shown as a series inductance **110** that is associated with a first transmission line segment extending from a sending end of the power transmission line to the series capacitor **105**. The distributed series inductance (X_{L2}), is shown as a series inductance **125** that is associated with a second transmission line segment extending from the series capacitor **105** to the receiving end of the power transmission line. It should be understood that the placement of the series capacitor **105** in this exemplary embodiment defines two transmission line segments of the segments of the series-compensated power transmission line system **100**. However, in another exemplary embodiment, the series capacitor **105** can be placed close to the receiving end of the series-compensated power transmission line system **100**, thereby defining a single transmission line segment rather than two transmission line segments.

[00022] A series capacitor protection element **115** is coupled to the series capacitor **105** for protecting the series capacitor **105** when a fault occurs in the series-compensated power transmission line system **100**. In one example implementation, the series capacitor protection element **115** can include a metal-oxide varistor (MOV). A combination of the series capacitor **105** and the series capacitor protection element **115** can be referred to as a compensating capacitor system **130**. It should be understood that each of the other two power transmission lines (not shown) incorporates a similar compensating capacitor system as well.

[00023] The series-compensated power transmission line system **100** provides a compensated power transfer capacity that can be expressed by the following equation:

$$P = \frac{|V_S| |V_R|}{|X_L - X_C|} \sin \delta \quad \text{Eqn. (1)}$$

where δ represents a power angle, V_S represents a first voltage at the sending end of the series-compensated power transmission line system **100** and V_R represents a second voltage at the receiving end of the series-compensated power transmission line system **100**.

[00024] The compensated power transfer capacity expressed by Eqn. (1) can provide an improvement over a power transfer capacity of an uncompensated power transmission line (not shown), where the power transfer capacity of the uncompensated power transmission line can be expressed by the following equation:

$$P = \frac{|V_S| |V_R|}{|X_L|} \sin \delta \quad \text{Eqn. (2)}$$

[00025] Attention is now drawn to FIG. 2, which illustrates an example circuit representation of the series-compensated power transmission line system **100** when a fault occurs at a location **215** between the series capacitor **105** and a sending end of the series-compensated power transmission line system **100**. The per unit distance “d” of the location **215** with reference to the series capacitor **105** can be determined using a fault location technique that is described below with respect to FIG. 3.

[00026] FIG. 3 illustrates a second example circuit representation of the series-compensated power transmission line system **100** when a fault occurs at a location **315** between the series capacitor **105** and a receiving end of the series-compensated power transmission line system **100** and at a per unit distance “d” from the series capacitor **105**. The fault, which can be a single-phase fault to ground for example, can lead to a significantly higher-than-normal current flow through the series capacitor **105**. The series capacitor protection element **115** turns active at this time to protect the series capacitor **105**. The various equations and procedures that can be used for determining the fault location **315** will now be described using FIG. 4, which illustrates exemplary positive, negative and zero sequences associated with the example circuit representation shown in FIG. 3.

[00027] The per unit distance “d” of the location **315** can be determined in accordance with an exemplary embodiment of the disclosure by using the following positive, negative and zero sequences:

$$d (Pos) = (V_1^S - mI_1^S Z_{1L} - \Delta V_1 - V_1^R + (1 - m)I_1^R Z_{1L}) / (1 - m)(I_1^S + I_1^R) Z_{1L} \quad \text{Eqn. (3)}$$

$$d (Neg) = (V_2^S - mI_2^S Z_{2L} - \Delta V_2 - V_2^R + (1 - m)I_2^R Z_{2L}) / (1 - m)(I_2^S + I_2^R) Z_{2L} \quad \text{Eqn. (4)}$$

$$d (Zero) = (V_0^S - mI_0^S Z_{0L} - \Delta V_0 - V_0^R + (1 - m)I_0^R Z_{0L}) / (1 - m)(I_0^S + I_0^R) Z_{0L} \quad \text{Eqn. (5)}$$

where (as shown in FIG. 4), V_0^S is a zero sequence voltage component at the sending end of the series-compensated power transmission line system **100**, V_1^S is a positive sequence voltage component at the sending end of the series-compensated power transmission line system **100**, I_0^S is a zero sequence current component at the sending end of the series-compensated power transmission line system **100**, I_1^S is a positive sequence current component at the sending end of the series-compensated power transmission line system **100**, V_0^R is a zero sequence voltage component at the receiving end of the series-compensated power transmission line system **100**, V_1^R is a positive sequence voltage component at the receiving end of the series-compensated power transmission line system **100**, I_0^R is a zero sequence current component at the receiving end of the series-compensated power transmission line system **100**, I_1^R is a positive sequence current component at the receiving end of the series-compensated power transmission line system **100**, Z_{0L} is a zero sequence total impedance component of the series-compensated power transmission line system **100**, and Z_{1L} is a positive sequence total impedance component of the series-compensated power transmission line

system **100**.

[00028] The per unit distance “d” of the fault at location **315** cannot be determined directly based on Eqns. (3), (4), and (5) above because the sequence components ΔV_0 , ΔV_1 , and ΔV_2 are not known. It may be pertinent to point out at this point that in contrast to the approach provided below in accordance with the disclosure for determining “d” based on solving Eqns. (3), (4), and (5), some conventional approaches use certain assumptions that can lead to erroneous results. For example, in one conventional approach, an estimate of a voltage drop across a series capacitor protection element (such as the series capacitor protection element **115**) is estimated on the basis of a MOV model. One or more simulations using electromagnetic transients programs are then carried out for different current levels from which the per unit distance “d” is determined. In this approach, not only is the calculation based on using only one end of a power transmission line but is also susceptible to providing erroneous results because the MOV model may not take into consideration various conditions such as ambient temperature and aging effects that can alter the characteristics of the MOV.

[00029] In another conventional approach, the use of a MOV model is avoided and measurements carried out from both ends of a series-compensated power transmission line are used. In this particular conventional approach, estimated voltages and current at a fault location are used for determining the fault location. However, in this conventional approach the voltage at a fault location is estimated using measurements from a first end of the series-compensated power transmission line that does not have a series capacitor system located between the fault location and the first end, which can yield erroneous results due to phasor estimation errors under certain types of fault conditions

[00030] Consequently, in contrast to such conventional approaches, and in accordance with an embodiment of the disclosure, the per unit distance “d” of the fault at location **315** can be determined by interpreting the combination of the series capacitor **105** and the series capacitor protection element **115** as a collective impedance representing the combined impedance of the series capacitor **105** and the series capacitor protection element **115** when a fault occurs in the series-compensated power transmission line system **100**.

[00031] The sequence impedance matrix of this collective impedance can be defined as follows:

$$Z_S = A^{-1} Z_P A \quad \text{Eqn. (6)}$$

where $A = \begin{bmatrix} 1 & 1 & 1 \\ 1 & \alpha^2 & \alpha \\ 1 & \alpha & \alpha^2 \end{bmatrix}$; $\alpha = 1 \angle 120$ degrees; Z_S is the sequence impedance matrix of the collective

impedance; and Z_P is the phase impedance matrix of the collective impedance.

[00032] Eqn. (6) can be expanded as follows:

$$Z_S = \frac{1}{3} \begin{bmatrix} 1 & 1 & 1 \\ 1 & \alpha & \alpha^2 \\ 1 & \alpha^2 & \alpha \end{bmatrix} \begin{bmatrix} Z_A & 0 & 0 \\ 0 & Z_B & 0 \\ 0 & 0 & Z_C \end{bmatrix} \begin{bmatrix} 1 & 1 & 1 \\ 1 & \alpha^2 & \alpha \\ 1 & \alpha & \alpha^2 \end{bmatrix} \quad \text{Eqn. (7)}$$

[00033] Eqn. (7) can be rewritten as follows:

$$Z_S = \frac{1}{3} \begin{bmatrix} Z_A + Z_B + Z_C & Z_A + \alpha^2 Z_B + \alpha Z_C & Z_A + \alpha Z_B + \alpha^2 Z_C \\ Z_A + \alpha Z_B + \alpha^2 Z_C & Z_A + Z_B + Z_C & Z_A + \alpha^2 Z_B + \alpha Z_C \\ Z_A + \alpha^2 Z_B + \alpha Z_C & Z_A + \alpha Z_B + \alpha^2 Z_C & Z_A + Z_B + Z_C \end{bmatrix} \quad \text{Eqn. (8)}$$

where Z_A , Z_B , and Z_C are the impedances of the combination of the series capacitor **105** and the series capacitor protection element **115** (i.e. the collective impedance) when applied to phases A, B, and C of a three-phase series-compensated power transmission line. The sequence component of a voltage drop across the combination of the series capacitor **105** and the series capacitor protection element **115** can be expressed as follows:

$$\begin{bmatrix} \Delta V_0 \\ \Delta V_1 \\ \Delta V_2 \end{bmatrix} = \frac{1}{3} \begin{bmatrix} Z_A + Z_B + Z_C & Z_A + \alpha^2 Z_B + \alpha Z_C & Z_A + \alpha Z_B + \alpha^2 Z_C \\ Z_A + \alpha Z_B + \alpha^2 Z_C & Z_A + Z_B + Z_C & Z_A + \alpha^2 Z_B + \alpha Z_C \\ Z_A + \alpha^2 Z_B + \alpha Z_C & Z_A + \alpha Z_B + \alpha^2 Z_C & Z_A + Z_B + Z_C \end{bmatrix} \begin{bmatrix} I_0^M \\ I_1^M \\ I_2^M \end{bmatrix} \quad \text{Eqn. (9)}$$

where I_0^M , I_1^M , and I_2^M are zero, positive, and negative sequence components of a current flowing through the impedances of the combination of the series capacitor **105** and the series capacitor protection element **115**. For the fault location 315, the values of I_0^M , I_1^M , and I_2^M can be estimated by voltage and current measurements obtained from the sending end of the series-compensated power transmission line system 100. It will be pertinent at this point to draw attention to the current I_M that is shown in FIG. 3. Though I_M can be assumed equal to I_S for purposes of some calculations, in one example embodiment in accordance with the disclosure, I_M is different from I_S due to various factors such as the presence of shunt line capacitance in the first transmission line segment between the sending end and the series capacitor 105, however, I_M can be estimated by voltage and current measurements obtained from the sending end of the series-compensated power transmission line system. Furthermore, it will be pertinent to point out that when no fault is present in the three-phase series-compensated power transmission line, $Z_A = Z_B = Z_C = -jX_{\text{cap}}$ where X_{cap} is the reactance of the series capacitor in each of the A, B, and C phases of the three-phase series-compensated power transmission line.

[00034] Equations and formulae pertaining to a single phase to ground fault condition and a double phase to ground fault condition will now be described. Typically, in a single phase to ground

fault condition, only a single series capacitor protection element (the one located in the faulted phase line) will be conducting in accordance with a fault current amplitude. Consequently, the collective impedance Z_A of the compensating capacitor system **130** in the faulted phase line A is an undetermined impedance parameter Z' whereas the impedances of the remaining un-faulted phase lines B and C, each having a series capacitor, can be defined as $Z_B = -jX_{cap}$ and $Z_C = -jX_{cap}$.

Substituting these values into Eqn. (9) provides the following:

$$\Delta V_1 = \frac{1}{3} \left[Z' (I_0^M + I_1^M + I_2^M) - jX_{cap} (2I_1^M - I_2^M - I_0^M) \right] \quad \text{Eqn. (10)}$$

$$\Delta V_2 = \frac{1}{3} \left[Z' (I_0^M + I_1^M + I_2^M) - jX_{cap} (2I_2^M - I_0^M - I_1^M) \right] \quad \text{Eqn. (11)}$$

$$\Delta V_0 = \frac{1}{3} \left[Z' (I_0^M + I_1^M + I_2^M) - jX_{cap} (2I_0^M - I_1^M - I_2^M) \right] \quad \text{Eqn. (12)}$$

[00035] Subtracting Eqn. (12) from Eqn. (10) provides the following:

$$\Delta V_1 - \Delta V_0 = -jX_{cap} (I_1^M - I_0^M) \quad \text{Eqn. (13)}$$

[00036] Furthermore, subtracting Eqn. (12) from Eqn. (11) provides the following:

$$(\Delta V_2 - \Delta V_0) = -jX_{cap} (I_2^M - I_0^M) \quad \text{Eqn. (14)}$$

[00037] Combining Eqn. (3) and Eqn. (5) and eliminating the undetermined impedance parameter Z' results in the following:

$$d = \frac{(V_1^S - V_0^S) - m(I_1^S Z_{1L} - I_0^S Z_{0L}) - (\Delta V_1 - \Delta V_0) - (V_1^R - V_0^R) + (1-m)(I_1^R Z_{1L} - I_0^R Z_{0L})}{(1-m)((I_1^S + I_1^R)Z_{1L} - (I_0^S + I_0^R)Z_{0L})} \quad \text{Eqn. (15)}$$

[00038] Substituting the expression $(\Delta V_1 - \Delta V_0)$ from Eqn. (13) into Eqn. (15) results in the following expression that can be used to determine the per unit distance “d” of the fault at location **315**:

$$d = \frac{(V_1^S - V_0^S) - m(I_1^S Z_{1L} - I_0^S Z_{0L}) + jX_{cap}(I_1^M - I_0^M) - (V_1^R - V_0^R) + (1-m)(I_1^R Z_{1L} - I_0^R Z_{0L})}{(1-m)((I_1^S + I_1^R)Z_{1L} - (I_0^S + I_0^R)Z_{0L})} \quad \text{Eqn. (16)}$$

[00039] The per unit distance “d” of the fault at location **315** can also be determined by using Eqn. (14) in lieu of Eqn. (13). Towards this end, Eqn. (4) can be combined with Eqn. (5) and the undetermined impedance parameter Z' eliminated, thus resulting in the following:

$$d = \frac{(V_2^S - V_0^S) - m(I_2^S Z_{2L} - I_0^S Z_{0L}) - (\Delta V_2 - \Delta V_0) - (V_2^R - V_0^R) + (1-m)(I_2^R Z_{2L} - I_0^R Z_{0L})}{(1-m)((I_2^S + I_2^R)Z_{2L} - (I_0^S + I_0^R)Z_{0L})}$$

Eqn. (17)

[00040] Substituting the expression $(\Delta V_2 - \Delta V_0)$ from Eqn. (14) into Eqn. (17) results in the following expression that can be alternatively used in lieu of Eqn. (16) for determining the per unit distance “d” of the fault at location **315**:

$$d = \frac{(V_2^S - V_0^S) - m(I_2^S Z_{2L} - I_0^S Z_{0L}) + jX_{cap}(I_2^M - I_0^M) - (V_2^R - V_0^R) + (1-m)(I_2^R Z_{2L} - I_0^R Z_{0L})}{(1-m)((I_2^S + I_2^R)Z_{2L} - (I_0^S + I_0^R)Z_{0L})}$$

Eqn. (18)

[00041] Equations and formulae pertaining to a double phase to ground fault condition will now be described. In this example double phase to ground fault condition, each of phase B and phase C develop fault conditions while Phase A is in a normal condition (i.e., no faults). As a result, the respective series capacitor protection elements in phases B and C are in an active state and the series capacitor protection element **115** in phase A is in an idle state (whereby current is flowing through the series capacitor **105** in Phase A and a zero (or insignificant) amount of current is flowing through the series capacitor protection element **115**). Thus, $Z_A = -jX_{cap}$ and $Z_B = Z_C =$ undetermined impedance parameter Z' . Substituting these values into Eqn. (9) results in the following:

$$\Delta V_1 = \frac{1}{3} \left[-jX_{cap}(I_0^M + I_1^M + I_2^M) + Z'(2I_1^M - I_2^M - I_0^M) \right] \quad \text{Eqn. (19)}$$

$$\Delta V_2 = \frac{1}{3} \left[-jX_{cap}(I_0^M + I_1^M + I_2^M) + Z'(2I_2^M - I_0^M - I_1^M) \right] \quad \text{Eqn. (20)}$$

$$\Delta V_0 = \frac{1}{3} \left[-jX_{cap}(I_0^M + I_1^M + I_2^M) + Z'(2I_0^M - I_1^M - I_2^M) \right] \quad \text{Eqn. (21)}$$

[00042] Adding Eqns. (19), (20) and (21) results in the following:

$$\sum_{i=0}^2 \Delta V_i = \Delta V_1 + \Delta V_2 + \Delta V_0 = -jX_{cap}(I_1^M + I_2^M + I_0^M) = -jX_{cap} \sum_{i=0}^2 I_i^M$$

Eqn. (22)

[00043] Combining Eqns. (3), (4) and (5) and eliminating the undetermined impedance parameter Z' results in the following:

$$d = \frac{\sum_{i=0}^2 V_i^S - m \sum_{i=0}^2 I_i^S Z_{iL} + jX_{cap} I_A^M - \sum_{i=0}^2 V_i^R + (1-m) \sum_{i=0}^2 I_i^R Z_{iL}}{(1-m) \sum_{i=0}^2 (I_i^S + I_i^R) Z_{iL}} \quad \text{Eqn. (23)}$$

[00044] Substituting $\sum_{i=0}^2 \Delta V_i = -jX_{cap} \sum_{i=0}^2 I_i^M$ from Eqn. (22) into Eqn. (23) results in the following expression that can be used to determine the per unit distance “d” of the double-phase-to-ground fault from the series capacitor protection element:

$$d = \frac{\sum_{i=0}^2 V_i^S - m \sum_{i=0}^2 I_i^S Z_{iL} + jX_{cap} I_A^M - \sum_{i=0}^2 V_i^R + (1-m) \sum_{i=0}^2 I_i^R Z_{iL}}{(1-m) \sum_{i=0}^2 (I_i^S + I_i^R) Z_{iL}} \quad \text{Eqn. (24)}$$

where V_i^S represents each of a zero sequence voltage component ($i = 0$) at the sending end of the three-phase series-compensated power line system, a positive sequence voltage component ($i = 1$) at the sending end of the three-phase series-compensated power line system, and a negative sequence voltage component ($i = 2$) at the sending end of the three-phase series-compensated power line system; V_i^R represents each of a zero sequence voltage component ($i = 0$) at the sending end of the three-phase series-compensated power line system, a positive sequence voltage component ($i = 1$) at the sending end of the three-phase series-compensated power line system, and a negative sequence voltage component ($i = 2$) at the sending end of the three-phase series-compensated power line system; I_i^S represents each of a zero sequence current component ($i = 0$) at the sending end of the three-phase series-compensated power line system, a positive sequence current component ($i = 1$) at the sending end of the three-phase series-compensated power line system, and a negative sequence current component ($i = 2$) at the sending end of the three-phase series-compensated power line system; I_i^R represents each of a zero sequence current component ($i = 0$) at the receiving end of the three-phase series-compensated power line system, a positive sequence current component ($i = 1$) at the receiving end of the three-phase series-compensated power line system, and a negative sequence current component ($i = 2$) at the receiving end of the three-phase series-compensated power line system; Z_{iL} represents each of a zero sequence total impedance component ($i = 0$), a positive sequence total impedance component ($i = 1$) of the three-phase series-compensated power line

system, and a negative sequence total impedance component ($i = 2$) of the three-phase series-compensated power line system, I_0^M is an estimated zero sequence current component propagating through the first, second, and third compensating capacitor systems, I_1^M is an estimated positive sequence current component propagating through the first, second, and third compensating capacitor systems, and I_2^M is an estimated negative sequence current component propagating through the first, second, and third compensating capacitor systems.

[00045] Attention is now drawn to FIG. 5, which illustrates a few example components that can be included in the line fault location detector **120** in accordance with an exemplary embodiment of the disclosure. In this exemplary embodiment, the line fault location detector **120** can include a number of input interfaces that are configured to receive various kinds of input data and can also include a number of output interfaces that are configured to transmit various kinds of signals such as control signals and fault location related signals to other devices (not shown) such as an alarm monitoring unit, a display unit, a user interface device, and/or an alarm. Among the exemplary input interfaces shown, a first input interface **505** can be configured to receive a set of electrical current measurements and a set of voltage measurements (via a link **501**) from one of the three-phase series-compensated power transmission lines of the series-compensated power transmission line system **100**. For example, the link **501** can represent one line from each of links **126** and **127** (shown in FIG. 1) that are coupled to a sending end of the series-compensated power transmission line system **100** and one line from each of links **128** and **129** (shown in FIG. 1) that are coupled to a receiving end of the series-compensated power transmission line system **100** (total of 4 lines) can be coupled into the first input interface **505**.

[00046] It should be understood that this coupling configuration is merely one example among many, and in other configurations, the first input interface **505** can have fewer or larger number of circuits that are coupled to fewer or larger number of monitoring elements associated with the series-compensated power transmission line system **100**. Accordingly, the first input interface **505** can include appropriate circuitry for receiving and processing various types of signals. For example, with respect to the example system configuration shown in FIG. 1, the first input interface **505** can include communications interfaces configured to receive electrical current measurements and voltage measurements in a first digital communications format via the lines **126** and **127** from the sending end of the series-compensated power transmission line system **100**, and can further include one or more different types of interface for receiving other electrical current measurements and voltage measurements via the lines **128** and **129** in a second digital communications format (or an analog format), from the receiving end of the series-compensated power transmission line system **100**.

[00047] The second interface **520** and the third interface **540** can be configured similar to the

first input interface **505** in order receive electrical current measurements and voltage measurements from the other two of the three-phase series-compensated power transmission lines of the series-compensated power transmission line system **100** (via the links **502** and **503**).

[00048] The line fault location detector **120** can include one or more output interfaces such as an output interface **535** that can be used for transmitting via line **504** various status and/or control signals. The line fault location detector **120** can also include one or more analog-to-digital converters and one or more digital-to-analog converters (not shown). For example, an analog-to-digital converter **515** can be used to convert an electrical current measurement provided by one of the input interfaces in an analog form into a digital current measurement value that can be processed by the processor **555**. Conversely, a digital-to-analog converter can be used to convert various types of digital information that can be provided by the processor **555**, into an analog output signal that can be transmitted out of the line fault location detector **120** via the output interface **504**. A signal processing module **530** can be used to process digital signals, provided by the analog-to-digital converter **515** for example.

[00049] One or more relays, such as a relay **560**, can be used for various types of switching purposes. For example, the relay **560** can be used to switch various currents and/or alarm signals when a fault is detected in the series-compensated power transmission line system **100**. A fault type detector **550** can be used for identifying the nature of a fault in the series-compensated power transmission line system **100** such as a short-circuit to ground. A synchronization module **545** can be used to ensure that the various electrical current measurements and the voltage measurements specifically relate to synchronous measurements that are carried out at the sending end and the receiving end of the series-compensated power transmission line system **100**. As can be understood, the synchronous fault-related measurements are obtained by concurrently executing a synchronous measurement procedure at both the sending end and the receiving end of the series-compensated power transmission line system **100**. In one example implementation, the various electrical current measurements and the voltage measurements can be provided to the line fault location detector **120** in the form of synchrophasors. The synchrophasors, which represent time-synchronized measurement data indicative of both magnitude information and phase information of the various electrical current measurements and the voltage measurements, can be obtained via phasor measurement units (PMUs) for example.

[00050] One or more processors, such as the processor **555**, can be configured to communicatively cooperate with various elements contained in the line fault location detector **120**, including a memory **525**. The processor **555** can be implemented and operated using appropriate hardware, software, firmware, or combinations thereof. Software or firmware implementations can

include computer-executable or machine-executable instructions written in any suitable programming language to perform the various functions described. In one embodiment, instructions associated with a function block language can be stored in the memory **525** and executed by the processor **555**.

[00051] The memory **525** can be used to store program instructions that are loadable and executable by the processor **555**, as well as to store data generated during the execution of these programs. Depending on the configuration and type of the line fault location detector **120**, the memory **525** can be volatile (such as random access memory (RAM)) and/or non-volatile (such as read-only memory (ROM), flash memory, etc.). In some embodiments, the memory devices can also include additional removable storage (not shown) and/or non-removable storage (not shown) including, but not limited to, magnetic storage, optical disks, and/or tape storage. The disk drives and their associated computer-readable media can provide non-volatile storage of computer-readable instructions, data structures, program modules, and other data. In some implementations, the memory **525** can include multiple different types of memory, such as static random access memory (SRAM), dynamic random access memory (DRAM), or ROM.

[00052] The memory **525**, the removable storage, and the non-removable storage are all examples of non-transient computer-readable storage media. Such non-transient computer-readable storage media can be implemented in any method or technology for storage of information such as computer-readable instructions, data structures, program modules or other data. Additional types of non-transient computer storage media that can be present include, but are not limited to, programmable random access memory (PRAM), SRAM, DRAM, ROM, electrically erasable programmable read-only memory (EEPROM), compact disc read-only memory (CD-ROM), digital versatile discs (DVD) or other optical storage, magnetic cassettes, magnetic tapes, magnetic disk storage or other magnetic storage devices, or any other medium which can be used to store the desired information and which can be accessed by the processor **555**. Combinations of any of the above should also be included within the scope of non-transient computer-readable media.

[00053] Turning to the contents of the memory **525**, the memory **525** can include, but is not limited to, an operating system (OS) and one or more application programs or services for implementing the features and aspects disclosed herein. Such applications or services can include a line fault location detector module (not shown). In one embodiment, the line fault location detector module can be implemented by software that is provided in configurable control block language and is stored in non-volatile memory. When executed by the processor **555**, the line fault location detector module can implement the various functionalities and features described in this disclosure.

[00054] Many modifications and other embodiments of the example descriptions set forth

herein to which these descriptions pertain will come to mind having the benefit of the teachings presented in the foregoing descriptions and the associated drawings. Thus, it will be appreciated the disclosure may be embodied in many forms and should not be limited to the exemplary embodiments described above. Therefore, it is to be understood that the disclosure is not to be limited to the specific embodiments disclosed and that modifications and other embodiments are intended to be included within the scope of the appended claims. Although specific terms are employed herein, they are used in a generic and descriptive sense only and not for purposes of limitation.

CLAIMS

What is Claimed:

1. A three-phase series-compensated power line system comprising:
 - a first series-compensated power transmission line configured to propagate electrical power having a first phase, the first series-compensated power transmission line including a first compensating capacitor system comprising a first series capacitor and a first series capacitor protection element;
 - a second series-compensated power transmission line configured to propagate electrical power having a second phase, the second series-compensated power transmission line including a second compensating capacitor system comprising a second series capacitor and a second series capacitor protection element;
 - a third series-compensated power transmission line configured to propagate electrical power having a third phase, the third series-compensated power transmission line including a third compensating capacitor system comprising a third series capacitor and a third series capacitor protection element; and
 - a line fault location detector comprising at least one processor, the at least one processor configured to execute a first fault location procedure for identifying a location of a single-phase-to-ground fault in the three-phase series-compensated power line system, the first fault location procedure comprising:
 - determining a zero sequence voltage drop based in part on a relationship between a first impedance presented by the first compensating capacitor system during the single-phase-to-ground fault, a second impedance presented by the second compensating capacitor system during the single-phase-to-ground fault, and a third impedance presented by the third compensating capacitor system during the single-phase-to-ground fault, wherein one of the first impedance, the second impedance, or the third impedance is an undetermined impedance that is attributable to a corresponding one of the first series capacitor protection element, the second series capacitor protection element, or the third series capacitor protection element turning active during the single-phase-to-ground fault;
 - determining at least one of a positive sequence voltage drop or a negative sequence voltage drop based in part on the relationship between the first impedance, the second impedance, and the third impedance; and
 - determining the location of the single-phase-to-ground fault at least in part, by using the zero sequence voltage drop and the at least one of the positive sequence voltage drop or the negative

sequence voltage drop to eliminate determining of the undetermined impedance.

2. The system of claim 1, wherein executing the first fault location procedure further comprises receiving in the line fault location detector, a plurality of electrical current measurements and a plurality of voltage measurements obtained by using a synchronous measurement procedure concurrently executed at a sending end and a receiving end of the first series-compensated power transmission line.

3. The system of claim 2, wherein executing the first fault location procedure precludes calculating an impedance value of any of the first series capacitor protection element, the second series capacitor protection element, or the third series capacitor protection element; precludes monitoring a status of any of the first, second, or third series capacitor protection elements; and precludes measuring a voltage drop across any of the first, second, or third series capacitors.

4. The system of claim 2, wherein the line fault location detector is located closer to the receiving end than the sending end of the three-phase series-compensated power line system.

5. The system of claim 1, wherein using the zero sequence voltage drop and the at least one of the positive sequence voltage drop or the negative sequence voltage drop for determining the location of the single-phase-to-ground fault comprises subtracting the zero sequence voltage drop from the positive sequence voltage drop and further comprises solving the following equation:

$$dl = \frac{(V_1^S - V_0^S) - m(I_1^S Z_{1L} - I_0^S Z_{0L}) + jX_{cap}(I_1^M - I_0^M) - (V_1^R - V_0^R) + (1-m)(I_1^R Z_{1L} - I_0^R Z_{0L})}{(1-m)((I_1^S + I_1^R)Z_{1L} - (I_0^S + I_0^R)Z_{0L})}$$

wherein dl is indicative of a distance to the single-phase-to-ground fault location, V_0^S is a zero sequence voltage component at a sending end of the three-phase series-compensated power line system, V_1^S is a positive sequence voltage component at the sending end of the three-phase series-compensated power line system, I_0^S is a zero sequence current component at the sending end of the first series-compensated power transmission line, I_1^S is a positive sequence current component at the sending end of the three-phase series-compensated power line system, V_0^R is a zero sequence voltage component at a receiving end of the three-phase series-compensated power line system, V_1^R is a positive sequence voltage component at the receiving end of the three-phase series-compensated power line system, I_0^R is a zero sequence current component at the receiving end of the three-phase series-compensated power line system, I_1^R is a positive sequence current component at the receiving end of the three-phase series-compensated power line system, Z_{0L} is a zero sequence total impedance

component of the three-phase series-compensated power line system, Z_{1L} is a positive sequence total impedance component of the three-phase series-compensated power line system, I_0^M is an estimated zero sequence current component propagating through the first, second, and third compensating capacitor systems, and I_1^M is an estimated positive sequence current component propagating through the first, second, and third compensating capacitor systems.

6. The system of claim 1, wherein using the zero sequence voltage drop and the at least one of the positive sequence voltage drop or the negative sequence voltage drop for determining the location of the single-phase-to-ground fault comprises subtracting the zero sequence voltage drop from the negative sequence voltage drop and further comprises solving the following equation:

$$d1 = \frac{(V_2^S - V_0^S) - m(I_2^S Z_{2L} - I_0^S Z_{0L}) + jX_{cap}(I_2^M - I_0^M) - (V_2^R - V_0^R) + (1-m)(I_2^R Z_{2L} - I_0^R Z_{0L})}{(1-m)((I_2^S + I_2^R)Z_{2L} - (I_0^S + I_0^R)Z_{0L})}$$

wherein $d1$ is indicative of a distance to the single-phase-to-ground fault location, V_0^S is a zero sequence voltage component at a sending end of the three-phase series-compensated power line system, V_2^S is a negative sequence voltage component at the sending end of the three-phase series-compensated power line system, I_0^S is a zero sequence current component at the sending end of the first series-compensated power transmission line, I_2^S is a negative sequence current component at the sending end of the three-phase series-compensated power line system, V_0^R is a zero sequence voltage component at a receiving end of the three-phase series-compensated power line system, V_2^R is a negative sequence voltage component at the receiving end of the three-phase series-compensated power line system, I_0^R is a zero sequence current component at the receiving end of the three-phase series-compensated power line system, I_2^R is a negative sequence current component at the receiving end of the three-phase series-compensated power line system, Z_{0L} is a zero sequence total impedance component of the three-phase series-compensated power line system, Z_{2L} is a negative sequence total impedance component of the three-phase series-compensated power line system, I_0^M is an estimated zero sequence current component propagating through the first, second, and third compensating capacitor systems, and I_2^M is an estimated negative sequence current component propagating through the first, second, and third compensating capacitor systems.

7. The system of claim 1, wherein the at least one processor of the line fault location detector is further configured to execute a second fault location procedure for identifying a location of a double-phase-to-ground fault in the three-phase series-compensated power line system, the double-phase-to-ground fault characterized in part by any two of the first series capacitor protection element,

the second series capacitor protection element, and the third series capacitor protection element turning active.

8. The system of claim 7, wherein executing the second fault location procedure comprises solving the following equation:

$$d2 = \frac{\sum_{i=0}^2 V_i^S - m \sum_{i=0}^2 I_i^S Z_{iL} + jX_{cap} I_A^M - \sum_{i=0}^2 V_i^R + (1-m) \sum_{i=0}^2 I_i^R Z_{iL}}{(1-m) \sum_{i=0}^2 (I_i^S + I_i^R) Z_{iL}}$$

wherein $d2$ is indicative of a distance to the double-phase-to-ground fault; V_i^S represents each of a zero sequence voltage component ($i = 0$) at the sending end of the three-phase series-compensated power line system, a positive sequence voltage component ($i = 1$) at the sending end of the three-phase series-compensated power line system, and a negative sequence voltage component ($i = 2$) at the sending end of the three-phase series-compensated power line system; V_i^R represents each of a zero sequence voltage component ($i = 0$) at the sending end of the three-phase series-compensated power line system, a positive sequence voltage component ($i = 1$) at the sending end of the three-phase series-compensated power line system, and a negative sequence voltage component ($i = 2$) at the sending end of the three-phase series-compensated power line system; I_i^S represents each of a zero sequence current component ($i = 0$) at the sending end of the three-phase series-compensated power line system, a positive sequence current component ($i = 1$) at the sending end of the three-phase series-compensated power line system, and a negative sequence current component ($i = 2$) at the sending end of the three-phase series-compensated power line system; I_i^R represents each of a zero sequence current component ($i = 0$) at the receiving end of the three-phase series-compensated power line system, a positive sequence current component ($i = 1$) at the receiving end of the three-phase series-compensated power line system, and a negative sequence current component ($i = 2$) at the receiving end of the three-phase series-compensated power line system; Z_{iL} represents each of a zero sequence total impedance component ($i = 0$), a positive sequence total impedance component ($i = 1$) of the three-phase series-compensated power line system, and a negative sequence total impedance component ($i = 2$) of the three-phase series-compensated power line system, I_0^M is an estimated zero sequence current component propagating through the first, second, and third compensating capacitor systems, I_1^M is an estimated positive sequence current component propagating through the first, second, and third compensating capacitor systems, and I_2^M is an estimated negative sequence current component propagating through the first, second, and third

compensating capacitor systems.

9. The system of claim 8, wherein executing the second fault location procedure precludes calculating an impedance value of any of the first series capacitor protection element, the second series capacitor protection element, or the third series capacitor protection element; precludes monitoring a status of any of the first, second, or third series capacitor protection elements; and precludes measuring a voltage drop across any of the first, second, or third series capacitors.

10. A line fault location detector coupled to a three-phase series-compensated power line system, the line fault location detector comprising:

a plurality of input interfaces configured to receive a set of electrical current measurements and a set of voltage measurements that are obtained via a synchronous measurement procedure concurrently executed at a sending end and a receiving end of the three-phase series-compensated power transmission line system; and

at least one processor configured to use the set of electrical current measurements and the set of voltage measurements to execute a first fault location procedure for identifying a location of a single-phase-to-ground fault in the three-phase series-compensated power line system, the first fault location procedure comprising:

determining a zero sequence voltage drop based in part on a relationship between a first impedance presented by the first compensating capacitor system during the single-phase-to-ground fault, a second impedance presented by the second compensating capacitor system during the single-phase-to-ground fault, and a third impedance presented by the third compensating capacitor system during the single-phase-to-ground fault, wherein one of the first impedance, the second impedance, or the third impedance is an undetermined impedance that is attributable to a corresponding one of the first series capacitor protection element, the second series capacitor protection element, or the third series capacitor protection element turning active during the single-phase-to-ground fault;

determining at least one of a positive sequence voltage drop or a negative sequence voltage drop based in part on the relationship between the first impedance, the second impedance, and the third impedance; and

determining the location of the single-phase-to-ground fault at least in part, by using the zero sequence voltage drop and the at least one of the positive sequence voltage drop or the negative sequence voltage drop to eliminate determining of the undetermined impedance.

11. The detector of claim 10, wherein using the zero sequence voltage drop and the at least

one of the positive sequence voltage drop or the negative sequence voltage drop for determining the location of the single-phase-to-ground fault comprises subtracting the zero sequence voltage drop from the positive sequence voltage drop and further comprises solving the following equation:

$$dl = \frac{(V_1^S - V_0^S) - m(I_1^S Z_{1L} - I_0^S Z_{0L}) + jX_{cap}(I_1^M - I_0^M) - (V_1^R - V_0^R) + (1-m)(I_1^R Z_{1L} - I_0^R Z_{0L})}{(1-m)((I_1^S + I_1^R)Z_{1L} - (I_0^S + I_0^R)Z_{0L})}$$

wherein dl is indicative of a distance to the single-phase-to-ground fault location, V_0^S is a zero sequence voltage component at a sending end of the three-phase series-compensated power line system, V_1^S is a positive sequence voltage component at the sending end of the three-phase series-compensated power line system, I_0^S is a zero sequence current component at the sending end of the first series-compensated power transmission line, I_1^S is a positive sequence current component at the sending end of the three-phase series-compensated power line system, V_0^R is a zero sequence voltage component at a receiving end of the three-phase series-compensated power line system, V_1^R is a positive sequence voltage component at the receiving end of the three-phase series-compensated power line system, I_0^R is a zero sequence current component at the receiving end of the three-phase series-compensated power line system, I_1^R is a positive sequence current component at the receiving end of the three-phase series-compensated power line system, Z_{0L} is a zero sequence total impedance component of the three-phase series-compensated power line system, Z_{1L} is a positive sequence total impedance component of the three-phase series-compensated power line system, I_0^M is an estimated zero sequence current component propagating through the first, second, and third compensating capacitor systems, and I_1^M is an estimated positive sequence current component propagating through the first, second, and third compensating capacitor systems.

12. The detector of claim 10, wherein using the zero sequence voltage drop and the at least one of the positive sequence voltage drop or the negative sequence voltage drop for determining the location of the single-phase-to-ground fault comprises subtracting the zero sequence voltage drop from the negative sequence voltage drop and further comprises solving the following equation:

$$dl = \frac{(V_2^S - V_0^S) - m(I_2^S Z_{2L} - I_0^S Z_{0L}) + jX_{cap}(I_2^M - I_0^M) - (V_2^R - V_0^R) + (1-m)(I_2^R Z_{2L} - I_0^R Z_{0L})}{(1-m)((I_2^S + I_2^R)Z_{2L} - (I_0^S + I_0^R)Z_{0L})}$$

wherein dl is indicative of a distance to the single-phase-to-ground fault location, V_0^S is a zero sequence voltage component at a sending end of the three-phase series-compensated power line system, V_2^S is a negative sequence voltage component at the sending end of the three-phase series-compensated power line system, I_0^S is a zero sequence current component at the sending end of the

first series-compensated power transmission line, I_2^S is a negative sequence current component at the sending end of the three-phase series-compensated power line system, V_0^R is a zero sequence voltage component at a receiving end of the three-phase series-compensated power line system, V_2^R is a negative sequence voltage component at the receiving end of the three-phase series-compensated power line system, I_0^R is a zero sequence current component at the receiving end of the three-phase series-compensated power line system, I_2^R is a negative sequence current component at the receiving end of the three-phase series-compensated power line system, Z_{0L} is a zero sequence total impedance component of the three-phase series-compensated power line system, Z_{2L} is a negative sequence total impedance component of the three-phase series-compensated power line system, I_0^M is an estimated zero sequence current component propagating through the first, second, and third compensating capacitor systems, and I_2^M is an estimated negative sequence current component propagating through the first, second, and third compensating capacitor systems.

13. The detector of claim 10, wherein the at least one processor is further configured to execute a second fault location procedure for identifying a location of a double-phase-to-ground fault in the three-phase series-compensated power line system, the double-phase-to-ground fault characterized in part by any two of the first series capacitor protection element, the second series capacitor protection element, and the third series capacitor protection element turning active.

14. The detector of claim 13, wherein executing the second fault location procedure comprises solving the following equation:

$$d2 = \frac{\sum_{i=0}^2 V_i^S - m \sum_{i=0}^2 I_i^S Z_{iL} + jX_{cap} I_A^M - \sum_{i=0}^2 V_i^R + (1-m) \sum_{i=0}^2 I_i^R Z_{iL}}{(1-m) \sum_{i=0}^2 (I_i^S + I_i^R) Z_{iL}}$$

wherein $d2$ is indicative of a distance to the double-phase-to-ground fault; V_i^S represents each of a zero sequence voltage component ($i = 0$) at the sending end of the three-phase series-compensated power line system, a positive sequence voltage component ($i = 1$) at the sending end of the three-phase series-compensated power line system, and a negative sequence voltage component ($i = 2$) at the sending end of the three-phase series-compensated power line system; V_i^R represents each of a zero sequence voltage component ($i = 0$) at the sending end of the three-phase series-compensated power line system, a positive sequence voltage component ($i = 1$) at the sending end of the three-phase series-compensated power line system, and a negative sequence voltage component

($i = 2$) at the sending end of the three-phase series-compensated power line system; I_i^S represents each of a zero sequence current component ($i = 0$) at the sending end of the three-phase series-compensated power line system, a positive sequence current component ($i = 1$) at the sending end of the three-phase series-compensated power line system, and a negative sequence current component ($i = 2$) at the sending end of the three-phase series-compensated power line system; I_i^R represents each of a zero sequence current component ($i = 0$) at the receiving end of the three-phase series-compensated power line system, a positive sequence current component ($i = 1$) at the receiving end of the three-phase series-compensated power line system, and a negative sequence current component ($i = 2$) at the receiving end of the three-phase series-compensated power line system; Z_{iL} represents each of a zero sequence total impedance component ($i = 0$), a positive sequence total impedance component ($i = 1$) of the three-phase series-compensated power line system, and a negative sequence total impedance component ($i = 2$) of the three-phase series-compensated power line system, I_0^M is an estimated zero sequence current component propagating through the first, second, and third compensating capacitor systems, I_1^M is an estimated positive sequence current component propagating through the first, second, and third compensating capacitor systems, and I_2^M is an estimated negative sequence current component propagating through the first, second, and third compensating capacitor systems.

15. The detector of claim 14, wherein executing the second fault location procedure precludes calculating an impedance value of any of the first series capacitor protection element, the second series capacitor protection element, or the third series capacitor protection element; precludes monitoring a status of any of the first, second, or third series capacitor protection elements; and precludes measuring a voltage drop across any of the first, second, or third series capacitors.

16. A method comprising:

executing a synchronous measurement procedure concurrently at a sending end and a receiving end of a three-phase series-compensated power transmission line system for obtaining a set of electrical current measurements and a set of voltage measurements;

receiving in a line fault location detector, the set of electrical current measurements and the set of voltage measurements based on the synchronous measurement procedure; and

using at least one processor in the line fault location detector to execute a first fault location procedure for identifying a location of a single-phase-to-ground fault in the three-phase series-compensated power line system, the first fault location procedure comprising:

determining a zero sequence voltage drop based in part on a relationship between a first

impedance presented by the first compensating capacitor system during the single-phase-to-ground fault, a second impedance presented by the second compensating capacitor system during the single-phase-to-ground fault, and a third impedance presented by the third compensating capacitor system during the single-phase-to-ground fault, wherein one of the first impedance, the second impedance, or the third impedance is an undetermined impedance that is attributable to a corresponding one of the first series capacitor protection element, the second series capacitor protection element, or the third series capacitor protection element turning active during the single-phase-to-ground fault;

determining at least one of a positive sequence voltage drop or a negative sequence voltage drop based in part on the relationship between the first impedance, the second impedance, and the third impedance; and

determining the location of the single-phase-to-ground fault at least in part, by using the zero sequence voltage drop and the at least one of the positive sequence voltage drop or the negative sequence voltage drop to eliminate determining of the undetermined impedance.

17. The method of claim 16, wherein using the zero sequence voltage drop and the at least one of the positive sequence voltage drop or the negative sequence voltage drop for determining the location of the single-phase-to-ground fault comprises subtracting the zero sequence voltage drop from the positive sequence voltage drop and further comprises solving the following equation:

$$dl = \frac{(V_1^S - V_0^S) - m(I_1^S Z_{1L} - I_0^S Z_{0L}) + jX_{cap}(I_1^M - I_0^M) - (V_1^R - V_0^R) + (1-m)(I_1^R Z_{1L} - I_0^R Z_{0L})}{(1-m)((I_1^S + I_1^R)Z_{1L} - (I_0^S + I_0^R)Z_{0L})}$$

wherein dl is indicative of a distance to the single-phase-to-ground fault location, V_0^S is a zero sequence voltage component at a sending end of the three-phase series-compensated power line system, V_1^S is a positive sequence voltage component at the sending end of the three-phase series-compensated power line system, I_0^S is a zero sequence current component at the sending end of the first series-compensated power transmission line, I_1^S is a positive sequence current component at the sending end of the three-phase series-compensated power line system, V_0^R is a zero sequence voltage component at a receiving end of the three-phase series-compensated power line system, V_1^R is a positive sequence voltage component at the receiving end of the three-phase series-compensated power line system, I_0^R is a zero sequence current component at the receiving end of the three-phase series-compensated power line system, I_1^R is a positive sequence current component at the receiving end of the three-phase series-compensated power line system, Z_{0L} is a zero sequence total impedance component of the three-phase series-compensated power line system, Z_{1L} is a positive sequence total impedance component of the three-phase series-compensated power line system, I_0^M is an estimated

zero sequence current component propagating through the first, second, and third compensating capacitor systems, and I_1^M is an estimated positive sequence current component propagating through the first, second, and third compensating capacitor systems.

18. The method of claim 16, wherein using the zero sequence voltage drop and the at least one of the positive sequence voltage drop or the negative sequence voltage drop for determining the location of the single-phase-to-ground fault comprises subtracting the zero sequence voltage drop from the negative sequence voltage drop and further comprises solving the following equation:

$$d1 = \frac{(V_2^S - V_0^S) - m(I_2^S Z_{2L} - I_0^S Z_{0L}) + jX_{cap}(I_2^M - I_0^M) - (V_2^R - V_0^R) + (1-m)(I_2^R Z_{2L} - I_0^R Z_{0L})}{(1-m)((I_2^S + I_2^R)Z_{2L} - (I_0^S + I_0^R)Z_{0L})}$$

wherein $d1$ is indicative of a distance to the single-phase-to-ground fault location, V_0^S is a zero sequence voltage component at a sending end of the three-phase series-compensated power line system, V_2^S is a negative sequence voltage component at the sending end of the three-phase series-compensated power line system, I_0^S is a zero sequence current component at the sending end of the first series-compensated power transmission line, I_2^S is a negative sequence current component at the sending end of the three-phase series-compensated power line system, V_0^R is a zero sequence voltage component at a receiving end of the three-phase series-compensated power line system, V_2^R is a negative sequence voltage component at the receiving end of the three-phase series-compensated power line system, I_0^R is a zero sequence current component at the receiving end of the three-phase series-compensated power line system, I_2^R is a negative sequence current component at the receiving end of the three-phase series-compensated power line system, Z_{0L} is a zero sequence total impedance component of the three-phase series-compensated power line system, Z_{2L} is a negative sequence total impedance component of the three-phase series-compensated power line system, I_0^M is an estimated zero sequence current component propagating through the first, second, and third compensating capacitor systems, and I_2^M is an estimated negative sequence current component propagating through the first, second, and third compensating capacitor systems.

19. The method of claim 16, wherein the at least one processor is further configured to execute a second fault location procedure for identifying a location of a double-phase-to-ground fault in the three-phase series-compensated power line system, the double-phase-to-ground fault characterized in part by any two of the first series capacitor protection element, the second series capacitor protection element, and the third series capacitor protection element turning active.

20. The method of claim 19, wherein executing the second fault location procedure

comprises solving the following equation:

$$d2 = \frac{\sum_{i=0}^2 V_i^S - m \sum_{i=0}^2 I_i^S Z_{iL} + jX_{cap} I_A^M - \sum_{i=0}^2 V_i^R + (1-m) \sum_{i=0}^2 I_i^R Z_{iL}}{(1-m) \sum_{i=0}^2 (I_i^S + I_i^R) Z_{iL}}$$

wherein $d2$ is indicative of a distance to the double-phase-to-ground fault; V_i^S represents each of a zero sequence voltage component ($i = 0$) at the sending end of the three-phase series-compensated power line system, a positive sequence voltage component ($i = 1$) at the sending end of the three-phase series-compensated power line system, and a negative sequence voltage component ($i = 2$) at the sending end of the three-phase series-compensated power line system; V_i^R represents each of a zero sequence voltage component ($i = 0$) at the sending end of the three-phase series-compensated power line system, a positive sequence voltage component ($i = 1$) at the sending end of the three-phase series-compensated power line system, and a negative sequence voltage component ($i = 2$) at the sending end of the three-phase series-compensated power line system; I_i^S represents each of a zero sequence current component ($i = 0$) at the sending end of the three-phase series-compensated power line system, a positive sequence current component ($i = 1$) at the sending end of the three-phase series-compensated power line system, and a negative sequence current component ($i = 2$) at the sending end of the three-phase series-compensated power line system; I_i^R represents each of a zero sequence current component ($i = 0$) at the receiving end of the three-phase series-compensated power line system, a positive sequence current component ($i = 1$) at the receiving end of the three-phase series-compensated power line system, and a negative sequence current component ($i = 2$) at the receiving end of the three-phase series-compensated power line system; Z_{iL} represents each of a zero sequence total impedance component ($i = 0$), a positive sequence total impedance component ($i = 1$) of the three-phase series-compensated power line system, and a negative sequence total impedance component ($i = 2$) of the three-phase series-compensated power line system, I_0^M is an estimated zero sequence current component propagating through the first, second, and third compensating capacitor systems, I_1^M is an estimated positive sequence current component propagating through the first, second, and third compensating capacitor systems, and I_2^M is an estimated negative sequence current component propagating through the first, second, and third compensating capacitor systems.

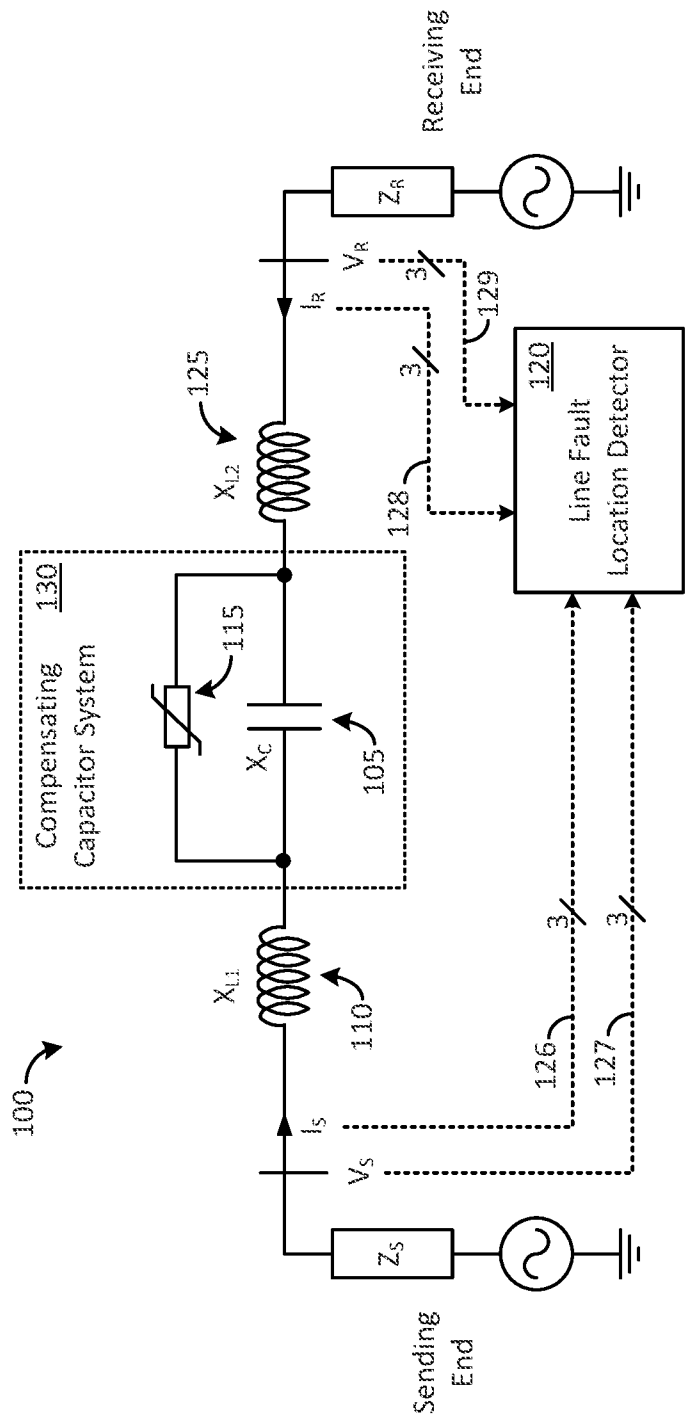


FIG. 1

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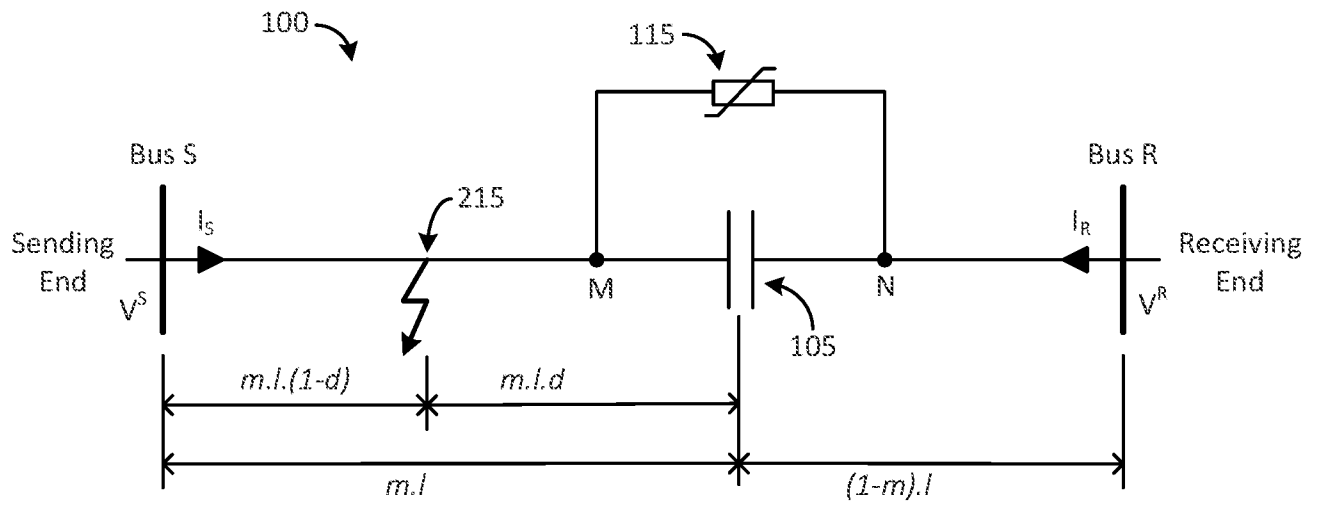


FIG. 2

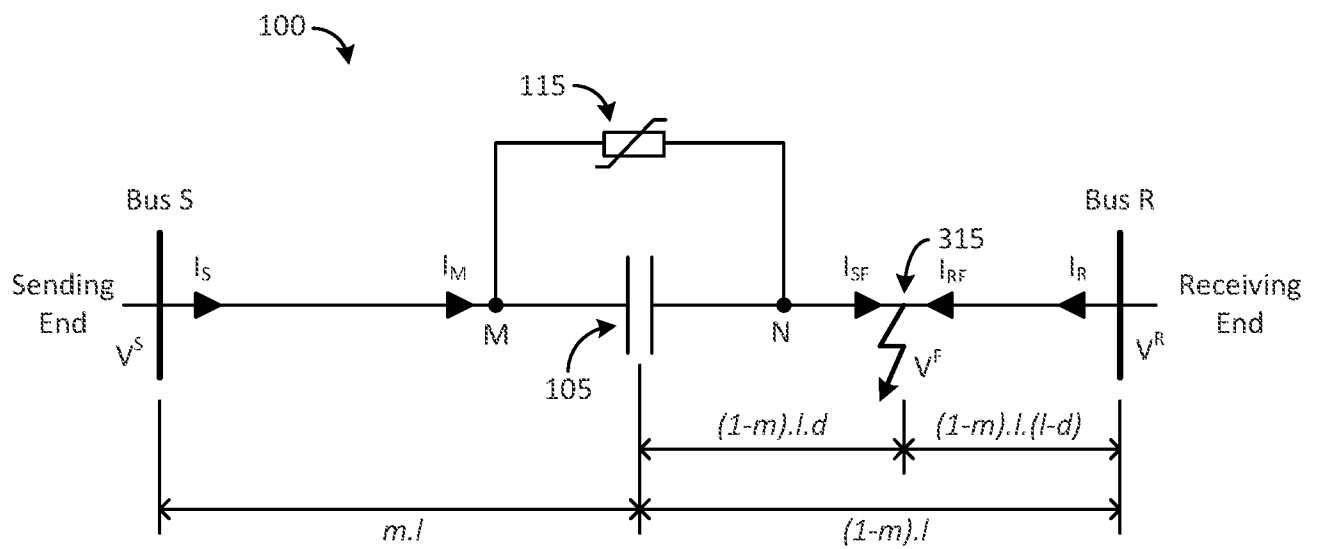


FIG. 3

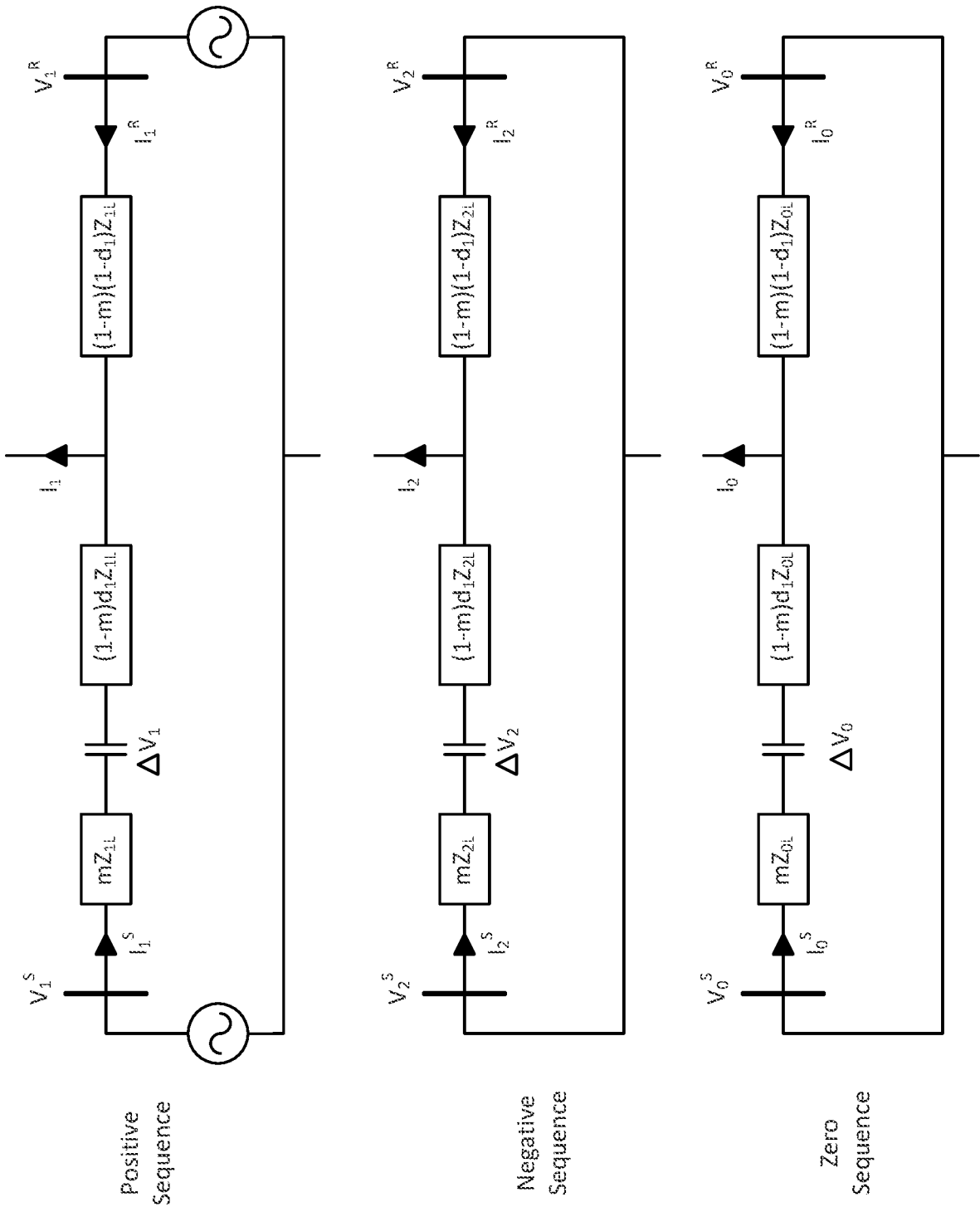


FIG. 4

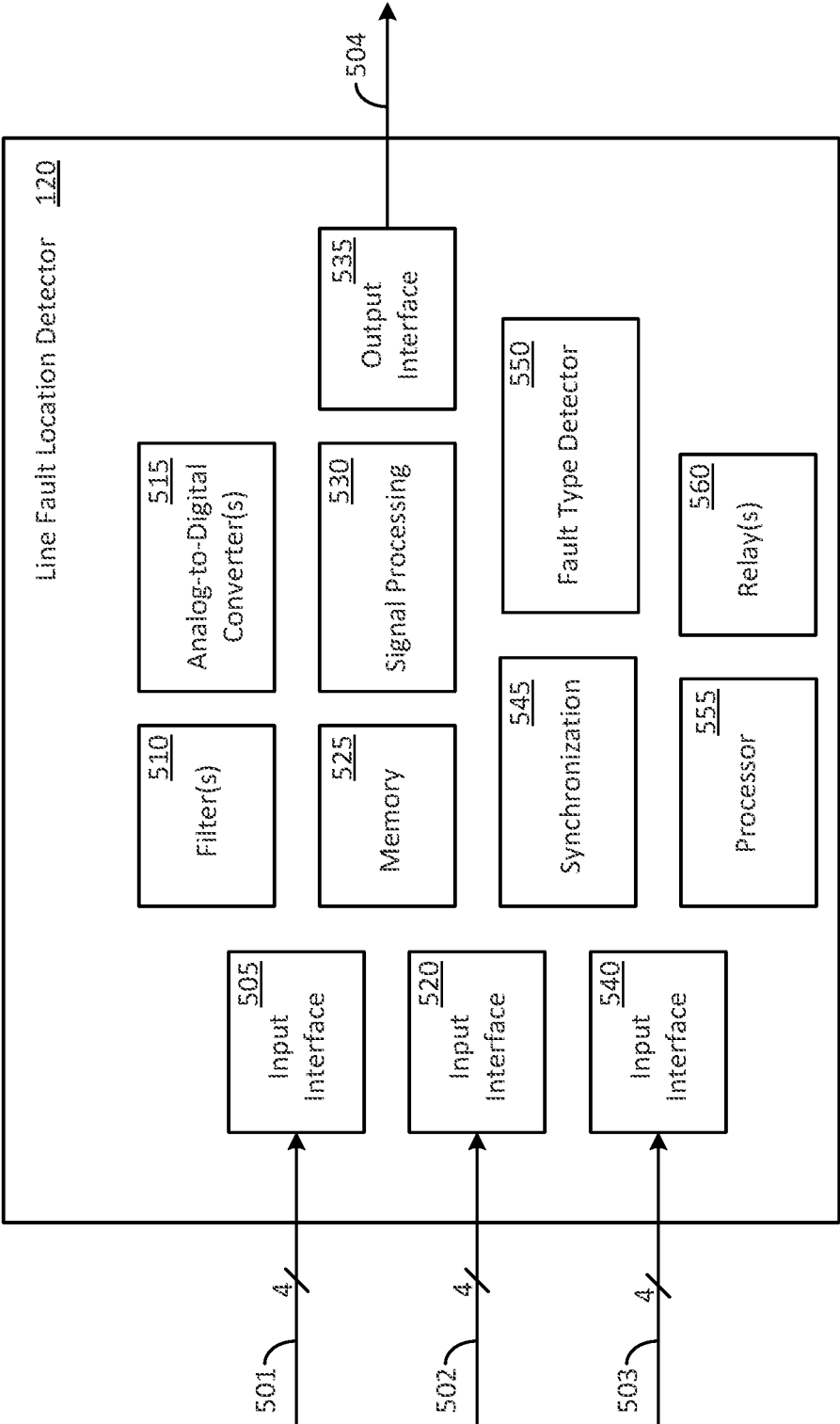


FIG. 5

INTERNATIONAL SEARCH REPORT

International application No
PCT/US2017/016915

A. CLASSIFICATION OF SUBJECT MATTER
INV. G01R31/08
ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
G01R

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 2011/082653 A1 (BALCEREK PRZEMYSŁAW [PL] ET AL) 7 April 2011 (2011-04-07) paragraphs [0001], [0018], [0052]; claim 1; figure 1	1-20
A	US 2011/178741 A1 (SAHA MURARI [SE]) 21 July 2011 (2011-07-21) paragraphs [0079], [0122] - [0125]; figures 1-3	1-20
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Further documents are listed in the continuation of Box C.



See patent family annex.

* Special categories of cited documents :

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"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"&" document member of the same patent family

Date of the actual completion of the international search

28 April 2017

Date of mailing of the international search report

11/05/2017

Name and mailing address of the ISA/

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O'Callaghan, D

INTERNATIONAL SEARCH REPORT

International application No
PCT/US2017/016915

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	FECTEAU C: "Accurate fault location algorithm for series compensated lines using two-terminal unsynchronized measurements and hydro-quebec's field experience", ANNUAL WESTERN PROTECTIVE RELAY CONFERENCE,, vol. 33, 1 January 2006 (2006-01-01), pages 1-16, XP007906022, page 2, left side, paragraph 2 to page 8, right side, paragraph 2; figures 1,5	1-20
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INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/US2017/016915

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