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(54) **WIRELESS DUPLEX OPTICAL COMMUNICATION SYSTEM**

DRAHTLOSES OPTISCHES DUPLEXKOMMUNIKATIONSSYSTEM

SYSTEME DE COMMUNICATION OPTIQUE SANS FIL EN DUPLEX

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- **PATENT ABSTRACTS OF JAPAN vol. 1995, no. 10, 30 November 1995 (1995-11-30) & JP 07 177092 A (KOKUSAI ELECTRIC CO LTD), 14 July 1995 (1995-07-14)**

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Description

[0001] The invention relates to wireless optical communication systems and can be used in digital communication systems, in particular for wireless information exchange, e.g. between computers that are moving in relation to each other, or are divided by a barrier impeding the use of wireless communication means.

[0002] An optical communication system is known, which uses two terminals located on the ends of an optical communication line formed thereby. Each terminal includes a combination of laser transmitters, which emit a set of laser beams carrying information signals received at the other terminal which are summed up incoherently. However such systems must use laser transmitters in order to operate for long periods, these are expensive and technically complex.

[0003] An optical communication system is known, which provides for wireless information exchange and contains the transmitting and receiving components made in the form of an optical transmitter and an optical receiver. The problem with this known system is that environmental conditions influence the stability of communication, when high rates of information transmission, and long range communication are required. In addition such optical communication systems have a short service life with rather high production and operation costs.

[0004] Another example of a prior art system can be found in WO9520845. Among the environmental conditions that degrade communication there are:

1. Atmospheric phenomena, such as fog, rain, snow. These conditions lead to attenuation of the signal in the communication line.
2. Deformations and slow vibrations of buildings and structures, where optical receivers and optical transmitters (emitters) are installed. These result in a loss or partial reduction of the received signal level due to broken mutual pointing of the optical receivers and optical transmitters (emitters) at the opposite communication points.
3. Crossing of the communication lines by non-transparent objects, e.g. birds, which can bring about sharp short-time weakening of the signal.
4. Position error and change of the angle at which the beam arrives at the optical receiver aperture.
5. When the beam passes through convection currents caused by heat from the sun, for example, fluctuations of the light capacity on the photodiode of the optical receiver can result causing poor communication quality

where large beam amplitudes are required.

[0005] The present invention is at least in part aimed at minimising the communication quality reduction that result from the above factors as well as providing a system that is cheap to produce and run.

[0006] In accordance with the present invention there is provided apparatus for wireless duplex communication, comprising, a first optical transceiver having a first optical transmitter and a first optical receiver, a second optical transceiver having a first optical transmitter and a first optical receiver, the first and second optical transceivers being located at the opposite end of an optical communication line formed thereby, wherein the output of each of the optical transmitters is a diverging beam of incoherent electromagnetic radiation arranged to have a cross sectional diameter which is larger than the cross sectional diameter of the respective optical receiver at that point on the communication line at which the respective optical receiver is situated.

[0007] Preferably, the optical transmitter emits electromagnetic radiation having a range of wavelengths.

[0008] Preferably, the optical transmitter emits radiation in the range 800 to 900 nanometres.

[0009] Preferably, the optical transmitter comprises a light emitting diode which provides the diverging beam of incoherent electromagnetic radiation.

[0010] Preferably, the optical transmitter comprises the LED and further comprises at least one optical condenser lens, the input to the optical condenser lens being provided by the LED and the output of the optical transmitter being provided by the optical condenser.

[0011] Preferably, the optical receiver consists of an optical condenser lens, diaphragm and photodiode, wherein the diaphragm is installed in the focal plane of the optical condenser lens.

[0012] Preferably the distance Δ between the photodiode and the diaphragm situated in the focal plane of the optical condenser lens is defined by the formula

$$\Delta = b\ F\ /\ Dc,$$

where

b - diameter of the light-sensitive site of the photodiode,
Dc - diameter of the optical condenser lens.

[0013] Preferably, the input of the optical condenser is the input of the optical receiver, and the output of the photodiode is the output of the first optical receiver.

[0014] Preferably the beam angle θ characterizing of the first optical transmitter and the first optical receiver of each of the said transceivers is defined from the following condition:

$$\mathrm{Tan}2\theta = a\ /\ F,$$

where

a - diameter of the diaphragm aperture;

F - focal distance of the optical condenser measured from the lens of the optical condenser to the centre of the stop aperture.

[0015] Preferably, the beam angle is between 30 and 60 angular minutes.

[0016] Preferably, the distance between the optical transmitter and optical receiver of a transceiver is greater than or equal to d/2, where d = 30cm.

[0017] Optionally d=60cm.

[0018] Preferably an input of the optical transmitter of the first transceiver is connected to an output of a converter through a modulator, and an output of the optical receiver of the first transceivers is connected to an input of a demodulator, the output thereof being connected to an input of a converter.

[0019] Preferably, an input of the optical transmitter of the second transceiver is connected to an output of a converter through a modulator, and an output of the optical receiver of the second transceivers is connected to an input of a demodulators, the output thereof being connected to the input of a converter.

[0020] Preferably, the converter is made in the form of a transformer, which transforms the signals of the input discrete information into a coded signal using the Manchester code during transmission, and which is capable of a reverse transformation of signals coming from the outputs of the respective demodulators during reception.

[0021] Preferably, each optical transceiver further comprises a second optical transmitter and a second optical receiver.

[0022] Preferably, said transceivers are connected to the input of the respective demodulators through a summator.

[0023] Preferably, the input of the second optical transmitter of each of the transceivers is connected to the output of the respective modulator, and the outputs of the first and second optical receivers is connected to the input of the respective demodulator through a summator.

[0024] In one embodiment of the present invention, the optical system is a two-element system, which uses one optical transmitter (optical emitter) and one optical receiver in each optical transceiver thereby forming two communication channels. When a two-element optical transceiver is used, the spacing of the optical transmitter and the optical receiver creates its own route of beam transmission for each beam of the duplex wireless optical communication line and therefore creates two communication channels. The probability of simultaneous emergence of conditions for maximum deviation of the beam in both transmission directions and thus the probability of simultaneous communication failure in both channels, is reduced as compared to the case of transmission along a single,common route.

[0025] In another embodiment of the present invention, the optical system is a four-element system. In this case, each of the said transceivers is equipped with a second optical transmitter and a second optical receiver similar to the first optical transmitter and the first optical receiver, which will together form four communication channels. In this embodiment, the optical transmitters and receivers of each transceiver are spaced on a plane perpendicular to their optical axes in relation to the straight line connecting their optical axes on the plane.

[0026] The optical transmitters and receivers of the first transceiver are arranged in the following order:

first optical receiver;
first optical transmitter;
second optical receiver; and
second optical transmitter.

[0027] In the second transceiver in relation to the first transceiver, the optical transmitters and receivers are arranged in the following order:

first optical transmitter;
first optical receiver;
second optical transmitter; and
second optical receiver.

[0028] It will be appreciated that the order of the first and the second transceivers could be reversed.

[0029] The spacing between each component of each transceiver is defined as being d/2, where d = 30cm. It has been found that this value represents a value below which the probability of protection against failures in the system reduces in cases where the line of sight between the transmitter and receiver is obscured by non-transparent objects or where errors in the angle of arrival of the light beam to the optical receiver have occurred or where the bean passes through turbulent atmosphere.

[0030] The outputs of the photodiodes of the first and second optical receivers of each of the said transceivers are connected to the input of the respective demodulator through a summator. The outputs of the second optical transmitter in each of the said transceivers are connected to the relevant modulator.

[0031] The invention will now be described by way of example only with reference to the accompanying drawings in which:

Fig. 1 shows a first embodiment of the present invention having a pair of two-element transceivers Fig. 1 also shows the location (spacing) of the optical transmitters (optical emitters) and the optical receivers of the transceivers as well as the transmission geometry of optical beams emitted by the optical transmitters;

Fig. 2 shows a second embodiment of the present invention having two four-element transceivers, the location (spacing) of the optical transmitters (optical emitters) and the optical receivers in the optical communication system is also shown along with the transmission geometry of optical beams emitted by the optical transmitters;

Fig. 3 is a flow chart of the optical communication system for two-element transceivers of Fig. 1;

Fig. 4 is a flow chart of the optical communication system for four-element transceivers of Fig 2; and

Fig. 5 shows an optical receiver (location of the optical receiver elements) used in the embodiment of the present invention illustrated in Figs. 1 to 4.

[0032] Referring to Figs. 1 and 3, the wireless optical duplex communication system uses two-element transceivers each of which are connected to an optical transceiver 3 and 5, a modulator 23 and 25, a demodulator 27 and 29 and a converter 39 and 41. The combination of optical transceiver, modulator, demodulator and converter is referred to as a semi-set. The first 3 and second 5 optical transceivers are located facing each other at the opposite ends of the optical communication line formed therebetween. The converters 39 and 41 are connected to the digital information exchange network (transmission and reception) (not shown). Since the system is duplex, and the operations of information transmission and reception from one semi-set to the other are the same in both directions, the information transmission process will be explained with reference to the communication line (channel) from the first semi-set to the second with two-element transceivers 3 and 5. The input information (input discrete signal) comes to a converter 39 of the first semi-set connected to the first optical transceiver 3, where it is coded utilising Manchester-type code. The input information is then fed at pre-defined logical levels to Modulator 23 which controls the emission of LED 43a which is part of the optical transmitter (optical emitter) 9 in such a way that during transmission of logical "1" light pulses are emitted in the first half of the given clock interval, and during transmission of logical "0" light pulses are transmitted in the second half of the given clock interval. The signal emitted by LED 43a comes to optical condenser 37a of the first optical transmitter 9. The optical condenser 37a forms the beam angle of the optical transmitter 9(optical emitter) to be between 30 and 60 angular minutes. In this example, the LED emits infra-red radiation containing a range of wavelengths typically between 820 and 870 nm. The radiation absorption characteristics in the transmission path of the optical emitter vary depending on atmospheric conditions. The use of a radiation emitter that emits a range of wavelengths ensures that at least some of the radiation reaches the receiver without being absorbed by the atmosphere irrespective of the atmospheric conditions. In other examples of the present invention, larger wavelength ranges can be used in the infra-red region or other parts of the electromagnetic spectrum.

[0033] Manchester-type coding is used, because it ensures resistance to impulse noise and reduces the probability of false alarms at the signal/noise ratios found in devices of this type. In the Manchester-type code the leading edge of the signal, is used for coding unities and zeros. During such coding, the bit period (time to transmit one bit of data) is divided into two parts. Information is coded by potential differences happening in the middle of each bit period. A unity is coded by a change from the low level to the high one, and zero by the reverse change. At the beginning of each bit period, there may be a service signal drop, if several unities or zeros are to be transmitted. Since the signal is changed at least once per bit period such a code possesses good self-synchronizing qualities and advantageously, allows the use of two signal levels for data transmission.

[0034] The optical radiation of the first optical transmitter 9 of the first transceiver 3 irradiates the optical condenser 37c of the first optical receiver 15 of the second transceiver 5, see beam A in Fig. 1). The optical energy collected by the optical condenser 37c of the first optical receiver 13 of the second transceiver 5 is directed through a stop or diaphragm aperture 45 (Fig.5) to a photodiode 35a. Thereafter, it is transformed into an electric signal, and then directed to demodulator 29. The optical condenser of the optical receiver 35 forms an angular beam of between 30 and 60 angular minutes. In the demodulator 29 of the second transceiver 5 the signal is transformed into logical levels of the Manchester-type code and is fed to converter 41 where it is transformed into an information signal in accordance with the requirements of the network protocols and directed to the information transmission digital network.

[0035] To reduce the probability of communication failures in case communication lines are crossed by non-transparent objects, the optical receiver and optical transmitter of each semi-set are spaced apart on a plane perpendicular to their optical axes to a distance of d/2 where d = 30 cm. This reduces the probability of simultaneous failure in both channels of the duplex communication line.

[0036] When a two-element optical transceiver, as described with reference to Figs. 1 and 3, is used, the spacing of the optical devices creates a separate route of beam transmission for each channel of the duplex communication line (beam A, beam B in Fig. 1). The probability of simultaneous emergence of conditions for the maximum beam deviation in both routes of transmission, and, thus, the probability of a simultaneous communication failure in both channels, is reduced as compared to the case of transmission along a common route.

[0037] The present invention, with two-element transceivers using two routes (two communication channels) of beam transmission (beams A, B in Fig. 1) provides for integral summation of signals by two spaced beam transmission routes. The integral summation thus formed in the communication system realizes the information transmission, reception and processing scheme, in which simultaneous failures in both channels are possible only in case of simultaneous communication failures in both beam transmission routes.

[0038] A special optical scheme is used for each of the optical receivers (Fig. 5), in which a diaphragm or stop aperture 45 is installed in the focal plane of the lens 37, forming the visual angle of the optical receiver (the beam angle). Angle θ characterizing the beam angle is defined from the condition

$$\mathrm{Tan}\ 2\theta = a\ /F$$

Where

a is the diaphragm aperture diameter.
F is the focal distance of the optical condenser measured from the optical condenser lens to the centre of the diaphragm aperture.

[0039] The optical scheme sets the maximum and minimum beam angle for transmission and, in conjunction with the diaphragm 45, reduces the density of the light flow on the photodiode surface and consequently increases the operation resource of LED.

[0040] The photodiode 35 is located behind the diaphragm 45 at distance Δ providing for reduced density of the light flow falling on the photodiode, without reducing the value of the light capacity of the said flow, where

$$\Delta = b\ F\ /D_c.$$

where

b is the diameter of the light sensitive photodiode site.
$\mathbf{D_c}$ is the diameter of the optical condenser lens.

[0041] To remove the effect of deformations and slow vibrations of buildings and structures, the beam angle of optical transmitters (beam divergence) and receivers (visual angle) is standardized. Allowable values of the beam angle of the optical transmitters and receivers are limited to maximum and minimum values and are selected using the above equation to be between 30 and 60 angular minutes in this example. In a typical example, an infra-red beam having a frequency of 340000 GHz and wavelength of 850 nm is created having a beam diameter of 10m at a distance of 1.5Km from its source.

[0042] In general, the minimum value of the beam angle is a practical limit which ensures the absence of communication failures in case of an error of mutual angular pointing caused by deformations and slow vibrations of buildings or position errors and change of the angle of arrival of the light beam to the aperture of the optical receiver when the beam passes through turbulent atmosphere. The maximum beam angle value is set to provide sufficient power in the communications line to allow effective communication.

[0043] In an optical communication system where four-element optical transceivers 103, 105 are used (Fig. 2, 4), each consisting of the first optical transmitter 109, the first optical receiver 107, the second optical transmitter 117, and the second optical receiver 119 are located as shown in Fig. 2 and are similar to the optical transmitters and optical receivers of the two-element transceivers 3, 5.

[0044] The information transmission process is as follows, and, since the system is duplex and the operations of information transmission from one transceiver to the other are the same in both directions, the information transmission process will be described with reference to the communication channel from the first transceiver 103 to the second transceiver 105 (Fig. 2, 4).

[0045] The information (signal) comes to converter 139 of the first optical transceiver 103, where it is coded using the Manchester-type code and then fed to Modulator M1 123 of first optical transceiver 103 to control emission of LED 143a and 143b of the first and second optical transmitters 109 and 117 through respective optical condensers 137a, 137c in such a way that during transmission of logical "1" light impulses are emitted in the first half of the given clock interval, and during transmission of logical "0" light impulses are transmitted in the second half. Optical condensers 137a and 137c of the first and second optical transmitters 109 and 117. respectively, form the beam angle of each optical transmitter (optical emitter) at between 30 and 60 angular minutes. Manchester-type coding is used as shown above, because it ensures resistance to impulse noise and reduces the probability of false alarm. The optical radiation of each of the optical transmitters 109 and 117 irradiates optical condensers 137b and 137d of the first and second optical receivers 111 and 119 of the second optical transceiver 105(beams C,D,E and F in Fig.2). The optical energy collected by the optical condensers 37 (fig.5) is directed through the respective diaphragm apertures 45 to respective photodiodes 35, transformed into electric signals summed later in electronic summator Σ2 133 of the second optical transceiver 105. The summator implements the information transmission and processing scheme. A failure of information transmission through the communication channel is possible only where a simultaneous failure in all four beam spreading routes has occured.

[0046] Optical condensers 137b and 137d form the beam angle of the respective optical receivers between 30 and 60 angular minutes, and angle θ characterizing the beam angle is also defined from the condition

$$\mathrm{Tan}\ 2\theta = a/\ F,$$

the optical receivers in the four-element system being similar to those in the two-element system.

[0047] In the proposed four-element system, integral summation of signals coming through the four beam transmission routes is made, which makes it possible to realize an information transmission and processing scheme that prevents failure of information transmission through the said communication channels except in case of simultaneous failures in all the four beam transmission routes.

[0048] In demodulator 129 of the second optical transceiver 105 the signal from the Σ2 summator 133a output is transformed into the logical levels of the Manchester-type code and fed to converter K2 of the second optical transceiver 105, where it is transformed into signals meeting the network protocol requirements and channeled to the digital information (consumer) network.

[0049] If we regard the four-element information transmission and reception system as a whole (two transceivers and four respective transmitters and four receivers), its realization allows for the formation of an integral summing system (since summation due to the beam transmission geometry shown in Fig. 2 is made in each communication channel: optical transmitter - optical receiver), which embodies the information transmission and processing system, where a simultaneous failure in all the channels is possible only in case of simultaneous failures in eight beam transmission routes (beams C, D, E, F. G. H, I and J in Fig. 2).

[0050] Thus, due to the design of the wireless optical duplex communication system and the use of the Manchester-type code, resistance to impulse noise is increased, and the probability of false alarm is lowered. In addition, the present invention incorporates a data confirmation routine in which confirmation that data has been received at a transceiver is provided by sending a separate data stream in the opposite direction in a different vector space. This is achieved by attaching a characteristic group of symbols to the data packet. The receipt of these symbols is acknowledged by the transmission of an acknowledgement to the data packet transmitter. Where receipt of the data packet has not been acknowledged, transmission of the original data package will be repeated.

[0051] Beam angle selection makes it possible to prevent communication failures in case of a mutual angular pointing error where the necessary energy potential in the communication line is available. Spacing of the optical transmitters and receivers at each end (point) of the communication line reduces the probability of failures, when the line is crossed by nontransparent objects. The use of a special optical receiver circuit helps reduce the density of the light flow on the photodiode surface and increases the LED operation resource.

[0052] The embodiments of the present invention shown above use LEDs as incoherent light sources. Incoherent light sources have a number of advantages over laser (or coherent) sources for use in communications systems.

[0053] The radiation spectrum width of a laser is many times smaller than that of an incoherent light source and the spectral emission width in the atmosphere can correspond to the typical laser radiation spectrum width. Therefore attenuation of the laser beam by atmospheric conditions can be severe. The larger spectrum width of the incoherent light source greatly decreases the likelihood of high attenuation. Therefore, in laser communications systems (depending upon the temperature of the laser, where the wavelength depends upon temperature) attenuation values can exist that correspond to maximum atmospheric spectral emission values, whereas in incoherent systems, such as LED systems, the much larger spectrum width obviates this problem.

[0054] In addition, LEDs are much cheaper than lasers to manufacture and unlike lasers, are safe even for personnel located in close proximity to the optical transmitters (emitters). In particular, where high power lasers are used to increase the range over which a communications system can operate, there is an increased health risk to people caught in the beam path. There is no associated health risk with incoherent or LED systems.

[0055] Operation costs are also lowered, since the mutual pointing procedure is simplified because the beam angle is wide enough to remove the need for highly accurate pointing of the transmitter at the receiver and the requirements for the structures upon which the optical transmitters and receivers are installed are less strict.

[0056] The use of incoherent light sources means that interference between signals in the present invention is minimised.

[0057] The apparatus in accordance with the present invention can have an optical path length of 3000m.

[0058] Improvements and modifications may be incorporated without deviating from the scope of the invention.

Claims

1. An apparatus for wireless duplex communication, comprising, a first optical transceiver (3) having a first optical transmitter (9) and a first optical receiver (7), a second optical transceiver (5) having a first optical transmitter (13) and a first optical receiver (11), the first and second optical transceivers (3, 5) being located at opposite ends of an optical communication line formed thereby, wherein the output of each of the optical transmitters (9, 13) is a diverging beam of incoherent electromagnetic radiation arranged to have a cross sectional diameter which is larger than the cross sectional diameter of the respective optical receiver (7, 11) at that point on the communication line at which the respective optical receiver (7, 11) is situated, wherein each of the optical receivers (7, 11) includes an optical condenser lens (37) having a focal plane, a photodiode (35), and a diaphragm (45) having an aperture and situated in the focal plane of the optical condenser lens (37) between the optical condenser lens (37) and

the photodiode (35), wherein the distance Δ between the diaphragm (45) and the photodiode (35) is defined by $\Delta = b\ F\ /\ Dc$, where b is the diameter of a light-sensitive site of the photodiode (35), *Dc* is the diameter of the optical condenser lens (37), and *F* is the focal distance of the optical condenser lens (37), and wherein a beam angle θ characterizing the first transmitters (9, 13) and the first receivers (7, 11) is defined by $Tan\ 2\theta = a\ /\ F$, where *a* is the aperture of the diaphragm (45).

2. An apparatus as claimed in claim 1 wherein, each of the first optical transmitters (9, 13) emits electromagnetic radiation in the range 800 to 900 nanometres.

3. An apparatus as claimed in claim 1 or 2 wherein each of the first optical transmitters (9, 13) comprises a light emitting diode (LED) providing a source of the diverging beam of incoherent electromagnetic radiation, further comprises at least one optical condenser lens, the input to the optical condenser lens being provided by the LED and the output of the optical transmitter (9, 13) being provided by the optical condenser lens.

4. An apparatus as claimed in any preceding claim wherein an input of the optical condenser lens (37) is an input of one of the first optical receivers (7, 11), and an output of the photodiode (35) is an output of one of the first optical receivers (7, 11).

5. An apparatus as claimed in any preceding claim wherein the beam angle θ is between 30 and 60 angular minutes.

6. An apparatus as claimed in any preceding claim wherein the distance between the first optical transmitters (9, 13) and first optical receivers (7, 11) of each of the first and second transceivers (3, 5) is greater than or equal to d/2, where d = 30cm.

7. An apparatus as claimed in any preceding claim wherein an input of the first optical transmitter (9) of the first transceiver (3) is connected to an output of a first converter (39) through a first modulator (23), and an output of the first optical receiver (7) of the first transceiver (3) is connected to an input of a first demodulator (27), the output thereof being connected to an input of the first converter (39); and an input of the first optical transmitter (13) of the second transceiver (5) is connected to an output of a second converter (41) through a modulator (25), and an output of the first optical receiver (11) of the second transceiver (5) is connected to an input of a second demodulator (29), the output thereof being connected to the input of the second converter (41).

8. An apparatus as claimed in claim 7 wherein the first and second converters (39, 41) are each made in the form of a transformer, wherein each of the first and second converter (39, 41) transforms signals of input discrete information into a coded signal using the Manchester code during transmission, and wherein each of the first and second converter (39, 41) is capable of a reverse transformation of signals coming from the outputs of the respective demodulators (27, 29) during reception.

9. An apparatus as claimed in any preceding claim wherein each of the first and the second optical transceivers (3, 5) further comprises a second optical transmitter (117) and a second optical receiver (111).

10. An apparatus as claimed in claim 9 wherein each of the first and second transceivers (3, 5) further comprises a summator (133a, 133b) and a demodulator (127, 129) having an input, and wherein the first and second optical receivers (7, 11, 111) in each optical transceiver (3, 5) are connected to the input of the respective demodulator (127, 129) through the summator (133).

Patentansprüche

1. Vorrichtung zur drahtlosen wechselseitigen Kommunikation, umfassend, eine erste optische Sendeempfangsanlage (3) mit einem ersten optischen Sender (9) und einem ersten optischen Empfänger (7); und eine zweite optische Sendeempfangsanlage (5) mit einem ersten optischen Sender (13) und einem ersten optischen Empfänger (11), wobei die erste und die zweite optische Sendeempfangsanlage (3; 5) gegenüberliegende Enden eines optischen Übertragungsweges bilden; wobei das Ausgangssignal eines jeden der optischen Sender (9; 13) durch einen divergierenden Strahl einer inkohärenten elektromagnetischen Strahlung gebildet ist, der einen Querschnittsdurchmesser aufweist, der größer ist als ein Querschnittsdurchmesser des zugehörigen optischen Empfängers (7; 11) in einem Punkt des Übertragungsweges, in welchem sich der zugehörige optische Empfänger (7; 11) befindet; wobei jeder der optischen Empfänger (7; 11) einen optischen Kondensor (37) mit einer Brennebene, einer Fotodiode (35) und einer Blende (45) mit einer Blendenöffnung in der Brennebene des optischen Kondensors (37) zwischen dem optischen Kondensor (37) und der Fotodiode (35) umfasst; wobei ein Abstand Δ zwischen der Blende (45) und der Fotodiode (35) durch $\Delta = b\ F\ /\ Dc$ definiert ist, wobei b ein Durchmesser eines lichtempfindlichen Bereiches der Fotodiode (35) ist, wobei Dc ein Durchmesser des optischen Kondensors (37) ist, und wobei F eine Brennweite des optischen Kondensors (37) ist; und wobei ein die ersten Sender (9; 13) und die ersten Empfänger (7; 11) charakterisierender Öffnungswinkel θ durch *Tan 2*θ = *a* / F definiert ist, wobei *a* ein Blendendurchmesser der Blende (45) ist.

2. Vorrichtung nach Anspruch 1, **dadurch gekennzeichnet, dass** jeder der ersten optischen Sender (9; 13) elektromagnetische Strahlung im Bereich von 800 nm bis 900 nm emittiert.

3. Vorrichtung nach Anspruch 1 oder 2, **dadurch gekennzeichnet, dass** jeder der ersten optischen Sender (9; 13) als Quelle des divergierenden Strahles der elektromagnetischen Strahlung eine Leuchtdiode (LED) und weiterhin mindestens einen optischen Kondensor umfasst, wobei ein Eingangssignal des optischen Kondensors von der LED bereitgestellt wird; und wobei ein Ausgangssignal des optischen Senders (9; 13) von dem optischen Kondensor bereitgestellt wird.

4. Vorrichtung nach einem der vorstehenden Ansprüche, **dadurch gekennzeichnet, dass** ein Eingang des optischen Kondensors (37) einen Eingang eines der ersten optischen Empfänger (7; 11) bildet; und dass ein Ausgang der Fotodiode (35) einen Ausgang eines der ersten optischen Empfänger (7; 11) bildet.

5. Vorrichtung nach einem der vorstehenden Ansprüche, **dadurch gekennzeichnet, dass** der Öffnungswinkel θ zwischen 30 Winkelminuten und 60 Winkelminuten beträgt.

6. Vorrichtung nach einem der vorstehenden Ansprüche, **dadurch gekennzeichnet, dass** ein Abstand zwischen den ersten optischen Sendern (9; 13) und den ersten optischen Empfängern (7; 11) einer jeden der ersten und der zweiten optischen Sendeempfangsanlage (3; 5) größer oder gleich *d*/*2* ist, wobei *d* = 30 cm ist.

7. Vorrichtung nach einem der vorstehenden Ansprüche, **dadurch gekennzeichnet, dass** ein Eingang des ersten optischen Senders (9) der ersten optischen Sendeempfangsanlage (3) mit einem Ausgang eines ersten Konverters (39) über einen ersten Modulator (23) verbunden ist; dass ein Ausgang des ersten optischen Empfängers (7) der ersten optischen Sendeempfangsanlage (3) mit einem Eingang eines ersten Demodulators (27) verbunden ist, dessen Ausgang mit einem Eingang des ersten Konverters (39) verbunden ist; dass ein Eingang des ersten optischen Senders (13) der zweiten optischen Sendeempfangsanlage (5) mit einem Ausgang eines zweiten Konverters (41) über einen Modulator (25) verbunden ist; und dass ein Ausgang des ersten optischen Empfängers (11) der zweiten optischen Sendeempfangsanlage (5) mit einem Eingang eines zweiten Demodulators (29) verbunden ist, dessen Ausgang mit einem Eingang des zweiten Konverters (41) verbunden ist.

8. Vorrichtung nach Anspruch 7, **dadurch gekennzeichnet, dass** der erste und der zweite Konverter (39; 41) jeweils als Wandler ausgeführt sind, wobei jeder des ersten und des zweiten Konverters (39; 41) diskrete Informationen am Eingang in ein kodiertes Signal wandelt, welches eine Manchester-Kodierung während der Übertragung nutzt; und wobei jeder des ersten und des zweiten Konverters (39; 41) während des Empfanges zur inversen Transformation der an den Ausgängen der zugeordneten Demodulatoren (27; 29) anliegenden Signale geeignet ist.

9. Vorrichtung nach einem der vorstehenden Ansprüche, **dadurch gekennzeichnet, dass** jede der ersten und der zweiten optischen Sendeempfangsanlage (3; 5) weiterhin einen zweiten optischen Sender (117) und einen zweiten optischen Empfänger (111) umfasst.

10. Vorrichtung nach Anspruch 9, **dadurch gekennzeichnet, dass** jede der ersten und der zweiten optischen Sendeempfangsanlage (3; 5) weiterhin einen Summator (133a; 133b) und einen Demodulator (127; 129) mit einem Eingang umfasst, wobei die ersten und die zweiten optischen Empfänger (7; 11; 111) jeder optischen Sendeempfangsanlage (3; 5) mit dem Eingang des zugehörigen Demodulators (127; 129) über den Summator (133) verbunden sind.

Revendications

1. Appareil pour communication duplex sans fil, comprenant un premier émetteur récepteur optique (3) ayant un premier émetteur optique (9) et un premier récepteur optique (7), un deuxième émetteur récepteur optique (5) ayant un premier émetteur optique (13) et un premier récepteur optique (11), les premier et deuxième émetteurs récepteurs (3, 5) étant situés à des extrémités opposées d'une ligne de communication optique constituée de ceux-ci, dans lequel la sortie de chacun des émetteurs optiques (9, 13) est un faisceau divergent de rayonnement électromagnétique incohérent agencé pour avoir un diamètre de coupe transversale qui est plus grand que le diamètre de coupe transversale du récepteur optique respectif (7, 11) au point de la ligne de communication auquel le récepteur optique respectif (7, 11) est situé, dans lequel chacun des récepteurs optiques (7, 11) comprend une lentille de condensateur optique (37) ayant un plan focal, une photodiode (35), et un diaphragme (45) ayant une ouverture et

situé dans le plan focal de la lentille de condensateur optique (37) entre la lentille de condensateur optique (37) et la photodiode (35), dans lequel la distance Δ entre le diaphragme (45) et la photodiode (35) est définie par Δ = b F / Dc, où b est le diamètre d'un site sensible à la lumière de la photodiode (35), Dc est le diamètre de la lentille de condensateur optique (37), et F est la distance focale de la lentille de condensateur optique (37), et dans lequel un angle de faisceau θ caractérisant les premiers émetteurs (9, 13) et les premiers récepteurs (7, 11) est défini par Tan 2θ = a / F, où a est l'ouverture du diaphragme (45).

2. Appareil selon la revendication 1, dans lequel chacun des premiers émetteurs optiques (9, 13) émet un rayonnement électromagnétique dans la plage de 800 à 900 nanomètres.

3. Appareil selon la revendication 1 ou 2, dans lequel chacun des premiers émetteurs optiques (9, 13) comprend une diode électroluminescente (DEL) fournissant une source du faisceau divergent de rayonnement électromagnétique incohérent, et comprend en outre au moins une lentille de condensateur optique, l'entrée de la lentille de condensateur optique étant assurée par la DEL et la sortie de l'émetteur optique (9, 13) étant assurée par la lentille de condensateur optique.

4. Appareil selon l'une quelconque des revendications précédentes, dans lequel une entrée de la lentille de condensateur optique (37) est une entrée de l'un des premiers récepteurs optiques (7, 11), et une sortie de la photodiode (35) est une sortie de l'un des premiers récepteurs optiques (7, 11).

5. Appareil selon l'une quelconque des revendications précédentes, dans lequel l'angle de faisceau θ est entre 30 et 60 minutes angulaires.

6. Appareil selon l'une quelconque des revendications précédentes, dans lequel la distance entre les premiers émetteurs optiques (9, 13) et les premiers récepteurs optiques (7, 11) de chacun des premier et deuxième émetteurs récepteurs (3, 5) est supérieure ou égale à d/2, où d = 30 cm.

7. Appareil selon l'une quelconque des revendications précédentes, dans lequel une entrée du premier émetteur optique (9) du premier émetteur récepteur (3) est connectée à une sortie d'un premier convertisseur (39) à travers un premier modulateur (23), et une sortie du premier récepteur optique (7) du premier émetteur récepteur (3) est connectée à une entrée d'un premier démodulateur (27), dont la sortie est connectée à une entrée du premier convertisseur (39) ; et une entrée du premier émetteur optique (13) du deuxième émetteur récepteur (5) est connectée à une sortie d'un deuxième convertisseur (41) à travers un modulateur (25), et une sortie du premier récepteur optique (11) du deuxième émetteur récepteur (5) est connectée à une entrée d'un deuxième démodulateur (29), dont la sortie est connectée à l'entrée du deuxième convertisseur (41).

8. Appareil selon la revendication 7, dans lequel les premier et deuxième convertisseurs (39, 41) sont chacun constitués sous la forme d'un transformateur, dans lequel chacun des premier et deuxième convertisseurs (39, 41) transforme des signaux d'informations discrètes d'entrée en un signal codé en utilisant le code de Manchester pendant la transmission, et dans lequel chacun des premier et deuxième convertisseurs (39, 41) est capable d'effectuer une transformation inverse de signaux provenant des sorties des démodulateurs respectifs (27, 29) pendant la réception.

9. Appareil selon l'une quelconque des revendications précédentes, dans lequel chacun des premier et deuxième émetteurs récepteurs optiques (3, 5) comprend en outre un deuxième émetteur optique (117) et un deuxième récepteur optique (111) .

10. Appareil selon la revendication 9, dans lequel chacun des premier et deuxième émetteurs récepteurs (3, 5) comprend en outre un sommateur (133a, 133b) et un démodulateur (127, 129) ayant une entrée, et dans lequel les premier et deuxième récepteurs optiques (7, 11, 111) dans chaque émetteur récepteur optique (3, 5) sont connectés à l'entrée du démodulateur respectif (127, 129) à travers le sommateur (133).

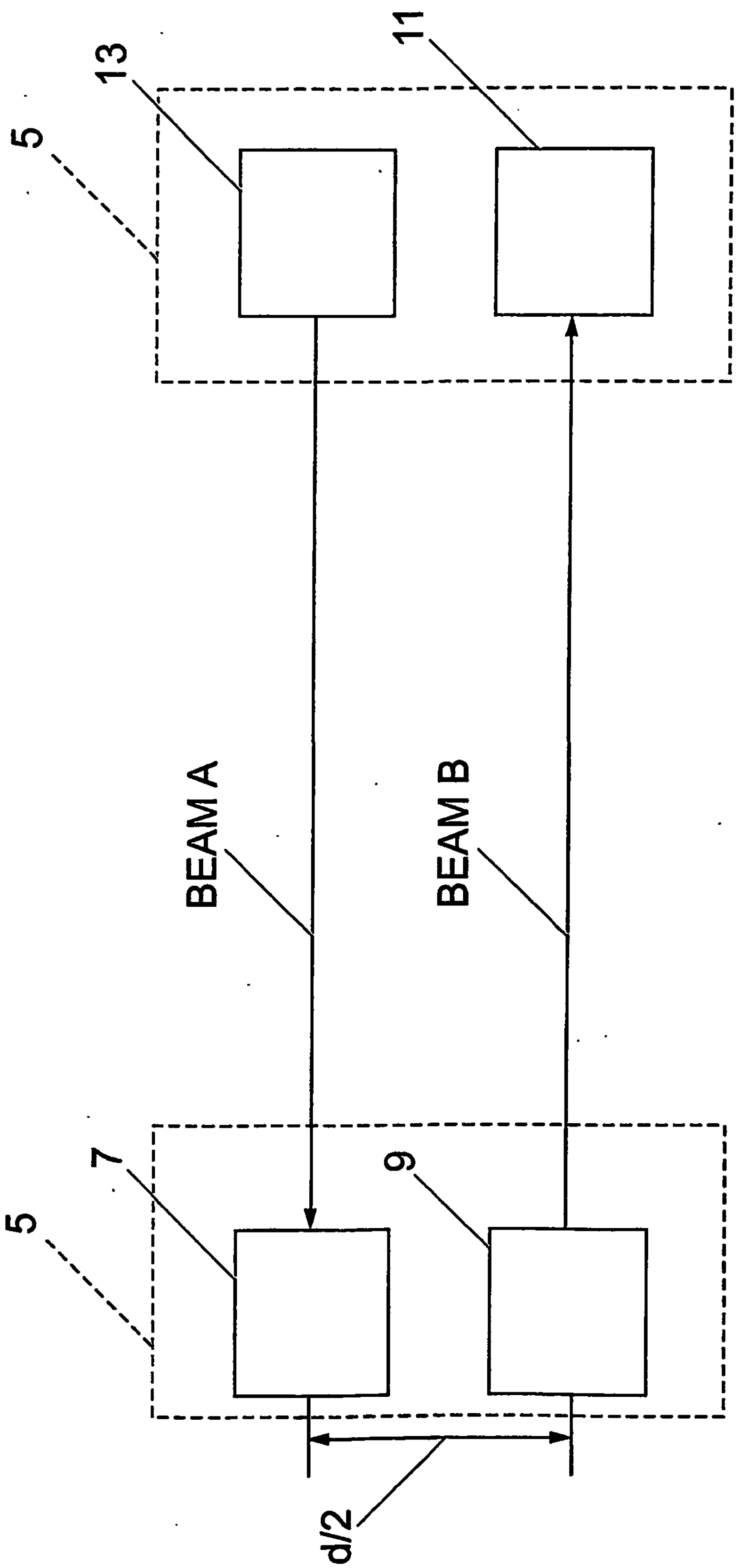

Fig. 1

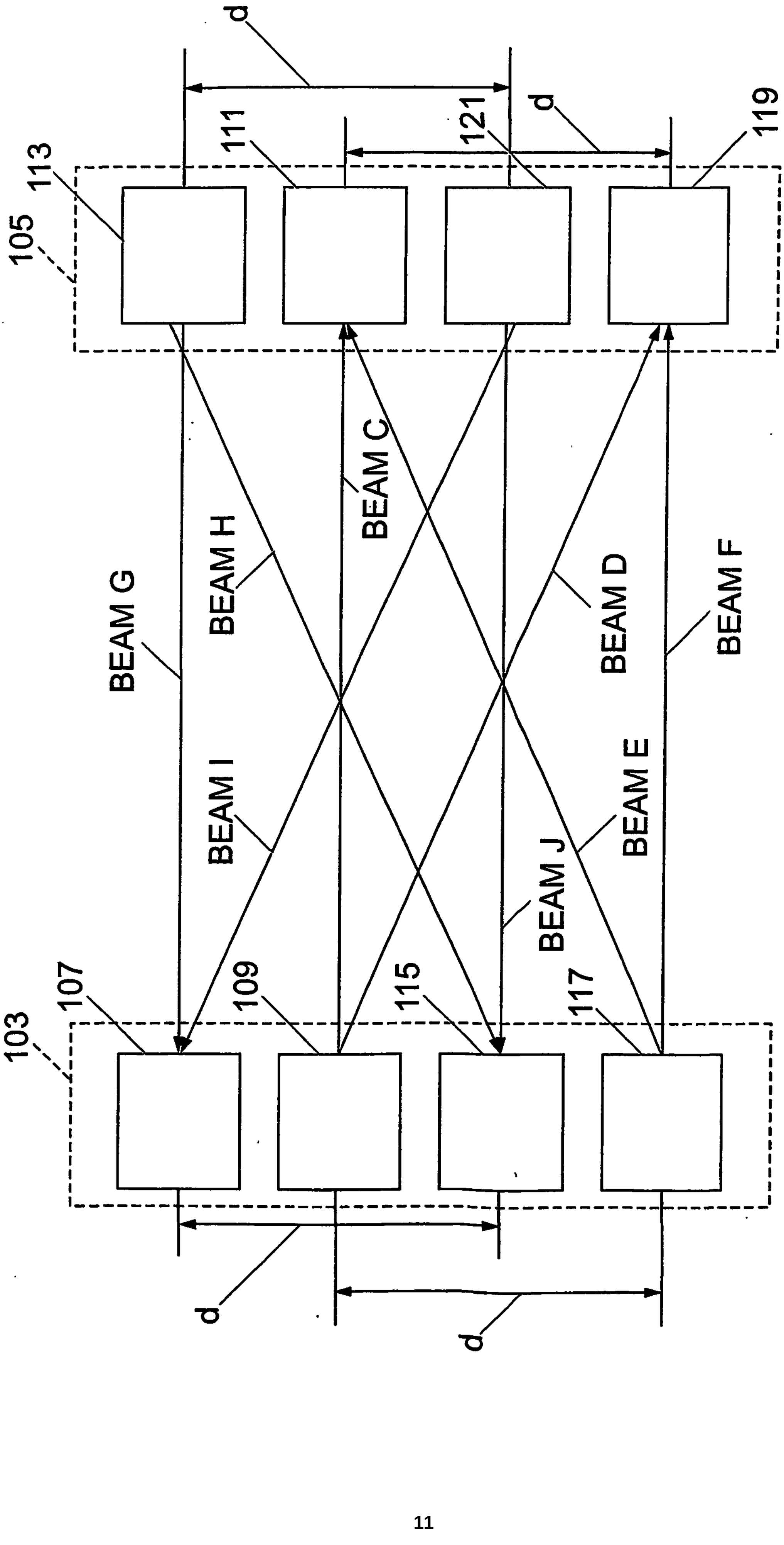
d
d
105
113
111
121
119
BEAM G
BEAM H
BEAM C
BEAM D
BEAM F
BEAM I
BEAM J
BEAM E
103
107
109
115
117
d
d

Fig. 2

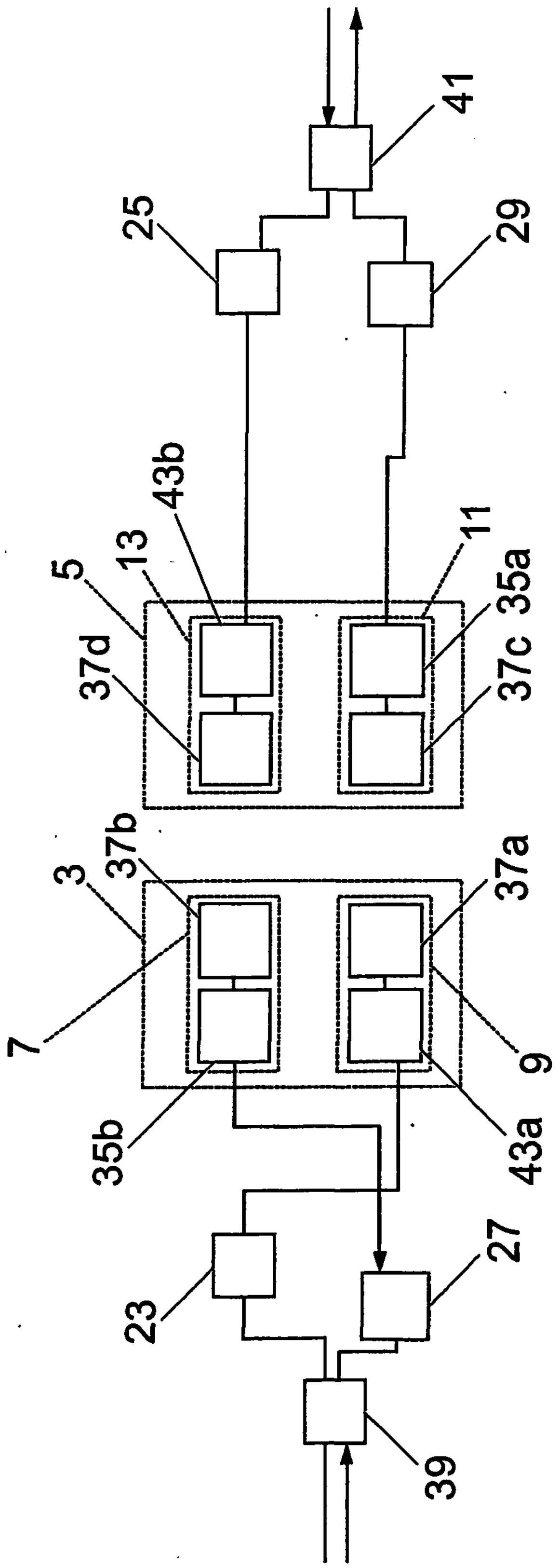

Fig. 3

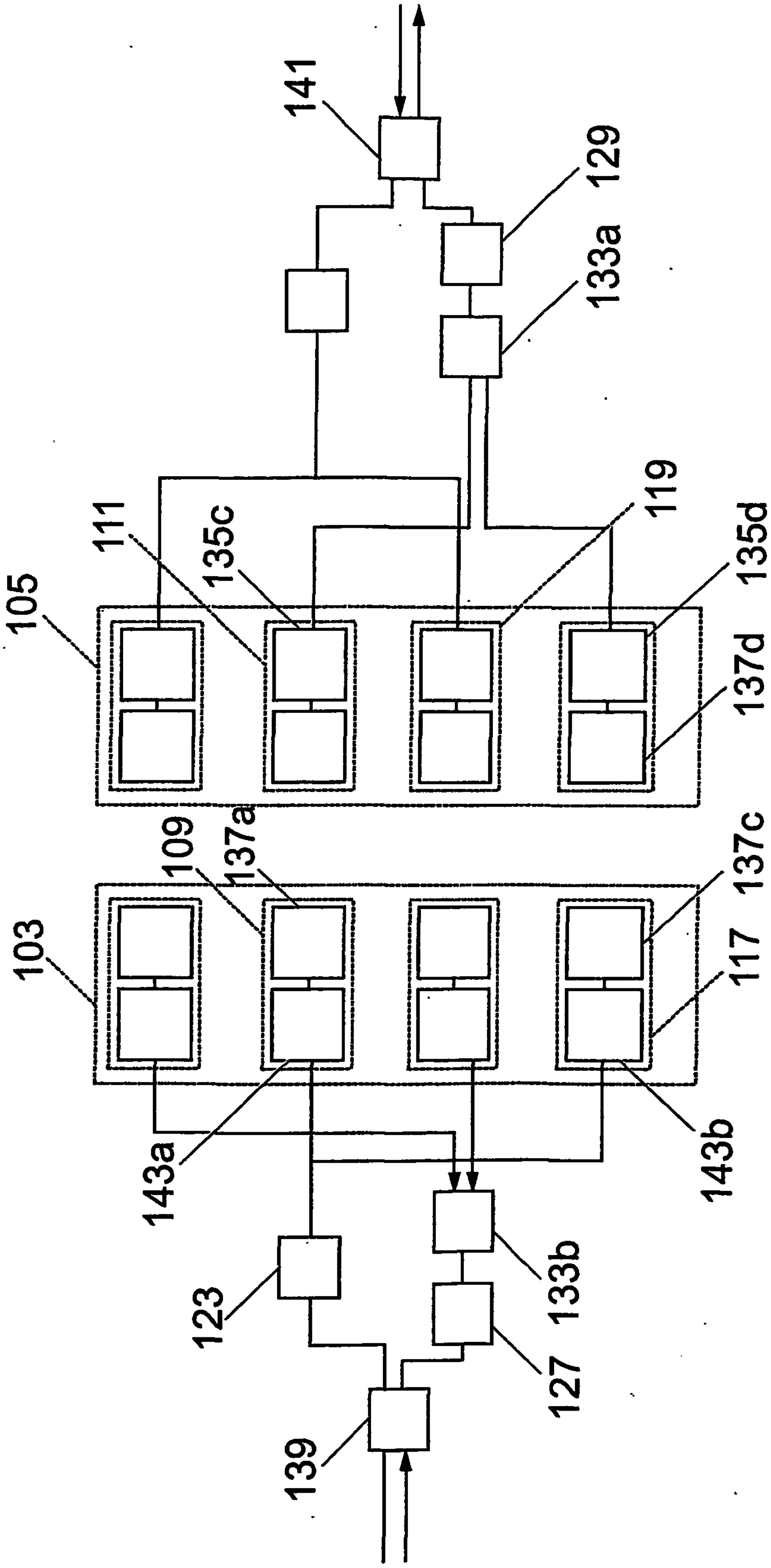
141
129
133a
105
111
135c
119
135d
137d
103
109
137a
137c
117
143a
143b
123
133b
127
139

Fig. 4

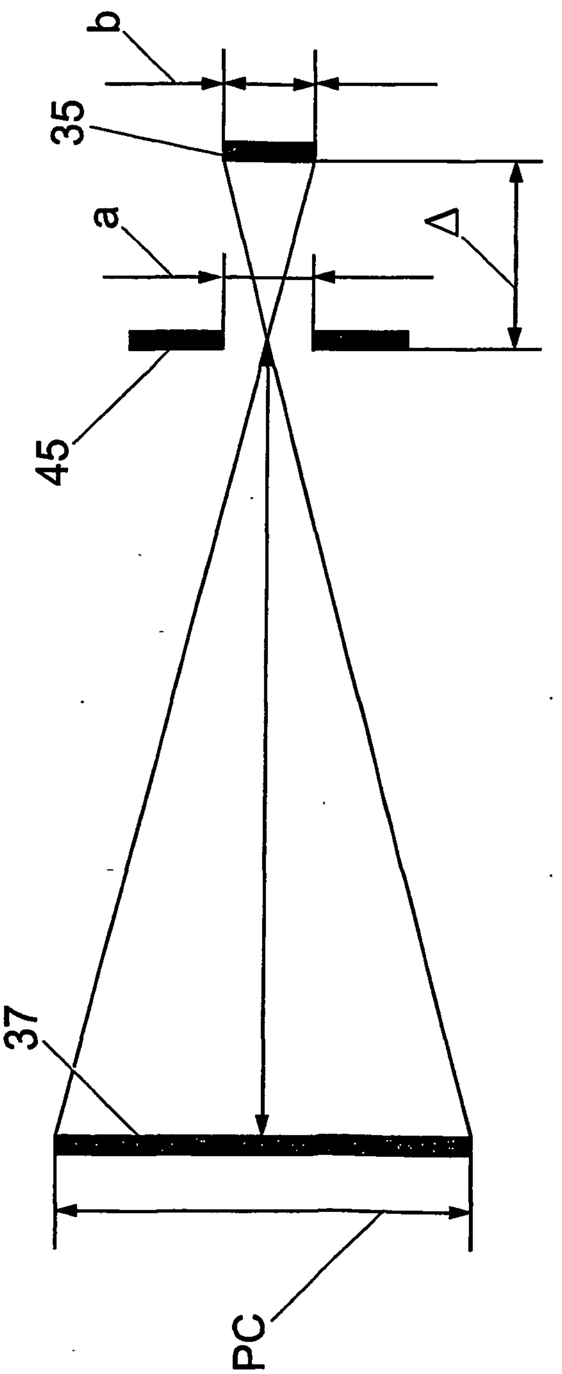

Fig. 5

REFERENCES CITED IN THE DESCRIPTION

Patent documents cited in the description

- WO 9520845 A **[0004]**