

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
12 June 2008 (12.06.2008)

PCT

(10) International Publication Number
WO 2008/068705 A1

(51) International Patent Classification:
H05B 33/08 (2006.01)

(21) International Application Number:
PCT/IB2007/054895

(22) International Filing Date:
3 December 2007 (03.12.2007)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:
06125476.9 6 December 2006 (06.12.2006) EP

(71) Applicant (for all designated States except US): **NXP B.V.**
[NL/NL]; High Tech Campus 60, NL-5656 AG Eindhoven (NL).

(72) Inventors; and

(75) Inventors/Applicants (for US only): **HOOGZAAD, Gian**
[NL/NL]; c/o NXP Semiconductors, IP Department, HTC 60 1.31 Prof Holstlaan 4, NL-5656 AG Eindhoven (NL). **MOBERS, Antonius, M., G.** [NL/NL]; c/o NXP Semiconductors, IP Department, HTC 60 1.31 Prof Holstlaan 4, NL-5656 AG Eindhoven (NL).

(74) Agent: **PENNINGS, Johannes, F., M.**; c/o NXP Semiconductors, IP Department, HTC 60 1.31 Prof Holstlaan 4, NL-5656 AG Eindhoven, (NL).

(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BH, BR, BW, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KN, KP, KR, KZ, LA, LC, LK, LR, LS, LT, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RS, RU, SC, SD, SE, SG, SK, SL, SM, SV, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IS, IT, LT, LU, LV, MC, MT, NL, PL, PT, RO, SE, SI, SK, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

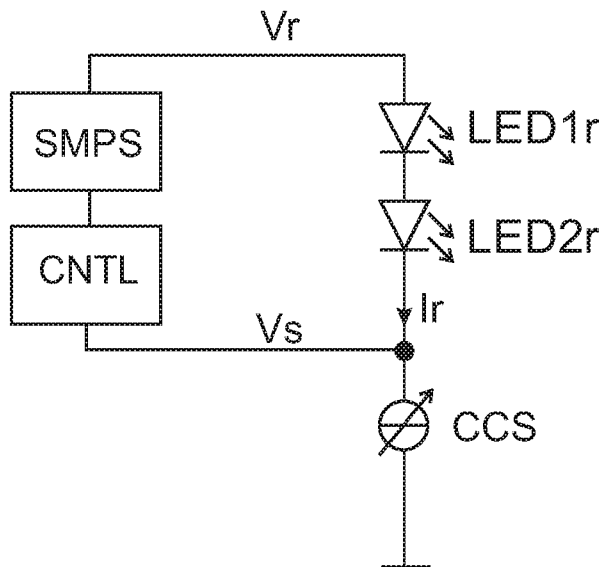
Declaration under Rule 4.17:

— as to applicant's entitlement to apply for and be granted a patent (Rule 4.17(ii))

Published:

— with international search report
— before the expiration of the time limit for amending the claims and to be republished in the event of receipt of amendments

(54) Title: CONTROLLED VOLTAGE SOURCE FOR LED DRIVERS



(57) Abstract: The present invention relates to an electronic device for driving a light emitting semiconductor device, which includes controlling means (CNTL) being adapted for controlling a switch mode power supply for supplying the light emitting semiconductor device in response to a sensing value received by the controlling means which is indicative of a voltage across a current source for determining a current through the light emitting semiconductor device, wherein the switch-mode power supply is controlled such that the voltage across the current source is minimum.

WO 2008/068705 A1

CONTROLLED VOLTAGE SOURCE FOR LED DRIVERS

FIELD OF THE INVENTION

The present invention relates to an electronic device for driving a light emitting diode, more specifically to a control mechanism for an electronic device for driving a light emitting diode. The invention further relates to a system comprising the electronic
5 device and the light emitting diodes, and a method of driving the diodes.

BACKGROUND OF THE INVENTION

Light emitting diodes are to be driven at a constant current. Linear current sources are broadly used for this purpose, as they are cheap and highly accurate. Further, the
10 linear current sources can be switched on and off quickly, a characteristic being advantageous for implementing pulse width modulation (PWM) dimming. Amplitude modulation (AM) dimming is also easy to implement by linear current sources, wherein different current levels or current digital-to-analog converters are used. Typically, linear current sources are used in one dimensional (1D) and two dimensional (2D) dimmable backlight systems, since many
15 independent current sources are required in those applications. Another approach consists in switch-mode solutions, which is, however, more expensive, but less power consuming. Linear current sources used for driving LED strings have only limited power efficiency, which is mainly due to voltage variations of the LEDs. These voltage variations find their origin in temperature dependence, spread, and aging. If a fixed voltage supply is used for
20 driving the light emitting diodes of a string, the current sources being coupled in series to the LED strings may experience a large voltage. The large voltage entails a large power dissipation, which in turn requires the current sources to be suitable to withstand high temperatures. Accordingly, design considerations are to be made, which result in more devices and packages in parallel, additional heat sinking mechanisms, and generally, in a
25 substantial increase in costs.

SUMMARY OF THE INVENTION

It is an object of the present invention to reduce the power consumption due to voltage variations of the light emitting semiconductor device.

According to a first aspect of the present invention, an electronic device for driving a light emitting semiconductor device is provided which includes controlling means adapted for controlling a switch mode power supply for supplying the light emitting semiconductor device in response to a sensing value received by the controlling means which is indicative of a voltage across a current source for determining a current through the light emitting semiconductor device, wherein the switch-mode power supply is controlled such that the voltage across the current source is minimum. Although the following description relates mainly to light emitting diodes as light emitting semiconductor devices, the present invention covers all kinds of light emitting semiconductor devices, which may be driven by the same or similar mechanisms as described here below. According to this aspect of the present invention the electronic device provides means to control a switch-mode power supply in response to the voltage across a current source that is e.g. coupled in series to the light emitting diode. Accordingly, the control mechanisms of power supply and current source are coupled to each other such that the power supply is adjusted in accordance with the voltage drop across the current source. If current source and voltage supply were controlled independently as provided by prior art solutions, the current through an LED is held constant by the current source as long as the light emitted by the LED satisfies the specific requirements as brightness or color. However, if the forward voltage across the LED, or even worse across a string of LEDs, varies during operation, the supply voltage provided by the controlled power supply may be higher than necessary. Any additional voltage drop across the current source produces undesirable power losses by way of heat. This aspect of the present invention takes account of this problem by providing a control mechanism that reduces (or increases) the supply voltage such that the voltage across the current source remains at a minimum voltage being just necessary to assure proper operation without producing any excess voltage across the current source, which would be turned into heat. The current source may be implemented as a linear or a switched current source being preferably controllable to provide an appropriate current through a single or through multiple LEDs. A current source in the present context, is to be understood as encompassing current sources or current sinks. The current source may be implemented by a current mirror, wherein one transistor is coupled in series with one or more light emitting diodes (e.g. a string of diodes). As the current source (or current sink) is dimensioned and biased for a specific current, any deviation from the predetermined value for the current will cause significant variations in the voltage across the transistor. The control mechanism according to the present invention allows to control the output voltage (and/or current) of the switch-mode power supply (such

as switch-mode power converter as buck- buck-boost or boost converter) in accordance with a minimum voltage drop across the current source. The minimum voltage drop is the voltage that is required to operate the current source, as for example a current mirror, in saturation.

To provide an appropriate sensing value that is indicative of the voltage drop across the current source, the voltage level at the input of the current source (or sink) may be measured. The so determined value may then be compared to a reference value, which is the minimum value of the voltage drop across the current mirror. Any deviation from the reference value may then be used to control the switch-mode power converter to re-establish the minimum value. However, as apparent for those skilled in the art, the sensing value may be another voltage or current that is suitable to indicate the voltage across the current source.

According to another aspect of the present invention, the electronic device as set out above, includes further the current source, wherein the current source is either a switched current source or a linear current source. The present invention is basically applicable to all kinds of current sources. It is therefore irrelevant whether or not the current source, or at least those components of the current source, which are coupled to the LED, are implemented according to switch mode principles or linear driving mechanisms. As the current source represents a component with a theoretically infinite impedance, the voltage across the current source will take any value necessary to maintain a specific current. If the supply voltage for the LEDs is increased, this may cause additional voltage across the current source, at least across those parts of the current source which are coupled with the LEDs. The present invention overcomes these problems by regulating the supply voltage in relation to the voltage drop.

According to an aspect of the present invention, the electronic device is adapted to switch the current through the LEDs on and off. The switching may in particular occur in response to a pulse width modulated signal. This aspect relates to control mechanisms using rapid pulse width modulated (PWM) signals for controlling the light emission of LEDs. According to this aspect of the invention it is provided that the switching activity of the current through the LEDs is in accordance with the control mechanism according to the above aspects of the present invention. Instead, the control means take account of the switching sequence and adapts the control appropriately in order to avoid any conflict.

According to another aspect of the present invention, the controlling means is further adapted to control the timing of a sample switch for sampling the sensing value, which is indicative of the voltage across the current source, such that the sensing value is

sampled in accordance with the timing of switching of the current through the current source. In particular, the sensing value is sampled if the current through the current source is switched on. As switch-mode power converters must be switched according to a specific timing in order to provide an appropriate output voltage, it is necessary to consider this
5 timing for the mechanism of retrieving the sensing value.

According to still another aspect of the present invention the switch-mode power supply and the controlling means are adapted to control the output voltage of the switch-mode power supply with a resolution or control accuracy of less than the variation of the forward voltage of the light emitting diode to be driven. According to this aspect of the
10 invention, the control mechanism, and the switch-mode power supply provide a specific control accuracy, such that the variations of the forward voltage of the light emitting diodes are compensated. If a plurality of light emitting diodes is coupled in a string, this aspect of the present invention relates to the total added variation of the forward voltages of the string. If, for example, a single light emitting diode has a forward voltage variation of several
15 millivolts, this comparatively small value can add up, if multiple LEDs are coupled in series. In this situation, the control range and accuracy take account of the overall variation as well as the smallest possible variation. Generally, the switch-mode power supply, or parts of it may be integrated on the same substrate as the control mechanism described here above with respect to the other aspects of the present invention.

According to another aspect of the invention, the electronic device is further adapted to provide pulse width modulation (PWM) signals for a plurality of strings of light emitting diodes for individually dimming of each of the strings. This aspect of the present invention relates to some typical applications, where a plurality of light emitting diodes is coupled to form a string. The electronic device according to this aspect of the invention is
25 adapted such that these strings may be dimmed individually. This requires that the timing of the control mechanism takes account of the control mechanism described here above.

According to still another aspect of the present invention a plurality of current sources and a minimum selector is provided, wherein the plurality of light emitting diodes (or as mentioned above a plurality of light emitting semiconductor devices) is coupled to the
30 plurality of current sources and the minimum selector is adapted to select the minimum voltage across the plurality of current sources, wherein the selected minimum voltage is used as a reference for controlling the switch-mode power supply. Accordingly, even if a plurality of light emitting diodes, as for example three strings of light emitting diodes are driven by the present electronic device, a mechanism is provided that allows to detect a current source with

a minimum voltage drop and to control all strings by the minimum voltage. This reduces complexity of the required circuits.

According to an aspect of the present invention, the control unit is electrically decoupled from the light emitting semiconductor devices (such as light emitting diodes), in particular by an inductive power converter or by an opto-coupler or by both. Accordingly, the present invention relates also to configurations, where the control unit, but also the switched mode power supply is decoupled by means of transformers, opto-couplers, or the like from the light emitting diodes.

According to an aspect of the present invention, an integrated semiconductor device is provided being arranged according to one or several aspects of the present invention, as set out here above. In particular, a integrated semiconductor device according to present invention may provide input and output pins to provide the functionality in accordance with the present invention. According to one aspect of the invention, a integrated semiconductor device, as for example a packaged chip, provides an input pin being configured to receive a sensing value to provide the control functions as described above. The above aspects of the present invention may be combined in any number or configuration.

BRIEF DESCRIPTION OF THE DRAWINGS

These and other aspects of the invention will be apparent from and elucidated with reference to the embodiments described hereinafter. In the following drawings

Fig. 1 shows a simplified schematic of a conventional circuitry for driving LEDs of a single string,

Fig. 2 shows a simplified schematic of a conventional circuitry for driving LED strings of three different colors,

Fig. 3 shows a simplified schematic of a first embodiment of the present invention

Fig. 4 shows a simplified schematic of a second embodiment of the present invention,

Fig. 5 shows a simplified schematic of a third embodiment of the present invention,

Fig. 6 shows a simplified schematic of a fourth embodiment of the present invention,

Fig. 7 shows a simplified schematic of a fifth embodiment of the present invention,

Fig. 8 shows a simplified schematic of a conventional circuitry for driving multiple LED strings by one voltage source,

Fig. 9 shows a simplified schematic of a sixth embodiment of the present invention, and

5 Fig. 10 shows a simplified schematic of a seventh embodiment of the present invention.

DETAILED DESCRIPTION OF EMBODIMENTS

Fig. 1 shows a simplified schematic of a conventional driver circuit for driving
10 two light emitting diodes LED1r, LED2r, as light emitting semiconductor devices. A constant voltage source V_r is coupled to the string of LEDs to supply a current through the LEDs. The appropriate current through the LEDs is determined by the current mirror (used as a current sink in this example) consisting of transistors T_r and $T'r$. The current mirror is biased by the bias current source with a current I_r . The dimming of the string of LEDs is implemented by
15 pulse width modulated switching of the transistor M_r by a signal PWM_r at the gate of transistor M_r . If M_r is turned on, the current mirror of T_r , $T'r$ mirrors the current I_r into the string of LED1r, LED2r. The resistors R_r and $R'r$ are provided for biasing and stabilizing the current mirror. If the voltage drop across the diodes LED1r and LED2r varies due to temperature, aging, or production spread the voltage drop across the current mirror, in
20 particular across transistor $T'r$ changes, too. Accordingly, instead of being driven at the edge of saturation, i.e. at the minimum voltage, the transistor $T'r$ experiences a greater voltage drop. The consequence is greater power consumption of the current mirror than necessary.

Fig. 2 shows a simplified schematic of a conventional circuit for driving LED strings of different color. There are three similar circuits, a first circuit including two red light emitting diodes LED1r, LED2r, a second circuit including two green light emitting diodes
25 LED1g, LED2g, and a third circuit including one blue light emitting diode LED1b. Throughout this application, the number of LEDs in a string is to be understood as being variable, such that a smaller or greater number of LEDs may form a string. There is further a bias current source I_r , I_g , I_b for each of the three circuits and a constant voltage source V_r ,
30 V_g , and V_b . The LEDs are coupled to a current mirror consisting of transistors T_r , $T'r$, T_g , $T'g$, and T_b , $T'b$. The bias current sources I_r , I_g , I_b are coupled via MOSFETs M_r , M_g , M_b to the current mirrors. The MOS transistors are individually controlled by pulse width modulated signals PWM_r , PWM_g , PWM_b in order to define the luminance of each of the

strings. Typically, the current mirrors provide a specific gain, which allows to reduce the current in the input branch provided by the bias current sources I_r , I_g , I_b ,

Fig. 3 shows a simplified schematic of a first embodiment of the present invention. The string of LED1r and LED2r is coupled to a switch-mode power supply SMPS and a control unit CNTL. The voltage drop across the controlled current source CCS is sensed and a value V_s , which is indicative of the voltage drop is supplied to the control unit CNTL. The controlled current source CCS may be implemented by a linear or by a switched mode current source. An example for a switched mode implementation is shown in Fig. 6 and will be described here below. However, the controlled current source CCS may be configured to receive a pulse width modulating signal PWM in order to switch the current through the light emitting diodes LED1r, LED2r on and off. This mechanism is used to control the properties of the light emission, such as luminance and color of the LEDs. The control unit CNTL transmits signals to the switch-mode power supply SMPS to control the output voltage V_r . If the voltage drop V_s across CCS is too high the voltage V_r is reduced. If the voltage drop is too small the voltage V_r is increased.

Fig. 4 shows a simplified schematic of an embodiment of an aspect of the present invention. Fig. 4 shows in particular a configuration according to an aspect of the present invention, where the switch mode power supply SMPS and the control unit CNTL are coupled to the LEDs LED1r, LED2r via a transformer T_r . The transformer T_r decouples the light emitting diodes LED1r, LED2r from the power supply. The secondary side of the transformer is, just as an example, coupled to a diode D_r and a capacitor C for rectifying or smoothing the output voltage V_r . The output voltage V_r is finally supplied to the LEDs LED1r, LED2r. The controlled current source CCS provides a current I_r through the LEDs LED1r, LED2r. The voltage drop across the controlled current source CCS is indicated by V_s . The voltage V_s is applied to a light emitting diode being part of an optocoupler OC. The optocoupler OC transmits the sensing voltage V_s , i.e. a corresponding value, which is indicative of the voltage drop across the controlled current source CCS to the control unit CNTL. As apparent from Fig. 4, the driving mechanism and the control mechanism disclosed with respect to various aspects of the present invention may all be implemented by use of a decoupling (or isolating) mechanism as shown in present Fig. 4. Decoupling (or isolating) as shown in Fig. 4 might be particularly useful for numerous applications.

Fig. 5 shows a simplified schematic of a second embodiment of the present invention. The basic control mechanism of the circuit shown in Fig. 5 is similar to the mechanism described with respect to Fig. 3. However, the components are now depicted in

more detail. Accordingly, there is a sampler S_r to sample the voltage V_r at the collector of transistor T . The voltage level at the collector is supplied to an amplifier A to compare the sampled voltage level with a predefined voltage level V_{sat} . The output signal of the amplifier is coupled to a control unit SMC being adapted to control the switch mode of the switch mode power converter that generates V_r from an input voltage V_{in} . The switch mode supply voltage is controlled such that the measured output voltage of the current source corresponds to a reference value that is equal to a minimum value V_{sat} . At V_{sat} the linear current source is - including a specific margin - at its edge of saturation. The sampler S_r is switched synchronously to the PWM signal. Accordingly, the sampler S_r is in a locked state, such that the control loop is open and the duty cycle of the switch mode converter is fixed to supply a constant V_r . If the analog settle times are small enough to recover from the switching, the sampler can be implemented in the switch-mode controller by fixing the duty cycle. The advantage of having the sampler immediately at the output node of the current source resides in the minimal amount of nodes in the circuits to be driven to their limits for the off state of the current source. It is also possible to control the output voltage of the current source to the same level as the input voltage of the mirror. This provides an improved thermal matching of the power components, and therefore in an enhanced current mirror accuracy in case the mirror has a current gain of 1.

Fig. 6 shows a simplified schematic of an aspect of the present invention. This aspect of the present invention provides a switch mode current source for controlling the current through the LEDs LED_{1r} , LED_{2r} . The current source includes an inductor L_r , a fly back diode D_r as well as a control switch transistor M_r and a resistor R_r . In response to the control and dimming signal $PWM/Control$, the MOSFET transistor M_r switches the current on and off, thereby controlling the voltage V_r and the current through the LEDs. Fig. 6 shows a self-oscillating buck converter. During the primary stroke, i.e. while the current through inductor L_r increases, the switch M_r is conducting. Upon detection of the peak-current, the switch M_r is turned off. During the secondary stroke, a decreasing current flows through inductor L_r , while the current is circulating via diode D_r , and LEDs LED_{1r} , LED_{2r} . When the current through the coil L_r is sensed to be zero, the switch transistor M_r is turned on. A current of zero is detected by measuring either the current through the coil L_r or the voltage at the LED string side of the coil, where a swap of polarity relative to an input voltage can be detected. Another approach is to measure the voltage at the output of control switch transistor M_r known as valley detection. The sensing voltage V_s , which is indicative of the voltage across control switch M_r , the coil L_r , and sensing resistor R_r is measured between L_r and the

light emitting diode LED2r. The different aspects of the present invention as explained throughout the present description are all susceptible to the switch mode current source as shown in Fig. 6. The switching mechanism of the switch Mr must take account of the timing of the control mechanism and vice versa. According to the circuit shown in Fig. 6, the supply voltage Vr is adapted such that the voltage across the string of LEDs LEDstr comes close to Vr, which means in different words that the difference between Vr and the voltage across the string of light emitting diodes LEDstr, i.e. the voltage across Lr, Mr, and Rr is controlled to be closer to zero, only satisfying the minimum requirements for proper operation. In fact, The advantage of minimizing the voltage across the "current source", i.e. the respective parts thereof, for a switched-mode converter is that smaller inductors Lr can be used, which provides a cost benefit.

Fig. 7 shows a simplified schematic of a third embodiment of the present invention. According to Fig. 7, the circuit shown in Fig. 5 is applied to LEDs of different colors, as red, green and blue (RGB). This configuration is useful to provide different colors by the respective RGB values. Accordingly, the currents Ir, Ig, Ib are mirrored via current mirrors T, T' to supply the strings of LED1r, LED2r, LED1g, LED2g and LED1b. The dimming of the strings is achieved by the respective pulse width modulating signals PWMr, PWMg and PWMb per string. Each string has its own sampling switch Sr, Sg, and Sb and sampling capacitor Cs to provide the respective sensing value at an appropriate point of time for the control mechanism according to the present invention. Vr, Vg, and Vb are the respective supply voltages for each of the strings. The capacitors C and inductors L complete each of the switch mode power supplies per string. The strings have different configurations (numbers of LEDs, electrical characteristics etc.) and each string has its own saturation voltage value Vsatr, Vsatg, Vsatb. According, to the present invention the voltages Vr, Vg and Vb are controlled such that the voltage across the current sources (current mirrors) becomes minimum.

Fig. 8 shows a simplified schematic of a conventional circuit for driving multiple LED strings by a single voltage supply. Accordingly, there is a constant voltage Vr being applied to the strings consisting of LED11 to LED1n, LED21 to LED2n, and LED31 to LED3n. Current source Ir supplies a current to transistor T1, which is supplied to switching transistors Ts1, Ts2, and Ts3. PWM1 to PWM3 are to perform the dimming of the strings.

Fig. 9 shows a simplified schematic of a fourth embodiment of the present invention. Accordingly, in addition to the circuitry shown in Fig. 8, there is the error amplifier A, the control unit SMC and the switch-mode power supply including voltage

source V_{in} , inductor L and capacitor C . Further, a minimum selector MINSEL is provided, which supplies a minimum signal to the amplifier A to compare the output signal of MINSEL with a minimum saturation voltage V_{sat} , and to supply the resulting signal to the switch mode controller SMC. SMC is provided to control the switch mode power converter. The
5 shown configuration implements a power converter in order to provide a voltage V_r to the multiple strings of LEDs. Controlling V_r according to the current source saturation criterion is now based on the minimum value that appears on the current source outputs being connected to V_r . The current source output voltages V_{OUT1} , V_{OUT2} , and V_{OUT3} differ due to different LED string temperatures, zero-hour forward-voltage spread and ageing.
10 Accordingly, the voltage V_r is controlled by the switch mode controller SMC such that the minimum output voltage, i.e. the minimum of V_{OUT1} , V_{OUT2} , and V_{OUT3} becomes close or equal to V_{sat} .

Fig. 10 shows a simplified schematic of a fifth embodiment of the present invention. The circuit shown in Fig. 10 implements basically the functions of the circuit
15 shown in Fig. 9. Fig. 10 shows the minimum selector in more detail. The configuration includes a voltage converter in order to provide a supply voltage V_r , which is controlled by a switch mode controlled current source. V_r is adjusted such that the minimum output voltage V_{OUT1} , V_{OUT2} , V_{OUT3} is controlled to equal V_{sat} . V_{sat} is adjusted by a current source I_{ref} passing a current through the transistor T_{ref} and the resistor R_{sat} . The sampler S_r
20 samples the voltage on the common PNP line being coupled to the emitters of PNP transistors T_6 , T_7 , and T_8 . Transistors T_3 , T_4 , and T_5 are used as before in order to switch the current according to a pulse width modulated signal PWM. The wired-OR PNP line serves as a minimum selector. The common source of the PNP line is compared to V_{sat} in the amplifier A . V_{sat} is generated by matched currents I_{ref} and I_{bias} , matched PNP transistors
25 and a matched resistor R_{sat} corresponding to the degeneration resistor of the current sources. Principally, the voltage across R_{sat} represents the minimum current source output voltage being the sum of degeneration voltage, V_{CEsat} (saturation voltage between collector and emitter of the NPN transistors) including a specific margin. The configuration is adapted such that the PWM on/off switching of the current sources does not interact with the control loop.
30 The output voltage raises, when the current source is turned off and has therefore no influence on the minimum detector. Further, capacitive effects of turning off the minimum selector will be filtered by the low pass characteristic of the switch mode controller. If all current sources are turned off, an additional breaking means is provided, in order to break the control loop and keep the duty cycle of the switch mode controller fix.

While the invention has been illustrated and described in detail in the drawings and foregoing description, such illustration and description are to be considered illustrative or exemplary and not restrictive; the invention is not limited to the disclosed embodiments.

5 Other variations to the disclosed embodiments can be understood and effected by those skilled in the art in practicing the claimed invention, from a study of the drawings, the disclosure, and the appended claims. A single LED may be replaced by multiple LEDs, in particular a string thereof. A light emitting diode may also be another light emitting semiconductor device as long as the aspects of the present invention are applicable. In the claims, the word "comprising" does not exclude other elements or steps, and the indefinite article "a" or "an" does not exclude a plurality. The mere fact that certain measures are recited in mutually different dependent claims does not indicate that a combination of these measured cannot be used to advantage. Any reference signs in the claims should not be construed as limiting the scope.

10

CLAIMS:

1. Electronic device for driving a light emitting semiconductor device, the electronic device comprising:
 - controlling means (CNTL) being adapted for controlling a switch mode power supply (SMPS) for supplying the light emitting semiconductor device (LED1r, LED2r) in response to a sensing value (VS) received by the controlling means (CNTL) which is indicative of a voltage across a current source for determining a current through the light emitting semiconductor device (LED1s, LED2r), wherein the switch-mode power supply (SMPS) is controlled such that the voltage across the current source is minimum.
2. The electronic device according to claim 1, comprising further the current source, wherein the current source is a switched current source or a linear current source.
3. The electronic device according to claim 1, wherein the control means (CNTL) provide signals to switch the current through the light emitting semiconductor device (LED1r, LED2r) on and off, in particular by a pulse width modulated signal (PWMr).
4. The electronic device according to one of the preceding claims, wherein the controlling means (CNTL) is further adapted to control the timing of a sampling means for sampling the sensing value, which is indicative of the voltage across the current source, such that sampling occurs when the current through the current source is turned on.
5. The electronic device according to one of the preceding claims, wherein the light emitting semiconductor device is a light emitting diode, the electronic device comprising further the switch-mode power supply (SMPS), wherein the switch-mode power supply and the controlling means are adapted to control the output voltage of the switch-mode supply with a control resolution of substantially less than the variation of the forward voltage of the light emitting diode to be driven.

6. The electronic device according to one of the preceding claims, comprising a plurality of light emitting diodes as light emitting semiconductor devices, the electronic device being further adapted to provide pulse width modulating signals for a plurality of light emitting diodes for individually dimming each of the light emitting diodes.

5

7. The electronic device according to claim 6, wherein the plurality of light emitting diodes is arranged in at least one string.

8. The electronic device according to claim 7, being further adapted to provide a pulse width modulated signal (PWM1) for dimming the diodes of the string.

9. The electronic device according to claim 7 or 8, comprising further a plurality of current sources and a minimum selector (MINSEL), wherein the plurality of light emitting diodes is coupled to the plurality of current sources and the minimum selector (MINSEL) is adapted to select the minimum voltage across the plurality of current sources, wherein the selected minimum voltage is used as a reference for controlling the switch-mode power supply.

10. The electronic device according to one of the preceding claims, wherein the control unit is electrically decoupled from the light emitting semiconductor devices, in particular by an inductive power converter or by an opto-coupler.

11. The electronic device according to one of the preceding claims, comprising an input pin to receive the sensing value (Vs).

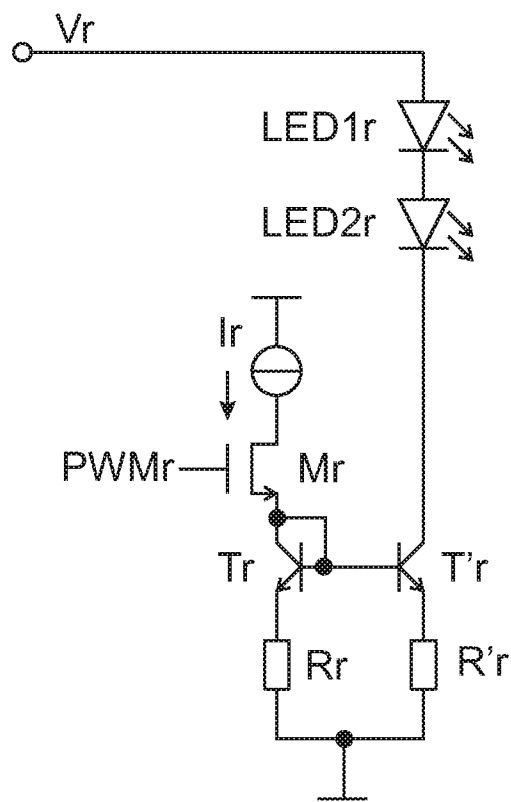


FIG. 1

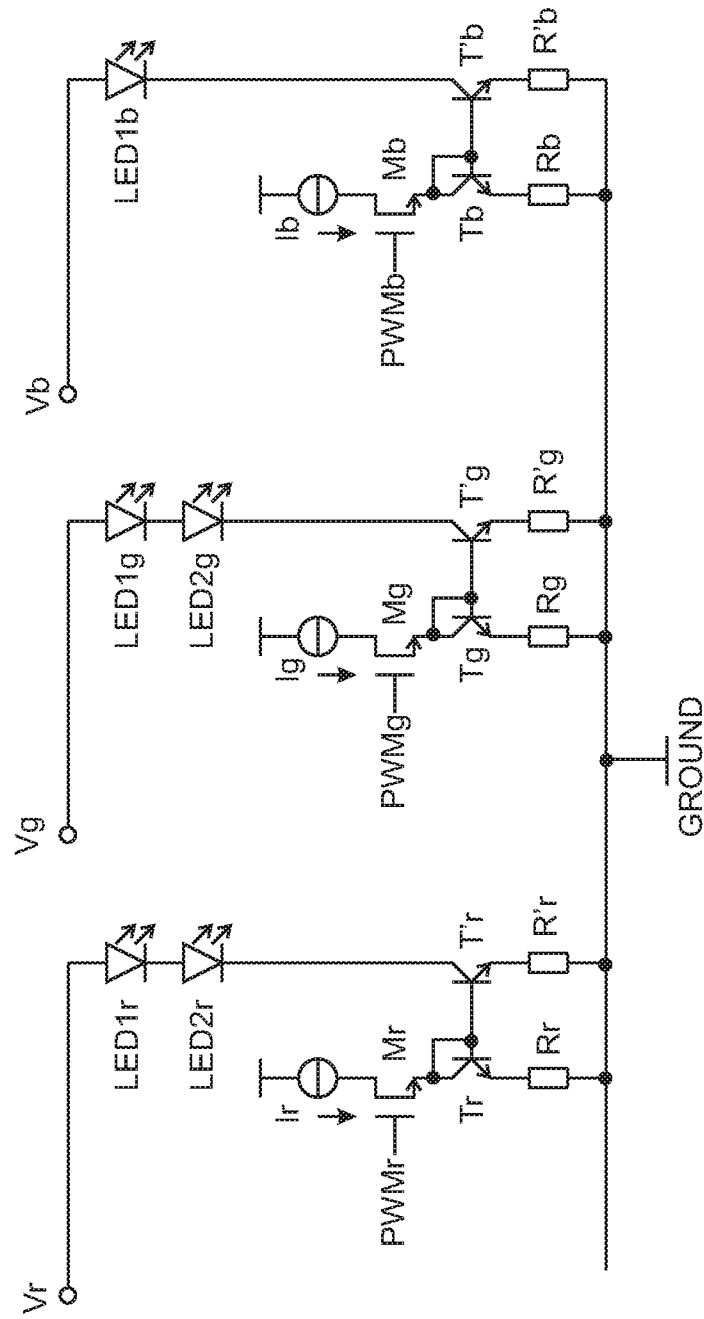


FIG. 2

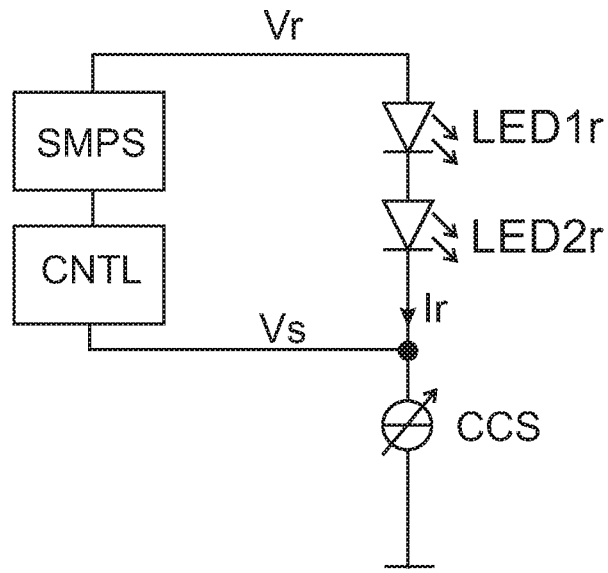


FIG. 3

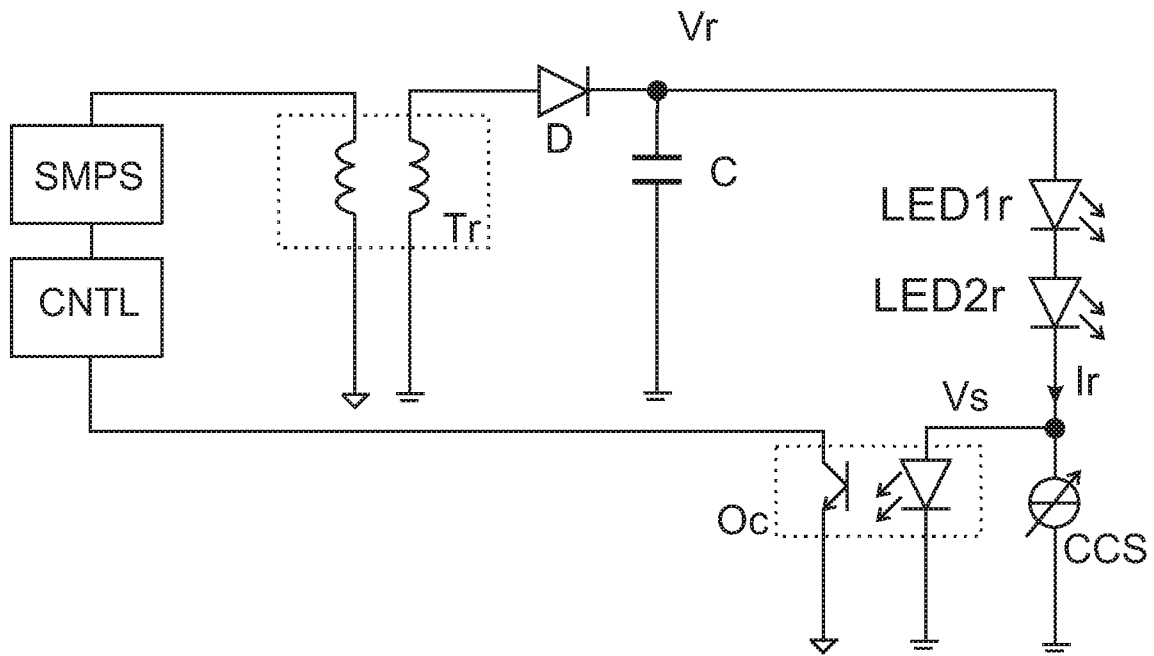


FIG. 4

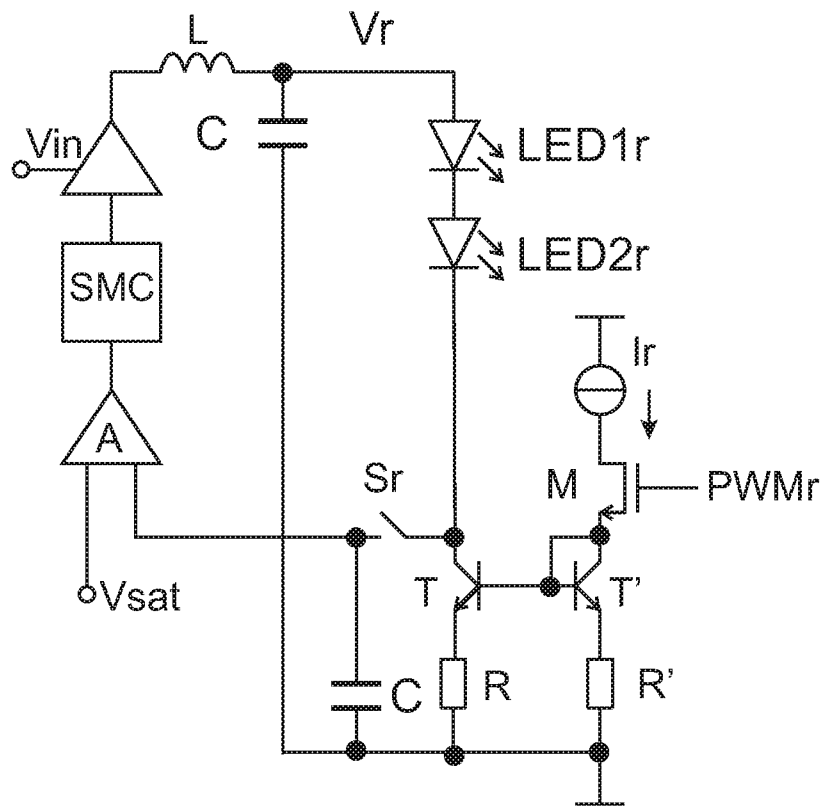


FIG. 5

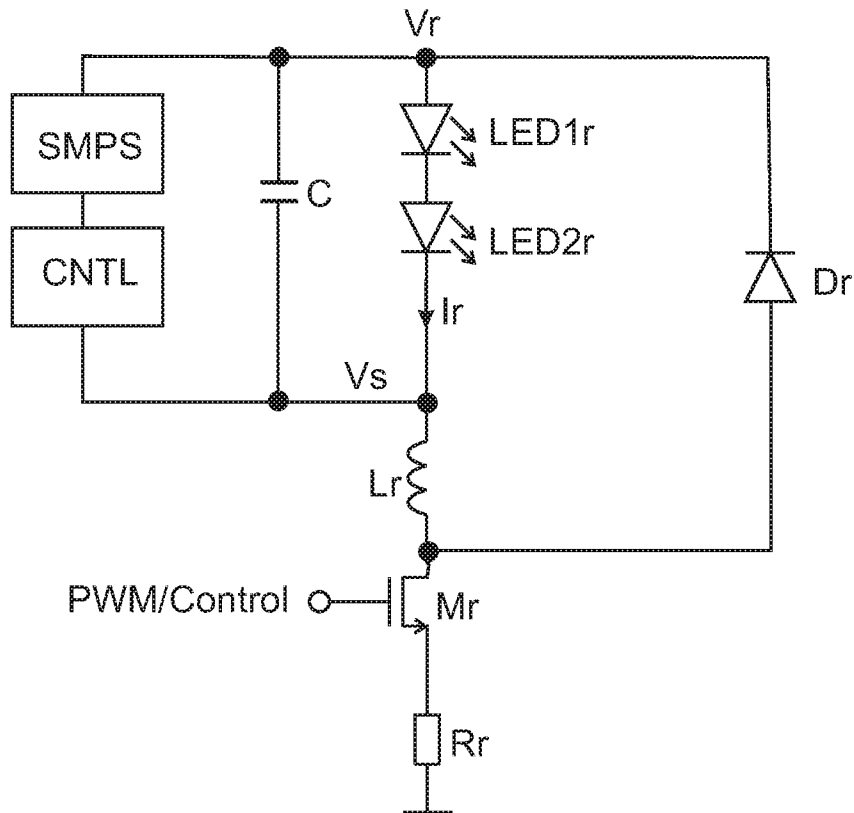


FIG. 6

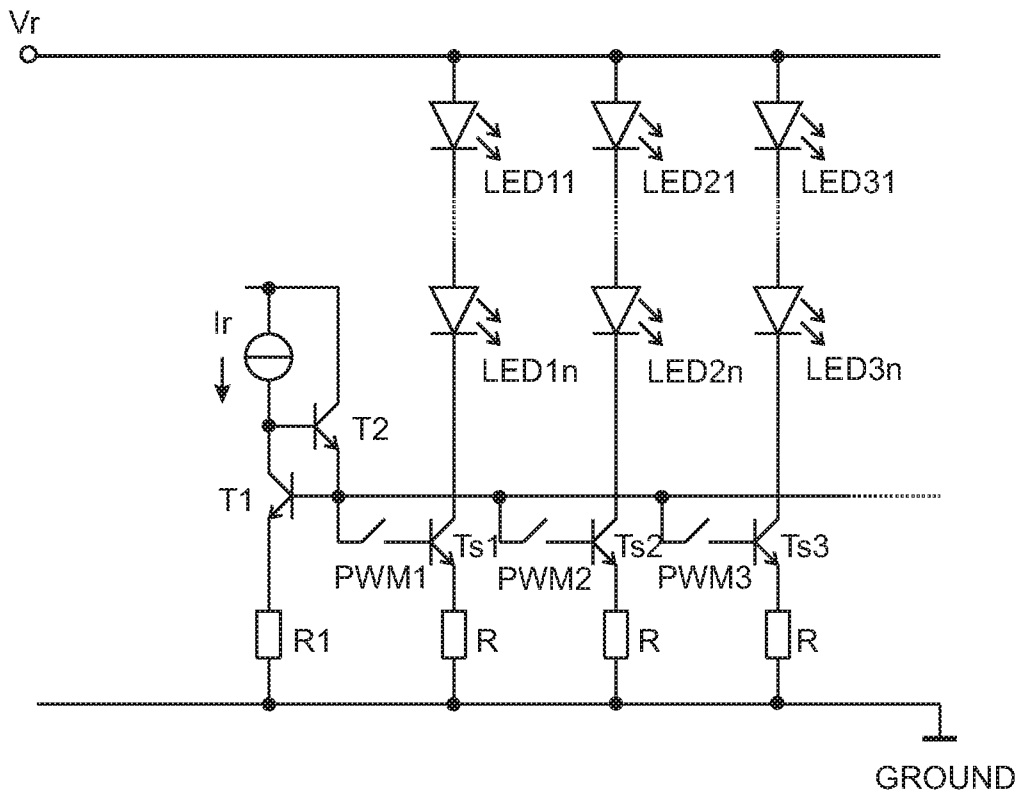


FIG. 8

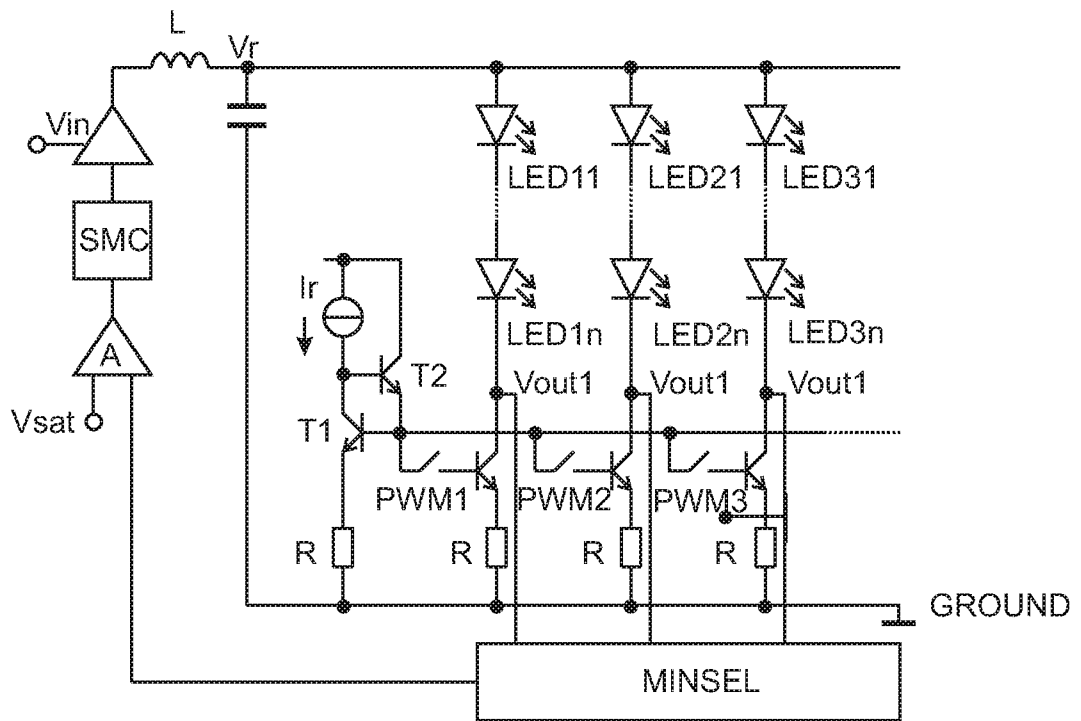


FIG. 9

INTERNATIONAL SEARCH REPORT

International application No
PCT/IB2007/054895

A. CLASSIFICATION OF SUBJECT MATTER INV. H05B33/08		
According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED		
Minimum documentation searched (classification system followed by classification symbols) H05B		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practical, search terms used) EPO-Internal, WPI Data		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	WO 2006/097329 A (AUSTRIAMICROSYSTEMS AG [AT]; BUEHLER TOBIAS [AT]; JESSENIG THOMAS [AT]) 21 September 2006 (2006-09-21)	1-3,11
A	page 1, line 6 - page 9, line 23; figure 1 -----	7,9
X	US 2003/235062 A1 (BURGYAN LAJOS [US] ET AL) 25 December 2003 (2003-12-25)	1-3,11
A	paragraph [0011] - paragraph [0020]; figures 1,2 -----	7,9
A	"480mA White LED 1x/1.5x/2x Charge Pump for Backlighting and Camera Flash" 2005, MAXIM, SUNNYVALE, CA, USA, XP002475922 page 7 - page 10; figures 1-5 -----	1-3,6-9, 11
A	DE 100 13 216 A1 (TRIDONIC BAUELEMENTE [AT]) 20 September 2001 (2001-09-20) ----- -/--	
<input checked="" type="checkbox"/> Further documents are listed in the continuation of Box C.		
<input checked="" type="checkbox"/> See patent family annex.		
* Special categories of cited documents :		
A document defining the general state of the art which is not considered to be of particular relevance	*T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention	
E earlier document but published on or after the international filing date	*X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone	
L document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	*Y* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.	
O document referring to an oral disclosure, use, exhibition or other means	*&* document member of the same patent family	
P document published prior to the international filing date but later than the priority date claimed		
Date of the actual completion of the international search <h2 style="text-align: center;">10 April 2008</h2>	Date of mailing of the international search report <h2 style="text-align: center;">28/04/2008</h2>	
Name and mailing address of the ISA/ European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo nl, Fax: (+31-70) 340-3016	Authorized officer <h2 style="text-align: center;">Albertsson, Gustav</h2>	

INTERNATIONAL SEARCH REPORT

International application No
PCT/IB2007/054895

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	DE 100 40 154 A1 (WESTIFORM HOLDING AG NIEDERWAN [CH]) 7 March 2002 (2002-03-07) -----	

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No PCT/IB2007/054895

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
WO 2006097329 A	21-09-2006	DE 102005012663 A1 EP 1859655 A1	28-09-2006 28-11-2007
US 2003235062 A1	25-12-2003	US 2004080301 A1	29-04-2004
DE 10013216 A1	20-09-2001	AT 256962 T EP 1185147 A1	15-01-2004 06-03-2002
DE 10040154 A1	07-03-2002	NONE	