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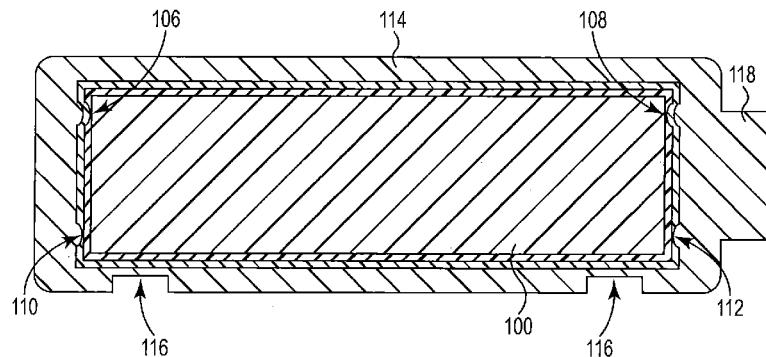


Fig. 2

(57) Abstract: A magnetic article with a corrosion resistant barrier formed from a poly (tetrafluoro-p- xylene) conformal coating or from a parylene conformal coating having a melting point of at least about 430°C and a moisture vapor transmission less than about 0.5 g-mm/m²/day at 90% RH and 37°C, the conformal coating being covered with a polysulfone thermoplastic overlayer.

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CORROSION-RESISTANT MAGNETIC ARTICLE

CROSS-REFERENCE TO RELATED APPLICATION

[0001] This application claims the benefit of U.S. Application Serial No. 14/603,027 filed January 22, 2015 and entitled "CORROSION-RESISTANT MAGNETIC ARTICLE", the disclosure of which is incorporated herein by reference.

FIELD OF THE INVENTION

[0002] This invention relates to coated magnetic articles.

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BACKGROUND

[0003] U.S. Patent Application Publication No. US 2013/0345646 A1 (Bertrand et al.) describes an implantable physiological shunt system which utilizes a magnetic coupling between an external adjustment tool and an internal magnetic rotor assembly in order to control the flow of fluids. The shunt system can include a locking feature to prevent unintended setting changes when the shunt is exposed to strong external magnetic fields. This feature can be particularly important when shunts used to control the flow of cerebrospinal fluid (CSF) from the brain ventricles of hydrocephalus patients are exposed to external magnetic fields during magnetic resonance imaging (MRI). However, if the shunt lock is set, the internal magnet may also be prevented from aligning with the external magnetic field, and in a sufficiently strong external magnetic field may become demagnetized or reverse magnetized. If this occurs, surgical replacement of the shunt may be required.

[0004] External magnetic fields of for example as high as 3 Tesla are generated in some MRI scanners. Fields of that strength can demagnetize or reverse magnetize samarium cobalt (SmCo) magnetic materials. NdFeB (Neodymium) rare earth permanent magnets have sufficiently high coercivity (H_{ci}) to resist demagnetization or reverse magnetization in such fields, but also have very poor corrosion resistance. Magnetic strength generally is lost in direct proportion to the mass loss caused by corrosion. NdFeB magnets typically are made more resistant to corrosion by applying protective coatings such as plating (e.g., nickel plating or layers of copper and nickel plating), powder

5 coatings or paints. However, when such protectively coated NdFeB magnets are submersed in aqueous saline solution, the protective coating may in some cases be breached within 24 hours after the start of exposure.

[0004A] Any discussion of documents, acts, materials, devices, articles or the like which has been included in the present specification is not to be taken as an admission that any or 10 all of these matters form part of the prior art base or were common general knowledge in the field relevant to the present disclosure as it existed before the priority date of each of the appended claims.

SUMMARY

15 [0005] The disclosed invention provides, in one aspect, a magnetic article comprising an NdFeB magnet having thereon a substantially continuous corrosion resistant barrier comprising a fluorinated parylene conformal coating covered with a polysulfone thermoplastic overlayer.

[0006] The disclosed invention provides, in another aspect, a magnetic article comprising an NdFeB magnet having thereon a substantially continuous corrosion resistant barrier comprising a parylene conformal coating having a melting point of at least about 430° C and a moisture vapor transmission less than about 0.5 g-mm/m²/day at 90% RH and 37° C, the parylene conformal coating being covered with a polysulfone thermoplastic overlayer.

[0007] The disclosed invention provides, in yet another aspect, a method for making a 20 coated magnetic article, which method comprises vapor depositing upon an NdFeB magnet a layer or layers of a fluorinated parylene conformal coating, and applying molten polysulfone over the conformal coating, to provide a substantially continuous corrosion resistant barrier over the magnet.

[0008] The disclosed invention provides, in a further aspect, a method for making a coated 25 magnetic article, which method comprises vapor depositing upon an NdFeB magnet a layer or layers of a parylene conformal coating having a melting point of at least about 430° C and a moisture vapor transmission less than about 0.5 g-mm/m²/day at 90% RH and 37° C, and applying molten polysulfone over the parylene conformal coating, to provide a substantially continuous corrosion resistant barrier over the magnet.

[0009] The disclosed invention provides, in another aspect, an implantable medical device 30 containing a coated magnetic article comprising an NdFeB magnet having thereon a substantially continuous corrosion resistant barrier comprising a fluorinated parylene conformal coating covered with a polysulfone thermoplastic overlayer.

5 [0010] The disclosed invention provides, in yet another aspect, an implantable medical device containing a coated magnetic article comprising an NdFeB magnet having thereon a substantially continuous corrosion resistant barrier comprising a parylene conformal coating having a melting point of at least about 430° C and a moisture vapor transmission less than about 0.5 g-mm/m²/day at 90% RH and 37° C, covered with a polysulfone
10 thermoplastic overlayer.

[0010A] Throughout this specification the word "comprise", or variations such as "comprises" or "comprising", will be understood to imply the inclusion of a stated element, integer or step, or group of elements, integers or steps, but not the exclusion of any other element, integer or step, or group of elements, integers or steps.

15

BRIEF DESCRIPTION OF THE DRAWING

[0011] **Fig. 1** is a side cross-sectional view of an NdFeB magnet coated with a poly(tetrafluoro-p-xylene) conformal coating;

20 [0012] **Fig. 2** is a side cross-sectional view of the **Fig. 1** magnet covered with a polysulfone thermoplastic overlayer;

[0013] **Fig. 3a** is a side cross-sectional view of a partially potted NdFeB magnet whose unpotted surfaces are coated with a poly(tetrafluoro-p-xylene) conformal coating;

[0014] **Fig. 3b** is a side cross-sectional view of the **Fig. 3a** magnet with a polysulfone thermoplastic overlayer;

25 [0015] **Fig. 4a** is a side cross-sectional view of a partially potted NdFeB magnet that has been partially coated with a poly(tetrafluoro-p-xylene) conformal coating;

[0016] **Fig. 4b** is a side cross-sectional view of the **Fig. 4a** magnet with a further poly(tetrafluoro-p-xylene) conformal coating and a polysulfone thermoplastic overlayer;

30 [0017] **Fig. 5** is a perspective view, partially in phantom, of an NdFeB ring magnet coated with a poly(tetrafluoro-p-xylene) conformal coating; and

[0018] **Fig. 6** is a perspective view, partially in phantom, of the **Fig. 5** magnet covered with a polysulfone thermoplastic overlayer.

[0019] Like reference symbols in the various figures of the drawing indicate like elements. The elements in the drawing are not drawn to scale.

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DETAILED DESCRIPTION

[0020] The following detailed description describes certain embodiments and is not to be taken in a limiting sense. The terms shown below have the following meanings:

5 [0021] The recitation of a numerical range using endpoints includes all numbers subsumed within that range (e.g., 1 to 5 includes 1, 1.5, 2, 2.75, 3, 3.80, 4, 5, etc.).

[0022] The terms “a,” “an,” “the,” “at least one,” and “one or more” are used interchangeably. Thus, for example, an article coated with “a” layer means that the article may be coated with “one or more” layers.

10 [0023] When words of orientation such as “atop”, “on”, “uppermost”, “underlying” and the like are used herein to refer to various elements in the disclosed coated articles, they identify the relative position of an element with respect to a horizontally-disposed, upwardly-facing substrate or support for such element. It is not intended that the disclosed coated articles should have any particular orientation in space during or after their manufacture.

15 [0024] The term “barrier” refers to a layer or layers of material that impede the transmission of gases (e.g., oxygen, air or water vapor), liquids (e.g., water) or ions (e.g., sodium or chlorine ions) into or out of a substrate or support.

[0025] The term “coating” means a thin (e.g., less than 0.5 mm average thickness) layer covering at least a portion of a support or substrate.

20 [0026] The term “condensing” means collecting vapor-phase material in a liquid or solid state on a support or substrate.

[0027] The term “corrosion resistant” when used with respect to a barrier on an NdFeB magnet means that the magnet does not exhibit visible corrosion after 2 days immersion in 37° C normal saline solution.

25 [0028] The term “conformal” when used with respect to a coating on a substrate or support means that the coating has the same shape as the underlying substrate or support topography including features such as crevices, points and edges.

[0029] The term “continuous” when used with respect to a barrier, coating, overlayer or overmolding on a substrate or support means that the barrier, coating, overlayer or overmolding covers the underlying substrate or support without measurable gaps, fissures, pin-holes or other discontinuities in coverage that would directly expose the substrate or support to external gases (e.g., ambient air) or external fluids (e.g. in the case of an implantable medical device, bodily fluids). The term “substantially continuous” means that the barrier, coating, overlayer or overmolding covers the underlying substrate or

5 support without gaps, fissures or other discontinuities in coverage that are visible to the naked eye.

[0030] The term “dimer” refers to an oligomer that is a combination of two monomers.

[0031] The term “hermetic” refers to a material that is substantially impermeable, for the typical projected working life of the disclosed magnetic articles, to the transmission of 10 corrosion-inducing quantities of gases (*e.g.*, oxygen, air or water vapor) and fluids (*e.g.*, water).

[0032] The term “magnet” refers to an article having a volume of at least 1 mm³ and magnetic or magnetizable properties.

[0033] The term “monomer” refers to a single unit molecule that is capable of

15 combining with itself or with other monomers or oligomers to form other oligomers or polymers.

[0034] The term “oligomer” refers to a compound that is a combination of 2 or more (and typically 2, 3 or 4 up to about 6) monomers, but that might not yet be large enough to qualify as a polymer.

20 [0035] The term “overlayer” refers to a thin (*e.g.*, less than 0.5 mm average thickness) or thick (*e.g.*, more than 0.5 mm average thickness) layer of a material atop a substrate or support. Such a layer may be formed using a thermoplastic material by for example melting and dip-coating, melting and spray-applying, or melting and injection molding the thermoplastic material over the support or substrate. The overlayer may be separated from

25 the substrate or support by a conformal coating such as the poly(tetrafluoro-p-xylene) conformal coating discussed above, and by one or more optional additional layers atop or underlying the conformal coating. The overlayer may have a constant or variable thickness. If present, a variable thickness may arise from one or more features in the support or substrate that penetrate below or project beyond the support or substrate

30 average thickness, or from one or more features in the overlayer that penetrate below or project beyond the covering average thickness. Exemplary such features may include grooves, notches, detents, apertures, splines, tabs, stops, steps, sealing surfaces, pivot points, axles, bearing surfaces, indicators to depict direction (*e.g.*, of fluid flow or magnetization), spring retaining collars, valves, valve actuators and other recesses or

35 protrusions.

5 [0036] The term “overmolding” refers to an overlayer made by injection molding.
[0037] The term “polymer” refers to an organic molecule that has multiple regularly or irregularly arranged carbon-containing monomer or oligomer repeating units.
[0038] The terms “preferred” and “preferably” refer to embodiments of the invention that may afford certain benefits, under certain circumstances. However, other 10 embodiments may also be preferred, under the same or other circumstances.

Furthermore, the recitation of one or more preferred embodiments does not imply that other embodiments are not useful, and is not intended to exclude other embodiments from the scope of the invention.

15 [0039] **Fig. 1** is a side cross-sectional view of a free-standing NdFeB magnet **100**. Magnet **100** serves as a substrate or support upon which may be formed the above-mentioned conformal coating, shown in **Fig. 1** as poly(tetrafluoro-p-xylene) layers **102** and **104**. For illustrative purposes, layers **102** and **104** have been depicted with exaggerated thickness. Layers **102** and **104** may have the same or different average 20 thicknesses, and may for example each be at least about 1, at least about 2, at least about 5, at least about 10 or at least about 20 micrometers thick, and may for example each be less than about 100, less than about 80, less than about 60, less than about 50 or less than about 40 micrometers thick. Small discontinuities **106**, **108** in portions of layer **102** and small discontinuities **110**, **112** in portions of layer **104** are artifacts arising from contact with a gripping fixture (not shown in **Fig. 1**) that supported magnet **100** during the formation of 25 layers **102** and **104**. Different fixtures, different grip positions or both desirably are employed prior to the formation of each such layer to ensure that discontinuities **106**, **108**, **110** and **112** are each confined to only small portions of layers **102** or **104** without overlap, so as to enable the overall formation of a continuous conformal coating.

30 [0040] **Fig. 2** is a side cross-sectional view of magnet **100** from **Fig. 1** in which layer **104** has been covered with polysulfone thermoplastic overlayer **114**. Overlayer **114** desirably has an average thickness at least several times greater (e.g., at least 2X, at least 3X, at least 5X or at least 10X greater) than the combined thickness of the layers **102** and **104**. As depicted in **Fig. 2**, overlayer **114** includes features **116** and **118** respectively representing recesses below and protrusions beyond the average thickness of overlayer 35 **110**.

5 [0041] **Fig. 3a** and **Fig. 3b** are side cross-sectional views of another embodiment of the disclosed magnetic article. As shown in **Fig. 3a**, NdFeB magnet **300** has been partially potted in potting material **302**. Potting material **302** may be formed from a variety of non-magnetic materials, *e.g.* zinc, aluminum or various hardenable organic potting compounds. Potting material **302** desirably is sufficiently thick and made from a material suitable to
10 provide a hermetic structure with respect to the portions of magnet **300** contacted by potting material **302**. In addition, potting of magnet **300** in potting material **302** desirably does not unduly detract from the magnetic or magnetizable properties of magnet **300**. Unpotted magnet surfaces **304**, **306** and **308** and the upper face **310** of potting material **302** have been coated with a layer **312** of a poly(tetrafluoro-p-xylene) conformal coating.
15 During the application of conformal coating **312**, magnet **300** may be fixtured by for example gripping potting material **302** and accordingly the application of a single layer of coating **312** can provide a continuous coating over the exposed portions of magnet **300**. If desired, some or the entire exposed upper surface of potting compound **302** may be masked prior to application of coating material **312**, with the mask being removed prior to
20 subsequent processing. In another embodiment, excess coating material **312** may be removed from some or the entire exposed upper surface of potting compound **302** after application of coating material **312** (*e.g.*, using solvents, abrasives or other techniques that will be familiar to persons having ordinary skill in the art). As depicted in **Fig. 3a**, no mask has been applied and no coating material **312** has been removed, and consequently
25 portions of layer **312** extend away from magnet **300** and lie atop potting compound **302**.

[0042] As shown in **Fig. 3b**, layer **312** has been covered with polysulfone thermoplastic overlayer **314**. As depicted in **Fig. 3b**, overlayer **314** includes features **316** and **318** respectively representing a recess below and protrusions beyond the average thickness of overlayer **314**.

30 [0043] **Fig. 4a** and **Fig. 4b** are side cross-sectional views of another embodiment of the disclosed magnetic article. As shown in **Fig. 4a**, NdFeB magnet **400** has been partially coated with a layer **401** of a poly(tetrafluoro-p-xylene) conformal coating. The uncoated portion of magnet **400** is an artifact arising from contact with a gripping fixture (not shown in **Fig. 4a**) that supported magnet **400** during the formation of layer **401**. Potting material
35 **402** contacts the submerged portion of layer **401**. Potting material **402** may be formed

5 from a variety of non-magnetic materials, *e.g.* zinc, aluminum or various hardenable organic potting compounds, and desirably is formed (*e.g.*, molded) from polysulfone.

[0044] As shown in **Fig. 4b**, the portions of magnet **400** and layer **401** that were exposed in **Fig. 4a** have been covered with a layer **404** of an additional poly(tetrafluoro-p-xylene) conformal coating. As also shown in **Fig. 4b**, potting material **402** and layer **404** have been covered with a polysulfone thermoplastic overlayer **406**. A mask (not depicted in **Fig. 4b**) has been used to limit the extent of layer **404** and prevent layer **404** from covering portions of potting material **402** that were exposed in **Fig. 4a**. A variety of masking techniques may be employed, and with care can provide embodiments in which layers **401** and **404** merge to provide a single layer of apparently uniform thickness.

10 Boundary **408** represents the contact area between potting material **402** and overlayer **406**. When potting material **402** and overlayer **406** are both made from polysulfone, boundary **408** desirably is not discernible due to melting of a portion of potting material **402** and merger with overlayer **406** when overlayer **406** is formed. As depicted in **Fig. 4b**, overlayer **406** includes features **410** and **412** respectively representing a recess below and 20 protrusions beyond the average thickness of overlayer **406**.

[0045] **Fig. 5** and **Fig. 6** are perspective views, partially in phantom, of another embodiment of the disclosed magnetic article. As shown in **Fig. 5**, NdFeB ring magnet **500** has been coated with a poly(tetrafluoro-p-xylene) conformal coating **502**. Magnet **500** includes central aperture **504** and notch **506**. Arrow **508** depicts the direction of 25 magnetization for magnet **500**.

[0046] As shown in **Fig. 6**, magnet **500** from **Fig. 5** has been covered with a polysulfone thermoplastic overlayer **610**. As depicted in **Fig. 6**, overlayer **610** includes aperture **612** through the center of magnet **500**, spring retaining collar **614** which protrudes above the remainder of magnet **500**, and valve actuation tab **616** which protrudes below 30 the remainder of magnet **500**.

[0047] A variety of NdFeB magnets may be used to make the disclosed magnetic articles and implantable medical devices. The magnet may be a monolithic, homogenous solid article made for example by molding or machining the chosen NdFeB alloy. The magnet may instead be a non-homogenous article made for example by sintering together 35 particles of the chosen NdFeB alloy or by molding such particles in a suitable binder. In

5 some embodiments solid magnets may be preferred so as to maximize their magnetic strength. The magnet may have a variety of sizes, and may for example have a volume of at least 2, at least 5, at least 10 or at least 25 mm³.

[0048] The magnet may have a variety of magnetic properties, and may for example have a magnetic strength (Maximum Energy Product or BH_{max}) of at least 28, at least 30, 10 at least 32 or at least 35 Mega Gauss Oersteds (MGOe). The magnet may also or instead have an Intrinsic Coercive Force (H_{ci}) of at least 10, at least 14, at least 20, at least 25, at least 30 or at least 35 kiloOersteds (kOe). The magnet may also or instead have a Curie Temperature (T_c) of at least 300, at least 310, at least 320 or at least 330 ° C. In some embodiments, H_{ci} values of at least 25, at least 30 or at least 35 may be preferred so as to 15 reduce the likelihood of demagnetization due to externally-applied magnetic fields such as MRI fields. In some embodiments including smaller volume magnets covered with a thick injection-molded polysulfone overlayer, T_c values at least 310, at least 320 or at least 330 ° C may be preferred so as to reduce the likelihood of demagnetization during the overlayer formation step. The magnet may if desired be demagnetized during processing (e.g., for 20 ease in machining, or as a consequence of heat applied during magnet processing), and remagnetized at a later time (e.g., before, between or after the conformal coating or overlayer formation steps).

[0049] The magnet may have a variety of shapes including balls, bars, rods (e.g., cylinders), rings, partial rings (e.g., horseshoes) and plates (e.g., rectangles). The magnet 25 may have a major planar surface or major axis with a polarity of magnetization parallel to or at an angle with respect to such major planar surface or major axis.

[0050] Exemplary magnetic material suppliers include Alliance, LLC, Dexter Magnetics, Magstar Technologies, Inc., Inc., Hitachi Corporation, Dailymag Motor (Ningbo) Limited, Ningbo Xinfeng Magnet Industry Co., Ltd., Shenzhen Feiya Magnet 30 Co., Ltd. and Yuyao Keyli Magnetics Co., Ltd.

[0051] The disclosed magnetic devices may employ a variety of conformal coatings. In some embodiments the parylene is fluorinated, e.g., with fluorine atoms on the aromatic rings (viz., fluoroaromatic groups), fluoroaliphatic groups between the aromatic rings, or both. In some such embodiments the aromatic rings, the fluoroaliphatic groups, or both 35 are perfluorinated, and thus have no hydrogen atoms. Suitable fluorinated parylene

5 conformal coating materials include poly(tetrafluoro-p-xylene) which may be obtained under the generic name parylene AF-4, with Formula I shown below:



[0052] Exemplary commercially available parylene AF-4 materials include Parylene HTTM from Specialty Coating Systems, Inc., which is said by its manufacturer to have an 10 MP greater than 500° C, and an MVT of 0.22 at 100% relative humidity (RH) and 38° C. Another suitable parylene AF-4 material is diX SFTTM parylene from Kisco Conformal Coating, LLC, which is said by its manufacturer to have an MP of 450° C and an MVT of 0.21 at 37° C. Other suitable fluorinated parylenes may be obtained under the generic names parylene VT-4, with Formula II shown below:



[0053] In some embodiments the parylene has a melting point (MP) of at least about 430° C, and a moisture vapor transmission (MVT) less than about 0.5 g-mm/m²/day at 90% RH and 37° C. Some of the fluorinated parylenes described above also satisfy these conditions. In some embodiments the parylene has an MP of at least about 450° C, at least 20 about 475° C or at least about 500° C. In some embodiments the parylene may also or instead have an MVT less than about 0.4 or less than about 0.3 g-mm/m²/day at 90% RH and 37° C. Suitable parylenes having a melting point of at least about 430° C and a moisture vapor transmission less than about 0.5 g-mm/m²/day at 90% RH and 37° C include diX CFTM parylene from Kisco Conformal Coating, LLC, which is said by its 25 manufacturer to have an MP of 434° C and an MVT of 0.28 at 37° C. This parylene may also be a fluorinated parylene, but it is said by its manufacturer to have a proprietary formula and its structure does not appear to have been published.

[0054] Coatings made using the parylene preferably are rated as being thermally stable, or as being suitable for continuous service, at temperatures of at least 200° C, at 30 least 250° C or at least 300° C in air, or at temperatures of least 300° C, at least 350° C or at least 400° C in an oxygen-free environment.

[0055] The parylene conformal coating typically is formed by converting a solid parylene dimer into vapor-phase parylene radicals using a vaporizer and pyrolizer, and 35 depositing the radicals onto the exposed surface or surfaces of the NdFeB magnet in a suitable deposition or coating chamber. The conformal coating procedures described in

5 U.S. Patent Nos. 4,508,760 (Olson et al.), 4,758,288 (Versic '288) and 5,069,972 (Versic '972) may be adapted for that purpose, while bearing in mind that these patents describe parylene deposition onto microparticles or microcapsules rather than onto discrete magnets, and that the non-halogenated or chlorinated parylenes they employ have lower melting points and may have lower dimer vaporization temperatures than the parylenes
10 described above. Additional parylene coating procedures are described in the 2007 Specialty Coating Systems, Inc. Technical Brochure entitled "SCS Parylene Properties" and in the 2011 Specialty Coating Systems, Inc. Technical Brochure entitled "SCS Medical Coatings".

15 [0056] The thus-formed parylene coating or coatings may range from angstroms to micrometers or mils in thickness and may for example have a thickness of about 2 to 100 μm per coating layer or layers. For magnets that can be supported or otherwise fixtured without covering any of the surface to be coated, the disclosed magnetic articles preferably have at least one conformal coating layer. For magnets that require a support or other fixture that covers part of the surface to be coated, the disclosed magnetic articles may
20 have at least two conformal coating layers, with relocation or refixturing of the magnet being carried out between application of the first and subsequent layer or layers so as to ensure full coverage. Surface pretreatments or primer coatings (*e.g.*, plasma etching pretreatments or organic silane primers applied from solution or by vapor deposition) may be used prior to deposition of the parylene conformal coating or between coating layers.

25 The parylene conformal coating may if desired include dyes, indicators or other adjuvants, *e.g.* to facilitate inspection and confirm attainment of a continuous conformal coating layer. The parylene conformal coating may if desired be annealed (*e.g.*, at about 300° C for parylene AF-4 materials) to increase crystallinity and thereby improve physical properties such as cut-through resistance, hardness or abrasion resistance.

30 [0057] The disclosed magnetic devices may employ a variety of polysulfone materials. Exemplary polysulfones include crystalline or amorphous materials, such as polyethersulfone (PES, PSU or PESU), sulfonated polyethersulfone (SPES or SPSF) and polyphenylsulfone (PPSF or PPSU). Exemplary polysulfones include UDEL™ PSU, VERADEL™ PESU and RADEL™ PPSU, ACUDEL™ modified PPSU and
35 EPISPIRE™ HTS high-temperature sulfone from Solvay Plastics. Low to medium

5 viscosity or high to medium flow rate injection molding grades such as UDEL P-1700, UDEL P-1710, UDEL P-1750 MR, UDEL P-3700 HC PES, UDEL P-3703, VERRADEL 3250 MR, VERRADEL 3300 PREM, VERRADEL 3400, VERRADEL A-301, RADEL R-5000, RADEL R-5100, RADEL R-5600, RADEL R-5800, RADEL R-5900, RADEL R-5900 MR, RADEL R-7159, RADEL R-7300, RADEL R-7400, RADEL R-7535, RADEL 10 R-7558 and RADEL R-7625 (all from Solvay Plastics) are preferred for some embodiments. The disclosed implantable medical devices preferably are made using a polysulfone material approved for use in medical devices by the applicable regulatory agencies.

[0058] The polysulfone overlayer may be formed using a variety of techniques that 15 will be familiar to persons having ordinary skill in the art, with injection molding using a one-shot or multiple-shot (*e.g.*, two-shot) process being preferred for some embodiments, and dip coating, powder coating, spray coating or other techniques sufficient to encapsulate or otherwise cover the parylene conformal coating being preferred for other embodiments. The polysulfone overlayer may have a variety of average thicknesses, and 20 may for example have an average thickness of at least 0.5 mm, at least 1 mm, at least 2 mm or at least 5 mm. The polysulfone overlayer may have any desired maximum average thickness coincident with attaining sufficient magnetic strength in the coated magnetic article, and may for example be less than 100 mm, less than 50 mm, less than 25 mm, less than 10 mm, less than 5 mm or less than 1 mm. The recommended melting or molding 25 temperature typically will vary depending on factors including the chosen magnetic material, chosen parylene, chosen polysulfone, and (when used), the chosen mold. The polysulfone may be dried prior to melting or molding, for example to provide a moisture level less than about 0.1% or less than about 0.05% in the dried product. The polysulfone melting point or molding temperature preferably is less than the parylene melting point 30 and more preferably is also less than the magnet Curie temperature T_c . Polysulfone melting or molding temperatures higher than T_c may cause loss of magnetic strength. However, use of a quick molding cycle, low volume overlayer or high volume magnet may ameliorate loss of strength. Remagnetization may be employed after overlayer formation to restore magnetic strength. Exemplary polysulfone drying conditions and 35 melting or molding temperatures are described for example in the 2013 Solvay Technical

5 Bulletin entitled "Quick Guide to Injection Molding Udel® PSU, Radel® PPSU, Veradel® PESU, Acudel® modified PPSU".

[0059] The disclosed barrier helps reduce corrosion of the magnet due to exposure to gases (e.g., oxygen, air or water vapor), liquids (e.g., water, blood or other bodily fluids) or ions (e.g., sodium or chlorine ions). In some embodiments the disclosed coated 10 magnetic articles do not exhibit visible corrosion after 5 days, 10 days or 20 days immersion in 37° C normal saline solution. Preferred embodiments of the disclosed magnetic articles both retain their full magnetic strength and do not exhibit visible corrosion after 5 days, 10 days, 20 days or even 28 days immersion in 87° C normal saline 15 solution. Inductively-coupled plasma (ICP) mass spectrophotometric analysis of the saline solutions after such immersion preferably finds no detectable magnetic elements compared to saline controls prepared without the immersed magnetic article.

[0060] The disclosed magnetic articles may be part of a detector, actuator, latch, indicator or other mechanical, electrical or other system. If housed inside or on a larger device, the magnet may be stationary or movable within or on such device, and if movable 20 may be slidable, pivotable or rotatable. The magnet may bear upon or move another part of the device. The magnet may be a single magnet or multiple magnets within or on such device. The device may be an implantable medical device, such as the implantable CSF shunt valves described in the above-mentioned Bertrand et al. application, urethral control devices such as those shown in U.S. Patent No. 7,223,228 B2 (Timm et al.), implantable 25 blood pumps such as those shown in U.S. Patent No. 8,512,013 B2 (LaRose et al.), pacemakers, implantable drug pumps, and other devices that will be familiar to persons having ordinary skill in the medical arts. If part of an implantable medical device, the device may be sold in sterile packaging and designed for one-time use. Exemplary sterilization techniques will be familiar to persons having ordinary skill in the art, and 30 include heat, steam, chemical processes (e.g., ethylene oxide, nitrogen dioxide, bleach or various aldehydes) and irradiation (e.g., UV, gamma radiation or electron beam processing). The magnet may be part of a variety of non-implantable medical devices including hearing aids, external drug pumps and dental or orthodontic appliances (e.g., bridges, plates, dentures and orthodontic correctional devices). The magnet may also be

5 part of a variety of non-medical devices including sensors, switches, valves, indicators or signaling devices for uses including marine, automotive and defense systems.

[0061] Other embodiments of the disclosed invention include:

— A magnetic article comprising an NdFeB magnet having thereon a substantially continuous corrosion resistant barrier comprising a parylene conformal coating having a melting point of at least about 430° C and a moisture vapor transmission less than about 0.5 g-mm/m²/day at 90% RH and 37° C, the parylene conformal coating being covered with a polysulfone thermoplastic overlayer, or

10 — a method for making a coated magnetic article, which method comprises vapor depositing upon an NdFeB magnet a layer or layers of a poly(tetrafluoro-p-xylene) conformal coating, and applying a molten polysulfone overlayer over the poly(tetrafluoro-p-xylene) conformal coating, to provide a substantially continuous corrosion resistant barrier over the magnet, or

15 — a method for making a coated magnetic article, which method comprises vapor depositing upon an NdFeB magnet a layer or layers of a parylene conformal coating having a melting point of at least about 430° C and a moisture vapor transmission less than about 0.5 g-mm/m²/day at 90% RH and 37° C, and applying a molten polysulfone overlayer over the parylene conformal coating, to provide a substantially continuous corrosion resistant barrier over the magnet, or

20 — an implantable medical device containing a coated magnetic article comprising an NdFeB magnet having thereon a substantially continuous corrosion resistant barrier comprising a poly(tetrafluoro-p-xylene) conformal coating covered with a polysulfone thermoplastic overlayer, or

25 — an implantable medical device containing a coated magnetic article comprising an NdFeB magnet having thereon a substantially continuous corrosion resistant barrier comprising a parylene conformal coating having a melting point of at least about 430° C and a moisture vapor transmission less than about 0.5 g-mm/m²/day at 90% RH and 37° C, covered with a polysulfone thermoplastic overlayer,

30 and wherein either individually or in any combination:

5 — the magnet has a Maximum Energy Product BH_{max} of at least 28 Mega Gauss Oersteds, an Intrinsic Coercive Force H_{ci} of at least 10 kiloOersteads and a Curie Temperature T_c of at least 300° C, or

10 — the magnet has a Maximum Energy Product BH_{max} of at least 32 Mega Gauss Oersteds, an Intrinsic Coercive Force H_{ci} of at least 35 kiloOersteads and a Curie Temperature T_c of at least 310° C, or

15 — the magnet comprises a bar, rod, ring, partial ring or plate, or

 — the conformal coating has a thickness of 2 to 100 μm , or

 — the overlayer comprises polyethersulfone, or

 — the overlayer comprises sulfonated polyethersulfone or polyphenylsulfone, or

20 — the overlayer has an average thickness of 0.5 to 10 mm, or

 — the overlayer has a variable thickness, or

 — the overlayer is an overmolding, or

 — the polysulfone melting point is less than the parylene melting point, or

 — the polysulfone melting point is also less than the magnet Curie temperature T_c , or

25 — the conformal coating has a thickness less than 0.5 mm and the overlayer has an average thickness greater than 0.5 mm, or

 — the magnet or overlayer has a recess or protrusion, or

 — the recess or protrusion comprises a groove, notch, detent, aperture, spline, tab, stop, step, sealing surface, pivot point, axle, bearing surface, indicator to depict direction of fluid flow or magnetization, spring retaining collar, valve or valve actuator, or

30 — the magnet does not exhibit visible corrosion after 5 days immersion in 37° C normal saline solution, or

 — The magnet retains its full magnetic strength without exhibiting visible corrosion after 20 days immersion in 87° C normal saline solution.

Example 1

[0062] NdFeB ring magnets having a 32 Mega Gauss Oersteds BH_{max} value and shaped like magnet 500 shown in Fig. 5 were coated with two 17 μm thick conformal

coating layers of Parylene HT from Specialty Coating Systems, Inc. Prior to the application of the conformal coating layers, the magnets were gripped at different fixturing positions in order to ensure application of a continuous conformal coating layer. The thus-coated magnets were covered with polyethersulfone using a two-shot injection molding process to produce encapsulated, barrier-coated magnets like those shown in **Fig. 6**. The magnets were immersed for 28 days in 87° C normal saline solution and then removed for evaluation. The magnets did not exhibit visible corrosion, and retained their full pre-immersion magnetic strength. Inductively-coupled plasma (ICP) mass spectrophotometric analysis of the saline solution found no detectable magnetic elements after such immersion compared to saline controls prepared without the immersed magnet.

Comparison Example 1

[0063] NdFeB ring magnets like those used in Example 1 could be coated with a conformal coating made using Parylene C ($-\text{CH}_2(\text{C}_6\text{H}_3\text{Cl})\text{CH}_2-$) from Specialty Coating Systems, Inc. Parylene C has a much lower melting point than that of polyethersulfone (*viz.*, 290° C for Parylene C and about 360° C for polyethersulfone). Overmolding with polyethersulfone would be expected to destroy the conformal coating.

Comparison Example 2

[0064] NdFeB ring magnets like those used in Example 1 could be coated with a conformal coating made using Parylene N ($-\text{CH}_2(\text{C}_6\text{H}_4)\text{CH}_2-$) from Specialty Coating Systems, Inc. Parylene N has a 420° C melting point and thus might be overmolded with polyethersulfone. However, Parylene N also has less temperature resistance than Parylene HT (*viz.*, a short term service temperature rating of 80° C for Parylene N and 450° C for Parylene HT, and a continuous service temperature rating of 60° C for Parylene N and 350° C for Parylene HT). Overmolding with polyethersulfone would require extra care in order not to compromise the conformal coating. Parylene N also has greater moisture vapor transmission than Parylene HT (*viz.*, 0.59 g-mm/m²/day at 90% RH and 37° C for Parylene N and 0.22 g-mm/m²/day at 100% RH and 37° C for Parylene HT). A barrier made using Parylene N overmolded with polyethersulfone would be expected to provide less corrosion resistance than the barrier of Example 1.

Comparison Example 3

[0065] NdFeB ring magnets like those used in Example 1 could be coated with a conformal coating made using Parylene D ($-\text{CH}_2(\text{C}_6\text{H}_2\text{Cl}_2)\text{CH}_2-$) from Specialty Coating Systems, Inc. Parylene D has a 380° C melting point, which is slightly higher than that of polyethersulfone. Parylene D has less temperature resistance than Parylene HT (*viz.*, Parylene D has a short term service temperature rating of 120° C and a continuous service temperature rating of 100° C). Overmolding with polyethersulfone would require extra care in order not to compromise the conformal coating.

Example 2

[0066] The barrier-coated magnets described in Example 1 can be used as a magnetic rotor assembly to control the flow of CSF fluid in a shunt valve like that shown in the above-mentioned Bertrand et al. application. In an initial field trial, shunt valves containing the disclosed barrier-coated magnets and magnetic rotor assemblies were successfully surgically implanted in 13 human patients and confirmed to be operational. The rotor assemblies are expected to resist corrosion by bodily fluids, as well as unintended changes in rotor (*viz.*, pressure) settings, demagnetization and re-magnetization when exposed to a 3 Tesla MRI field.

[0067] The complete disclosure of all cited patents, patent applications, technical bulletins and other publications are incorporated herein by reference as if individually incorporated.

[0068] Although specific and in some cases preferred embodiments have been illustrated and described, it will be appreciated by those of ordinary skill in the art that a variety of alternate or equivalent embodiments calculated to achieve the same purposes may be substituted for the specific embodiments shown and described above. This application is intended to cover any such adaptations or variations of the embodiments discussed herein. Therefore, it is manifestly intended that this invention be limited only by the claims and the equivalents thereof.

Claims:

1. A magnetic article comprising an NdFeB magnet having thereon a substantially continuous corrosion resistant barrier comprising:
 - a) a fluorinated parylene conformal coating, or
 - b) a parylene conformal coating having a melting point of at least 430° C and a moisture vapor transmission less than 0.5 g-mm/m²/day at 90% RH and 37° C, the conformal coating being covered with a polysulfone thermoplastic overlayer.
2. A method for making a coated magnetic article, which method comprises:

vapor depositing upon an NdFeB magnet a layer or layers of:

 - a) a poly(tetrafluoro-p-xylene) conformal coating, or
 - b) a parylene conformal coating having a melting point of at least about 430° C and a moisture vapor transmission less than about 0.5 g-mm/m²/day at 90% RH and 37° C, and

applying molten polysulfone over the poly(tetrafluoro-p-xylene) or parylene conformal coating, to provide a substantially continuous corrosion resistant barrier over the magnet.
3. An implantable medical device containing a coated magnetic article comprising an NdFeB magnet having thereon a substantially continuous corrosion resistant barrier comprising:
 - a) a poly(tetrafluoro-p-xylene) conformal coating, or
 - b) a parylene conformal coating having a melting point of at least 430° C and a moisture vapor transmission less than 0.5 g-mm/m²/day at 90% RH and 37° C, the conformal coating being covered with a polysulfone thermoplastic overlayer.
4. A magnetic article according to claim 1, method according to claim 2 or medical device according to claim 3, wherein the conformal coating has a moisture vapor transmission less than 0.3 g-mm/m²/day at 90% RH and 37° C.

5. A magnetic article according to claim 1, method according to claim 2 or medical device according to claim 3, wherein the magnet has a Maximum Energy Product BH_{max} of at least 32 Mega Gauss Oersteds, an Intrinsic Coercive Force H_{ci} of at least 35 kiloOersteads and a Curie Temperature T_c of at least 310° C.
6. A magnetic article according to claim 1, method according to claim 2 or medical device according to claim 3, wherein the magnet comprises a bar, rod, ring, partial ring or plate.
7. A magnetic article according to claim 1, method according to claim 2 or medical device according to claim 3, wherein the fluorinated parylene has fluoroaliphatic groups.
8. A magnetic article according to claim 1, method according to claim 2 or medical device according to claim 3, wherein the fluorinated parylene has fluoroaromatic groups.
9. A magnetic article according to claim 1, method according to claim 2 or medical device according to claim 3, wherein the conformal coating comprises poly(tetrafluoro-p-xylene) or parylene VT-4.
10. A magnetic article according to claim 1, method according to claim 2 or medical device according to claim 3, wherein the overlayer comprises polyethersulfone.
11. A magnetic article according to claim 1, method according to claim 2 or medical device according to claim 3, wherein the overlayer comprises sulfonated polyethersulfone or polyphenylsulfone.
12. A magnetic article according to claim 1, method according to claim 2 or medical device according to claim 3, wherein the conformal coating has a thickness of 2 to 100 μm and the overlayer has an average thickness of 0.5 to 10 mm.
13. A magnetic article according to claim 1, method according to claim 2 or medical device according to claim 3, wherein the overlayer has a variable thickness.
14. A magnetic article according to claim 1, method according to claim 2 or medical device according to claim 3, wherein the overlayer is an overmolding.

15. A magnetic article according to claim 1, method according to claim 2 or medical device according to claim 3, wherein the polysulfone melting point is less than the parylene melting point.
16. A magnetic article, method or medical device according to claim 15, wherein the polysulfone melting point is also less than the magnet Curie temperature T_c .
17. A magnetic article according to claim 1, method according to claim 2 or medical device according to claim 3, wherein the magnet or overlayer has a recess or protrusion.
18. A magnetic article, method or medical device according to claim 17, wherein the recess or protrusion comprises a groove, notch, detent, aperture, spline, tab, stop, step, sealing surface, pivot point, axle, bearing surface, indicator to depict direction of fluid flow or magnetization, spring retaining collar, valve or valve actuator.
19. A magnetic article according to claim 1, method according to claim 2 or medical device according to claim 3, wherein the magnet does not exhibit visible corrosion after 5 days immersion in 37° C normal saline solution.
20. A magnetic article according to claim 1, method according to claim 2 or medical device according to claim 3, wherein the magnet retains its full magnetic strength without exhibiting visible corrosion after 20 days immersion in 87° C normal saline solution.

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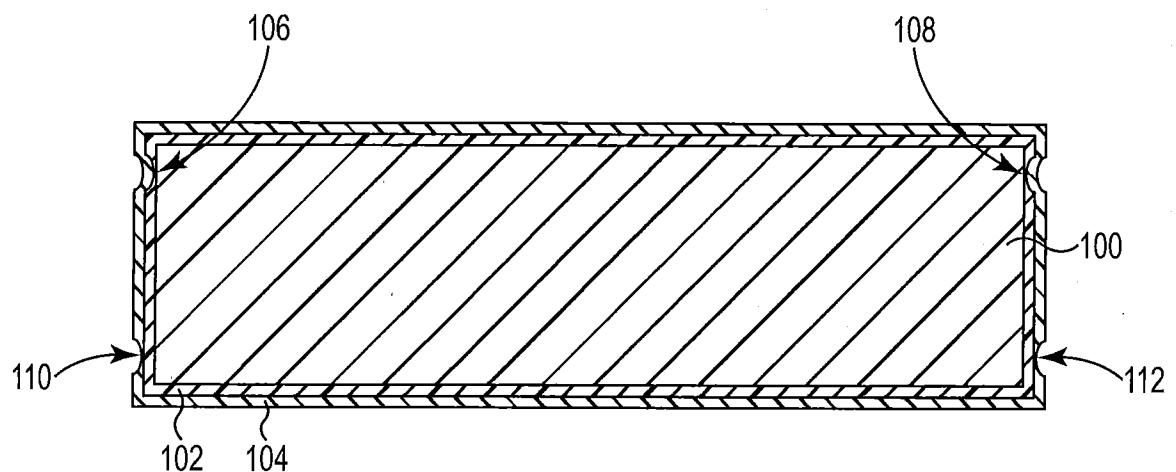


Fig. 1

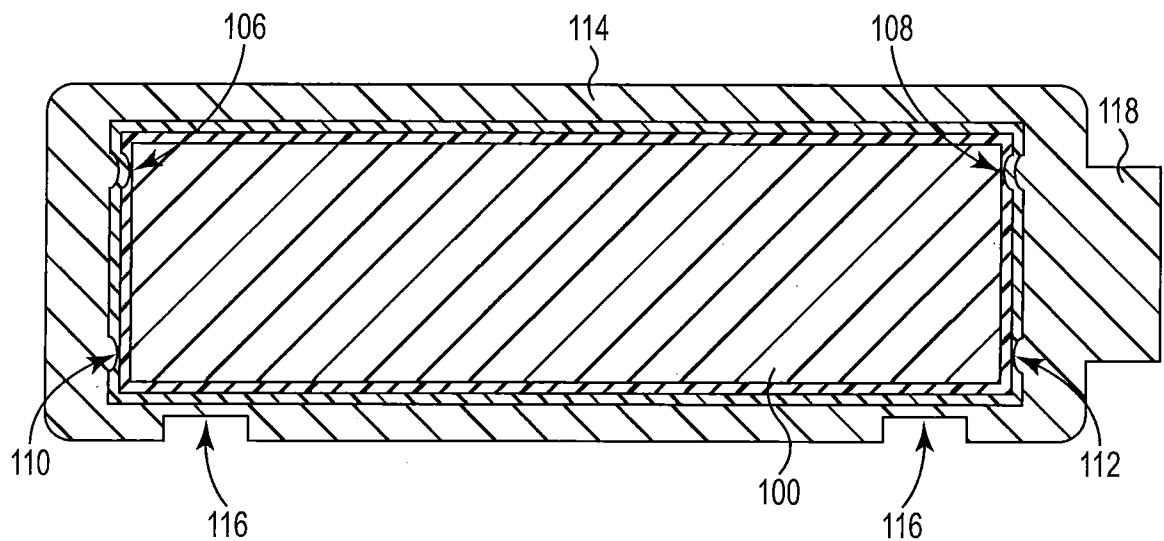
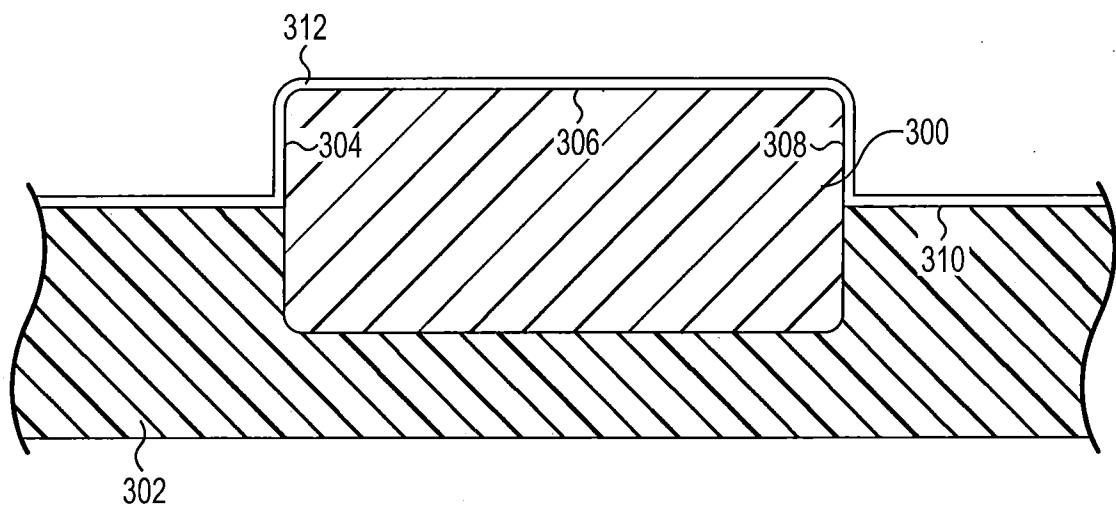
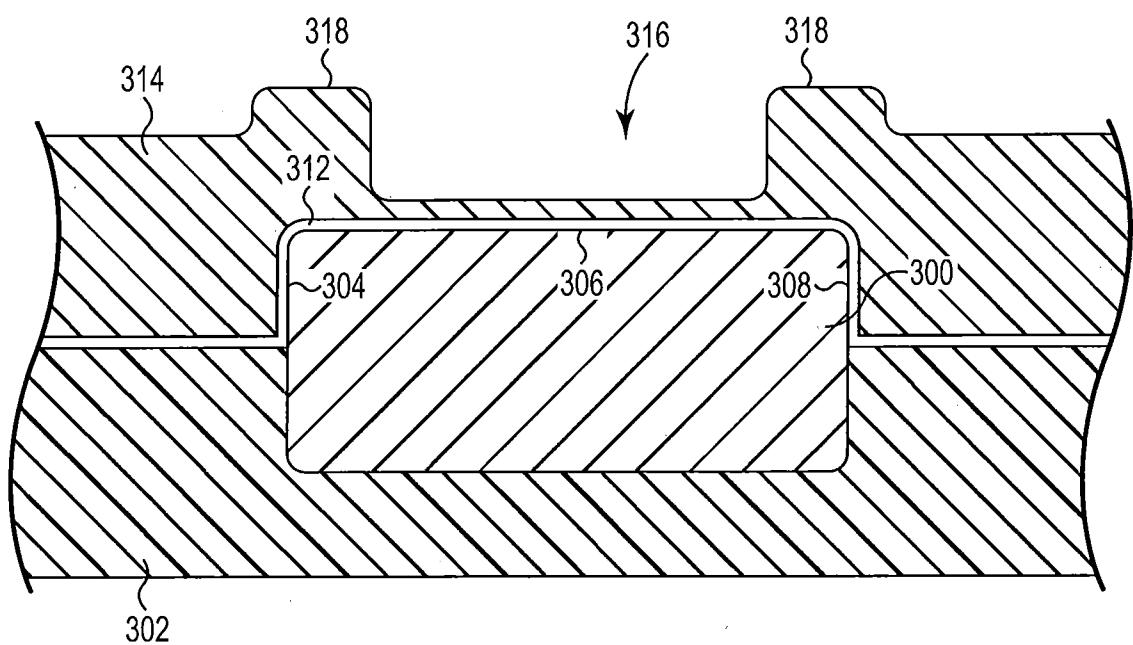
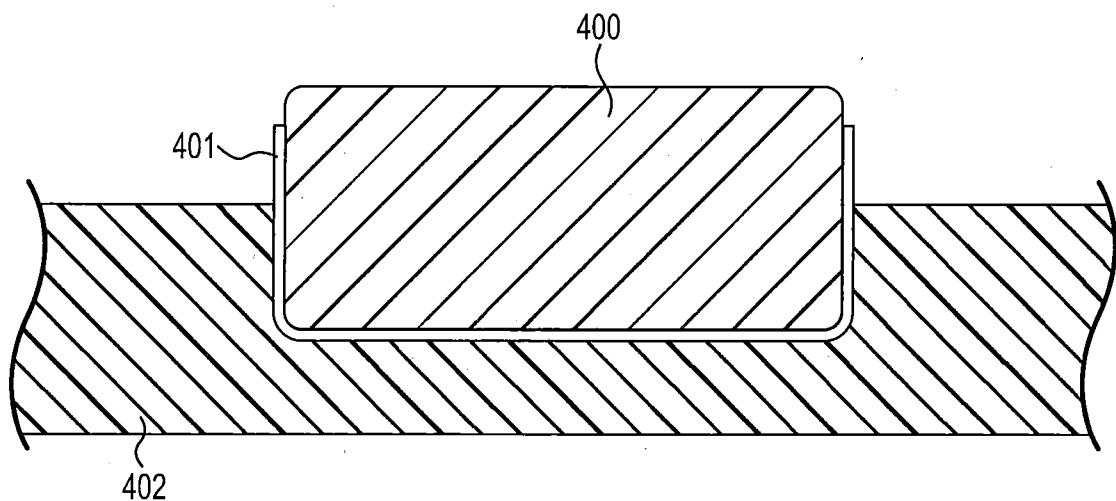
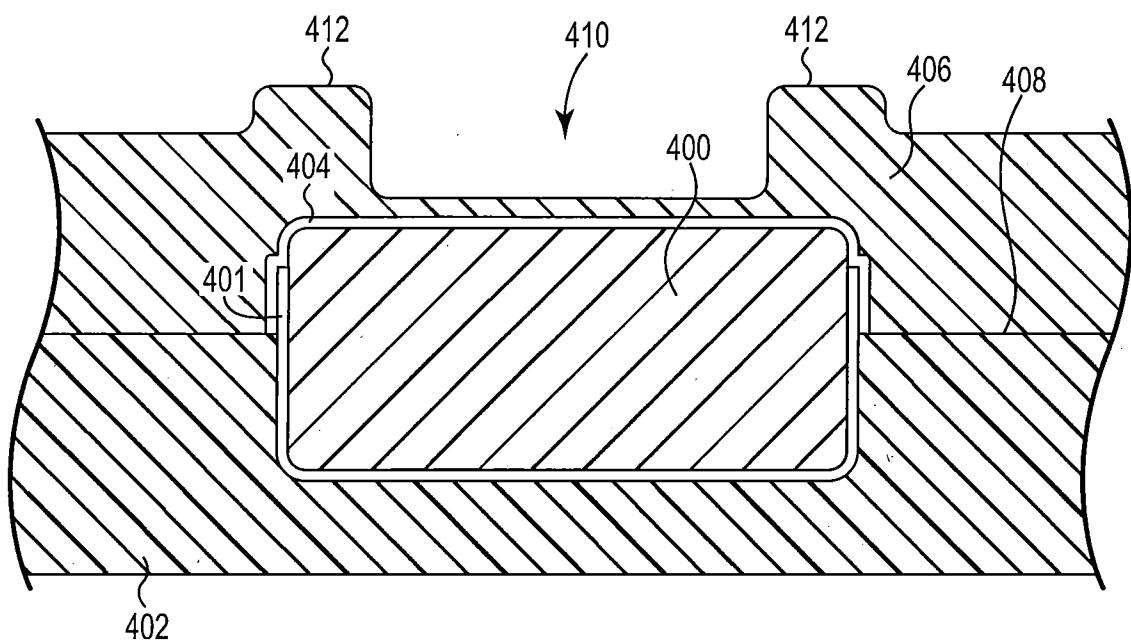


Fig. 2

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**Fig. 3a****Fig. 3b**

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**Fig. 4a****Fig. 4b**

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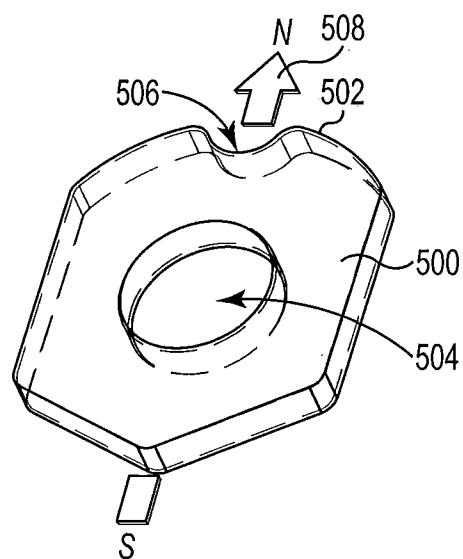


Fig. 5

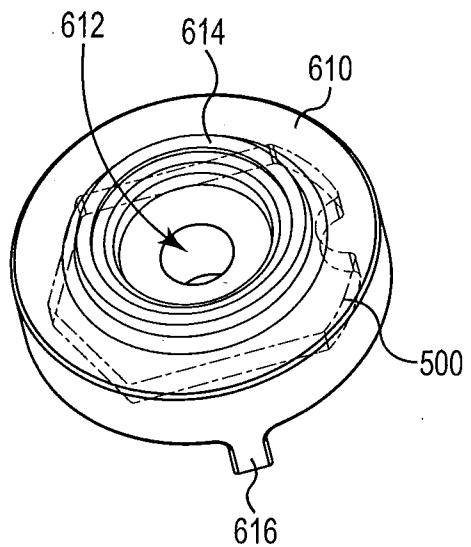


Fig. 6