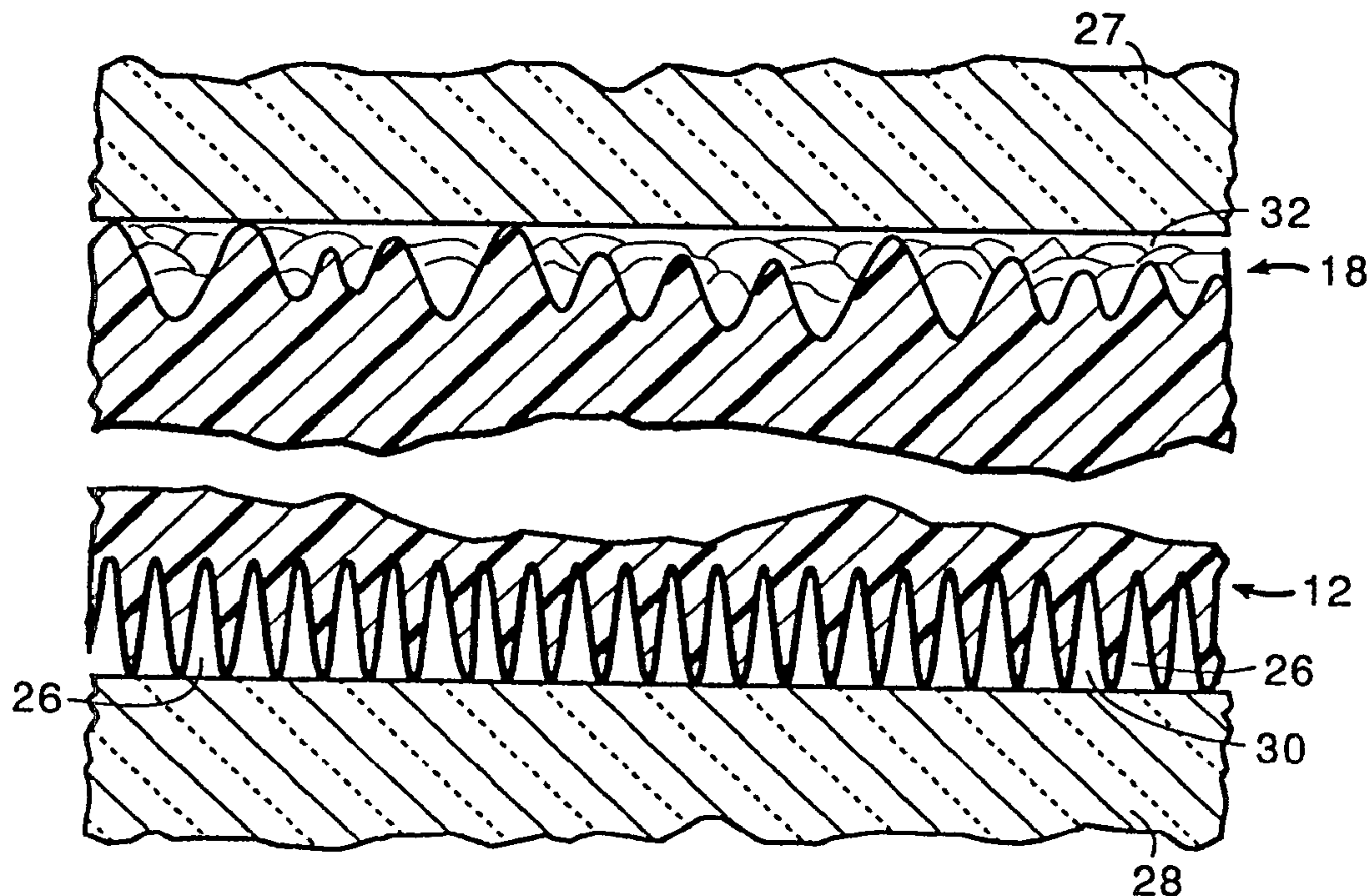




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(54) Title: ROUGH-SURFACED INTERLAYER



(57) Abrégé/Abstract:

A thermoplastic interlayer (10) having a first air removal surface (12) which includes a multiplicity of microscopic embossments (14) of substantially identical shape integrally projecting from the plane of one side of the interlayer in a regular pattern and a second air removal surface (18) on the other side of the interlayer (10) which is different from the first air removal surface (12) and includes a multiplicity of microscopic peaks (20) and valleys (22) of varying heights and depths arranged in an irregular, non-linear pattern; the height, Rz, of the embossments and peaks being less than about 75 microns and the distance, Sm, between embossments and peaks being less than about 650 microns. During deairing in forming a safety glazing, the first air removal surface (12) is partially transferred to and imposed on the second air removal surface (18) to provide deair paths of reduced obstruction.



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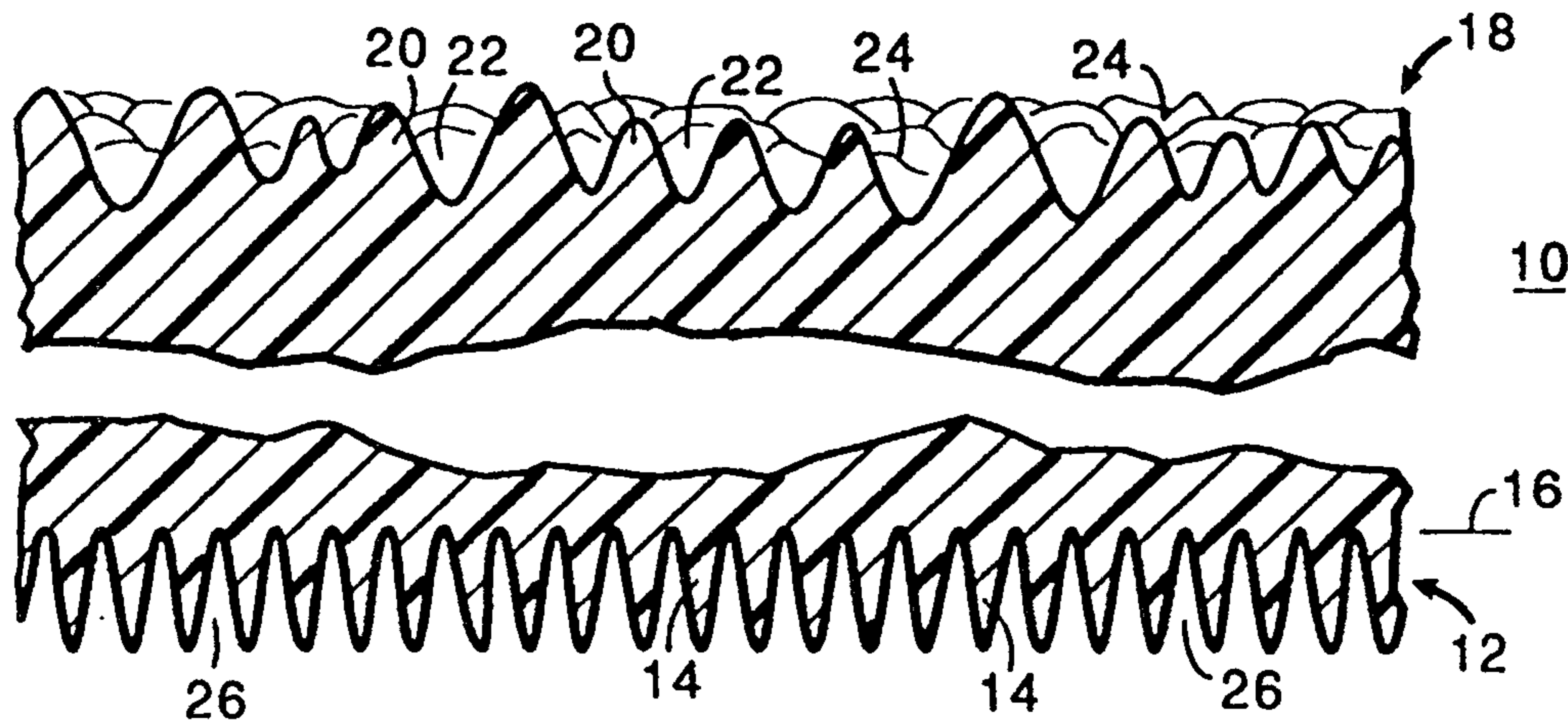
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(54) Title: ROUGH-SURFACED INTERLAYER



(57) Abstract

A thermoplastic interlayer (10) having a first air removal surface (12) which includes a multiplicity of microscopic embossments (14) of substantially identical shape integrally projecting from the plane of one side of the interlayer in a regular pattern and a second air removal surface (18) on the other side of the interlayer (10) which is different from the first air removal surface (12) and includes a multiplicity of microscopic peaks (20) and valleys (22) of varying heights and depths arranged in an irregular, non-linear pattern; the height, R_z , of the embossments and peaks being less than about 75 microns and the distance, S_m , between embossments and peaks being less than about 650 microns. During deairing in forming a safety glazing, the first air removal surface (12) is partially transferred to and imposed on the second air removal surface (18) to provide deair paths of reduced obstruction.

ROUGH-SURFACED INTERLAYER
BACKGROUND OF THE INVENTION

This invention relates to thermoplastic interlayer having rough surfaces and more particularly to a particular form of rough surface for optimum deairing in a prelamine with glass.

Plastic sheet, typically of polyvinyl butyral (PVB), is known as an interlayer for use with optically transparent glass in laminated safety glass assemblies used, for example, in vehicle windshields, building windows and the like.

It is further known, (see, for example, U.S. 4,035,549, to Kennar) to make the surface of the sheet rough to facilitate deairing, i.e. evacuating air from an interface between the sheet and a glass layer during preparation of a prelamine of the sheet with glass. More specifically, minute channels between the smooth surface of the glass and the rough surface of the opposing contiguous sheet form routes for air to escape from between the two members when pressure or vacuum is applied with heat during preparation of the prelamine. The deaired prelamine is then subjected to elevated temperature and pressure bonding conditions, usually in a downstream autoclave, to form the finished safety glass assembly.

Inadequate deairing results in visual defects in the finished safety glass assembly in the form of undesirable bubbles or local unlaminated regions. Deair completeness is conveniently measured by light transmission through the prelamine before final laminating in the autoclave. The greater such transmission, the greater the quality of deairing provided by a particular profile of rough surface.

Optimum deairing is a continuing need in the laminated safety glass art.

SUMMARY OF THE INVENTION

Now, improvements have been made in interlayer surface roughness which increase the quality of prelaminates formed therewith.

10 Accordingly, a feature of one embodiment of this invention is to provide an interlayer with a particular roughness profile which optimizes deairing during preparation of a prelamine for use in a safety glass assembly.

Another feature of another embodiment is the provision of a prelamine of high quality as determined by a remarkably high degree of light transmission therethrough.

Other features will in part be obvious and will in part appear from the following detailed description and claims.

20 These and other features are accomplished by a thermoplastic interlayer which comprises a) a first air removal surface comprising a multiplicity of microscopic embossments of substantially identical shape integrally projecting from the plane of one side of the interlayer in a regular pattern; and b) a second air removal surface on the other side of the interlayer which is different from the first air removal surface and comprises a multiplicity of microscopic peaks and valleys of varying heights and depths arranged in an irregular, non-linear pattern; the height, R_z , of
30 said embossments and peaks being less than about 75 microns and the distance S_m , between said embossments and peaks being less than about 650 microns; such interlayer in a prelamine press-bonded on each side to a layer of glass being capable of transmitting at least 85% of incident light.

In a specific aspect, the regular pattern of the first air removal surface comprises i) or ii) following:

5 i) a multiplicity of microscopic embossments of substantially identical shape arranged in mutually perpendicular rows;

10 ii) a multitude of substantially uninterrupted, parallel narrow linear channels defined by ridges evenly spaced from each other arranged diagonally with respect to a linear edge of the interlayer.

The preferred form of first air removal surface is ii) above.

15 Also provided in the method of preparing a pre laminate for a safety glazing by deairing the interface with glass on each rough-surfaced side of a thermoplastic interlayer and heating the interlayer and glass to collapse the rough surfaces, is the improvement facilitating deairing
20 wherein a regular roughness pattern on one side of the interlayer is partially transferred to and imposed on a random roughness pattern on the other side of the interlayer to provide deair paths which are less obstructed than those of the unmodified
25 random pattern.

In yet a more specific aspect, a method is provided for preparing a pre laminate for a safety glazing which comprises:

30 a) providing a thermoplastic interlayer having:

i) a first air removal surface on one side comprising a multiplicity of microscopic embossments of substantially identical shape integrally projecting from the plane of one side of
35 the interlayer in a regular pattern of rows; and

ii) a second air removal surface on the other side which is different from the first air removal surface comprising a multiplicity of microscopic peaks and valleys of varying heights and depths arranged in an irregular, non-linear pattern;

b) interposing the interlayer between two layers of glass;

c) increasing the temperature of the interlayer between the glass layers to above the glass transition temperature of the thermoplastic;

d) developing a negative pressure on the assembly of c) to draw air from the interface between one glass sheet and the first air removal surface at a rate greater than occurring at the interface between the other glass sheet and the second air removal surface;

e) partially collapsing embossments of the first air removal surface to cause the regular pattern to at least partially transfer to and modify the second air removal surface thereby facilitating air removal from the interface of the modified second air removal surface through channels formed by the transferred regular pattern; and then

f) increasing the temperature of the assembly of e) to substantially completely collapse the embossments and peaks of the first and modified second air removal surfaces to provide the pre laminate.

Further provided is a pre laminate producible by the methods noted above which is capable of transmitting at least 85%, and even as much as 95% or more, of light incident thereon.

BRIEF DESCRIPTION OF THE DRAWINGS

In describing the overall invention, reference will be made to the accompanying drawings wherein:

Fig. 1 is a partial, vertical, sectional view on an enlarged scale of an interlayer according to the invention;

Figs. 2 and 3 are views similar to Fig. 1 illustrating deformation of the interlayer during preparation of the prelaminate; and

Fig. 4 is an isometric view similar to Fig. 1 of a preferred form of interlayer.

DETAILED DESCRIPTION OF THE INVENTION

Thermoplastic interlayer usable in the invention must be capable of strongly bonding to a rigid panel such as glass to form an impact-dissipating layer in a laminated safety glass assembly. Exemplary thermoplastics include poly(ethyl-vinyl acetate), poly(ethylene-vinyl acetate-vinyl alcohol), poly(ethylene-methyl methacrylate-acrylic acid), polyurethane, plasticized polyvinyl chloride, polycarbonate, etc. Polyvinyl butyral (PVB) and more particularly partial PVB containing about 10 to 30 weight % hydroxyl groups expressed as polyvinyl alcohol is preferred. Such partial PVB further comprises about 0 to 2.5 weight % acetate expressed as polyvinyl acetate with the balance being butyral, expressed as polyvinyl butyral. The non-critical thickness of the thermoplastic sheet can vary and is typically about 0.25 to 1.5, preferably about 0.35 to 0.75 mm. PVB sheet is commercially available from Monsanto Company as Saflex® sheet and E.I. duPont de Nemours and Co. as Butacite® polyvinyl butyral resin sheeting.

PVB sheet is plasticized with about 20 to 80, preferably 25 to 45 parts of plasticizer per 100

parts of PVB resin. Such plasticizers are known to those skilled in the art and are typically disclosed in U.S. No. 4,654,179, col. 5, lines 56-65. Dihexyl adipate is preferred.

In addition to plasticizer(s), sheet of the invention may optionally contain additives to improve performance such as dyes, pigment colorants, light stabilizers, antioxidants, glass
10 adhesion control agents and the like. The sheet may be provided with a colored anti-glare gradient band extending along one side adjacent its edge which may be incorporated into the sheet according to the method and system disclosed in U.S.
4,316,868.

Referring to the drawings, thermoplastic interlayer sheet 10 is depicted in Fig. 1. Interlayer 10 differs from the prior art in having
20 different surface roughness profiles on its opposite major sides. More particularly, interlayer 10 includes a first air removal surface 12 comprising a multiplicity of microscopic embossments 14 substantially identical in shape which, in the illustrated embodiment, are V-shaped in vertical cross section when surface 12 faces downwardly. As illustrated, each embossment 14 projects from the plane of the sheet (schematically identified as 16) and forms an integral
30 continuation of one side of interlayer 10. Embossments 14 are arranged in the regular pattern shown in Fig. 1 in the form of linear rows extending in mutually perpendicular directions on one side of interlayer 10.

Embossments 14 may differ in shape from the preferred pyramidal configuration shown. Conical,

cylindrical, frusto-conical and the like may alternatively be used.

Second air removal surface 18 on the other side of the interlayer 10 is different from first air removal surface 12 and comprises a multiplicity of microscopic peaks 20, the surfaces of which define valleys 22, such peaks and valleys being of varying heights and depths. In contrast to first air removal surface 12, peaks 20 and valleys 22 are in an irregular, random, non-linear pattern on such other side of interlayer 10. This irregularity is schematically highlighted as 24 in Fig. 1 representing the outline of peaks of differing heights behind the plane of the cross section defining peaks 20.

The inverted V-shaped open spaces 26 between immediately adjacent embossments 14 collectively provide straight, unobstructed, relatively short, linear, uniform deair corridors to the open-ended edges of interlayer 10 through which air relatively quickly exhausts during formation of a prelamine in a manner to be presently described. In contrast, the randomized pattern of peaks 20 and associated valleys 22 of unmodified (Fig. 1) second air removal surface 18 can be expected to clog the paths through which air passes in moving to the edges of the interlayer. More particularly, with the random pattern the exhausting air collides with the randomly oriented peaks as it moves to the periphery of the interlayer tending to lengthen the exhaust paths and incrementally extend the time for air removal in comparison with that of regular first air removal surface 12.

Fig. 4 depicts an alternate form 50 of first air removal surface, the second air removal surface 52 in this embodiment being random and equivalent

to 18 in Fig. 1. As in Fig. 1, surface 50 comprises a multiplicity of microscopic embossments of substantially identical shape projecting from the plane of one side of the interlayer in a regular pattern. The embossments in this embodiment are in the form of continuous, uninterrupted ridges 54 evenly spaced from each other and integrally formed in the surface of one side of the interlayer. Ridges 54 are preferably arranged in the sheet surface diagonally to a straight longitudinal edge, typically at 45 degrees to a straight edge of the interlayer. Ridges 54 form the sides of a multitude of parallel, narrow, open top, flat bottom linear deairing channels 56 which are substantially unobstructed along their length and are open-ended at the edge of the sheet to accommodate passage of air. Immediately adjacent, neighboring ridges 54 are spaced (S_m - defined hereafter) (58 in Fig. 4) less than about 300 microns from each other and in height (R_z - defined hereafter) (60 in Fig. 4) are less than about 50 microns above the base of a channel 56.

Surface roughness is defined by the frequency which is the number of embossments 14 or peaks 20 or ridges 54 per unit of distance in a given direction (usually the direction of extrusion (MD) and 90° thereto (CMD)) and the amplitude or height of embossments 14, peaks 20 and ridges 56 which is the distance from the lowest valley to the highest peak. Techniques and systems for measuring these parameters are known to those skilled in the art and are disclosed in: U.S. 2,904,844, col. 3, lines 15-18; U.S. 3,591,406, col. 3, lines 49-53; U.S. 4,035,549, col. 2, lines 5-28; U.S. 4,925,725, col. 2, line 40 to col. 3, line 47; U.S. 5,091,258, col. 7, lines 34-53.

The system used herein to characterize roughness is a model S8P Perthometer from Mahr Corporation, Cincinnati, Ohio which uses a tracing stylus to measure actual roughness. In this regard, R_z (in microns, μ), defined according to DIN 4768 (May 1990), is the average peak to valley height which is the arithmetic mean of the individual measurement lengths l_e aligned together. l_e can be set as desired and is 2.5 mm herein.

Frequency is characterized in this system according to DIN 4762 in terms of the average distance between profile irregularities (S_m) (μ) within a reference length l_m wherein l_m can be set as desired and is 12.5 mm herein.

Prelaminate light transmission is measured with a photometer from Tokyo Denshoku Co., or equivalent. A light transmission measurement is relative to a clear laminate obtained after autoclave bonding which is taken to be 100%.

Conventional techniques known in the art are used to produce first and second air removal surfaces 12, 18. First air removal surface 12, 50 is roll molded downstream of a sheet-shaping die, not shown, by passage through a nip between two rotating rolls, i.e. an embossing roll having indentations formed in its surface which are complementarily-shaped negatives of embossments 14 or ridges 54 and a cooperating backup roll. An equipment system capable of modification to provide surface 12, 50 is described in and shown in Fig. 1 of U.S. 4,671,913. Second air removal surface 18 is formed by controlling one or more of the following during shaping of the interlayer, usually by extrusion: polymer molecular weight distribution, water content of polymer melt, melt and die exit temperature, die exit geometry, etc.

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Systems describing such techniques are disclosed in U.S. Patent Nos. 2,904,844; 2,909,810; 3,994,654; 4,575,540; 5,151,234 and European Application No. 0185,863, published July 2, 1986.

5 The different roughness profiles on the two sides of interlayer 10 provide an unexpected improvement in deair performance brought about by cooperative interaction of the different surface profiles. Figs. 2 and 3 illustrate the postulated
10 behavior of the surfaces of the Fig. 1 embodiment of interlayer 10 during preparation of a prelaminated for a safety glazing. More particularly, interlayer 10 is interposed between two layers of preheated glass 27, 28 (Fig. 2).
15 Contact with such glass conductively increases the temperature to that of the glass - i.e. to a temperature adequate to facilitate collapsible deformation of the surface, which temperature is typically above the glass transition temperature of
20 the thermoplastic of the interlayer. The glass/interlayer/glass trilayer assembly of Fig. 2 is then placed in a flexible rubber bag or equivalent, having an opening communicating with a source of negative pressure. A vacuum ring
25 encompassing the periphery of the trilayer assembly is an acceptable equivalent. The negative pressure draws air from interface 30 (Fig. 2) between glass sheet 28 and first air removal surface 12 at a removal rate considered greater than occurring
30 along interface 32 between glass sheet 27 and second air removal surface 18. This difference is due to the previously described unobstructed paths for air passage between the embossments of air removal surface 12 as compared with the tortuous
35 paths delimited by the random peaks and valleys of surface 18. Such preferential rush of air from

interface 30 creates a slight negative pressure along surface 12 which partially collapses embossments 14 of first air removal surface 12 as illustrated by flattened cross section 34 in Fig. 3. This flattening is aided by the momentary greater pressure on the opposite side along interface 32 containing the randomized second air removal surface 18. Since interlayer 10 is at elevated deformation temperature and is trapped between glass layers 27, 28, the downwardly collapsing embossments 14 deflect the thermoplastic on the opposite (upper in Fig. 2) side upwardly to at least partially transfer the regular pattern to and modify the randomized pattern of second air removal surface 18. This is brought out in Fig. 3. A downwardly collapsing regular embossment 14 on the lower surface will cause upward deflection of a particular random peak on the upper surface, which peak is of sufficient initial height such that on deflecting it becomes high enough to abut against the glass surface. This is depicted by modified peak 35 in the plane of Fig. 3 abutting glass surface 37. Other modified peaks behind the plane of Fig. 3 generated the same way as 35 are shown as 39 and this represents the regular pattern superimposed on the initial random surface. However, random peaks of upper surface 18 of lesser initial height than just described continue to provide a random pattern in modified surface 18 and these are identified in the plane of Fig. 3 as 41. 43 in Fig. 3 schematically represents modified peaks of such initial lesser height behind the plane of Fig. 3. Paths 38 of the thus modified second air removal surface 18 formed by the transferred regular pattern from the opposite side are considered to facilitate flow of air from

interface 32 of the modified second air removal surface. This effect of introducing an array of regular peaks from the regular pattern to a previously entirely random surface results in shorter, less tortuous air escape paths. Air flow through the modified random pattern is similar to that occurring on the side with the regular pattern and is considered less obstructed than that occurring through the unmodified random pattern.

Subsequently increasing the temperature of the glass/interlayer/glass assembly of Fig. 3 in an oven or equivalent, substantially completely collapses the embossments and peaks of the first and modified second air removal surfaces of interlayer 10 and press bonds the interlayer to the glass to provide the pre laminate. Subjecting such pre laminate to conventional bonding conditions of elevated temperature and pressure, in a manner known to those in the art, usually in a downstream autoclave, firmly bonds the opposing surfaces of the interlayer 10 to the contiguous glass layers to form the finished safety glass assembly.

Performance of the interlayer of Fig. 4 wherein each side has a different pattern (regular on one side and random on the other) is considered to substantially follow the mechanism above described for the Fig. 1 embodiment.

The invention is further described in the following examples which are for illustration only and not to limit or restrict the invention.

EXAMPLE C1

This is not according to the invention.

Thirty mils (0.76 mm) thick Saflex® sheet containing a nominal level of 32 parts plasticizer per 100 parts PVB resin is obtained from Monsanto Company having a surface roughness on each side

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characterized by values of R_z of 30-35 microns and S_m of 450-500 microns. The pattern is random as illustrated at 18 in Fig. 1. Such roughness profile is generated by melt fracture, typically by
5 passage of the thermoplastic forming the sheet through a rectangular sheeting die opening formed by lands which are at a temperature less than that of the bulk of the extruding melt. This is achieved by flow of an appropriate temperature
10 conditioning fluid through channels just below the land surfaces.

40 x 60 in (102 x 154 cm) sections of such sheet are placed on a heating surface at 80-180°F (26 to 82°C) to heat the sections to this
15 temperature. An embossing station comprises a 4 inch (10 cm) diameter embossing roll pressing against a 4 inch (10 cm) diameter rubber-faced backup roll at a pressure of 30 pounds per lineal inch. The entire surface of the embossing roll has
20 sharply profiled abutting pyramidal cavities forming a retiform surface thereon at a frequency of 88 cavities per inch. The face of the back up roll is covered with a high extensibility, temperature resistant rubber chosen to be capable
25 of stretching without fracturing. An anti-stick release coating is on the surface of the embossing roll which is at 177°C. The embossing roll rotates at a surface speed of about 10-20 fpm (3-6 m per min.). A vacuum roll adjacent the nip formed by
30 the embossing and back up rolls pulls the embossed sheet from the embossing roll surface. The precut sheet sections are passed through the nip, removed by the vacuum roll beyond the nip and placed on a table at room temperature. Each sheet section is
35 then turned over and the process repeated to emboss the other side.

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Sheet sections sharply embossed on each side with a regular pattern in the manner just described are visually displeasing to the eye and therefore considered commercially unacceptable. The appearance is described as a moire pattern and is caused by the frequency of the embossments not being in exact accurate register on each side of the sheet - i.e. the slightly different frequency on each side results in interference patterns which are not in phase with each other. Sheet with such moire effect presents an undulating pattern similar to a wood grain appearance.

Using the roughness measuring system previously described, the sheet was characterized by an R_z of 30 microns and S_m of 280 microns.

EXAMPLE C2

This likewise is not according to the invention.

Unembossed Saflex sheet as initially described above having a random roughness surface profile on each side ($R_z = 30-35$ microns and $S_m = 450-500$ microns) is cut into sections as in Example C1. Sheet sections at about $15-18^\circ\text{C}$ are placed between two layers of similarly dimensioned float glass at about 30°C to raise the sheet to this temperature which is above the glass transition temperature of the plasticized PVB. The three layer glass/sheet/glass assembly is placed in a flexible rubber bag connected to a negative pressure source to develop a pressure of $1/3$ atmosphere (33.5 kPa) within the bag thereby drawing air from the two interfaces of the sheet with the glass. The three layer assembly is then passed through an oven to raise the temperature of the three layers to about 100°C and then removed from the oven and cooled to room temperature. Percent light transmission of

the prelaminate thus formed is measured as 60-70%. Such a laminate is industrially unacceptable since at least 85% is required to be commercially viable. This control Example illustrates unacceptable
5 performance of a surface roughness profile in the form of a random pattern on each side of the sheet.

EXAMPLE C3

A commercially available plasticized PVB sheet different from that of the invention has a random
10 pattern on each side similar to that described in Example C2 except R_z is 34 microns and S_m is 291 microns. A prelaminate formed using the procedure described in Example C2 has a light transmission of 85-87%.

15

EXAMPLE 1

This is according to the invention.

Sheet sections as described in Example C1 are embossed using the procedure of C1 on only one side - i.e. the second side is not embossed and has the
20 initially present randomized pattern having R_z of 30-35 microns and S_m of 450-500 microns. As in C1, the regular roughness profile of the embossed side has R_z of 30 and S_m of 280 microns. No moire pattern is present.

25

Measured light transmission in (4-6 samples) prelaminate formed therewith is as high as 95% and is generally in the 87-95% range. This
unexpectedly high light transmission obtained using interlayer having different roughness profiles on
30 each side is the result of the mechanism previously described with reference to Figs. 2 and 3. This is contrasted with the lower light transmission in Examples C2 and C3 where the interlayer sheet has a random roughness pattern on each side.

35

EXAMPLE 2

This is likewise according to the invention and describes the performance of the interlayer of Fig. 4.

5 Saflex sheet is used having a random rough surface on each side wherein $R_z = 52-57$ microns and $S_m = 591-615$ microns. Such sheet 40 inches (102 cm) wide as just described in roll form at 55°F (13°C) is continuously unwound at 10 to 30 fpm (3
10 to 9 meters per min) and fed to an embossing station comprising a 6.5 inch (16.5 cm) diameter embossing roll pressing against a 6.5 inch (16.5 cm) diameter rubber-faced backup roll at a contact pressure of 30 to 62 pounds per sq. inch (207 to
15 427 kPa). The entire shaping surface of the embossing roll is engraved with a sawtooth configuration, a sawtooth being V-shaped in vertical cross section with the sides of immediately adjacent sawteeth at ninety degrees to
20 each other. The sawteeth form continuous helical ridges on the roll surface oriented at 45 degrees with respect to the longitudinal roll axis. The frequency of the ridges is 80 per inch (203 per cm) measured across the direction of the helix. The
25 face of the cooperating backup roll is covered with a high extensibility, temperature-resistant rubber capable of stretching without fracturing. An anti-stick release coating is on the surface of the embossing roll which is regulated at 163°C by the
30 conventional presence of an appropriate heating medium beneath the embossing surface. A conventional vacuum roll (not shown) downstream of the nip formed by the embossing and backup rolls pulls the embossed sheet from the embossing roll
35 surface. The unembossed sheet passes through the nip, is removed by the vacuum roll beyond the nip,

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passes (270 degree wrap) over a chilled (minus 7°C) cooling roll and is rewound.

Sheet sections embossed on one side with a regular pattern in the manner just described having the original unembossed random surface on the other side are as illustrated in Fig. 4. The amplitude (height) of the ridges in first air removal surface of the sheet (or depth of the channels between ridges) (R_z) is about 60 microns. When the interlayer before embossing has an initial rough surface as in the present Example, the embossing depth should be at least as deep as the height (R_z) of the peaks in the initial rough surface. The distance between adjacent ridges (or width of a channel between ridges) is 312 microns thereby providing the multitude of long, uninterrupted narrow channels running across each side of the sheet which are open at their ends at the edges of the interlayer to the surroundings to optimize deairing in forming the prelaminate.

The procedure described in Example C2 is used to form prelaminates. Percent light transmission through such prelaminates thus formed is as follows:

25	97.0
	90.8
	94.1

This high light transmission is unexpected and industrially quite acceptable and indicative of the high quality of deairing provided by the regular/random surface roughness profiles of the invention.

EXAMPLES 3-5 AND C2-C4

This simulates shaping an interlayer having the regular/rough deair surface combination of the preferred Fig. 4 embodiment. Shaping involves

stretching the interlayer usually for the purpose of aligning an initially horizontal gradient color band in the interlayer with the arcuate peripheral contour of the stretched sheet section, such

5 curvature being desired for use of the sheet in a similarly configured contoured vehicle windshield. See, for example, U.S. 5,137,673, issued August 11, 1992 for further disclosure of shaping. Since

10 deairing occurs after shaping it is desirable that the rough surface not substantially collapse during shaping.

12 by 12 in (30.5 x 30.5 cm) interlayer sections having the surface topography described in Example 2 (30 mm thick) are vertically suspended in

15 a rack and a 2.6 kg steel bar attached at their lower ends. The weighted sections are placed in an oven at 100°C for 4 min. to vertically elongate the sections 15% and cause the bar to abut a stop in the oven below the elongated sections. This extent

20 of stretch simulates the maximum stretch encountered in a typical full size sheet section intended for use in a contoured vehicle windshield. The stretched sections are removed from the oven and cooled to room temperature. Prelaminates are

25 prepared using the procedure described in Example C2 and light transmission results obtained are as follows:

	<u>Example</u>	<u>Unshaped (from Ex.2)</u>	<u>Shaped</u>
	3	97.0	93.1
30	4	90.8	91.1
	5	94.1	94.3

To contrast the above with representative prior art sheet surface topographies, the above procedure is repeated with sheet having a random

35 rough surface on each side - i.e. of the general type described with respect to the initially

unembossed sheet in Example 1. Typical roughness values are $R_z = 44$ microns and $S_m = 384$ microns. Results obtained are as follows:

	<u>Example</u>	<u>Unshaped</u>	<u>Shaped</u>
5	C2	87.0	80.9
	C3	91.6	87.4
	C4	92.9	84.0

10 The above data (Examples 3, 4, 5) dramatically illustrates that the combination of sheet surface patterns according to the invention importantly survive shaping with minimal loss in deairing performance in contrast with the significantly greater loss in deair performance of the prior art random rough surfaces of Examples C2-C4.

15 Interlayer of the present invention preferably has an R_z on each side of less than about 75 microns, preferably less than about 50 microns and most preferably between 20-70 microns and a frequency on each side as characterized by S_m of
20 less than about 650 microns, for example, less than about 300 microns, preferably between 80 and 320 microns.

The preceding description is for illustration and should not be taken as limiting. Various
25 modifications and alterations will be readily suggested to persons skilled in the art. It is intended, therefore, that the foregoing be considered as exemplary only and that the scope of the invention be ascertained from the following
30 claims.

I CLAIM:

1. A thermoplastic interlayer which comprises:

5 a) a first air removal surface comprising a multiplicity of microscopic embossments of substantially identical shape integrally projecting from the plane of one side of the interlayer in a regular pattern; and

10 b) a second air removal surface on the other side of the interlayer which is different from the first air removal surface and comprises a multiplicity of microscopic peaks and valleys of varying heights and depths arranged in an irregular, non-linear pattern;

15 the height, R_z , of said embossments and peaks being less than about 75 microns and the distance S_m , between said embossments and peaks being less than about 650 microns;

20 said interlayer in a prelamine press-bonded on each side to a layer of glass being capable of transmitting at least 85% of incident light.

2. A thermoplastic interlayer which comprises:

25 a) a first air removal surface integrally projecting from the plane of one side of the interlayer in a regular pattern comprising i) or ii) defined below:

30 i) a multiplicity of microscopic embossments of substantially identical shape arranged in mutually perpendicular rows;

35 ii) a multitude of substantially uninterrupted, parallel narrow linear channels defined by ridges evenly spaced from each other arranged diagonally with respect to a linear edge of the interlayer;

b) a second air removal surface on the other side of the interlayer which is different from the first air removal surface and comprises a multiplicity of microscopic peaks and valleys of varying heights and depths arranged in an irregular, non-linear pattern;

the height, R_z , of said embossments, peaks and ridges being less than about 75 microns and the distance S_m , between said embossments, peaks and ridges being less than about 650 microns;

said interlayer in a prelamine press-bonded on each side to a layer of glass being capable of transmitting at least 85% of incident light.

3. The thermoplastic interlayer of claim 2 wherein the first air removal surface comprises ii).

4. A thermoplastic interlayer which comprises:

a) a first air removal surface comprising a multiplicity of microscopic embossments of substantially identical shape integrally projecting from the plane of one side of the interlayer in a regular pattern of mutually perpendicular rows; and

b) a second air removal surface on the other side of the interlayer which is different from the first air removal surface and comprises a multiplicity of microscopic peaks and valleys of varying heights and depths arranged in an irregular, non-linear pattern;

the height, R_z , of said embossments and peaks being less than about 75 microns and the average distance S_m , between said embossments and peaks being less than about 300 microns;

said interlayer in a prelamine press-bonded on each side to a layer of glass being capable of transmitting at least 85% of incident light.

5. The interlayer of claim 4 wherein the embossments are V-shaped in cross section.

6. The interlayer of claim 5 wherein R_z of the embossments is less than about 50 microns.

7. The interlayer of any of claims 4, 5 or 6 wherein the thermoplastic is polyvinyl butyral.

8. The interlayer of claim 7 including a colored anti-glare gradient band along one side adjacent its edge.

9. A method of preparing a prelamine for a safety glazing by deairing the interface with glass on each rough-surfaced side of a thermoplastic interlayer and heating the interlayer and glass to collapse the rough surfaces, the improvement facilitating deairing wherein a regular roughness pattern on one side of the interlayer is partially transferred to and imposed on a random roughness pattern on the other side of the interlayer to provide deair paths which are less obstructed than those of the unmodified random pattern.

10. A method of preparing a prelamine for a safety glazing which comprises:

a) providing a thermoplastic interlayer having:

i) a first air removal surface comprising a multiplicity of microscopic embossments of substantially identical shape integrally projecting from the plane of one side of the interlayer in a regular pattern of rows; and

ii) a second air removal surface on the other side of the interlayer which is different

from the first air removal surface, and comprises a multiplicity of microscopic peaks and valleys of varying heights and depths arranged in an irregular, non-linear pattern;

5 b) interposing the interlayer between two layers of glass;

 c) increasing the temperature of the interlayer between the glass layers to above the glass transition temperature of the thermoplastic;

10 d) developing a negative pressure on the assembly of c) to draw air from the interface between one glass sheet and the first air removal surface at a rate greater than occurring at the interface between the other glass sheet and the
15 second air removal surface;

 e) partially collapsing embossments of the first air removal surface to cause the regular pattern of such first air removal surface to partially transfer to and modify the second air
20 removal surface thereby facilitating air removal from the interface of the modified second air removal surface through channels formed by the transferred regular pattern of the modified second air removal surface; and then

25 f) increasing the temperature of the assembly of e) to substantially completely collapse the embossments and peaks of the first and modified second air removal surfaces of the interlayer to provide said prelamine.

30 11. A prelamine producible by the method of either of claims 9 or 10 capable of transmitting at least 85% of light incident thereon.

 12. The prelamine of claim 11 capable of transmitting 95% of light incident thereon.

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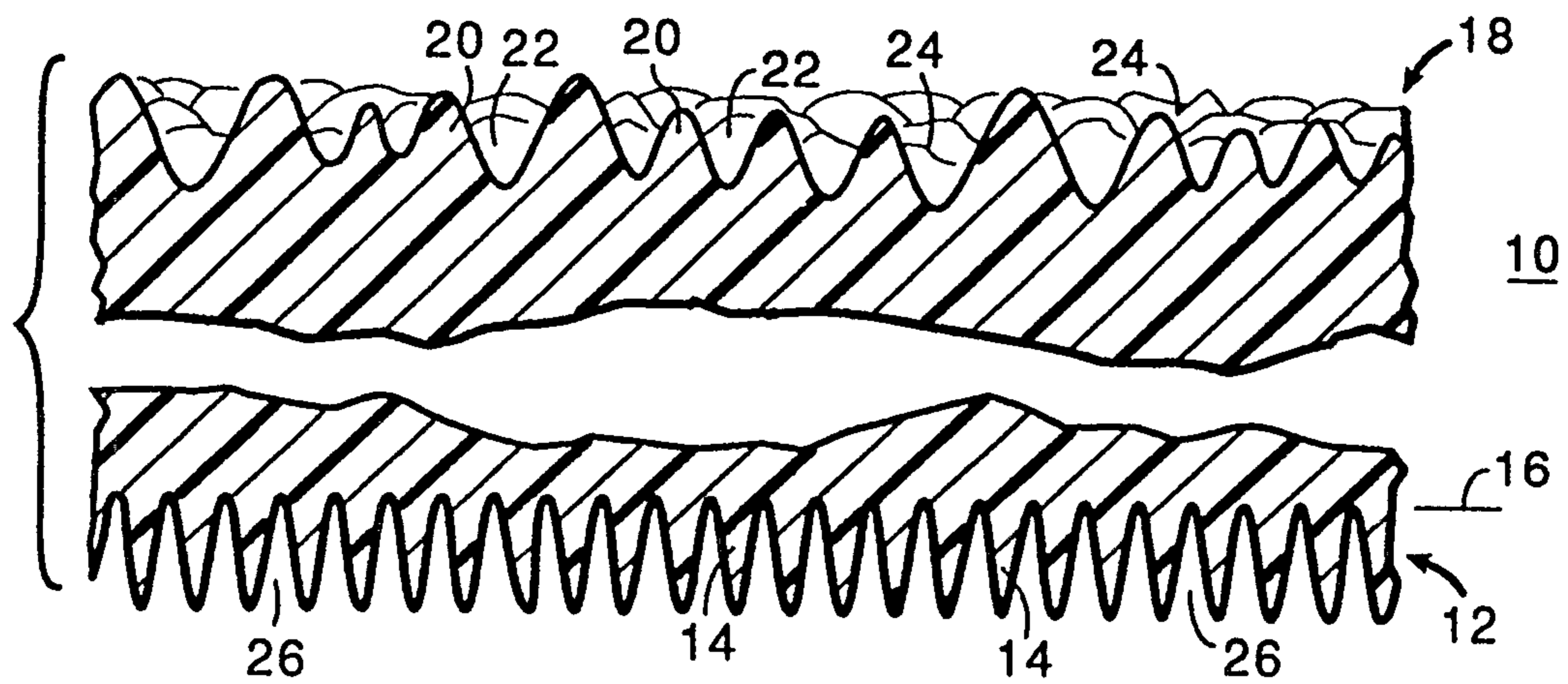


FIG. 1

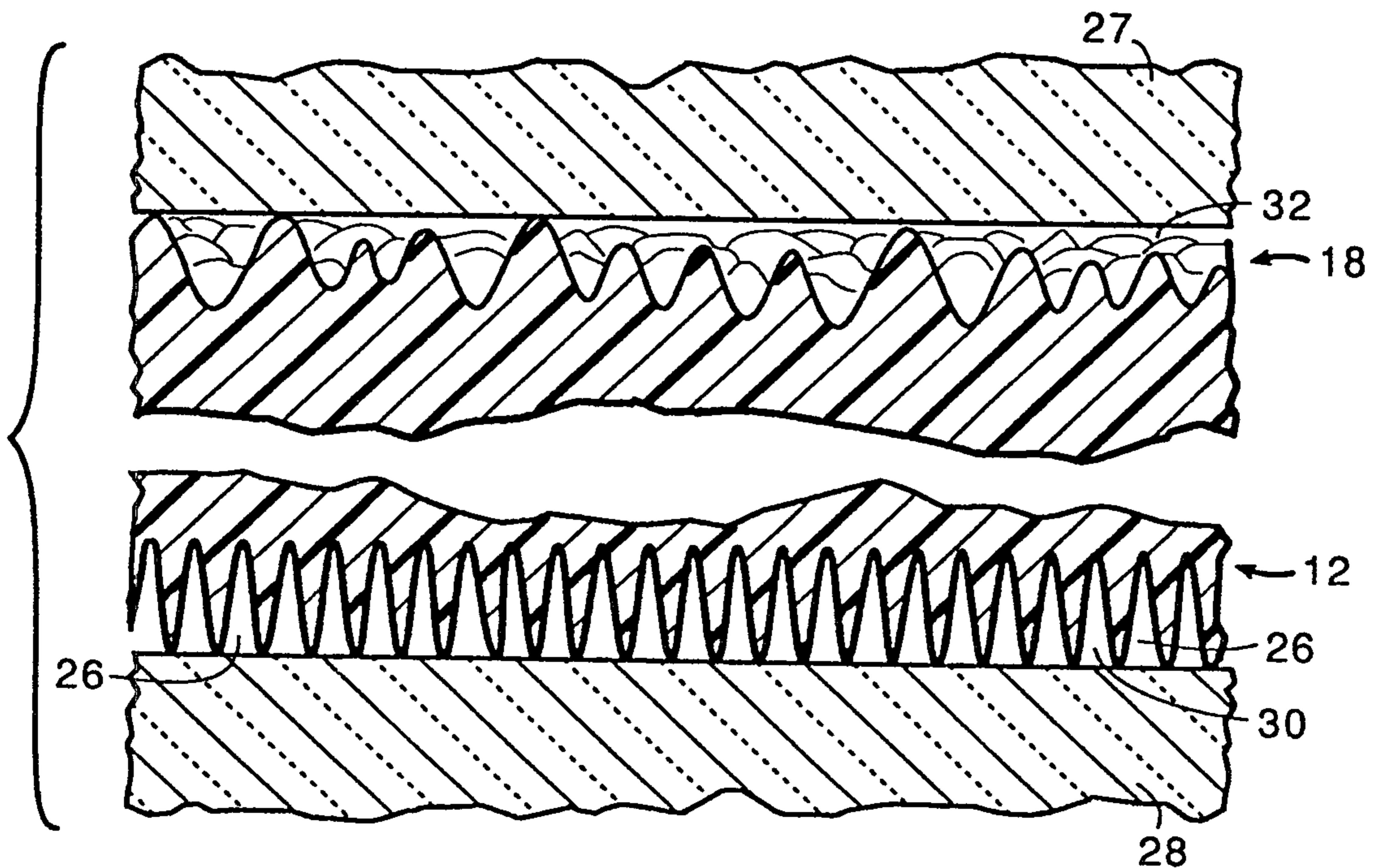


FIG. 2

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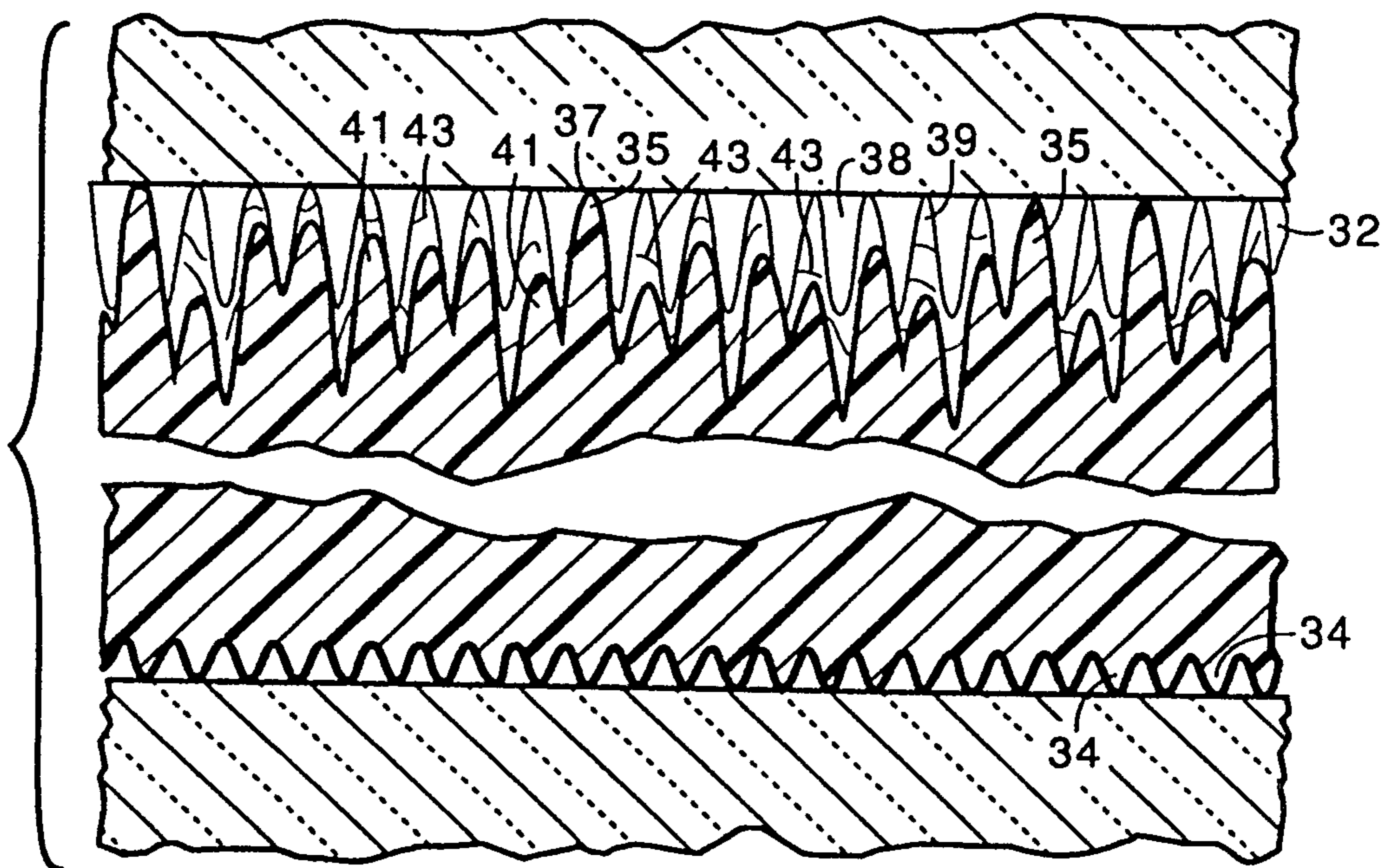


FIG. 3

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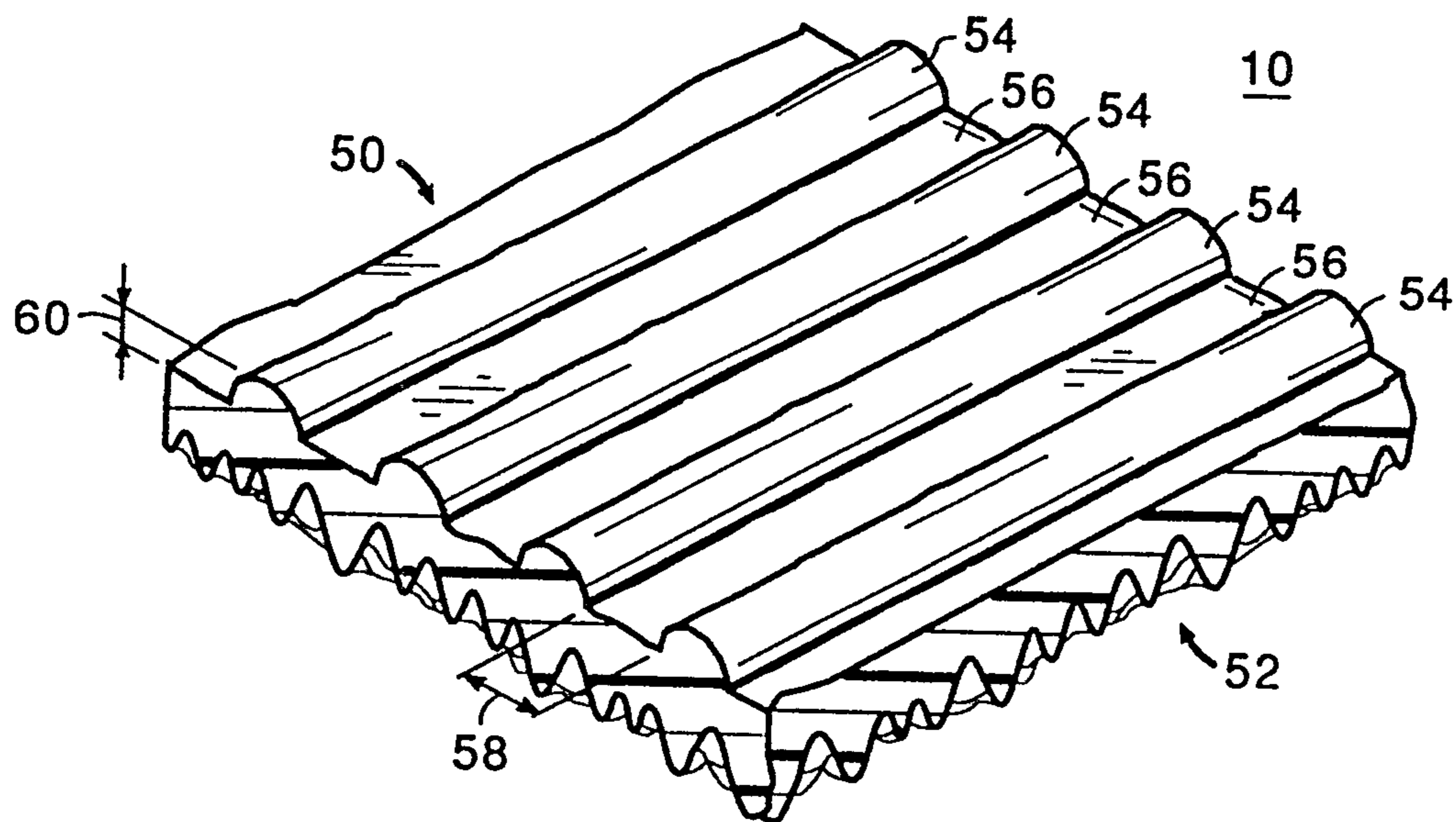


FIG. 4

