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(54) **FERROELECTRIC ENERGY GENERATOR WITH VOLTAGE-CONTROLLED SWITCH**

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(57) **ABSTRACT**

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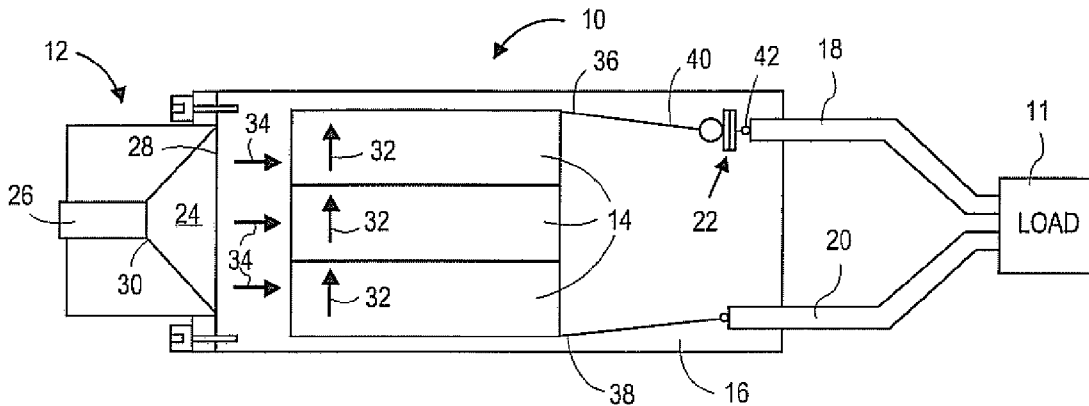
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A ferroelectric energy generator system comprises an explosive unit, a ferroelectric element, a first and a second output terminal, and a voltage-controlled switch. The explosive unit may include an explosive charge and a detonator which in combination may supply a shock wave. The ferroelectric element may include a third output terminal coupled to the voltage-controlled switch and a fourth output terminal coupled to the second output terminal. Upon receiving the shock wave, the ferroelectric element may be compressed and depolarized and, as a result, may generate a pulse of voltage between the third and the fourth output terminals. When the voltage reaches a breakdown level, the voltage-controlled switch may close and quickly deliver electric current to a load coupled to the ferroelectric energy generator system.



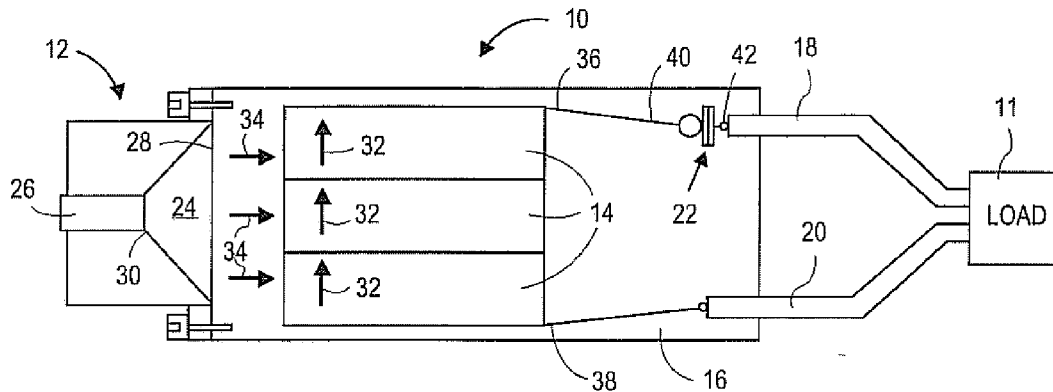


FIG. 1

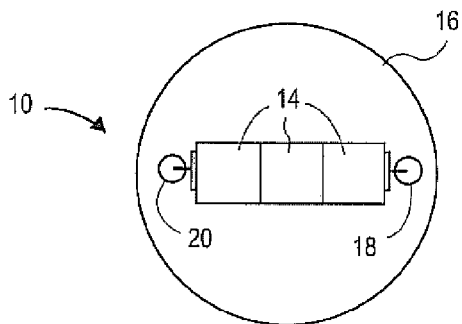


FIG. 2

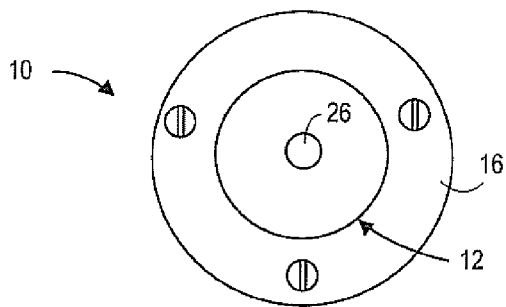


FIG. 3

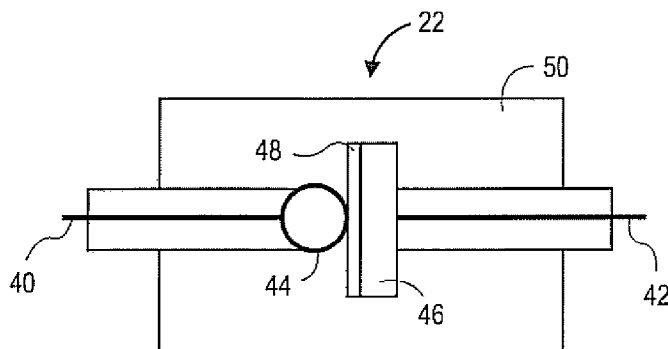


FIG. 4

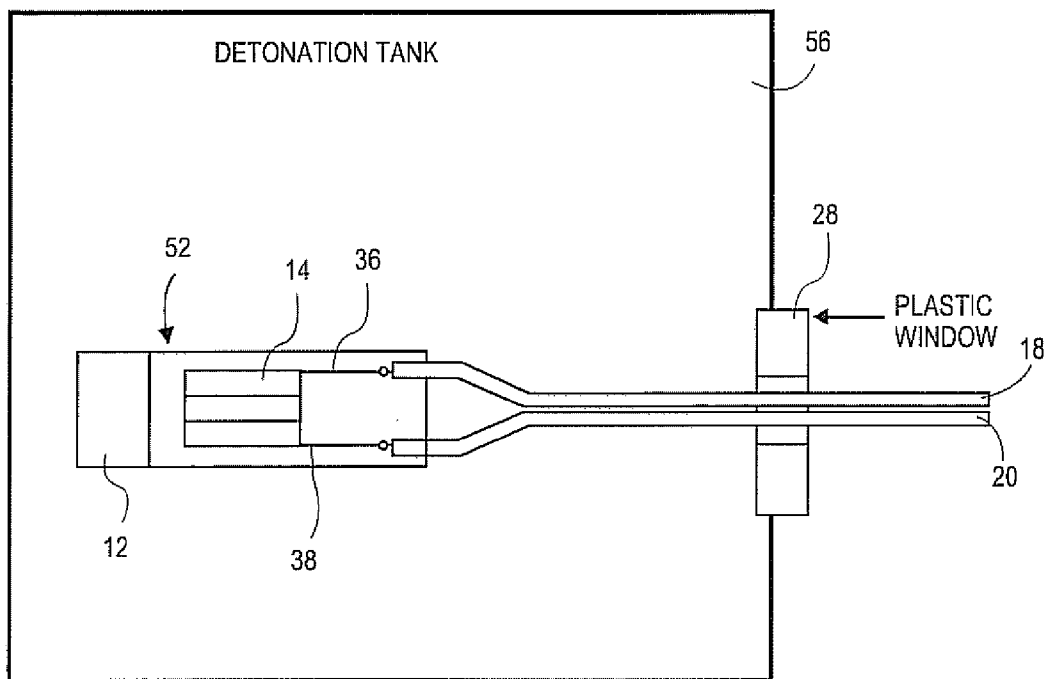


FIG. 5

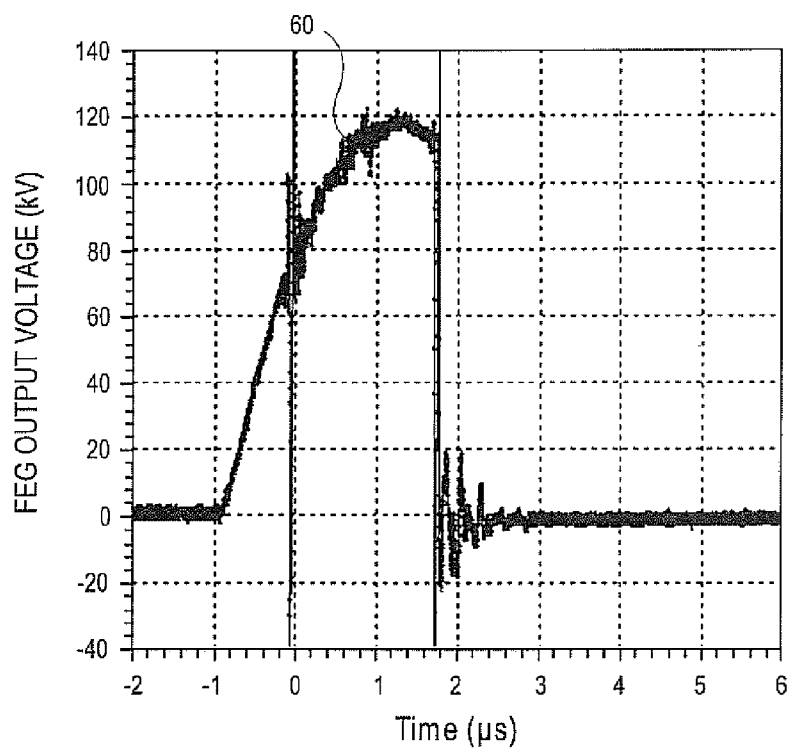


FIG. 6

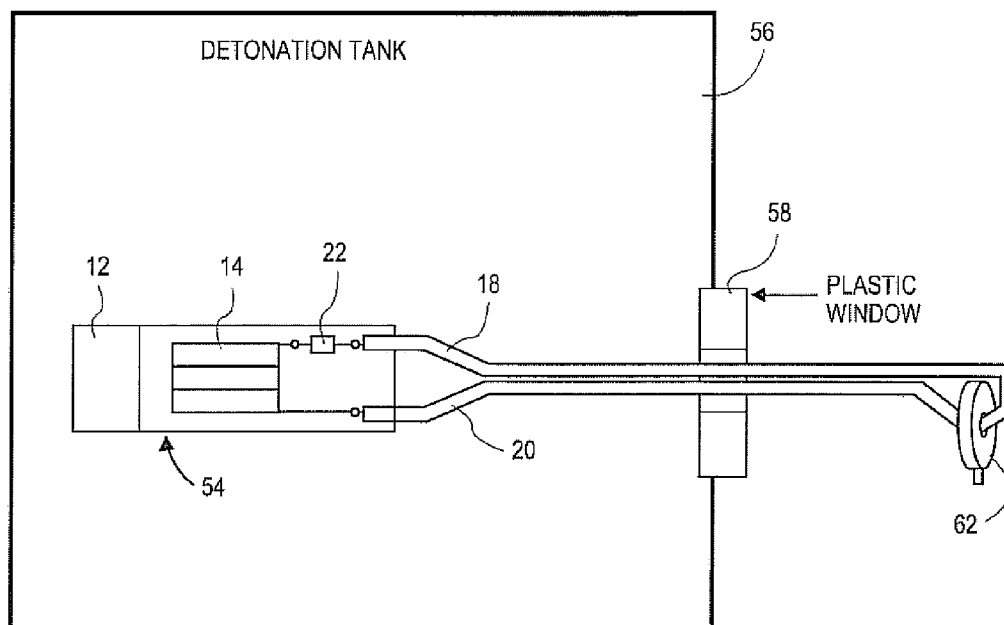


FIG. 7

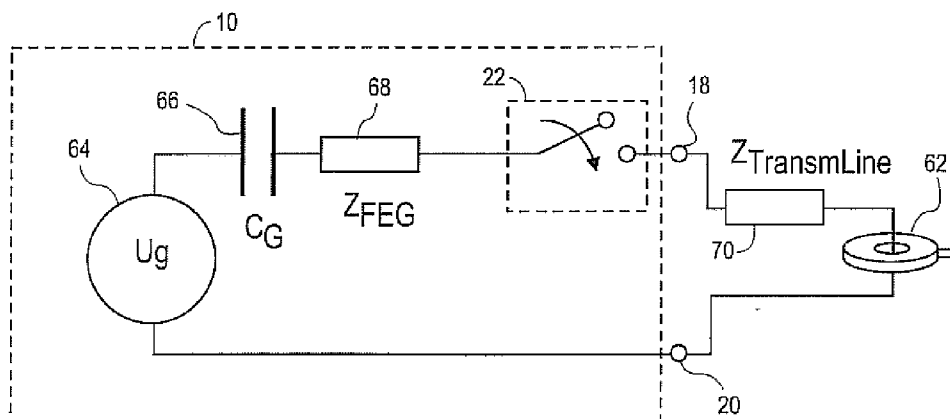


FIG. 8

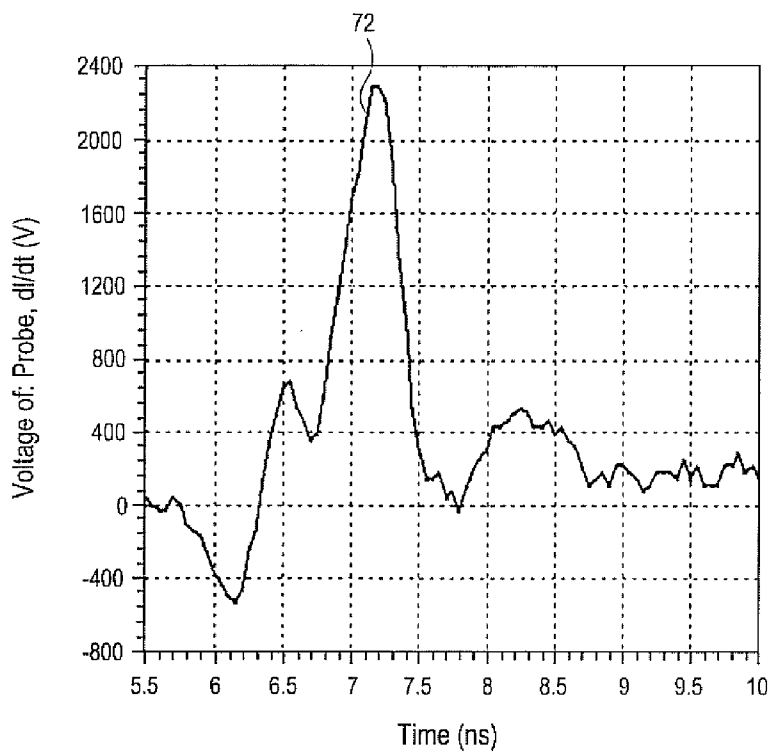


FIG. 9

**FERROELECTRIC ENERGY GENERATOR WITH VOLTAGE-CONTROLLED SWITCH**

FEDERALLY SPONSORED RESEARCH OR DEVELOPMENT PROGRAM

[0001] The present invention was developed with support from the U.S. government under Contract Nos. W9113M-07-C-0215 and W9113M-08-C-0006 with the U.S. Department of Defense. Accordingly, the U.S. government has certain rights in the present invention.

BACKGROUND OF THE INVENTION

[0002] 1. Field of the Invention

[0003] Embodiments of the present invention relate to ferroelectric energy generator systems. More particularly, embodiments of the present invention relate to an energy generator that utilizes direct explosive shock wave depolarization of at least one ferroelectric element to deliver electrical energy to a load through a voltage-controlled switch.

[0004] 2. Description of the Related Art

[0005] Explosive-driven pulsed power energy generators, such as ferroelectric energy generators, supply large amounts of electrical energy and may be used in many commercial and scientific applications. One exemplary application that may utilize a ferroelectric energy generator is a microwave transmitter system. The output of the ferroelectric energy generator may be coupled to an antenna that transmits microwave radiation when it receives electrical energy. Although conventional ferroelectric energy generators may produce a large amplitude pulse of voltage, they may not be able to quickly deliver electric current to the antenna. As a result, the antenna may not receive the rapid electrical energy pulse that it needs to oscillate and transmit microwaves.

SUMMARY OF THE INVENTION

[0006] Embodiments of the present invention solve the above-mentioned problems and provide a distinct advance in the art of ferroelectric energy generation. More particularly, embodiments of the invention provide a ferroelectric energy generator system that includes a voltage-controlled switch that is able to deliver a rapid change in electrical current over time,  $dI/dt$ .

[0007] In certain embodiments, the present invention may provide an energy generating system broadly comprising a ferroelectric energy generator configured to generate a pulse of voltage between a pair of output terminals, and a voltage-controlled switch that is connected in series with one of the output terminals of the ferroelectric energy generator wherein the voltage-controlled switch closes when the generated voltage pulse reaches a breakdown level.

[0008] In other embodiments, the present invention may provide a method of generating electrical energy broadly comprising the steps of compressing a ferroelectric element to generate a voltage between a pair of output terminals, closing a switch connected in series with one of the output terminals when the voltage reaches a first level, and delivering a quick pulse of electric current when the switch closes to a load coupled to the ferroelectric element and the switch.

[0009] This summary is provided to introduce a selection of concepts in a simplified form that are further described below in the detailed description. This summary is not intended to

identify key features or essential features of the claimed subject matter, nor is it intended to be used to limit the scope of the claimed subject matter.

[0010] Other aspects and advantages of the present invention will be apparent from the following detailed description of the embodiments and the accompanying drawing figures.

BRIEF DESCRIPTION OF THE DRAWING FIGURES

[0011] Embodiments of the present invention are described in detail below with reference to the attached drawing figures, wherein:

[0012] FIG. 1 is a block diagram of a ferroelectric energy generator system constructed in accordance with various embodiments of the present invention;

[0013] FIG. 2 is a top view of the energy generator of FIG. 1;

[0014] FIG. 3 is a bottom view of the energy generator of FIGS. 1-2;

[0015] FIG. 4 is a block diagram of a voltage-controlled switch;

[0016] FIG. 5 is a block schematic diagram of a first embodiment of the ferroelectric energy generator system positioned in a detonation tank;

[0017] FIG. 6 is a plot of the voltage versus time for a first output waveform of the ferroelectric energy generator system;

[0018] FIG. 7 is a block schematic diagram of a second embodiment of the ferroelectric energy generator system positioned in a detonation tank;

[0019] FIG. 8 is a schematic diagram of a circuit that is equivalent to the second embodiment of the ferroelectric energy generator system; and

[0020] FIG. 9 is a plot of the voltage versus time for a second output waveform of the ferroelectric energy generator system.

[0021] The drawing figures do not limit the present invention to the specific embodiments disclosed and described herein. The drawings are not necessarily to scale, emphasis instead being placed upon clearly illustrating the principles of the invention.

DETAILED DESCRIPTION OF THE EMBODIMENTS

[0022] The following detailed description of the invention references the accompanying drawings that illustrate specific embodiments in which the invention can be practiced. The embodiments are intended to describe aspects of the invention in sufficient detail to enable those skilled in the art to practice the invention. Other embodiments can be utilized and changes can be made without departing from the scope of the present invention. The following detailed description is, therefore, not to be taken in a limiting sense. The scope of the present invention is defined only by the appended claims, along with the full scope of equivalents to which such claims are entitled.

[0023] The present application is related to U.S. patent application titled "FERROELECTRIC ENERGY GENERATOR, SYSTEM, AND METHOD," Ser. No. 11/461,349, filed Jul. 31, 2006. The identified earlier-filed application is hereby incorporated by reference in its entirety into the present application.

[0024] A ferroelectric energy generator system **10** may be utilized as an energy source with power conditioning abilities to supply energy to other components, systems, or loads **11**, as seen in FIG. 1. Power conditioning may involve controlling a property or aspect of the energy that a source is able to deliver. For example, the ferroelectric energy generator system **10** with power conditioning abilities may be able to deliver a pulse of electric voltage or a pulse of electric current.

[0025] One application that may utilize the ferroelectric energy generator system **10** is a microwave transmitter. The output of the ferroelectric energy generator system **10** may be coupled to an antenna, that acts as the load **11**. The ferroelectric energy system **10** may deliver a burst of electric current that is switched on very quickly. Hence, the change in electrical current over time,  $dl/dt$ , may be very large. The rapid delivery of electrical current to the antenna may drive the antenna into oscillation that generates microwave radiation.

[0026] The ferroelectric energy generator system **10**, constructed in accordance with various embodiments of the present invention and shown in FIGS. 1-3 and 7, broadly comprises an explosive unit **12**, a ferroelectric element **14**, a generator body **16**, a first output terminal **18**, a second output terminal **20**, and a voltage-controlled switch **22**.

[0027] The explosive unit **12** generally provides directional explosive shock wave energy to the ferroelectric element **14**. Accordingly, the explosive unit **12** may be coupled to the generator body **16** in close proximity to the ferroelectric element **14**. The explosive unit **12** may include an explosive charge **24** and a detonator **26**.

[0028] The explosive charge **24** may be any explosive element operable to initiate a shock wave that propagates at least partially through the ferroelectric element **14**. The explosive charge **24** may include high explosive elements to reduce the volume and amount of material required to initiate the desired shock wave discussed below. In various embodiments, the explosive charge **24** may include or is otherwise formed from a cyclotrimethylene trinitramine (RDX) high explosive or other detonable high explosive.

[0029] The explosive charge **24** may present a shape having a tapered width, such that the explosive charge **24** may include a narrow end and an opposing widened end, with the widened end being of greater dimension, such as width, than the narrow end. In various embodiments, the explosive charge **24** may present a generally conical configuration having a base **28** and an apex **30**. As shown in FIG. 1, the explosive charge **24** may be positioned such that the base **28** is directed towards the ferroelectric element **14** and the apex **30** is directed away from the ferroelectric element **14**. The explosive charge **24** is coupled with the detonator **26** in proximity to the apex **30**. Such a configuration facilitates generation of the desired transverse shock wave discussed below. Utilization of a malleable explosive also facilitates formation of the various embodiments of the present invention by enabling the explosive charge **24** to be easily formed into the desired conical configuration. However, as should be appreciated, the explosive charge **24** may present any shape and be malleable or non-malleable.

[0030] The detonator **26** is generally coupled with the explosive charge **24** to enable detonation of the explosive charge **24** and generation of the desired shock wave. As discussed above, the detonator **26** may be coupled with the apex **30** of the explosive charge **24**. However, the detonator **26** may be directly or indirectly coupled in any configuration with the explosive charge **24**. In various embodiments, the

detonator **26** includes an RD-501 EBW detonator. However, the detonator **26** may include any elements operable to detonate the explosive charge **24** and may be specifically configured for compatibility with the explosive charge **24**. The detonator **26** may be coupled with an external control system to control the function and timing of the detonation of the explosive charge **24**.

[0031] The ferroelectric element **14** may include any ferroelectric or piezoelectric material. "Ferroelectric material" as utilized herein refers to any material that possesses a spontaneous dipole moment. The spontaneous dipole moment provided by ferroelectric materials is in contrast to the permanent magnetic moment provided by ferromagnetic materials. In various embodiments, the ferroelectric element **14** is comprised of lead zirconate titanate,  $PbZr_{0.52}Ti_{0.48}O_3$  (PZT). Utilization of lead zirconate titanate is desirable in various embodiments as it provides a marked piezoelectric effect. Specifically, when compressed and/or depolarized, lead zirconate titanate will develop a substantial voltage difference across two of its faces, as is discussed below in more detail. However, in some embodiments, the ferroelectric element **14** may comprise barium titanate,  $BaTiO_3$ , or other ferroelectric or piezoelectric materials. The ferroelectric element **14** may be comprised of hard or soft lead zirconate titanate.

[0032] The ferroelectric element **14** may present a generally rectangular configuration to enable the ferroelectric element **14** to present opposed ends and four sides extending therebetween. However, as should be appreciated, the ferroelectric element **14** may be formed in any shape or configuration, including cylindrical and non-uniform configurations.

[0033] The polarization of the ferroelectric element **14** is represented by a polarization vector **32**. As shown in FIG. 1, the polarization vector **32** is generally transverse to the longitudinal axis of the ferroelectric element **14**. As discussed in more detail below, such a configuration facilitates the generation of energy by allowing a shock wave **34** generated by detonation of the explosive charge **24** to propagate generally transverse to the polarization vector **32** instead of generally parallel to the polarization vector **32**. However, the ferroelectric element **14** may be polarized in any direction or orientation.

[0034] When the ferroelectric energy generator system **10** is operable, in some embodiments, the generated shock wave **34** may not necessarily be transverse to the polarization vector **32** of the ferroelectric element **14**. For instance, the generated shock wave **34** may propagate through the ferroelectric element **14** at any angle relative to the polarization vector **32**, including non-transverse, parallel, or any other angle, depending on the particular configuration of the ferroelectric element **14** and explosive charge **24**.

[0035] Consequently, the present invention enables the ferroelectric element **14** to be compressed and depolarized through direct shock wave action, thereby increasing the reliability, effectiveness, and efficiency of the ferroelectric energy generator system **10**. As should be appreciated, the ferroelectric element **14** does not need to be completely or totally compressed and depolarized by the shock wave **34**. Thus, embodiments of the present invention may generate energy through only partial depolarization and compression of the ferroelectric element **14**.

[0036] The ferroelectric element **14** may present any size. For example, the size, such as the volume, length, and width of the ferroelectric element **14** may be varied to provide certain or desired voltages. In various embodiments, the fer-

roelectric element **14** presents a generally elongated rectangular configuration having dimensions of approximately 12.7 mm by 12.7 mm by 51 mm. In some embodiments, the ferroelectric element **14** may be an EC-64 bar of lead zirconate titanate sold by EDO Corp. of New York, N.Y. In other embodiments, the ferroelectric element **14** may be a PZT 95/5 element from TRS Technologies, Inc. of State College, Pa.

[0037] The ferroelectric element **14** may include a third output terminal **36** and a fourth output terminal **38** that are coupled to the sides of the ferroelectric element **14**, such that shock wave compression and depolarization of the ferroelectric element **14** generates a voltage across the third output terminal **36** and the fourth output terminal **38**. Accordingly, the third output terminal **36** and the fourth output terminal **38** may possess a polarity. For example, the third output terminal **36** may generate a relatively positive voltage and the fourth output terminal **38** may generate a relatively negative voltage, or vice-versa.

[0038] In various embodiments, a plurality of ferroelectric elements **14** may be utilized in the same ferroelectric energy generator system **10**, as shown in FIGS. 1, 2, 5, and 7, wherein three ferroelectric elements **14** are utilized. The additional ferroelectric elements **14** may be included in order to meet greater energy output requirements or other design criteria or specifications. In such embodiments, the ferroelectric elements **14** are typically positioned and oriented such that their polarization vectors **32** are aligned. Furthermore, the ferroelectric elements **14** may be connected in a series fashion, with the positive terminal of one ferroelectric element **14** connected to the negative terminal of the next, such that the voltage output of the plurality of ferroelectric elements **14** is the sum of the voltage outputs of each individual ferroelectric element **14**. In alternative embodiments, the plurality of ferroelectric elements **14** may be connected in a parallel fashion, with the positive terminals of all the ferroelectric elements **14** connected together and the negative terminals of all the ferroelectric elements **14** connected together, such that the current output of the plurality of ferroelectric elements **14** is the sum of the current output of each of the ferroelectric elements **14**.

[0039] The body **16** of the ferroelectric energy generator system **10** generally provides a medium in which to connect the ferroelectric element **14** with the voltage-controlled switch **22**, the first output terminal **18**, and the second output terminal **20**. The body **16** further holds the ferroelectric element **14** in proximity to the explosive unit **12**. In various embodiments, the ferroelectric energy generator system **10** may further include a housing (not shown) to surround the body **16** and the explosive unit **12** to protect the ferroelectric energy generator system **10** during transport and handling.

[0040] The body **16** may present any shape or configuration. In some embodiments, the body **16** may present a generally cylindrical or tubular configuration as shown in FIGS. 1-3. In some embodiments employing a cylindrical configuration, the body **16** has a length of approximately 100 mm and an outer diameter of approximately 55 mm. Thus, the present invention may be compactly employed to provide large amounts of electrical energy. However, the body **16** may be any size in order to include any number of ferroelectric elements **14**.

[0041] The body **16** may be at least partially filled with a dielectric filling to facilitate positioning and shock matching of the ferroelectric element **14**. For instance, the dielectric

filling may include epoxy or any other hardening substance to solidify the position of the ferroelectric element **14** and the explosive charge **24**.

[0042] The voltage-controlled switch **22** generally enables the ferroelectric energy generator system **10** to deliver energy from the ferroelectric element **14** to the load **11** or another component or system much more quickly than the system **10** would without the switch **22**. Thus, the ferroelectric element **14** acts as a source of voltage for the voltage-controlled switch **22**. As shown in FIG. 4, the voltage-controlled switch **22** may include a fifth output terminal **40**, a sixth output terminal **42**, a first electrode **44**, a second electrode **46**, a dielectric film **48**, and a switch body **50**. As explained in more detail below, the voltage-controlled switch **22** is normally open but closes when the voltage across the fifth output terminal **40** and the sixth output terminal **42** reaches or exceeds a breakdown level.

[0043] The fifth output terminal **40** and the sixth output terminal **42** generally couple the voltage-controlled switch **22** to other components. The fifth output terminal **40** may be coupled to the third output terminal **36** (of the ferroelectric element **14**), while the sixth output terminal **42** may be coupled to the first output terminal **18** (of the ferroelectric energy generator system **10**). The fifth output terminal **40** and the sixth output terminal **42** may typically be manufactured from electrically-conductive material.

[0044] The first electrode **44** and the second electrode **46** generally hold electrical charge such that there is a potential difference, or voltage, between the first electrode **44** and the second electrode **46**. Accordingly, the first electrode **44** and the second electrode **46** may typically be manufactured from electrically-conductive material. In various embodiments, the first electrode **44** may be spherical shaped and the second electrode **46** may be of square or rectangular plate shape. In general, the first electrode **44** and the second electrode **46** may assume any shape or dimension. However, one of either the first electrode **44** or the second electrode **46** may have a curved, spherical, or otherwise rounded shape to counter physical edge-effect phenomena that a flatter electrode **44** may possess. These phenomena may lead to a reduced and/or inconsistent switching voltage or to premature closing of the voltage-controlled switch **22**. The shape and dimension of the first electrode **44** and the second electrode **46** may depend on the switching voltage or other parameter of the specific application of the voltage-controlled switch **22**.

[0045] The dielectric film **48** generally controls the function of the voltage-controlled switch **22**. When the voltage between the first electrode **44** and the second electrode **46** remains below the breakdown level, the dielectric film **48** is insulating, and the voltage-controlled switch **22** remains open. When the voltage between the first electrode **44** and the second electrode **46** reaches the breakdown level, the dielectric film **48** loses its insulating properties and becomes conductive, thereby closing the voltage-controlled switch **22**. Since the ferroelectric element **14** supplies the voltage to the voltage-controlled switch **22**, the ferroelectric element **14** must be able to supply at least the breakdown voltage level, and preferably even more than the breakdown level.

[0046] The dielectric film **48** is generally positioned between the first electrode **44** and the second electrode **46**, and in contact with both. In various embodiments, the dielectric film **48** may be of similar shape to the second electrode **46**,



as seen in FIG. 4. Although, in general, the dielectric film 48 may be shaped similar to either the first electrode 44 or the second electrode 46 or both.

[0047] The dielectric film 48 may be created using any dielectric material. In various embodiments, the dielectric film 48 may be created using solid materials including a polymer or polyimide such as Kapton, mylar, parylene, Teflon, or a similar material. The dielectric strength of the material and the thickness of the dielectric film 48 may determine the voltage at which the dielectric film 48 breaks down and becomes conductive. Generally, a thicker film 48 and a higher dielectric strength will lead to a higher breakdown voltage. The thickness of the dielectric film 48 may also determine the closing time of the switch 22, or the time it takes for the dielectric film 48 to change from mostly insulating to mostly conductive. Generally, a thinner film 48 will lead to a shorter closing time or a faster voltage-controlled switch 22. Furthermore, the thickness of the film 48 may determine the electrical resistance and inductance of the conductive channel once the film 48 breaks down. Generally, a thinner film 48 will lead to smaller resistance and inductance. These properties may determine the performance of the voltage-controlled switch 22.

[0048] As may be appreciated, the thickness of the dielectric film 48 and the dielectric strength, as determined by the material used, may be chosen to achieve a desired breakdown voltage, closing time, or other performance parameter. Exemplary embodiments of the voltage-controlled switch 22 have preferable closing times from about 100 picoseconds (ps) to about 50 nanoseconds (ns), more preferable closing times from about 100 ps to about 5 ns, and most preferable closing times from about 100 ps to about 500 ps, depending on the properties of the film 48 employed, such as thickness of the film 48 and dielectric strength. Embodiments of the dielectric film 48 made of Kapton have a thickness of approximately 75 microns and a breakdown voltage of approximately 35 kilovolts (kV), a thickness of approximately 125 microns and a breakdown voltage of approximately 75 kV, and a thickness of approximately 150 microns and a breakdown voltage of approximately 100 kV.

[0049] The thickness of the dielectric film 48 and its dielectric strength were chosen to produce the ranges of closing time and breakdown voltage discussed above in order to work with a particular application. For other applications, the voltage-controlled switch 22 may have a higher or a lower breakdown voltage than discussed above. The voltage-controlled switch 22 may also have a closing time that is longer than shown above—perhaps even on the order of microseconds.

[0050] The switch body 50 generally provides a medium in which to properly house the fifth output terminal 40, the sixth output terminal 42, the first electrode 44, the second electrode 46, and the dielectric film 48. The switch body 50 further electrically insulates and provides structural strength for the components during handling and installation of the voltage-controlled switch 22. The switch body 50 may be manufactured from a dielectric material such as polyurethane.

[0051] The voltage-controlled switch 22 may present any shape or size. For example, the voltage-controlled switch 22 may be spherical, tubular or cylindrical, cubic or rectangular-box shaped. The volume of the voltage-controlled switch 22 may range from about 1 centimeter<sup>3</sup> (cm<sup>3</sup>) down to about 0.25 cm<sup>3</sup>.

[0052] In various embodiments, the ferroelectric energy generator system 10 may include a plurality of voltage-con-

trolled switches 22 in order to control the performance characteristics of the system 10. For example, the amplitude, the rise time, or other waveform characteristics of either the voltage or the current output of the ferroelectric energy generator system 10 may be modified by increasing the number of voltage-controlled switches in the system 10. The additional voltage-controlled switches may be connected in series, in parallel, or configurations that are a series-parallel combination.

[0053] The first output terminal 18 and the second output terminal 20 generally provide electrical output of the ferroelectric energy generator system 10 in order to electrically couple the ferroelectric energy generator system 10 to another component or system. Thus, the first output terminal 18 and the second output terminal 20 are typically constructed of metallic material, such as wiring or cabling. As is known in the art, the first output terminal 18 and the second output terminal 20 may be coated or covered with insulating material with the end of each terminal exposed. The first output terminal 18 and the second output terminal 20 may be positioned in proximity to one another to protrude from one end of the body 16—typically the end of the body 16 opposing the explosive unit 12. The first output terminal 18 may be coupled to the sixth output terminal 42 (from the voltage-controlled switch 22). The second output terminal 20 may be coupled to the fourth output terminal 38 (from the ferroelectric element 14). Furthermore, the first output terminal 18 and the second output terminal 20 may possess a polarity. In various embodiments, the first output terminal 18 may have a relatively positive voltage while the ferroelectric energy generator system 10 is active, and the second output terminal 20 may have a relatively negative voltage while the ferroelectric energy generator system 10 is active. In other embodiments, the polarity of the first output terminal 18 and the second output terminal 20 may be reversed.

[0054] The ferroelectric energy generator system 10 may operate as follows. The detonator 26 of the explosive unit 12 may be energized from an external source. Consequently, the explosive charge 24 may be detonated resulting in an explosive shock wave 34 propagating toward the ferroelectric element 14. The shock wave 34 may compress the ferroelectric element 14 generally transverse to its polarization vector 32. Upon compression, the ferroelectric element 14 may generate a high amplitude pulse of voltage across the third output terminal 36 and the fourth output terminal 38.

[0055] The generation of voltage from the ferroelectric element 14 may lead to an accumulation of charge on the first electrode 44 of the voltage-controlled switch 22, thus creating a voltage across the terminals of the switch 22 (the fifth output terminal 40 and the sixth output terminal 42). Initially, the dielectric film 48 may be insulating and the voltage-controlled switch 22 may be open. As charge builds on the first electrode 44, the voltage across the terminals of the switch 22 and in turn, across the dielectric film 48, increases to the level of the breakdown voltage of the dielectric film 48. Once this happens, the dielectric film 48 becomes conductive and an electric path is established from the first electrode 44 to the second electrode 46, the sixth output terminal 42, the first output terminal 18, and ultimately the load 11 of the ferroelectric energy generator system 10. The buildup of charge in the voltage-controlled switch 22 forces a pulse of electrical current to flow along the electrical path in a short amount of time. Thus, the ferroelectric energy generator system 10 may deliver a large change in current,  $dl/dt$ , to the load 11. Rise

times, which may be the time during which the current increases from 10% of its peak value to 90% of its peak value, of the change in current  $dl/dt$  may range from 100 ps to 10 ns.

[0056] Various embodiments of the ferroelectric energy generator system 10 were tested to compare the performance of a first embodiment 52 of the system 10 without the voltage-controlled switch 22 to a second embodiment 54 of the system 10 that includes the voltage-controlled switch 22.

[0057] The first embodiment 52 of the ferroelectric energy generator system 10 excluded the voltage-controlled switch 22, as shown in FIG. 5. Thus, the third output terminal 36 was coupled directly to the first output terminal 18. There were three EC-64 ferroelectric elements 14 connected in series. The first embodiment 52 was placed in a detonation tank 56 with the first output terminal 18 and the second output terminal 20 extended through a plastic window 58, as seen in FIG. 5. An oscilloscope probe was connected to the first output terminal 18 and the second output terminal 20 to measure the open circuit voltage output of the first embodiment 52 of the ferroelectric energy generator system 10. The explosive unit 12 was detonated and the output voltage was recorded and displayed as a first waveform 60 in FIG. 6. As can be seen, the first waveform 60 has a peak voltage of approximately 121 kV and a rise time of approximately 2.2 microseconds ( $\mu$ s).

[0058] The second embodiment 54 of the ferroelectric energy generator system 10 was substantially similar to the system 10 of FIG. 1 and was placed in the detonation tank 56 with the first output terminal 18 and the second output terminal 20 extended through the plastic window 58, as shown in FIG. 7. There were three EC-64 ferroelectric elements 14 connected in series, and the voltage-controlled switch 22 had a breakdown voltage of approximately 35 kV. To measure the current output of the second embodiment 54, the first output terminal 18 and the second output terminal 20 were shorted together. An induced current probe 62, operable to measure the change in current over time,  $dl/dt$ , was inserted in the loop of the first output terminal 18 and the second output terminal 20. In various embodiments, the induced current probe 62 was a Prodyne I-265 probe, manufactured by Prodyne, Inc. of Albuquerque, N. Mex. The induced current probe 62 measured  $dl/dt$ , from which the voltage could be derived through the relationship:  $dl/dt \times M$ , where M is the mutual inductance of the induced current probe 62.

[0059] An equivalent circuit to the second embodiment 54 of the ferroelectric energy generator system 10 is shown in FIG. 8 with the ferroelectric element 14 modeled as a voltage source 64 in series with a capacitance 66 and an impedance 68. The voltage-controlled switch 22 is coupled thereto. The first output terminal 18 and the second output terminal 20 shorted together are modeled as a transmission line impedance 70, with the induced current probe 62 in series.

[0060] The explosive unit 12 of the second embodiment 54 was detonated and  $dl/dt$  was measured and recorded by the induced current probe 62. The results are shown in a second waveform 72 of FIG. 9. As can be seen, the rise time of the second waveform 72 is on the order of 700 ps. Compared with the voltage rise time of approximately 2.2  $\mu$ s for the system 10 without the voltage-controlled switch 22, the system with the voltage-controlled switch 22 is able to deliver a change in electric current by several orders of magnitude. A system 10 such as the second embodiment 54 may be utilized with a microwave transmitter to deliver a burst of electric current that may drive the antenna into oscillation in order to generate microwave radiation.

[0061] Although the invention has been described with reference to the embodiments illustrated in the attached drawing figures, it is noted that equivalents may be employed and substitutions made herein without departing from the scope of the invention as recited in the claims.

Having thus described various embodiments of the invention, what is claimed as new and desired to be protected by Letters Patent includes the following:

1-8. (canceled)

9. The energy generating system of claim 11, wherein the dielectric film is solid material.

10. (canceled)

11. An energy generating system comprising:

a ferroelectric energy generator configured to generate a pulse of voltage between a pair of output terminals; and a voltage-controlled switch that is connected with one of the output terminals of the ferroelectric energy generator, wherein the voltage-controlled switch closes when the generated voltage pulse reaches a breakdown level, the voltage-controlled switch including—

a first output terminal and a second output terminal configured to couple the voltage-controlled switch to at least one component,

a first electrode and a second electrode coupled to the first output terminal and the second output terminal, respectively, and configured to possess a voltage therebetween, and

a dielectric film positioned between the first electrode and the second electrode and configured to become electrically conductive when the voltage between the first electrode and the second electrode reaches the breakdown level.

12. The energy generating system of claim 11, wherein closing the voltage-controlled switch delivers electric current to a load coupled to the energy generating system with a closing time between approximately 100 picoseconds to approximately 500 picoseconds.

13. The energy generating system of claim 11, wherein one of the first electrode or the second electrode has a spherical shape to avoid the dielectric film becoming electrically conductive before the breakdown level of voltage is reached.

14. The energy generating system of claim 11, wherein the ferroelectric generator includes—

a ferroelectric element,

an explosive charge, and

a detonator coupled with the explosive charge, wherein the detonator is configured to detonate the explosive charge to generate a shock wave that propagates at least partially through the ferroelectric element to generate the voltage across the output terminals.

15. The energy generating system of claim 14, wherein the ferroelectric element has a polarization represented by a polarization vector and the generated shock wave propagates at least partially through the ferroelectric element generally transverse to the polarization vector to at least partially depolarize the ferroelectric element.

16. The energy generating system of claim 14, wherein the explosive charge has a configuration presenting a narrowed end and a widened end that is wider than the narrowed end.

17. The energy generating system of claim 16, wherein the widened end of the explosive charge is directed towards the ferroelectric element, and the narrowed end of the charge is directed away from the ferroelectric element.

**18.** The energy generating system of claim **14**, further including a plurality of ferroelectric elements each having output terminals coupled therewith, the ferroelectric elements positioned such that detonation of the explosive charge causes the shock wave to propagate at least partially through each of the ferroelectric elements to generate a voltage across at least two of the output terminals.

**19-20.** (canceled)

**21.** The energy generating system of claim, wherein the first electrode has a spherical shape and the second electrode has a planar shape to avoid the dielectric film becoming electrically conductive before the breakdown level of voltage is reached.

**22.** The energy generating system of claim **11**, further including a body of dielectric material configured to house the first electrode, the second electrode, the dielectric film, at least a portion of the first output terminal, and at least a portion of the second output terminal.

**23.** The energy generating system of claim **11**, wherein the dielectric film is insulating when the voltage between the first electrode and the second electrode is below the breakdown level.

**24-28.** (canceled)

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