

(19) World Intellectual Property
Organization
International Bureau



(43) International Publication Date
19 February 2004 (19.02.2004)

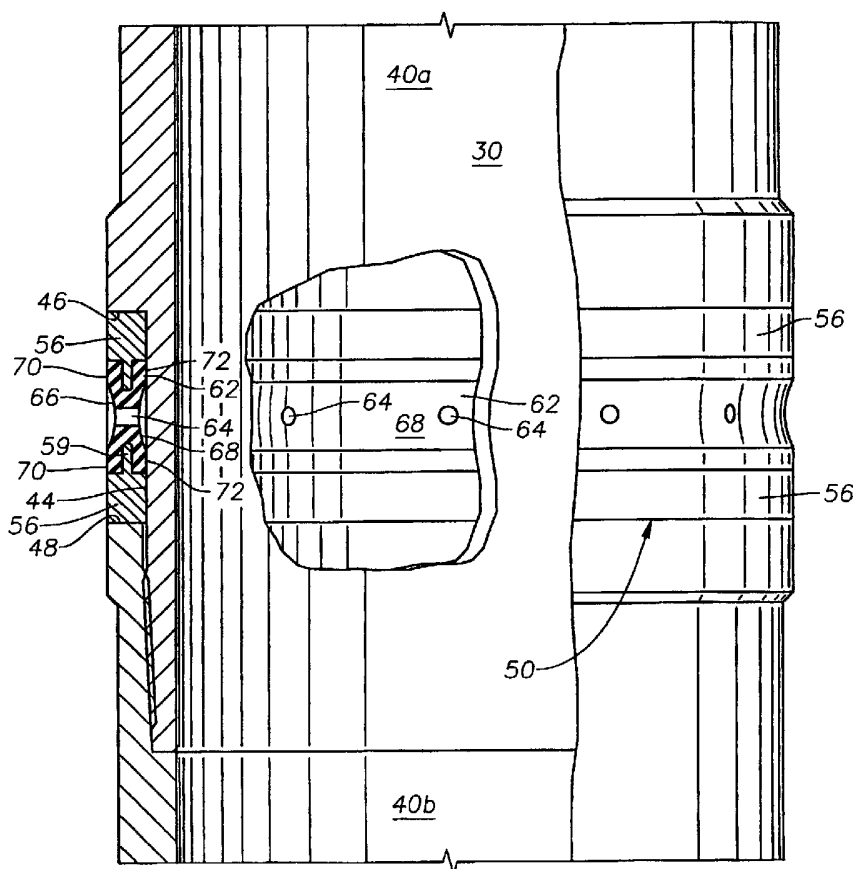
PCT

(10) International Publication Number
WO 2004/015240 A1

- (51) International Patent Classification⁷: **E21B 33/12**, F16L 15/04, F16J 15/32
- (21) International Application Number: PCT/US2003/021431
- (22) International Filing Date: 3 July 2003 (03.07.2003)
- (25) Filing Language: English
- (26) Publication Language: English
- (30) Priority Data: 10/213,863 7 August 2002 (07.08.2002) US
- (71) Applicant: **BAKER HUGHES INCORPORATED**
[US/US]; 3900 Essex Lane, Houston, TX 77027 (US).
- (72) Inventors: **NELSON, John, A.**; 15815 Township Glen Lane, Cypress, TX 77429 (US). **SALERNI, John, V.**; 3503 Deerbrook Drive, Kingwoos, TX 77339 (US).
- (74) Agent: **CARSON, Matt., W.**; Baker Oil Tools, A Division of Baker Hughes Incorporated, 9100 Emmott Road, Houston, TX 77040 (US).
- (81) Designated States (*national*): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RU, SC, SD, SE, SG, SK, SL, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, UZ, VC, VN, YU, ZA, ZM, ZW.
- (84) Designated States (*regional*): ARIPO patent (GH, GM, KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IT, LU, MC, NL, PT, RO, SE, SI, SK, TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

[Continued on next page]

(54) Title: SEAL RING FOR WELL COMPLETION TOOLS



(57) Abstract: A high pressure ring (50) seal for tube assembly joints provides structural foundation ring (52) having inside and outside circumferential channels (54) between end rims (56). The channels and rims are separated by a web (59) of interal ring material. This web is perforated by a plurality of apertures (60). As an integral coating within both channels and integrally tied through the web apertures is a coating of polymer sealant material. Inside and outside faces of the sealant are pressure equalized by vent apertures (64) through the web apertures.

WO 2004/015240 A1



Published:

— *with international search report*

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

SEAL RING FOR WELL COMPLETION TOOLS

BACKGROUND OF THE INVENTION

FIELD OF THE INVENTION

[0001] The present invention relates to earth boring arts and devices for subterranean well completion. In particular, the invention relates to fluid sealing elements for axially translated tubular members that are dynamically operative in chemically hostile, high pressure environments such as cross-over flow assemblies.

DESCRIPTION OF RELATED ART

[0002] Deep subterranean wells are drilled to recover economically valuable fluids such as natural gas and crude petroleum. In many cases, these wells penetrate geologic zones that confine extreme pressure. When encountered, high pressure must be controlled and maintained. For those reasons, high pressure zones are often isolated by packers and casing liners.

[0003] Completion of a well for extended fluid production includes many complex procedures. Among these procedures are formation fracturing, gravel packing and cementing. To execute some of these procedures, it is necessary to redirect the normal course of well working fluid. Well working fluids are generally characterized as "mud" but the term expansively includes water, solvents and particulate mixtures for gravel and sand packing. The normal working fluid circulation route in a well starts from the fluid pumps at the surface. The fluid pump discharge is piped into the well tubing string (or drill pipe) and down the central flow bore of the tubing string. The working fluid exits the flow bore at the bottom of the tubing string or at a desired intermediate point through selectively opened apertures in the tubing wall.

[0004] In many cases, an annular space exists between the tubing string and the well bore or casing wall. This annular space, characterized as the annulus, provides a channel for the working fluid return flow stream to the well surface and back to fluid reservoir pits or the pump suction.

[0005] There are many circumstances in the life of a well that require fluid and pressure isolation of an axial section of the annulus from an adjacent section. For example, it may be desired to isolate the bottomhole pressure from the upper annulus and at the same time, shield a bottomhole production zone from contamination fluid entering

the well bore from a higher strata. This desire is satisfied by means of a "packer" that provides an annular barrier between the tubing string and the well wall. Difficulty arises, however, when other well operations below the packer require fluid circulation. The packer blocks the working fluid return flow channel. This difficulty is overcome by means of a "cross-over assembly" which provides an additional flow annulus between the tubing string inner flow bore and an inner bore of the packer. Depending on the cross-over assembly setting, fluid may be pumped down the tubing flow bore into the annulus below the packer. From the annulus below the packer, the well working fluid (mud) may be channeled into the cross-over inner annulus to by-pass the packer and back into the well annulus above the packer.

[0006] In another typical example, working fluid may be pumped down the tubing flow bore to a cross-over point below the packer but above the tubing string bottom end. At the cross-over point, the working fluid is channeled out into the lower well annulus below the packer. The working fluid flows down the lower annulus to the bottom end of the tubing string to enter the tubing string flow bore. Working fluid flow from the bottom end of the tubing string is up the flow bore to the cross-over point where the flow enters the cross-over inner annulus. Further upward fluid flow proceeds along the inner annulus to a point above the packer where the flow is channeled out into the upper well annulus to complete the return flow circuit.

[0007] Typically, a cross-over assembly comprises an outer tube to which the packer is secured. Below the packer, the outer tube may have apertures through the tube wall. These outer tube apertures are internally isolated by reduced I.D. ring sections having smoothly finished sealing surfaces along the I.D. wall face of a ring section. A cross-over tube secured to the end of a tubing work string, has an O.D. less than the sealing surface of the outer tube ring section I.D. O.D. ring seals along the length of the cross-over tube are dimensioned to cooperate with the sealing surface I.D. Depending on the relative axial alignment between the cross-over pipe and the outer packer tube, controlled circulation flow past the packer is achieved while maintaining a pressure differential across the packer and ring seals.

[0008] Due to the hydrostatic head and bottom hole temperature of certain wells, this pressure differential across the packer and ring seals is considerable and imposes great pressure loads against the seals between the cross-over pipe and the sealing surfaces in the outer packer tube. These hydrostatic pressure and geothermal stresses may be compounded by an extremely hostile chemical environment. For example, a well may be

treated with amine corrosion inhibitors to reduce the corrosive deterioration of the casing and production tube. Compounds such as zinc bromide may be used for well pressure containment and control. Additionally, inhibitor and containment compounds may be used in mixed combination. Both such well treatment compounds have aggressive consequences on the elastomers and polymers normally used to seal the tubular interface of completion and production equipment.

[0009] To resist these highly reactive well treatment compounds, special purpose sealant compounds such as fluoroelastomers based upon alternating copolymers of tetrafluoroethylene and propylene (AFLAS[®]) have been developed. However, these AFLAS[®] types of sealing compounds do not bond (Vulcanize) well with metallic substructures. When the high pressure load on a seal is abruptly released over the seal, such as when the cross-over tube is axially shifted, a resulting rush of fluid across a seal tends to dislodge and damage the seal.

[0010] It is an objective of the present invention, therefore, to provide reliable bore sealing elements for substantially coaxial tube members.

[0011] Another object of the invention is a highly improved cross-over assembly seal.

SUMMARY OF THE INVENTION

[0012] The present crossover tube seal comprises a metallic ring member having inside and outside diameter channels between opposite end shoulders. A plurality of radial apertures distributed about the ring circumference penetrate the ring wall between the inside and outside channels.

[0013] The desired, chemically resistant elastomer such as AFLAS[®] is coated into both channels with a seal band proximate of the opposite end shoulders. Between the seal bands, elastomer surfaces, both inside and outside, are formed to a shallow concavity.

[0014] Additional to traditional surface bonding such as Vulcanizing, the inner and outer coatings of elastomer are unitized through the ring apertures by an integral plug of elastomer. Preferably, each aperture plug is perforated by a smaller aperture for equalizing the pressure differential between the inside and outside cylindrical surfaces of the ring.

[0015] The present sealing ring is positioned in the cross-over tube assembly in the traditional assembly position between adjacent cross-over tube mandrels. Threaded joint assembly of the adjacent joints axially confines the ring between opposing joint shoulders. Inside diameter sealing bands bear a static seal against a cylindrical seal

surface on the mandrel pin joint. Outside sealing bands cooperate with the spaced bore surfaces on the cross-over outer tube to provide pressure isolated cells along the cross-over assembly length.

BRIEF DESCRIPTION OF DRAWINGS

[0016] For a thorough understanding of the present invention, reference is made to the following detailed description of the preferred embodiments, taken in conjunction with the accompanying drawings in which like reference characters designate like or similar elements throughout the several figures of the drawing.

Figure 1 is a partially sectioned wellbore and cross-over assembly;

Figure 2 is a partially sectioned pipe joint sealed by the present invention;

Figure 3 is an isometric view of the present invention foundation ring; and

Figure 4 is an isometric view of the present invention showing a partial section removal.

DESCRIPTION OF PREFERRED EMBODIMENTS

[0017] For environmental orientation, a representative application of the present invention is illustrated by the **Figure 1** sectional schematic of a well casing **10**. Within the well casing is a cross-over assembly **20** having an outer tube **22** and an inner, cross-over tube **24**. The cross-over tube **24** is secured by a threaded pipe joint to the lower end of a tubing string **26**. The outer tube **22** is secured to the inside wall of the casing **10** by means of one of more packers **28**. The outer tube **22** and cross-over tube **24** are joined by an assembly thread **34** for downhole placement as a unit. After the packer **28** is located at the desired position, the packer and associated slip (not shown) is set against the inside wall surface of the casing **10**. This packer and slip setting secures the outer tube **22** to the casing **10**. Subsequently, the work string **26** is rotated to disassemble the cross-over tube **24** from the anchored and sealed outer tube.

[0018] The cross-over tube **24** also includes a central flow bore **30** and an inner annular flow channel **32**. The inner flow channel **32** is open by aperture **36** through the cross-over tube wall.

[0019] The length of the cross-over tube **24** comprises a serial assembly of numerous flow mandrels **40a**, **40b**, etc. joined by threaded seal joints **42**. With respect to **Figure 2**, the "pin" (male) portion of a joint **40a** comprises a sealing sleeve **44** between the thread **42** and a compression shoulder **46**. The "box" (female) portion of a joint **40b** comprises a compression shoulder **48** about the distal end of the joint portion. The joint elements and

features are dimensioned to confine a seal ring **50** between the shoulders **46** and **48** when the thread joint is closed. The inside seals of the ring **50** provide a fluid pressure sealing interface with the sealing sleeve surface **44** and thereby, a fluid pressure seal of the threaded assembly **42** between pressure differentials respective to the mandrel flow bore **30** and the external mandrel environment.

[0020] Outside seals on the ring **50** interface with bore seal surfaces **38** on the outer cross-over assembly tube **22**. Longitudinal dimensioning between the bore seal surfaces and the separation between ring seals **50** is coordinated to accomplish respective cross-over tool functions by each of several axial alignments between the outer tube **22** and the cross-over tube **24**.

[0021] With respect to **Figures 3 and 4**, construction of a ring seal **50** includes a structural foundation ring **52** fabricated from a suitable material. The foundation ring material should be selected with due consideration of the intended operational environment. In most well operations, a mild steel alloy is suitable. Wells treated with highly reactive components such as amines and bromides may require a stainless steel alloy or Inconel. Other applications may allow non-ferrous metals or dense polymers as the material source of the foundation ring.

[0022] Assuming an original material shape in the form of a cylinder, an outside channel **54** is formed into the outer ring perimeter between opposite end rims **56**. Similarly, an inside channel **58** is formed between the opposite end rims **56**. A cylindrical web **59** of foundation material remains between the inside and outside channels. Linking the inside and outside channels are a plurality of apertures **60** through the web **59** distributed substantially uniformly about the ring perimeter.

[0023] Cast, for example, on and into the channels **54** and **58** and the apertures **60**, as an integral coating, is a suitable sealing polymer such as the fluoroelastomer AFLAS®. Whether cast or machined, a smaller aperture **64** perforates the polymer web within each of the foundation web apertures **60**. The polymer seal coating is further formed with outside and inside cavities, **66** and **68**, respectively. The outside cavity **66** is formed between a pair of outside seal bands **70** whereas the inside cavity is formed between a pair of inside seal bands **72**.

[0024] The cavities **66** and **68** are functional voids in the invention design to distribute the pressure differential load on the seal substantially uniformly across the transverse plane of the seal (pressure force vectors parallel with the wellbore axis).

Although an accurate void shape **66** and **68** is illustrated as the preferred embodiment, it will be understood that other void shapes such as a box or channel may be used to accommodate seal material movement due to pressure distortion and temperature expansion. Ideally, the pressure differential load imposed on that seal band directly engaged with the highest pressure environment is distributed across the full annulus of the low pressure side of the seal whereby the unsupported ridge of low pressure sealing band carries only a fractional portion of the full pressure differential load.

[0025] Dimensionally, the O.D. of the outside seal bands **70** is greater than the O.D. of the end rims **56**. Similarly, the I.D. of the inside seal bands **72** is less than the I.D. of the end rims **56**. It is the outside seal bands **70** that make interface contact with the seal bore faces **38** on the outer assembly tube **22**. It is the inside seal bands **72** that make interface contact with the seal sleeve surface **44** of the mandrel joint pin.

[0026] Those of skill in the art will appreciate the fact that fluid pressures within the cross-over flow bore **30** may be developed in excess of a high formation pressure that is restrained by the packer **28**. These high pressures are generated by surface pumps for some well treatment purpose such as chemical fracturing or cementing. A portion of this high flow bore pressure will bleed past the inner seal band **72** into the inside cavity **68**. At the same time, a portion of the bottomhole pressure will bleed past the outer seal bands **70** into the outer cavity **66**. When a particular seal **50** is drawn above the uppermost bore seal surface **38**, the fluid confined under high pressure in the outside cavity **66** is released abruptly. Although the fluid volume within the outside cavity **66** is small, the escape velocity of such volume over the seal band face is such as may damage or destroy prior art seals. To further resist such decompression destruction, the elastomer sealant of the present invention is vulcanized to the foundation ring to reinforce the mechanical interlock that is inherent with the invention.

[0027] The apertures **64** between the inside and outside cavities serve to equalize pressure differentials that would otherwise develop between the opposing surfaces. The aperture vents **64** of the present invention release the inside cavity pressure at the same time as the outside cavity pressure is released.

[0028] An alternative embodiment of the invention may take the form of independent rings respective to each of the sealing bands **70/72** whereby an unsealed mating interface is provided between the outside cavity **66** and inside cavity **68**. This unsealed interface between separate seal band rings provides the same function as the apertures **64** for venting the inside cavity **68** in the event of sudden pressure changes.

[0029] Although the invention has been described in the application environment of a cross-over assembly, those of skill in the art will appreciate the design relevance of this ring seal to many other high pressure, chemically hostile applications such as long term formation fluid production. The design may also be used in many piston/cylinder and rod/tube applications unrelated to subterranean wells.

[0030] It should be understood that this description of our preferred embodiment is by illustration only and that the invention is not necessarily limited thereto. Alternative embodiments and operating techniques will become apparent to those of ordinary skill in the art in view of the present disclosure. Accordingly, modifications of the invention are contemplated which may be made without departing from the spirit of the claimed invention.

CLAIMS

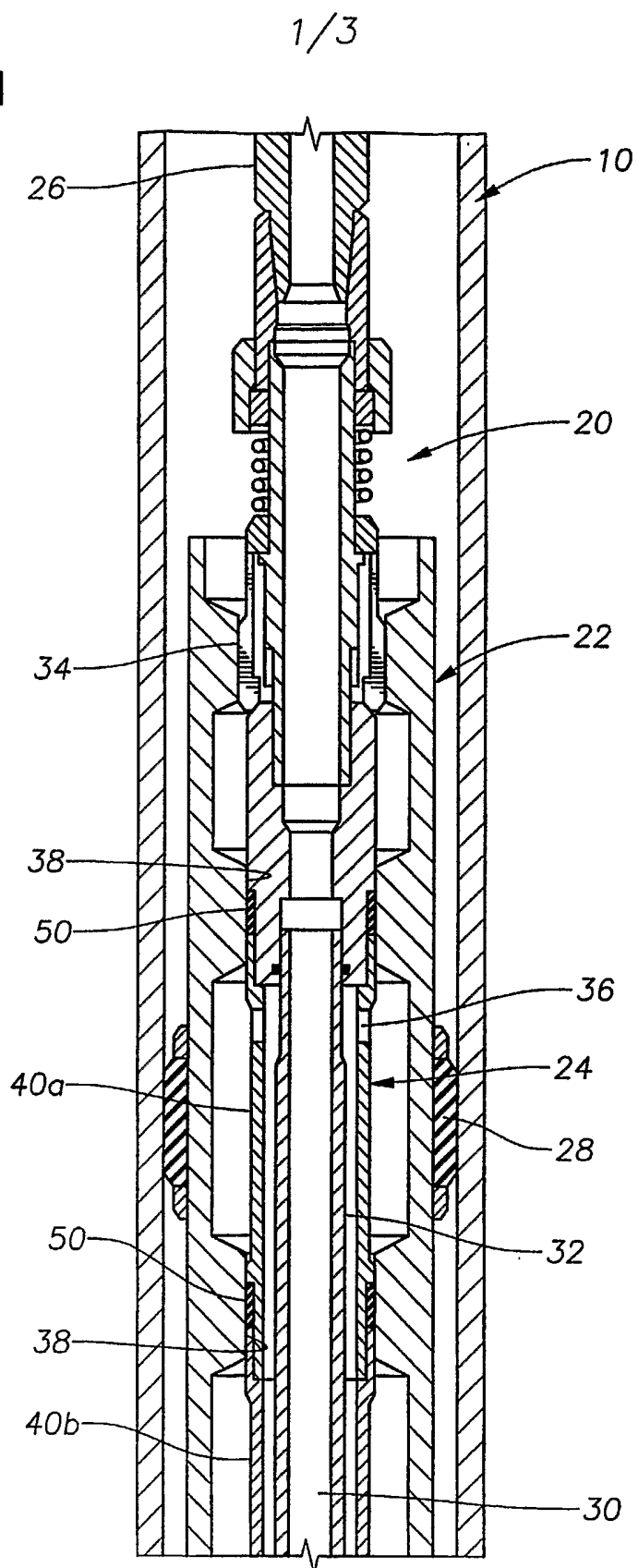
1. A pressure seal ring having an elastomer sealant material coated onto a foundation ring, said sealant material formed to profile a materially integral pair of inside and outside diameter seal bands.
2. A pressure seal ring as described by claim 1 having a pair of outside diameter seal bands separated by an outside chamber space and a pair of inside diameter seal bands separated by an inside chamber space.
3. A pressure seal ring as described by claim 2 wherein said inside and outside chamber spaces are mutually vented.
4. A pressure seal ring as described by claim 1 wherein said sealant material is formed into respective inside and outside diameter channels in said foundation ring.
5. A pressure seal ring as described by claim 1 wherein said sealant material is a fluoroelastomer.
6. A well tubing seal for isolating a formation fluid flow stream in a tubing flow bore from a non-formation wellbore fluid environment, said seal comprising:
 - (a) a cylindrical foundation ring having inside and outside perimeter channels;
 - (b) a sealant material coating into said inside and outside channels
 - (c) a pair of outside perimeter seal bands integrally profiled from said sealant material; and,
 - (d) a pair of inside perimeter seal bands integrally profiled from said sealant material, said sealant material of said inside and outside seal being integrally continuous.
7. A well tubing seal as described by claim 6 wherein said sealant material is fluoroelastomer.

8. A well tubing seal as described by claim 7 wherein said sealant material coating into said inside and outside channels is bonded to said foundation ring.
9. A well tubing seal as described by claim 6 wherein said inside and outside perimeter channels are mutually vented.
10. A tubing seal ring comprising:
 - (a) a substantially cylindrical foundation ring having inside and outside perimeter channels between end ridges, said ridges being integrally linked by a substantially cylindrical web between said channels;
 - (b) a plurality of first apertures through said web and distributed thereabout;
 - (c) a sealant material coating of said channels having integral continuity through said web apertures between inside and outside channels; and,
 - (d) a plurality of second apertures through said first apertures.
11. A seal ring as described by claim 10 wherein said sealant material is profiled adjacent said end ridges with perimeter bands whereby an O.D. of said bands is greater than an O.D. of said end ridges and an I.D. of said bands is less than an I.D. of said end ridges.
12. A seal ring as described by claim 11 wherein sealant material coating of said channels between said bands is formed to an arc profile.
13. A seal ring as described by claim 11 wherein sealant material coating of said channels between said bands is formed to a shallow concavity.
14. A seal ring as described by claim 10 wherein said sealant material is fluoroelastomer.
15. A seal ring as described by claim 14 wherein said fluoroelastomer is based upon an alternating copolymer of tetrafluoroethylene and propylene.

16. A seal ring as described by claim 15 wherein said fluoroelastomer is bonded to said foundation ring.
17. A cross-over tool for subterranean well management, said cross-over tool having a plurality of tubing joints that are pressure sealed by sealing rings, one tube of a joint having a substantially cylindrical seal surface for engaging a ring sealing band, said sealing rings comprising a substantially cylindrical unit having a circumferential web linking respective end ribs to delineate respective I.D. and O.D. channels, said web having a plurality of apertures distributed thereabout, a polymeric coating of said I.D. and O.D. channels, said coating respective to said I.D. and O.D. channels being integrally linked through said apertures.
18. A cross-over tool as described by claim 17 wherein said polymeric coating is bonded to said web.
19. A cross-over tool as described by claim 17 wherein said polymeric coating is perforated through said apertures.
20. A cross-over tool as described by claim 17 having I.D. sealing bands formed in said coating adjacent respective end ribs, said I.D. sealing bands having an I.D. less than an I.D. of said end ribs for engaging said cylindrical seal surface.
21. A cross-over tool as described by claim 20 having a shallow concavity between respective sealing bands.
22. A cross-over tool as described by claim 20 having an arced profile between respective sealing bands.
23. A cross-over tool as described by claim 20 having O.D. sealing bands formed in said coating adjacent respective end ribs, said O.D. sealing bands having an O.D. greater than an O.D. of said end ribs for engaging a cooperative sealing surface.

24. A cross-over tool as described by claim 23 having a shallow concavity between respective sealing bands.
25. A cross-over tool as described by claim 23 having an arced profile between said O.D. sealing bands.
26. A cross-over tool as described by claim 17 wherein said polymeric coating is a fluoroelastomer.
27. A cross-over tool as described by claim 26 wherein said fluoroelastomer is an alternating copolymer of tetrafluoroethylene and propylene.

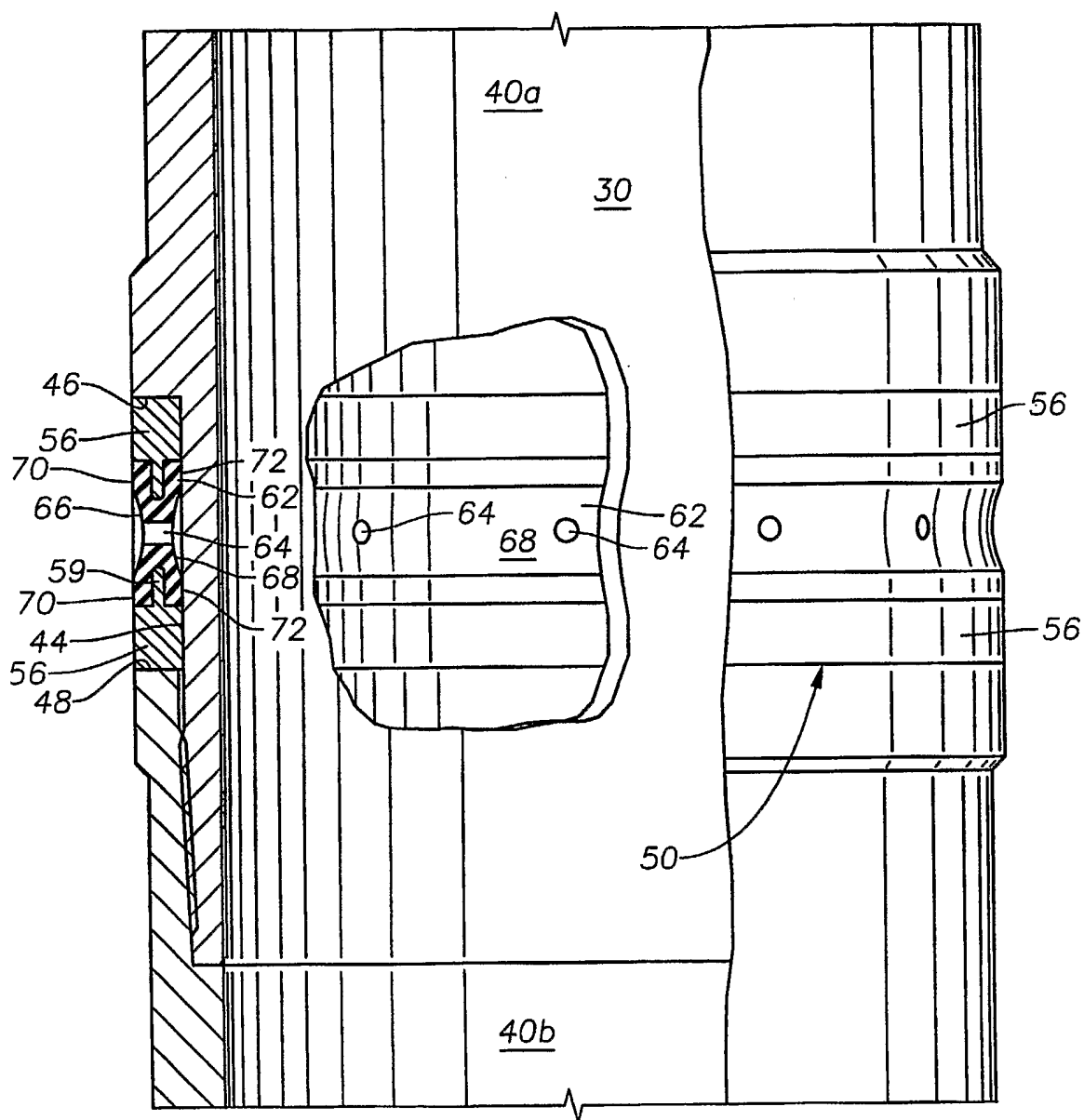
Fig. 1



SUBSTITUTE SHEET (RULE 26)

2/3

Fig. 2



3/3

Fig. 3

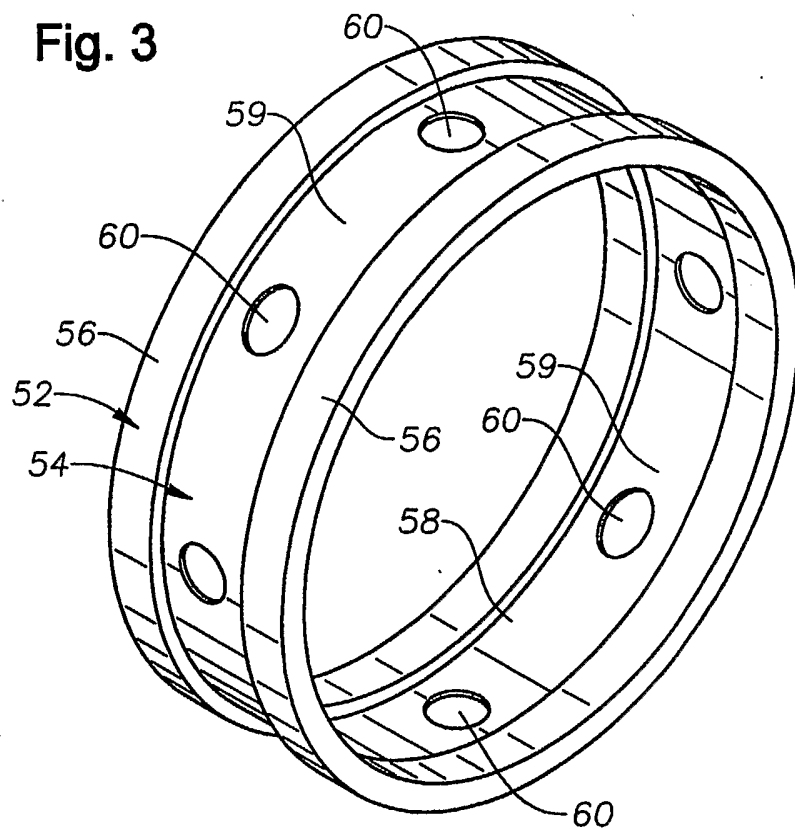
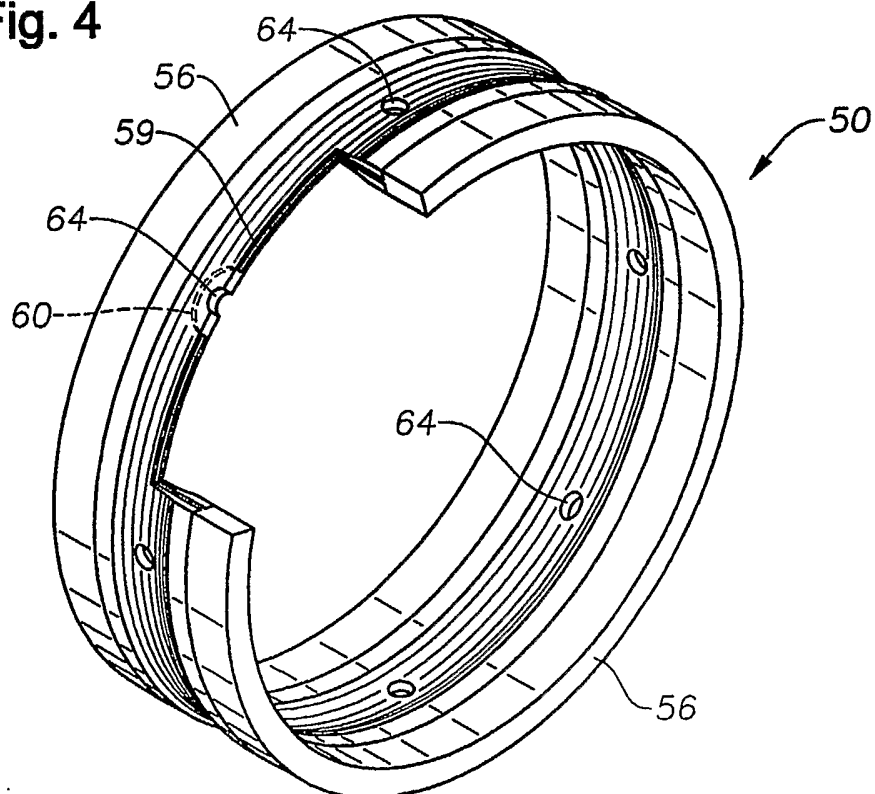


Fig. 4



INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 03/21431

A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 E21B33/12 F16L15/04 F16J15/32

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 F16L E21B F16J

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 4 827 834 A (LEIGH-MONSTEVENS KEITH V) 9 May 1989 (1989-05-09) column 1, line 59 - line 68; figure 1	1,2
Y	---	3,5
Y	US 5 584 488 A (LEMBCKE JEFFREY J) 17 December 1996 (1996-12-17) column 1, line 23 - column 2, line 3; figures 1,2 column 2, line 25 - line 31	5
Y	US 4 337 956 A (HOPPER JAMES A) 6 July 1982 (1982-07-06) column 1, line 38 - line 48; figures 1,2 --- -/--	3



Further documents are listed in the continuation of box C.



Patent family members are listed in annex.

* Special categories of cited documents:

- *A* document defining the general state of the art which is not considered to be of particular relevance
- *E* earlier document but published on or after the international filing date
- *L* document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- *O* document referring to an oral disclosure, use, exhibition or other means
- *P* document published prior to the international filing date but later than the priority date claimed

- *T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- *X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- *Y* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.
- *Z* document member of the same patent family

Date of the actual completion of the international search

13 November 2003

Date of mailing of the international search report

25/11/2003

Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2
NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
Fax: (+31-70) 340-3016

Authorized officer

Dantinne, P

INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 03/21431

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP 0 964 191 A (AUTOMOTIVE PROD USA) 15 December 1999 (1999-12-15) paragraph '0014! - paragraph '0016!; figures 4,5 ---	1
X	FR 2 672 097 A (PEUGEOT ;CITROEN SA (FR)) 31 July 1992 (1992-07-31) See abstract figures 1,2 ---	1
A	US 4 131 287 A (GUNDERSON RICHARD H ET AL) 26 December 1978 (1978-12-26) column 2, line 39 - line 58; figure 3 ---	1,6,10, 17
A	US 2001/045700 A1 (RUSSELL LARRY R) 29 November 2001 (2001-11-29) paragraph '0075!; figures 8,13 -----	1,6,10, 17

INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 03/21431

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
US 4827834	A	09-05-1989	AU 1930188 A WO 8809889 A1 GB 2230321 A ,B US 4821627 A	04-01-1989 15-12-1988 17-10-1990 18-04-1989
US 5584488	A	17-12-1996	NONE	
US 4337956	A	06-07-1982	CA 1156282 A1 CA 1159489 A2	01-11-1983 27-12-1983
EP 0964191	A	15-12-1999	US 6196552 B1 EP 0964191 A2 GB 2340897 A ,B JP 2000009231 A	06-03-2001 15-12-1999 01-03-2000 11-01-2000
FR 2672097	A	31-07-1992	FR 2672097 A1	31-07-1992
US 4131287	A	26-12-1978	NONE	
US 2001045700	A1	29-11-2001	AU 3854401 A CA 2404629 A1 GB 2363632 A WO 0163166 A1 US 2001045747 A1 US 2001045746 A1 AU 3854301 A CA 2404469 A1 GB 2363630 A WO 0163153 A1	03-09-2001 30-08-2001 02-01-2002 30-08-2001 29-11-2001 29-11-2001 03-09-2001 30-08-2001 02-01-2002 30-08-2001