(12) INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(19) World Intellectual Property Organization

International Bureau





(10) International Publication Number WO 2017/076773 A1

(43) International Publication Date 11 May 2017 (11.05.2017)

(51) International Patent Classification: F24J 2/28 (2006.01) F24J 2/20 (2006.01) F24J 2/04 (2006.01)

(21) International Application Number:

PCT/EP2016/076109

(22) International Filing Date:

28 October 2016 (28.10.2016)

(25) Filing Language:

English

(26) Publication Language:

English

(30) Priority Data:

EP15020221.6 6 November 2015 (06.11.2015)

EP

(71) Applicant: TATA STEEL IJMUIDEN B.V. [NL/NL]; Wenckebachstraat 1, 1951 JZ Velsen-Noord (NL).

- (72) Inventors: WIP, Erik Petrus Johan; Tata Steel Nederland Technology B.V. - Group Intellectual Property Services 3G.37 PO Box 10000, 1970 CA Ijmuiden (NL). JENTINK, Christiaan; Tata Steel Nederland Technology B.V. Group Intellectual Property Services 3G.37 PO Box 10000, 1970 CA Ijmuiden (NL).
- (74) Agent: BLAUW, Frans, Gerard; PO Box 10000, 1970 CA IJmuiden (NL).

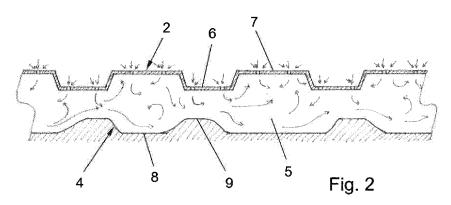
(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BN, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CZ, DE, DJ, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IR, IS, JP, KE, KG, KN, KP, KR, KW, KZ, LA, LC, LK, LR, LS, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PA, PE, PG, PH, PL, PT, QA, RO, RS, RU, RW, SA, SC, SD, SE, SG, SK, SL, SM, ST, SV, SY, TH, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM,

(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LR, LS, MW, MZ, NA, RW, SD, SL, ST, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, RU, TJ, TM), European (AL, AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MK, MT, NL, NO, PL, PT, RO, RS, SE, SI, SK, SM, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, KM, ML, MR, NE, SN, TD, TG).

Published:

with international search report (Art. 21(3))

(54) Title: TRANSPIRED SOLAR COLLECTOR



(57) Abstract: The invention relates to a transpired solar collector (1) comprising an absorber plate (2), provided with multiple perforations (3), and a back plate (4), wherein the absorber plate (2) and the back plate (4) define a collector space (5), wherein at least one of the absorber plate (2) and back plate (4) is profiled, the profile comprising one or more troughs and ridges (6, 7) and wherein the transpired solar collector (1) is designed to operate at low air approach velocities.





TRANSPIRED SOLAR COLLECTOR

Field of the invention

5

15

20

25

30

35

The invention relates to a transpired solar collector wherein outside air is heated by drawing outside air into the collector and leading the air through the collector. The heated outside air is subsequently used for purposes requiring heat such as interior heating, industrial processes and agricultural processes such as drying of goods and storing of products.

10 Background of the invention

A transpired solar collector comprises an absorber plate provided with multiple perforations wherein the absorber is part of an enclosure forming an air collector space. By providing a negative pressure in the collector space outside air is drawn through the perforations into the collector space. The negative pressure is often realized with a ventilation system, wherein the ventilation system is connected to the collector space by means of a duct. The heated air is led through this duct to the interior of a building for heating purposes or to processing equipment.

Transpired solar collectors are in most cases mounted on an outside wall of a building, on a roof of a building or both in a position that as much solar radiation is captured as possible. The wall or roof of the building may form part of the collector space if the wall or roof is suitable for that purpose, which in the first place means that it has to be sufficient insulated to prevent temperature losses.

Transpired solar collectors according to the prior art are very efficient when it comes to heating air at high approach velocities, which according to literature are velocities over 0.02 m/s. The approach velocity is the speed with which outside air passes through the perforations in the absorber plate into the collector space. At high approach velocities large volumes of air pass through the perforations in the absorber plate of the transpired solar collector. With high approach velocities the efficiency is high meaning that much of the solar energy absorbed in the absorber plate is transferred to the outside air passing through the absorber plate. However, because of the large velocity and consequently the large volumes of air there is only a relatively small increase in the temperature of the outside air.

At lower approach velocities and therefore at lower air volumes the outside air passing through the perforations in the absorber plate could be heated to higher temperatures. However, the efficiency of transpired solar collectors rapidly decreases at lower approach velocities, wherein the decrease in efficiency is

5

10

15

20

25

30

35

exponentially or about exponentially with respect to the efficiency at higher approach velocities. This is because much of the heating of the air drawn into the collector space takes place at the outside of the absorber plate and for that reason is wind-sensitive. At lower approach velocities the influence of the wind is far larger than at high approach velocities. This practically limits the application of known transpired solar collectors to circumstances where the user is satisfied with a limited increase in temperature.

Objectives of the invention

It is an objective of the present invention to provide a transpired solar collector wherein air is heated to higher temperatures.

It is an objective of the present invention to provide a transpired solar collector with an improved heat exchange at low approach velocities.

It is another objective of the present invention to provide a transpired solar collector wherein the heat transfer inside the transpired solar collector is increased considerably.

It is another objective of the present invention to provide a transpired solar collector which can be manufactured using standard profiled metal plates and/or panels.

It is another objective of the present invention to provide a transpired solar collector which can be manufactured easily and at low costs.

Description of the invention

The invention relates to a transpired solar collector as defined in claims 1-11 and a transpired solar collector system as defined in claims 12-14.

With conventional transpired solar collectors the areas immediately around the perforations on the exterior of the absorber plate heat up outside air before it is drawn through the perforations. The largest heat gain of the outside air comes from these surrounding areas. A further part of the total heat gain is provided by the edges of the perforations, which heat up the air when passing through the perforations. Finally, there is a small contribution to the total heat gain from the interior side of the absorber plate.

With high approach velocities, that is the speed with which the air approaches and passes through the perforations of the absorber plate, the known transpired solar collectors are very efficient and the performance is hardly dependent on any effect of the wind. However, with low approach velocities, the boundary layer of air outside the

collector is easily disrupted and with these low approach velocities the known transpired solar collectors are much less efficient.

One or more of the objectives of the invention are realized by providing a transpired solar collector comprising an absorber plate provided with multiple perforations and a back plate, wherein the absorber plate and the back plate define a collector space, wherein outside air enters the collector space through the perforations and wherein the collector space is provided with at least one air outlet, wherein at least one of the absorber plate and back plate is profiled, wherein the profile comprises one or more troughs and ridges and wherein the longitudinal direction of the troughs and ridges of at least one of the absorber plate and back plate is at an angle to the general direction of the air flow in the collector space.

5

10

15

20

25

30

35

Because of the increased surface area the contact of the incoming air with the transpired solar collector inside the collector space is prolonged resulting in an increased heat transfer. Preferably it is provided that the longitudinal direction of the troughs and ridges of at least one of the absorber plate and back plate is at an angle to the general direction of the air flow in the collector space. As a result of the varying cross-sectional area of the collector space in the general direction of the air flow the velocity of the air flow will be high where the cross-sectional area is small and low where the cross-sectional area is large. At the location with lower air flow velocities the residence time of the air is longer resulting in an increased air temperature.

At the transition from small to large cross-sectional area and vice versa the air will respectively be compressed and expanded resulting in turbulence in the air flow within the collector space. Because of the turbulent air laminar flow along the absorber plate is prevented which in turn results in mixing of the air by means of which heated air is directed away from the absorber plate and air of lower temperature is coming into contact with the absorber plate. Instead of that the temperature of part of the air is further increased through contact with the collector space side of the absorber plate all the air or almost all of the air inside the collector space is further heated through contact with the absorber plate. This is an important advantage over the prior art, see for instance US4899728, wherein the air flow is laminar.

Preferably the absorber plate is profiled because most of the energy is at least initially stored in the absorber plate.

Preferably both the absorber plate and the back plate are profiled. By

providing that both the absorber plate and back plate are profiled has its effect on the flow of the air in the collector space by means of which the time of the air inside the collector space will be further increased and the contact of the air with the

- 4 -

absorber plate will also be further increased.

5

10

15

20

25

30

35

It is further provided that the profile of at least one of absorber plate and back plate is rectangular or trapezoidal in transverse cross-section. The use of profiled plates result in a turbulent air flow inside the collector space which is further enhanced by using a rectangular or trapezoidal profile because of the sharp transitions between successive planes of the profile. In order to generate as much turbulence as possible and at the same time prevent that air might be trapped in the troughs of such a trapezoidal profiled absorber plate and/or back plate the angle of the trapezoidal profiled absorber plate and/or back plate is in the range of >90-140°, preferably in the range of 105-135°. For the avoidance of doubt this is the angle between successive planes of the profile.

The troughs and ridges of the absorber plate and the back plate form a number of channels which dependent on the orientation with respect to each other has influence on the air flow in the collector space and therewith the turbulence of the air flow and as a result the heat exchange between the transpired solar collector and the air. The general air flow induced in the collector space by ventilation means or the like depends on the position of these means with respect to the collector space. With parallel troughs and ridges of the absorber plate and back plate turbulence and contact of the air with the absorber plate and back plate will be optimal if the general air flow in the collector space is transverse to the troughs and ridges of both the absorber plate and back plate.

It is preferably provided that the longitudinal direction of the trough and ridges of the absorber plate and the back plate run at an angle to each other. With this embodiment the interior of the collector space is shaped into one or more air channels in which the air flows in a controlled way from the absorber plate through the collector space to outside the collector space where the heated air is used for one or more possible purposes. Because the troughs and ridges of absorber plate and back plate run at an angle with respect to each other the channels are shaped such that the cross-sectional surface area of the channels vary along the length direction of the channels. As a result of this varying channel shape the air velocity in the channels will vary, a high velocity where the cross section is narrow and a low velocity where the cross section is wide. The variation in air velocity and channel geometry results in a

5

10

15

20

25

30

35

- 5 -

turbulent air flow. This turbulence improves the contact between air and the inside surface of the absorber plate significantly. A third effect is that the air will be longer in contact with the inside surface of the absorber plate, at locations where the air velocity is low. These effects together generate a much better heat transfer, especially at lower approach velocities.

For practical reasons it is provided that in such an embodiment the longitudinal direction of the trough and ridges of the absorber plate and the back plate run transverse to each other. In transverse direction will mean in most cases at a right angle to each other in order to facilitate the manufacturing and mounting of the transpired solar collector.

According to a further aspect it is provided that the absorber plate and back plate are mounted against each other. The direct mounting of the absorber plate against the back plate results in that heat will be conducted from the absorber plate to the back plate, which further increases the heat transfer to the air inside the collector space. A further advantage of mounting absorber plate and back plate against each other is that the construction and mounting of the transpired solar collector becomes very easy.

By providing that the absorber plate and/or back plate comprise one or more profiled metal panels, for which a choice can be made from a wide range of profiled metal panels available in the industry, the construction and mounting of the transpired becomes even more cost-effective.

If the back plate is to be mounted against a non-insulated part of a wall or a roof it is provided that the back plate is formed by one or more insulated composite profiled panels. These composite profiled panels have an internal insulation layer of for instance a foam material which if off sufficient thickness will easily give the desired degree of insulation.

Further a transpired solar collector system is provided comprising a transpired solar collector as described above, a duct connected to the air outlet of the transpired solar collector and means connected to the duct to provide a negative pressure in the duct and the collector space, wherein the air outlet is provided along at least part of the length of a side of the transpired solar collector.

Preferably the air outlet is provided at a side of the transpired solar collector at the end of the troughs with the largest cross-sectional area.

A connecting channel is provided in order to connect the air outlet with the duct wherein the connecting channel has a first connection to connect to the air

- 6 -

outlet of the transpired solar collector and a second connection to connect to the duct. Such a connecting channel is a transition part between the air outlet formed at the side of the transpired solar collector by the absorber plate and back plate and a duct of for instance circular, square or rectangular cross-section.

In a further embodiment a connecting channel is provided to connect at least two transpired solar collectors to the duct. With transpired solar collectors with the air outlet at the side of the collector such a connecting channel is mounted between two transpired solar collectors to guide the heated air of both collectors through the same duct.

10

20

5

Brief description of the drawings

The invention will be further explained on hand of the drawing, in which:

Fig.1 shows a cross-section of a known transpired solar collector,

Fig.2 15 shows a cross- section of a transpired solar collector with profiled absorber plate and back plate,

Fig.3 shows a transpired solar collector in perspective with profiled absorber plate and back plate with parallel troughs and ridges,

Fig.4a-c shows a transpired solar collector in perspective with a profiled absorber plate and a single channel in a supporting structure as back plate and cross-sections transverse and parallel to the troughs and ridges,

Fig.5a-c shows a transpired solar collector in perspective with profiled absorber plate and back plate with transverse troughs and ridges, wherein the troughs in the absorber plate form horizontal channels and crosssections transverse and parallel to the troughs and ridges, and

Fig.6a-c shows a transpired solar collector in perspective with profiled absorber plate and back plate with transverse troughs and ridges, wherein the troughs in the back and absorber plate form horizontal channels and cross-sections transverse and parallel to the troughs and ridges.

30

35

25

Detailed description of the drawings

Fig.1 shows a cross- section of a known transpired solar collector 1 with an absorber plate 2, provided with perforations 3, and a back plate 4. By applying a negative pressure in the collector space, outside air is drawn through perforations 3 in the collector space 5. Applying such a negative pressure is for instance accomplished by means of a ventilator in a duct connected to the air outlet of the

-.7 -

transpired solar collector. The difference between the pressure inside the collector space 5 and outside atmospheric pressure is such that the outside air is drawn into the collector space with a high approach velocity. Because of the high approach velocity the outside wind conditions cause little or no disturbance in the air flow resulting in a high efficiency, that is much of the solar energy is transferred to the air drawn into the collector space. Although the efficiency of such a known transpired solar collector is high the temperature increase of the air is only limited because of the large volume of air drawn into the collector space per unit of time.

5

10

15

20

25

30

35

Fig.2 shows a cross-section of a transpired solar collector 1 with profiled absorber plate 2 and back plate 4, wherein the troughs and ridges 6,7 of absorber plate 2 and the troughs and ridges 8,9 of back plate 4 run parallel to each other. Back plate 4 is formed in the supporting structure of the transpired solar collector 1 such as a wall of a building.

The air drawn into the collector space 5 through the perforations 3 is guided by means of the negative pressure in a direction transverse to the troughs and ridges to outside the collector space where the heated air is needed. By guiding the air through the channel along these troughs and ridges 6-9, that is through sections with successive narrow and wide sections, results in higher and lower air velocities and in turn turbulence and vortices in the air. As a result the time during which the air is guided from perforation 3 to the air outlet of the transpired solar collector increases as well as the contact of the air with the interior side of the absorber plate 2, resulting in an increased temperature of the air leaving the collector space. This temperature is further increased by using a limited negative pressure inside the collector space, resulting in a lower approach velocity and a longer travel time of the air through the collector space. Although the lower approach velocity may result in disturbance of the air drawn into the transpired collector limiting the efficiency, the overall result is that the air leaving the collector space is heated to a higher temperature than realised with the known transpired solar collectors. The increase in temperature makes this transpired solar collector technically and economically more suitable for processes that require higher temperature increases, such as room heating.

Fig.3 shows schematically a view in perspective of a transpired solar collector 1 as in fig.2 with the difference that the back plate 4 in this embodiment is made from a profiled sheet material, for instance a metal profiled sheet material. Since the collector space should be a closed space except for the outlet for the heated air, filler material 10 is provided where necessary along the sides of the collector space

- 8 -

5, in the figure only shown for the top and bottom sides. Instead of or in combination with this filler material closure caps can be provided or the rims of the absorber plate 3 and the back plate can be profiled in order to provide an airtight closure of the collector space.

5

10

15

20

25

30

35

Fig.4a shows a transpired solar collector 1 in perspective with a profiled absorber plate 2 and a single channel 11 in a supporting structure for the profiled absorber plate 2, such as the wall of a building. The single channel 11 functions as a back plate. Fig.4b shows a transverse cross-section with the air outlet of the collector space at the right hand side in the figure. Fig.4c shows a cross-section through a ridge 7 parallel to the troughs and ridges 6,7 in the absorber plate 2.

Fig.5a shows a transpired solar collector 1 in perspective with profiled absorber plate 2 and back plate 4 wherein the troughs and ridges 6-9 of absorber plate 2 and back plate 4 run transverse to each other. The back plate 4 is provided with three parallel channels 12,13,14. These about horizontal channels 12,13,14 have exit openings at the right hand side of the figure, as is also visible in the transverse cross-section according to fig.5b. Fig.5c shows a cross-section transverse to the channels 12,13,14.

Fig.6a-c show a transpired solar collector 1 in perspective similar to the one shown in fig.5a-c with the difference that the channels 12,13,14 are now in the absorber plate 2 and that the back plate 4 has troughs and ridges 8,9 running in an about vertical direction.

The transpired solar collector 1 according to fig.5 and fig.6 has a construction wherein the absorber plate 2 and the back plate 4 are mounted against each other. With absorber plate 2 and the back plate 4 both made from a heat conducting material, for example profiled metal plates part of the heat of the absorber plate 2 is conducted to the back plate 4, which is beneficial for the heat exchange with the air inside the collector space 5.

The length of a trough or channel is preferably in the range of 2-12 meters, more preferably in the range of 4-9 meters.

Another important dimension is the ratio between the depth of the troughs of the absorber plate and the depth of the troughs of the back plate which are in the range of 1:1 - 1:3 preferably 1:1 - 1:2. If the depth of the troughs is too large this will result in dead zones with stagnant air resulting in a reduced heat exchange, if the channels are too deep relative to the transverse ridges, then the turbulence generation becomes weak and hence for the heating effect insignificant. The given depth ratio of

the troughs is most effective with the absorber plate and back plate mounted against each other.

-9-

The performance of the transpired solar collector according to the invention has been measured and compared to existing transpired solar collectors. At a low approach velocity of 0,014 m/s a collector according to the invention has an efficiency of ~60%, resulting in measured temperature increases of 32°C.

5

10

Transpired solar collector according to known technology have an efficiency of ~45% as documented in "Solar air systems – a design handbook" of the Solar heating and cooling executive committee of the International Energy Agency, Editors: S. Robert Hastings, Ove Mørck, James & James Science publishers Itd, London UK, 2000.

CLAIMS

5

10

20

25

- 1. Transpired solar collector comprising an absorber plate provided with multiple perforations and a back plate, wherein the absorber plate and the back plate define a collector space, wherein outside air enters the collector space through the perforations and wherein the collector space is provided with at least one air outlet, characterised in that both the absorber plate and back plate are profiled, wherein the profiles comprises one or more troughs and ridges and wherein the longitudinal direction of the troughs and ridges of at least one of the absorber plate and back plate is at an angle to the general direction of the air flow in the collector space.
- 2. Transpired solar collector according to claim 1, wherein the profile of at least one of absorber plate and back plate is rectangular or trapezoidal in transverse cross-section.
 - 3. Transpired solar collector according to claim 2, wherein the angle of the trapezoidal profiled absorber plate and/or back plate is in the range of > 90-140°, preferably in the range of 105-135°.
 - 4. Transpired solar collector according to any one of claims 1-4, wherein the longitudinal direction of the trough and ridges of the absorber plate and the back plate run at an angle to each other.

5. Transpired solar collector according to any of the preceding claims, wherein the longitudinal direction of the trough and ridges of the absorber plate and the back plate run transverse to each other.

- 30 6. Transpired solar collector according to any of the preceding claims, wherein the distance between successive ridges is different for absorber plate and back plate.
- 7. Transpired solar collector according to any of the preceding claims, wherein the length of a trough is preferably in the range of 2-12 meters, more preferably in the range of 4-9 meters.

8. Transpired solar collector according to any of the preceding claims, wherein the ratio between the depth of the troughs of the absorber plate and the depth of the troughs of the back plate are in the range of 1:1 - 1:3, preferably 1:1 - 1:2.

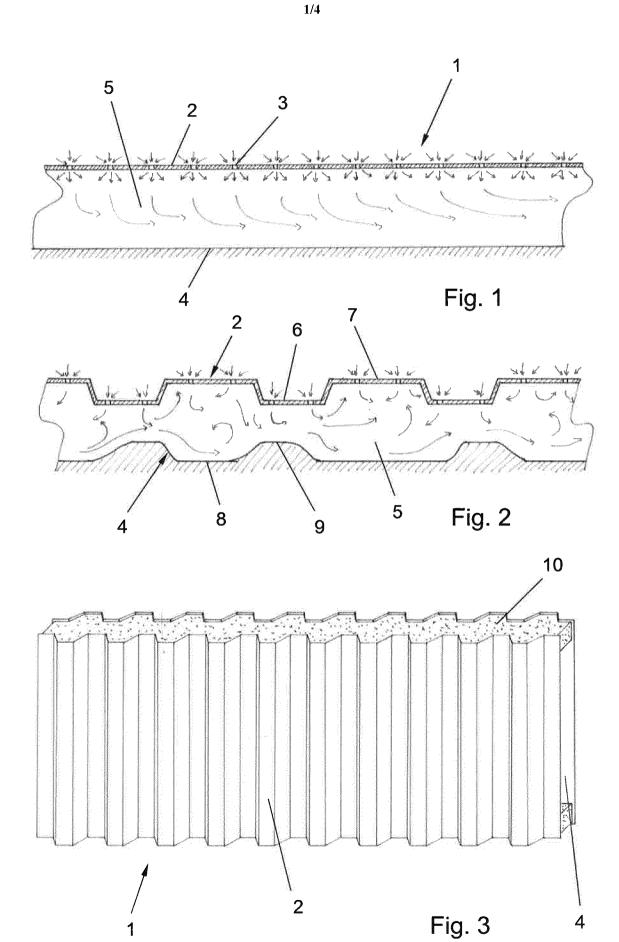
5

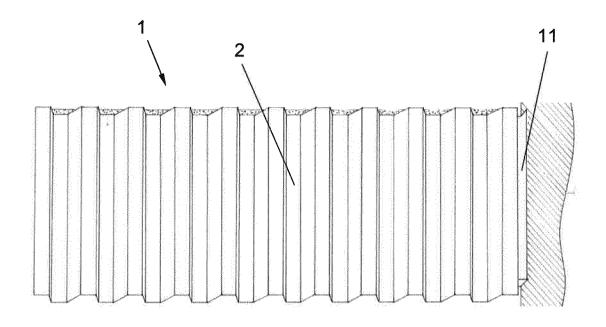
20

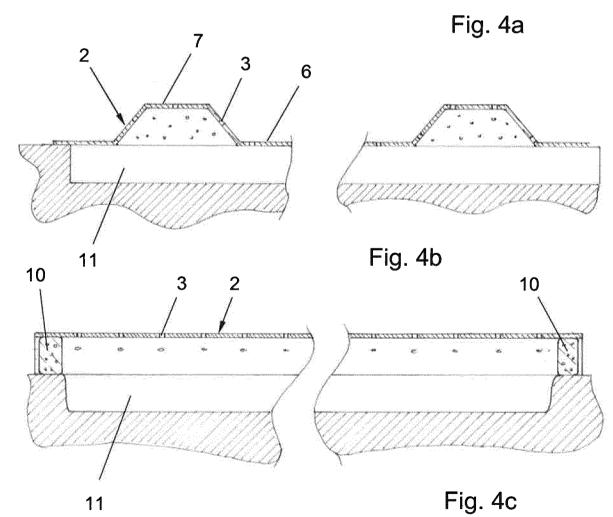
30

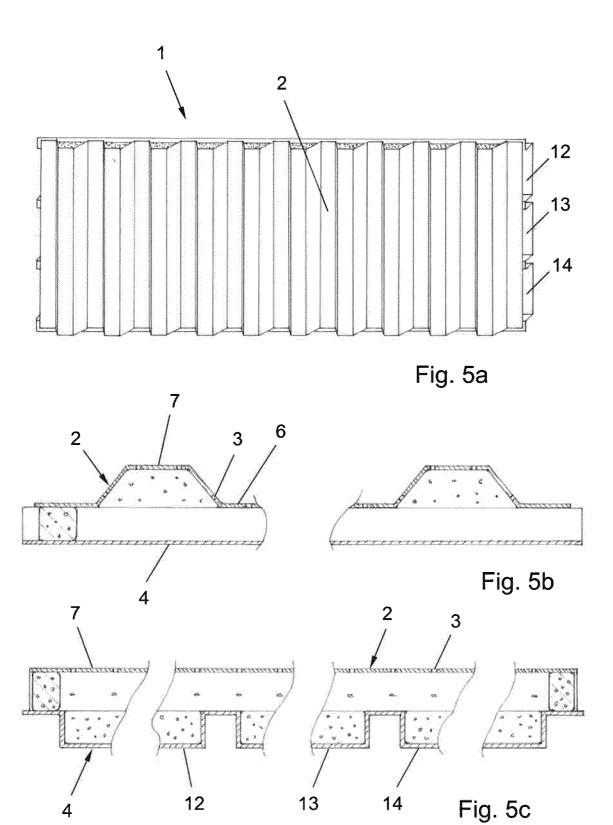
- 11 -

- 9. Transpired solar collector according to any of the preceding claims, wherein the absorber plate and back plate are mounted against each other.
- 10 10. Transpired solar collector according to any of the preceding claims, wherein the absorber plate and/or back plate comprise one or more profiled metal panels.
- 11. Transpired solar collector according to any of the preceding claims, wherein the back plate is formed by one or more insulated composite profiled panels.
 - 12. Transpired solar collector system comprising a transpired solar collector according to any of the preceding claims, a duct connected to the air outlet of the transpired solar collector and means connected to the duct to provide a negative pressure in the duct and the collector space, wherein the air outlet is provided along at least part of the length of a side of the transpired solar collector.
- 13. Transpired solar collector system according to claim 12, wherein the air outlet is provided at a side of the transpired solar collector at the end of the troughs with the largest cross-sectional area.
 - 14. Transpired solar collector system according to claim 12 or 13, wherein a connecting channel is provided to connect at least two transpired solar collectors to the duct.









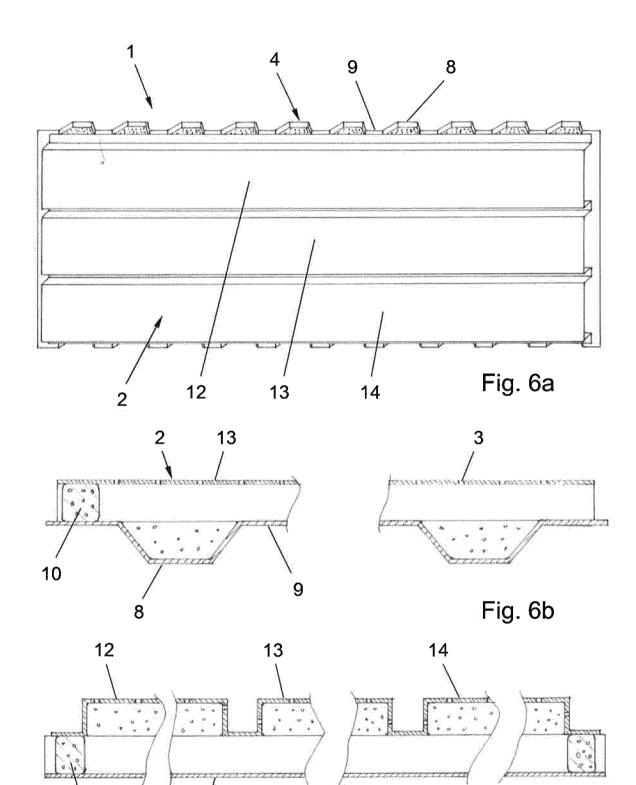


Fig. 6c

10

INTERNATIONAL SEARCH REPORT

International application No PCT/EP2016/076109

A. CLASSIFICATION OF SUBJECT MATTER INV. F24J2/28 F24J2/04 F24J2/20 ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols) $F24J\,$

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal, WPI Data

C. DOCUM	ENTS CONSIDERED TO BE RELEVANT	
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Υ	CN 201 637 145 U (BEIJING INST CIVIL ENG & ARCH) 17 November 2010 (2010-11-17) abstract; figures	1-14
Υ	US 4 201 195 A (SAKHUJA RAVINDER K [US]) 6 May 1980 (1980-05-06) column 3, line 53 - line 60; figures 1,2 column 4, line 27 - line 36; figure 3	1-14
Υ	US 4 534 337 A (JANSON GOESTA [SE]) 13 August 1985 (1985-08-13) column 1, line 61 - column 2, line 7; figures 1-3	2-5,9
Υ	US 2009/084521 A1 (VOLSTAD OVE CHARLES [NO]) 2 April 2009 (2009-04-02) paragraph [0031] - paragraph [0033]; figure 3	11
	-/	

Further documents are listed in the continuation of Box C.	X See patent family annex.
* Special categories of cited documents: "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier application or patent but published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art "&" document member of the same patent family
Date of the actual completion of the international search	Date of mailing of the international search report
21 December 2016	05/01/2017
Name and mailing address of the ISA/ European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Fax: (+31-70) 340-3016	Authorized officer Mootz, Frank

1

INTERNATIONAL SEARCH REPORT

International application No
PCT/EP2016/076109

C(Continua	ation). DOCUMENTS CONSIDERED TO BE RELEVANT	
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Υ	DE 10 2009 011318 A1 (JENNER FRANK [DE]) 9 September 2010 (2010-09-09) paragraphs [0011], [0017]; figure 1	12,13
Υ	US 4 267 822 A (DIAMOND EDWARD H) 19 May 1981 (1981-05-19) figures 15,19,20	14
A	FR 2 535 444 A1 (DALMAS ETS [FR]) 4 May 1984 (1984-05-04) page 2, line 9 - line 29; figures 2,3	1-14

1

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No
PCT/EP2016/076109

Patent document cited in search report		Publication date	Patent family member(s)			Publication date
CN 201637145	U	17-11-2010	NONE			•
US 4201195	A	06-05-1980	DE ES FR GB JP US	2943159 8100723 2439957 2034458 S5585846 4201195	A1 A1 A A	08-05-1980 01-02-1981 23-05-1980 04-06-1980 28-06-1980 06-05-1980
US 4534337	A	13-08-1985	AU AU DE EP SE US WO	557010 1474983 3372305 0105318 452188 4534337 8303660	A D1 A1 B A	27-11-1986 04-11-1983 06-08-1987 18-04-1984 16-11-1987 13-08-1985 27-10-1983
US 2009084521	A1	02-04-2009	AU CA EP NO US WO ZA	1668200 321435 2009084521 2005014951	A1 A1 B1 A1 A1	17-02-2005 17-02-2005 14-06-2006 08-05-2006 02-04-2009 17-02-2005 27-06-2007
DE 102009011318	A1	09-09-2010	NONE			
US 4267822	Α	19-05-1981	NONE			
FR 2535444	A1	04-05-1984	NONE			