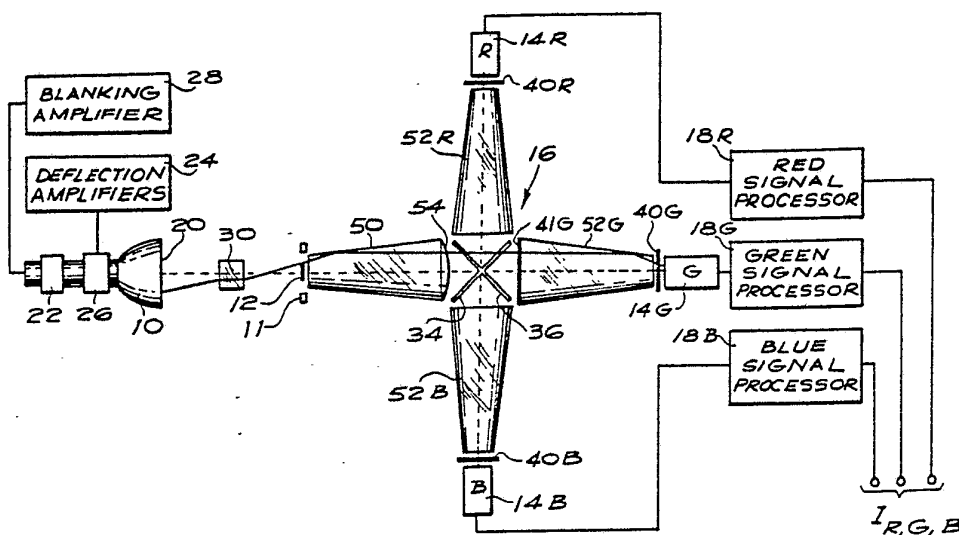




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(54) Title: LIGHT COLLECTION APPARATUS FOR A SCANNER



(57) Abstract

In apparatus for scanning a transparent original with a scanning beam relative an optical axis, a tapered optical bar is positioned adjacent the transparent original to collect a diverging beam emerging from the original and, by means of internal reflection, reduce the divergence of the beam relative the optical axis. The emerging beam is especially diverged when the scanning beam sweeps away from the optical axis or is scattered by a blemish, such as a scratch, on the original. Particularly in the case of a polychromatic beam emerging from a color transparency, the tapered bar is interposed between the transparency and color dichroic beam separating mirrors to reduce angle shift and polarization color shading due to light rays diverging from the optical axis upon the dichroic interference layers.

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LIGHT COLLECTION APPARATUS FOR A SCANNER

The invention generally relates to an optical scanning apparatus for collecting the light rays of a scanning beam emerging from a scanned transparency. More specifically the invention relates to an apparatus for collecting and separating a polychromatic scanning beam into a plurality of separate beams composed of different wavelengths and, especially, to such optical apparatus having means for suppressing the effect of light-scattering blemishes in the transparency.

In a color-separating apparatus for optically separating a beam of polychromatic light, the beam is ordinarily split into several components - red, green and blue - and directed toward separate photosensitive targets. This is conventionally done by passing the beam through two or more partially reflecting mirrors (often referred to as dichroic mirrors) having optical interference layers with color-selective reflecting and transmitting properties. The band of wavelengths reflected by an interference layer is strongly dependent on the effective optical path taken by a ray through the layer as determined mainly by the angle of incidence of the impinging beam relative to the normal. Where two or more interference layers are applied to a mirror, as is frequently the case, the selective reflection effect is further affected by incident angle-shift as the path length is changed in varying degrees in the different layers. In either case, as the incident angle increases further from the normal, the spectral cut of the dichroic filter, i.e., as exemplified by the reflection curve, shifts toward progressively smaller wavelengths.



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In addition, with an increasing angle of incidence, an undesirable polarization phenomenon occurs due to asymmetry in the response of the electric vector characterizing the light beam. The electric vector for each wavetrain in the light beam can be resolved into two components, one perpendicular to the plane of incidence (the perpendicular component) and one lying in this plane (the parallel component). With increasing angle of incidence the coefficient of reflection becomes greater for the perpendicular component and smaller for the parallel component, meaning that the perpendicular component is preferentially reflected. As a result, the mean reflection caused by both components is color-shifted as the angle of incidence is increased. In the case of either effective optical path shift or polarization effect, undesirable color shifts occur across the images formed upon the photosensitive targets.

A number of optical designs have been proposed to control polarization and angle shift characteristics in color scanners. For example, in using a flying spot scanner to form a raster scan upon a transparency, at least one condenser lens is usually inserted in the optical path to refract the beams emanating from points outside the middle of the raster towards the axis of the system. This is done in such a way that the axes of most beams reach the dichroic mirrors at a similar angle irrespective of their point of origin on the raster (see H. van Ginkel, "Flying-Spot Scanners for Colour Television" Philips Technical Review, vol. 21, 1959/60, pp. 234-250). Another optical design is based on the Philips color-separating prism system described in the de Lang and Bouwhuis article "Color Separation



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in Colour-Television Cameras" in the Philips
Technical Review, Vol. 24, 263-271, 1962/63. This
prism system utilizes a compact combination of
interference layers cemented between faces of prisms
and small air gaps between selected sets of prisms.
The Philips optical geometry in combination with
glass prisms allows the angles of incidence to be
reduced over what can be obtained with conventional
open air plate type color separation systems.

Neither the condenser lens nor the prism
system, however, is sufficiently effective to
control the widely diverging rays. Particularly in
the case of a transparency, light-scattering
blemishes (such as scratches, dust particles, and
the like) are common sources of widely diverging
rays. A typical blemish is a scratch on the
transparency which scatters light from a scanning
beam. The scattered light may be at such an extreme
angle that it cannot be collected by the light
collection apparatus. In these cases, the signal to
the photosensitive targets will be less than that
for areas immediately adjacent to the scratch that
contain the same scene detail. Where a reproduction
is made from such target signals, the scratch is
visible because of the decreased signal.

An electronic partial solution to this
problem is described in U.K. Specification 1409153
which describes a procedure for detecting light
scattered from blemishes on cine film in order to
electrically substitute a grey level or adjacent
picture signal for the scanning signal obtained from
the blemished area. Besides the circuit complexity
of implementing such a procedure, the blemished area
is incorrectly reproduced relative its original
color and density.



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The present invention was made in view of the above-described defect of the prior technology and its object is to provide an apparatus for collecting light emerging from a scanned area of a color transparency having a light-scattering blemish therein. The effect of our invention is to produce a correctly colored correct density image of the colored copy made from the output signals of the apparatus.

The present invention resides in an apparatus for scanning a transparent original with a light beam relative to an optical axis and for collecting the portion of the beam transmitted through said original wherein the direction of the light beam rays emerging from respective areas of the original varies with respect to the optical axis, said apparatus comprising:

- means (10) for generating a light beam;
- means (11) for supporting the transparent original in the path of the beam;
- means (26) for scanning the beam across at least one dimension of the transparent original; a tapered optical element (50) is positioned on the optical axis, said element having differently sized apertures at opposite ends thereof and a tapered reflecting surface therebetween; the optical element being positioned with its smaller aperture adjacent said transparent original to collect the light beam rays emerging from said transparent original and its tapered surface oriented to internally reflect at least some of the light beam rays toward the larger aperture such that the direction of the rays emerging from the larger aperture vary less with respect to the optical axis than the direction of the rays emerging from the transparent original.



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The invention has particular utility for collecting light emerging from a scanned area of a transparency having a light-scattering blemish thereon. The transparency is supported in the scanning light beam whereby the beam emerging from the transparency is scattered by the blemish. The tapered optical element is positioned adjacent the transparency to collect a substantial portion of the scattered light at its smaller input aperture and substantially reduce the divergence of the scattered beam at the output end of the element.

In a preferred embodiment, a color transparency is scanned by a polychromatic beam. Means are provided for separating the polychromatic beam emerging from the transparency into a plurality of spectral components. The tapered optical element is interposed between the transparency and the spectral separating means for reducing the angular divergence of the beam of light passing to the spectral separating means.

The invention will be described with reference to the drawings, wherein:

Figure 1 is a block diagram illustrating the optical design of a flying spot transparency scanner known in the prior art;

Figures 2A and 2B are ray diagrams of typical light paths of light beams passing through a transparency without hindrance and scattering from a scratch on a transparency, respectively;

Figure 3 is a block diagram illustrating the optical design of a flying spot scanner incorporating a light collecting and color separating apparatus in accordance with the invention;



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Figures 4A and 4B are enlarged diagrams of the light collecting and color separating apparatus of Figure 3 showing also a ray diagram of a typical path of a light ray scattered from a scratch on the transparency and through tapered bars in accordance with the invention;

Figure 5 is a diagram of one of the tapered bars incorporating a high gain light diffusion filter on one end thereof;

Figure 6 is an alternative embodiment of the invention useful with apparatus that provides movement of the transparency during scanning; and

Figure 7 is a further embodiment of the invention for use without a beamsplitter.

Since optical scanners are well known in which transparent material such as slides, negatives or movie film is scanned, the present description will be directed in particular to elements forming part of, or cooperating more directly with, the present invention. Optical scanner elements not specifically shown or described herein may be selected from those known in the art. Scanning equipment with such elements includes graphic arts scanners, telecine and slide scanning apparatus, as well as photographic printers. Since the invention has particular utility with the optical scanning of color transparencies, the description will be directed to this application. However, the invention may be used with color or black and white transparencies, positive or negative transparencies, or transparencies in separate "still" form or joined together as motion picture film. Moreover, apparatus in accordance with the invention is useful wherever it is desirable to reduce the incident angle of a beam of light - whether or not



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polychromatic - relative to a receiving surface. Furthermore, the source of the scanning beam is clearly a matter of choice. For illustrative purposes only, the invention is described in terms
5 of a beam generated by a cathode ray tube flying spot scanner. Other scanning beams generated from, for example, a laser or a solid state light source are suitable for use with the invention.

Referring to Figure 1, a conventional
10 flying spot scanner is illustrated using a conventional combination of crossed dichroic beamsplitting mirrors (34 and 35) and beam converging condenser lenses (32, 38R, 38C and 38B). A uniformly bright scanning raster is produced by
15 exciting phosphors on a cathode ray tube 10. The raster is imaged upon a transparency 12 positioned in a film gate 11 on the optical axis 13 of the scanner apparatus. (An exemplary transparency for such a system is a photographic film transparency,
20 either a color negative or positive.) The modulated light emerging from the transparency 12 is directed upon three photoelectric cells 14R, 14G and 14B, for red, green and blue light respectively, via beamsplitting apparatus (16). The photoelectric
25 cells may be conventional photocells, phototubes, solid state receptors, or the like. The resultant output, after amplification and suitable processing in processors 18R, 18G and 18B, constitutes the image signal I. With this scanning arrangement,
30 illumination of each elementary area of the transparency occurs only at the moment of scanning and for a short period immediately afterward during which emission from the phosphor persists.

In order to get a sharply focused spot on
35 the faceplate of the scanning tube 10, the electron



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beam generated within is converged toward the phosphor screen 20 by a magnetic field generated by a focusing coil 22. The horizontal and vertical sweeping of the beam is provided by horizontal and vertical waveforms generated in deflection amplifiers 24 and applied to a deflection coil 26. The electron beam is suppressed during the flyback period by a blanking amplifier 28. To be satisfactory for color rendition of a photographic film transparency, a suitably doped phosphor is incorporated into the phosphor screen to generate emissions in the desired portions of the spectrum. While selected for a short afterglow, phosphors continue to emit light for some time after their excitation thereby affecting the electrical response of the signals obtained from the photocells 14R, 14G and 14B. Suitable equalization is therefore provided in the processors 18R, 18G and 18B to compensate for the effects of phosphor afterglow.

20 A conical scanning beam is formed by an objective lens 30 from the scanning spot of light on the faceplate 20 of the scanning tube 10. The scanning beam is imaged to a spot upon a small area of the transparency 12. The intensity of the beam emerging from the other side of the transparency 12 depends upon the optical density of each small area of the transparency interposed in the path of the scanning beam, i.e., the optical density of each small area modulates the intensity of the beam. A condenser lens 32 refracts the modulated beam emanating from points away from the middle of the raster toward the axis of the beamsplitting arrangement 16 so that the beam reaches the beamsplitter at a reduced angle relative the optical axis 13. A pair of dichroic mirrors 34 and 36



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arranged in cruciform position constitute the beamsplitter. Each mirror includes one or more interference layers for selectively reflecting and transmitting portions of the spectrum. The mirror
5 34 reflects the red component of the beam to the red photocell 14R while transmitting the blue and green components. The mirror 36 reflects the blue component of the beam to the blue photocell 14B while transmitting the red and green components.
10 The green component of the beam is passed through both mirrors to the green photocell 14G.

The condenser lens 32 cooperates with a set of condenser lenses 38R, 38G and 38B to form an
15 image of the exit pupil of the objective lens 30 at the plane of the photosensitive surfaces of respective photocells 14R, 14G and 14B. The red, green and blue beams are ordinarily passed through respective color trimming filters 40R, 40G, and 40B
20 to improve the spectral characteristics of each color channel. The electrical signals generated by the photocells 14R, 14G and 14B are applied to the processors 18R, 18G and 18B, which typically comprise a set of video amplifiers, for the
25 aforementioned afterglow correction and for a contrast correction to render correct tone reproduction (gamma correction). The processed red, green and blue signals $I_{R,G,B}$ are then available
for use in a variety of imaging processes.

Figures 2A and 2B illustrate respective
30 disadvantages of the system of Figure 1 when scanning a transparency, especially at its periphery, and when scanning over a scratch or dust particles on the transparency. Referring first to Figure 2A, light rays A1 and A2 (generated by the
35 flying spot scanning tube 20, shown in Figure



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1, and focused by the objective lens 30) represent the extreme rays of a beam striking the central portion of the transparency 12. Light rays B1 and B2 represent the extreme rays of a beam striking a peripheral portion of the transparency 12. Each beam is refracted by the condenser lens 32 and directed toward the crossed dichroic mirrors 34 and 36.

Each dichroic filter is designed to provide optimum spectral separation of a predetermined narrow-band spectral component for a specified incident angle relative to the normal, i.e., in this case a design angle of 45° relative the normal. However, as hereinbefore explained, the transmission (and reflection) characteristic of dichroic filters is strongly affected by incident angle shift, i.e., as the incidence angle increases(decreases) relative the normal, the spectral cut of a dichroic filter shifts toward progressively smaller(larger) wavelengths. While any angle shift is detrimental, dichroic mirrors arranged at 45° will ordinarily tolerate a small shift before the band edge characteristics change so substantially as to grossly affect the desired spectral separation. For example, if the objective lens 30 operates at F/4 the rays A1 and A2 will converge toward the transparency 12 at $\pm 7^{\circ}$. Although the transmission passband of the mirror 36 and the mirror 34 will be affected as the incidence angle varies from the design angle, such a small shift is customarily tolerated despite its contribution of color shading problems.

However, unlike rays A1 and A2, extreme ray B1 strikes 1) the blue reflecting dichroic mirror 36 at an angle significantly greater than the design



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angle of 45° and 2) the red reflecting mirror 34 at an angle significantly less than 45° . This introduces unwanted polarization shifts and respectively increases(decreases) the optical path(s) through the dichroic mirror 36(34) and shifts the cutoff wavelength of the reflection passband toward smaller(larger) wavelengths. For angles greater than the design angle, the blue reflecting mirror 36 cuts off at shorter wavelengths of nominally blue light, permitting some longer wavelength blue light to transmit and eventually reach the green photocell 14G. Moreover, the reflection band of the red reflecting mirror 34 now shifts toward longer wavelength red light thus permitting some shorter wavelength red light to pass through to the green photocell 14G. This leads to an undesirable color shading of the output signal for affected wavelengths of rays derived from the periphery of the transparency, i.e., portions of the image will be incorrectly colored if a colored copy is made from the output signals.

Referring now to Figure 2B, a scratch S located on the transparency 12 has irregular surfaces that refract and scatter light over a wide angular range. Some of the light C1 escapes from the optical system and is not collected by the condenser lenses 32, 38R, 38G or 38B so that the resultant signal to the photocells 14R, 14G or 14B will be less than that for areas immediately adjacent to the scratch that contain the same scene detail. The scratch will be readily visible in a color copy because of the decreased signal. The scratch may also appear on, for example, a color copy in a different color from the adjacent areas because of the changed angle of incidence relative



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to the dichroic mirrors 34 and 36 that accompanies the collection of some of the scattered light.

Incident beam C is exemplary of a green component of a beam that, but for the scratch S, would strike the dichroic mirrors 34 and 36 substantially at the designed incidence angle of 45° and transmit (as shown by broken line) to the photocell 14G. (Red and blue components of a beam may be similarly analyzed with respect to photocells 14R and 14B.) However the scratch S scatters the light beam C into a wide angular field. Rays C1 and C3 are exemplary of the light scattered entirely away from the dichroic mirrors 34 and 36. Depending on the arrangement of the beamsplitting apparatus (particularly regarding baffles and other light blocking elements), the ray C1 is not collected by any of the condenser lenses 38R, 38G and 38B and therefore results in a signal loss for the corresponding area on the transparency. The ray C3 is collected by the condenser lens 38B without intercepting the dichroic mirrors 34 and 36 and therefore produces a false color signal for the scratched area on the transparency. A ray C2 is intercepted by the dichroic mirror 34 but at an incident angle significantly greater (with respect to the normal) than intended by the design. Consequently, the greater angle shifts the spectral cut of the red-reflecting band of the mirror 36 toward shorter wavelengths reaching into the green component of the spectrum and causes the reflection of a portion of the green light to the red photocell 14R. The result is a false color signal from the corresponding scratched area of the transparency leading to undesirable color shading for that area in a copy made from the output signals from the



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photocells.

These problems are particularly critical in the green channel since the bandwidth of the light reaching the photocell 14G is ordinarily determined by the cutoffs of the reflection curves of the interference layers of both mirrors 34 and 36, i.e., angle shifts can affect the green bandwidth at each side of its passband. While Figures 2A and 2B have been discussed in connection with such particular bands of wavelengths, i.e., green, it should be clear that many other bands, or combinations of bands, of wavelengths will produce similar unwanted reflections and, in some cases, unwanted transmissions.

Figure 3 is a diagram of a flying spot scanner incorporating a beamsplitting and light collection apparatus in accordance with the invention. Elements having the same reference numbers as in Figure 1 have similar functions in Fig. 3. The flying spot on the face plate 20 of the scanner tube 10 is imaged by the objective lens 30 upon the transparency 12 positioned in the gate 11. A tapered bar 50 is positioned in close proximity to the surface of the transparency. A 1-3mm spacing therebetween has been found suitable. Sometimes referred to as an integrating bar, the tapered bar 50 has the property of total internal reflection for a light ray entering its entrance aperture. It is formed of a relatively light-transparent material, for example, glass or a suitable plastic such as PlexiglasTM acrylic plastic. (Glass is preferable as it is more optically homogeneous than plastic.) Substantially all light emerging from the transparency 12 is captured by the entrance aperture of the tapered bar 50 and is transmitted either



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directly or by total internal reflection to the exit aperture of the bar 50. While the tapered bar 50 may have a substantially planar exit aperture surface, it has been found useful to have the exit aperture rendered convex to act as a condenser lens 54, which serves to further collimate the light diverging from the spot focused on the transparency 12. The light exiting the tapered bar 50 is split into three spectral components by the crossed dichroic mirrors 34 and 36 and collected by the tapered bars 52R, 52G and 52B to strike the respective photocells 14R, 14G and 14B. The tapered bars 52R, 52G and 52B permit total internal reflection and are formed in a manner similar to the tapered bar 50.

Depending on the taper ratio, i.e., the ratio of the diameters (or like dimensions) of the exit aperture and entrance aperture faces, collimation or decollimation can be effected with a tapered bar. For example, a light beam entering the small end of a 3:1 taper at a 40° angle with respect to the optical axis will emerge from the large end within 12° of the optical axis (see discussion and data in S. E. Glazer, "Taper Measurement Techniques," Proc. of the Soc. of Photo-Optical Instrumentation Engineers, Vol. 31, 1972, pp. 13-22). The desired effect is obtained by internal reflection upon a surface inclining away from the optical axis. The condenser lens 54 formed at the exit aperture of the tapered bar 50 is useful for increasing collimation relative a given taper ratio but it is unessential in the practice of the invention.

As better seen in Figure 4A with respect to a ray diagram, the taper half angle X of the bar 50



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and the power of its condenser lens 54 are chosen to collimate or at least reduce the angular spread of the light accepted by the entrance aperture such that all the light exiting the bar and striking the dichroic filters is contained within a narrower angular range. With each internal reflection the angle which a light ray makes with the longitudinal axis Y of the bar 50 decreases by $2X^\circ$. As depicted in Figure 4A, an incoming beam D strikes a light-scattering blemish (such as a scratch S, a particle of dust, or the like) on the transparency 12 and scatters a ray D1 into the entrance aperture of the bar 50, becoming then a refracted ray D1 that reflects as ray D2. Thus the angle which ray D2 makes with the longitudinal axis Y of the bar 50 is $2X^\circ$ less than the angle which ray D1 makes therewith. The finally reflected ray D3 makes an angle with respect to the longitudinal axis Y that is $2nX^\circ$ less than the angle which ray D1 makes therewith, where n is the total number of reflections ($n=2$ in this illustration). The output ray is then further refracted by the condenser lens formed on the end of the bar 50.

The emergent ray D4 is therefore incident upon the dichroic mirrors 34 and 36 within a relatively small angular spread very near the design angle of 45° . To study the collimating power of a tapered bar, the narrowed angular spread was simulated by means of a pair of computer ray trace analyses. For both analyses, the rays emerging from a tapered bar were simulated for light (entering the bar) that originates at a point source located on the axis of the bar and 1.0mm from its first surface, i.e., on the surface of a hypothetical transparency. The bar used was 285mm in length and



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had an entrance face of 16x21mm and an exit face of 62x78mm with a condenser lens formed thereon. In the first analysis, light emanating from the point source on the transparency was assumed to be uniformly distributed over the angular range of $\pm 7^\circ$ to simulate a cone of focused specular light emerging from a substantially blemish-free area of the transparency. A ray emerging from the tapered bar was found to be substantially collimated. In the second analysis, light emanating from the point source on the transparency was assumed to be uniformly distributed over an angular range of $\pm 40^\circ$ to simulate the effect of diffuse light scatter when a specular scanning beam strikes a scratch or similar blemish on the transparency. In such case, rays emerging from the bar (corresponding to D4 in Figure 4) were found to be confined to a maximum angular range of $\pm 9.8^\circ$ relative to the optical axis.

Referring again to Figure 3, the crossed dichroic mirrors 34 and 36 intercept the beam composed of relatively collimated rays emerging from the tapered bar 50 and separate the beam into red, green and blue spectral components that enter the front aperture surfaces of the tapered collecting bars 52R, 52G and 52B, respectively. Being positioned in reverse with respect to the tapered bar 50, the bars 52R, 52G and 52B converge respective beams of incoming light rays into smaller cross-sectional areas at the smaller exit aperture surfaces of the bars. However, as seen in Figure 4B, the cross-sectional convergence of the beam is accompanied by an increased angular divergence of the rays as, in the example, the incoming ray D4 is diverted as emergent ray D5 having a greater angular



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divergence relative to the optical axis of the tapered bar. As in the case of the bar 50 - but now observed in reverse - this is due to internal reflections within the bars 52R, 52G and 52B relative to the taper half angles of the bars.

The photosensitive faces of the photocells 14R, 14G and 14B are preferably placed in either physical or optical contact with the exit aperture surfaces of bars 52R, 52G and 52B (with the trimming filters 40R, 40G and 40B positioned therebetween) to intercept the emergent beam. Because the green channel is substantially defined by the red and blue cutoffs of the mirrors 34 and 36, it has been found preferable to place a green transmitting dichroic filter 41G (see Figure 3) on or near the entrance face of the bar 52G where the light rays are substantially collimated. Such a dichroic filter possesses superior band edge cut off characteristics compared to the usual gelatin filter used for trim filters 40R, 40G and 40B. If dichroic trim filter 41G is used, then the trim filter 40G may be omitted.

The cross-sectional shape or configuration of the tapered bars may be related to the shape of the light originating or receiving elements at either end. If the transparency 12 and the dichroic mirrors 34 and 36 present rectangular surfaces to either end of the bar 50, then similarly the bar 50 may be provided with rectangular end faces. However the cross-sectional shape of the input or small end of the bar 50 could be elliptical, circular or elongated in some other manner depending upon the size and shape of the light-originating area of the transparency 12. The bars 52R, 52G and 52B may have large rectangular input ends to correspond to the surfaces of the dichroic mirrors 34 and 36 while



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having smaller output ends specially configured to correspond to the shapes of the photosensitive areas of the photocells 14R, 14G and 14B, e.g., a circular end to correspond to a circular photosensitive area. It therefore should be apparent that the respective shapes can be modified to suit a desired arrangement of elements. Moreover, the edge faces of the bars extending longitudinally with respect to the optical axes may be planar, i.e., forming angular corners therebetween, or may be smoothed into a conical form.

For optimum light efficiency, it is desirable to use an appropriately sized bar 50, especially regarding the cross-sectional area of its input end, for differently sized transparencies. This means that, for a given bar length and output cross-sectional area, the taper of the bar 50 increases as the size of the transparency decreases. Table I illustrates this relationship regarding the tapered bar 50 for three common film formats used as transparencies. It should be apparent that any similar film format can be accommodated. Also indicated in Table I are the collecting tapered bars 52R, 52G and 52B and their relative specific dichroic and phototube cross-sectional areas.

Table I

	<u>Bar</u>	<u>Format</u>	<u>Input Dimension</u>	<u>Length</u>	<u>Output Dimension</u>
30	50	135	28x40mm	285mm	62x78mm
	50	110	16x21mm	285mm	62x78mm
	50	16	9x11.5mm	285mm	62x78mm
35	52R, 52G, 52B		100x120mm	200mm	35x35mm



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A change from one transparency format to another may also involve the adjustment or replacement of the objective lens 30. Moreover, the increased taper for smaller transparency formats has the beneficial effect of improving the degree of collimation obtained for diffuse rays emerging from a scratched area of the transparency. However, the same benefit is obtained for any format by selecting an appropriate input-output dimensional relationship.

The cruciform arrangement of the dichroic mirrors 34 and 36 is helpful in reducing the size of the optical design. However other arrangements are equally possible with the invention. In another typical arrangement, the dichroic mirrors are spaced apart such that one color component is completely separated before the remaining portion of the beam encounters the next dichroic mirror. While the cruciform arrangement is preferred for compactness, the thickness of the glass at the intersection of the crossed dichroic mirrors forms an irregularity which can intercept and absorb or scatter light under certain conditions. Some rays from a specular scanning beam are attenuated when scanned across the irregularity and decrease the output signal corresponding to that area, causing band-like shading in the corresponding area of a copy made from the signal.

Moreover, under certain conditions the signals resulting from specular scanning of the corners of a rectangular transparency may be attenuated. It is believed that such attenuation is caused by light escaping from the longitudinal edges (especially if the edges are rounded) of the adjacent end face of the bar 50 near the entrance aperture when the specular scanning beam scans very



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close to the corners of the transparency and has an insufficiently small cone angle of divergence.

It was found that both of these sources of shading non-uniformity could be eliminated by placing a high gain lenticulated acetate diffuser over the entrance aperture of the bar as shown in Figure 5 to narrow the divergence of the emergent scanning beam. (The theory, design and fabrication of lenticulated light diffusers having controlled light spread is described by Gerhard Schwesinger in "Experiments with Lenticulated Rear Projection Screens," Photographic Engineering, pp. 172-181, vol. 5, No. 3, 1954.) The diffuser, having transmission of greater than 85%, was constructed by solvent embossing acetate with a master embossing cylinder to form a surface of small spherical lenticles. The master cylinder may be milled on a precision lathe to form spherical master lenticles having a pitch of 0.001 inch. The surface of an acetate sheet is then softened with acetone and pressed against the master embossing roller to form an image of the metal lenticles in the cylinder. The sheet is cut to proper size and fastened to the entrance aperture end of the bar. A goniophotometric analysis showed the maximum emergent light cone from the sheet due to a specular beam to sharply fall off at $\pm 5^\circ$ essentially lacking a tail component, an angular distribution found to be acceptable. It should also be acceptable to use a fiber optic faceplate having small fiber diameter of, e.g., 20-50 microns, in place of the lenticle-embossed acetate sheet.

It has been suggested that shading non-uniformity may be avoided by constructing the crossed dichroic mirrors so as to minimize the



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shading effect caused by the irregularity at the crossover. For example, in the previously cited article by P. M. van Alphen, a form of mirror construction is described in which the cruciform design is split into v-shaped halves joined at a knife edge. The cruciform half that first intercepts the scanning beam is made thicker than the other half. The refraction in the thicker mirrors displaces the beam so far laterally that no light falls on the knife-edge crossover surface and reportedly the shading problem is avoided.

In another embodiment of the invention illustrated in part in perspective in Figure 6, a two dimensional scan of the transparency 12 is effected by the combination of a lateral x-direction traverse of the scanning beam (line scan) and a vertical y-direction movement of the transparency. A flying spot on the faceplate 20 of the scanning tube 10 translates laterally back and forth in a path 70 in an x direction only. The spot is imaged by the objective lens 30 upon a horizontal line section 72 of the transparency 12. The y page scan of the transparency may be obtained in a number of ways. The film gate 11 (illustrated in Figure 3) may be adapted for precise movement in the page direction. More commonly, a number of transparencies may be joined together end-to-end in a web (e.g., transparencies 12-2, 12-3, etc.) and transported from an unwind reel 74 to a takeup reel 76 by suitable transport drivers 78 and 80. The light-collecting bar 50 may in this embodiment be reduced in entrance aperture cross section to capture light emerging and scattered only from the scan line 72. The design of Figure 6 is particularly adapted for scanning by means of a



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highly collimated pencil beam of electromagnetic radiation, such as produced by a laser. In the absence of scratches, such a pencil beam will enter the entrance face of the bar 50 on axis or at a small angle relative to the axis and emerge as a collimated beam at or near the design angle of the dichroic mirrors without reflecting off the walls of the tapered bar 50. Optimum color separation results. A scratch will scatter at least some of the light from the pencil beam, thus acting as a source of diffuse illumination that is re-collimated by internal reflection within the tapered bar 50, as discussed in connection with Figures 3, 4A and 4B. In practice a set of lasers will provide the necessary components of the color scanning beam, being formed into one composite scanning beam through a set of mirrors and a scanning prism.

While the preferred embodiment has been described in terms of three color scanning involving a beamsplitter, apparatus in accordance with the invention is fully realized as further indicated in Figure 7 by the combination of a scratch suppressing tapered bar 50 and a photocell 62 near the output aperture of the bar 50. Such an application is suggested where, e.g., a monochromatic beam 64 of light scans the transparent original 12, as in the black and white telecine projector illustrated in the previously cited U.K. patent specification 1409153, and the signal 64 derived from the photocell 62 is sufficiently represented by the monochromatic absorptions of the original 12. The beam 64 may be polychromatic but the photocell sensitivity will mainly depend on its own spectral sensitivity rather than the spectral selectivity of the absorptions in the original 12.



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A number of modifications and variations are possible depending on the level of performance desired (or obtained in practice) and the particular arrangement of scanner elements. For example, depending on the attained level of performance relative to the magnitude of the usual blemishes on the transparency, only one light-collecting bar 50 may be sufficient for several transparency formats. Furthermore, one could replace the beam-converging bars 52R, 52G and 52B of Figure 3 with the condenser lens 38R, 38G and 38B of Figure 1, thereby retaining much of the scratch suppression advantages of the embodiment of Figure 3 at the expense of larger photosensitive faces on the photocells 14R, 14G and 14B. In another modification, the length of the bars 52R, 52G and 52B could be reduced by placing condenser lens near or on the entrance apertures of the respective bars. Moreover, the taper of the bars 52R, 52G, and 52B may be optimized for minimum exit aperture depending on whether the respective photocells 14R, 14G and 14B are optically or physically coupled to the exit aperture ends of the bars.



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I claim:

1. Apparatus for scanning a transparent original with a light beam relative to an optical axis and for collecting the portion of the beam transmitted through said original wherein the direction of the light beam rays emerging from respective areas of the original varies with respect to the optical axis, said apparatus comprising:

means (10) for generating a light beam;

means (11) for supporting the transparent original in the path of the beam;

means (26) for scanning the beam across at least one dimension of the transparent original; characterized in that a tapered optical element (50) is positioned on the optical axis, said element having differently sized apertures at opposite ends thereof and a tapered reflecting surface therebetween; the optical element being positioned with its smaller aperture adjacent said transparent original to collect the light beam rays emerging from said transparent original and its tapered surface oriented to internally reflect at least some of the light beam rays toward the larger aperture such that the direction of the rays emerging from the larger aperture vary less with respect to the optical axis than the directions of the rays emerging from the transparent original.

2. Apparatus according to claim 1 characterized in that said tapered optical element comprises a tapered bar having a ratio of at least 2:1 between its larger and smaller apertures as measured relative to said at least one scanned dimension of the transparent original.

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3. Apparatus according to claim 1
characterized in that said transparent original
contains light-scattering blemishes on the surface
thereof and said tapered optical element (50) is
5 positioned adjacent said transparent original to
collect both scattered and unscattered light rays
whereby the scattered rays are redirected more nearly
in parallel with the unscattered rays.

4. Apparatus according to claim 1 or 3
10 characterized in that a polychromatic light beam is
generated by said light generating means (10) and a
beam splitter (16) for separating the polychromatic
emerging beam into a plurality of spectral component
rays is positioned adjacent the larger aperture of
15 optical element (50).

5. Apparatus according to claim 1 or 3
characterized in that said light generating means
(10) includes means for sweeping the light beam
across the lateral dimension of a moving transparent
20 original.

6. Apparatus according to claim 1 or 3
characterized in that a high gain diffuser (60) is
positioned adjacent the small aperture of optical
element (50) and a condenser lens (54) is formed on
25 the larger aperture to reduce divergence of the light
beam relative the optical axis.



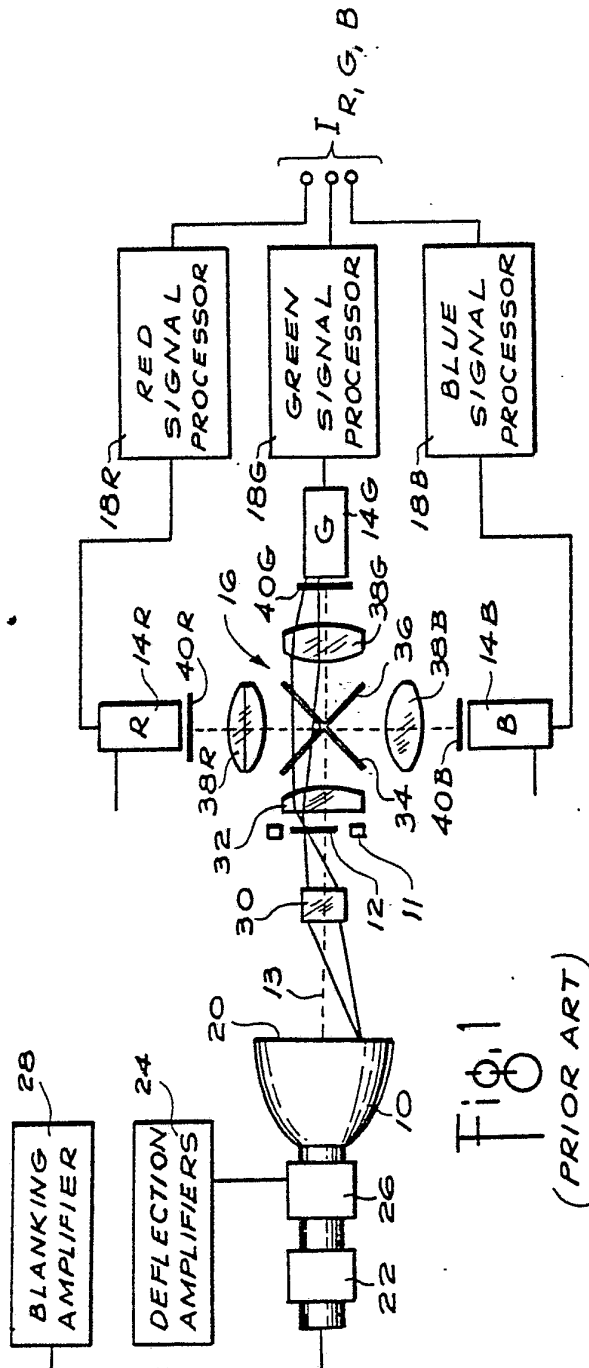


Fig. 1
(PRIOR ART)

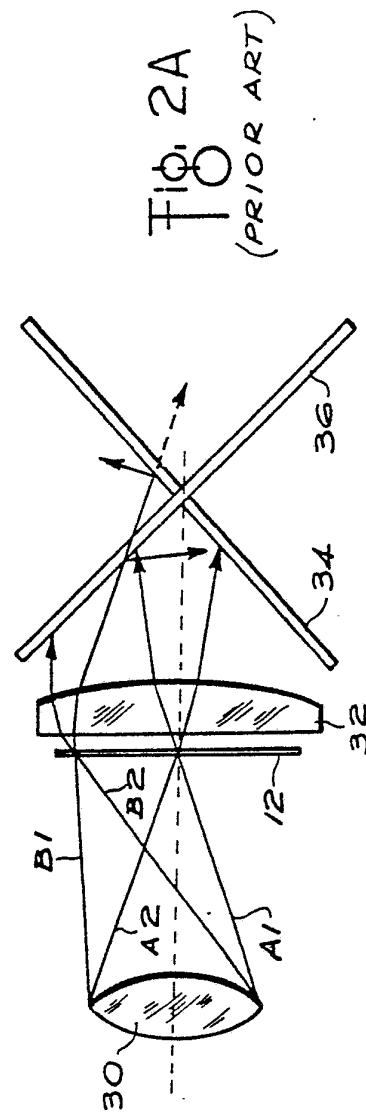
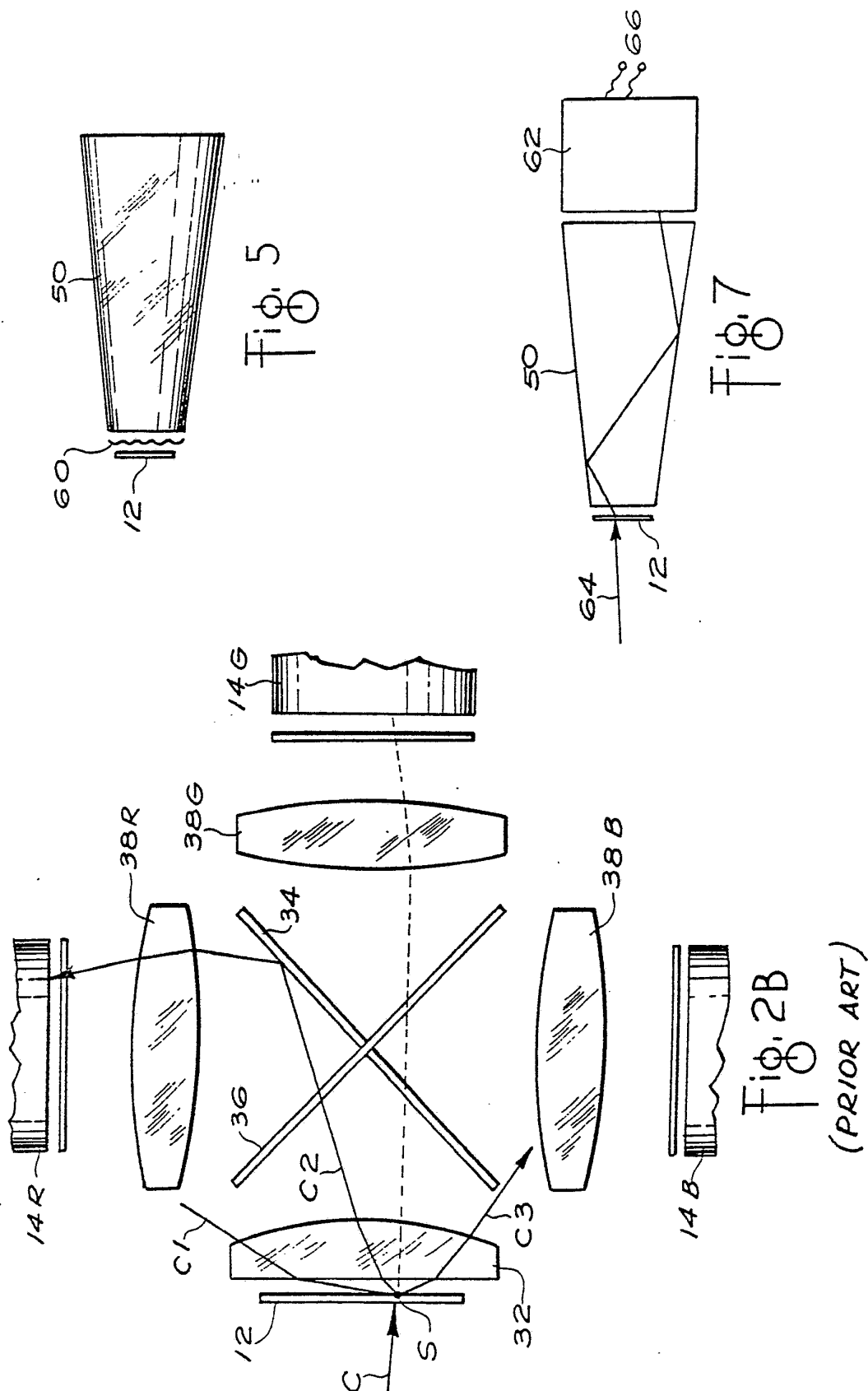
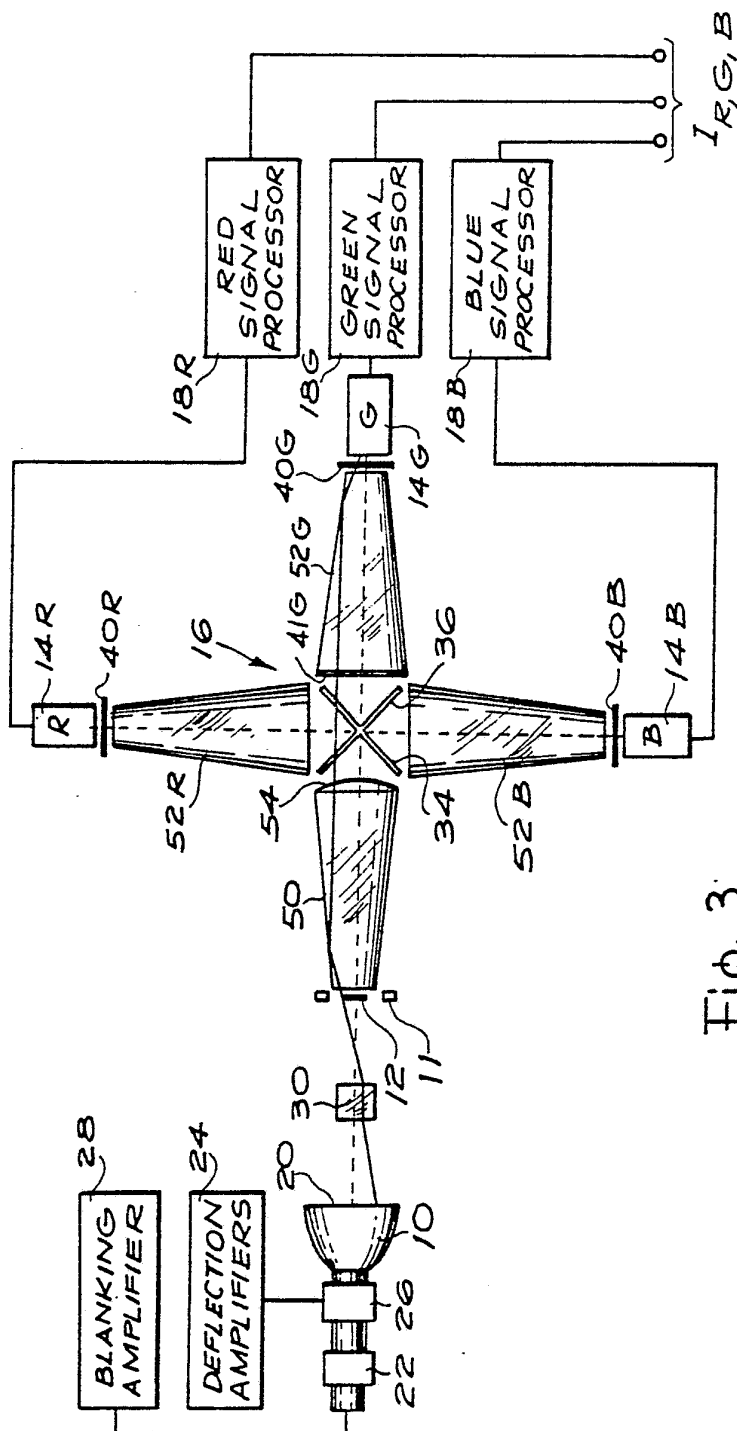


Fig. 2A
(PRIOR ART)

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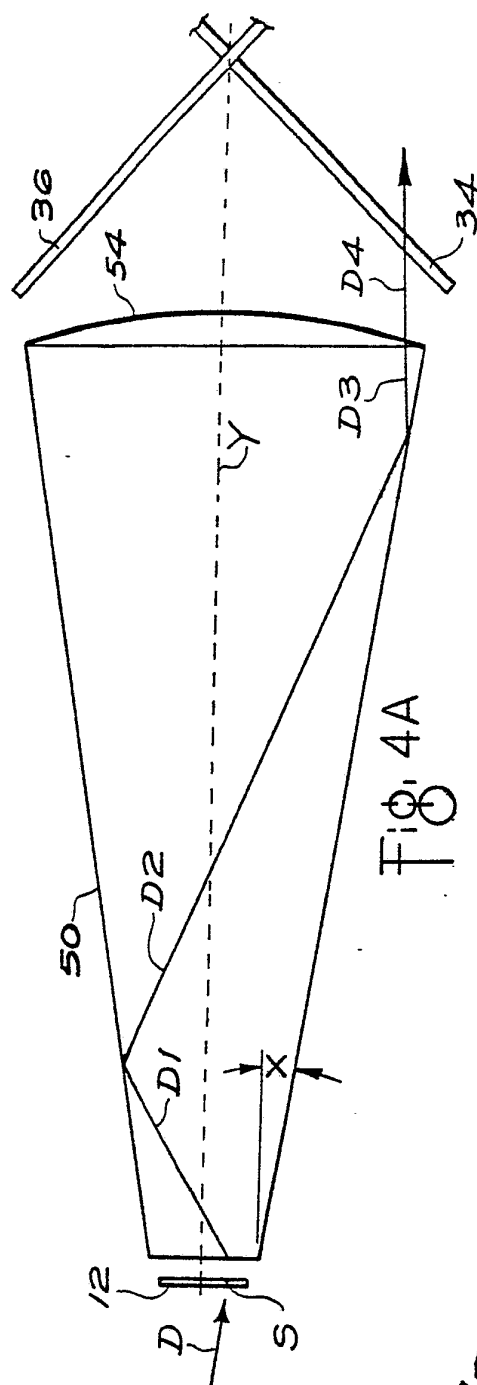
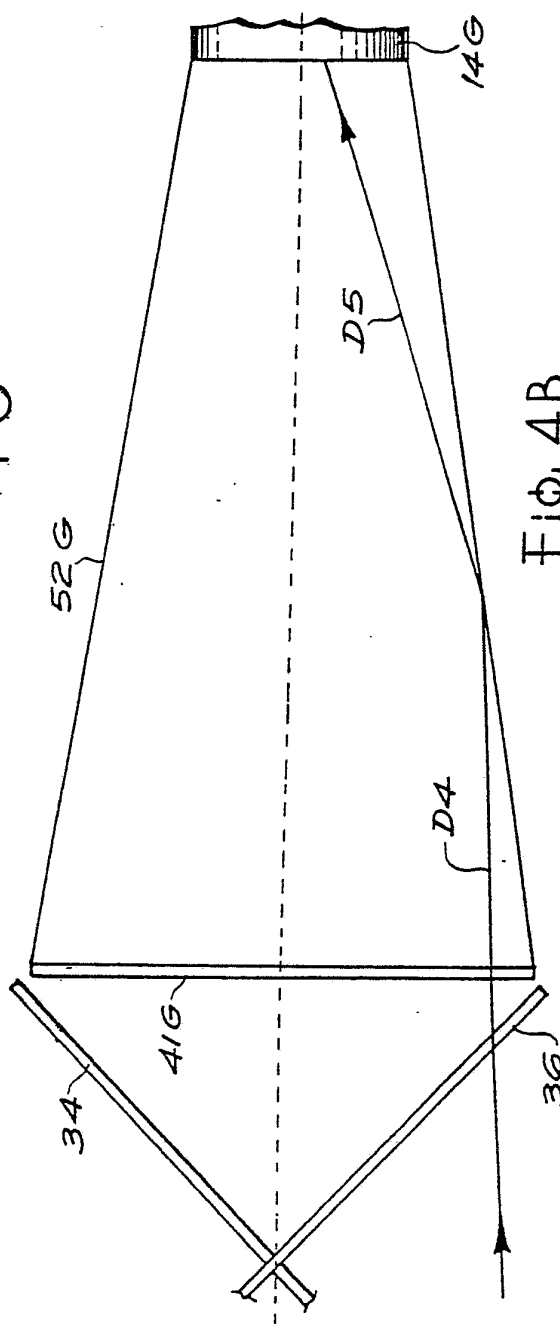
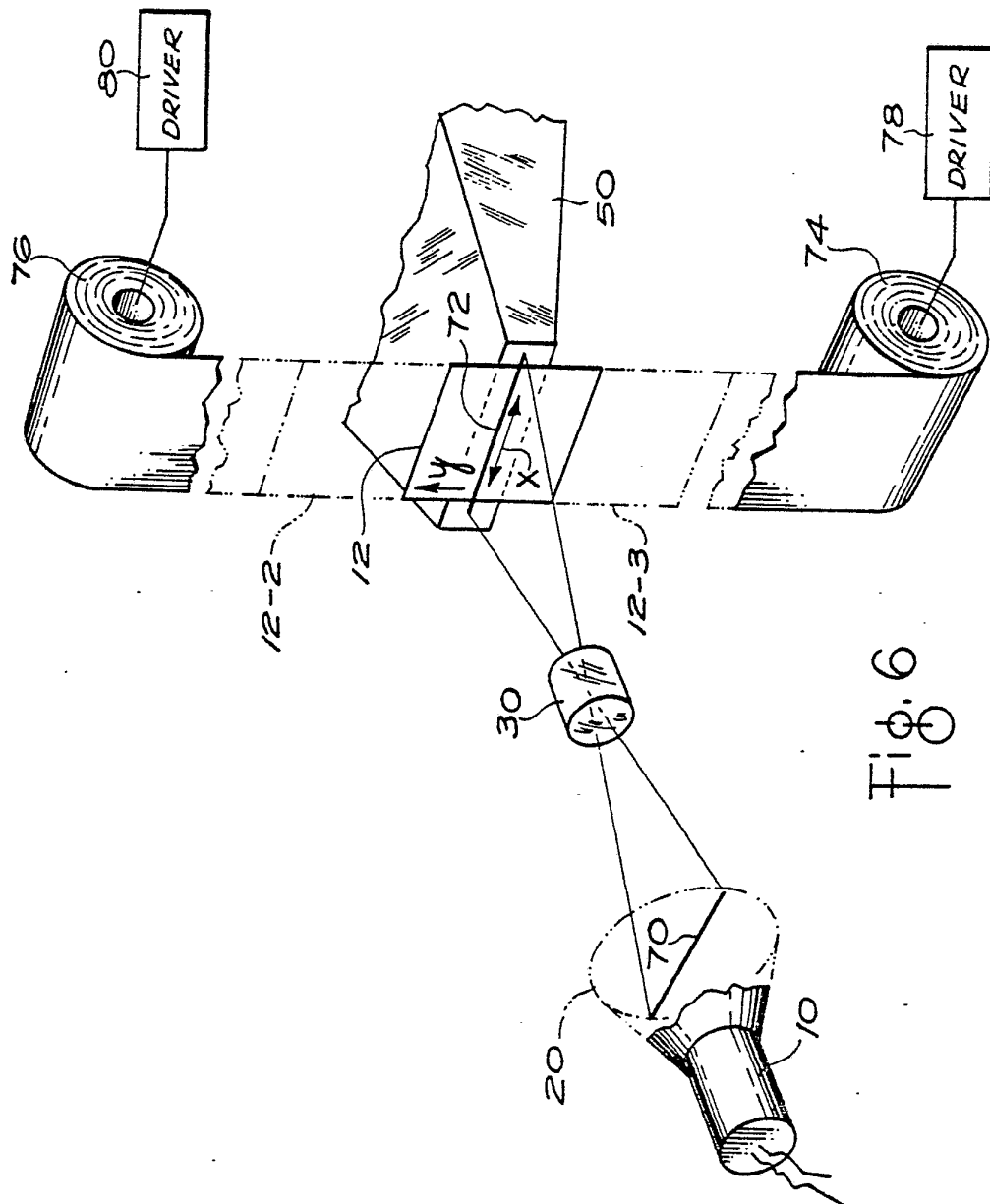


Fig. 4A



4B

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INTERNATIONAL SEARCH REPORT

International Application No PCT/US 83/00149

I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) ³ According to International Patent Classification (IPC) or to both National Classification and IPC IPC ³ : H 04 N 1/46; H 04 N 9/11						
II. FIELDS SEARCHED <div style="text-align: center; border-top: 1px solid black; border-bottom: 1px solid black; margin: 5px 0;">Minimum Documentation Searched ⁴</div> <table style="width: 100%; border-collapse: collapse;"> <tr> <th style="width: 20%; border-bottom: 1px solid black;">Classification System</th> <th style="border-bottom: 1px solid black;">Classification Symbols</th> </tr> <tr> <td style="border: 1px solid black; padding: 10px; vertical-align: top;">IPC³</td> <td style="border: 1px solid black; padding: 10px; text-align: center;">H 04 N; G 01 J 1/00</td> </tr> </table> <div style="text-align: center; border-top: 1px solid black; border-bottom: 1px solid black; margin: 5px 0;">Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched ⁵</div>			Classification System	Classification Symbols	IPC ³	H 04 N; G 01 J 1/00
Classification System	Classification Symbols					
IPC ³	H 04 N; G 01 J 1/00					
III. DOCUMENTS CONSIDERED TO BE RELEVANT ¹⁴						
Category [*]	Citation of Document, ¹⁶ with indication, where appropriate, of the relevant passages ¹⁷	Relevant to Claim No. ¹⁸				
Y	DE, A, 1816189 (PRINTING DEVELOPMENTS INTERNATIONAL) 14 August 1969 see page 10, line 11 - page 11, paragraph 3 --	1-6				
Y	US, A, 4225782 (KUPPENHEIMER) 30 September 1980 see column 2, line 36 - column 4, line 9 --	1-6				
Y	GB, A, 1409153 (B.B.C.) 8 October 1975 see page 1, line 81 - page 2, line 38, (cited in the application) --	3				
Y	US, A, 3624286 (BOSOMWORTH) 30 November 1971 see column 4, lines 37-70 --	4				
Y	DE, A, 2001019 (ELTRO) 15 July 1971 see page 2, line 1 - page 3, line 8 --	5 ./.				
<div style="display: flex; justify-content: space-between;"> <div style="width: 45%;"> <p>[*] Special categories of cited documents: ¹⁵</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> </div> <div style="width: 45%;"> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"Z" document member of the same patent family</p> </div> </div>						
IV. CERTIFICATION						
Date of the Actual Completion of the International Search ¹ <div style="text-align: center; font-size: 1.2em;">10th June 1983</div>		Date of Mailing of this International Search Report ² <div style="text-align: center; font-size: 1.2em;">28 JUIN 1983</div>				
International Searching Authority ¹ <div style="text-align: center; font-weight: bold;">EUROPEAN PATENT OFFICE</div>		Signature of Authorized Officer ²⁰ <div style="text-align: right;"> G.L.M. Kruidenberg </div>				

III. DOCUMENTS CONSIDERED TO BE RELEVANT (CONTINUED FROM THE SECOND SHEET)		
Category *	Citation of Document, ¹⁶ with indication, where appropriate, of the relevant passages ¹⁷	Relevant to Claim No ¹⁸
Y	<p>IBM Technical Disclosure Bulletin, vol. 17, no. 3, August 1974 (New York, US) D.H. Cronquist: "Hollow reflecting light collector tube", pages 906-908, see page 906, line 1 - page 907, line 10</p> <p style="text-align: center;">--</p>	5
Y	<p>Proceedings of the Society of Photo-Optical Instrumentation Engineers, vol. 31, 1972; S.E. Glazer: "Taper measurement techniques", pages 13-22 see page 14, left-hand column, lines 9-35; page 14, right-hand column, line 18 - page 15, right-hand column, line 34; page 18, left-hand column, line 5 - page 19, left-hand column, line 27 (cited in the application)</p> <p style="text-align: center;">-----</p>	6

ANNEX TO THE INTERNATIONAL SEARCH REPORT ON

INTERNATIONAL APPLICATION NO. PCT/US 83/00149 (SA 4836)

This Annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report. The members are as contained in the European Patent Office EDP file on 21/06/83

The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
DE-A- 1816189	14/08/69	NL-A- 6818441	24/06/69
		GB-A- 1234966	09/06/71
		US-A- 3585281	15/06/71
US-A- 4225782	30/09/80	None	
GB-A- 1409153	08/10/75	None	
US-A- 3624286	30/11/71	None	
DE-A- 2001019	15/07/71	None	

For more details about this annex :
see Official Journal of the European Patent Office, No. 12/82