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(57) Zusammenfassung: Bei der Vorrichtung ist eine aus einer Kammerrakel (511), einem Rasterelement (510) und mindestens einem in der Kammerrakel (511) angeordneten ersten Strömungselement (518) bestehende Zuführeinrichtung (51) vorgesehen, die aus einer Mischeinrichtung geladene Tonerteilchen und Trägerflüssigkeit aufweisende Entwicklerflüssigkeit entnimmt und einer Applikatorwalze (520) zuführt. Von der Applikatorwalze (520) geht die Entwicklerflüssigkeit in Abhängigkeit der Potentialbilder auf den Zwischenbildträger (1) über. Zwischen dem Strömungselement (518) und dem Rasterelement (510) liegt eine derartige Spannung an, dass die Tonerteilchenkonzentration in den Nöpfchen des Rasterelementes (510) erhöht wird.

PUBLISHED SPECIFICATION

VERIFICATION OF TRANSLATION

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declare as follows:

1. That I am well acquainted with both the English and German languages, and
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 - (a) The specification of International Bureau pamphlet numbered

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(Signature of Translator)

(No witness required)

Schaumburg Thoenes Thurn Landskron Eckert

New PCT Application

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5 Inventor: Berg et al.

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APPARATUS AND METHOD FOR DEVELOPMENT OF POTENTIAL IMAGES, PRODUCED ON AN INTERMEDIATE IMAGE CARRIER, FOR AN ELECTROGRAPHIC PRINTING OR COPYING DEVICE

- 5 For single-color or multicolored printing of a recording medium (for example of a single sheet or a band-shaped recording medium) made of the most varied materials (for example paper or thin plastic or metal films) it is known to generate image-dependent potential images (charge images) on an intermediate image carrier (for example a photoconductor) that correspond to the images to be printed,
10 made up of regions that are to be inked and regions that are not to be inked. The regions of the potential images that are to be inked are made visible with a developer station (inking station) via toner. The toner image is subsequently transfer-printed onto the recording medium.
- 15 Toner particles and developer fluid containing carrier fluid can thereby be used for inking of the potential images. The carrier fluid thereby exhibits a resistance of greater than 10^8 Ohm*cm. Possible carrier fluids are, among other things, silicon oil and hydrocarbons.
- 20 A method for electrophoretic fluid development (electrographic development) in digital printing systems is known from WO 2005/013013 A2, for example. A carrier fluid containing silicon oil, with ink particles (toner particles) dispersed therein, is thereby used as a developer fluid. More detail in this regard can be learned from WO 2005/013013 A2, which is a component of the disclosure of the
25 present application.

The feed of the developer fluid to the intermediate image carrier can occur via an applicator roller to which the developer fluid is supplied by a raster roller at which a chamber scraper is arranged. The use of chamber scrapers for supplying ink is
30 known from offset printing (EP 1 097 813 A2). The use of a chamber scraper in electrophoretic printing can be learned from WO 2005/013013 A2. A

disadvantage of the known chamber scrapers is that the flow of the developer fluid is not directed in a targeted manner. Eddies can therefore occur and air bubbles can be introduced. The filling of the cups of the raster roller additionally occurs without potential assistance, such that the transition of the toner particles to the raster roller is limited. The achievable toner application per surface element is thereby limited, and with this the inking region or, respectively, the speed of the transition of the developer fluid onto the raster roller, and with this the achievable process speed given constant inking.

10 The design of a raster roller that works together with a chamber scraper is known from DE 44 08 615 A1. In order to enlarge the shape of the cups of the raster roller, a voltage is applied to the chamber scraper and the raster roller. The raster roller is designed such that the shape of the cups can be altered via an electrical voltage.

15 Mathes, H. ("Gibt es die optimale Kammerrakel?" part 1 in Flexo+Tief-Druck 1-2003, p. 54 – 58, January 2003, part 3 in Flexo+Tief-Druck 6-2003, p. 68 – 71, November 2003) describes the realization of an arrangement made up of raster roller and chamber scraper. In order to press the air out from the cups of the raster roller upon filling with ink, it is proposed to direct the ink over the raster roller under pressure. For this a profile body in the chamber scraper can be arranged adjacent to the raster roller, via which profile body the transport channel for the ink is constricted adjacent to the raster roller.

25 According to EP 0 727 720 B1, the cleaning of the residual image (that remains after the development of the potential images on the applicator roller) from the applicator roller occurs via a scraper adjoining the applicator roller. However, an elastic coating of the applicator roller that is required for the neighboring image point formation at the intermediate image carrier is quickly abraded with this.

30 Contrarily, if the contact pressure of the scraper is too weak, a low cleaning efficiency is accepted, which leads to memory effects given high print utilization

(areal degree of coverage of the print image) since not every point of the applicator roller exhibits the same toner quantity/area after a cycle. The cleaning of the applicator roller can also occur via a cleaning roller with scrapers. Since the toner particles are then drawn towards the surface of the cleaning roller, this leads to

5 high stress on the toner particles at the point of action of the scraper on the cleaning roller. This leads to the agglomeration of toner particles and macroscopic thickenings. If the efficiency of the scraper is insufficient, this leads to film formation on the cleaning roller or to the development of memory effects.

10 The problem to be solved by the invention is to specify a device and a method with which a stable, uniformly high level of inking of the potential images on an intermediate image carrier can be achieved at high transfer efficiency. A high printing speed should thereby be possible.

15 A further problem is to achieve a stable inking for a degree of coverage region in stationary operation. Furthermore, a large dynamic range should be possible with regard to inking (very slight level of inking, very high level of inking = inking levels), with regard to a change of inking levels, changing degrees of coverage and changing process speeds. Finally, a high process stability (long-term stability) is
20 aimed for by minimizing stressing of the toner particles.

These problems are solved according to the features of claim 1 and claim 57.

It is advantageous when the function elements participating in the transfer process
25 of the developer fluid on the way to the intermediate image carrier are designed such that, in each transfer process, the accumulation time of the toner particles on the participating function elements due to an electrical field effect and the distance of the participating function elements from one another is less than the respective transfer time of the toner particles from function element to function element.

To avoid the accumulation of toner particles on function elements participating in the transfer process of the developer fluid on the way to the intermediate image carrier, it is advantageous when the function elements are designed such that a force effect towards and away from the respective function element is generated at
5 each participating function element in every cycle in a cyclical process of the transition of the developer fluid from function element to function element.

The force effect can thereby be generated by an electrical field acting on the charged toner particles or by a flow (i.e. a shear effect). The transfer of the toner
10 particles can additionally be supported in the electrical force effect in that the function elements participating in this alternately exhibit a high-ohmic and low-ohmic resistance.

Developments of the invention result from the dependent claims.
15

The device for development of potential images (generated on an intermediate image carrier) of images to be printed initially possesses as a first component a feed device that extracts developer fluid from a mixing device.

The components can possess as function elements

- 20
- a raster roller,
 - a chamber scraper,
 - flow elements (within the chamber scraper).

A field that enables the dosing of a low-concentration (and therewith low-viscosity) fluid is present between these. This has the advantage that the developer
25 fluid can exhibit lower viscosity in the mixing device and the feed device and therewith can be transported more easily. Only on the raster roller is the toner particle concentration increased to the value required for development.

Furthermore, an applicator device that (for example) possesses a applicator roller
30 or applicator belt as a function element is provided as a second component that accepts the developer fluid from the feed device and from which the developer

fluid passes onto the intermediate image carrier dependent on the potential images. In order to optimize the transfer of the toner particles, an electrical voltage is applied between feed device and applicator device such that the extent of the toner particle transfer from the feed device to the applicator device is thereby
5 established. The toner concentration in the developer fluid can thereby additionally be further increased.

A cleaning device that cleans the residual image remaining on the applicator device after the development of the potential images is additionally provided as a
10 third component. The cleaning device can possess the function elements: cleaning roller, cleaning scraper and cleaning flow element.

It is advantageous when an electrical voltage exists between the cleaning device and the applicator device that establishes the transfer of the toner particles of the
15 residual image from the applicator device to the cleaning device.

Moreover, it is advantageous when an electrical voltage that makes the detachment of the toner particles of the residual image from the cleaning roller easier is applied between cleaning roller and cleaning flow element. The result is that the cleaning
20 of the cleaning roller by the adjoining cleaning scraper does not lead to a strong mechanical stressing of the toner particles.

When the raster roller of the feed device or, respectively, the cleaning roller of the cleaning device exhibit [sic] a high resistance, only a minimal electrical current
25 conduction of advantageously $< 1000 \mu\text{A}/\text{m}$, advantageously $< 100 \mu\text{A}/\text{m}$ occurs at the transfer region for the developer fluid between feed device and applicator device or, respectively, cleaning device and applicator device. Potential fluctuations over their surfaces are then advantageously $< 10\text{V}$, and the different potentials can be kept stable. The applicator device (applicator roller) transporting
30 the developer fluid can thus exhibit a small resistance and the voltage drop over its surface can therewith be small, such that the potential difference (this results from

the distance between charge potential or, respectively, discharge potential of the photoconductor and the bias potential of the applicator device symmetrically arranged between them [sic]) present in the developer gap between applicator device and intermediate image carrier (photoconductor, for example) is converted
5 into a large electrical field strength across the developer fluid. For example, the surface layer of the applicator device can be selected such that the resistance is $< 10^8 \Omega \cdot \text{cm}$, advantageously 10^5 to $10^7 \Omega \cdot \text{cm}$.

The function elements transporting the developer fluid from cleaning device, feed
10 device or applicator device can respectively be at least one roller that exhibit [sic] a surface coating to establish its specific resistance according to the criteria indicated above. The resistance of the surface coating of the roller in the cleaning device (cleaning roller) and the roller in the feed device (raster roller) can thereby lie in the range from $10^6 \Omega \cdot \text{cm}$ to $10^{10} \Omega \cdot \text{cm}$, advantageously $5 \cdot 10^8$ to $5 \cdot 10^9 \Omega \cdot \text{cm}$ [sic],
15 and that of the roller in the applicator device (applicator roller) can be more conductive by a factor of at least 10. The function element transporting the developer fluid can also be a belt; however, in the following rollers are assumed in the explanation without limiting the invention to these.

20 It is advantageous when a conditioning device adjacent to the applicator device is arranged as a fourth component in front of the intermediate image carrier (as viewed in the movement direction of the developer fluid). The developer fluid to be fed to the intermediate image carrier can be influenced with this conditioning device such that the toner particles in the developer fluid move towards the surface
25 of the applicator device. A layer that predominantly comprises carrier fluid thereby forms on the surface of the developer fluid, with the result that the unwanted inking of afterimage [sic] locations on the intermediate image carrier is reduced. The conditioning device can be made up of a corotron (for example wire corotron) lying at a potential or of a roller (conditioning roller) lying at an
30 electrical potential. The potential should be selected such that charges in comparison to toner particles of the same polarity are raised on the applicator roller.

If the diameters of the conditioning roller and the applicator roller are selected such that a spacing flow arises between the applicator roller and conditioning roller, the fluid surface on the applicator roller can be smoothed, with the result that the toner particles are more uniformly distributed on the surface of the applicator roller.
5 This leads to an improved print image.

An advantageous realization of the feed device possesses a raster roller with cups and webs and a chamber scraper arranged at the raster roller. The chamber scraper
10 can thereby contain a chamber open to the raster roller, with an inlet and an overflow for the developer fluid, wherein the inlet is designed such that the supplied quantity of developer fluid is greater than or equal to the quantity that passes to the raster roller and that drains off via the overflow as an excess quantity. The sufficient and uniform feed of toner particles into the cups of the raster roller
15 is achieved via a sufficient feed and distribution of the developer fluid in the chamber scraper and via an electrical field assistance within the chamber scraper.

The function of the chamber scraper is further improved in that a first flow element in the chamber is provided adjacent to the raster roller for distribution of the developer fluid transverse to the printing direction in the region of the transfer of
20 the developer fluid to the raster roller. The toner particle concentration in the cups of the raster roller is increased when an electrical voltage is applied between the first flow element and the raster roller. For this the electrical field strength between the first flow element and the raster roller can be selected in a range
25 between 10 to $5 \cdot 10^4$ V/cm.

A further improvement of the function of the chamber scraper is achieved via a second flow element that is arranged adjacent to the first flow element in the chamber and at which an electrical voltage is applied whose polarity is the reverse
30 of that of the first flow element. This serves to stir the developer fluid of the chamber with the remaining fluid located in the cups of the raster roller (which

remaining fluid remains on the applicator roller after transfer of the developer fluid). The second flow element is therefore arranged before the first flow element (as viewed in the rotation direction of the raster roller) and lies adjacent to the raster roller.

5

It is advantageous when both flow elements at the raster roller and at the inner contour of the chamber are arranged and shaped such that a flow of the developer fluid that is parallel to the movement direction of the raster roller surface arises in the gap between the flow elements and the raster roller. No discontinuous cross-sectional changes of the surfaces through which fluid flows (both in the axial direction and radial direction) thereby occur, and there are no zones with a flow speed of zero. The flow elements can be executed as electrically conductive profile elements that are arranged in the chamber adjacent to its opening (parallel to the raster roller) and extend over the width of the chamber and, for example, are attached in an electrically insulated manner at the side walls of the chamber. In order to achieve a large effective surface, the flow elements can be flattened in the direction towards the raster roller. The distance from the flow elements to the raster roller can be set to 10 to 2000 μm , advantageously 100 to 1000 μm .

20 The cleaning device can possess a cleaning roller and a cleaning scraper abutting the cleaning roller. The cleaning scraper can thereby be part of a half chamber into which the scraped-off residual image flows. From there the remaining fluid can be discharged into a mixing device. The half chamber that lies at one electrical potential is designed such that the level of the developer fluid always lies above the cleaning scraper in order to enable that the toner particles present on the cleaning roller can disperse in the half chamber. A fill level sensor that controls a discharge pump can be provided in the half chamber to adjust the level, or the adjustment of the level in the half chamber can occur via an overflow that is arranged above the cleaning scraper.

30

The function of the cleaning device can be improved via a cleaning flow element that is arranged in the half chamber adjacent to the cleaning roller and that is shaped such that a flow in the region between the cleaning flow element and the cleaning roller arises that is parallel to the movement direction of the surface of the cleaning roller and that exhibits no discontinuities in the flow cross-section. For this the distance from cleaning roller to cleaning flow element should be set to 10 to 2000 μm , advantageously 100 to 1000 μm . It is optimal when the cleaning flow element is arranged above the cleaning scraper but partially or completely below the level of the developer fluid in the half chamber. Furthermore, at the cleaning flow element it is appropriate to apply an electrical potential that, for example, is more negative given positive toner polarity than the potential at the cleaning roller and the cleaning scraper. The electrical voltage between cleaning roller and cleaning flow element should be selected such that the toner particles are detached from the surface of the cleaning roller, however an accumulation of the toner particles on the cleaning flow element is prevented. The electrical voltage between cleaning roller and cleaning flow element can be between 10 V and 5000 V, advantageously between 200 V and 2000 V.

A movable element (for example a helical spindle) that can be actively moved via an actuator can be arranged below the fluid level in the lower region of the half chamber, the bowl. Accumulations of toner particles in the half chamber can be avoided with this or, respectively, accumulations present there can be detached.

The advantages of the inventive device can be summarized as follows:

- 25 - The toner particles are deposited in a defined manner on the function elements (raster roller, applicator roller, cleaning roller) or, respectively, detached from the function element within the developer fluid. Fluctuations of the toner particles (charge, diameter) are thereby compensated.
- 30 - The cups of the raster roller are filled with toner particles in a defined manner due to the field support between first flow element and raster roller.

The toner concentration is thereby first increased upon filling; a low-concentration (and therewith more free-flowing) developer fluid can thus be dosed beforehand.

- The increase or, respectively, the stabilization of the toner concentration in the cups of the raster roller initially enables a sufficient feed of toner particles to the applicator roller
 - a) for a high inking level of the intermediate image carrier given a thickness of the developer fluid film on the applicator roller from 10 to 20 μm , advantageously 5 to 10 μm ;
 - b) for high speed, for example $> 1.5 \text{ m/straight edge}$ (transfer between raster roller and applicator roller).
- The use of a conditioning roller has the following advantages:
 1. it leads to the formation of a layer made up predominantly of carrier fluid on the surface of the developer fluid on the applicator roller and therewith to an increase of the limit process speed without unwanted inking of the non-image points;
 2. a stabilization of the film separation of the developer fluid in the gap between conditioning roller and applicator roller, and therewith a smoothing of the developer fluid film, and therewith a smoothing of the developer fluid film on the applicator roller, and therewith a more uniform deposition of toner particles on the intermediate image carrier, is achieved via the suitable selection of the diameter of the conditioning roller and of the applicator roller and their adjustable relative speeds;
 3. the toner particle concentration of the developer fluid film remaining on the applicator roller can be increased via scraping off the carrier fluid located on the conditioning roller. Until then a better free-flowing developer fluid can be dosed. In contrast to this, in the contact between anatomical representation and intermediate image carrier a higher-concentration developer fluid leads to a lesser film thickness of the developer fluid and therewith to an

increase of the electrical field, and thus to an improvement of the deposition of toner particles on the intermediate image carrier, in particular for high process speeds.

- 5 The invention is explained further using an exemplary embodiment that is presented in Figures.

Shown are:

- Fig. 1 the principle representation of an electrographic printing system,
10
Fig. 2 the design of the device with indication of the electrical potentials present at the function elements,
Fig. 3 a further design of the feed device,
15
Fig. 4 a design of the conditioning device within the developer device,
Fig. 5 a second realization of the conditioning device within the developer device.
20

Fig. 1 shows the components of a printing system DS as it is known from WO 2005/013013 A2; this is herewith incorporated into the disclosure. A regeneration exposure 2, a charging station 3, an element 4 for exposure according to the image, a developer device 5, a transfer unit 6 for transfer-printing the developed potential
25 images onto a recording medium 7, an element for cleaning of the photoconductor drum is [sic] arranged along an intermediate image carrier 1 (a photoconductor drum in Fig. 1). The transfer unit 6 possesses an elastic transfer roller 60, a counter-pressure roller 61 and a cleaning unit 62.

- 30 In the following the developer device 5 is addressed in more detail from the components (listed in regard to Fig. 1) arranged along the photoconductor drum;

the design and the function of the remaining components is known and can be learned from WO 2005/013013 A2, for example.

5 The developer device 5 possesses a feed device 51, an applicator device 52, a cleaning device 53 and optionally a conditioning device 54 (Fig. 2).

The applicator device 52 can be an applicator roller 520 or a developer belt which is arranged in contact with the intermediate image carrier 1. In the following an applicator roller 520 is discussed in the explanation without limiting the invention
10 to this. The potential images are developed on the intermediate image carrier 1 with the applicator roller 520. For this the applicator roller 520 feeds a developer fluid (made up of at least one carrier fluid and charged toner particles) to the intermediate image carrier 1. The development occurs in a known manner.

15 The developer fluid is fed to the applicator roller 520 via a feed device 51. This feed device 51 possesses a raster roller 510 with cups and webs and a chamber scraper 511 arranged at the raster roller 510. The chamber scraper is made up of at least one chamber 512, an inlet 513 and an overflow 514. The chamber scraper 511 according to Fig. 1 is described in terms of its function in WO 2005/013013
20 A2. The developer fluid is drawn from a mixing device MS and is fed to the chamber scraper 511 via a first pump 515. The excess developer fluid in the chamber 512 is directed via the overflow 514 into a capture basin 516 and from there the developer fluid can be pumped into the mixing device MS with the aid of a second pump 517.

25

The more detailed design of the feed device 51 can be learned from Fig. 2 and Fig. 3. This contains the chamber scraper 511 with the chamber 512, the inlet 513, the overflow 514 and the raster roller 510 with the cups and webs. A first insulated flow element 518 to which an electrical potential $U_{RW_POT-element}$ can be applied,
30 which first insulated flow element 518 is adjacent to the raster roller 510, is arranged within the chamber 512 of the chamber scraper 511 that is open to the

raster roller 510. In a development, a second insulated flow element 519 that can be supplied with an electrical potential $U_{RW_POT-Element2}$ independent of the first flow element 518 is arranged in the chamber 512. The flow elements 518, 519 are situated parallel to the raster roller 510 and extend across the width of the chamber
5 512. They can be attached in an electrically insulated manner on the side walls of the chamber 512 and can consist of an electrically conductive profile element. The chamber 512 can likewise lie at an electrical potential $U_{Chamber}$, the raster roller 510 at a potential U_{RW} .

10 The sufficient feed of toner particles in the developer fluid into the cups of the raster roller 510, which is necessary for a high inking level of the potential images on the intermediate image carrier 1 at high printing speed, is achieved via a sufficient feed and distribution of the developer fluid into the chamber scraper 511 and via an electrical field assistance within the chamber scraper 511. An optimum
15 of volumes of the developer fluid to be streamed along the raster roller 510 and the achievable electrical field strength is achieved as a result of the distance between raster roller 510 and the first flow element 518 provided with the potential $U_{RW_Pot-Element}$.

20 The supplied developer fluid is distributed via the inlet 513 into the chamber scraper 511 such that

- the fluid quantity supplied via the inlet 513 is greater than or equal to the quantity that can drain off via the cups of the raster roller 510 and the overflow 514;
- 25 - the excess quantity of developer fluid can drain off via the overflow 514;
- the flow elements 518, 519 arranged in the chamber 512 enable and support the distribution of the developer fluid transverse to the printing direction;
- the flow elements 518, 519 are arranged and shaped relative to the raster roller 510 and relative to the inner contour of the chamber 512 such that no
30 discontinuities of the developer fluid can occur in the flow cross-section, and as a result a flow in the gap between the flow elements 518, 519 and

raster roller 510 arises that is parallel to the movement direction of the surface of the raster roller 510.

5 The electrical field assistance is achieved via the electrical voltage between the first flow element 518 and the raster roller 510. The voltage can optionally exhibit a superimposed alternating voltage portion.

10 The arrangement and contour of the first flow element 518 thereby has the effect that no field strength spikes arise, and the region between the first flow element 518 and the raster roller 510 is always filled with developer fluid. The achievable field strength is correspondingly clearly higher than the blowout field strength and lies in the range between 10 to $5 \cdot 10^4$ V/cm.

15 Optionally, the second flow element 510 can be used at which a straight alternating voltage or an alternating voltage superimposed with a direct voltage with reversed polarity can be applied. It is arranged before the first flow element 518 (as viewed in the rotation direction of the raster roller 510). The electrical field between the second flow element 519 and the raster roller 510 thus serves to stir the developer fluid with the remaining fluid located in the cups of the raster roller 510.

20 Contrarily, the field between the first flow element 518 and the raster roller 510 serves to increase the toner concentration in the cups of the raster roller 510.

25 Via this realization of the feed device 51, the cups of the raster roller 510 are filled with toner particles in a defined manner via field assistance between the first flow element 518 and the raster roller 510. The toner concentration is thereby only increased upon filling the cups of the raster roller 510; a low-concentration (and therewith better free-flowing) developer fluid can thus be dosed beforehand.

30 The cleaning device 53 according to Fig. 2 possesses a cleaning element (realized as a cleaning roller 530 or cleaning belt) that abuts the applicator roller 520; in the following the cleaning roller is used as an example in the discussion. A cleaning

scraper 531 rests on the cleaning roller 530, which cleaning scraper 531 wipes the residual image cleaned from the applicator roller 520 off the cleaning roller 530. The cleaning scraper 531 is part of a half chamber 532 that possesses a basin 533 and a drain 534. A fill level sensor 537 can optionally be provided. An
5 electrically insulated cleaning flow element 535 can be arranged in the half chamber 532.

The cleaning scraper 531 arranged at the cleaning roller 530 is integrated into the half chamber 532. This possesses lateral seals 536, the cleaning scraper 531 and a
10 half chamber 532. With this it is achieved that all developer fluid wiped off the cleaning roller 530 by the cleaning scraper 531 flows into the half chamber 532. the half chamber 532 is designed such that a level of developer fluid that lies above the cleaning scraper 531 is maintained, with the result that toner particles located on the cleaning roller 530 disperse in the present quantity of developer fluid. For
15 this either a drain 534 is provided above the level of the cleaning scraper 531 or a discharge pump (not shown in Fig. 2) that can be adjusted via a fill level sensor 537 is provided.

To assist the dispersal of the toner particles in the developer fluid, the cleaning
20 flow element 535 can be arranged near the cleaning roller 530 above the cleaning scraper 531, however partially or entirely below the level of the developer fluid. The distance can lie in the range from 10 to 2000 μm , advantageously 100 to 1000 μm . The electrical potential $U_{\text{ReW_Pot-Element3}}$ applied to the cleaning flow element 535 is more negative for a positive toner particle polarity than the potential $U_{\text{Half-}}$
25 chamber at the cleaning scraper 531 and the potential U_{ReW} at the cleaning roller 530. The electrical voltage derived from this is sufficiently large in order to detach the toner particles from the surface of the cleaning roller 530 but small enough that an accumulation of the toner particles on the cleaning flow element 535 is prevented by the flow in the gap between cleaning roller 530 and cleaning flow element 535.
30 The electrical voltage lies between 10 V and 5000 V, advantageously between 200 to 2000 V.

The cleaning flow element 535 is additionally shaped such that no discontinuities in the flow cross-section can occur in the gap between cleaning flow element 535 and cleaning roller 530, and therefore a flow in the gap between the cleaning flow
5 element 535 and the cleaning roller 530 arises that is parallel to the movement direction of the surface of the cleaning roller 530.

Furthermore, a movable element (for example a helical spindle) can be arranged below the intended fluid level in the basin 533 of the half chamber 532. This
10 element can be actively moved via an actuator and serves to avoid accumulations or, respectively, to break up deposits, for example after longer operating pauses due to sedimentation.

The conditioning device 54 (that can be optionally provided) can consist of either a
15 corotron (for example a wire corotron 540 (Fig. 4)) to which an electrical potential in the polarity of the toner particles is applied or a conditioning roller 541 (Fig. 5).

Charges of the same polarity as the toner particles are applied to the applicator roller 520 via the corotron 540. The charges remain at the surface of the developer
20 fluid due to the insulating carrier fluid. As a result of this the toner particles are displaced from the surface of the developer fluid film in the direction towards the applicator roller 520; a cover layer of carrier fluid arises on the developer fluid, which cover layer serves to prevent toner accumulations at non-image points on the intermediate image carrier 1 in the following development step.

25 The design of the conditioning device 54 with conditioning roller 541 arises from Fig. 5. This is located in contact with the developer fluid film on the applicator roller 520. The conditioning roller 541 is provided with a separate electrical potential U_{Con} that is higher than the electrical potential of the applicator roller
30 U_{AW} . The resulting voltage between conditioning roller 541 and applicator roller 520 lies in the range from 10 V to 2000 V, advantageously in the range from 200 V

to 1000 V. The applicator roller 520 and the conditioning roller 541 roll on one another. The surface speed of the conditioning roller 541 is 0.8:1 to 1:0.8 (advantageously 1:1) in comparison to the applicator roller 520. Here the toner particles are likewise displaced from the surface of the developer fluid film
5 towards the applicator roller 520.

A separator flow between conditioning roller 541 and applicator roller 520 is additionally generated via the suitable selection of the diameter of the conditioning roller 541. For this the diameter of the conditioning roller 541 is selected in a
10 range from 0.1 to 0.7 of the diameter of the applicator roller 520, advantageously 0.2 to 0.5. Due to the small diameter of the conditioning roller 541, the separator flow exhibits a pronounced speed vector perpendicular to the surface of the applicator roller 520. The disruption of the fluid layer thickness arising in the film division after the roller contact exhibits a small period length ($< 100 \mu\text{m}$) and
15 simultaneously low amplitude. This has the effect of a macroscopic smoothing of the fluid surface, corresponding with a uniform distribution of the toner particles on the applicator roller 520 and subsequently in the print image.

A conditioning scraper 542 can optionally be arranged at the conditioning roller
20 541. The conditioning scraper 542 removes the carrier fluid located on the conditioning roller 541 (which carrier fluid is impoverished of toner particles due to the applied electrical field) and returns this into the mixing device MS. The film of developer fluid remaining on the applicator roller 520 exhibits an increased concentration of toner particles with simultaneously lower overall layer thickness.
25 The field strength in the gap is determined by the unchanged applied potentials and the distance between the two. The distance reduces corresponding to the reduced layer thickness of the developer fluid and therefore leads to a higher field strength in the gap between intermediate image carrier 1 and applicator roller 520, which higher field strength is advantageous for the development process. Alternatively, it
30 is possible to use a low-concentration developer fluid (that is therefore more free-flowing) for the conditioning device.

The rollers (raster roller 510, cleaning roller 530, conditioning roller 541, applicator roller 520) used in the devices respective possess a surface coating. The coatings are selected such that

- 5 - no or only a slight electrical current flows via direct contact (for example webs of the raster roller 510 on the applicator roller 520, cleaning roller 530 or conditioning roller 541 on applicator roller 520), such that different electrical potentials of the rollers due to the connected mains supply circuits can be kept stable (current advantageously $< 100 \mu\text{m}/1 \text{ m}$ roller width;
10 potential fluctuations advantageously $< \pm 10 \text{ V}$),
 - the current-limiting coating is thereby (advantageously) applied not at the applicator roller 520 but rather at the respective abutting roller (510, 530, 541)
 - in order to ensure a conductive coating of the applicator roller 520
15 (specific resistance $< 10^7 \Omega \cdot \text{cm}$), whereby a low voltage drop ($< 10 \text{ V}$) occurs via the coating of the applicator roller 520,
• with which the potential difference (resulting from the distance between charge potential or, respectively, discharge potential of the intermediate image carrier 1 and the bias potential of the applicator
20 roller 520 that is arranged symmetrically between them) present in the developer gap (applicator roller 520 to intermediate image carrier 520) is converted into an optimally large electrical field strength (voltage/layer thickness) via the developer fluid in the developer gap;
- 25 - the current-limiting coating on the raster roller 510, cleaning roller 530 and conditioning roller 541 lies in a range between $10^8 \Omega \cdot \text{cm}$ and $10^{10} \Omega \cdot \text{cm}$, advantageously $5 \cdot 10^8$ and $5 \cdot 10^9 \Omega \cdot \text{cm}$, wherein the voltage drop occurring across these coatings is $< 100 \text{ V}$,
 - a current limiter is thus present at every contact point.

The coating of the elastic applicator roller 520 can exhibit a specific resistance in the range between 10^4 to $10^8 \Omega \cdot \text{cm}$, advantageously between 10^5 and 10^7 ; the resistance fluctuations can be $< \pm 20\%$ (advantageously $< \pm 10\%$); the layer thickness lies between 3 and 12 mm, advantageously 7 to 10 mm. Among other things, NBR rubber, PUR rubber can be selected as materials. When the coating of the applicator roller 520 possesses two layers, the outer layer can consist of PVDF, ECO, fluoroelastomer, Teflon and have a layer thickness $< 0.7 \text{ mm}$; the inner layer can consist of the aforementioned materials.

10 The coating of the raster roller 510 and of the cleaning roller 530 can exhibit a resistance between $10^8 \Omega \cdot \text{cm}$ and $10^{10} \Omega \cdot \text{cm}$ and a layer thickness between 10 and $400 \mu\text{m}$, advantageously between 50 and $200 \mu\text{m}$. Among other things, hard-anodized coating, [sic] ceramic (Al oxide, chromium oxide, titanium oxide or a mixture of these) can be selected as a material.

15

As results from the explanation of the inventive device, all function elements are provided with a defined electrical potential. The following viewpoints have been selected for the choice of the potential:

- all potentials result from the superimposition of a direct voltage portion and alternating voltage portion; each portion can thereby be zero;
- all rollers (belts) – thus the applicator roller 520, the raster roller 510, the cleaning roller 530 and the conditioning roller 541 – are provided with a separate potential;
- the chamber scraper 511 advantageously has the same potential as the raster roller 510, optionally even a higher potential in comparison to the raster roller 510;
- the cleaning scraper 531 and the half chamber 532 (lateral sealing) advantageously have the same potential as the cleaning roller 530, optionally even a higher potential;
- the potentials at the flow elements 518, 519, 535 have been described above.

The potentials in the rollers (510, 520, 530, 541) are applied at their cores; given belts they are applied on their inner sides.

5 The potential differences listed above between the function elements have been designated as voltages in the specification.

The surface coatings of the rollers form a system of specific resistances ρ adapted to one another. It thereby applies that:

- $\rho(\text{raster roller}) > \rho(\text{applicator roller})$;
- 10 - $\rho(\text{cleaning roller}) > \rho(\text{applicator roller})$;
- $\rho(\text{conditioning roller}) > \rho(\text{applicator roller})$.

The particular advantages of the inventive device are presented summarized in the following:

- 15 - For each function element (for example raster roller 510, applicator roller 520) participating in the transfer process of the developer fluid on the way to the intermediate image carrier 1, the accumulation time of the toner particles in each transfer process is less than the quotient of the length of the respective transfer zone for the developer fluid between the respective function elements and the process speed (respective transfer time of the toner particles from function element to function element). Based on an electrical field effect, this is achieved via the combination of the resistances and the capacitances of the participating function elements and the distance of the participating function elements from one another.
- 20

25 As a formula this can be formulated as:

$$\frac{l_{Nip}}{v_{Process}} > \frac{d_{Nip}}{v_{Accumulation}}$$

wherein

$v_{accumulation} = \mu \cdot E$ with μ - [sic] toner mobility and E = electrical field strength;

30 l = length of the transfer zone;

v = speed

d = thickness of the transfer zone

- To avoid permanent adhesions of toner particles on function elements participating in the transfer process of the developer fluid on the way to the intermediate image carrier 1, these are designed such that, at each participating function element in a cyclical process of the transfer of the developer fluid or portions thereof from function element to function element, in each cycle a force effect is generated towards the function element and away from the function element. The force effect can be generated by an electrical field acting on the charged toner particles or by a flow, i.e. a shear effect.

Reference list

	DS	printing system
	MS	mixing device
5	1	intermediate image carrier
	2	regeneration exposure
	3	charging station
	4	graphical exposure
	5	developer device
10	6	transfer unit
	7	recording medium
	8	cleaning element
	61	transfer roller
	62	counter-pressure roller
15	63	cleaning unit
	51	feed device
	52	applicator device
	53	cleaning device
	54	conditioning device
20	520	applicator roller
	510	raster roller
	511	chamber scraper
	512	chamber of the chamber scraper
	513	inlet
25	514	overflow
	515	first pump
	516	capture basin
	517	second pump
	518	first flow element
30	519	second flow element
	530	cleaning roller

	531	cleaning scraper
	532	half chamber
	533	basin of the half chamber
	534	drain of the half chamber
5	535	cleaning flow element
	536	seals
	540	wire corotron
	541	conditioning roller
	542	conditioning scraper

Patent claims

1. Device for development of potential images (generated on an intermediate image carrier) of images to be printed using a developer fluid comprising charged
5 toner particles and carrier fluid in an electrographic printing or copying device ,
 - in which a feed device (51) is provided that provides as function elements at least one chamber scraper (511), a raster element (510) comprising cups to receive the developer fluid, and at least one first flow element (518) arranged in the chamber scraper (511), between which at least one flow
10 element (518) and the raster element (510) an electrical voltage is applied such that the toner particle concentration in the cups of the raster element (510) is increased,
 - in which an applicator device (52) is provided that accepts the developer fluid from the feed device (51) and supplies this to the intermediate image
15 carrier (1).
2. Device according to claim 1,
in which, to avoid the unwanted accumulation of toner particles on function elements participating in the transfer process of the developer fluid in the transfer
20 process of the developer fluid on the way to the intermediate image carrier (1), these function elements are designed and operated such that, in the cyclical process of the transition of the developer fluid from function element to function element, a force effect on the toner particles towards the next function element and away from the preceding function element is generated in each cycle with regard to the
25 transfer path of the developer fluid.
3. Device according to claim 2,
in which the force effect is respectively generated via an electrical field acting on the charged toner particles.
30
4. Device according to claim 2 or 3,

in which the force effect is generated via a flow.

5. Device according to any of the preceding claims,
in which the function elements transporting the developer fluid are rollers or belts.

5

6. Device according to claim 5,
in which the resistances of the function elements transporting the developer fluid
are alternately high-ohmic and low-ohmic.

10 7. Device according to any of the preceding claims,
in which a cleaning device (53) is provided that cleans the residual image
remaining on the applicator device (52) off after the development of the potential
images, and an electrical voltage between said cleaning device (53) and the
applicator device (52) is applied that establishes the transfer of the toner particles
15 of the residual image onto the cleaning device (53).

8. Device according to any of the preceding claims,
in which a conditioning device (54) is provided that is arranged adjacent to the
applicator device (52) and before the intermediate image carrier (1) (as viewed in
20 the movement direction of the developer fluid), and that influences the developer
fluid to be supplied to the intermediate image carrier (1) such that the toner
particles in the developer fluid move to the surface of the applicator device (52).

9. Device according to any of the preceding claims,
25 in which the feed device (51) possesses as function elements at least one chamber
scraper (511) and a raster roller (510), in which the raster roller (510) accepts the
developer fluid from the chamber scraper (511).

10. Device according to any of the preceding claims,
30 in which the applicator device (52) possesses as a function element an applicator
roller (520) or an applicator belt.

11. Device according to any of the claims 7 through 10,
in which the cleaning device (53) possesses as a function element at least one
cleaning roller (530) or a cleaning belt.

5

12. Device according to claim 9, 10 or 11,
in which the raster roller (510) exhibits a high resistance in comparison to the
applicator roller (520), such that only a minimal electrical current transfer occurs at
the transfer region for the developer fluid between raster roller (501 [sic]) and
applicator roller (520).

10

13. Device according to any of the claims 10 through 12,
in which the applicator roller (520) transporting the developer fluid exhibits a
slight resistance, and the voltage drop across its surface is therefore small.

15

14. Device according to any of the claims 11 through 13,
in which the cleaning roller (530) exhibits a high resistance in comparison to the
applicator roller (520), such that only a minimal electrical current transfer occurs at
the transfer region for the developer fluid between cleaning roller (530) and
applicator roller (520).

20

15. Device according to any of the claims 9 through 15,
in which the resistance of raster roller (510) or, respectively, of the cleaning roller
(530) is selected such that the current transfer between them and the applicator
roller (520) is $< 1000 \mu\text{A}/1\text{m}$, advantageously $< 100 \mu\text{A}/1\text{m}$.

25

16. Device according to claim 15,
in which the resistance of the cleaning roller (530) or, respectively, of the raster
roller (510) lies in the range from $10^8 \Omega \cdot \text{cm}$ to $10^{10} \Omega \cdot \text{cm}$, advantageously $5 \cdot 10^8$
to $5 \cdot 10^9 \Omega \cdot \text{cm}$, and that of [sic] the applicator roller (520) is more conductive be
at least a factor of 10.

30

17. Device according to claim 16,
in which the surface layer of the applicator roller (520) is selected such that its
resistance is $< 10^8 \Omega \cdot \text{cm}$, advantageously is 10^5 to $10^7 \Omega \cdot \text{cm}$.

5

18. Device according to any of the claims 9 through 17,
in which the chamber scraper (511) possesses a chamber (512) open towards the
raster roller (510), with an inlet (513) and an overflow (514) for the developer fluid,
wherein the inlet (513) is designed such that the supplied quantity of developer
10 fluid is greater than or equal to the quantity that passes to the raster roller (510),
and such that the excess quantity drains off via the overflow (514).

19. Device according to claim 18,
in which a sufficient feed of toner particles into the cups of the raster roller (510)
15 can be achieved via a sufficient feed and distribution of the developer fluid into the
chamber scraper (511) and via an electrical field assistance within the chamber
scraper (511).

20. Device according to one of the claims 18 or 19,
20 in which at least the first flow element (518) is arranged in the chamber (512) of
the chamber scraper (511), between which first flow element (518) and the raster
roller an electrical voltage is applied.

21. Device according to claim 20,
25 in which the electrical field strength (caused by the electrical voltage) between the
first flow element (518) and the raster roller (510) is selected in the range between
 10 to $5 \cdot 10^4 \text{ V/cm}$.

22. Device according to one of the claims 20 to 21,
30 in which a second element (519) adjacent to the first flow element (518) is
provided as an additional function element in the chamber (512), which additional

function element lies at an electrical voltage that consists of a direct voltage portion and an alternating voltage portion, wherein each portion can be zero and its polarity is the reverse of that of the first flow element (518), such that the developer fluid is stirred with the remaining fluid located in the cups of the raster roller (510) or, respectively, accumulations of toner particles in the chamber scraper (511) are prevented.

23. Device according to claim 22,
in which the second flow element (519) is arranged before the first flow element (518) as viewed in the rotation direction of the raster roller (510).

24. Device according to any of the claims 22 or 23,
in which the flow elements (518, 519) at the raster roller (510) and at the inner contour of the chamber (512) are arranged and shaped such that a flow of developer fluid arises in the gap between the flow elements (518, 519) and the raster roller (510), which flow is parallel to the movement direction of the roller surface, and such that no discontinuous cross-section changes of the streamed surfaces occur both in the axial direction and in the radial direction, and no zones with a flow speed of zero occur.

25. Device according to any of the claims 22 through 24,
in which the flow elements (518, 519) are designed as electrically conductive profile elements that are arranged parallel to the raster roller (510) in the chamber (512), adjacent to the opening of said chamber (512), and extend across the width of the chamber (512) and exhibit a distance from the raster roller in the range from 10 to 2000 μm , advantageously 100 to 1000 μm .

26. Device according to any of the claims 22 through 25,
in which the flow elements (518, 519) exhibit a cross-section that is flattened in the direction of the raster roller (510).

27. Device according to any of the claims 11 through 26,
- in which the cleaning device (53) comprises the cleaning roller (530) and,
as a further function element, a cleaning scraper (531) abutting the cleaning
roller,
5 - in which the cleaning scraper (531) is part of a half chamber (532) into
which the scraped-off residual image flows.
28. Device according to claim 27,
in which the half-chamber (532) comprises lateral seals (536), the cleaning scraper
10 (531) and a basin (533), wherein the half chamber (532) is designed such that the
level of the developer fluid always lies above the cleaning scraper (531), such that
the toner particles present on the cleaning roller (530) disperse in the half chamber
(532).
- 15 29. Device according to claim 28,
in which a movable drive element (in particular a helical spindle) is arranged in
the basin (533) of the half chamber (532) in order to prevent deposits or,
respectively, to detach accumulations.
- 20 30. Device according to any of the claims 27 through 29,
in which a fill level sensor (537) that controls a discharge pump is provided to
adjust the level in the half chamber (532).
31. Device according to any of the claims 27 through 30,
25 in which an overflow (534) to adjust the level in the half chamber (532) is provided
above the cleaning scraper (531).
32. Device according to any of the claims 27 through 31,
in which a cleaning flow element (535) as a further function element is arranged in
30 the half chamber (532) next to the cleaning roller (530), which cleaning flow
element (535) is shaped such that a flow arises in the region between the cleaning

flow element (535) and the cleaning roller (530), which flow is parallel to the movement direction of the surface of the cleaning roller (530), and such that no discontinuous cross-section changes of the streamed surfaces occur both in the axial direction and in the radial direction.

5

33. Device according to claim 32,
in which the distance from cleaning roller (530) to cleaning flow element (535) is set to 10 to 2000 μm , advantageously 100 to 1000 μm .

10

34. Device according to claim 32 or 33,
in which the cleaning flow element (535) is arranged above the cleaning scraper (531) but partially or entirely below the level of the developer fluid in the half chamber (532).

15

35. Device according to any of the claims 32 through 34,
in which an electrical potential that consists of a direct voltage portion and an alternating voltage portion is applied at the cleaning flow element (535), wherein each portion can be zero, and which potential is more negative than the potential at the cleaning roller (530) and the cleaning scraper (531) given positive toner
20 polarity.

20

36. Device according to claim 35,
in which the electrical voltage between cleaning roller (530) and cleaning flow element (535) is selected such that the toner particles are detached from the surface
25 of the cleaning roller (530), however an accumulation of the toner particles on the cleaning flow element (535) is prevented.

25

37. Device according to claim 36,
in which the electrical voltage between cleaning roller (530) and cleaning flow
30 element (535) lies between 10 V and 5000 V, advantageously between 200 V and 2000 V.

30

38. Device according to any of the claims 27 through 37,
in which the half chamber (532) is connected with the mixing device (MS).

5 39. Device according to any of the claims 8 through 38,
in which, as a function element, the conditioning device (54) is a corotron (540)
arranged adjacent to the surface of the applicator roller (520), which corotron (540)
lies at such an electrical potential that charges of the same polarity in comparison
to the toner particles are raised on the applicator roller (520).

10

40. Device according to claim 38,
in which a wire corotron (540) is provided that is arranged parallel to the applicator
roller (520).

15 41. Device according to any of the claims 8 through 39,
in which the conditioning device (54) as a function element comprises a
conditioning roller (541) that lies at such an electrical potential that charges of the
same polarity in comparison to the toner particles are raised on the applicator roller
(520).

20

42. Device according to claim 41,
in which the electrical voltage between the applicator roller (520) and the
conditioning roller (541) lies in the range from 10 V to 2000 V, advantageously
200 V to 1000 V.

25

43. Device according to any of the claims 41 or 42,
in which the conditioning roller (541) exhibits a resistance that is greater than that
of the applicator roller (520).

30 44. Device according to any of the claims 41 through 43,

in which the conditioning roller (541) rolls on the applicator roller (520), wherein their speed ratio lies between 0.8:1 to 1:0.8, advantageous is 1:1.

45. Device according to any of the claims 41 through 44,
5 in which the diameters of the conditioning roller (541) and the applicator roller (520) are selected such that a separator flow arises between applicator roller (520) and the conditioning roller (541), which separator flow causes a smoothing of the surface of the developer fluid on the applicator roller (520).
- 10 46. Device according to any of the claims 45,
in which the diameter of the conditioning roller (541) lies in the range from 0.1 to 0.7 of the diameter of the applicator roller (520), advantageously is 0.2. to 0.5.
47. Device according to any of the claims 41 through 46,
15 in which a conditioning scraper (542) abuts the conditioning roller (541).
48. Device according to any of the claims 41 through 47,
in which the conditioning roller (541) possesses a current-limiting coating that exhibits a specific resistance of 10^8 to $10^{10} \Omega \cdot \text{cm}$, advantageously $5 \cdot 10^8$ to $5 \cdot 10$
20 $\Omega \cdot \text{cm}$.
49. Device according to any of the claims 10 through 48,
in which the applicator roller (520) possesses a coating that exhibits a specific resistance that advantageously lies in the range from 10 to $10^8 \Omega \cdot \text{cm}$,
25 advantageously between 10^5 and $10^7 \Omega \cdot \text{cm}$, wherein a layer thickness between 4 and 12 mm is provided, advantageously 7 to 10 mm.
50. Device according to claim 49,
in which the surface of the applicator roller (520) possess a coating made from
30 NBR rubber or PUR rubber.

51. Device according to claim 49,
in which the surface of the applicator roller (520) consists of two layers, in which
the cover layer consists of PVDF, ECO, fluoroelastomer or Teflon.
- 5 52. Device according to claim 51,
in which the layer thickness of the cover layer is < 0.7 mm.
53. Device according to any of the claims 9 through 52,
in which the surface of the raster roller (510) or, respectively, the surface of the
10 cleaning roller (530) possesses a coating whose specific resistance lies between 10^8
and $10^{10} \Omega \cdot \text{cm}$ and exhibits a layer thickness between 10 and 400 μm ,
advantageously 50 to 200 μm .
54. Device according to claim 53,
15 in which the material of the coating of the raster roller (510) or, respectively,
cleaning roller (530) is a hard-anodized coating or ceramic (Al oxide, chromium
oxide, titanium oxide or a mixture of these).
55. Device according to any of the claims 9 through 54,
20 in which the applicator roller (520) in the applicator device (52) is replaced by an
applicator belt.
56. Device according to any of the claims 11 through 55,
in which the cleaning roller (530) in the cleaning device (53) is replaced by a
25 cleaning belt.
57. Method for development of potential images arranged on an intermediate
image carrier (1) in an electrographic printing device, in which a device according
to any of the claims 1 through 56 is used.
30
58. Method according to claim 57,

in which developer fluid consisting of charged toner particles and carrier fluid is drawn at low toner particle concentration (and therefore at low viscosity) from a mixing device (MS) and is increased to the toner particle concentration required for inking of the potential images before the transfer of the developer fluid to the
5 intermediate image carrier (10).

59. Method according to claim 58,

- in which the developer fluid is drawn at low toner particle concentration from the mixing device (MS) via a feed device (51) consisting of a chamber scraper (511) and a raster roller (510),
10
- in which the developer fluid is concentrated with toner particles in the transfer from the chamber scraper (511) into the cups of the raster roller (510) and is applied in concentrated form to an applicator roller (520) that directs the developer fluid in concentrated form over the intermediate
15 image carrier (1).

60. Method according to claim 59,

- in which the concentration of the developer fluid is achieved in that an electrical voltage that increases the number of the toner particles in the cups of the raster roller (510) is applied between chamber scraper (511) and raster roller (510).
20

61. Method according to any of the claims 58 through 60,

- in which the developer fluid on the applicator roller (520) is further concentrated with toner particles by a conditioning roller (541) running on the applicator roller via acceptance of carrier fluid before this developer fluid is supplied to the
25 intermediate image carrier (1).

62. Method according to claim 61,

- in which such an electrical potential is applied to the conditioning roller (541) that the toner particles in the developer fluid on the applicator roller (520) are displaced
30 in the direction of its surface.

63. Method according to any of the claims 57 through 62,
- in which the developer fluid remaining on the applicator roller (520) after
the development of the potential images on the intermediate image carrier
5 (1) is cleaned off by a cleaning roller (530),
- in which the cleaned-off developer fluid is scraped into a half chamber
(532) by a cleaning scraper (531) and drains from there into the mixing
device (MS).
- 10 64. Method according to claim 63,
in which an electrical potential is applied to the cleaning roller to improve the
cleaning function of the cleaning roller (530), via which electrical potential the
transfer of the toner particles is assisted.
- 15 65. Method according to claim 64,
in which the applicator roller (520), the raster roller (510), the cleaning roller (530)
and the conditioning roller (541) are provided with a separate electrical potential.
- 20 66. Method according to claim 65,
in which an advantageously identical potential as at the raster roller (510) is
applied at the chamber scraper (511), optionally even a higher potential in
comparison to the raster roller.
- 25 67. Method according to any of the claims 63 through 66,
in which the same potential as at the cleaning roller (530) is advantageously
applied at the cleaning scraper (531) and the half chamber (532) (lateral sealing),
optionally even a higher potential.
- 30 68. Method according to any of the claims 63 through 67,
in which the surface coatings of the applicator roller (520), the raster roller (510),
the cleaning roller (530) and the conditioning roller (541) is [sic] selected such that

a system of specific resistances ρ adapted to one another arises, whereby it applies that:

- $\rho(\text{raster roller}) > \rho(\text{applicator roller});$
- $\rho(\text{cleaning roller}) > \rho(\text{applicator roller});$
- 5 - $\rho(\text{conditioning roller}) > \rho(\text{applicator roller}).$

10

15

Patent claims

1. Device for development of potential images (generated on an intermediate image carrier) of images to be printed using a developer fluid comprising charged
5 toner particles and carrier fluid in an electrographic printing or copying device ,
 - in which a feed device (51) is provided that provides as function elements at least one chamber scraper (511), a raster element (510) comprising cups to receive the developer fluid, and at least one first flow element (518) arranged in the chamber scraper (511), between which at least one flow
10 element (518) and the raster element (510) an electrical voltage is applied such that the toner particle concentration in the cups of the raster element (510) is increased,
 - in which an applicator device (52) is provided that accepts the developer fluid from the feed device (51) and supplies this to the intermediate image
15 carrier (1).
2. Device according to claim 1,
in which, to avoid the unwanted accumulation of toner particles on function elements participating in the transfer process of the developer fluid in the transfer
20 process of the developer fluid on the way to the intermediate image carrier (1), these function elements are designed and operated such that, in the cyclical process of the transition of the developer fluid from function element to function element, a force effect on the toner particles towards the next function element and away from the preceding function element is generated in each cycle with regard to the
25 transfer path of the developer fluid.
3. Device according to claim 2,
in which the force effect is respectively generated via an electrical field acting on the charged toner particles.
30
4. Device according to claim 2 or 3,

in which the force effect is generated via a flow.

5. Device according to any of the preceding claims,
in which the function elements transporting the developer fluid are rollers or belts.

5

6. Device according to claim 5,
in which the resistances of the function elements transporting the developer fluid
are alternately high-ohmic and low-ohmic.

10 7. Device according to any of the preceding claims,
in which a cleaning device (53) is provided that cleans the residual image
remaining on the applicator device (52) off after the development of the potential
images, and an electrical voltage between said cleaning device (53) and the
applicator device (52) is applied that establishes the transfer of the toner particles
15 of the residual image onto the cleaning device (53).

8. Device according to any of the preceding claims,
in which a conditioning device (54) is provided that is arranged adjacent to the
applicator device (52) and before the intermediate image carrier (1) (as viewed in
20 the movement direction of the developer fluid), and that influences the developer
fluid to be supplied to the intermediate image carrier (1) such that the toner
particles in the developer fluid move to the surface of the applicator device (52).

9. Device according to any of the preceding claims,
25 in which the feed device (51) possesses as function elements at least one chamber
scraper (511) and a raster roller (510), in which the raster roller (510) accepts the
developer fluid from the chamber scraper (511).

10. Device according to any of the preceding claims,
30 in which the applicator device (52) possesses as a function element an applicator
roller (520) or an applicator belt.

11. Device according to any of the claims 7 through 10,
in which the cleaning device (53) possesses as a function element at least one
cleaning roller (530) or a cleaning belt.

5

12. Device according to claim 9, 10 or 11,
in which the raster roller (510) exhibits a high resistance in comparison to the
applicator roller (520), such that only a minimal electrical current transfer occurs at
the transfer region for the developer fluid between raster roller (501 [sic]) and
applicator roller (520).

10

13. Device according to any of the claims 10 through 12,
in which the applicator roller (520) transporting the developer fluid exhibits a
slight resistance, and the voltage drop across its surface is therefore small.

15

14. Device according to any of the claims 11 through 13,
in which the cleaning roller (530) exhibits a high resistance in comparison to the
applicator roller (520), such that only a minimal electrical current transfer occurs at
the transfer region for the developer fluid between cleaning roller (530) and
applicator roller (520).

20

15. Device according to any of the claims 9 through 15,
in which the resistance of raster roller (510) or, respectively, of the cleaning roller
(530) is selected such that the current transfer between them and the applicator
roller (520) is $< 1000 \mu\text{A}/1\text{m}$, advantageously $< 100 \mu\text{A}/1\text{m}$.

25

16. Device according to claim 15,
in which the resistance of the cleaning roller (530) or, respectively, of the raster
roller (510) lies in the range from $10^8 \Omega \cdot \text{cm}$ to $10^{10} \Omega \cdot \text{cm}$, advantageously $5 \cdot 10^8$
to $5 \cdot 10^9 \Omega \cdot \text{cm}$, and that of [sic] the applicator roller (520) is more conductive be
at least a factor of 10.

30

17. Device according to claim 16,
in which the surface layer of the applicator roller (520) is selected such that its
resistance is $< 10^8 \Omega \cdot \text{cm}$, advantageously is 10^5 to $10^7 \Omega \cdot \text{cm}$.

5

18. Device according to any of the claims 9 through 17,
in which the chamber scraper (511) possesses a chamber (512) open towards the
raster roller (510), with an inlet (513) and an overflow (514) for the developer fluid,
wherein the inlet (513) is designed such that the supplied quantity of developer
10 fluid is greater than or equal to the quantity that passes to the raster roller (510),
and such that the excess quantity drains off via the overflow (514).

19. Device according to claim 18,
in which a sufficient feed of toner particles into the cups of the raster roller (510)
15 can be achieved via a sufficient feed and distribution of the developer fluid into the
chamber scraper (511) and via an electrical field assistance within the chamber
scraper (511).

20. Device according to one of the claims 18 or 19,
20 in which at least the first flow element (518) is arranged in the chamber (512) of
the chamber scraper (511), between which first flow element (518) and the raster
roller an electrical voltage is applied.

21. Device according to claim 20,
25 in which the electrical field strength (caused by the electrical voltage) between the
first flow element (518) and the raster roller (510) is selected in the range between
 10 to $5 \cdot 10^4 \text{ V/cm}$.

22. Device according to one of the claims 20 to 21,
30 in which a second element (519) adjacent to the first flow element (518) is
provided as an additional function element in the chamber (512), which additional

function element lies at an electrical voltage that consists of a direct voltage portion and an alternating voltage portion, wherein each portion can be zero and its polarity is the reverse of that of the first flow element (518), such that the developer fluid is stirred with the remaining fluid located in the cups of the raster roller (510) or, respectively, accumulations of toner particles in the chamber scraper (511) are prevented.

23. Device according to claim 22,
in which the second flow element (519) is arranged before the first flow element (518) as viewed in the rotation direction of the raster roller (510).

24. Device according to any of the claims 22 or 23,
in which the flow elements (518, 519) at the raster roller (510) and at the inner contour of the chamber (512) are arranged and shaped such that a flow of developer fluid arises in the gap between the flow elements (518, 519) and the raster roller (510), which flow is parallel to the movement direction of the roller surface, and such that no discontinuous cross-section changes of the streamed surfaces occur both in the axial direction and in the radial direction, and no zones with a flow speed of zero occur.

25. Device according to any of the claims 22 through 24,
in which the flow elements (518, 519) are designed as electrically conductive profile elements that are arranged parallel to the raster roller (510) in the chamber (512), adjacent to the opening of said chamber (512), and extend across the width of the chamber (512) and exhibit a distance from the raster roller in the range from 10 to 2000 μm , advantageously 100 to 1000 μm .

26. Device according to any of the claims 22 through 25,
in which the flow elements (518, 519) exhibit a cross-section that is flattened in the direction of the raster roller (510).

27. Device according to any of the claims 11 through 26,
- in which the cleaning device (53) comprises the cleaning roller (530) and,
as a further function element, a cleaning scraper (531) abutting the cleaning
roller,
5 - in which the cleaning scraper (531) is part of a half chamber (532) into
which the scraped-off residual image flows.
28. Device according to claim 27,
in which the half-chamber (532) comprises lateral seals (536), the cleaning scraper
10 (531) and a basin (533), wherein the half chamber (532) is designed such that the
level of the developer fluid always lies above the cleaning scraper (531), such that
the toner particles present on the cleaning roller (530) disperse in the half chamber
(532).
- 15 29. Device according to claim 28,
in which a movable drive element (in particular a helical spindle) is arranged in
the basin (533) of the half chamber (532) in order to prevent deposits or,
respectively, to detach accumulations.
- 20 30. Device according to any of the claims 27 through 29,
in which a fill level sensor (537) that controls a discharge pump is provided to
adjust the level in the half chamber (532).
31. Device according to any of the claims 27 through 30,
25 in which an overflow (534) to adjust the level in the half chamber (532) is provided
above the cleaning scraper (531).
32. Device according to any of the claims 27 through 31,
in which a cleaning flow element (535) as a further function element is arranged in
30 the half chamber (532) next to the cleaning roller (530), which cleaning flow
element (535) is shaped such that a flow arises in the region between the cleaning

flow element (535) and the cleaning roller (530), which flow is parallel to the movement direction of the surface of the cleaning roller (530), and such that no discontinuous cross-section changes of the streamed surfaces occur both in the axial direction and in the radial direction.

5

33. Device according to claim 32,
in which the distance from cleaning roller (530) to cleaning flow element (535) is set to 10 to 2000 μm , advantageously 100 to 1000 μm .

10

34. Device according to claim 32 or 33,
in which the cleaning flow element (535) is arranged above the cleaning scraper (531) but partially or entirely below the level of the developer fluid in the half chamber (532).

15

35. Device according to any of the claims 32 through 34,
in which an electrical potential that consists of a direct voltage portion and an alternating voltage portion is applied at the cleaning flow element (535), wherein each portion can be zero, and which potential is more negative than the potential at the cleaning roller (530) and the cleaning scraper (531) given positive toner
20 polarity.

20

36. Device according to claim 35,
in which the electrical voltage between cleaning roller (530) and cleaning flow element (535) is selected such that the toner particles are detached from the surface
25 of the cleaning roller (530), however an accumulation of the toner particles on the cleaning flow element (535) is prevented.

25

37. Device according to claim 36,
in which the electrical voltage between cleaning roller (530) and cleaning flow element (535) lies between 10 V and 5000 V, advantageously between 200 V and 2000 V.
30

30

38. Device according to any of the claims 27 through 37,
in which the half chamber (532) is connected with the mixing device (MS).

5 39. Device according to any of the claims 8 through 38,
in which, as a function element, the conditioning device (54) is a corotron (540)
arranged adjacent to the surface of the applicator roller (520), which corotron (540)
lies at such an electrical potential that charges of the same polarity in comparison
to the toner particles are raised on the applicator roller (520).

10

40. Device according to claim 38,
in which a wire corotron (540) is provided that is arranged parallel to the applicator
roller (520).

15 41. Device according to any of the claims 8 through 39,
in which the conditioning device (54) as a function element comprises a
conditioning roller (541) that lies at such an electrical potential that charges of the
same polarity in comparison to the toner particles are raised on the applicator roller
(520).

20

42. Device according to claim 41,
in which the electrical voltage between the applicator roller (520) and the
conditioning roller (541) lies in the range from 10 V to 2000 V, advantageously
200 V to 1000 V.

25

43. Device according to any of the claims 41 or 42,
in which the conditioning roller (541) exhibits a resistance that is greater than that
of the applicator roller (520).

30 44. Device according to any of the claims 41 through 43,

in which the conditioning roller (541) rolls on the applicator roller (520), wherein their speed ratio lies between 0.8:1 to 1:0.8, advantageous is 1:1.

45. Device according to any of the claims 41 through 44,
5 in which the diameters of the conditioning roller (541) and the applicator roller (520) are selected such that a separator flow arises between applicator roller (520) and the conditioning roller (541), which separator flow causes a smoothing of the surface of the developer fluid on the applicator roller (520).
- 10 46. Device according to any of the claims 45,
in which the diameter of the conditioning roller (541) lies in the range from 0.1 to 0.7 of the diameter of the applicator roller (520), advantageously is 0.2. to 0.5.
47. Device according to any of the claims 41 through 46,
15 in which a conditioning scraper (542) abuts the conditioning roller (541).
48. Device according to any of the claims 41 through 47,
in which the conditioning roller (541) possesses a current-limiting coating that exhibits a specific resistance of 10^8 to $10^{10} \Omega \cdot \text{cm}$, advantageously $5 \cdot 10^8$ to $5 \cdot 10$
20 $\Omega \cdot \text{cm}$.
49. Device according to any of the claims 10 through 48,
in which the applicator roller (520) possesses a coating that exhibits a specific resistance that advantageously lies in the range from 10 to $10^8 \Omega \cdot \text{cm}$,
25 advantageously between 10^5 and $10^7 \Omega \cdot \text{cm}$, wherein a layer thickness between 4 and 12 mm is provided, advantageously 7 to 10 mm.
50. Device according to claim 49,
in which the surface of the applicator roller (520) possess a coating made from
30 NBR rubber or PUR rubber.

51. Device according to claim 49,
in which the surface of the applicator roller (520) consists of two layers, in which
the cover layer consists of PVDF, ECO, fluoroelastomer or Teflon.
- 5 52. Device according to claim 51,
in which the layer thickness of the cover layer is < 0.7 mm.
53. Device according to any of the claims 9 through 52,
in which the surface of the raster roller (510) or, respectively, the surface of the
10 cleaning roller (530) possesses a coating whose specific resistance lies between 10^8
and $10^{10} \Omega \cdot \text{cm}$ and exhibits a layer thickness between 10 and 400 μm ,
advantageously 50 to 200 μm .
54. Device according to claim 53,
15 in which the material of the coating of the raster roller (510) or, respectively,
cleaning roller (530) is a hard-anodized coating or ceramic (Al oxide, chromium
oxide, titanium oxide or a mixture of these).
55. Device according to any of the claims 9 through 54,
20 in which the applicator roller (520) in the applicator device (52) is replaced by an
applicator belt.
56. Device according to any of the claims 11 through 55,
in which the cleaning roller (530) in the cleaning device (53) is replaced by a
25 cleaning belt.
57. Method for development of potential images arranged on an intermediate
image carrier (1) in an electrographic printing device, in which a device according
to any of the claims 1 through 56 is used.
30
58. Method according to claim 57,

in which developer fluid consisting of charged toner particles and carrier fluid is drawn at low toner particle concentration (and therefore at low viscosity) from a mixing device (MS) and is increased to the toner particle concentration required for inking of the potential images before the transfer of the developer fluid to the
5 intermediate image carrier (10).

59. Method according to claim 58,

- in which the developer fluid is drawn at low toner particle concentration from the mixing device (MS) via a feed device (51) consisting of a chamber scraper (511) and a raster roller (510),
10
- in which the developer fluid is concentrated with toner particles in the transfer from the chamber scraper (511) into the cups of the raster roller (510) and is applied in concentrated form to an applicator roller (520) that directs the developer fluid in concentrated form over the intermediate
15 image carrier (1).

60. Method according to claim 59,

- in which the concentration of the developer fluid is achieved in that an electrical voltage that increases the number of the toner particles in the cups of the raster roller (510) is applied between chamber scraper (511) and raster roller (510).
20

61. Method according to any of the claims 58 through 60,

- in which the developer fluid on the applicator roller (520) is further concentrated with toner particles by a conditioning roller (541) running on the applicator roller via acceptance of carrier fluid before this developer fluid is supplied to the
25 intermediate image carrier (1).

62. Method according to claim 61,

- in which such an electrical potential is applied to the conditioning roller (541) that the toner particles in the developer fluid on the applicator roller (520) are displaced
30 in the direction of its surface.

63. Method according to any of the claims 57 through 62,
- in which the developer fluid remaining on the applicator roller (520) after
the development of the potential images on the intermediate image carrier
5 (1) is cleaned off by a cleaning roller (530),
- in which the cleaned-off developer fluid is scraped into a half chamber
(532) by a cleaning scraper (531) and drains from there into the mixing
device (MS).
- 10 64. Method according to claim 63,
in which an electrical potential is applied to the cleaning roller to improve the
cleaning function of the cleaning roller (530), via which electrical potential the
transfer of the toner particles is assisted.
- 15 65. Method according to claim 64,
in which the applicator roller (520), the raster roller (510), the cleaning roller (530)
and the conditioning roller (541) are provided with a separate electrical potential.
- 20 66. Method according to claim 65,
in which an advantageously identical potential as at the raster roller (510) is
applied at the chamber scraper (511), optionally even a higher potential in
comparison to the raster roller.
- 25 67. Method according to any of the claims 63 through 66,
in which the same potential as at the cleaning roller (530) is advantageously
applied at the cleaning scraper (531) and the half chamber (532) (lateral sealing),
optionally even a higher potential.
- 30 68. Method according to any of the claims 63 through 67,
in which the surface coatings of the applicator roller (520), the raster roller (510),
the cleaning roller (530) and the conditioning roller (541) is [sic] selected such that

a system of specific resistances ρ adapted to one another arises, whereby it applies that:

- $\rho(\text{raster roller}) > \rho(\text{applicator roller});$
- $\rho(\text{cleaning roller}) > \rho(\text{applicator roller});$
- 5 - $\rho(\text{conditioning roller}) > \rho(\text{applicator roller}).$

10

15

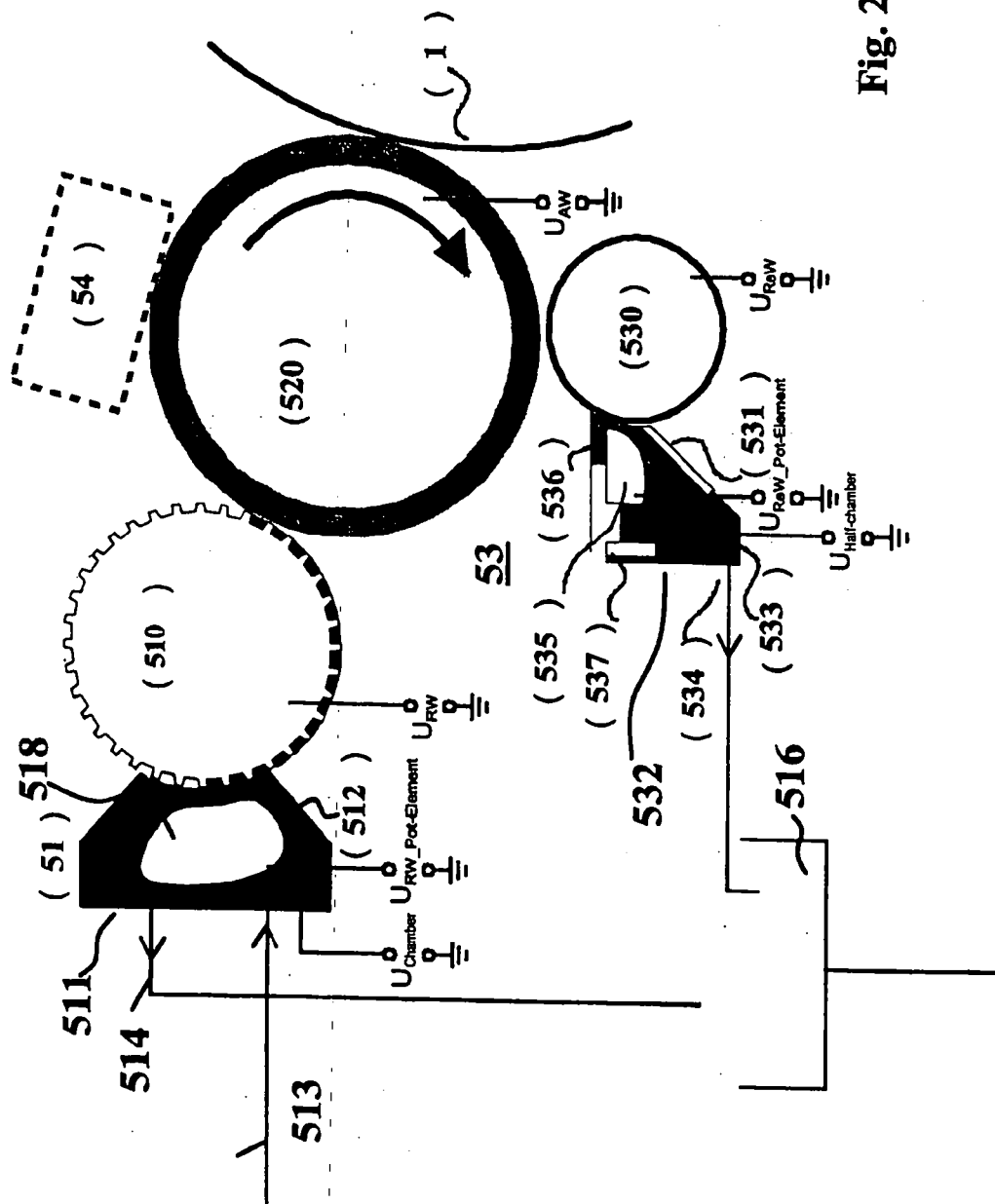


Fig. 2

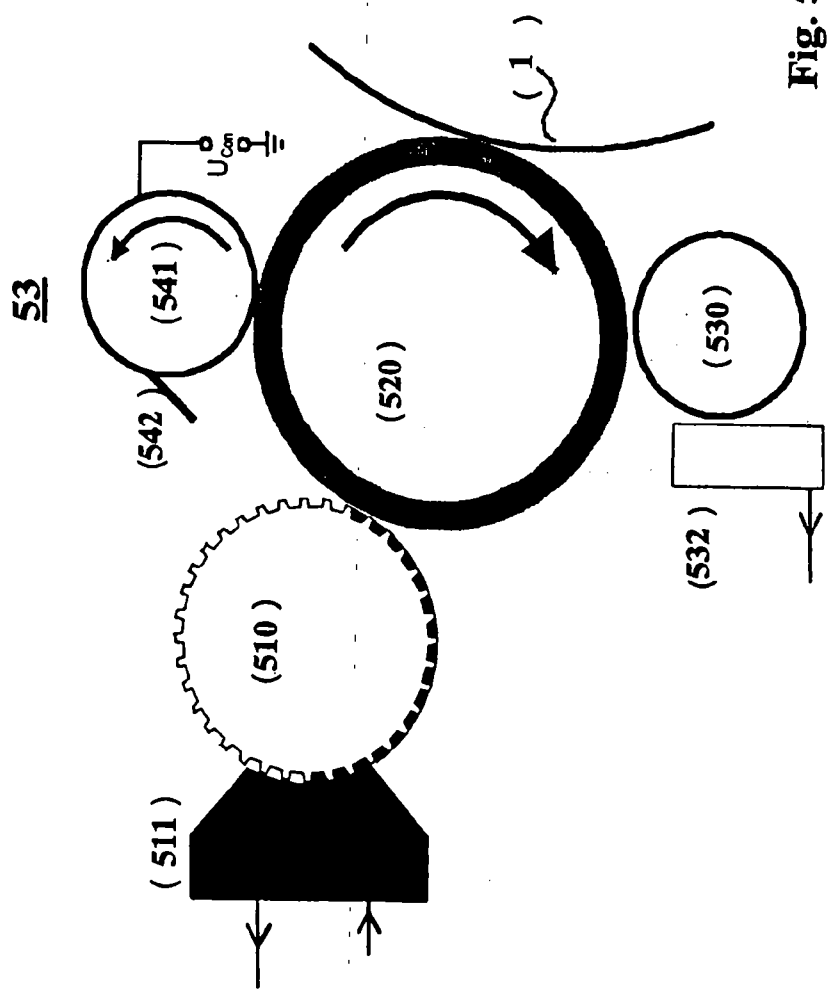


Fig. 5