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(54) LIGHTWEIGHT ENHANCED BALLISTIC ARMOR SYSTEM

LEICHTES VERBESSERTES BALLISTISCHES PANZERUNGSSYSTEM

SYSTÈME DE BLINDAGE BALISTIQUE AMÉLIORÉ LÉGER

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DescriptionFIELD OF THE INVENTION

[0001] The present invention generally relates to lightweight ballistic armor systems which can be integrally formed within, or secured to, a structure, such as a trailer, shipping containers, and the like, for protecting individuals, structures, missile canisters, vehicles and the like against low, medium and high velocity and low, medium and high caliber projectiles, as well as systems and structures, such as trailers, shipping containers, vehicles, body armor, aircraft, missile canisters and the like being integrally formed of such a lightweight ballistic armor system. More particularly, the present invention relates to an enhanced ballistic armor system which is integrally formed within a structure or vehicle, or secured directly thereto, for protection of individuals, structures, vehicles, cargo and the like against low, medium and high velocity and low, medium and high caliber projectiles. These projectiles can include low-caliber to high-caliber bullets, rockets, exploding grenades, exploding mortar shells, exploding mines and the like.

DESCRIPTION OF THE PRIOR ART

[0002] Ceramic-based armors and armor systems are well known in the art. However, many conventional armors and armor systems tend to be too heavy and/or bulky to be easily employed as a protection system against high caliber artillery and projectiles, or even lower caliber threats. Moreover, many conventional armors and armor systems can also tend to be too expensive for practical use or manufacture. Furthermore, ballistic armor and armor systems are subjected to a variety of projectiles or fragments over a wide range of velocities and calibers designed to defeat the armor or armor systems by penetrating the armor or armor systems, or by causing an impact against the armor or armor system that can cause spalling (i.e., flaking off of material from an object due to impact from another object), in particular spalling through mechanical stress which in turn eventually defeats the armor.

[0003] Many and various types of armor and armor systems are known for protecting personnel, vehicles, equipment and the like from damage or destruction caused by high caliber artillery and projectiles. Many such armor and armor systems are employed in military applications to protect individuals (such as via body armor), aircraft, tanks, ships and vehicles from damage or destruction caused by high caliber artillery and projectiles. In yet other applications, many such armor and armor systems are employed in military applications to protect missiles during their storage or transport, such as for example in the form of canisters in which the missiles are stored, held or transported.

[0004] The use of such armor and armor systems for protecting missiles maintained in protective canisters during storage or transport of the missiles is also well known. However, munitions must comply with the MIL-STD-2105 bullet impact and fragment impact requirements as defined in STANAG 4241 and STANAG 4496. Meeting these requirements by protecting the munitions with conventional ceramic armor systems is difficult due to the limited multi-hit performance of ceramic systems. In some known applications, the armor or armor systems is incorporated into the structure that is to be protected. Such applications can include military vehicles, armored vehicles or missile storage canisters. In such applications, it is typically not possible for the armor or armor systems to be temporarily applied but rather thus tend to be permanent aspects of the structure. In this regard, the armor systems can be difficult or even impossible to replace in the event of damage or failure.

[0005] In order to address the issue of weight in armor or armor systems, some conventional systems employ ceramic materials that can protect against a range of projectiles or fragments of projectiles. Ceramic tiles can often be used to break up and dissipate the energy of high caliber projectiles, and can be applied in specific thicknesses or patterns of the arrangement of tiles to maximize effectiveness. However, a disadvantage of conventional ceramic tiles is that ceramic is brittle and is more susceptible to cracking after impact, thus reducing the effectiveness against subsequent impacts. Cracking of the conventional ceramics can also leave the underlying structure to be protected vulnerable to exposure to outside elements, such as water, air, heat, cold, wind, chemicals, biological agents, etc., thereby further weakening the structure to be protected.

[0006] One known disadvantage in certain conventional armored applications is the allowable road weight that limits the numbers of encased missiles from being transported together. Due to the strict road weight limits, the excessive load created by the combined weight of the missiles, truck, etc. allows for only a few (e.g., 1-4) missiles to be transported together. For example, the Department of Transportation (DOT) has established that the total road weight of a truck, including the weight of the load, cannot exceed 36.287 kg (80,000 pounds) per vehicle. It should of course be understood that different trucks have different weights, while the specific weight of the particular load, such as missiles to be transported and the respective container or canister, can vary depending on the nature of the type of missile at issue. Typically, the combined weight of a single missile and the respective canister may be about 3.402 kg (7,500 pounds). Nevertheless, the combined weight of the truck and the missiles being transported which comprise the respective load cannot exceed 36.287 kg (80,000 pounds). Consequently, the missiles are oftentimes unprotected (i.e., lack a protective structure) in order to maximize the number of missiles that are transported together while also meeting the strict road weight limits

or only have the standard protective canisters without additional protective means. Oftentimes, the excessive load caused by the combined weight of the missiles and storage protective canister allows for just one, or at most two, missiles to be transported together. In the event more missiles are transported, such as 3-4, the transport might be done in a manner without any additional protection in which case the missiles are vulnerable to attack. To achieve the requirement of not exceeding the 36.287 kg (80,000 pound) load limit, the protective system of the present invention in an embodiment may be provided at a weight in the range of about 87,9 - 146,5 kg/m² (18 - 30 lb. / square foot (psf)). However, it should be appreciated that the specific weight per m² in accordance with the present invention depends on the specific nature of the application type with which the present invention is employed.

[0007] Another disadvantage with conventional armor systems in the case of armor systems employed as protection for vehicles is that the excessive weight of the armor systems can tend to render the vehicles relatively immobile, or at least significantly slower. This in turn can tend to cause the vehicles to be more vulnerable to attacks by high velocity and high caliber projectiles, and more significantly more vulnerable to attack, and even more significantly more vulnerable to repeated attacks by projectiles or fragments of projectiles.

[0008] In some known applications, the armor or armor systems is incorporated into the structure that is to be protected. Such applications can include military vehicles, armored vehicles or missile storage canisters. In such applications, it is typically not possible for the armor or armor systems to be temporarily applied but rather are aspects of the structure. In this regard, the armor systems could be difficult to replace in the event of damage or failure.

[0009] Projectiles, such as armor piercing ammunition, are designed to specifically penetrate conventional armor and armor systems. Conventional ceramic-faced armor systems were consequently developed to defeat armor piercing ammunition. For example, at impact, the projectile can be blunted or otherwise damaged by the conventional ceramic-faced armor system. At the same time, cracking or other damage to the conventional ceramic-faced armor system is inevitable which leads to a weakening of the integrity of the conventional ceramic-faced armor system and thus more vulnerable to future attacks.

[0010] Some specific examples of conventional prior art armor and armor systems are now set forth below.

[0011] Document US 2009/0320676 A1 is directed to the use of an armor for protection against projectiles having a ceramic layer with a confinement layer on the front thereof. The ceramic layer is backed by a first metallic layer and the first metallic layer in turn is backed by a composite layer. The composite layer is backed by a second metallic layer, which in turn is backed by an anti-trauma layer.

[0012] Document W0 91/00490 A1 discusses a composite ballistic article comprising at least one hard rigid layer, at least one fibrous layer and a void layer between the rigid layer and the at least one fibrous layer. The relative weight percents of the hard rigid layer and the fibrous layer(s), and the relative positions of the layers are such that the article is said to exhibit a mass efficiency equal to or greater than about 2.5.

[0013] Document US 4 061 815 A discusses a laminated sheet material having high impact resistance for use in with armor plates. One or more layers of cellular or non-cellular polyurethane is sandwiched between a rigid, high impact resistant sheet of material, such as aluminum armor plate and fiberglass, in the one face and a thin retaining skin on the other. A filler, such as ceramic, particulate refractory or strip metal, can be embedded in the polyurethane layer(s).

[0014] Document US 2010/0212486 A1 discusses a strike plate including a base armor plate having an outwardly facing surface and a hard layer deposited on the base armor plate to substantially overlay the outwardly facing surface. A ballistic attenuation assembly is allegedly provided having multiple sheets of a first fibrous material and a sheet of a second fibrous material laminated together by a modified epoxy resin with the first sheet of a second fibrous material being exposed along an outward facing surface. An alternative ballistic attenuation assembly is also discussed having a first panel having opposed inward and outward facing surfaces, a second panel having opposed inward and outward facing surfaces, and a spacer interposed between the first and second panels forming a gap between the inward facing surfaces of the first and second panels.

[0015] Document US 5 200 256 A discusses an armor lining for protecting objects from high velocity projectiles having an extended sheet-like body having a weight of less than eight pounds per square foot and having an inner strike surface being positioned away from the object to be protected. A first layer of woven fabric material is carried at a position adjacent the outer strike surface layer and a second layer of material is carried internally of the woven layer between the outer strike surface and an inner attachment surface. A third layer of energy absorbent material is positioned adjacent the inner attachment surface and interfaces with the second fabric layer.

[0016] Document US 2009/0293709 A1 discusses an armor system for protecting a vehicle from high energy projectiles having a leading layer, relative to the projectile trajectory, positioned exterior to the hull, a first plurality of sheet-like layers of a low density material positioned between the leading layer and the hull; and a second plurality of sheet-like high strength metal layers positioned between the leading layer and the hull. The individual ones of the first plurality of high strength metal layers are positioned alternating with and to the rear of individual ones of the second plurality of low density material layers. The leading layer can be one of a sheet-like metallic layer, a metalized grid layer, and the outer-most layer of the first plurality of low materials layers. The materials of the high strength metal layers can be steel and high strength aluminum, and the materials of the low density material may be low density polypropylene composites

and R-Glass composites.

[0017] Document US 2010/0294123 A1 discusses a modular armor system having a leading layer with a metal and an intermediate sheet-like layer of a low density material lesser than that of metal, abutting a rear surface of the leading layer. The armor system also has an intermediate sheet-like layer having glass fiber material and abutting a rear surface of the intermediate low density material layer, and an intermediate sheet-like layer having metal and abutting a rear surface of the intermediate glass fiber layer.

[0018] Document US 4 836 084 A discusses an armor plate composite having four main components, namely, a ceramic impact layer, a sub-layer laminate, a supporting element and a backing layer. The ceramic layer serves for allegedly blunting the tip of a projectile. The sub-layer laminate of metal sheets alternate with fabrics impregnated with a viscoelastic synthetic material for absorbing the kinetic energy of the projectile by plastic deformation. The backing layer away from the side of impact consists of a pack of impregnated fabrics.

[0019] Document US 2006/0065111 A1 discusses an armor system having an outer case of woven or unidirectional fibers filled with one or more protective materials. The outer case includes a pressure sensitive adhesive bonded to one side for allegedly quick and easy application to a body to be protected. The protective materials may include ceramic material which may be in the form of ceramic tile sheets, loose ceramic balls or perforated tiles, multiple layers of woven or unidirectional cloth and steel mesh.

[0020] With reference to Figure 1, an example of a conventional prior art protective system for transporting missiles is shown and referenced generally at numeral 1. As shown in Figure 1, the conventional prior art system includes a flatbed trailer 10 having a standard dimension of about 16,15 m x 2,59 m (53' x 102") and a set of missiles (not shown) inside a corresponding protective canister 12. Protective canister 12 may comprise any missile protective material known in the art, such as steel. A frame 14 is provided for securing each canister 12 to the flatbed trailer 10. Frame 14 may comprise any material conventional in the art, such as wood or steel. As depicted in Figure 1, the conventional prior art system for the transport of missiles inside protective canisters 12 lacks any additional type of protective structure since an additional protective structure that would provide sufficient protection to the canisters 12 would be too heavy to comply with STANG 4241 and STANAG 4496 requirements and thus would cause the weight of the entire load to exceed 36.287 kg (80,000 pounds). Therefore, an additional protective structure cannot be employed and the missiles must be transported in a vulnerable manner as shown in Figure 1.

[0021] Document US 2014/0013934 A1 on which the preamble of claim 1 is based discloses a lightweight ballistic armor system for protection against projectiles comprising: at least one metal strike face plate comprising a plurality of slotted holes; a laminate composite backing material secured to said metal strike face plate, wherein said metal strike face plate includes a proximate metal strike face plate that is proximate to said laminate composite backing material, said proximate metal strike face plate and said composite backing material being separated by a space to define a maximum distance of 30,48 cm, wherein said metal strike face plate is a perforated metal, and wherein said metal strike face plate comprises at least one material selected from the group consisting of steel, perforated hardened steel, steel alloys, aluminum, magnesium and titanium, wherein said plurality of slotted holes are selected from the group consisting of angled slotted holes and straight slotted holes, wherein said plurality of slotted holes are set at an angle in a range of 0° - 60° relative to the vertical orientation of said metal strike face plate, and wherein said laminate composite backing material comprises a thickness in the range of 0,254 cm to 10,16 cm (0,1 to 4 inches).

[0022] Document US 2009/095147 A1 discloses an armor panel system including a strike face assemblage formed of a high-hardness material which is bonded to a fiber reinforcement. The high-hardness material is formed as "discrete elements" or "tiles". Furthermore, this conventional system includes a support plate and a containment element which are fixed together by a fastening structure such as stitching, clamps or bolts.

[0023] Finally, document US 2004/216595 A1 discloses an armor assembly, wherein a metallic armor assembly includes a metallic facing element with a plurality of perforations, an adhesive layer, and a composite fiber backing. Moreover, the assembly includes an encapsulating cover for encapsulating the whole assembly structure.

[0024] It is an object of the present invention to provide a lightweight ballistic armor system, a body armor system, an armored vehicle system, a missile canister armor system and an armored structures system which is robust against extreme temperatures, humidity, thermal shock, fluids, radiation, fungus etc. while still being light weight and having good protection capabilities.

SUMMARY OF THE INVENTION

[0025] According to the present invention this object is achieved by the characterizing features of the independent claims 1, 10, 11, 12, and 13.

[0026] The dependent claims define advantageous embodiments of the present invention.

[0027] It is to be understood that both the foregoing general description and the following detailed description are exemplary and explanatory only and are intended to provide a further explanation of the present invention, as claimed.

BRIEF DESCRIPTION OF THE DRAWINGS**[0028]**

Figure 1 is a perspective view of a prior art missile container transport system.
 Figure 2 is a perspective view of an example of an armor system.
 Figure 3 is a perspective view of a further example of an armor system.
 Figure 3A is a cross-sectional view of the example of the armor system as shown in Figure 3.
 Figure 3B is a perspective view of the example of the armor system as shown in Figures 3 and 3A.
 Figure 4 is a front view of an example of a perforated metal strike face plate.
 Figure 5 is an exploded schematic view of a portion of the perforated metal strike face plate as shown in Figure 4.
 Figure 5A is a cross-sectional view of a portion of the perforated metal strike face plate taken in the direction 5A-5A in Figure 5.
 Figure 5B is a schematic view of a portion of the perforated metal strike face plate taken in the direction B-B in Figure 5.
 Figure 6 is a cutaway cross-sectional view of an example of the metal strike face plate.
 Figure 7 is a cutaway cross-sectional view of an alternative example of a metal strike face plate.
 Figure 8 is a perspective view of a further example of a metal strike face plate.
 Figure 9A is a cross-sectional view of an example of the layers of an armor.
 Figure 9B is a cross-sectional view of an alternative example of the layers of an armor system.
 Figure 10 is an exploded perspective view of an example of an armor system in an exemplary application of use thereof being a missile transport system.
 Figure 11 is a rear view of the armor system in an example application of use as shown in Figure 10.
 Figure 12 is an exploded perspective view of a frame system for use with the armor system in an example application of use as shown in Figure 10.
 Figure 13 is a perspective view of a flatbed truck trailer for use with the armor system in an example application of use as shown in Figure 10.
 Figure 14 is a perspective view of the armor system in an alternative example application of use.
 Figure 15 is a schematic drawing of a test configuration of the present invention.
 Figure 16 is a schematic drawing of a bullet impact instrumentation configuration of the present invention.
 Figure 17 is a schematic drawing of the gun barrel arrangement of the test configuration of the present invention.
 Figure 18 is a schematic drawing of the velocity screen arrangement of the test configuration of the present invention.
 Figure 19 is a perspective schematic drawing of the plate arrangement of the test configuration of the present invention.
 Figure 20 is a schematic drawing of the plate projectile impact locations of the test configuration of the present invention.
 Figure 21 is a schematic drawing of the post-test plate condition of the test configuration of the present invention.
 Figure 22 is a schematic drawing of the test plate shown secured to the target stand of the test configuration of the present invention.
 Figure 23 is a schematic drawing of the projectile impact locations of the test configuration of the present invention.
 Figure 24 is a schematic drawing of the post-test plate condition of the test configuration of the present invention.
 Figure 25 is a schematic drawing of the witness plate of the test configuration of the present invention.
 Figure 26 is a schematic drawing of a fragment impact test configuration of the present invention.
 Figure 27 is a schematic drawing of the fragment impact test instrumentation configuration of the present invention.
 Figure 28 is a schematic drawing of the fragment impact target points.
 Figure 29 is a schematic drawing of the test plate configuration pre-fragment impact test of the present invention.
 Figure 30 is a schematic drawing of the test plate post-fragment impact test of the present invention.
 Figure 31 is a schematic drawing of the witness plate post-fragment impact test of the present invention.
 Figure 32 is a schematic side view of the plate configuration during the fragment impact test of the present invention.
 Figure 33A is a schematic side view of the plate configuration post-fragment impact test of the present invention.
 Figure 33B is a schematic side view of the witness plate post-fragment impact test of the present invention.
 Figure 34 is a perspective view of a semi-truck trailer for use with an armor system wherein the armor system is integrally formed within the parameters of the flatbed truck trailer.
 Figure 35 is a perspective view of an example not forming part of the present invention.
 Figure 36 is a perspective view of the embodiment in accordance with the present invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0029] The present invention is now described with reference to the drawings, wherein like reference numerals are

used to refer to like elements throughout. In the following description, for purposes of explanation, numerous specific details are set forth in order to provide a thorough understanding of the present invention. It will be evident, however, to one skilled in the art that the present invention may be practiced without these specific details.

[0030] Turning now to Figures 2, 3, 3A and 3B, the armor system according to a first example (Figure 2) and a second or alternative example (Figure 3) is shown generally at numerals 100 and 200, respectively. It should be understood that the armor system as described herein may be employed for use in an armor trailer system, or alternatively for use as body armor, missile canisters or with a vehicle including for use with the body of a vehicle or portions thereof, as described below. Armor systems 100 and 200 both comprise a perforated metal strike face plate 110, 210 and a laminate composite backing 120, 220. It should be appreciated that multiple layers of both metal strike face plate and/or laminate composite backing may be employed in accordance with the present invention. However, for purposes of explanation a single layer of both metal strike face plate and laminate composite backing is shown and described herein. It should also be appreciated that any type, configuration, design or style of metal strike face plate (i.e., tipping plate) may be employed with the present invention as known in the art. However, for purposes of explanation, particular versions of the metal strike face plate (i.e., tipping plate) are shown and described herein. The term "metal strike face plate" refers to a high strength metal that has a front face surface that would receive the initial impact of a projectile or shock waves or material from a blast. The back surface of the metal strike face plate can be adjacent to the front surface of the laminate composite backing in an example not forming part of the present invention. In other words, the perforated metal strike face plate provides a ballistic strike face which is the first layer of the ballistic armor or armor system that is struck by a projectile or fragment. The perforated metal plate 110, 210 fractures and/or rotates the projectile or fragment. In accordance with the present invention, metal strike face plate 110, 210 is provided at a thickness in the range of about 0.254 - 3.81 cm (0.10 - 1.5 inches) or even 0.635 cm - 3.81 cm (0.25 inch - 1.5 inches). More particularly, in accordance with the present invention, metal strike face plate 110, 210 is provided at a thickness in the range of about 0.38 cm to 1.27 cm (0.15 inch to 0.50 inch) or even 1.27 cm - 1.59 cm (1/2 inch - 5/8 inch). It should be appreciated that the particular thickness of metal strike face plate or plates 110, 210 depends on the specific application with which the present invention is employed as discussed below.

[0031] Perforated metal strike face plate 110, 210 may be a material that is for example, but not limited to, steel or steel alloys, hardened steel, cast irons, aluminum, magnesium, titanium and the like, or a combination thereof. In an embodiment, strike face plate 110, 210 may comprise a cast iron material such as a cast steel material, i.e., ductile cast iron. It should be appreciated, however, that metal strike face plate 110, 210 can be any buffer plate of a high strength material that receives impact or impact-induced stress waves prior to a shock-absorbing element. In this regard, metal strike face plate 110, 210 can alternatively be a flat sheet of a high strength metal. It should be appreciated that any wrought iron plate or casting in accordance with MIL-PRF-32269 would be in accordance with the present invention. In particular, it should be appreciated that MIL-PRF-32269 provides that 4130 steel alloy and 4330 steel alloy are acceptable alloys for cast perforated plate (Class 2 armor), that MIL-A-12560 rolled homogenous steel (Class 1a armor) and MIL-A-46100 high hard rolled homogenous steel armor (Class 1b armor) is acceptable for imparting a hole pattern into to make perforated plate. These are examples of perforated material types which are qualified to date and are by no means comprehensive. It should be appreciated by the skilled artisan that other candidate alloys for making cast perforated plates may exist.

[0032] In an alternative example, a composite layer or metal skin layer 211 may optionally cover the perforated metal strike face plate 210 as shown in Figures 3 and 7. Composite layer or metal skin layer 211 is depicted only in the example of Figure 3 (i.e., armor system 200), but it should be appreciated that composite layer or metal skin layer 211 may be employed with the example as shown in Figure 2 as well (i.e., armor system 100) or any other example of the present invention as discussed below. It should also be appreciated that composite layer or metal skin layer 211 covers the entire front surface of metal strike face plate 210, but only a cut-away portion of composite layer or metal skin layer 211 is depicted in Figure 3 for illustrative purposes only. The optional, thin metal skin layer provides reinforcement protection against any projectile effect and aids in the breakup of a projectile striking armor systems 100 or 200. The optional, thin metal skin layer also facilitates cleaning and painting of perforated metal strike face plate 210.

[0033] In accordance with the present invention, composite layer or metal skin layer 211 may be a material that is the same as or different from the material of metal strike face plate 210. As understood from Figure 3, composite layer or metal skin layer 211 comprises a thickness that is relatively thin and is thinner than the thickness of metal strike face plate 210. In particular, composite layer or metal skin layer 211 can comprise a thickness in the range of from about 0.079 cm to 0.635 cm (1/32 inch to 1/4 inch), or even 0.317 cm to 0.635 cm (1/8 inch - 1/4 inch).

[0034] As shown in Figures 2-5, metal strike face plate 110, 210 comprises a plurality of slotted holes 130 (230 in Figure 3) which are set at an oblique angle relative to the vertical orientation of perforated metal strike face plate 110, 210. Plurality of holes 130, 230 of perforated metal or expanded metal strike face plate 110, 210 is preferably produced by a casting method, a punching method, or by an additive manufacturing method which should be understood by those skilled in the art. Alternatively, plurality of holes 130, 230 can be produced in perforated metal strike face plate 110, 210 via a water jet, laser, or plasma cutting method.

[0035] As shown in Figure 6, a cutaway cross-sectional view of perforated metal strike face plate 110 is provided along line a - a' of Figure 8. As depicted in Figure 6, perforated metal strike face plate 110 comprises a plurality of oblique-angled holes or slots. Still referring to Figures 2 and 3, metal strike face plate 110, 210 comprises a plurality of holes or perforations 130, 230. As shown in Figure 4, plurality of holes 130 is uniformly distributed along the entire front face of strike face plate 110. Holes 130, 230 may comprise any configuration conventional in the art, such as but not limited to circular, rectangular, oblong, rectangular or of any polygon shape (or different shapes), or any combination thereof, and can be created in the solid plate by any mechanism conventional in the art, such as punching, casting, water jet, laser or plasma cutting. Plurality of holes 130, 230 may be perpendicular to or provided at any angle relative to the front surface of strike face plate 110, 210 and may be oriented upwardly or downwardly, or by any other orientation conventional in the art. Plurality of holes 130, 230 may be arranged in a repetitive manner in two planes that form webs 132 (Figure 5) whose width and thicknesses can be varied as necessary, but are uniformly distributed throughout. Perforated metal strike face 110, 210 and laminate composite backing 120, 220 may be flat, bent or formed into compound angles. It should also be understood that the plurality of holes or slots are not limited to being oblique, but may alternatively be straight (i.e., non-oblique) in accordance with the present invention. For example, multiple layers of perforated metal may alternatively be employed in accordance with the present invention in a desired embodiment, wherein the plurality of slots or holes are straight (i.e., non-oblique). In this instance, the multiple layers of perforated metal and/or the configuration of the respective plurality of holes or slots may be advantageously offset. For example, multiple layers of perforated metal plates could be simultaneously employed with each having an individual thickness of about in the range of 0,635 cm to 0,953 cm (¼ inch - 3/8 inch) such that the overall thickness of the multiple layers of perforated metal plates would be consistent with the desired constant overall thickness if a single perforated metal plate had been employed.

[0036] The sizes of the openings of the slots which may be advantageously used in embodiments of the present invention range from about 0,381 cm to 5,08 cm (0.15 inch to about 2 inches) in length, or even about 1,27 cm to 5,08 cm (0.50 inch to about 2.0 inches) in length for an embodiment (i.e., the vertical orientation of the openings of the slots), by about 0,381 cm to 5,08 cm (0.15 inches to about 2 inches), or even about 0,635 cm to 2,54 cm (0.25 inch to about 1.0 inch) in width for an embodiment in width (i.e., the horizontal orientation of the openings of the slots). The web 132, defined as the solid material between the plurality of slots or holes 130, 230 can vary in thickness from about 0,254 cm to 2,54 cm (0.10 inches to 1 inch) (i.e., the spacing between adjacent slots or holes). It should be understood that the spacing between each hole or slot of the plurality of holes or slots may advantageously be consistent there-between, but need not be consistent there-between. The number of slots, for example, per square foot, may be within the range of about 161 to 7317 slots/m² (15 to 680 slots/square foot). This number, however, may be left for the skilled artisan to determine depending on the nature of the particular application with which the present invention is employed. Slots or holes 130, 230 are preferably arranged in a uniformed fashion and are equally spaced apart from each other. Moreover, the slots of the present invention are set in obliquity of up to about 60 degrees, such as from 0 degrees to 50 degrees measured from a vertical orientation or axis. For example, plurality of holes that are designed for use with protecting against 30 caliber bullets would be approximately half the size of the plurality of holes that are designed for use with protecting against 50 caliber bullets. In a particular embodiment in accordance with the present invention in which holes comprise a substantially oval-shaped configuration defined by two opposing arced ends, the distance between the respective focal points (shown by opposing "F's") of the opposing arced ends is about 1,27 cm (½ inch) and the angle of each opposing arced end is about 0.17 - 0.19°, in particular about 0.1875° (Figures 5A, 5B) with each hole angled at about 20°-30° relative to the vertical orientation of the present invention, and more particularly at about 25° relative to the vertical orientation of the present invention. It should also be appreciated that the number, size, arrangement, angle, and the like of the holes employed in accordance with the present invention may depend on the use of perforated metal for the strike face plate, and which may be left for the skilled artisan to determine depending on the nature of the particular application with which the present invention is employed.

EXAMPLE

[0037] The armor of an example may be produced and represented by the following: Styrofoam master sheets having a thickness of about 1,27 cm (0.50 inches) and dimensions of about 35,56 cm (14 inches) by about 76 cm (30 inches) are used. The styrofoam sheets have slots in a regular pattern produced from a die and the slots have the dimensions of 1,587 cm (0.625 inches) by 4,127 cm (1.625 inches) on 1,587 cm (0.625 inch) vertical centers and 4,127 cm (1.625 inch) horizontal centers. These slots are set at an obliquity of 30 degrees relative to a vertical orientation or axis. The web, defined as the solid material between the slots, is about 0,381 cm (0.150 inches) in thickness.

[0038] As shown in Figures 2 and 3, plurality of holes 130, 230 are provided in a pattern referred to as the "historic" pattern. It should be appreciated that any pattern of plurality of holes 130, 230 conventional in the art may be employed in accordance with the present invention. For example, in a particular example, plurality of holes 130, 230 can be provided in a non-homogenous cross-sectional pattern.

[0039] With specific reference to Figure 7, an alternative example of the perforated metal strike face plate 210 having thin metal skin 211 over the facing of perforated metal or expanded metal strike face plate 210 is provided. Plurality of holes 230 is shown having an oblique-angled configuration relative to a vertical orientation or axis. In particular, plurality of holes 230 may comprise an oblique-angle configuration of about between 20°- 60° relative to the vertical orientation of the metal strike face plate 210. More particularly, plurality of holes 230 may comprise an oblique-angle configuration of about 25° relative to the vertical orientation of the metal strike face plate 210. Of course, plurality of holes 230 may even be straight. Onto composite layer or metal skin layer 211, a further optional hard surface material 212 can be placed. The additional hard faced material 212 may be composed of carbon cloth, tungsten carbide particles, FeCr coating, FeCr-/Mo/V surfacing, 1642 CrC surfacing or Ceramo Cr₇Cr₃ surfacing and can be employed to provide an additional protective layer. The hard faced material may be sintered to the thin composite layer or metal skin layer 211 during the casting process and aids in the breakup of a high caliber projectile.

[0040] With reference to Figures 2 and 3, armor system 100, 200 further comprises laminate composite backing 120 (220 in Figure 3). Laminate composite backing 120, 220 can comprise a cross-sectional composition of fibers such as, but not limited to, at least one of a synthetic aramid fibers or para-aramid fibers known as KEVLAR® fibers, E-glass, S-Glass, polypropylene, Ultrahigh Molecular Weight Polyethylene (UHMWPE), including fibrous UHMWPE such as a pressed SPECTRA SHIELD II® SR-3130 ballistic composite material from Honeywell Advanced Fibers and Composites, Colonial Heights, Virginia, and integrally combined with polymer resin-based binders such as, but not limited to, at least one of silicones, epoxies, urethanes, polyethylenes, polyurethanes, and polyureas. In accordance with the present invention, polymer resin-based binders such as, but not limited to, at least one of silicones, epoxies, urethanes, polyethylenes, polyurethanes, and polyureas may be those sold under the trademark HOTBLOX® which may be readily obtained from American Technical Coatings, Inc. located in Cleveland, Ohio. In accordance with examples, laminate composite backing 120, 220 comprises a thickness in the range of about 0,635 cm (¼ inch) to about 12, 7 cm (5 inches), and in particular in the range of about 2,54 cm to 10,16 cm (1-4 inches), or even about 0,635 cm - 10,16 cm (0.25-4 inches). More particularly, laminate composite backing 200 comprises a thickness of about 1,27 cm - 7,62 cm (0.5-3 inches), or even about 6,35 cm (2.5 inches), in accordance with the embodiment of the present invention. It should be appreciated, however, that the particular thickness of the laminate composite backing depends on the particular type of application with which the present invention is used. For example, use of the laminate composite backing in an armor system according to the present invention would be comparatively thinner for use with body armor than for use with, for example, an armor system for protecting vehicles or missile transport canisters.

[0041] In accordance with an example of the present invention, laminate composite backing 120, 220 can comprise a layered configuration of cross-sectional composition of fibers such as, but not limited to, at least one of synthetic aramid fibers or para-aramid fibers known as KEVLAR® fibers, E-glass, S-Glass, polypropylene, Ultrahigh Molecular Weight Polyethylene (UHMWPE), such as a plurality of layers of standard ballistic cloth based on a UHMWPE known under the trademark DYNEEMA®, and integrally combined with polymer resin-based binders such as, but not limited to, at least one of silicones, epoxies, urethanes, polyethylenes, polyurethanes, and polyureas. In accordance with the present invention, polymer resin-based binders such as silicones, epoxies, urethanes, polyethylenes, polyurethanes, and polyureas may be those sold under the trademark HOTBLOX® which may be readily obtained from American Technical Coatings, Inc. located in Cleveland, Ohio as discussed above. A bottom layer, side layers and a top layer of a polymer resin-based binder material such as a silicone, epoxy, polyurethane, urethane and/or poly-urea, such as those sold under the trademark HOTBLOX® readily obtained from American Technical Coatings, Inc. located in Cleveland, Ohio, are provided for encasing the layered configuration comprising the laminate composite backing 120, 220. The layered configuration comprising the laminate composite backing 120, 220 is treated under pressure, such as in the range of about 13,79 MPa - 24,13 MPa (2,000 psi - 3,500 psi) for a period of time as needed, such as in the range of between ½ hour - 10 hours, and preferably in the range between 1 - 5 hours, to arrive at an appropriate laminate composite backing for use with the protective system of the present invention.

[0042] Alternatively, the optional encasing or encapsulation in accordance with an example may be replaced by employing an environmentally insensitive layer or wrap, such as a polymer layer, sheet, or encasing (e.g., polypropylene) or a metal layer, sheet, or encasing (e.g., aluminum, titanium, and the like). One such example not forming an embodiment of the present invention is shown generally at numeral 700 in Figure 35. As shown in Figure 35, armor system 700 includes a layered configuration of perforated metal and composite backing 702, shown as adjacent to each other. An environmentally insensitive sheet or layer 704, comprising an appropriate material such as but not limited to a polymer (e.g., polypropylene) or a metal (e.g., aluminum, titanium, and the like) is applied directly onto at least one surface, such as the outwardly facing surface of layered configuration 702 exposed to external environmental conditions, or even all surfaces thereof (e.g., entirely wrapped). Environmentally insensitive sheet or layer 704 may be advantageously bonded or otherwise secured to layered configuration 702 by conventional methods known in the art, such as heat, pressure or bonding materials. It should also be understood that environmentally insensitive sheet or layer 704 could alternatively comprise an encasing to fully encase or enclose layered configuration. As shown in Figure 35, an optional molding, edging or frame 706 comprising a material such as but not limited to a glass epoxy composite (or a comparable con-

ventional protective material) may advantageously be provided around the outside edges of layered configuration 702 having sheet or layer 704 bonded or secured thereon for reinforcing layer 704 onto layered configuration 702. Of course, frame 706 may also be employed in the case of an environmentally insensitive material fully encases or wraps layered configuration 702. It should be appreciated that frame 706 is optional for providing additional reinforcement and/or ballistic characteristics to armor system 700.

[0043] Turning now to Fig. 36, the embodiment of the present invention is shown and described. As discussed above, the optional encasing or encapsulation in accordance with an example may optionally be replaced by employing an environmentally insensitive layer or wrap, such as a polymer layer, sheet, or encasing (e.g., polypropylene) or a metal layer, sheet, or encasing (e.g., aluminum, titanium, and the like). This embodiment armor system is shown generally at numeral 800 in Figure 36. As shown in Figure 36, armor system 800 includes a composite backing 802 having an environmentally insensitive sheet or layer 804, comprising an appropriate material such as but not limited to a polymer (e.g., polypropylene) or a metal (e.g., aluminum, titanium, and the like) applied directly onto at least one surface, such as the outwardly facing surface of layered configuration 802 exposed to external environmental conditions, or even all surfaces thereof (e.g., entirely wrapped). Environmentally insensitive sheet or layer 804 may be advantageously bonded or otherwise secured to composite backing 802 by conventional methods known in the art, such as heat, pressure or bonding materials. As shown in Figure 36, an optional molding, edging or frame 806 comprising a material such as but not limited to a glass epoxy composite (or a comparable conventional protective material) may advantageously be provided around the outside edges of composite backing 802 having sheet or layer 804 bonded or secured thereon for reinforcing layer 804 onto composite backing 802. It should be appreciated that frame 806 is optional for providing additional reinforcement and/or ballistic characteristics to armor system 800. As also shown in Fig. 36, armor system 800 also includes at least one layer of perforated metal 803 adjacent to composite backing 802 relative to the external environment at a distance as described above.

[0044] It should be appreciated that a process for encapsulating the laminate composite backing layer can be as follows. It should also be appreciated that the process for forming the laminate composite backing layer in accordance with the present invention would envision any alternative or modifications that would be apparent to one skilled in the art. In particular, a material in a liquid form is encapsulated around a fibrous bundle core in a manner conventional in the art. The liquid is solidified to form an encapsulating skin. The transformation from liquid may occur, for example, via solvent evaporation, chemical reaction, or cooling from a molten state or by any alternative comparable manner conventional in the art. For example, a two-component system which is liquid under normal ambient conditions without the addition of a solvent can be poured over the fibrous bundle core and the components solidify by a chemical reaction. Alternatively, a thermoplastic material can be melted and molded around the fibrous bundle core, i.e., by insert injection molding.

[0045] Regardless of the actual chemistry of the resin material, the preferred material properties of the resultant solidified optional encapsulating skin for the laminate composite backing in accordance with the present invention can be the following. In particular, thermoset elastomeric resins may be employed in accordance with the present invention as follows.

- Hardness, via ASTM D 2240: Shore 60A-60D, preferably 75A-55D;
- Ultimate Tensile Strength (psi), via ASTM D 412: 8,27 MPa - 62,05 MPa (1200-9000 psi), preferably 20,68 MPa - 55,16 MPa (3000-8000 psi);
- Modulus at 100% elongation (psi), via ASTM D412: 2,76 MPa - 15,17 MPa (400-2200 psi), preferably 4,82 MPa - 10,34 MPa (700-1500 psi);
- Modulus at 300% elongation (psi), via ASTM D412: 4,82 MPa - 34,47 MPa (700-5000 psi), preferably 6, 2 MPa - 27,58 MPa (900-4000 psi);
- Elongation-to-break (%), via ASTM D412: 150-1000, preferably 300-800.

Example

[0046] An example of the formulation can be as follows. It should be appreciated that the formation is not limited to this example, but would envision any alternatives or modifications that would be understood by one skilled in the art. A polyurethane that is made by the reaction of a multifunctional amine and a multifunctional isocyanate without the addition of a solvent is provided. More specifically, an oligomeric ether or ester with diamine functionality reacted with a diisocyanate is provided.

[0047] As discussed above, alternatively the bundle or layered composite configuration may be environmentally protected by pressing or wrapping protective layers of polypropylene or other comparable materials, such as metal, Kevlar, S-glass, and the like, around the bundle or layered composite configuration. Edges may be reinforced with glass epoxy composites or other comparable protective and/or reinforcement materials as shown in Fig. 36. It should therefore be understood that in accordance with the embodiment of the present invention, embodiments for lower weight systems of

the present invention may be advantageously used for example in connection with "on canister" ballistic systems for protecting missile canisters. In that case, it should be understood that such embodiments may include at least one metal strike face plate against a corresponding composite backing with or without a polypropylene or other protection layer and with or without a corresponding frame for reinforcing.

[0048] In an example, as discussed in greater detail below, a layer, sheet or board of a high tensile strength material, such as a high tensile strength polymer board, may be employed adjacent to laminate composite backing 200 at a thickness in the range of about 0,079 cm - 10, 16 cm (1/32 inch - 4 inches), or about 0,317 cm (1/8 inch) to about 10,16 cm (4 inches), or about 0,635 cm (¼ inch) to about 10,16 cm (4 inches), or even about 0,16 cm - 10,16 (1/16 inch - 4 inches) and more particularly at a thickness in the range of about 0,8 cm - 5,08 cm (1/32 inch - 2 inches). It should be appreciated that the thickness of the high tensile strength polymer board would depend on the specific requirements of the particular application with which the present invention is employed. High tensile strength polymer board may supplement the laminate composite backing 200, or replace at least a portion of the cross-sectional composition of the laminate composite backing 200.

[0049] As shown in the example in Figure 2, armor system 100 is provided with the metal strike face plate 110 and laminate composite backing 120 bonded together by bonding methods conventional in the art, such as by a urethane or polyurethane bonding. As shown in Figure 2, metal strike face plate 110 and composite backing 120 are bonded directly together with no air space there between. It should be appreciated that metal strike face plate 110 and laminate composite backing 120 could also be secured together via mechanical means conventional in the art, as discussed further below. Such a configuration may be employed, for example, for use of the present invention in a body armor type of application.

[0050] As shown in the example of Figures 3, 3A and 3B, armor system 200 is provided with an air space 300 between metal strike face plate 210 and laminate composite backing 220. According to the examples, air space 300 may be provided at a distance or depth in the range of about 0,635 cm to 12,7 cm or 15,24 cm (0.25 to 5 or 6 inches). More particularly, air space 300 may be provided at a distance or depth of about 0,634 cm to 5,08 cm (0.25 inches to 2 inches), or even about 13,02 cm (5 1/8 inches) to about 13,97 cm (5 ½ inches). It should be appreciated that the particular depth of the air space would depend on the particular type of application with which the present invention is employed, including no air space at all, i.e., air space having zero cm (inches) depth. In other words, armor system 200 may be devoid of air space 300 in an embodiment of the invention. Air space 300 may be optionally filled with a foam energy absorbing material, such as low density foam, or other comparable energy absorbing material as conventional in the art.

[0051] Turning now to Figures 9A and 9B, cross-sectional schematic diagrams of an example are shown and described. As shown in Figures 9A and 9B, the armor system according to an example may be employed for use as an armor system for missile transport canisters, for body armor, for the missile canisters, or for vehicles including for incorporation into the body of the vehicle or portion(s) of the vehicle body. With reference to Figure 9A, armor system is shown at numeral 100 comprising perforated metal plate 110 having plurality of holes 130, laminate composite backing 120 and air space 300 between perforated metal strike face plate 110 having plurality of holes 130 and laminate composite backing 120. Laminate composite backing comprises a thickness defined as thickness X, which may be for example about 0,635 cm - 12,7 cm (0.25 - 5 inches), or 0,635 cm - 10,16 cm (0.25 - 4 inches), or even about 6,35 cm (2.5 inches). With reference to Figure 9B, an alternative example of armor system is shown at numeral 100a comprising perforated metal plate 110a having plurality of holes 130a, laminate composite backing 120a and air space 300a between perforated metal plate 110a having plurality of holes 130a and laminate composite backing 120a. A sheet of material or board, shown at numeral 140a, may be provided on top of and adjacent to laminate composite backing 120a. Sheet of material or board 140a may be, but is not limited to, a high tensile strength urethane board having a defined thickness of y1. The defined thickness of laminate composite backing 120a is thus reduced as compared to the laminate composite backing 120 of Figure 9A and is shown at numeral y2. It should be appreciated that the defined thicknesses of sheet of material or board 140a and laminate composite backing 120a (Figure 9B) is substantially equal to the thickness of laminate composite back 120 (Figure 9A). In other words, the defined thicknesses of y1 + y2 = x depending on the particular application with which the present invention is employed. It should be appreciated that sheet of material or board 140a may be employed for partially replacing a desired thickness or amount of laminate composite backing 120a for reducing overall production costs while maintaining overall system strength, thickness and integrity. It should also be understood that multiple layers of perforated metal sheet may be employed, as discussed above, depending on a particular desirable application for the present invention with the overall thickness of the metal layer(s) being constant as desired for a particular embodiment regardless of whether a single-layer of perforated metal or multiple layers of perforated metal is/are employed.

[0052] In accordance with the examples of the present invention, the armor system of the present invention meets the appropriate military weight specifications and requirements for defeating high velocity and high caliber projectiles, or alternatively for disrupting/deflecting/dissipating the energy of small arms impact (i.e., a reduction of the energy of the small arms threat). In particular, the armor system of the present invention meets the appropriate military weight specifications and requirements as defined by NATO Standardization Agreement (STANAG) Bullet Impact, Munitions Test

Procedures promulgated on April 15, 2003 and NATO Standardization Agreement (STANAG) Fragment Impact, Munitions Test Procedures promulgated on December 13, 2006, both of which are incorporated herein by reference in their entireties. For example, the present invention meets the appropriate test of stopping, or alternatively slowing down (i.e., deflecting, disrupting, dissipating the energy of) three (3) 50-caliber bullets shot within a 2-inch diameter area and shot in a time interval of 1/10 second apart.

[0053] In accordance with an embodiment of the present invention, the armor system of the present invention comprises a weight in the range of about 87,9 - 180,9 kg/m² (18-35 psf) for use with missile canister protection systems. More particularly, in accordance with the present invention, the armor system comprises a weight of no greater than about 141,6 kg/m² (29 psf) in the embodiment in which the present invention is employed for use with a missile canister armor system. Even more particularly, in accordance with the present invention, the armor system comprises a weight of about 112,3 kg/m² (23 psf) in the embodiment in which the present invention is employed for use with a missile canister armor system. In accordance with the present invention, the respective weights meet those that are needed by the particular application of use with which the present invention is employed.

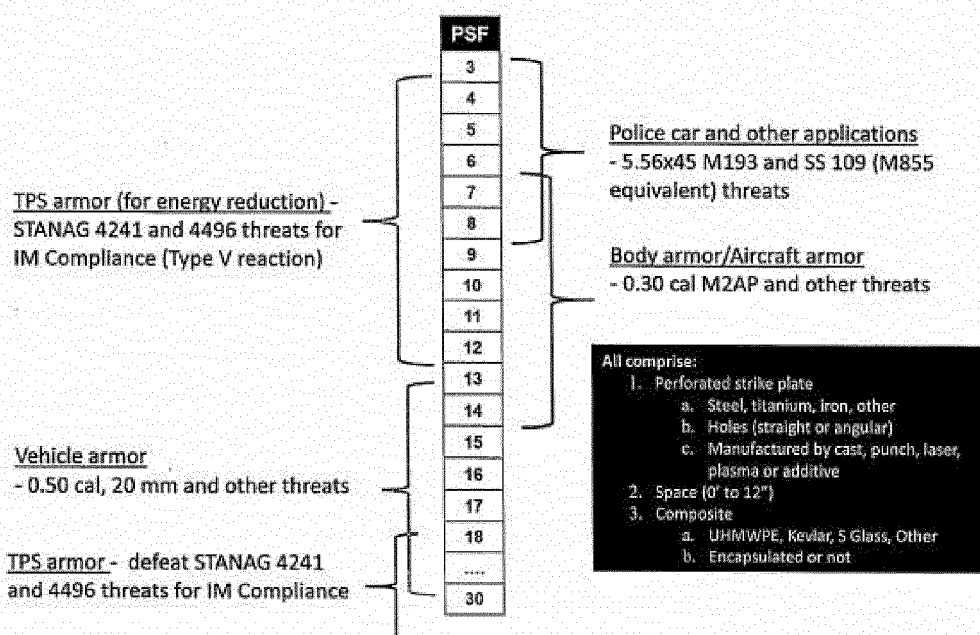
[0054] In an alternative embodiment, the lightweight armor system of the present invention comprises a weight of about 14,6 - 73,2 kg/m² (3-15 psf), including about 29,3 - 53,7 kg/m² (6-11 psf). More particularly, the lightweight armor system of the present invention comprises a weight in the range of about 34,2 - 53,7 kg/m² (7-11 psf), or even 34,7 - 52,7 kg/m² (7.1-10.8 psf), when employed with a metal strike plate, such as steel or titanium, for defeating, for example, 0.30 caliber armor piercing threats. In accordance with the present invention, the respective weights meet those that are needed by the particular application of use with which the present invention is employed.

[0055] In another alternative embodiment, the lightweight armor system of the present invention comprises a weight in the range of about 19,5 - 39,1 kg/m² (4-8 psf), or even about 24,4 - 29,3 kg/m² (5-6 psf), or more particularly about 27,3 kg/m² (5.6 psf), when employed with a hardened steel plate for defeating threats such as 5.56 X 45 M193 and SS 109 (M855 equivalent). In this instance, the embodiment of the present invention may be employed for use with vehicles, such as a material for forming at least a portion of the vehicle body, such as a police vehicle or military vehicle. In this embodiment of the present invention, Ultrahigh Molecular Weight Polyethylene (UHMWPE) may be advantageously employed as the component of the composite backing.

[0056] In another alternative embodiment, the lightweight armor system of the present invention comprises a weight in the range of about 13,5 - 43,9 kg/m² (4-9 psf), or even about 19,5 - 37,6 kg/m² (4-7.7 psf), or more particularly about 19,5 - 32,7 kg/m² (4.0-6.7 psf), or even more particularly in the range of about 21 - 30,7 kg/m² (4.3-6.3 psf) or still even more particularly about 19,5 - 26,9 kg/m² (4.0-5.5 psf), when employed for use as a missile canister for encasing and protecting missiles during transport. In this embodiment of the present invention, S-Glass may be advantageously employed as the component of the composite backing, such as for lowering flammability properties. As also discussed above, the fibers or composite material may be advantageously used to wrap the perforated metal plate directly. For use on a missile canister, it should be appreciated that, for example, the wrapped perforated strike plate can be used as a singular item for improving ballistic and/or environmental properties.

[0057] Chart 1 - Embodiments of different applications in accordance with the present invention. "TPS" meaning "transportation protection system". As shown in the below Chart, the overall weight of the perforated metal and composite backing psf (pounds per square foot) may vary with respect to the particular and specific desired need and application in accordance with the present invention.

CHART 1

5
10
15
20
25

[0058] As shown in Figure 3, a mechanical attachment mechanism 400 can be fabricated into the components 110 and 120 for attaching components 110 and 120 to each other and/or for attaching an armor system to another object to be protected, such as a vehicle, and which is employed with the specific application of use. For example, referring to Figures 6-8, metal strike face plate 110 comprises recessed pockets 42 through which tubular spacers 40, each having a threaded end 41 passes through. Metal strike face plate 110 is attached to a structure 13 to be protected (e.g., a vehicle) (Figure 8) through tubular spacers 40 by a washer 30 and nut 32. As shown in Figure 6, metal strike face plate 110 comprises an opening 45 through which tubular spacer 40 may be accommodated. In an example, mechanical attachment mechanism 400 may be a conventional threaded screw and nut engagement mechanism as known in the art.

[0059] Turning now to Figures 10-14, an exemplary use of the armor system in accordance with the present invention in connection with a particular type of application will be shown and described, namely for use with an armor system for the transport of missile canisters. It should be appreciated, however, that the specific application of the present invention shown in Figures 10-14 is for illustrative purposes only and the armor system of the present invention should not be considered limited or exclusive to such an application or use. As indicated above, the present invention may alternatively and advantageously be employed for use with body armor, missile canisters, or the vehicle body itself or a portion or portions of the vehicle body as within the scope of the present invention.

[0060] As shown in Figure 10, the armor system is shown generally at numeral 500. A flatbed truck trailer 510 is provided for carrying at least one missile canister 512. As shown in Figure 10, four missile canisters 512 are provided on flatbed truck trailer 510. A frame 514, such as a wooden or metal frame as known in the art, is provided for securing each individual canister 512 to flatbed truck trailer 510. Spacers 534, such as wood spacers or metal spacers, are provided on the floor of the flatbed truck trailer 510 to further ensure stability of canisters 512 (Figure 13). An additional frame system 516, such as an aluminum frame system (Figure 11) having a top frame 516a and side frames 516b, is provided for securing the armor system panels 518 to the side of the flatbed truck trailer 510 and totally surrounding the canisters 512 secured by frame 514. It should be appreciated that any comparable material to aluminum may be employed for frame system 516. As shown in Figure 11, each segment of frame system 516 contains or houses strike face plate 520 and laminate composite backing 524, with air space 522 therebetween, and regardless of whether the respective segment of frame system 516 is employed on a side, front, top or back of the trailer bed 510. Each segment of frame system 516 is employed in series so as to directly and securely abut the respective adjacent segment of frame system 516 to form a secure protective system in all directions surrounding the canisters 512, including top and all sides.

[0061] Referring to Figure 12, top frame 516a and side frames 516b of frame system 516 are secured to together via a mechanical locking mechanism. The mechanical locking mechanism comprises a plurality of upwardly angled hooks, forks or the like 530 on top frame 516a which secure into and lock with corresponding grooves, holes, pockets or the like on side frames 516b. Side frames 516b are directly secured to each armor system panel 518, such as via conventional

threaded bolt and nut securing mechanism or any other comparable mechanism conventional in the art. Straps 536 (Figure 14) may be employed to further stabilize canisters 512 in place on flatbed truck trailer 510.

Examples - Ballistic Testing

[0062] The Ballistic Barrier Test was conducted in order to test ballistic armored panels in accordance with the present invention.

STANAG 4241-0.50 Caliber Bullet Impact Test

[0063] The objective of the test was to impact each candidate plate in a specified quadrant with a volley of three 0.50-caliber armor-piercing (AP) projectiles, fired at 100 +/- 8 msec intervals from 0.50 caliber Mann barrel devices. The projectiles were required to have velocities of 849, 8 +/- 20,1 m/s (2788 +/- 66 ft./sec). These projectiles were to impact the specified plate quadrant within a 2-in circle, without key-holing or overlapping.

Test Item Configuration

[0064] The overall general test configuration is shown in Figure 15 and is discussed in greater detail below.

[0065] The instrumentation setup was as shown in Figure 16. A total of four Phantom cameras were used, and are described in Table 1 below.

TABLE 6- BULLET IMPACT TEST CAMERA SPECIFICATIONS

Camera	Type	Frame Rate	Resolution	Exposure Time	Purpose
A	Phantom 710	5,000 frames/s	1280 x 308	20 μ s	Projectile Velocity
B	Phantom 7.3	6,400 frames/s	800 x 600	3-10 μ s*	Witness Plate
C	Phantom 7.3	6,400 frames/s	800 x 600	3-10 μ s*	Target Front/Rear Face
D	Phantom 7.3	6,400 frames/s	800 x 600	3-10 μ s*	Target Front Face
* Adjusted for lighting conditions					

[0066] Figure 17 depicts the three Mann barrels (M1, M2 and M3) used in the testing of the present invention. The center muzzle distance to the target plate was approximately 9,0 m (29.6 feet). The guns were sequenced to fire at 100 msec intervals.

[0067] Projectile velocities were measured using Oehler infrared screens and high-speed video. The Oehler screen and Phantom high-speed camera setup was as shown in Figure 18.

Test Execution

[0068] Once the equipment was verified to be fully functional, and the projectile grouping was within a 5,08 cm (2-inch) circle, the target plate was secured to the test stand. The target plate consisted of a 1,587 cm (5/8-inch) perforated grate up-range and a 6,35 cm (2.5-inch) thick piece of composite down-range. The target panels were bolted to the test stand as shown in Figure 19. The distance from the perforated plate to the composite plate was approximately 13,02 cm (5 1/8-inches).

[0069] Three laser bore-sights were used to give an approximate visual reference as to where the Mann barrels were aimed. The point of impact was on the face of the perforated metal grate at the center of the lower-left quadrant as demonstrated in Figure 19.

[0070] Once the instrumentation was reset and shown to be ready, a volley of three .50 caliber armor-piercing projectiles was fired at the target. The projectiles impacted the plate within a 5,08 cm (2-inch) circle as shown in Figure 20. The aim point was approximately 6 inches from the left side of the grate and approximately 15,24 cm (6 inches) from the bottom of the grate.

[0071] As shown in Figure 21, the test panel according to the present invention prevented all three projectiles from impacting the witness plate.

[0072] Velocity data for this volley is shown in Table 2 below.

TABLE 7- PROJECTILE VELOCITY & INTERVAL DATA

	Oehler	Phantom	Projectile	Δ Time
	m/s	m/s	Weight	from HS
	([ft/s])	[ft/s]	[grains]	video
				[ms]
1	857	861	693	N/A
	(2812)	(2826)		
2	853	857	693	101
	(2797)	(2811)		
3	849	851	693	98
	(2786)	(2791)		

Additional Test Plate

[0073] Another target test plate in accordance with the present invention was secured in a similar fashion as the first test plate. In this additional test, the difference between the respective plates was that the former had a composite plate thickness of 4,44 cm (1.75 inches). This required the use of a 1,9 cm ($\frac{3}{4}$ -inch) standoff directly behind and down-range of the composite plate in order to maintain a plate separation of 13,02 cm (5 $\frac{1}{8}$ -inches) as shown in Figure 22.

[0074] A volley of three 0.50 caliber AP projectiles was fired at the target. Upon post-test inspection it was observed that projectile grouping and impact locations were similar to the initial test results as shown in Figure 23.

[0075] As shown in Figures 24 and 25, extensive damage was witnessed on the front side of the composite portion of the barrier (Figure 24). However, no damage was observed on the witness plate (Figure 25).

[0076] The velocity and firing interval data for the additional test plate armor system in accordance with the present invention is presented in Table 3.

TABLE 8- PROJECTILE VELOCITY AND INTERVAL DATA

	Oehler	Phantom	Projectile	ΔTime from
	m/s	m/s	Weight	HS video
	([ft/s])	([ft/s])	[grains]	[ms]
1	849	852	693	N/A
	(2787)	(2796)		
2	851	856	693	101
	(2792)	(2810)		
3	847	852	692	98
	(2782)	(2797)		

STANAG (NATO Standardization Agreement) 4496-Fragment Impact Test

[0077] The objective of the test was to impact each candidate plate in a specified quadrant with a single North Atlantic Treaty Organization (NATO) standardized fragment with a nominal mass of 18.6 grams, traveling at a velocity of 2530 +/- 91 m/s (8300 +/-300 ft/s).

[0078] The fragment was fired from a 40mm High-Performance Powder Gun, which is an electrically-actuated, mechanically-fired cannon. A schematic depiction of the test site is shown in Figure 26.

[0079] The instrumentation setup was as set forth as shown in Figure 27.

[0080] Multiple cameras were used and their types and settings are described in the following Table 4. Cameras C and D were redundant units for each other.

TABLE 9- 40MM CANNON CAMERA SPECIFICATIONS

Camera	Type	Frame Rate	Resolution	Exposure Time	Purpose
A	Phantom 7.3	6,400 frames/s	800 x 600	3-10 μ s*	Target Front/Rear Face
B	Phantom 7.3	6,400 frames/s	800 x 600	3-10 μ s*	Target Front/Rear Face
C	Phantom 710	12,000 frames/s	1280 x 224	2 μ s	Fragment Velocity
D	Phantom 710	12,000 frames/s	1280 x 224	2 μ s	Fragment Velocity
E	Phantom 7.3	6,400 frames/s	800 x 600	3-10 μ s*	Target Front Face
F	Video	28 frames/s	standard	N/A	Muzzle safety
* Adjusted for lighting conditions					

Test Execution

[0081] The same target fixture was utilized for both the bullet impact and fragment impact portions of the test. Mounting arrangements were identical, and a clean quadrant diagonally opposite of the previously targeted quadrant was used as illustrated in Figure 28.

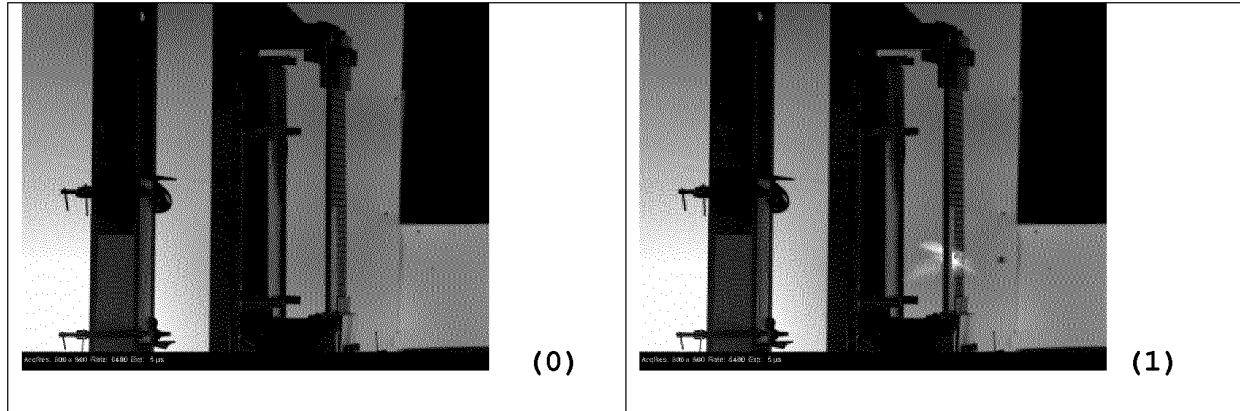
Test Plate

[0082] The test plate was secured to the target test stand as shown in Figure 29.

[0083] A post-test inspection revealed that the fragment impacted at the intended aim point as shown in Figure 30.

[0084] The test plate reactions during the fragment impact are shown in Table 5 along with the associated frame number, as set forth below.

TABLE 5 - FRAGMENT REACTION



5

10

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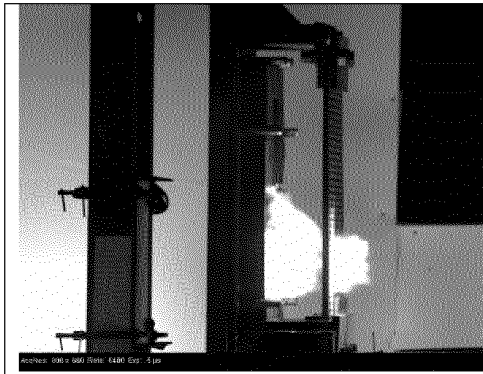
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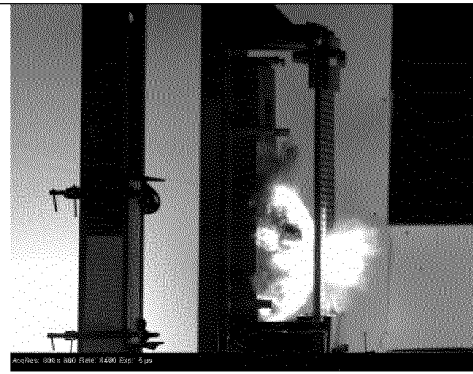
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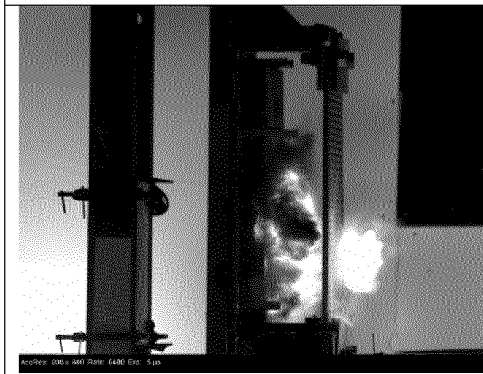
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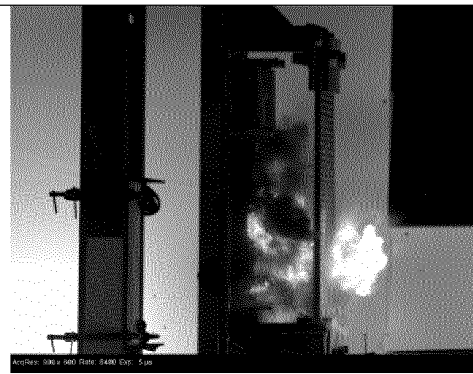
(2)



(3)



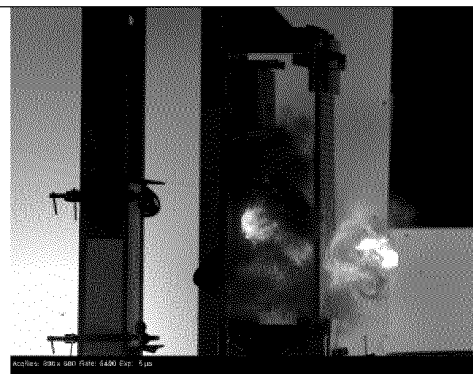
(4)



(5)



(6)



(7)

[0085] As shown in Figure 31, the witness plate showed no evidence of fragment penetration.

[0086] The fragment velocity was measured using one primary and one redundant Phantom camera. The fragment velocity data is presented in the following Table 5.

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50

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TABLE 10- FRAGMENT PROPERTIES

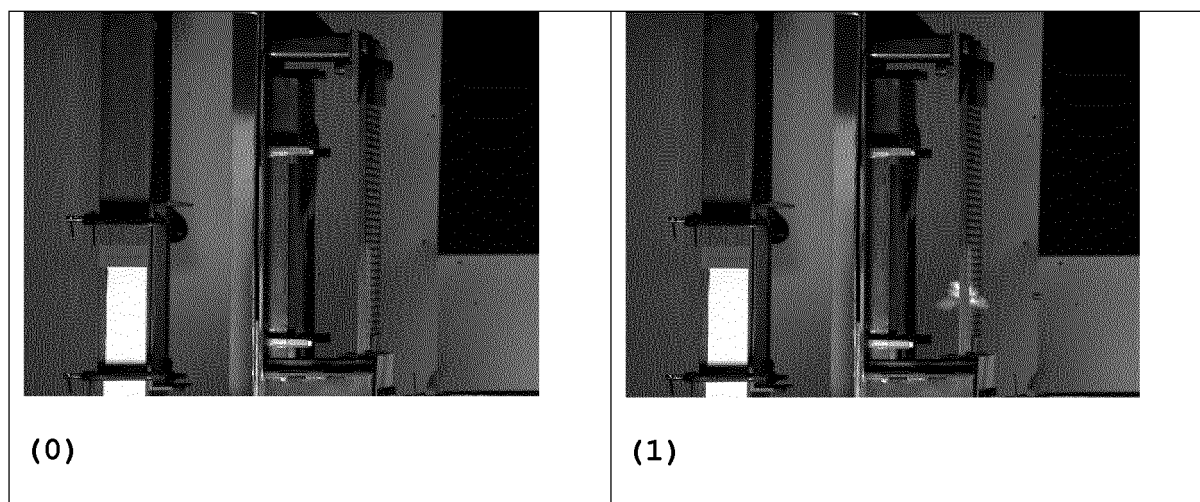
Shot	Phantom	Projectile
Number	m/s	Weight
	([ft/s])	[grams]
1	2508	18.5
	(8231)	

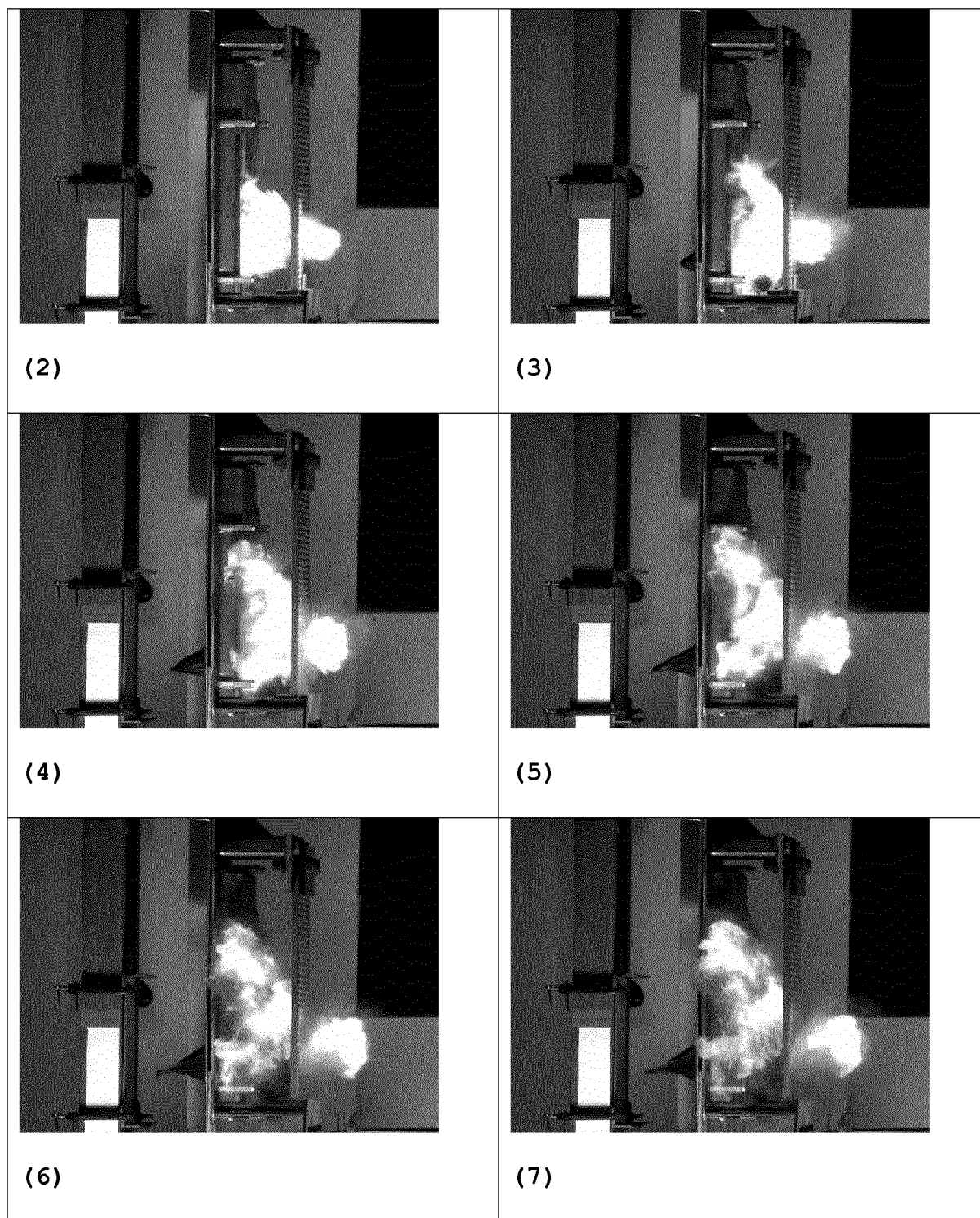
Additional Test Plate

[0087] The additional test plate in accordance with the present invention was installed with the same standoff used for the bullet impact portion of the test. A distance of 13,02 cm (5 1/8-inches) was measured from the back side of the grate to the face of the composite plate as shown in Figure 32.

[0088] The post-test inspection revealed a large amount of damage to the front of the composite plate and no damage to the witness plate, as shown in Figures 33A and 33B.

[0089] The reactions during the fragment impact are shown in the Table 6 along with associated frame number, as set forth below.

TABLE 6 - FRAGMENT REACTION



[0090] The velocity was measured using one primary and one redundant Phantom camera. The fragment velocity data is presented in the following Table 7.

TABLE 7 - FRAGMENT PROPERTIES

Shot	Phantom	Projectile
Number	m/s	Weight
	([ft/s])	[grams]
1	2501	18.6
	(8207)	

[0091] The tests were conducted in accordance with the approved test parameters. The projectile velocities and firing intervals for the bullet impact test were in accordance with STANAG 4241. The projectile velocity for the fragment impact test was in accordance with STANAG 4496.

[0092] It should be appreciated that the armor system in accordance with the present invention may be employed in any type of appropriate application for protection against high velocity and high caliber projectiles. Such applications for employment may include, but is not limited to, individual protective systems, i.e., body armor, armor for tanks, armor for ships or boats, armor for trucks, armor for vehicles, armor for aircraft including airplanes, jets and helicopters, armor for barriers, armor for protective structures, i.e., blast panels and armor for missile containers for storage or transport.

[0093] Turning now to Figure 34, an alternative example of the armor system will be shown and described, namely for use with an armored structure, such as an armored trailer or armored shipping container and the like in which the armor system is integrally built into the respective walls, floors and ceiling of the armored structure, such as an armored trailer or armored shipping container. For purposes of illustration, the armored structure as depicted in Figure 34 is an armored trailer. However, it should be appreciated that the armored structure is not limited to an armored trailer but can include other types of structures requiring an integral armor system including but not limited to an armored shipping container. It should be appreciated, however, that the specific example shown in Figure 34 is for illustrative purposes only and the armor system of the present invention should not be considered limited or exclusive to such an application or use. Moreover, it should be further understood that the incorporation of an armor system in accordance with the present invention into the parameters of an armored trailer is not limited in such a manner, but that incorporation of such an armored system into the parameters of other types of vehicles and/or structures are within the scope of the present invention.

[0094] As shown in Figure 34, the armored trailer system is shown generally at numeral 600. A flatbed semi-truck trailer 610 is provided and comprises a conventional configuration including two opposing walls 612a, 612b, a ceiling or roof 614, a rear end 616, a front end 618 and a floor 620 of the armored trailer system 600. It should be understood that armored trailer system 600 as shown includes a conventional rear end 616 that is configured for loading and unloading of cargo into and from armored trailer 610 in known conventional mechanisms. However, it should be understood that the armored trailer system 600 is not limited to such armored trailers for exclusive rear loading and unloading, but can also be employed with modified armored trailer systems which employ alternative methods for loading or unloading cargo conventional in the art including side loading and unloading systems or top loading and unloading systems or even combinations of the foregoing loading and unloading systems.

[0095] As shown in Figure 34, all of opposing walls 612a, 612b, ceiling or roof 614, rear end 616, front end 618 and, optionally, floor 620 comprise the armor system of the present invention discussed herewith integrally formed within the parameters of flatbed semi-truck trailer 610. In other words, the aforementioned described framework system is omitted in the instant alternative example and the ballistic armor system is employed directly and integrally into each of opposing walls 612a, 612b, ceiling or roof 614, rear end 616, front end 618 and, optionally, floor 620 thereby forming a singular and unitary armored trailer system 600 having the ballistic armor system of the present invention integrally formed into armored trailer system 600. It should be understood that in accordance with the embodiment shown in Fig. 34, alternative comparable structures may be employed such as but not limited to armored shipping containers, armored boxes, armored rooms, armored shelters and the like.

[0096] It should be understood that the armored trailer system 600 need not be limited to the particular application described herein of carrying cargo in the nature of missiles, but rather can be modified for protection of alternative types of cargo that might be less sensitive or less vulnerable. For example, the threats against an armored trailer for transport can be defined by the particular classes of weapons that are mobile, can be fired by an individual or individuals can

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engage a moving type target at a given range, including small arms to heavy machine gun threats, and fragments from roadside improvised explosive devices (IEDs). It should be further understood that kinetic energy threats, for example, can include but are not limited to threats ranging in caliber from about 5 mm - 15 mm, more particularly from about 5.45 mm to about 14.5 mm, in both steel and tungsten carbide cores. Still further, these threats can be fired from single and multiple shot assault weapons, sniper rifles and machine guns at near or extended ranges. Even further, it should be understood that the presently claimed armored trailer system 600 can protect against a second class of threats including but not limited to IED type weapons that can be simulated in testing by fragment simulating projectiles (FSP) in calibers up to 20mm in diameter.

[0097] In accordance with the present alternative embodiment of the present invention, the armored trailer system 600 of the present invention comprises a weight in the range of about 87,9 - 170,9 kg/m² (18-35 psf) for use with missile canister protection systems for munitions, and comprises a weight in the range of about 4,9 - 170,9 kg/m² (1-35 psf) for use in carrying other types of cargo. More particularly, in accordance with the present invention, the armor system comprises a weight of no greater than about 141,6 kg/m² (29 psf) in the embodiment in which the present invention is employed for use with a missile canister armor system for munitions. Even more particularly, in accordance with the present invention, the armor system comprises a weight of about 112,3 kg/m² (23 psf) in the embodiment in which the present invention is employed for use with a missile canister armor system for munitions. Still further, the armored trailer system 600 in accordance with the present alternative embodiment of the present invention can have a total thickness of about 20,32 cm (8.0 inches) as set forth above, and can be further modified by elimination of certain components and/or materials. For example, metal strike face plate may be an optional metal strike face plate in accordance with the armored trailer system 600 of the alternative example of the present invention and may comprise a material including but not limited to carbon steels, alloyed steels, stainless steels or titanium. In other words, metal strike face plate may be omitted in armored trailer system 600 depending on the required level of protection desired for the particular cargo being protected. The airspace according to armored trailer system 600 may be in the range of about 0 cm (inches) (i.e., negligible or no airspace) to about 25,4 cm (10 inches). The rear composite layer of armored trailer system 600 may comprise any material as described above, including but not limited to polyethylene, aramid- or glass-based composite materials. In accordance with the present invention, the respective weights meet those that are needed by the particular application of use with which the present invention is employed. It should be further appreciated that each of two opposing walls 612a, 612b, ceiling or roof 614, rear end 616, front end 618 and floor 620 which are integrally formed with the armor system of the present invention may be joined to each other or otherwise interconnected by mechanisms known in the art, such as but not limited to welding, conventional threaded bolt and nut securing mechanisms and the like, or any other comparable mechanisms that are conventional in the art.

Additional Examples:

[0098] Table 8A below sets forth and describes testing results regarding armor systems comprising perforated titanium / polymer composite backing for 0.30 caliber armor-piercing (APM2) threats. "Total weight" in Table 8A is shown as kg/m² ("pounds per square feet") and "velocity" is shown as m/s "feet per second."

TABLE 8A

Design #	Total Weight	Shot#	Velocity	Penetration
9	41,6 (8.52)	1	873,2 (2856)	Full
		2	875,7 (2873)	Partial
9	50,4 (10.32)	1	873,6 (2866)	Partial
		2		Partial
		3	877,8 (2880)	Partial
12	49,6 (10.16)	1	874,8 (2870)	Partial
14	52,6 (10.78)	1	873,3 (2865)	Partial
		2	874,8 (2870)	Full
16	42,9 (8.78)	1	876,3 (2875)	Partial
		1	872,3 (2862)	Partial
		2	871,1 (2858)	Partial

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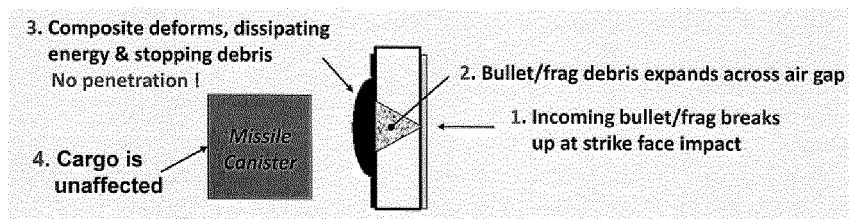
[0099] Table 8B below sets forth and describes additional testing results regarding light weight armor systems for defeating 0.30 caliber M2AP projectiles. Weights of 34,7 - 50,8 kg/m² (7.1 to 10.4 psf) are shown. All systems tested comprise at least one perforated metal strike plate, a 2" space, and a corresponding composite backing.

TABLE 8B: 30 caliber M2AP Test

Sample #	Thickness	kg/m ² (psf)	Shot 1		Shot 2	
			Velocity m/s (ft/s)	Result	Velocity m/s (ft/s)	Result
031615-07M		50,3 (10.3)	868,7 (2850)	full penetration	870,8 (2857)	partial penetration
031615-08S		50,8 (10.4)	820,2 (2691)	partial penetration	858,3 (2816)	partial penetration
031615-09S		44,4 (9.1)	863,5 (2833)	partial penetration	872,6 (2863)	full penetration
031615-10S		39,5 (8.1)	869 (2851)	partial penetration	865,5 (2810)	full penetration
031615-11S		34,7 (7.1)	861,7 (2827)	partial penetration		

[0100] Testing of Tables 8A and 8B demonstrates that the perforated metal and composite backing configuration in accordance with the present invention is effective at stopping 0.30 cal APM2 threats at weights as low as 34,7 kg/m² (7.1 psf). This system could be employed as an armor system for aircraft, vehicles, shields, shelters, body armor, and the like.

[0101] A schematic rendering of a TPS (transportation protection system) in accordance with any embodiment of the present invention is shown below.



Claims

1. A lightweight ballistic armor system for protection against projectiles comprising:

at least one metal strike face plate (110; 210; 803) having a predetermined defined thickness and comprising a plurality of slotted holes (130; 230) set at an angle relative to the vertical orientation or axis of said metal strike face plate (110; 210; 803), said plurality of slotted holes (130; 230) being sufficiently small to prevent the passage of a projectile (P) therethrough;

a laminate composite backing material (120; 220; 802) secured to said metal strike face plate (110; 210; 803), wherein said laminate composite backing material (120; 220; 802) comprises a cross-sectional composition of a backing material of fibers being at least one material selected from the group consisting of aramid fiber, S-glass, E-glass, polypropylene, and UHMWPE, and being in combination with a polymer resin-based binder material;

wherein said at least one metal strike face plate (120; 210; 803) includes a proximate metal strike face plate that is proximate to said laminate composite backing material (120; 220; 802), said proximate metal strike face plate and said composite backing material being separated by a space to define a distance therebetween, wherein said space comprises a maximum distance of 30,48 cm (12 inches),

wherein said metal strike face plate (110; 210; 803) is a perforated metal, and wherein said metal strike face (110; 210; 803) plate comprises at least one material selected from the group consisting of steel, perforated

hardened steel, steel alloys, aluminum, magnesium and titanium,
 wherein said at least one metal strike face plate (110; 210; 803) comprises a total thickness in the range from 0,254 cm (0,1 inch) to 3,81 cm (1,5 inches),
 wherein said plurality of slotted holes (130; 230) are selected from the group consisting of angled slotted holes and straight slotted holes, wherein said plurality of slotted holes (130; 230) are set at an angle in a range of 0° - 60° relative to the vertical orientation of said metal strike face plate (110; 210; 803), and
 wherein said laminate composite backing material (120; 220; 802) comprises a thickness in the range of 0,254 cm to 10,16 cm (0,1 to 4 inches),

characterized by

an environmentally insensitive layer (804) comprising a polymer or metal applied directly onto a surface of said laminate composite backing material (120; 220; 802) facing said metal strike face plate (110; 210; 803), wherein said system has a weight in a range of 4,9 to 170,9 kg/m² (1,0 to 35 psf).

2. The lightweight ballistic armor system according to claim 1, further comprising an energy-absorbing foam for filling said distance, wherein said energy-absorbing foam is a low density foam selected from the group consisting of a polyurethane-based foam and a polypropylene-based foam.
3. The lightweight ballistic armor system according to claim 1, further comprising an additional protective layer (212) selected from the group consisting of a composite layer and a metal skin layer (211) for covering the front face of said metal strike face plate (210; 803), wherein said additional protective layer (212) comprises a material being the same as or different from the material of said metal strike face plate and having a thickness in the range from 0,079 cm to 0,635 (1/32 inch to 1/4 inch).
4. The lightweight ballistic armor system according to claim 1, wherein said metal strike face plate (110; 210; 803) and said laminate composite backing material (120; 220; 802) are secured together by a mechanical threaded securing mechanism.
5. The lightweight ballistic armor system according to claim 1, wherein said laminate composite backing material (120; 220; 802) further comprises a layer of high tensile strength material adjacent to said cross-sectional composition, wherein said layer of high tensile strength material is a high tensile strength polymer board having a thickness in the range of 0,158 cm to 10,16 cm (1/16 inch to 4 inches).
6. The lightweight ballistic armor system according to claim 1, wherein said backing material of fibers comprises a plurality of layers of ballistic grade UHMWPE tape.
7. The lightweight ballistic armor system according to claim 1, further comprising a frame (806) secured or bonded around said environmentally insensitive layer (804) for reinforcing said environmentally insensitive layer (804) onto said laminate composite backing material (120; 220; 802).
8. The lightweight ballistic armor system according to claim 1, wherein said environmentally insensitive layer (804) is a wrap for encasing said composite backing material (120; 220; 802).
9. The lightweight ballistic armor system according to claim 1, wherein the armor system is configured to protect insensitive munitions from projectiles, and wherein said armor system at least meets the appropriate military weight specifications and requirements for defeating, decelerating or slowing low, medium or high velocity and/or low, medium or high caliber projectiles, said appropriate military weight specifications and requirements being selected from the group consisting of the military weight specifications and requirements as defined by NATO Standardization Agreement (STANAG 4241) Bullet Impact, Munitions Test Procedures promulgated on April 15, 2003 and NATO Standardization Agreement (STANAG 4496) Fragment Impact, Munitions Test Procedures promulgated on December 13, 2006.
10. A body armor system comprising a lightweight ballistic armor system for protection against projectiles, said lightweight ballistic armor system comprising:

at least one metal strike face plate (110; 210; 803) having a predetermined defined thickness and comprising a plurality of slotted holes (130; 230) set at an angle relative to the vertical orientation of said metal strike face plate (110; 210; 803), said plurality of slotted holes (130; 230) being sufficiently small to prevent the passage of a projectile (P) therethrough; and

a laminate composite backing material (120; 220; 802) secured to said metal strike face plate (110; 210; 803), wherein said laminate composite backing material (120; 220; 802) comprises a cross-sectional composition of a backing material of fibers being at least one material selected from the group consisting of aramid fiber, S-glass, E-glass, polypropylene and UHMWPE, and being in combination with a polymer resin-based binder material,

wherein said at least one metal strike face plate (110; 210; 803) comprises a material selected from the group consisting of titanium and perforated titanium,

characterized by

an environmentally insensitive layer (704; 804) comprising a polymer or metal applied directly onto a surface of said laminate composite backing material (120; 220; 802) facing said metal strike face plate (110; 210; 803), wherein said system has a weight in the range of 29,3 to 58,6 kg/m² (6 to 12 psf).

11. An armored vehicle system comprising a lightweight ballistic armor system for protection against projectiles, said lightweight ballistic armor system comprising:

at least one metal strike face plate (110; 210; 803) having a predetermined defined thickness and comprising a plurality of slotted holes (130; 230) set at an angle relative to the vertical orientation of said metal strike face plate (110; 210; 803), said plurality of slotted holes (130; 230) being sufficiently small to prevent the passage of a projectile therethrough; and

a laminate composite backing material (120; 220; 802) secured to said metal strike face plate (110; 210; 803), wherein said laminate composite backing material (120; 220; 802) comprises a cross-sectional composition of a backing material of fibers being at least one material selected from the group consisting of aramid fiber, S-glass, E-glass, polypropylene and UHMWPE, and being in combination with a polymer resin-based binder material,

characterized by

an environmentally insensitive layer (704; 804) comprising a polymer or metal applied directly onto a surface of said laminate composite backing material (120; 220; 802) facing said metal strike face plate (110; 210; 803), wherein said system has a weight in the range of 19,5 to 73,2 kg/m² (4 to 15 psf) .

12. A missile canister armor system comprising a lightweight ballistic armor system for protection against projectiles, said lightweight ballistic armor system comprising:

at least one metal strike face plate (110; 210; 803) having a predetermined defined thickness and comprising a plurality of slotted holes (130; 230) set at an angle relative to the vertical orientation of said metal strike face plate (110; 210; 803), said plurality of slotted holes (130; 230) being sufficiently small to prevent the passage of a projectile therethrough; and

a laminate composite backing material (120; 220; 802) secured to said metal strike face plate (110; 210; 803), wherein said laminate composite backing material (120; 220; 802) comprises a cross-sectional composition of a backing material of fibers being at least one material selected from the group consisting of aramid fiber, S-glass, E-glass, polypropylene, and UHMWPE, and being in combination with a polymer resin-based binder material, and

wherein said missile canister armor system is a missile canister,

characterized by

an environmentally insensitive layer (704; 804) comprising a polymer or metal applied directly onto a surface of said laminate composite backing material (120; 220; 802) facing said metal strike face plate (110; 210; 803), wherein said missile canister armor system has a weight in the range of 19,5 to 73,2 kg/m² (4 to 15 psf).

13. An armored structure system having at least one of an armored roof, two armored walls, an armored rear end, an armored front end and an armored floor, wherein said armored structure system is integrally formed of a ballistic armor system for protection against projectiles comprising:

at least one metal strike face plate (110; 210; 803) having a predetermined defined thickness, each of said at least one metal strike face plate (110; 210) comprising a plurality of slotted holes (130; 230) set at an angle relative to the vertical orientation of said metal strike face plate (110; 210; 803), said plurality of slotted holes (130; 230) being sufficiently small to prevent the passage of a projectile therethrough; and

a laminate composite backing material (120; 220; 802) secured to said metal strike face plate (110; 210; 803), wherein said laminate composite backing material (120; 220; 802) comprises a cross-sectional composition of a backing material of fibers being at least one material selected from the group consisting of aramid fiber, S-

glass, E-glass and UHMWPE, and being in combination with a polymer resin-based binder material; and wherein said at least one metal strike face plate includes a proximate metal strike face plate proximate to said laminate composite backing material, wherein said metal strike face plate (110; 210; 803) is separated from said composite backing material (120; 220; 802) by a maximum distance of 30,48 cm (12 inches) for defining a space, and wherein said armored structure system has a weight in the range of up to about 170,9 kg/m² (35 psf), and

wherein said armored structure system is selected from the group consisting of an armored semi-trailer, an armored trailer system, an armored shipping container and an armored missile canister,

characterized by

an environmentally insensitive layer (704; 804) comprising a polymer or metal applied directly onto a surface of said laminate composite backing material (120; 220; 802) facing said metal strike face plate (110; 210; 803).

Patentansprüche

1. Leichtes ballistisches Armierungssystem zum Schutz vor Projektilen, mit:

zumindest einer metallischen Aufprallseiten-Platte (110; 210; 803) mit einer bestimmten vordefinierten Dicke und mit einer Vielzahl von Schlitzlöchern (130; 230), die in einem Winkel relativ zur vertikalen Orientierung oder Achse der metallischen Aufprallseiten-Platte (110; 210; 803) angeordnet sind, wobei die Vielzahl von Schlitzlöchern (130; 230) ausreichend klein sind, um einen Durchlass eines Projektils (P) zu verhindern;

ein laminiertes Verstärkungs-Verbundmaterial (120; 220; 802), das an der metallischen Aufprallseiten-Platte (110; 210; 803) befestigt ist, wobei das laminierte Verstärkungs-Verbundmaterial (120; 220; 802) einen Querschnittverbund eines Verstärkungsmaterials aus Fasern aufweist, welche zumindest ein Material aufweisen, welches aus der Gruppe bestehend aus Aramidfasern, S-Glas, E-Glas, Polypropylen, und UHMWPE ausgewählt ist, und in Kombination mit einem harzbasierenden Polymer-Bindermaterial vorliegt;

wobei die zumindest eine metallische Aufprallseiten-Platte (110; 210; 803) eine nahegelegene metallische Aufprallseiten-Platte aufweist, die nahe an dem laminierten Verstärkungs-Verbundmaterial (120; 220; 802) angeordnet ist, wobei die nahegelegene metallische Aufprallseiten-Platte und das Verstärkungs-Verbundmaterial durch einen eine Entfernung definierenden Abstand getrennt ist, wobei der Abstand eine maximale Entfernung von 30,48 cm (12 inch) aufweist,

wobei die metallische Aufprallseiten-Platte (110; 210; 803) ein perforiertes Metall ist, und wobei die metallische Aufprallseiten-Platte (110; 210; 803) zumindest ein Material aufweist, welches aus der Gruppe bestehend aus Stahl, perforiertem gehärteten Stahl, Stahllegierungen, Aluminium, Magnesium und Titan ausgewählt ist,

wobei die zumindest eine metallische Aufprallseiten-Platte (110; 210; 803) eine Gesamtdicke im Bereich von 0,254 cm (0,1 inch) bis 3,81 cm (1,5 inch) aufweist,

wobei die Vielzahl von Schlitzlöchern (130; 230) aus einer Gruppe ausgewählt ist, bestehend aus schrägen Schlitzlöchern und geraden Schlitzlöchern, wobei die Vielzahl von Schlitzlöchern (130; 230) in einem Winkel von 0° - 60° relativ zur vertikalen Orientierung der metallischen Aufprallseiten-Platte (110; 210; 803) eingestellt ist, und

wobei das laminierte Verstärkungs-Verbundmaterial (120; 220; 802) eine Dicke im Bereich von 0,254 cm bis 10,16 cm (0,1 bis 4 inch) aufweist,

gekennzeichnet durch

eine umweltunempfindliche Schicht (804), welche ein direkt auf eine Oberfläche des laminierten Verstärkungs-Verbundmaterials (120; 220; 802) aufgebracht Polymer oder Metall aufweist, die der metallischen Aufprallseiten-Platte (110; 210; 803) zugewandt ist,

wobei das System ein Gewicht in einem Bereich von 4,9 bis 170,9 kg/m² (1,0 bis 35 psf) besitzt.

2. Leichtes ballistisches Armierungssystem nach Patentanspruch 1,

ferner umfassend einen Energie-absorbierenden Schaum zum Auffüllen des Abstands, wobei der Energie-absorbierende Schaum ein Schaum mit geringer Dichte ist, welcher aus der Gruppe bestehend aus Polyurethan-basiertem Schaum und Polypropylen-basiertem Schaum ausgewählt ist.

3. Leichtes ballistisches Armierungssystem nach Patentanspruch 1,

ferner umfassend eine zusätzliche Schutzschicht (212), welche aus der Gruppe bestehend aus einer Verbundschicht und einer Metallhautschicht (211) zum Bedecken der Vorderseite der metallischen Aufprallseiten-Platte (210; 803) ausgewählt ist, wobei die zusätzliche Schutzschicht (212) ein Material aufweist, das gleich oder verschieden zum Material der metallischen Aufprallseiten-Platte ist, und eine Dicke im Bereich von 0,079 cm bis 0,635 cm (1/32 bis

¼ inch) besitzt.

4. Leichtes ballistisches Armierungssystem nach Patentanspruch 1, wobei die metallische Aufprallseiten-Platte (110; 210; 803) und das laminierte Verstärkungs-Verbundmaterial (120; 220; 802) durch einen mechanischen Gewinde-Befestigungsmechanismus miteinander verbunden sind.
5. Leichtes ballistisches Armierungssystem nach Patentanspruch 1, wobei das laminierte Verstärkungs-Verbundmaterial (120; 220; 802) ferner eine Schicht mit einem Material von hoher Zugfestigkeit angrenzend an den Querschnittverbund aufweist, wobei die Schicht mit einem Material von hoher Zugfestigkeit eine Polymertafel mit hoher Zugfestigkeit und mit einer Dicke im Bereich von 0,158 cm bis 10,16 cm ((1/16 inch bis 4 inch) ist.
6. Leichtes ballistisches Armierungssystem nach Patentanspruch 1, wobei das Verstärkungsmaterial aus Fasern eine Vielzahl von Schichten eines UHMWPE Klebebands von ballistischer Qualität aufweist.
7. Leichtes ballistisches Armierungssystem nach Patentanspruch 1, ferner umfassend einen Rahmen (806), der um die umweltunempfindliche Schicht (804) herum befestigt oder gebondet ist, zum Verstärken der umweltunempfindlichen Schicht (804) auf dem laminierten Verstärkungs-Verbundmaterial (120; 220; 802) .
8. Leichtes ballistisches Armierungssystem nach Patentanspruch 1, wobei die umweltunempfindliche Schicht (804) eine Hülle zum Einkapseln des laminierten Verstärkungs-Verbundmaterials (120; 220; 802) ist.
9. Leichtes ballistisches Armierungssystem nach Patentanspruch 1, wobei das Armierungssystem zum Schutz von insensitiver Munition gegenüber Projektilen konfiguriert ist, und wobei das Armierungssystem zumindest die entsprechenden militärischen Gewichtsspezifikationen und Anforderungen an die Zerschlagung, Abbremsung und Entschleunigung von Projektilen mit geringer, mittlerer oder hoher Geschwindigkeit und/oder kleinem, mittleren oder großen Kaliber erfüllt, wobei die entsprechenden militärischen Gewichtsspezifikationen und Anforderungen aus der Gruppe bestehend aus der militärischen Gewichtsspezifikationen und Anforderungen gemäß NATO Geschosseinschlag-Standardisierungsübereinkommen (STANAG 4241) bekanntgemacht am 15. April 2003 in Munitions-Testprozeduren und gemäß NATO Fragmenteinschlag-Standardisierungsübereinkommen (STANAG 4496) bekanntgemacht am 13. Dezember 2006 in Munitions-Testprozeduren, ausgewählt ist.
10. Körper-Armierungssystem mit einem leichten ballistischen Armierungssystem zum Schutz vor Projektilen, wobei das leichte ballistische Armierungssystem umfasst:
 - zumindest eine metallische Aufprallseiten-Platte (110; 210; 803) mit einer bestimmten vordefinierten Dicke und mit einer Vielzahl von Schlitzlöchern (130; 230), die in einem Winkel relativ zur vertikalen Orientierung oder Achse der metallischen Aufprallseiten-Platte (110; 210; 803) angeordnet sind, wobei die Vielzahl von Schlitzlöchern (130; 230) ausreichend klein sind, um einen Durchlass eines Projektils (P) zu verhindern; und
 - ein laminiertes Verstärkungs-Verbundmaterial (120; 220; 802), das an der metallischen Aufprallseiten-Platte (110; 210; 803) befestigt ist, wobei das laminierte Verstärkungs-Verbundmaterial (120; 220; 802) einen Querschnittverbund eines Verstärkungsmaterials aus Fasern aufweist, welche zumindest ein Material aufweisen, welches aus der Gruppe bestehend aus Aramidfasern, S-Glas, E-Glas, Polypropylen, und UHMWPE ausgewählt ist, und in Kombination mit einem harzbasierenden Polymer-Bindermaterial vorliegt,
 - wobei die zumindest eine metallische Aufprallseiten-Platte (110; 210; 803) ein Material, ausgewählt aus der Gruppe bestehend aus Titan und perforiertem Titan, umfasst, **gekennzeichnet durch**
 - eine umweltunempfindliche Schicht (704; 804), welche ein direkt auf eine Oberfläche des laminierten Verstärkungs-Verbundmaterials (120; 220; 802) aufgebracht Polymer oder Metall aufweist, die der metallischen Aufprallseiten-Platte (110; 210; 803) zugewandt ist,
 - wobei das System ein Gewicht in einem Bereich von 29,3 bis 58,6 kg/m² (6,0 bis 12 psf) besitzt.
11. Fahrzeug-Armierungssystem mit einem leichten ballistischen Armierungssystem zum Schutz vor Projektilen, wobei das leichte ballistische Armierungssystem umfasst:

zumindest eine metallische Aufprallseiten-Platte (110; 210; 803) mit einer bestimmten vordefinierten Dicke und mit einer Vielzahl von Schlitzlöchern (130; 230), die in einem Winkel relativ zur vertikalen Orientierung der metallischen Aufprallseiten-Platte (110; 210; 803) angeordnet sind, wobei die Vielzahl von Schlitzlöchern (130; 230) ausreichend klein sind, um einen Durchlass eines Projektils zu verhindern; und ein laminiertes Verstärkungs-Verbundmaterial (120; 220; 802), das an der metallischen Aufprallseiten-Platte (110; 210; 803) befestigt ist, wobei das laminierte Verstärkungs-Verbundmaterial (120; 220; 802) einen Querschnittverbund eines Verstärkungsmaterials aus Fasern aufweist, welche zumindest ein Material aufweisen, welches aus der Gruppe bestehend aus Aramidfasern, S-Glas, E-Glas, Polypropylen, und UHMWPE ausgewählt ist, und in Kombination mit einem harzbasierenden Polymer-Bindermaterial vorliegt,

gekennzeichnet durch

eine umweltunempfindliche Schicht (704; 804), welche ein direkt auf eine Oberfläche des laminierten Verstärkungs-Verbundmaterials (120; 220; 802) aufgebrachtes Polymer oder Metall aufweist, die der metallischen Aufprallseiten-Platte (110; 210; 803) zugewandt ist, wobei das System ein Gewicht in einem Bereich von 19,5 bis 73,2 kg/m² (4 bis 15 psf) besitzt.

12. Raketenbehälter-Armierungssystem mit einem leichten ballistischen Armierungssystem zum Schutz vor Projektilen, wobei das leichte ballistische Armierungssystem umfasst:

zumindest eine metallische Aufprallseiten-Platte (110; 210; 803) mit einer bestimmten vordefinierten Dicke und mit einer Vielzahl von Schlitzlöchern (130; 230), die in einem Winkel relativ zur vertikalen Orientierung der metallischen Aufprallseiten-Platte (110; 210; 803) angeordnet sind, wobei die Vielzahl von Schlitzlöchern (130; 230) ausreichend klein sind, um einen Durchlass eines Projektils zu verhindern; und ein laminiertes Verstärkungs-Verbundmaterial (120; 220; 802), das an der metallischen Aufprallseiten-Platte (110; 210; 803) befestigt ist, wobei das laminierte Verstärkungs-Verbundmaterial (120; 220; 802) einen Querschnittverbund eines Verstärkungsmaterials aus Fasern aufweist, welche zumindest ein Material aufweisen, welches aus der Gruppe bestehend aus Aramidfasern, S-Glas, E-Glas, Polypropylen, und UHMWPE ausgewählt ist, und in Kombination mit einem harzbasierenden Polymer-Bindermaterial vorliegt, und wobei das Raketenbehälter-Armierungssystem ein Raketenbehälter ist,

gekennzeichnet durch

eine umweltunempfindliche Schicht (704; 804), welche ein direkt auf die Oberfläche des laminierten Verstärkungs-Verbundmaterials (120; 220; 802) aufgebrachtes Polymer oder Metall aufweist, die der metallischen Aufprallseiten-Platte (110; 210; 803) zugewandt ist, wobei das Raketenbehälter-Armierungssystem ein Gewicht in einem Bereich von 19,5 bis 73,2 kg/m² (4 bis 15 psf) besitzt.

13. Struktur-Armierungssystem mit zumindest einem armierten Dach, zwei armierten Wänden, einer armierten Rückseite, einer armierten Vorderseite und einem armierten Boden, wobei das Struktur-Armierungssystem integral aus einem ballistischen Armierungssystem zum Schutz vor Projektilen ausgebildet ist, umfassend:

zumindest eine metallische Aufprallseiten-Platte (110; 210; 803) mit einer bestimmten vordefinierten Dicke, wobei jede der zumindest einen metallischen Aufprallseiten-Platte (110; 210) eine Vielzahl von Schlitzlöchern (130; 230) aufweist, die in einem Winkel relativ zur vertikalen Orientierung der metallischen Aufprallseiten-Platte (110; 210; 803) angeordnet sind, wobei die Vielzahl von Schlitzlöchern (130; 230) ausreichend klein sind, um einen Durchlass eines Projektils zu verhindern; und

ein laminiertes Verstärkungs-Verbundmaterial (120; 220; 802), das an der metallischen Aufprallseiten-Platte (110; 210; 803) befestigt ist, wobei das laminierte Verstärkungs-Verbundmaterial (120; 220; 802) einen Querschnittverbund eines Verstärkungsmaterials aus Fasern aufweist, welche zumindest ein Material aufweisen, welches aus der Gruppe bestehend aus Aramidfasern, S-Glas, E-Glas, Polypropylen, und UHMWPE ausgewählt ist, und in Kombination mit einem harzbasierenden Polymer-Bindermaterial vorliegt, und

wobei die zumindest eine metallische Aufprallseiten-Platte eine nahegelegene metallische Aufprallseiten-Platte aufweist, die nahe an dem laminierten Verstärkungs-Verbundmaterial angeordnet ist, wobei die metallische Aufprallseiten-Platte (110; 210; 803) durch eine maximale Entfernung von 30,48 cm (12 inch) zum Definieren eines Abstands vom Verstärkungs-Verbundmaterial (120; 220; 802) getrennt ist, und wobei das Struktur-Armierungssystem ein Gewicht im Bereich von bis zu ca. 170,9 kg/m² (35 psf) besitzt, und

wobei das Struktur-Armierungssystem aus der Gruppe bestehend aus einem armierten Sattelanhänger, einem armierten Aufliegersystem, einem armierten Schiffscontainer und einem armierten Raketenbehälter ausgewählt ist,

gekennzeichnet durch

eine umweltunempfindliche Schicht (704; 804), welche ein direkt auf die Oberfläche des laminierten Verstärkungs-Verbundmaterials (120; 220; 802) aufgebracht Polymer oder Metall aufweist, die der metallischen Aufprallseiten-Platte (110; 210; 803) zugewandt ist.

5

Revendications

1. Système de blindage balistique léger pour la protection contre les projectiles comprenant:

10 au moins une plaque frontale d'impact en métal (110; 210; 803) ayant une épaisseur définie prédéterminée et comportant une pluralité de trous fendus (130; 230) disposés à un certain angle par rapport à l'orientation verticale ou à l'axe de ladite plaque frontale d'impact en métal (110; 210; 803), ladite pluralité de trous fendus (130; 230) étant suffisamment petits pour empêcher le passage d'un projectile (P);

15 un matériau de renfort composite stratifié (120; 220; 802) fixé sur ladite plaque frontale d'impact en métal (110; 210; 803), ledit matériau de renfort composite stratifié (120; 220; 802) comprenant une composition en coupe transversale d'un matériau de renfort de fibres étant au moins un matériau choisi parmi les fibres d'aramide, la fibre de verre S-glass, la fibre de verre E-glass, le polypropylène et l'UHMWPE, et se trouvant combiné à un matériau liant à base de résine polymère;

20 ladite au moins une plaque frontale d'impact en métal (120; 210; 803) comprenant une plaque frontale d'impact en métal proche qui est proche dudit matériau de renfort composite stratifié (120; 220; 802), ladite plaque frontale d'impact en métal proche et ledit matériau de renfort composite étant séparés par un espace pour définir une distance entre eux, ledit espace comprenant une distance maximum de 30,48 cm (12 pouces), ladite plaque frontale d'impact en métal (110; 210; 803) étant un métal perforé, et ladite plaque frontale d'impact en métal (110; 210; 803) comprenant au moins un matériau choisi dans le groupe consistant en acier, acier trempé perforé, alliages d'acier, aluminium, magnésium et titane,

25 ladite au moins une plaque frontale d'impact en métal (110; 210; 803) comprenant une épaisseur totale comprise entre 0,254 cm (0,1 pouce) et 3,81 cm (1,5 pouces), ladite pluralité de trous fendus (130; 230) étant choisie dans le groupe constitué par les trous fendus coudés et les trous fendus droits, ladite pluralité de trous fendus (130; 230) étant placée selon un angle compris entre 0° et 60° par rapport à l'orientation verticale de ladite plaque frontale d'impact en métal (110; 210; 803), et

30 ledit matériau de renfort composite stratifié (120; 220; 802) comprenant une épaisseur comprise entre 0,254 cm et 10,16 cm (0,1 à 4 pouces),

caractérisé par une couche insensible à l'environnement (804) comprenant un polymère ou un métal appliqué directement sur une surface dudit matériau de renfort composite stratifié (120; 220; 802) faisant face à ladite

35 plaque frontale d'impact en métal (110; 210; 803),

ledit système ayant un poids dans une plage de 4,9 à 170,9 kg/m² (1,0 à 35 psf).

2. Système de blindage balistique léger selon la revendication 1, comprenant en outre une mousse absorbant l'énergie pour remplir ladite distance, dans lequel ladite mousse absorbant l'énergie est une mousse de faible densité choisie dans le groupe constitué par une mousse à base de polyuréthane et une mousse à base de polypropylène.

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3. Système de blindage balistique léger selon la revendication 1, comprenant en outre une couche protectrice supplémentaire (212) choisie dans le groupe constitué d'une couche composite et d'une couche de peau métallique (211) pour couvrir la face avant de ladite plaque frontale d'impact en métal (210; 803), dans lequel ladite couche protectrice supplémentaire (212) comprend un matériau identique ou différent du matériau de ladite plaque frontale d'impact en métal et ayant une épaisseur comprise entre 0,079 cm et 0,635 (1/32 pouce et 1/4 pouce).

45

4. Système de blindage balistique léger selon la revendication 1, dans lequel ladite plaque frontale d'impact en métal (110; 210; 803) et ledit matériau de renfort composite stratifié (120; 220; 802) sont fixés ensemble par un mécanisme de fixation mécanique fileté.

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5. Système de blindage balistique léger selon la revendication 1, dans lequel ledit matériau de renfort composite stratifié (120; 220; 802) comprend en outre une couche de matériau à haute résistance à la traction adjacente à ladite composition transversale,

55 dans lequel ladite couche de matériau à haute résistance à la traction est un panneau de polymère à haute résistance à la traction ayant une épaisseur comprise entre 0,158 cm et 10,16 cm (1/16 pouce et 4 pouces) .

6. Système de blindage balistique léger selon la revendication 1, dans lequel ledit matériau de renfort de fibres comprend

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une pluralité de couches de ruban UHMWPE de qualité balistique.

7. Système de blindage balistique léger selon la revendication 1, comprenant en outre un cadre (806) fixé ou collé autour de ladite couche insensible à l'environnement (804) pour renforcer ladite couche insensible à l'environnement (804) sur ledit matériau de renfort composite stratifié (120; 220; 802).

8. Système de blindage balistique léger selon la revendication 1, dans lequel ladite couche insensible à l'environnement (804) est une enveloppe pour envelopper ledit matériau de renfort composite (120; 220; 802).

9. Système de blindage balistique léger selon la revendication 1, dans lequel le système de blindage est configuré pour protéger des munitions insensibles contre des projectiles, et ledit système de blindage répondant au moins aux spécifications et exigences de poids militaire appropriées pour vaincre, décélérer ou ralentir des projectiles à basse, moyenne ou haute vitesse et/ou à faible, moyen ou haut calibre, lesdites spécifications et exigences appropriées relatives au poids militaire étant choisies dans le groupe constitué des spécifications et exigences relatives au poids militaire telles que définies par l'Accord de normalisation de l'OTAN (STANAG 4241) - Impact des balles, Procédures d'essai des munitions promulgué le 15 avril 2003 et l'Accord de normalisation de l'OTAN (STANAG 4496) - Impact des fragments, Procédures d'essai des munitions promulgué le 13 décembre 2006.

10. Système de blindage corporel comprenant un système de blindage balistique léger pour la protection contre les projectiles, ledit système de blindage balistique léger comprenant:

au moins une plaque frontale d'impact en métal (110; 210; 803) ayant une épaisseur définie prédéterminée et comportant une pluralité de trous fendus (130; 230) disposés à un certain angle par rapport à l'orientation verticale de ladite plaque frontale d'impact en métal (110; 210; 803), ladite pluralité de trous fendus (130; 230) étant suffisamment petits pour empêcher le passage d'un projectile (P); et

un matériau de renfort composite stratifié (120; 220; 802) fixé sur ladite plaque frontale d'impact en métal (110; 210; 803),

ledit matériau de renfort composite stratifié (120; 220; 802) comprenant une composition en coupe transversale d'un matériau de renfort de fibres étant au moins un matériau choisi parmi les fibres d'aramide, la fibre de verre S-glass, la fibre de verre E-glass, le polypropylène et l'UHMWPE, et se trouvant combiné à un matériau liant à base de résine polymère,

ladite au moins une plaque d'impact en métal (110; 210; 803) comprenant un matériau choisi dans le groupe constitué par le titane et le titane perforé,

caractérisé par une couche insensible à l'environnement (704; 804) comprenant un polymère ou un métal appliqué directement sur une surface dudit matériau de renfort composite stratifié (120; 220; 802) faisant face à ladite plaque frontale d'impact en métal (110; 210; 803),

ledit système ayant un poids allant de 29,3 à 58,6 kg/m² (6 à 12 psf).

11. Système de véhicule blindé comprenant un système de blindage balistique léger pour la protection contre les projectiles, ledit système de blindage balistique léger comprenant:

au moins une plaque frontale d'impact en métal (110; 210; 803) ayant une épaisseur définie prédéterminée et comportant une pluralité de trous fendus (130; 230) disposés à un certain angle par rapport à l'orientation verticale de ladite plaque frontale d'impact en métal (110; 210; 803), ladite pluralité de trous fendus (130; 230) étant suffisamment petits pour empêcher le passage d'un projectile; et

un matériau de renfort composite stratifié (120; 220; 802) fixé sur ladite plaque frontale d'impact en métal (110; 210; 803),

ledit matériau de renfort composite stratifié (120; 220; 802) comprenant une composition en coupe transversale d'un matériau de renfort de fibres étant au moins un matériau choisi parmi les fibres d'aramide, la fibre de verre S-glass, la fibre de verre E-glass, le polypropylène et l'UHMWPE, et se trouve combiné à un matériau liant à base de résine polymère,

caractérisé par une couche insensible à l'environnement (704; 804) comprenant un polymère ou un métal appliqué directement sur une surface dudit matériau de renfort composite stratifié (120; 220; 802) faisant face à ladite plaque frontale d'impact en métal (110; 210; 803),

ledit système ayant un poids allant de 19,5 à 73,2 kg/m² (4 à 15 psf).

12. Système de blindage de récipient métallique pour missiles comprenant un système de blindage balistique léger pour la protection contre les projectiles, ledit système de blindage balistique léger comprenant:

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au moins une plaque frontale d'impact en métal (110; 210; 803) ayant une épaisseur définie prédéterminée et comportant une pluralité de trous fendus (130; 230) disposés à un certain angle par rapport à l'orientation verticale de ladite plaque frontale d'impact en métal (110; 210; 803), ladite pluralité de trous fendus (130; 230) étant suffisamment petits pour empêcher le passage d'un projectile; et

un matériau de renfort composite stratifié (120; 220; 802) fixé sur ladite plaque frontale d'impact en métal (110; 210; 803), ledit matériau de renfort composite stratifié (120; 220; 802) comprenant une composition en coupe transversale d'un matériau de renfort de fibres étant au moins un matériau choisi parmi les fibres d'aramide, la fibre de verre S-glass, la fibre de verre E-glass, le polypropylène et l'UHMWPE, et se trouvant combiné à un matériau liant à base de résine polymère, et

ledit système de blindage de récipient métallique pour missiles étant un récipient métallique pour missiles, **caractérisé par** une couche insensible à l'environnement (704; 804) comprenant un polymère ou un métal appliqué directement sur une surface dudit matériau de renfort composite stratifié (120; 220; 802) faisant face à ladite plaque frontale d'impact en métal (110; 210; 803),

ledit système de blindage de récipient métallique pour missiles ayant un poids allant de 19,5 à 73,2 kg/m² (4 à 15 psf).

13. Système de structure blindée ayant au moins l'un parmi un toit blindé, deux parois blindées, une extrémité arrière blindée, une extrémité avant blindée et un plancher blindé, ledit système de structure blindée étant formé intégralement d'un système de blindage balistique pour la protection contre des projectiles comprenant:

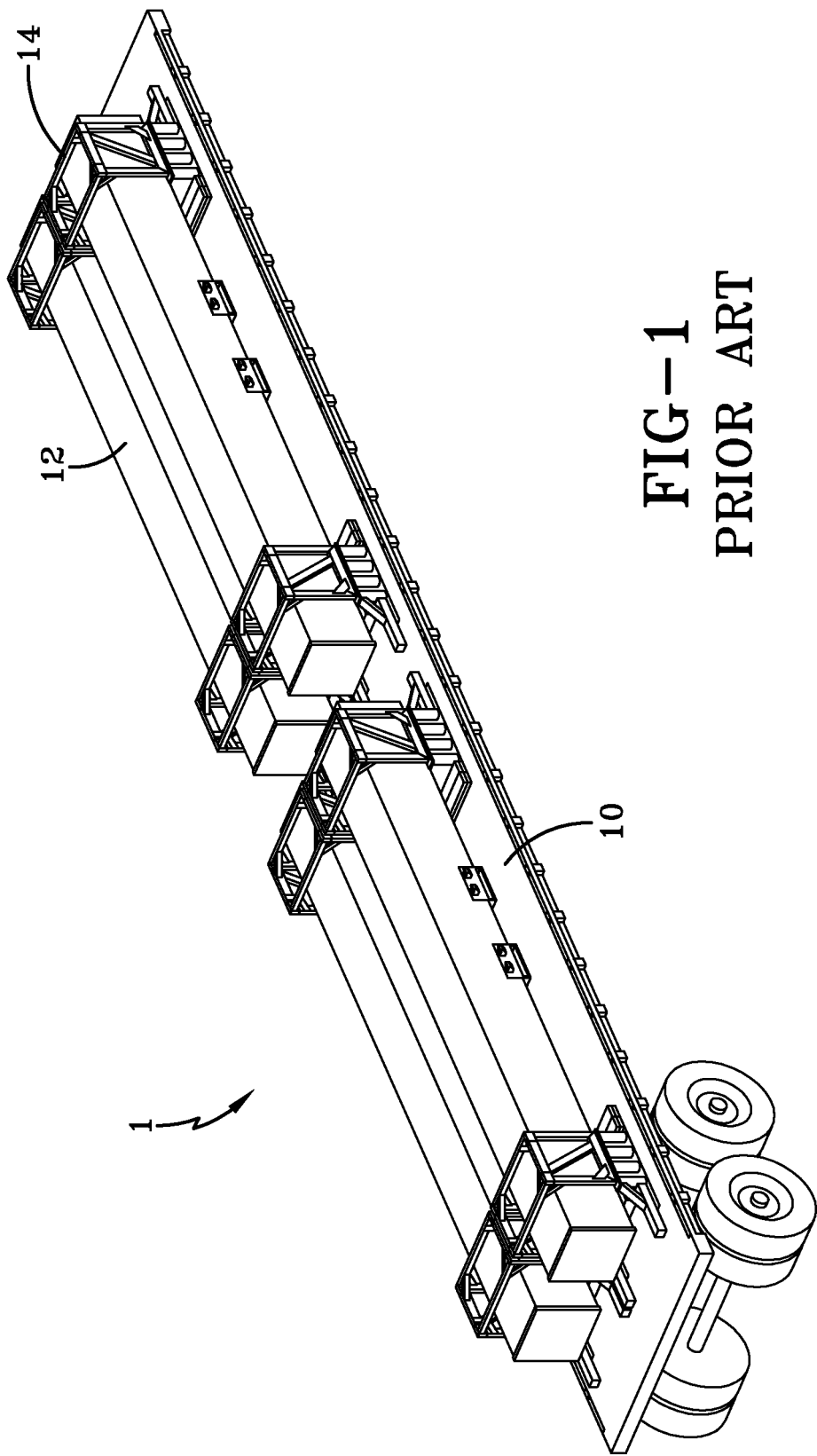
au moins une plaque frontale d'impact en métal (110; 210; 803) ayant une épaisseur définie prédéterminée, chacune desdites au moins une plaque frontale d'impact en métal (110; 210) comprenant une pluralité de trous fendus (130; 230) disposés à un certain angle par rapport à l'orientation verticale de ladite plaque frontale d'impact en métal (110; 210; 803), ladite pluralité de trous fendus (130; 230) étant suffisamment petits pour empêcher le passage d'un projectile; et

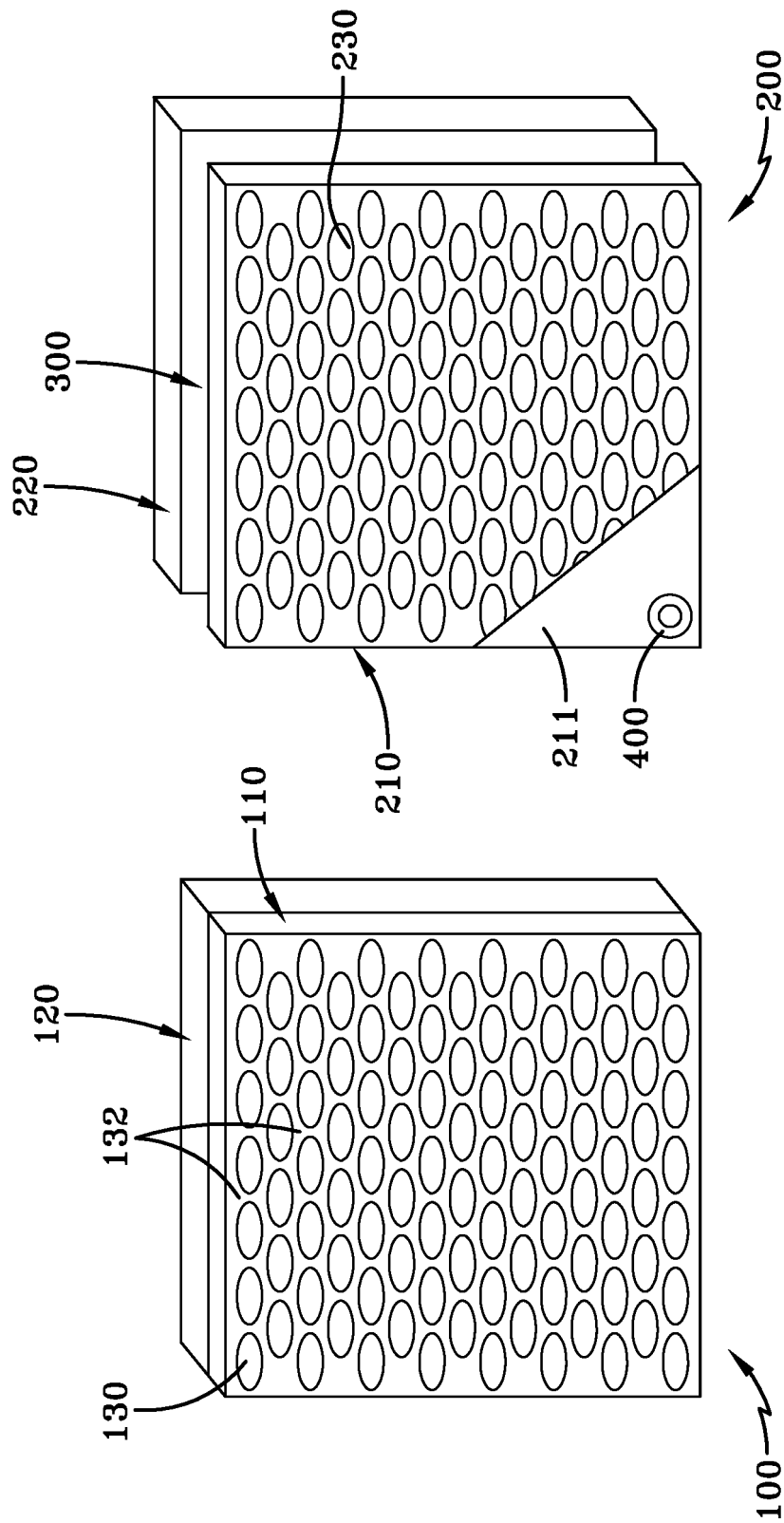
un matériau de renfort composite stratifié (120; 220; 802) fixé à ladite plaque frontale d'impact en métal (110; 210; 803), ledit matériau de renfort composite stratifié (120; 220; 802) comprenant une composition en coupe transversale d'un matériau de renfort de fibres étant au moins un matériau choisi parmi les fibres d'aramide, la fibre de verre S-glass, la fibre de verre E-glass et l'UHMWPE, et se trouvant combiné à un matériau liant à base de résine polymère; et

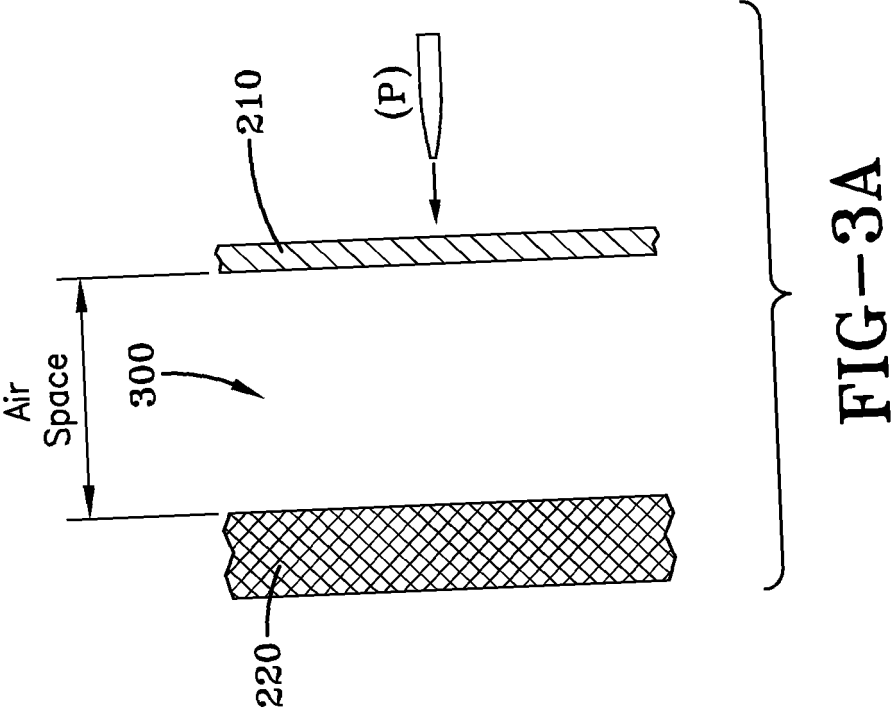
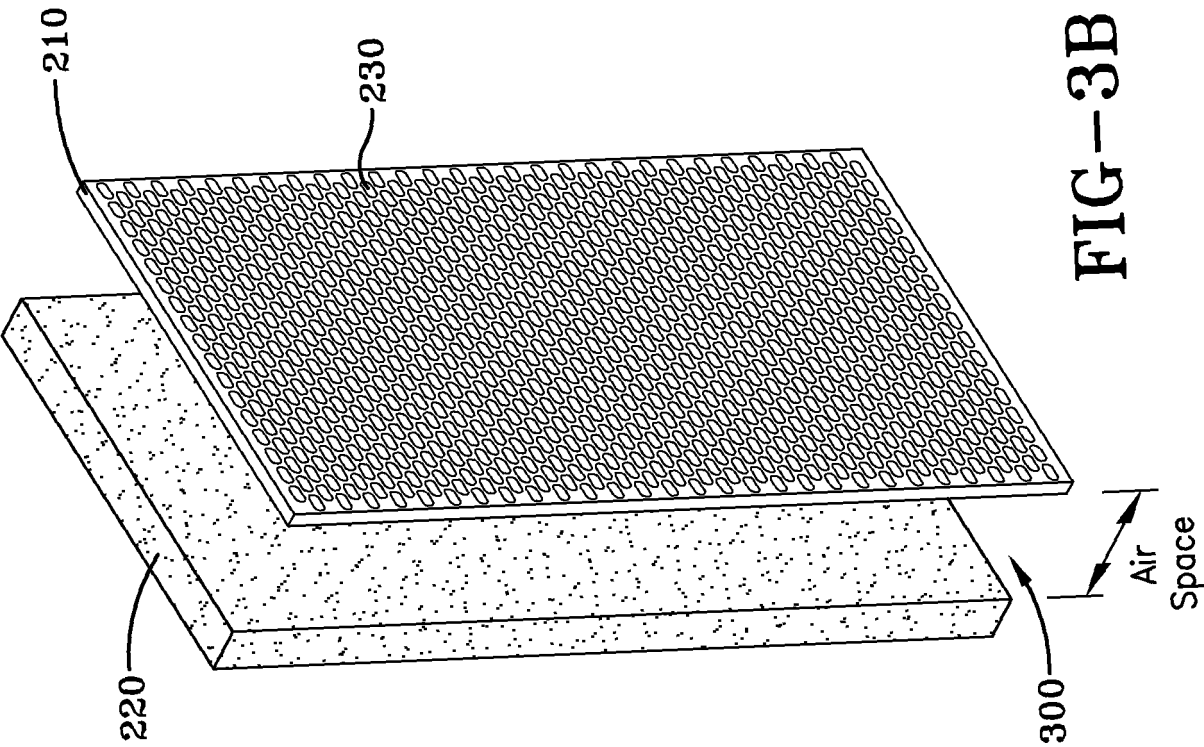
ladite au moins une plaque frontale d'impact en métal comprenant une plaque frontale d'impact en métal proximale à proximité dudit matériau de renfort composite stratifié, ladite plaque frontale d'impact en métal (110; 210; 803) étant séparée dudit matériau de renfort composite (120; 220; 802) par une distance maximale de 30,48 cm (12 pouces) pour définir un espace, et ledit système de structure blindée ayant un poids allant jusqu'à environ 170,9 kg/m² (35 psf), et

ledit système de structure blindée étant choisi dans le groupe constitué d'une semi-remorque blindée, d'un système de remorque blindée, d'un conteneur de transport blindé et d'un récipient métallique pour missiles blindé,

caractérisé par une couche insensible à l'environnement (704; 804) comprenant un polymère ou un métal appliqué directement sur une surface dudit matériau de renfort composite stratifié (120; 220; 802) faisant face à ladite plaque frontale d'impact en métal (110; 210; 803).







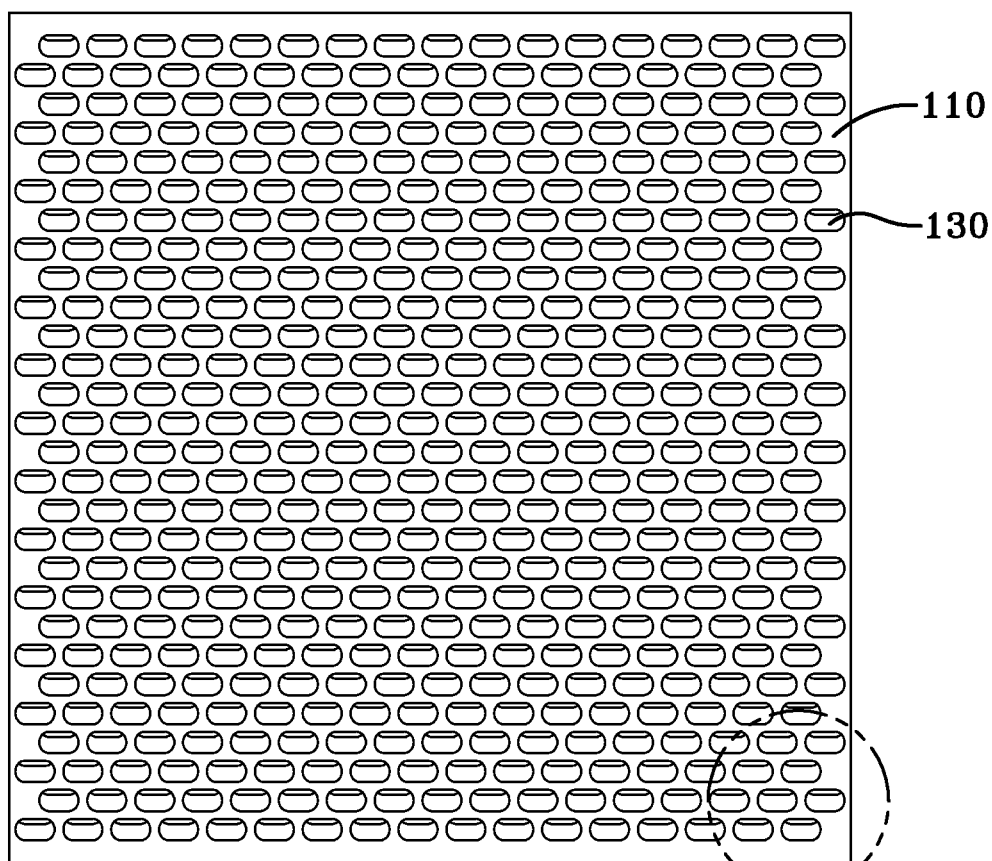


FIG-4

SEE
FIG-5

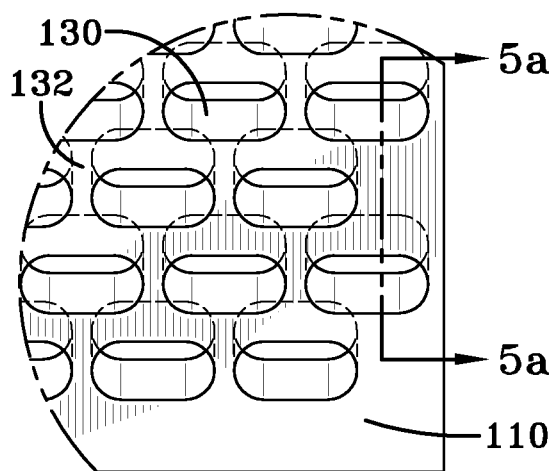


FIG-5

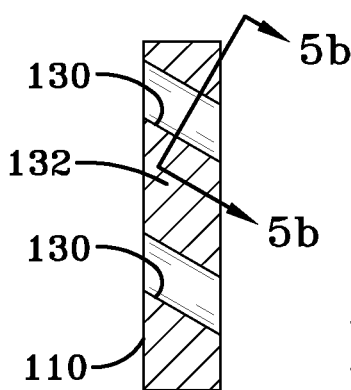


FIG-5a

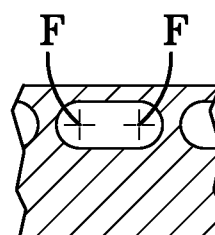


FIG-5b

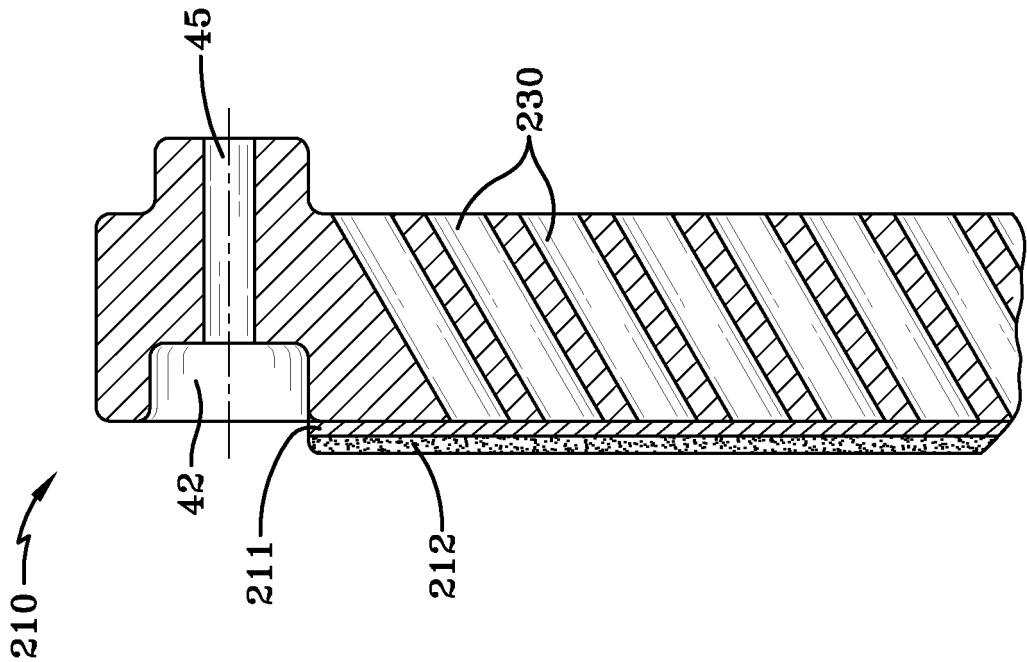


FIG-7

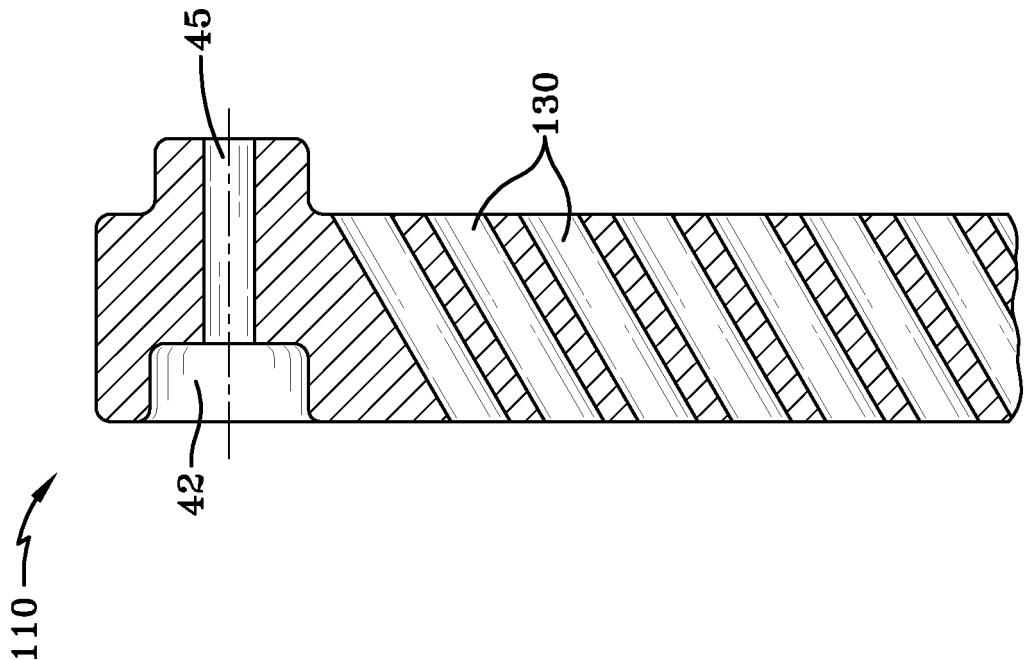


FIG-6

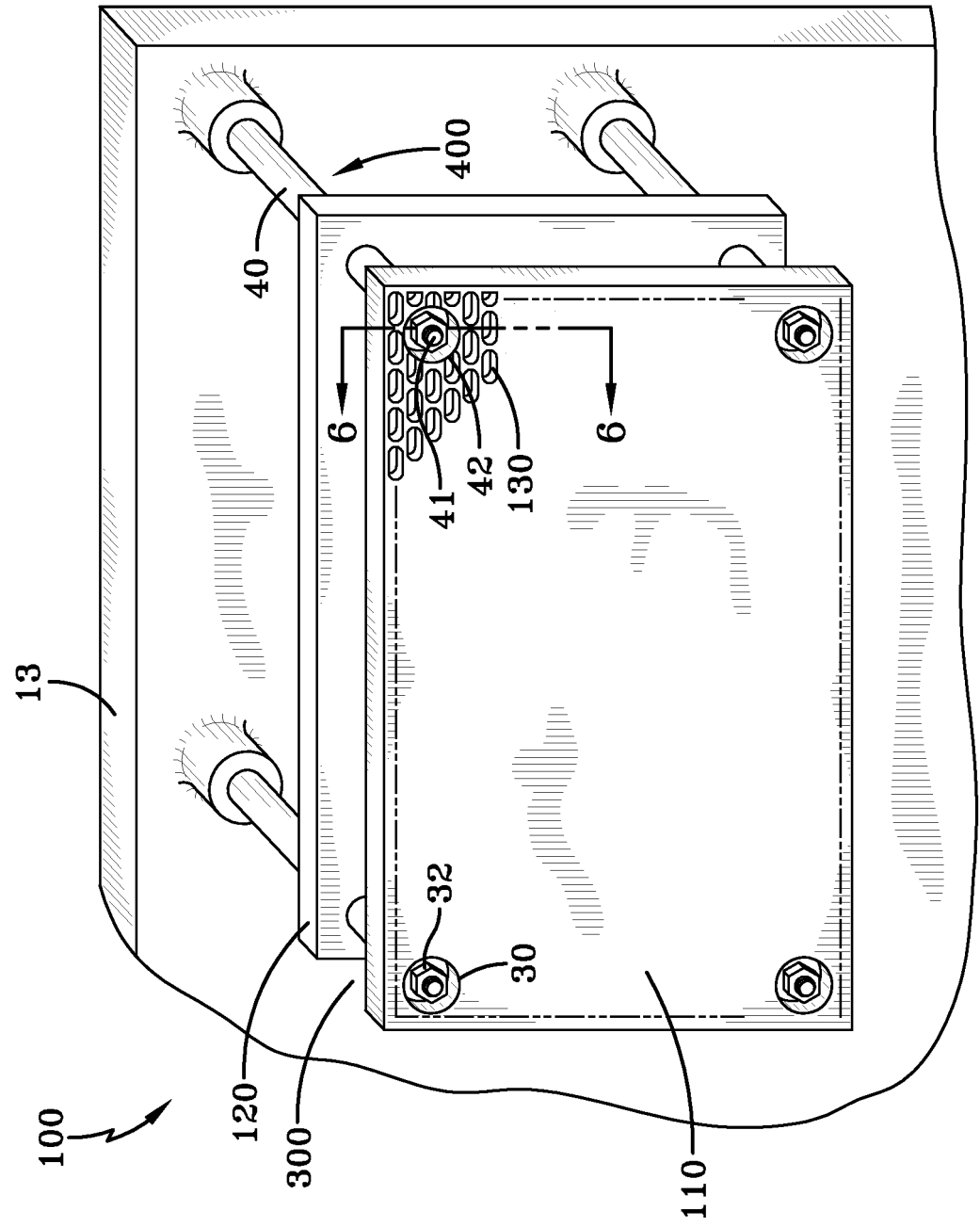


FIG-8

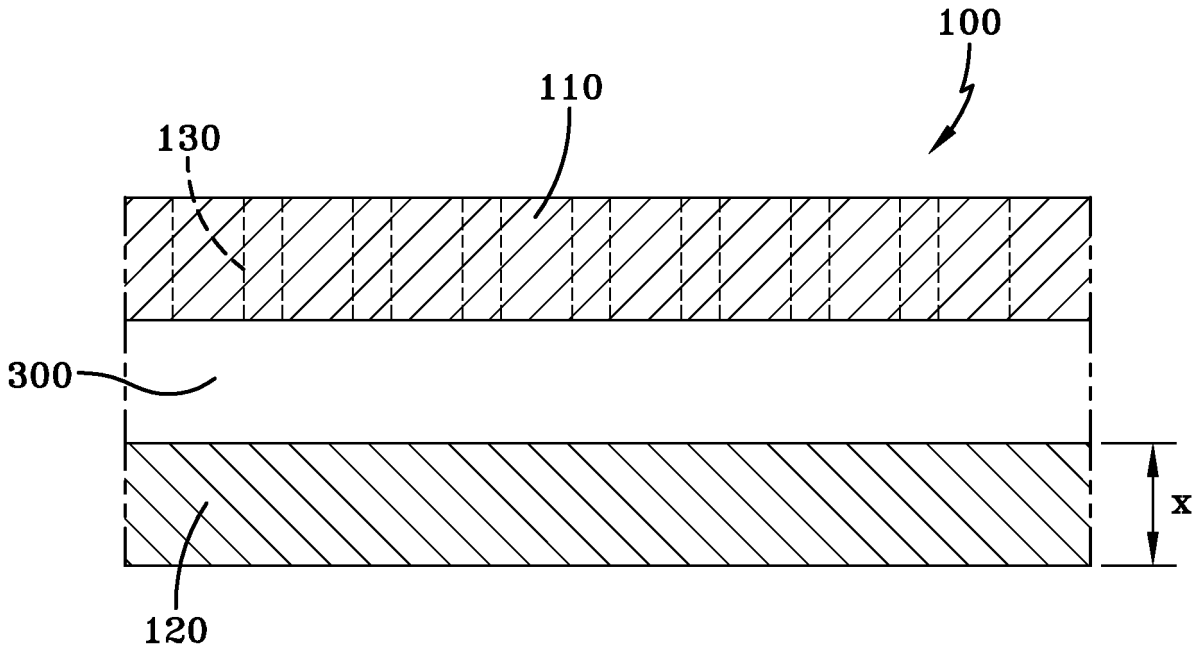


FIG-9A

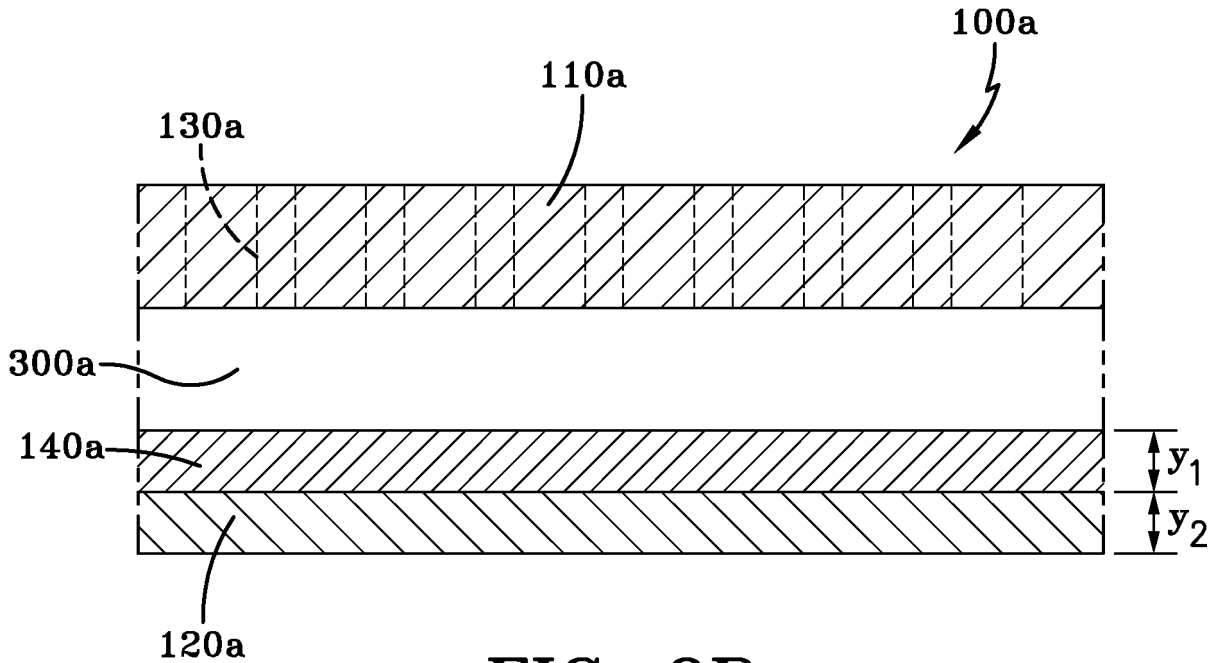


FIG-9B

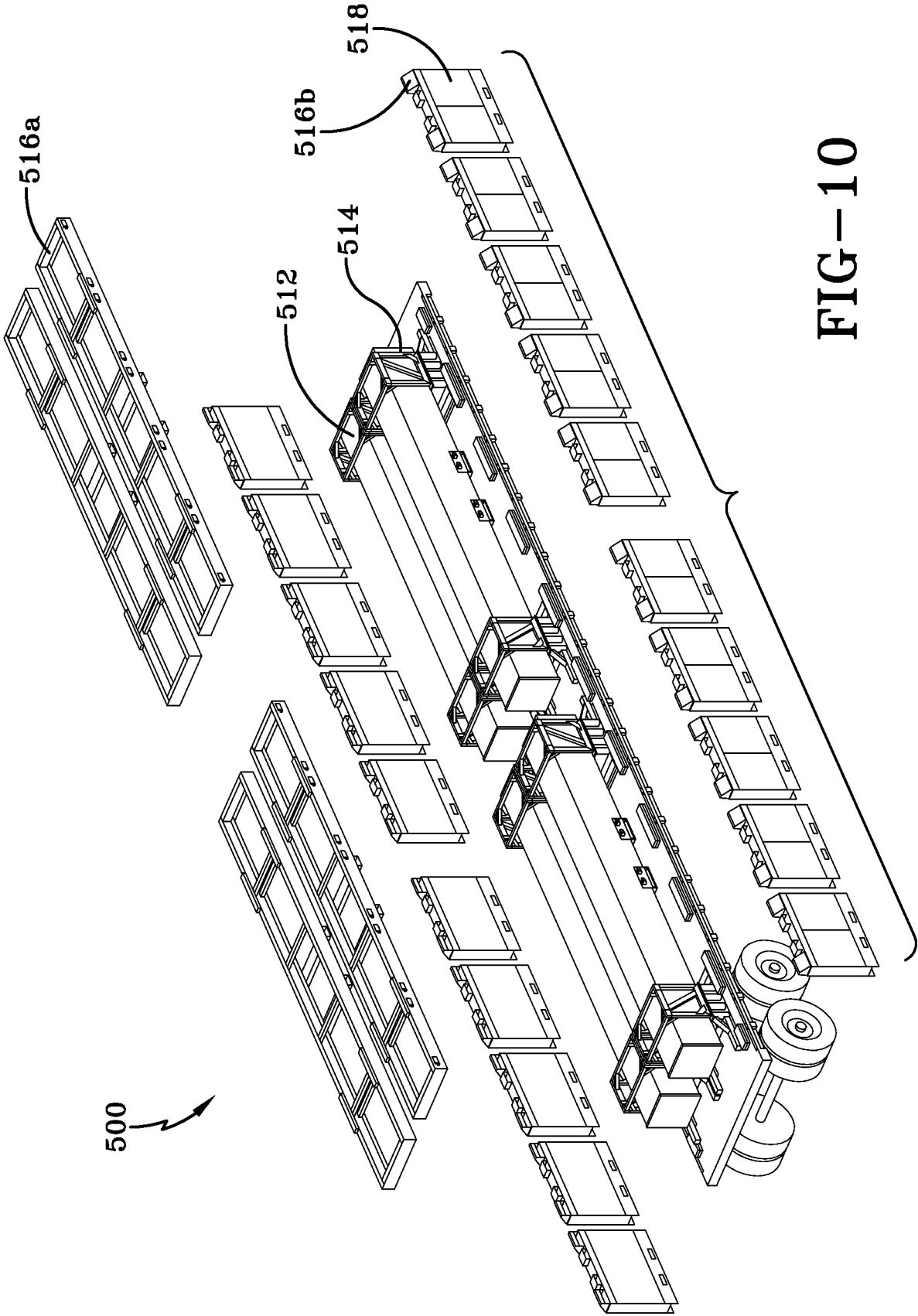


FIG-10

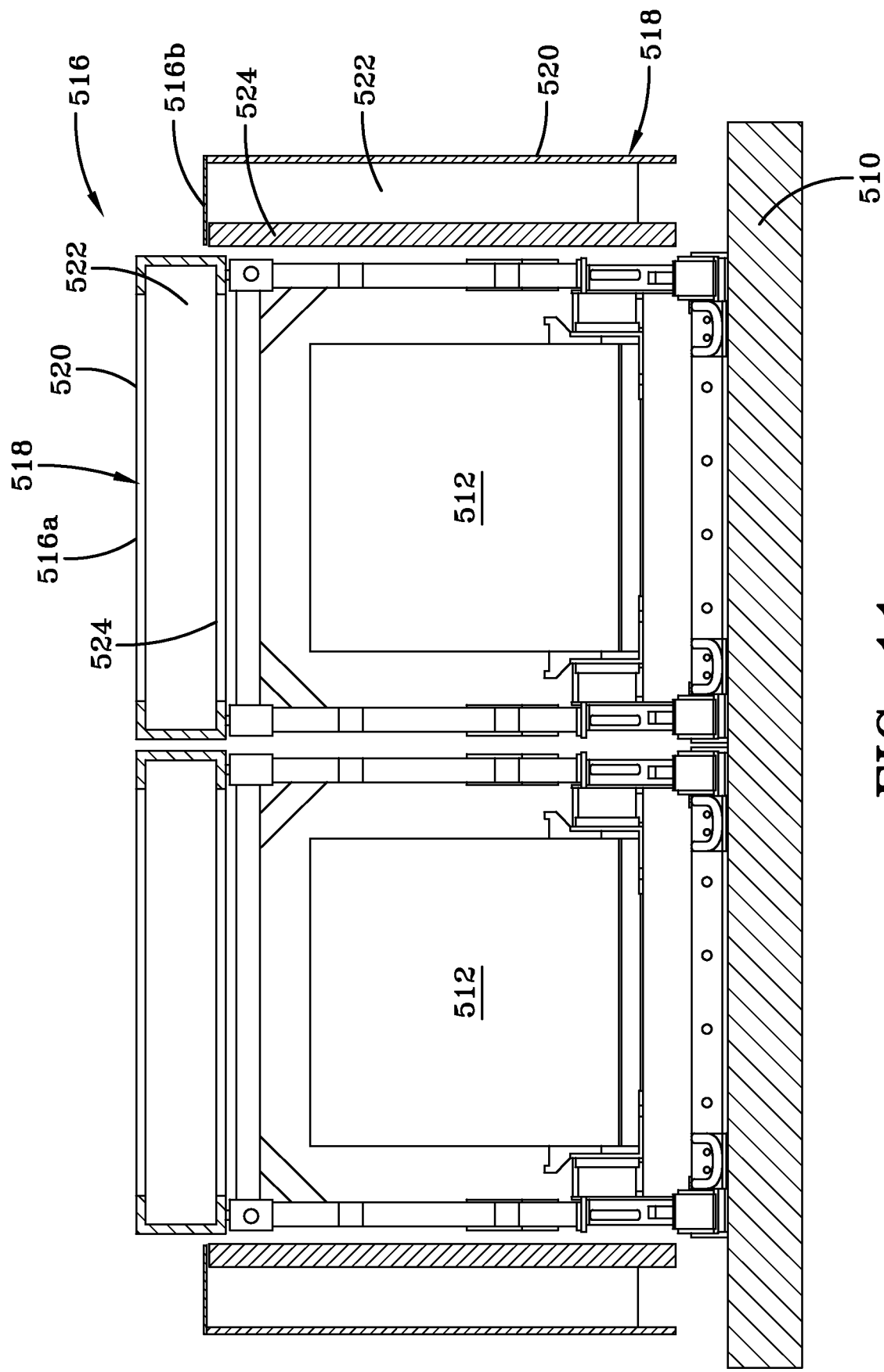


FIG-11

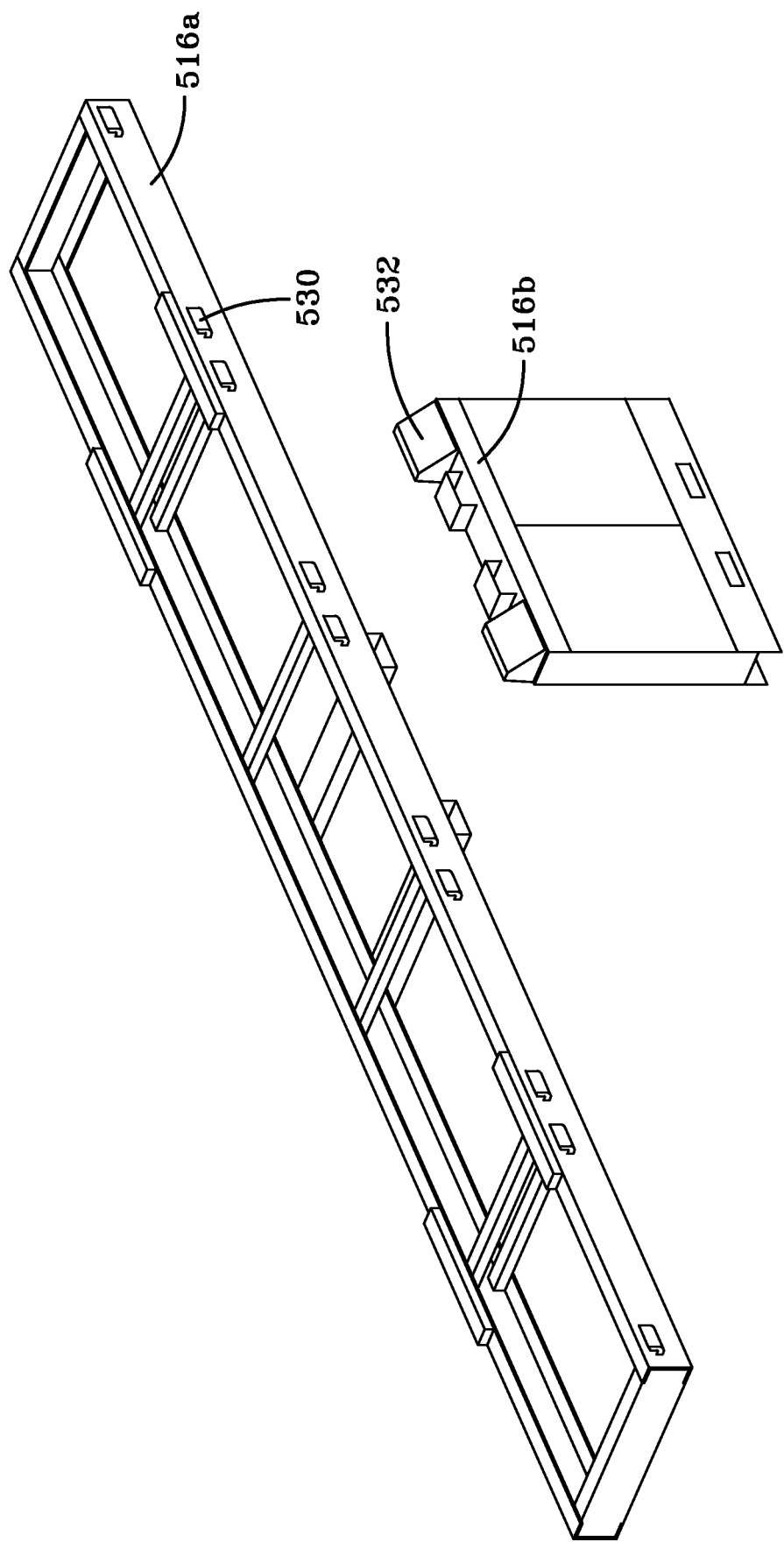
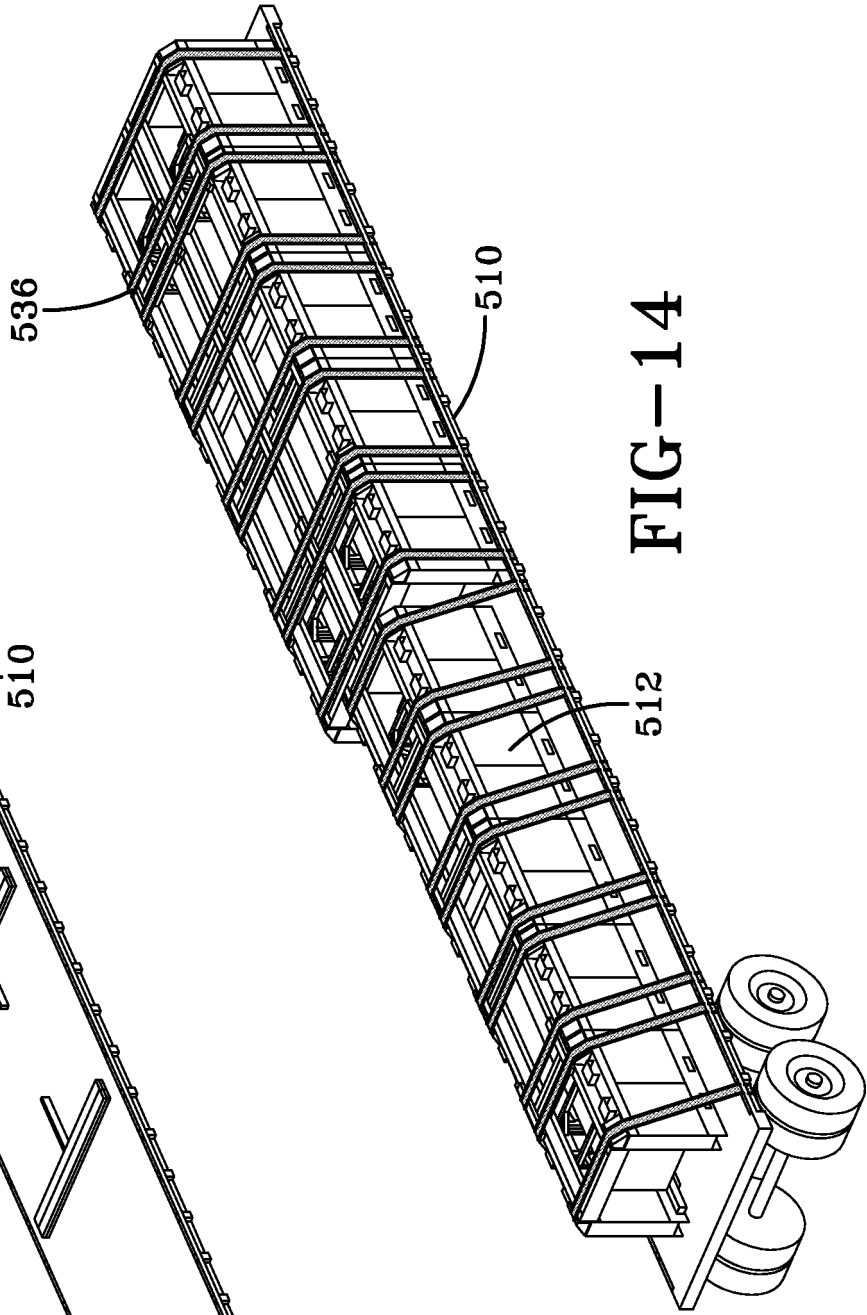
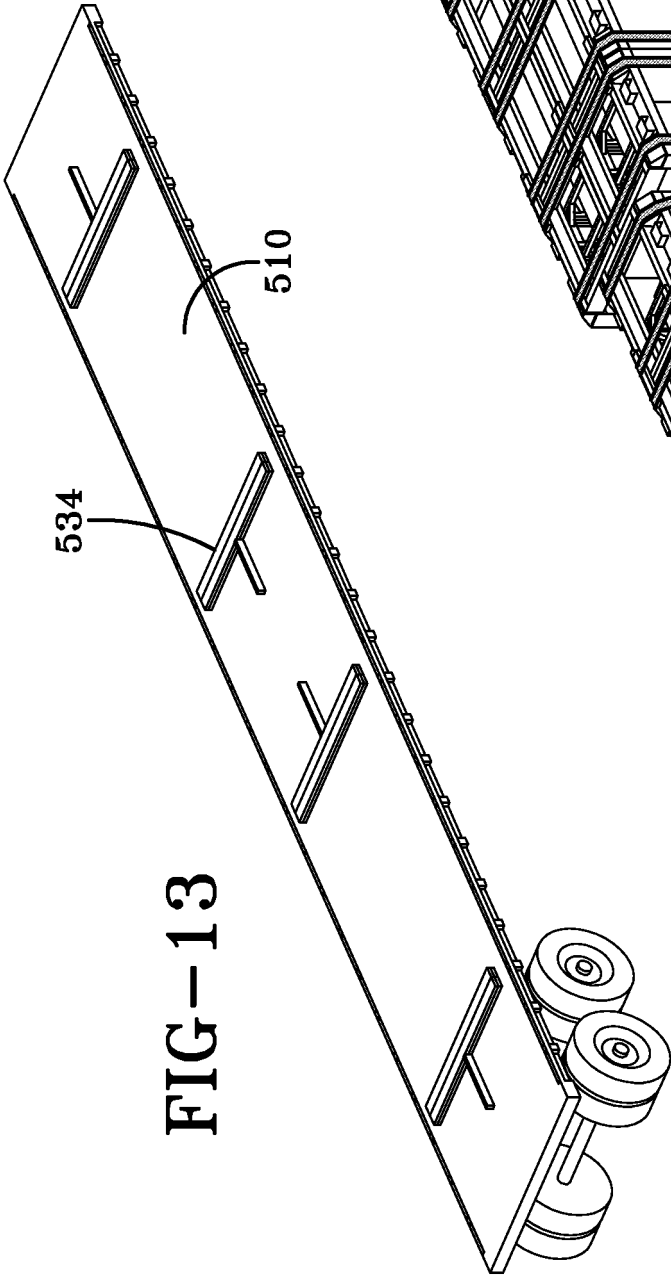
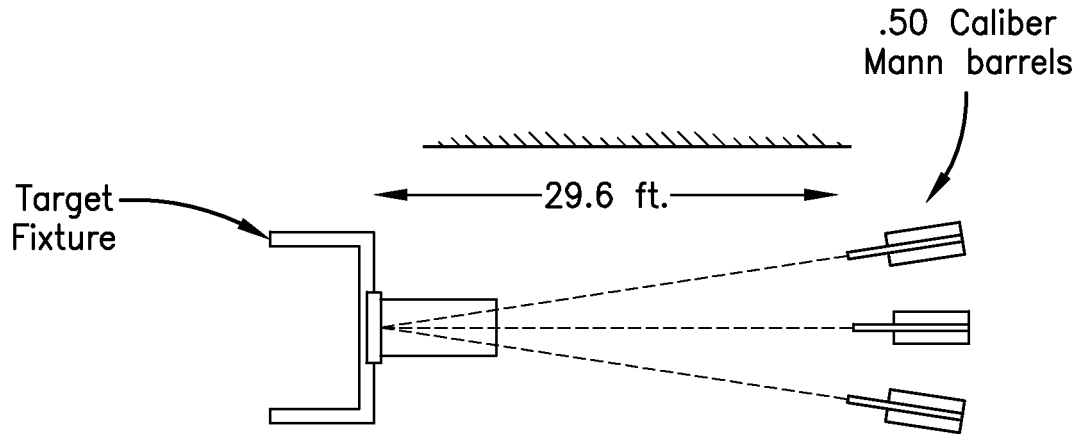


FIG-12





Overall General Test Configuration

FIG-15

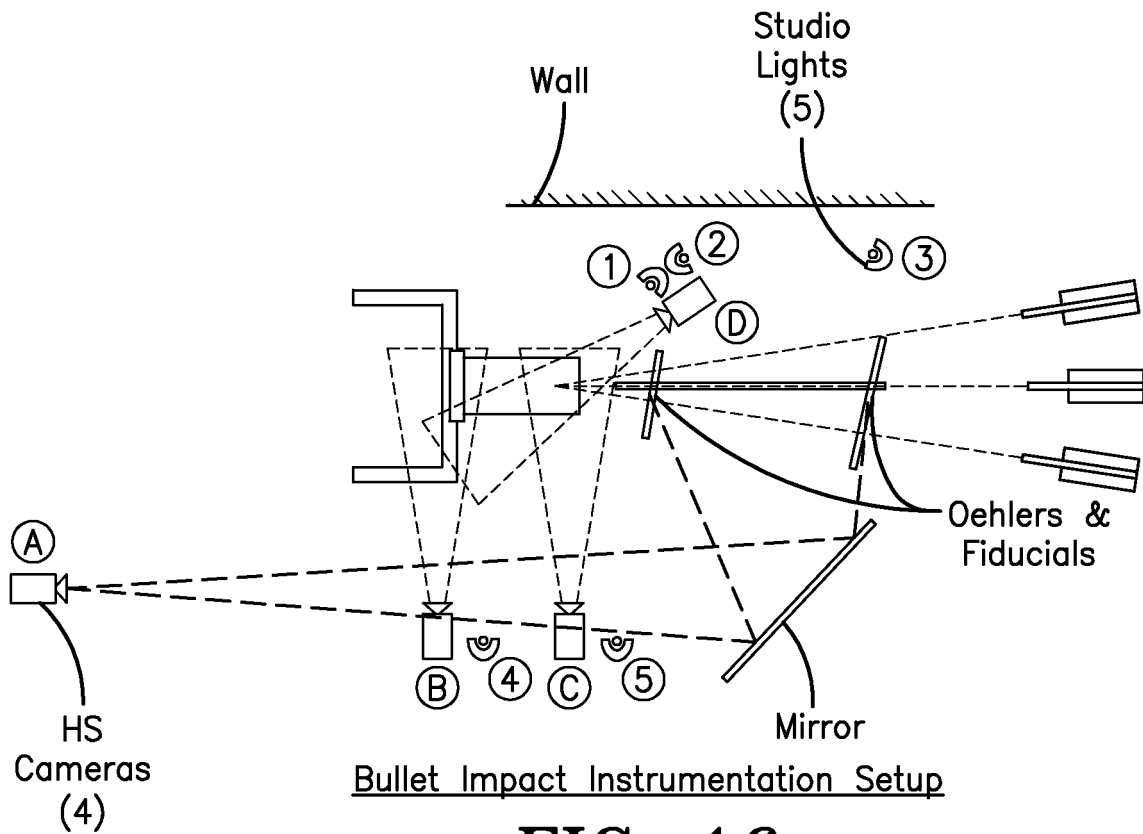


FIG-16

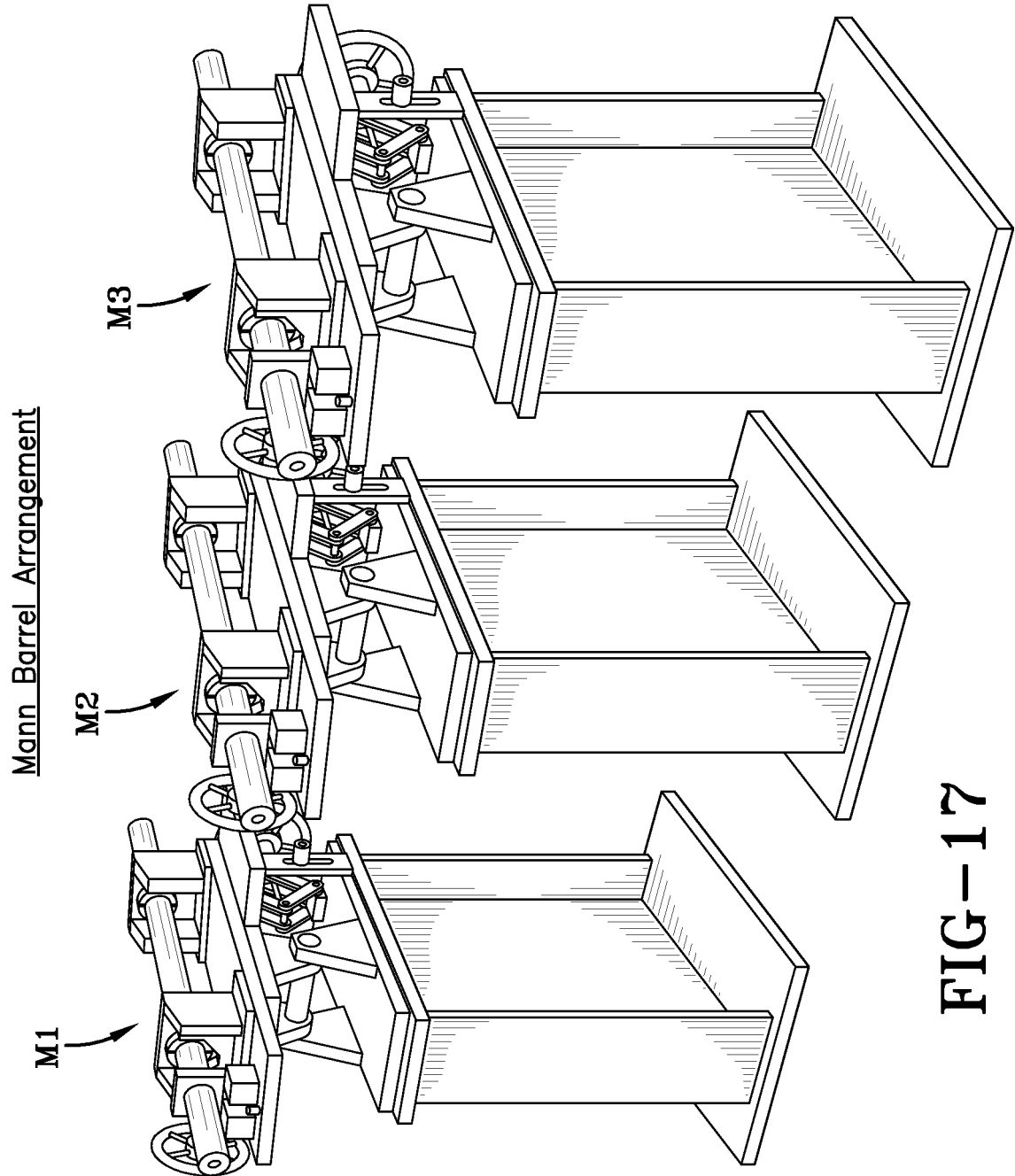


FIG-17

Velocity Screen Setup

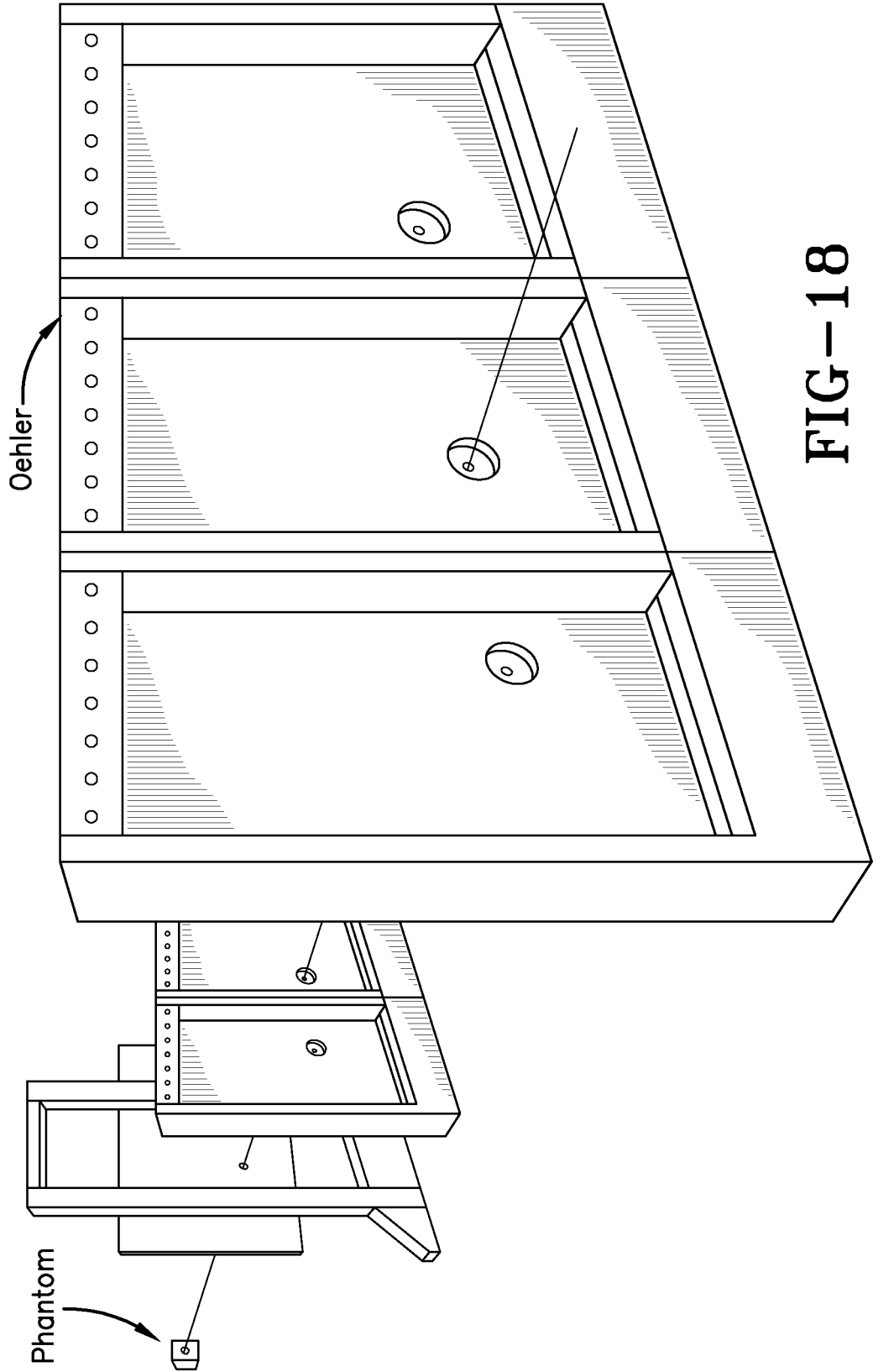


FIG-18

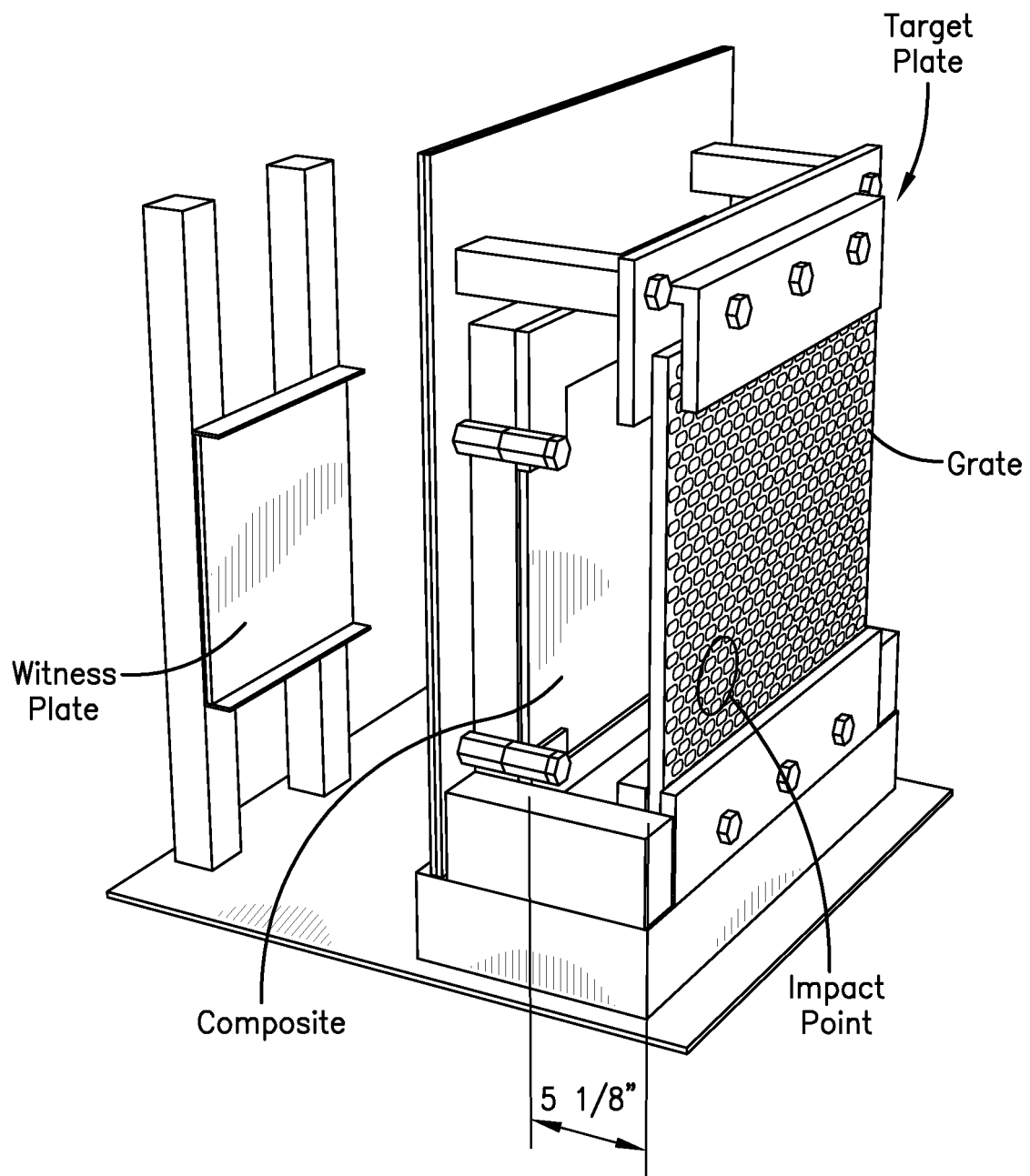


FIG-19

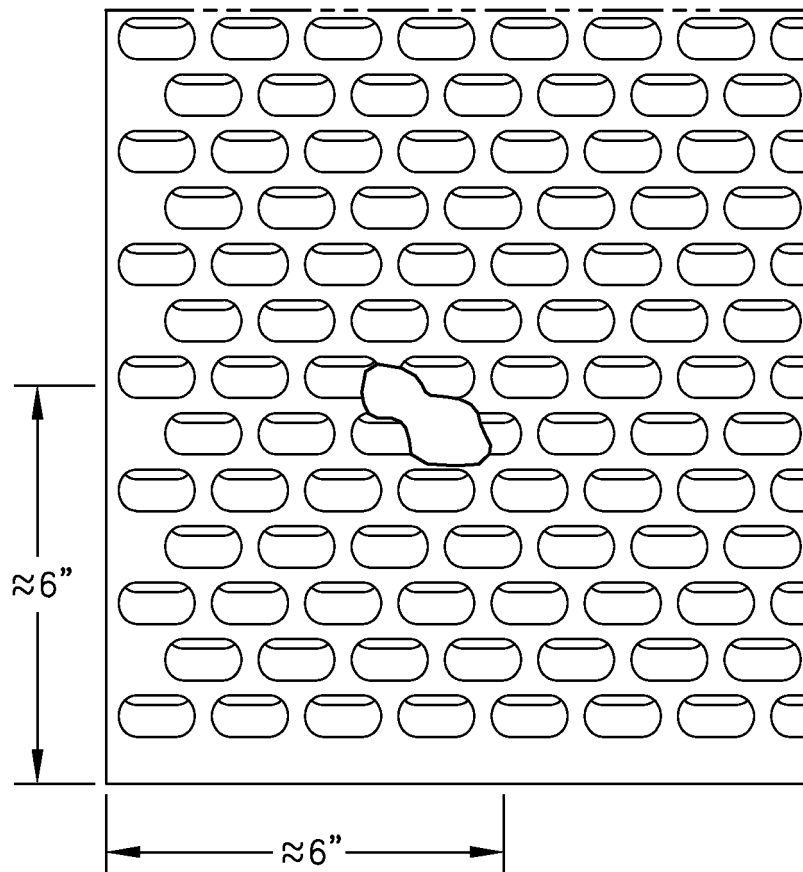


FIG-20

Post-Test Condition

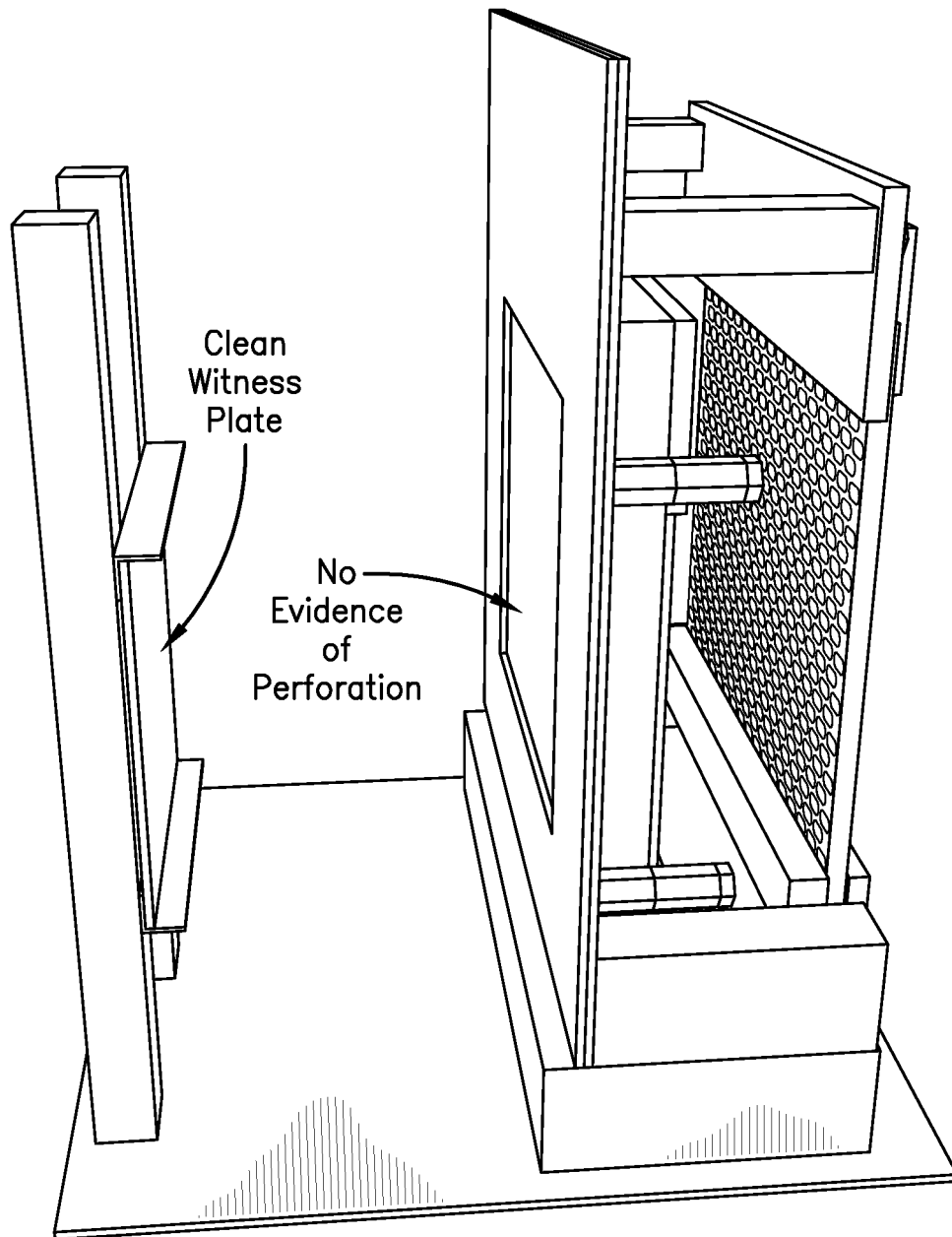


FIG-21

Test Plate Secured to Target Stand

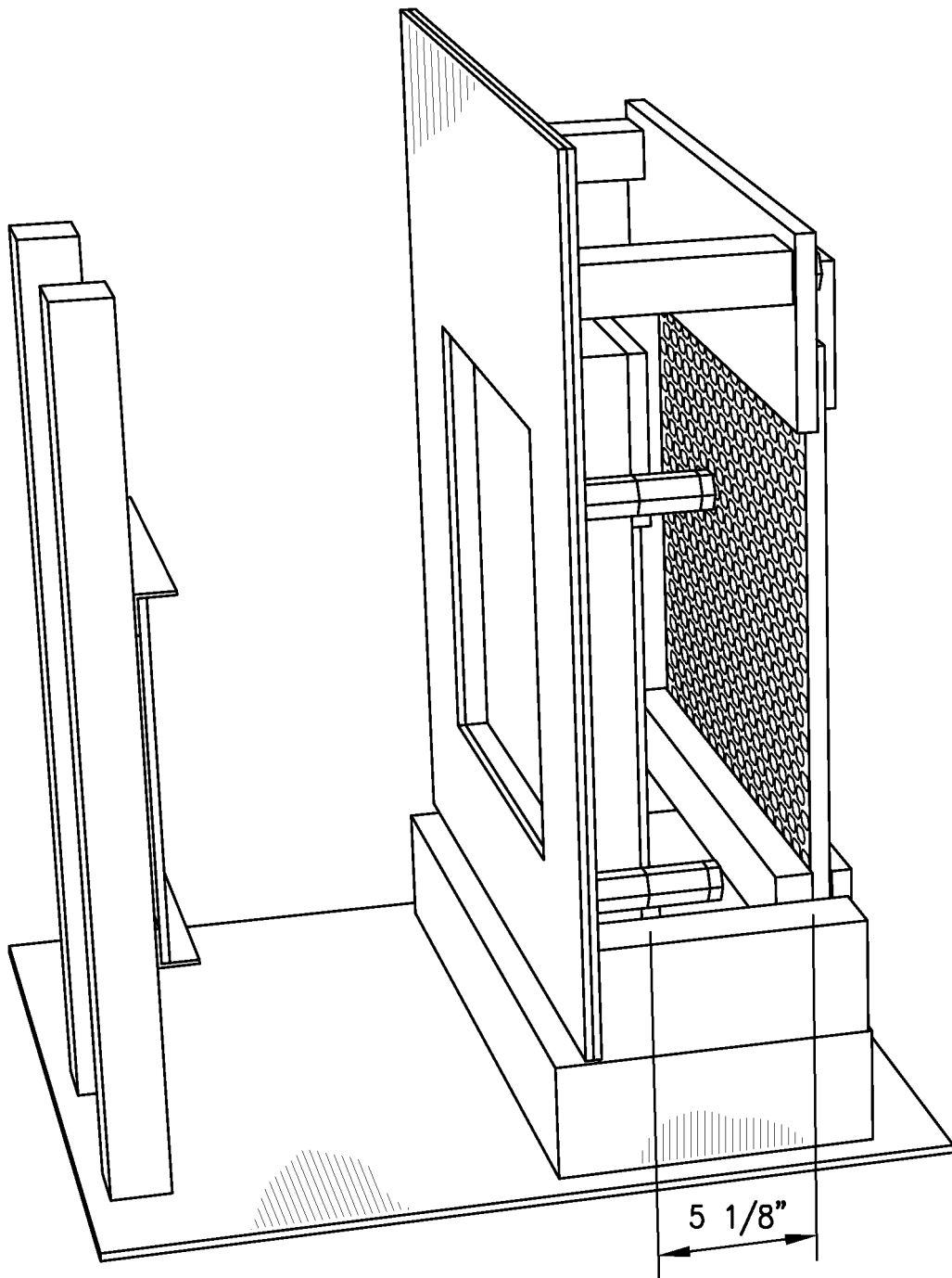


FIG-22

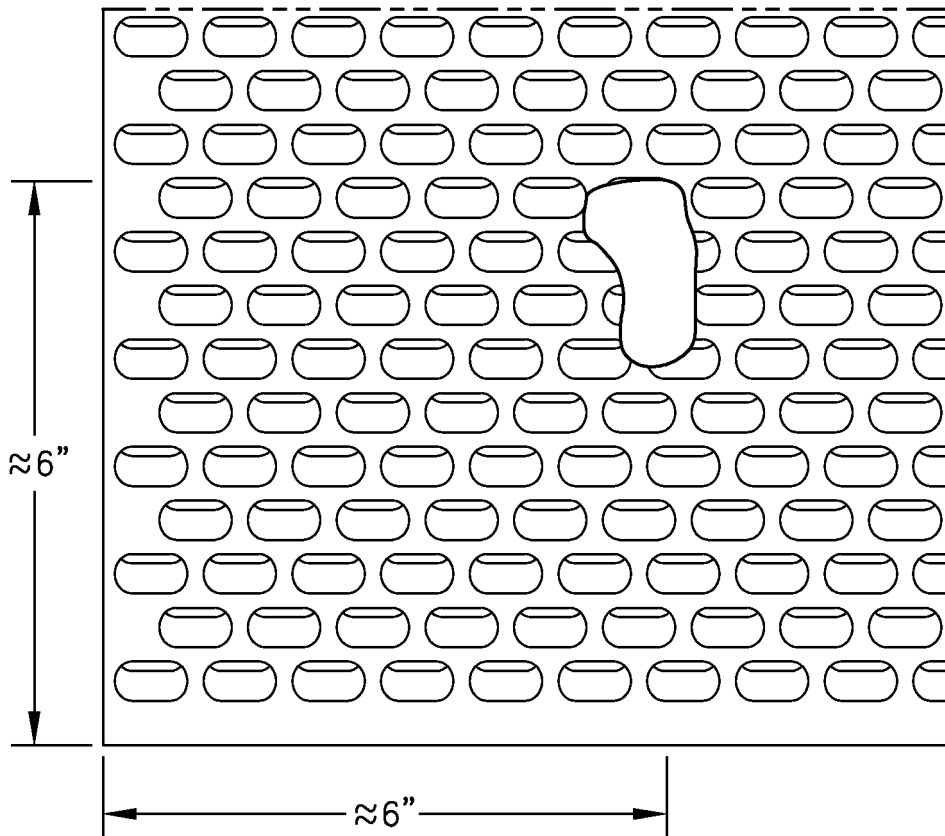


FIG-23

Post-Test Condition

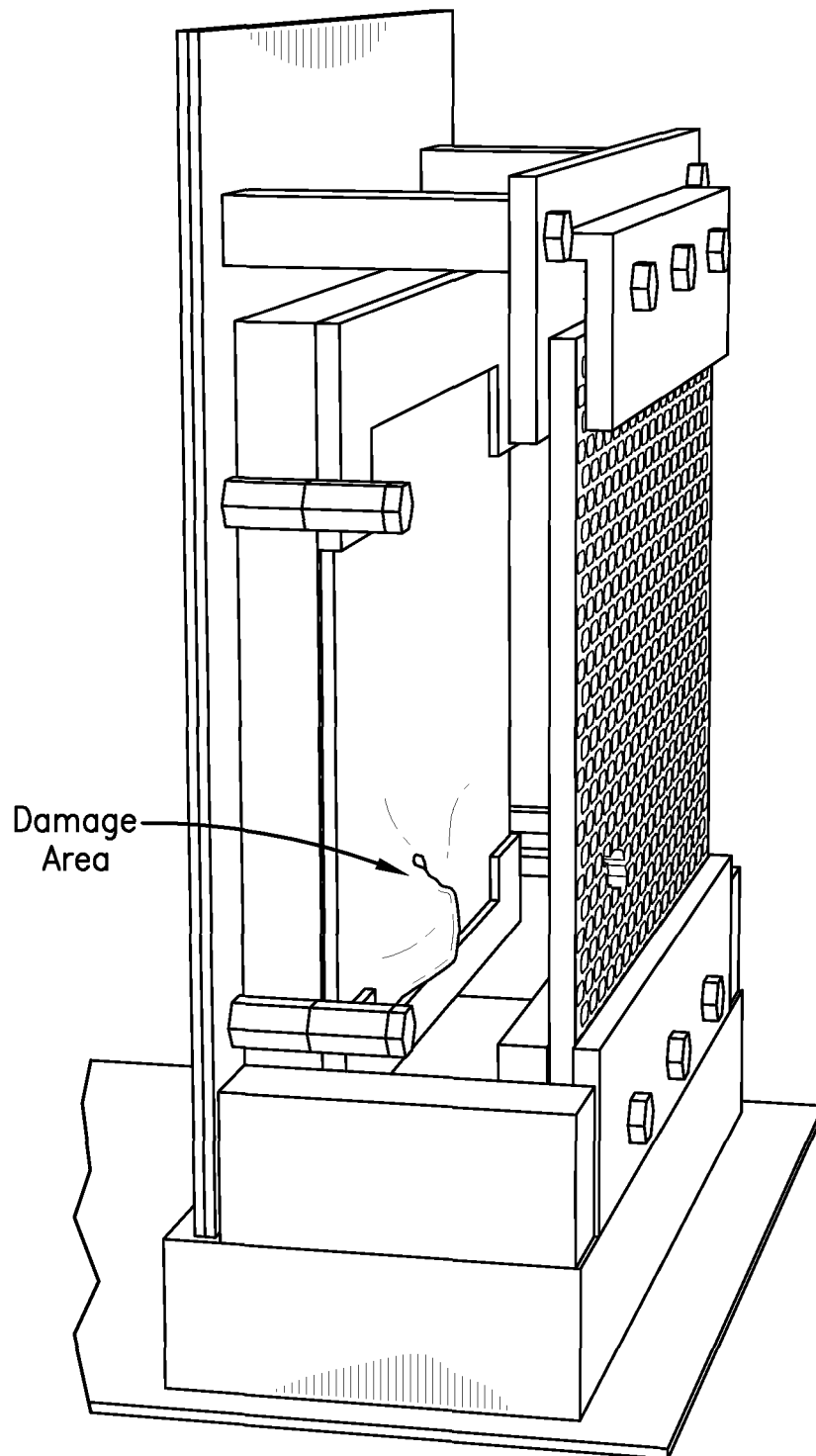


FIG-24

Post-Test Witness Plate

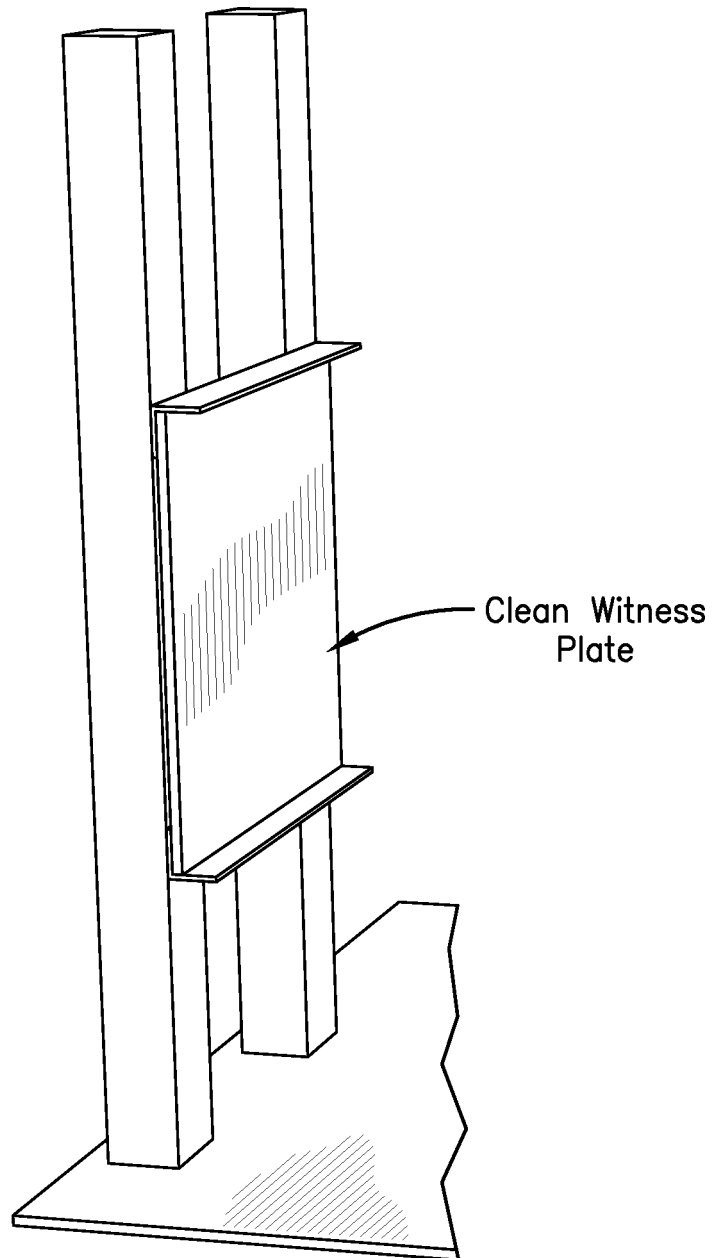


FIG-25

Fragment Impact Test Setup

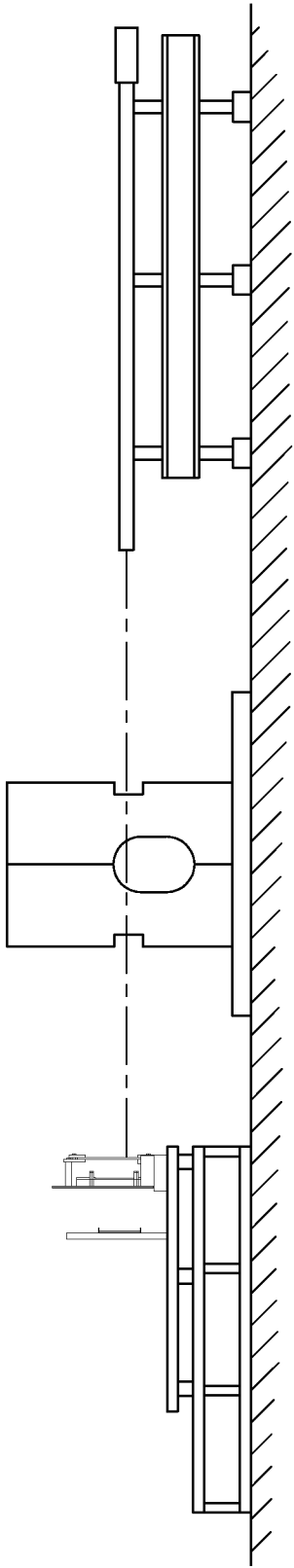
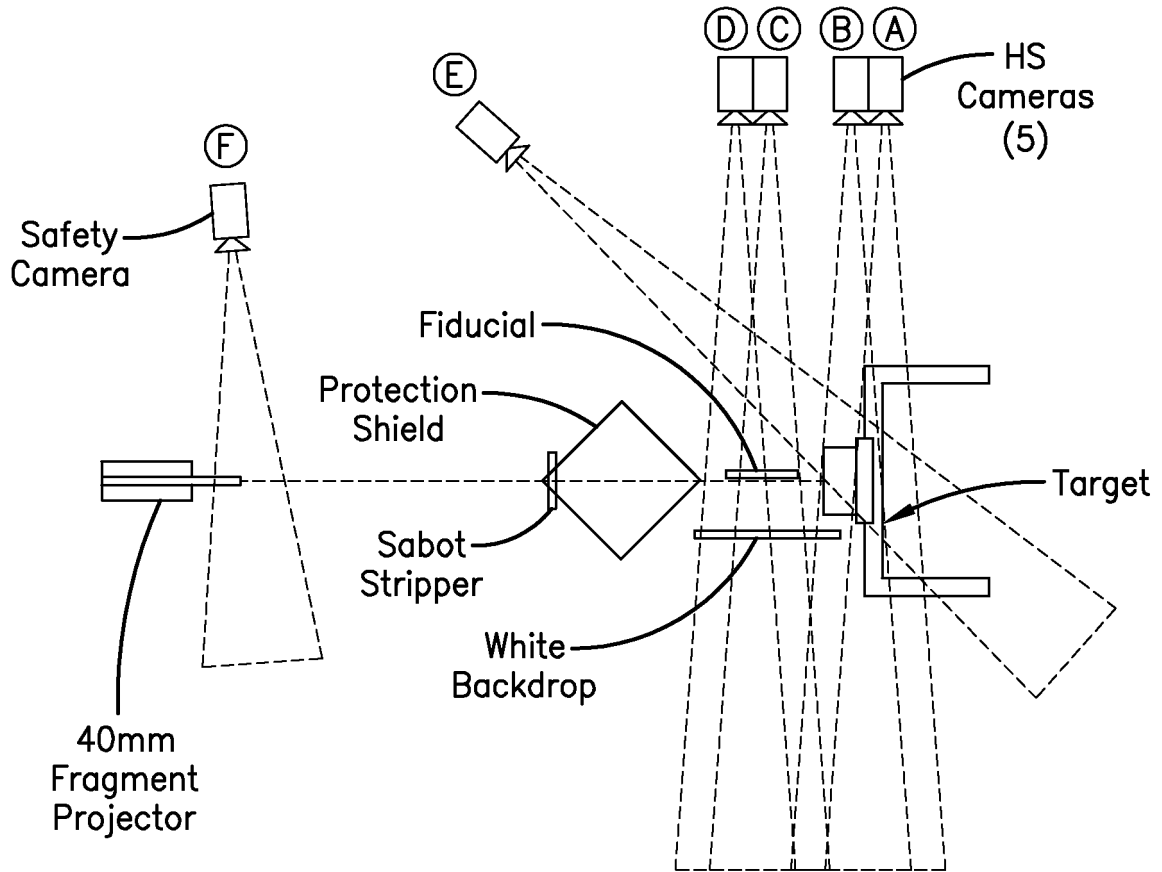


FIG-26



Fragment Impact Test Instrumentation Setup

FIG-27

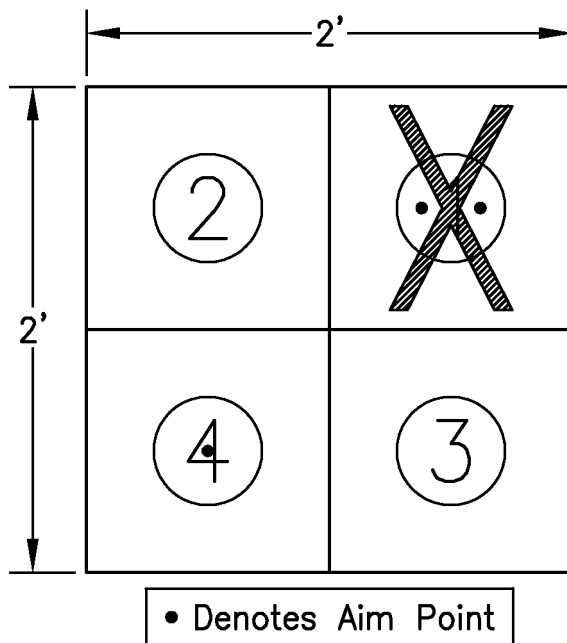


FIG-28

Test Plate Pre-Test Setup

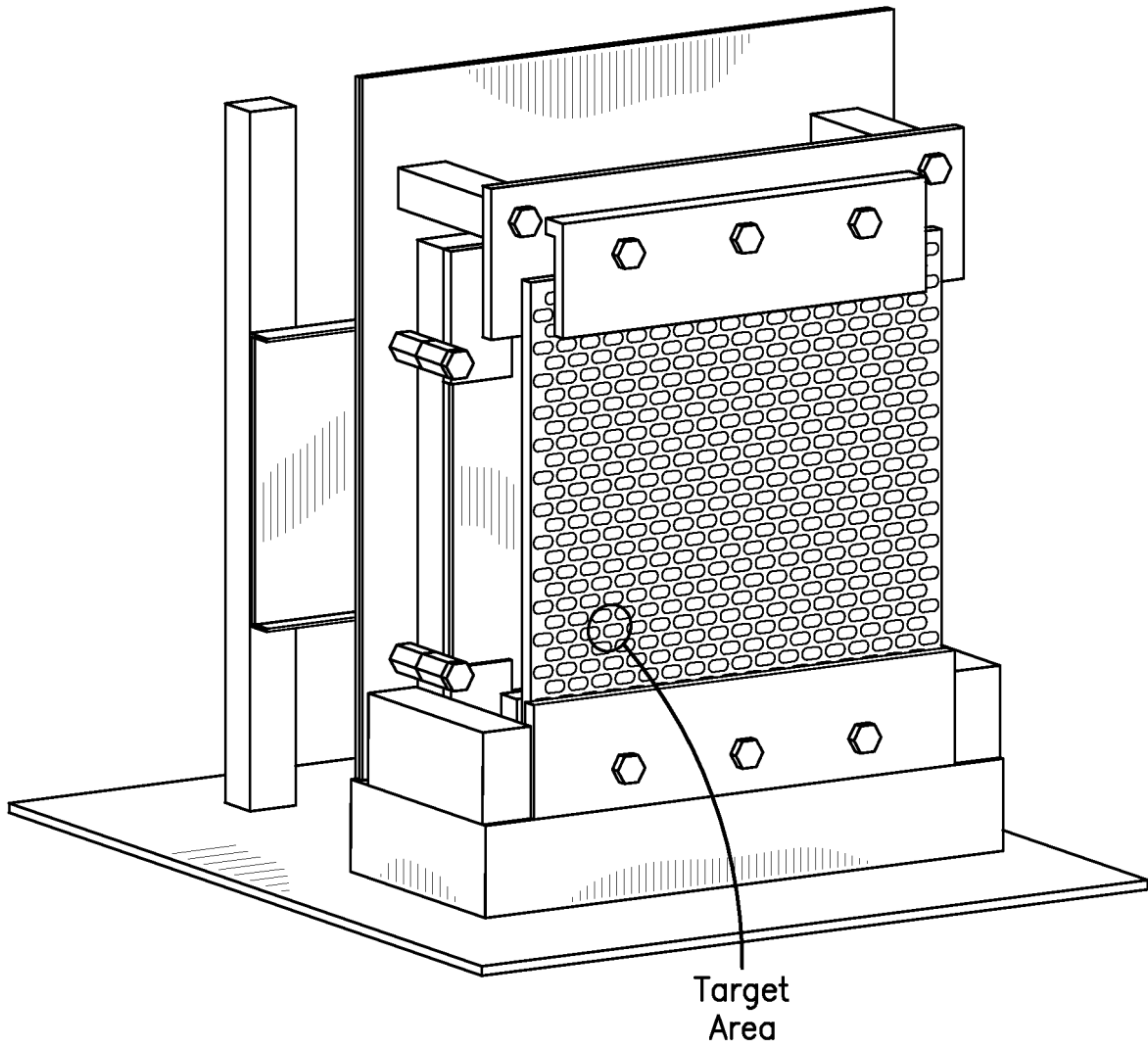


FIG-29

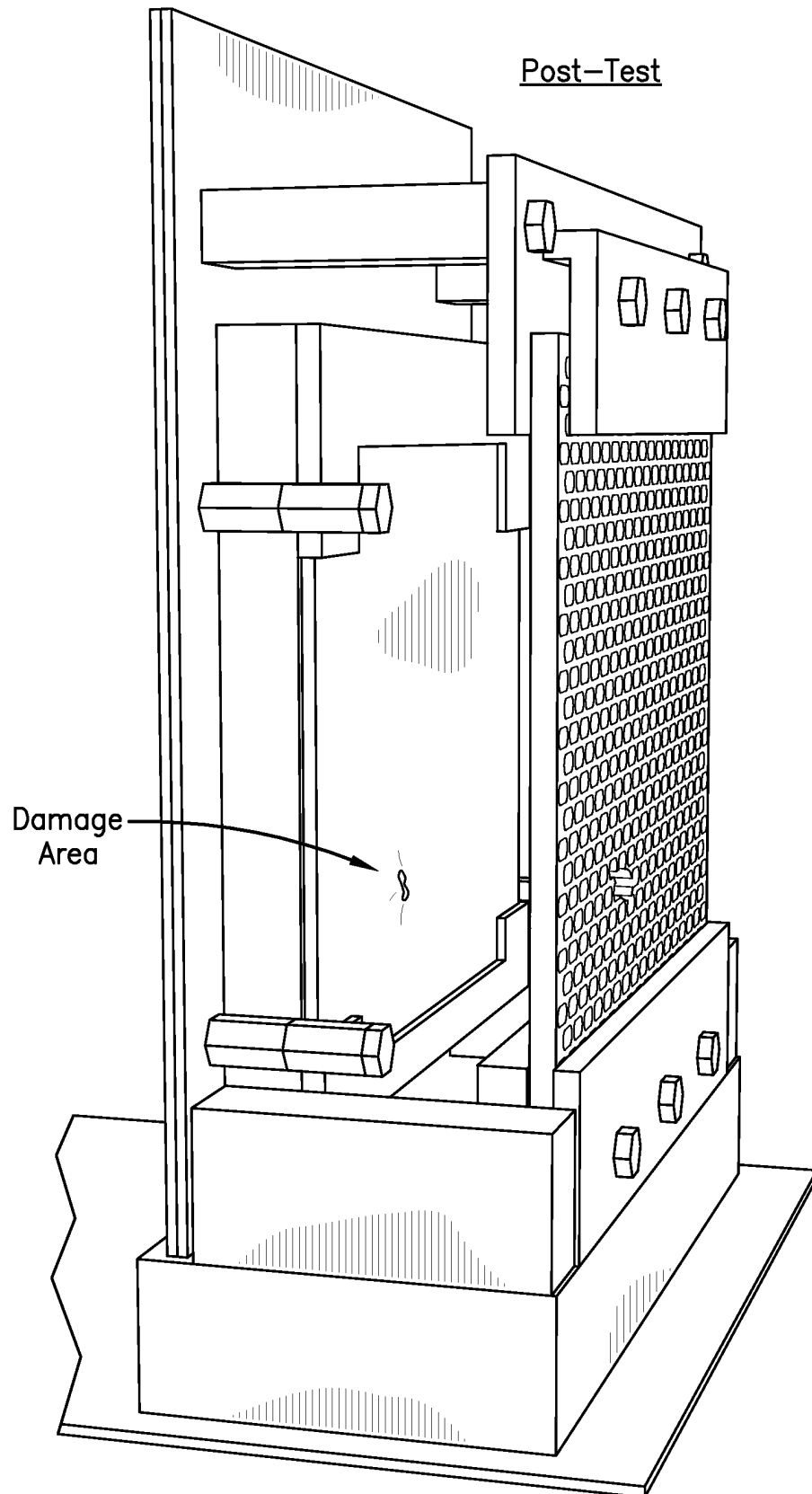


FIG-30

Post-Test Witness Plate

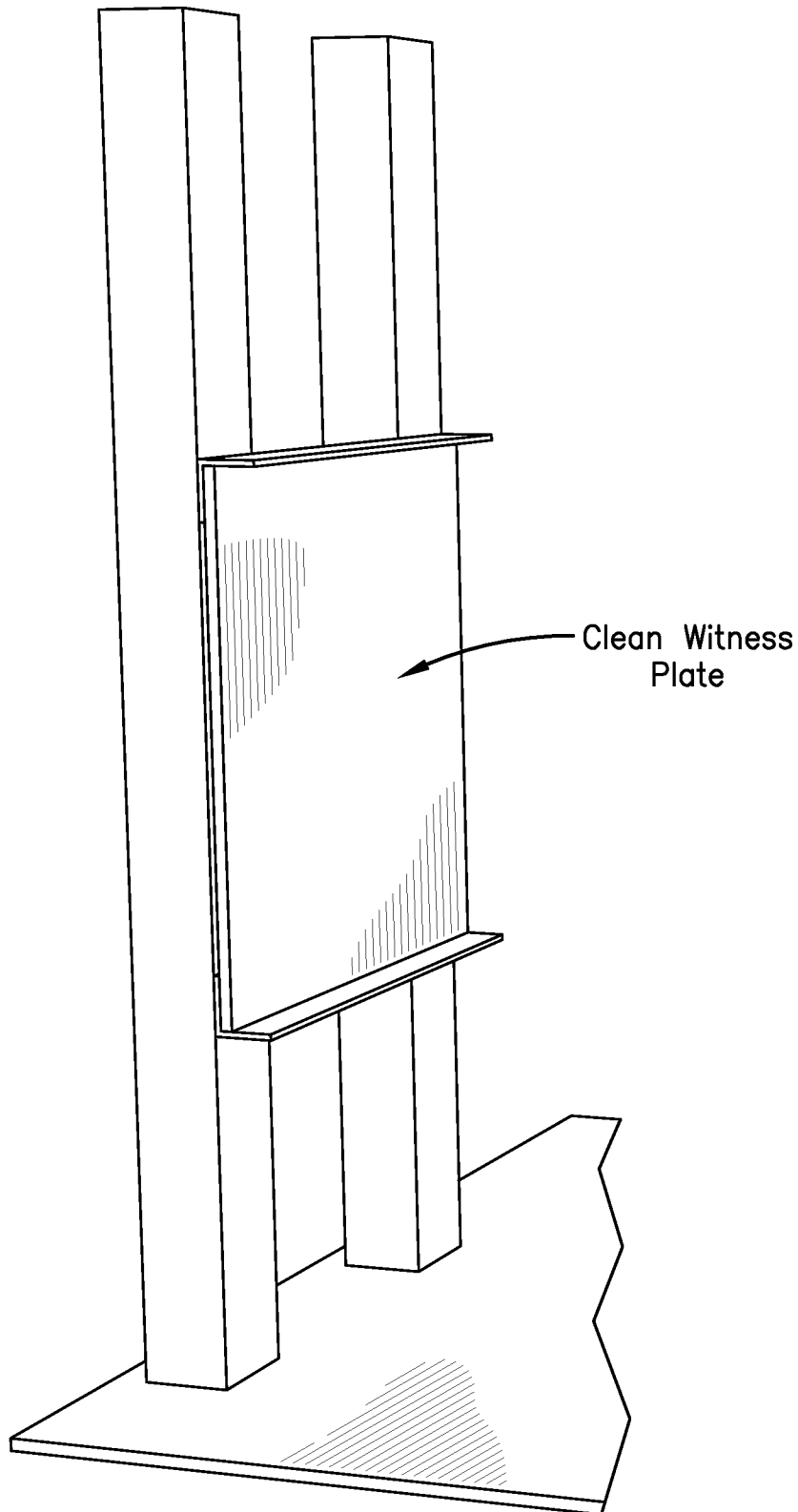


FIG-31

Pre-Test Setup

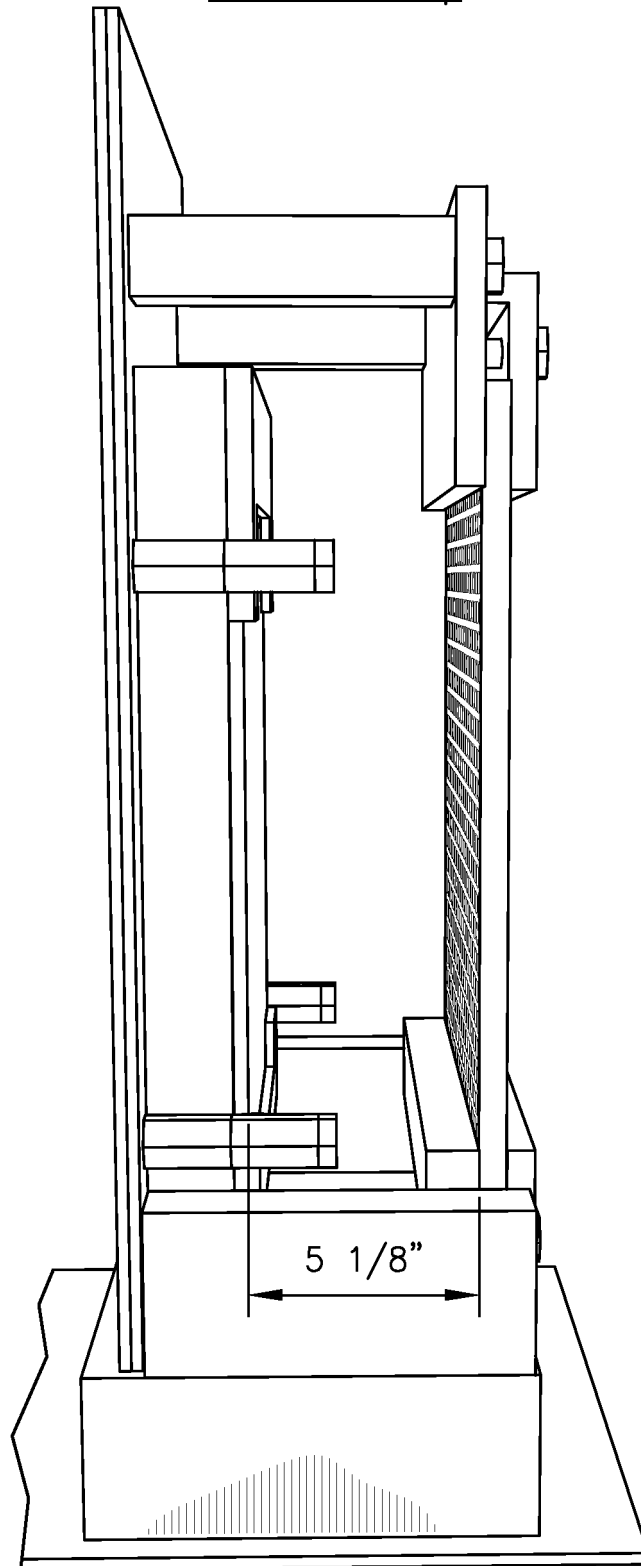


FIG-32

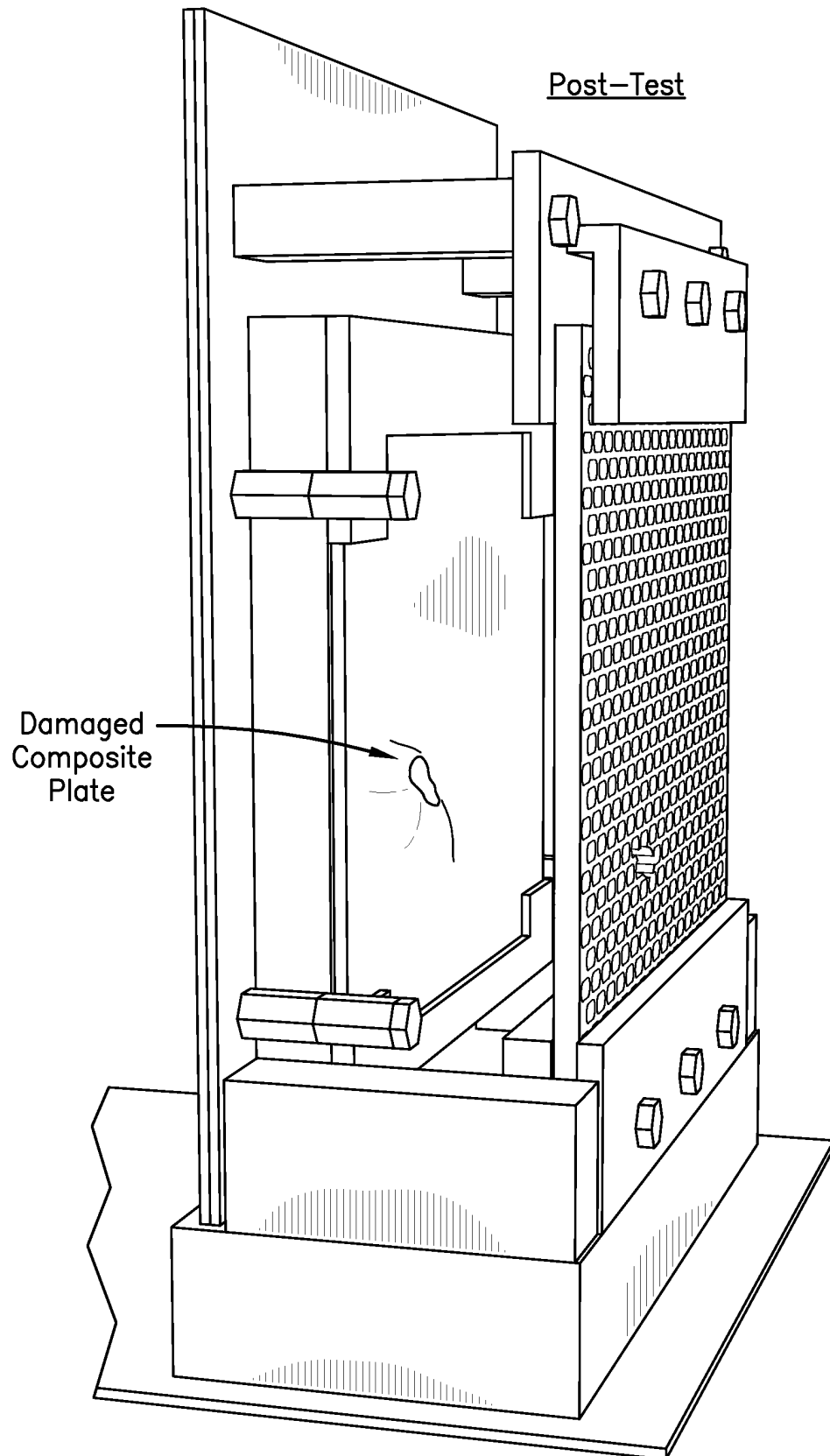


FIG-33A

Post-Test Witness Plate

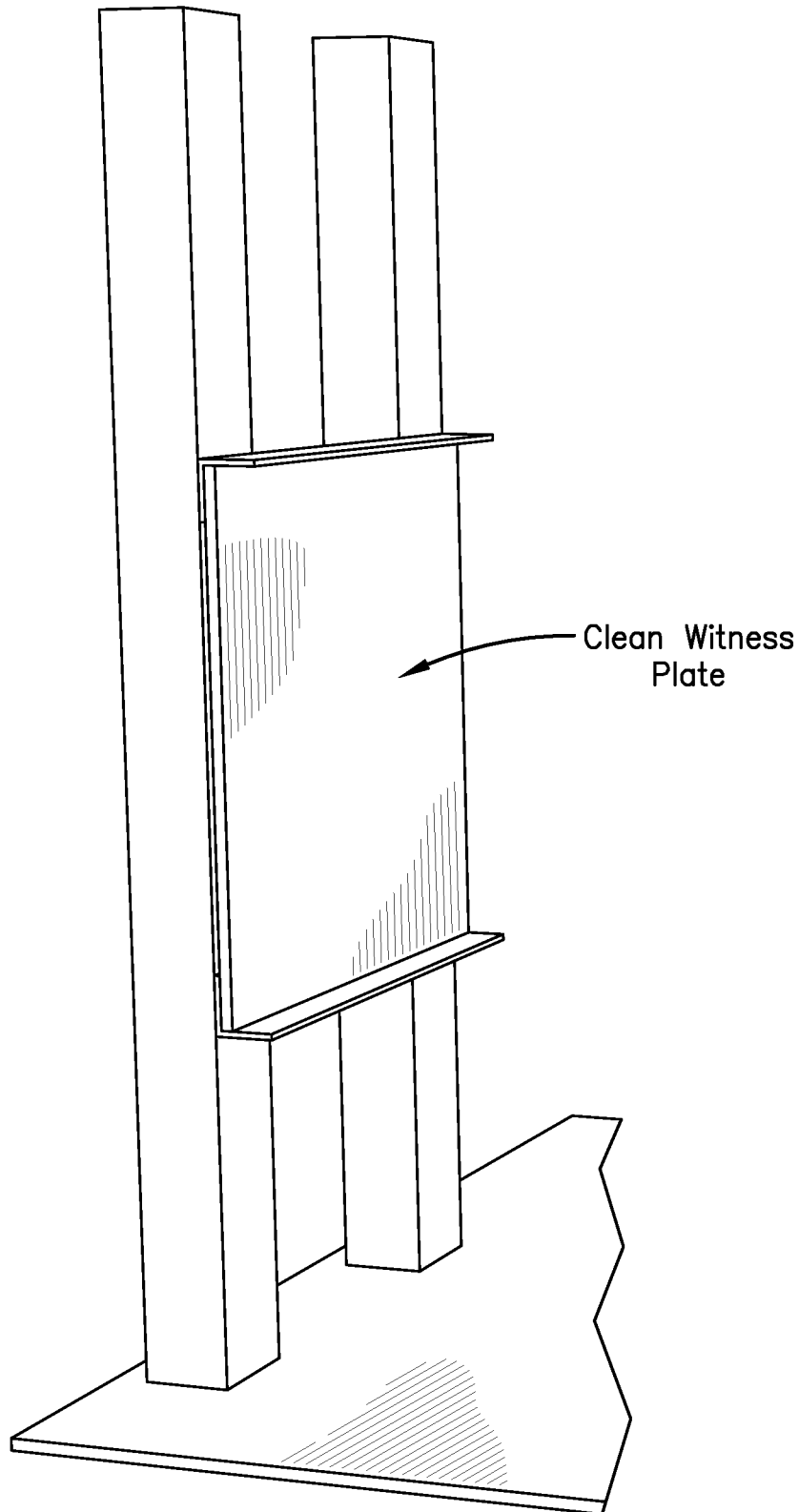
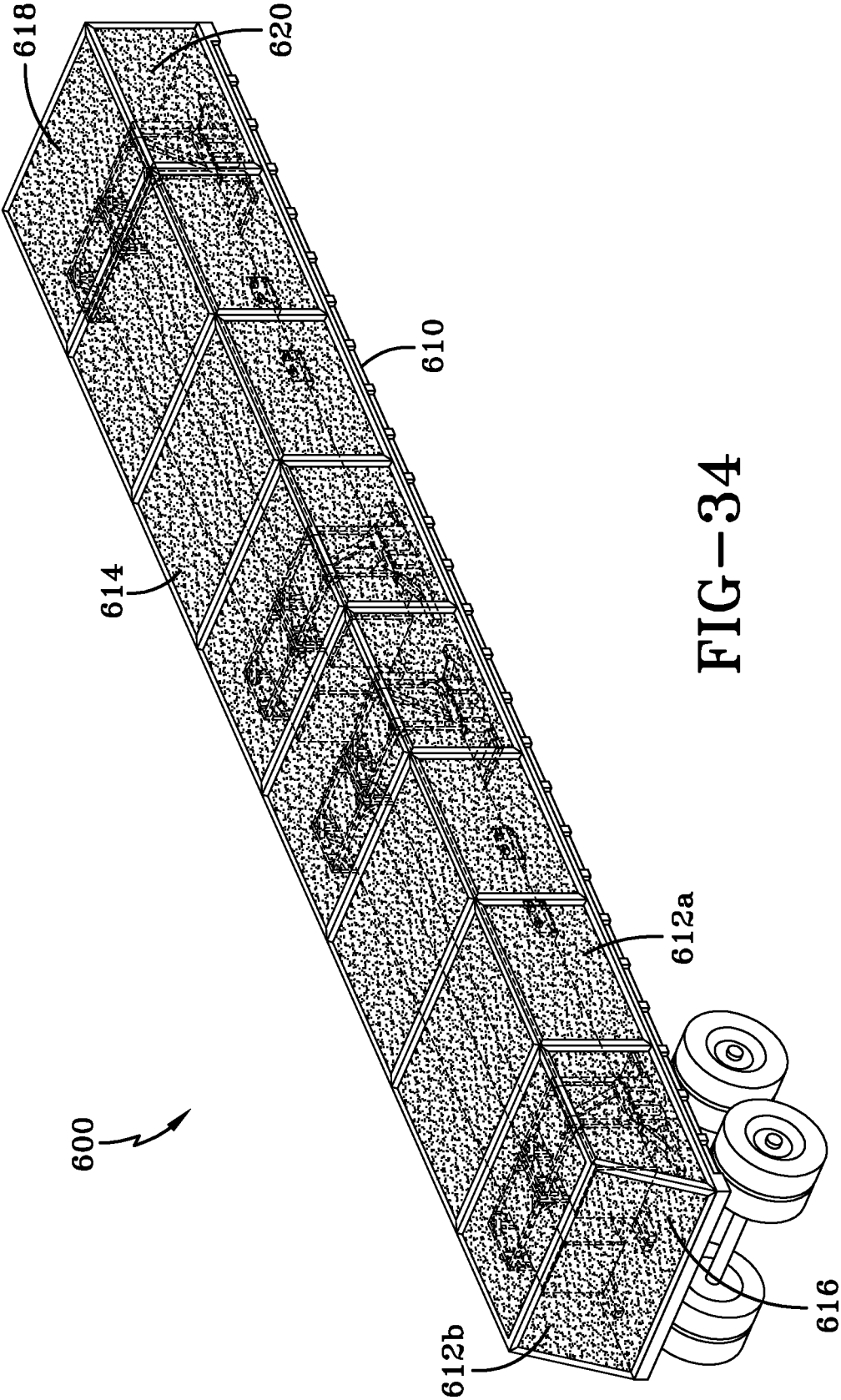


FIG-33B



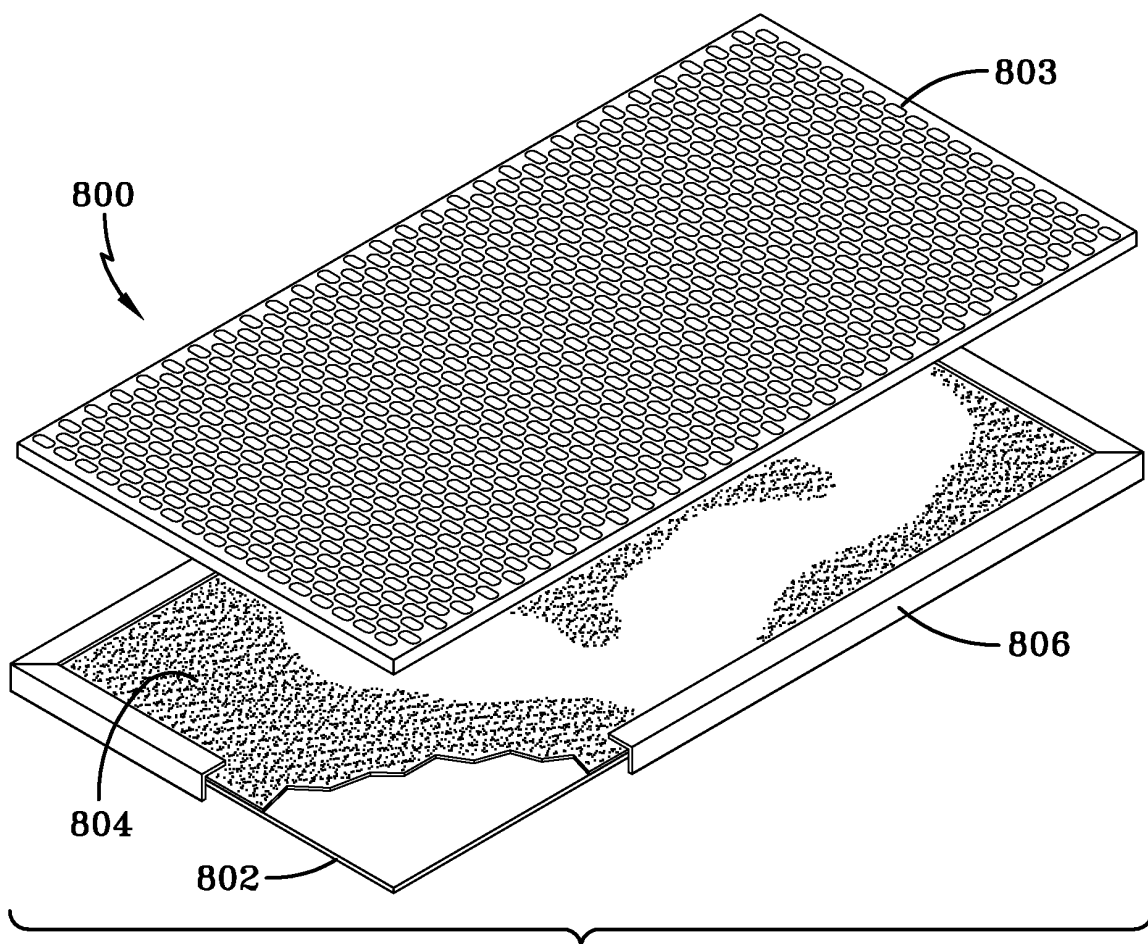
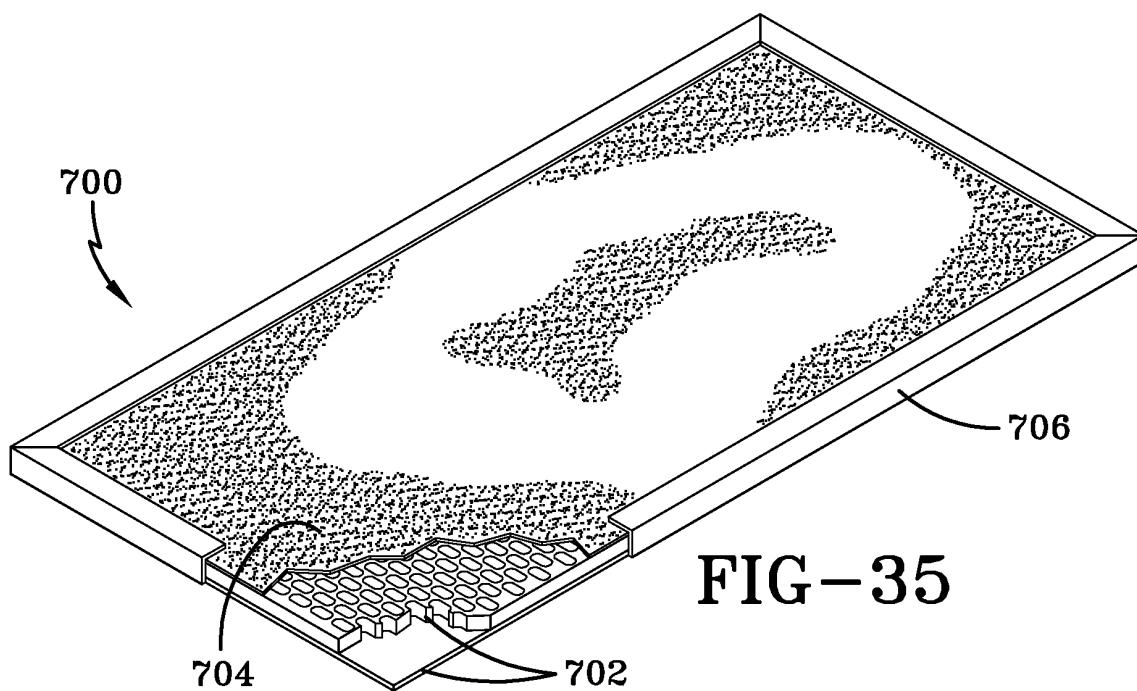


FIG-36

REFERENCES CITED IN THE DESCRIPTION

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