(19) DANMARK

(10) DK/EP 2627997 T3

(12) Oversættelse af europæisk patentskrift

Patent- og Varemærkestyrelsen

(51) Int.Cl.: *G 01 N 27/02 (2006.01)*

(45) Oversættelsen bekendtgjort den: **2018-03-05**

(80) Dato for Den Europæiske Patentmyndigheds bekendtgørelse om meddelelse af patentet: **2017-12-06**

(86) Europæisk ansøgning nr.: **11784807.7**

(86) Europæisk indleveringsdag: **2011-10-12**

(87) Den europæiske ansøgnings publiceringsdag: **2013-08-21**

(86) International ansøgning nr.: **NO2011000291**

(87) Internationalt publikationsnr.: **WO2012050460**

(30) Prioritet: **2010-10-12 NO 20101411**

(84) Designerede stater: **AL AT BE BG CH CY CZ DE DK EE ES FI FR GB GR HR HU IE IS IT LI LT LU LV MC MK MT NL NO PL PT RO RS SE SI SK SM TR**

(73) Patenthaver: **Hammertech AS, Postboks 14 Fantoft, 5899 Bergen, Norge**

(72) Opfinder: **HAMMER, Erling, A., Lonerenen 91, N-5718 Frekhaug, Norge**

(74) Fuldmægtig i Danmark: **RWS Group, Europa House, Chiltern Park, Chiltern Hill, Chalfont St Peter, Bucks SL9 9FG, Storbritannien**

(54) Benævnelse: **ANORDNING TIL MÅLING AF VANDINDHOLD**

(56) Fremdragne publikationer:
WO-A1-03/050529
WO-A1-2004/025288
WO-A2-2007/109772
US-A- 3 946 308
US-A- 5 585 729

DESCRIPTION

Field of the invention

[0001] The present invention relates to water content measuring apparatus, for example to a water content measuring apparatus for monitoring water content in fluid flows, for example for monitoring water content in fluid flows wherein conditions for hydrate deposit formation can potentially arise. Moreover, the present invention relates to methods of measuring water content in fluid flows, for example to methods of measuring water content in fluid flows in conditions wherein hydrate deposit formation can potentially arise. Furthermore, the present invention concerns software products recorded on machine-readable media, wherein the software products are executable on computing hardware for implementing aforesaid methods.

Background of the invention

[0002] It is known to employ a pair of coils of wire exhibiting mutually different responses and excited with alternating signals for determining phase characteristics of a fluid region intersected by magnetic and electrical fields generated by the pairs of coils when excited. Such coils conventionally have relatively few turns, for example less than 10 turns each, and can determine fluid composition to within an accuracy of a few percent by way of measurement of their resonance characteristics, for example resonance Q-factor. The pair of coils is susceptible, for example, to being used to monitor fluids extracted from a production borehole when water, oil, sand particles and scum can potentially simultaneously be present in the fluids. Apparatus for determining phase characteristics of a fluid region are described in a published international PCT application no. WO2004/025288A1, "Method and arrangement for measuring conductive component current of a multiphase fluid flow and uses thereof", inventor Erling Hammer. WO03/050529 discloses a further apparatus for the analysis of multiphase fluid flow. A contemporary issue is that geological oil reserves are becoming rapidly depleted, requiring oil companies to revert to difficult and expensive off-shore drilling and production to meet World demand for oil; the World demand is presently estimated to be 85 million barrels of oil equivalent per day. Many newly discovered oil and gas fields, for example in the Barents Sea lying North of Norway, are found to contain a higher ratio of gas to oil than expected from earlier discovered oil and gas fields. Consequently, there is found to be a need to monitor to an increasing extent gas production in Northern latitudes which are often subjected to severe operating conditions, for example low ambient operating temperatures, for example below 0 °C.

[0003] A contemporary problem encountered with gas production is spontaneous formation of hydrate deposits which can block tubes completely and therefore threaten gas production with associated financial loss. Hydrate formation occurs when gas hydrocarbon molecules, for example on account of strong polarization of their hydrogen atoms, attract oxygen atoms of

water molecules so that the hydrocarbon molecules become encapsulated in water molecules to form miniature hydrate ice crystals which can precipitate to cause aforementioned hydrate deposit blockages in tubes. The blockages grow initially on inside walls of tubes, and eventually obstruct a central region of the tubes. Once hydrate ice crystal deposition commences on the inside walls, hydrate crystal nucleation is enhanced such that hydrate blockages can potentially form rapidly, for example within minutes. Moreover, the blockages are also often rather difficult to remove when formed, sometimes requiring costly "pigging" or heat treatment to be performed. A conventional approach to hinder hydrate formation is to include additives in a flow of gas. However, using additives is expensive and can also potentially cause a degree of contamination in gas flows.

[0004] Contemporary sensors and associated measuring instruments for sensing hydrate formation in tubes are complex and costly, thereby limiting locations whereat they can be installed in gas production systems. Consequently, many locations along gas tubes and pipes which could beneficially be provided with measuring instruments capable of detecting potential formation of hydrate deposits are hindered from being accordingly equipped on account of cost of conventional hydrate measuring instruments.

Summary of the invention

[0005] The present invention seeks to provide a more cost effective and robust water content measuring apparatus, for example for detecting conditions under which hydrate deposits are potentially susceptible to arise.

[0006] The invention is of advantage in that the apparatus is capable of measuring minute quantities of water present within the tube, for example indicative of potential early hydrate formation. Further aspects of the invention are defined in the appended claims.

Description of the diagrams

[0007] Embodiments of the present invention will now be described, by way of example only, with reference to the following diagrams wherein:

FIG. 1
: is an illustration of an embodiment of a water content measuring apparatus pursuant to the present invention;

FIG. 2
: is an illustration of signals to be analyzed in the apparatus of FIG. 1;

FIG. 3A
: is an illustration of a signal received from a pickup coil of the apparatus of FIG. 1 when a fluid flow tube of the apparatus is devoid of water;

FIG. 3B

is an illustration of a signal received from the pickup coil of the apparatus of FIG. 1 when the fluid flow tube of the apparatus contains spring water;

FIG. 4
is an illustration of changes in a parameter (*tau, τ*) representative of Q-factor as a function of a water content of the fluid flow tube of the apparatus of FIG. 1;

FIG. 5
is a graph illustrating sensitivity of the apparatus of FIG. 1 to saline solution;

FIG. 6
is a graph illustrating sensitivity of the apparatus of FIG. 1 to salt weight in saline solution present within a sensing tube of the apparatus;

FIG. 7
is a schematic illustration of noise sources of a water content measuring apparatus pursuant to the present invention;

FIG. 8
is a schematic illustration of an electronic circuit for use when implementing a water content measuring apparatus pursuant to the present invention;

FIG. 9
is an illustration of a resonance characteristic of a sensing resonant coil arrangement of the apparatus associated with FIG. 7 and FIG. 8, illustrating a driven resonance ω_0 and an undriven natural resonance ω_n;

FIG. 10
is an illustration of a sample of measured Q-factors of a sensing coil arrangement of the apparatus associated with FIG. 7 and FIG. 8; and

FIG. 11
is an illustration of a resonance characteristic of a sensing coil arrangement of the apparatus associated with FIG. 7 and FIG. 8.

[0008] In the accompanying diagrams, an underlined number is employed to represent an item over which the underlined number is positioned or an item to which the underlined number is adjacent. A non-underlined number relates to an item identified by a line linking the non-underlined number to the item. When a number is non-underlined and accompanied by an associated arrow, the non-underlined number is used to identify a general item at which the arrow is pointing.

Description of embodiments of the invention

[0009] It is well known that cylindrical conductor coils exhibit electrical resonances on account of inductance and distributed capacitances associated with such conductor coils; such "distributed capacitances" contributed to resonant circuit tuning capacitors pursuant to the present invention. The distributed capacitances correspond to inter-winding capacitances. Moreover, the inductance arises on account of magnetic flux developed by the coils. However,

as aforementioned, it is conventionally perceived that such coils are only capable of providing multiphase mixture measurement to an error deviation of a few percent. For measuring conditions of potential hydrate formation, it is necessary to measure water content to concentrations of a few parts per million (p.p.m.). Thus, it has been conventional practice to regard an electrical resonance coil as being quite unsuitable for use in making precision hydrate-related measurements.

[0010] Experimental studies associated with devising the present invention have surprisingly shown that suitable excitation of a coil having a sufficient number of turns and an adequate length in relation to its diameter allows water content measurements to be performed to concentrations as low as a few parts per million (p.p.m.). Such high accuracy measurement is feasible utilizing a water content measurement apparatus as illustrated in FIG. 1; the water content measurement apparatus is indicated generally by **10.** The apparatus **10** includes a polymer material tube **20,** for example fabricated from polycarbonate, acrylic-type or PEEK plastics materials; such polymer materials are chosen to exhibit relatively low dielectric losses at a frequency of several MHz. The tube **20** beneficially has an inside diameter *d* in a range of 70 to 90 mm, and a length provided with windings in a range of 280 mm to 320 mm; however, the apparatus **10** is susceptible to being adapted at larger diameters above 90 mm. The tube **20** is provided at its first end with an excitation coil **30A** comprising a single turn. In a middle portion of the tube **20,** there is provided a resonance coil **30B** comprising in a range of 30 to 50 turns which is optionally terminated with a capacitor C of value 32 pF; for example, 34 turns for the coil **30B** is found to function well in practice. The capacitor C is beneficially a high-quality capacitor exhibiting low dielectric losses at operating frequencies of a few MHz, for example a high-quality ceramic capacitor, Mica dielectric capacitor or sealed air-cored capacitor. The resonance coil **30B** coupled to its associated capacitor C is operable to exhibit a resonance frequency in an order of a few MHz, for example in a range of 1 MHz to 5 MHz, although other operating frequencies can be employed if required. The resonance coil **30B** is beneficially uniformly wound along the length /, such that the coil **30B** has a diameter:length ratio in a range of 1:3 to 1:5. Ratios in excess of 1:5 can optionally be employed. Beneficially, the coil **30B** is wound from Litz wire (namely individually insulated wire strands) or from thin Copper tape with associated insulation to reduce conductor skin-depth effects in the coil **30B** from adversely affecting its Q-factor to detriment of sensitivity of the apparatus **10** to minute quantities of water present in the tube **20.** Optionally, an outer conducting surface of windings of the coil **30B** is silver plated to increase a resonance Q-factor of the coil **30B.** Moreover, the tube **20** also includes a pickup coil **30C** comprising a single turn. The capacitor *C* is beneficially spatially located in close proximity to the coil **30B** as illustrated for obtaining most accurate measurement of water content, for example in gases flowing in operation through the tube **20** in conditions in which hydrate deposition would be expected to arise. The tube **20** and its coils **30A, 30B, 30C** are furnished with an outer peripheral screening shield **40** fabricated from Aluminium sheet, stainless steel or similar. Beneficially, the shield is designed to be able to withstand a pressure that is likely to be encountered within the tube 20. Optionally, the Aluminium sheet employed to fabricate the shield 40 has a thickness which is less than 1 mm, for preferably less than 0.5 mm. Alternatively, or additionally, outer fibre glass or carbon composite shielding for the tube 20 and its coils 30A, 30B, **30C** is employed.

[0011] The excitation coil 30A is coupled to a generator 50 which is operable, for example, to output a temporal series of pulses **60** having a pulse duration τ_p and a pulse repetition frequency f_p. Beneficially, the pulse duration τ_p is much shorter than a period between pulses **60,** namely

$$\frac{1}{f_p}$$

by at least an order of magnitude.

[0012] The pickup coil **30C** is connected via two well-screened coaxial cables **70** to a signal processing unit **80** employing computing hardware executing software products for analyzing signals induced in operation in the pickup coil **30C** to generate corresponding analysis results. The processing unit **80** is operable to present the analysis results on a display **90** indicative of concentration of water content present within the tube **20,** for example potentially to trace levels as low as a few parts per million (p.p.m.) of water content being present within the tube **20.** Optionally, the processing unit **80** is adapted to monitor water concentration, temperature and conductivity on an inside surface of the tube **20** for identifying conditions in which hydrate deposition is likely to arise.

[0013] Resonance characteristics of the coil **30B** are strongly affected depending upon whether or not water present within the tube **20** is saline in nature. Salt content in a salt solution affects a freezing temperature of the solution, and therefore affects a temperature at which hydrate deposition can arise when the solution is present together with a hydrocarbon, for example methane or propane. On account of the highly conductive nature of saline solution, it is necessary for the apparatus **10** to include additionally a sensor arrangement **100** on an inside surface of the tube **20,** wherein the sensor arrangement **100** includes a temperature sensor for measuring a temperature *T* of the inside surface of the tube **20** and a surface electrical conductivity sensor for measuring an electrical conductivity σ of a film formed in operation of the inside surface of the tube **20.** Signals associated with the sensor arrangement **100** conveyed to the processing unit **80** are illustrated in FIG. 2. The processing unit **80** is programmed to perform a computation represented by Equation 1 (Eq. 1):

$$w = F(Q, f_r, T, \sigma, P) \qquad \text{Eq. 1}$$

wherein

w =
: water concentration;

P =
: pressure within the tube **20;**

Q =
: Q-factor of resonance of the coil **30B** subject to excitation;

T =
: temperature of inside surface of the tube **20;**

σ =
: electrical low-frequency or d.c. conductivity of a moisture film formed on the inside

surface of the tube **20;** and

F =

a conversion function determined from experimental calibration measurements.

[0014] The function *F* is beneficially implemented as a lookup table implemented in computer memory of the processing unit **80.** Optionally, the function *F* is determined empirically by performing a series of experimental tests to derive measurement data, and then synthesizing intermediate measurements by mathematical extrapolation to provide the function *F* as a continuously variable function. Alternatively, the function *F* can be derived analytically from theoretical consideration of the sensor arrangement **100.** The Q-factor *Q* is determined from an envelope of a temporal signal decay characteristic as illustrated in FIG. 3A and FIG. 3B wherein the signal is described substantially by Equation 2 (Eq. 2):

$$s = v_0 e^{\frac{t}{\tau}} \sin \omega t \qquad \text{Eq. 2}$$

wherein

s =

signal induced in the pickup coil **30C;**

v_0 =

amplitude coefficient of the signal *s*;

τ =

exponential decay time constant of the response signal arising from electrical responance of the coil **30B;**

ω =

resonance frequency of the coil **30B;** and

t =

time.

[0015] The sensor arrangement **100** can be implemented in various different ways. For example electrodes of the sensor arrangement **100** for measuring electrical conductivity can be implemented as annular ring electrodes around an inner circumferential surface of the tube **20** and disposed in a direction along an elongate axis of the tube **20.** Alternatively, or additionally, electrodes of the sensor arrangement **100** for measuring electrical conductivity can be implemented as sectors of limited angular extent for sensing inhomogeneous deposition of hydrates onto the inner surface of the tube **20.** Beneficially, the conductivity sensing electrodes are selected or treated to have a similar wetting characteristic to other parts of the tube **20** so that hydrate formation measurements provided by the apparatus **10** are as representative as possible for other tube connected to the tube **20.** Similarly, the temperature sensor of the sensor arrangement **100** can be implemented as one or more individual temperature sensors which are spatially disposed for sensing temperature gradients within the tube **20.** For purposes of computing Equation 1 (Eq. 1), an aggregate or average of the several temperature measurements from a plurality of temperature sensors of the sensing

arrangement **100** can be used. The inside surface of the tube **20** is beneficially smooth for avoiding non-representative deposition of hydrate deposits onto the inside surface.

[0016] FIG. 3A and FIG. 3B are illustrations of resonance characteristics exhibited by the coil **30B** as sensed using the pickup coil **30C.** In a preferred embodiment of the invention, the coil **30B** beneficially has 34 turns and is optionally tuned with a capacitor *C* having a capacitance value 32 pF. Alternatively, the coil **30B** has 15 turns and is optionally tuned with a capacitor *C* having a capacitance value 100 pF. Correct impedance matching of the excitation coil **30A** is highly beneficial for obtaining an uncluttered waveform as presented in FIG. 3A and FIG. 3B; the impedance matching corresponds to a filter which reduces excitation of higher-order resonances within the coil **30B,** for example at frequencies approximately an order of magnitude above its main resonance frequency, for example at around 35 MHz when the coil **30B** has a fundamental resonance around 3.5 MHz. Matching components as illustrated in FIG. 2 including a T-arrangement comprising a series connection of 50 Ω, 33 Ω resistors and a1000 pF capacitor to signal ground at a midpoint between the resistors has been found from experimental studies to function well for the apparatus **10.** A relatively high Q-factor resonance of FIG. 3A corresponds to the tube **20** devoid of water; in contrast, FIG. 3B corresponds to a lower Q-factor response arising when the tube **20** contains a quantity of fresh water. By accurate measurement of Q-factor executed by the processing unit **80** when processing the pickup signal from the pickup coil **30C,** the apparatus **10** is capable of detecting very small concentrations of water within the tube **20,** for example to concentrations of a few parts per million (p.p.m.). The very high sensitivity of the apparatus **10** is also illustrated in FIG. 4 which is a graph having an abscissa axis representative of water fraction β present within the tube **20,** and an ordinate axis providing a measured parameter (*tau,* τ) indicative of the Q-factor of resonance of the coil **30B** a sensed via the pickup coil **30C.**

[0017] As will be elucidated in greater detail later, by exciting the coil **30B** to resonate, there is providing thereby an indication, via Q-factor measurement pursuant to the present invention, for establishing whether or not hydrate formation is likely to occur within a region encircled by the coil **30B.** The Q-factor measurement is beneficially determined from a natural undriven Q-factor of the coil **30B,** namely without disturbances arising from a finite driving impedance of the excitation coil **30A.** The pickup coil **30C** is beneficially arranged to represent a high impedance to the coil **30B,** and thereby has a negligible influence upon the resonance of the coil **30B.** Beneficially, the excitation coil **30A** is driven momentarily to excite the coil **30B** into resonance, and then the resonance of the coil **30B** is allowed to decay naturally with the excitation coil **30A** "open circuit" so that the excitation coil **30A** does not influence the Q-factor of the coil **30B,** namely permits the coil **30B** to exhibit its natural resonance having a natural resonant frequency ω_n. By monitoring the natural resonance of the coil **30B,** an improved measurement accuracy can be achieved from the apparatus **10.** In the apparatus **10,** the Q-factor measurement of the coil **30B** can either be performed in a continuous driven manner or in a pulse-resonant excited manner, or by employing a mixture of such measurement techniques.

[0018] The apparatus **10** provides a benefit that its pulse excitation manner of operation

enables the generator **50** and the data processor **80** to be located spatially remotely from the tube **20** and its associated coils **30A, 30B, 30C** and optional sensor arrangement **100.** Such flexibility is highly beneficial when the tube **20** is required to operate at temperatures which would be hostile to electronic components associated with the data processor **80** and the generator **50.** The apparatus **10** is susceptible to being employed in a large range of applications. For example, the apparatus **10** can be used in ocean-bed hydrate handling equipment, in separation tanks, down boreholes, in carbon dioxide capture and sequestration systems associated with climate change carbon tax funded facilities, in chemical industries, in space probes and similar. Measurement methods employed in the apparatus **10** will be described in more detail later.

[0019] It will be appreciated that the apparatus **10** is not operable to measuring a presence of hydrate deposits directly, but rather is able to provide an indication of a likelihood of hydrate deposit formation (hydrate ice crystals) based upon measured conditions of conductivity, temperature and pressure in combination with determining a concentration of water present within the tube **20.** Optionally, the generator **50** is operable to excite the coil **30A** by way of a repetitive burst of a plurality of pulses as an alternative to periodic single pulses; such burst excitation enables a better signal-to-noise (S/N) to be achieved in relation to electronically-generated noise arising within the apparatus **10,** in combination with a reduced tendency to excite higher order resonances within the coil **30B.**

[0020] In FIG. 1, the peripheral screening shield **40** is described in the foregoing as being fabricated from Aluminium. Alternatively, the screen **40** is fabricated from a recognized type of steel which is able to withstand gas and liquids which the apparatus **10** will encounter during transportation and operation. A region between an outside surface of the tube **20** and the screen **40** is beneficially filled with a mechanical robust insulating material exhibiting a relative permeability of approximately unity; for example the coils **30A, 30B, 30C** can beneficially be appropriately encapsulated (namely "potted") in a hydrocarbon polymer materials resin, for example an epoxy or polyurethane material. Optionally, the screen **40** includes fibre glass, carbon fibre or other strong polymer structural components, for example fabricated from stainless steel which can withstand a pressure within the tube **20** and thereby enable the instrument **10** to survive structurally in an unlikely event that the tube **20** ruptures in operation.

[0021] Referring again to Equation 1 (Eq. 1), the apparatus **10** operates to measure subtle characteristics whose nature is not generally appreciated. For example, a kink **500** in the curve of FIG. 4 is not a measurement inaccuracy, but rather a genuine relaxation effect resulting from spontaneous momentary alignments of groups of polarized water molecules to form larger momentary dipole moments which are many orders of magnitude larger than the dipole moments of individual water molecules. Such larger dipole moments are observed in the formation of ice crystals. In FIG. 5, there is a shown a graph pertaining to the Q-factor exhibited by the coil **30B** as a proportion of saline solution within the tube **20** is varied. An abscissa axis **400** denotes a percentage of saline solution present in the tube **20** and an ordinate axis **410** denoting the time constant *tau,* τ of resonance of the coil **30B;** the Q-factor Q of the coil **30B** is directly susceptible to being computed from the time constant *tau,* τ. It will be

observed in FIG. 5 that a minimum Q-factor occurs at a saline proportion β of around 0.5% with a high sensitivity below 0.5%, namely below 5000 p.p.m., wherein discrimination of presence of saline solution to within tens' of p.p.m. is achievable using the apparatus **10.**

[0022] In FIG. 6, a response of the apparatus **10** to saline solution within the tube **20** is shown, wherein an abscissa axis **500** denotes percentage weight of salt within a saline solution present within the tube **20,** and an ordinate axis **510** denotes the time constant *tau,* τ. The resonance characteristic of the coil **30B** exhibits a distinct peak **520** at around 3% salt (Sodium Chloride, *NaCl*) by weight present in the solution corresponding to greatest Q-factor, reducing with salt percentage above 3% as conductivity of the solution increases and also falling for concentrations below 3% on account of aforementioned relaxation effects caused by spontaneous momentary polarisation alignment of water molecules to create a large effective dipole moment. Between 0% salt weight content and 3% salt weight content, increasing salt content hinders spontaneous association of water molecules to form a large momentary effective dipole moment by way of Chlorine atoms screening highly polarized hydrogen atoms (protons), thereby resulting in a corresponding progressive increase in Q-factor. Both FIG. 5 and FIG. 6 exhibit a rapidly changing measurement characteristic near zero which imparts the apparatus **10** with excellent measurement characteristics for trace amounts of fresh water or saline solution. Such a measurement characteristic is well suited for identifying conditions where there is a potential risk of hydrate deposits being formed which can block tubes, for example in an offshore gas production and processing facility.

[0023] In FIG. 7, sources of noise arising within the apparatus **10** are illustrated schematically. These noise sources influence an accuracy to which the Q-factor of the coil **30B** can be measured. The Q-factor of the coil **30B** is greatest when its encircled region is filled with dry gas; this is conveniently referred to as being Q_{dry}. When traces of fresh water or saline water are introduced into the encircled region, the Q-factor of the coil **30B** is reduced; this is conveniently referred to as being Q_{wet}. The Q-factor Q_{dry} is influenced by the temperature *T,* for example as a result of winding resistances of the coil **30B** changing with the temperature *T.* Thus, inherent in Equation 1 (Eq. 1) is a subtraction function as described in Equation 3 (Eq. 3):

$$w = F((Q_{dry}(T)-Q_{wet}(T)),f_r,T,\sigma,P) \quad \text{Eq. 3}$$

$Q_{dry}(T)$ can be determined by accurate measurement. $Q_{wet}(T)$ is determined as the apparatus **10** is employed in practice. It will be appreciated that Q_{dry} and Q_{wet} can be relatively large numbers, for example in an order of 100 or more, and hence need to be measured to high precision for detecting occurrence of water to a sensitivity in an order of p.p.m. Such precision is influenced by noise and drift effects occurring within the apparatus **10** when in use.

[0024] In FIG. 7, the sources of noise occurring within the apparatus **10** include a first noise source **600** affecting the Q-factor arising from flow turbulence within a spatial region surrounded by the tube **20** surrounded by the coil **30B.** Such flow turbulence is quasi-constant within a time period of signal decay illustrated in FIG. 3A and FIG. 3B, but will vary from one measurement of Q-factor of the coil **30B** to another thereof over a monitoring period of several

seconds or minutes, for example. Electronic noise *E1* arising in an electronic amplifier **610** receiving signals from the pickup coil **30C** arises, but is relatively constant; however, the electronic noise *E1* is influenced by an operating temperature of the amplifier **610.** Beneficially, the amplifier **610** is cooled by Peltier elements or a cryogenic engine to reduce its electronic noise *E1.* Digital electronic circuits **620** which receive an output signal from the amplifier **610** cause electronic noise *E2,* for example quantization noise, which is beneficially reduced by suitable design choice of components, for example by employing high-resolution ADC components for converting amplified analog signals from the amplifier 610 into corresponding digital sampling data. Noise sources **630, 640, 650** are associated with conductivity measurements, temperature measurements and pressure measurements respectively and can arise from corrosion (i.e. drift effects), electrochemical effects and ageing of electronic components. In practice, the noise source **600** is dominant and beneficially requires novel approaches to measurement technique pursuant to the present invention to obtain p.p.m. measurement accuracy results when detecting a presence of water within the tube **20.**

[0025] Measurements of resonance Q-factor of the coil **30B** are beneficially performed using a circuit as illustrated in FIG. 8. The circuit is indicated generally by **700** and includes a gated phase-locked-loop (PLL) including the aforesaid amplifier **610** for receiving a signal from the pickup coil **30C,** a phase detector **710** for receiving an output signal S_1 of the amplifier **610,** a phase integrator **720** for receiving a phase error output signal S_2 of the phase detector **710** wherein the phase integrator **720** is provided with an associated gating switch **730** for locking an output signal S_3 of the integrator **720** when required, a voltage-controlled oscillator (VCO) **740** controlled by the output signal S_3 of the phase integrator **720,** a drive amplifier **750** for receiving an output signal S_4 from the oscillator (VCO), and a switch **760** for receiving an output signal S_5 of the drive amplifier **750** and coupled to the excitation coil **30A.** There is also included a microprocessor **800** for providing a phase reference signal φ_K to the phase detector **710,** for providing a gating signals G to the switches **730, 760,** and for receiving the signal S_1. The microprocessor **800** is operable to execute software products recorded on machine-readable data storage media to generate an output indicative of water content as measured by the apparatus **10.**

[0026] The phase integrator **720** is implemented either by analog components or digitally, and is provided with the switch **730** for momentarily holding the output signal S_3 of the integrator **720** constant, thereby maintaining an output frequency of the signal S_4 momentarily constant. Optionally, the oscillator **740** synthesizes a sine-wave for the signal S_4 and its output is derived from a stable high-frequency reference, for example derived from a high-stability quartz-crystal oscillator forming a part of the oscillator **720.**

[0027] In operation, the circuit **700** functions in two modes, namely a first excitation mode and a second measurement mode. In the first excitation mode, the oscillator **730** is swept to find a driven resonance frequency ω_0 of the coil **30B** and the phase signal φ_K is then adjusted by the microprocessor **800** so that the amplitude of the signal S_1 is adjusted to its maximum

amplitude; this occurs with the switch **760** closed to couple the signal S_5 to the excitation coil **30A.** When a maximum amplitude for the signal S_1 is achieved, the coil **30B** is resonating at its driven resonance frequency ω_0.

[0028] Thereafter, the circuit **700** is operated in its second mode, wherein the oscillator **730** is locked at the frequency ω_0 via use of the switch **730** controlled from the microprocessor **800;** optionally, the oscillator **740** is adjusted slightly down in frequency to an estimate of its natural undriven resonant frequency ω_n, namely when the coils **30A, 30C** are effectively open-circuit. The microprocessor **800,** via the switch **760,** then pulse excites the excitation coil **30A,** and hence excites the coil **30B,** using one or more pulses preferably at a frequency ω_n and thereafter opens the switch **760,** so that the coil **30B** exhibits a natural resonance at a frequency ω_n with a decay envelope akin to that illustrated in FIG. 3A and FIG. 3B from which a measure of Q-factor may be derived using the microprocessor **800** to digitize and analyze the signal S_1 during the decay envelope, for example as illustrated in FIG. 3A and FIG. 3B. The first mode followed by the second mode is beneficially implemented within a time period during which the noise source **600** on FIG. 7 is quasi-constant.

[0029] FIG. 9 illustrates a difference between the driven resonance frequency ω_0 of the coil **30B** in comparison to the natural resonance frequency ω_n. An amplitude of the signal S_1 is denoted along an ordinate axis **830** and the driving frequency of the signal S_5 is denoted along an abscissa axis **820.**

[0030] By repeating the first mode followed promptly by the second mode a plurality of times, a series of Q-factor measurements Q_1, ... Q_m are obtained during a measurement time period. On account of turbulence noise arising within the tube **20** and electronic noise as aforementioned, the series of Q-factors fall generally within a Gaussian-bell frequency-of-occurrence distribution as illustrated in FIG. 10 as computed by the microprocessor **800.** An abscissa axis **900** denotes frequency of resonance as approximately determined from the signal S_5, and an ordinate axis **910** denotes a frequency-of-occurrence of given Q-factors in the sample of Q-factor Q_1, ... Q_m., denoted by g(Q). In the results illustrated, the microprocessor **800** determines a most representative Q-factor to employ for Equation 1 (Eq. 1) by performing analytical processing on the series of measured Q-factors Q_1, ... Q_m as will now be described.

[0031] In signal processing performed by the microprocessor **800,** lower and upper results denoted by **920, 930** are beneficially ignore, namely truncated, and more central Q-factor results are in a region **940** are employed to derive a reliable measure of the Q-factor to employ for Equation 1 (Eq. 1). For example, the upper and lower results **920, 930** correspond to upper and lower quartiles of the Q-factor distribution of FIG. 10. In a first processing method, the results in the region **940** are averaged to derive a representative value of Q-factor at the natural resonant frequency ω_n of the coil **30B.** In an alternative second processing method, the Q-factor results in the region **940** are subject to one or more auto-correlations which defines

very accurately a best measurement of Q-factor at an auto-correlation peak. By such an approach, the microprocessor **800** of the instrument **10** is capable of determining a representative value for the Q-factor of the coil **30B** to extreme precision, which subsequently enables water factions present in the tube **20** in vicinity of the coil **30B** to be measure to potentially p.p.m. accuracy using Equation 1 (Eq. 1).

[0032] In overview, the circuit **700** is beneficially operable to measure the Q-factor of the coil **30B** at natural resonance ω_n, and then process corresponding Q-factor measurements to remove stochastic errors which, in turn, enables Equation 1 (Eq. 1) to be employed to high accuracy to determine a water faction present within the tube **20,** for example potentially to p.p.m. accuracy.

[0033] As an alternative, the circuit **700** is capable of being employed in other manners for measuring Q-factor of the coil **30B.** For example, the circuit **700** is adjusted to find a driven peak resonance of the coil **30B** at a frequency ω_0, and then a phase adjustment provided by way of the phase control φ_K is applied by the microprocessor **800** to switch between phase intervals below and/or above resonance of the coil **30B,** for example corresponding to -3 dB points, and corresponding Q-factor measurements Q_1, ... Q_m obtained which are then optionally processed as aforementioned to correct for stochastic influences to derive a final measure of the Q-factor to employ in Equation 1 (Eq. 1) for computing the water faction w present in the tube **20.** Such continuous non-pulse measurement is illustrated in FIG. 11 where an abscissa axis **950** denotes phase and an ordinate axis **960** denotes amplitude of the signal S_1, for example for -3 dB, 0 dB, -3 dB points corresponding to operating control phases of -45°, 0°, +45° respectively, corresponding to excitation frequencies ω_l, ω_0, ω_u respectively; a measure of Q-factor of the coil 30B can be computed readily from the frequencies ω_l, ω_0, ω_u.

[0034] From the foregoing, it will be appreciated that operation of the instrument **10** to measure water content to an accuracy of p.p.m. requires that the coil **30B** be appropriately designed together with advanced signal processing techniques being employed to reduce error sources so that a highly reliable and accurate measurement of Q-factor can be derived from which the water fraction w present can be accurately and reliably computed.

[0035] Modifications to embodiments of the invention described in the foregoing are possible without departing from the scope of the invention as defined by the accompanying claims. Expressions such as "including", "comprising", "incorporating", "consisting of", "have", "is" used to describe and claim the present invention are intended to be construed in a non-exclusive manner, namely allowing for items, components or elements not explicitly described also to be present. Reference to the singular is also to be construed to relate to the plural. Numerals included within parentheses in the accompanying claims are intended to assist understanding of the claims and should not be construed in any way to limit subject matter claimed by these claims.

REFERENCES CITED IN THE DESCRIPTION

This list of references cited by the applicant is for the reader's convenience only. It does not form part of the European patent document. Even though great care has been taken in compiling the references, errors or omissions cannot be excluded and the EPO disclaims all liability in this regard.

Patent documents cited in the description

- WO2004025288A1 **[0002]**
- WO03050529A **[0002]**

Patentkrav

1. Anordning til måling af vandindhold (10) til at måle vandindhold, der er til stede i en fluidstrøm gennem et rør (20), hvor anordningen (10) indbefatter en generator (50) til at generere et pulseret anslagssignal (60) under drift, en spoleindretning (30A, 30B, 30C), der er anbragt omkring røret (20), som er indrettet til at blive anslået i resonans med anslagssignalet (60) og samvirke med fluidstrømmen gennem røret (20), og en signalprocessor (80), der er indrettet til at modtage resonanssignaler fra spoleindretningen (30A, 30B, 30C) til at bestemme et vandindhold, som er til stede inden i røret (20), hvor spoleindretningen (30A, 30B, 30C) indbefatter en resonansspole (30B), der har et forhold mellem længde og diameter, som i det mindste er 3:1, hvor resonansspolen (30B) indbefatter i det mindste 10 vindinger, og hvor generatoren (50) er indrettet til at generere impulser, der har en impulslængde, som er meget kortere end en periode mellem impulser.

2. Anordning til måling af vandindhold (10) ifølge krav 1, hvor generatoren (50) er indrettet til at generere anslagssignalet til at være en midlertidig serie af anslagsimpulser.

3. Anordning til måling af vandindhold (10) ifølge krav 1 eller 2, hvor røret (20) og dets forbundne spoleindretning (30A, 30B, 30C) er omgivet af en elektrostatisk afskærmning (40) til afskærmning af spoleindretningen (30A, 30B, 30C), når den er i drift.

4. Anordning til måling af vandindhold (10) ifølge krav 1, 2 eller 3, der yderligere indbefatter en sensoranordning (100) til at registrere lavfrekvent elektrisk ledningsevne og temperatur på en indvendig væg af røret (20) og for at tilvejebringe tilsvarende sensorsignaler til dataprocessoren (80) for at muliggøre signalprocessoren (80) at beregne vandindholdet indeni røret (20) uafhængigt af saltholdigheden

af vandindholdet.

5. Anordning til måling af vandindhold (10) ifølge krav 1, 2, 3 eller 4, hvor spoleindretningen (30) indbefatter anslags-, resonans og pickupspoler (30A, 30B, 30C), hvor anslagsspolen (30A) er koblet til generatoren (50), pickupspolen (30B) er koblet til signalprocessoren (80) og resonansspolen (30B) er koblet til en afstemningskondensator (C) til at tilvejebringe en resonansegenskab, som er følsom over for vandindhold indeni røret (20).

6. Anordning til måling af vandindhold (10) ifølge krav 5, hvor spolerne (30A, 30B, 30C) er fremstillet af i det mindste en af: individuelt isolerede Litzetråde og/eller isolerede metalbånd.

7. Anordning til måling af vandindhold (10) ifølge et hvilket som helst af de foregående krav, hvor i det mindste en af generatoren (50) og signalprocessoren (80) under drift er indrettet til at være rumligt fjern fra røret (20) og dets spoleindretning (30A, 30B, 30C).

8. Anordning til måling af vandindhold (10) ifølge et hvilket som helst af de foregående krav, hvor røret (20) er fremstillet af i det mindste en af: polycarbonatpolymer og/eller acrylpolymer og/eller PEEK.

9. Fremgangsmåde til betjening af en anordning til måling af vandindhold (10) ifølge et hvilket som helst af de foregående krav, hvor anordningen (10) er indrettet til at overvåge betingelserne for potentiel hydratdannelse indeni røret (20), og
hvor detektion af meget små mængder af vand, som er til stede inden i røret, er indikativ for potentiel tidlig hydratdannelse.

10. Fremgangsmåde til måling af vandindhold, der er til stede i en fluidstrøm gennem et rør (20), kendetegnet ved, at

fremgangsmåden indbefatter:

(a) anvendelse af en generator (50) til at generere et pulseret anslagssignal (60) under drift for at anslå en spoleindretning (30A, 30B, 30C), der er anbragt omkring røret (20), til at samvirke med fluidstrømmen gennem røret (20); og

(b) modtagelse ved en signalprocessor (80) af resonanssignaler fra spoleindretningen (30A, 30B, 30C) til at bestemme et vandindhold, som er til stede inden i røret (20), hvor spoleindretningen (30A, 30B, 30C) indbefatter en resonansspole (30B), der har et forhold mellem længde og diameter, som i det mindste er 3:1, hvor resonansspolen (30B) indbefatter i det mindste 10 vindinger;

og hvor impulserne har en impulslængde, som er meget kortere end en periode mellem impulser

11. Programprodukt, som er registreret på et maskinlæsbart medium, hvor programproduktet kan eksekveres på computer hardwaren (80; 800) til at implementere en fremgangsmåde ifølge krav 10.

DRAWINGS

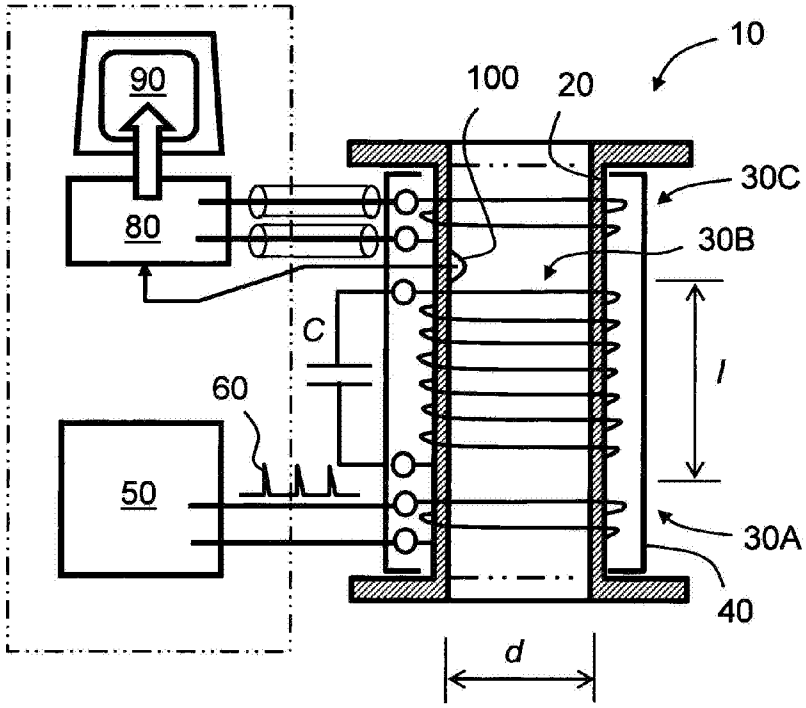


FIG. 1

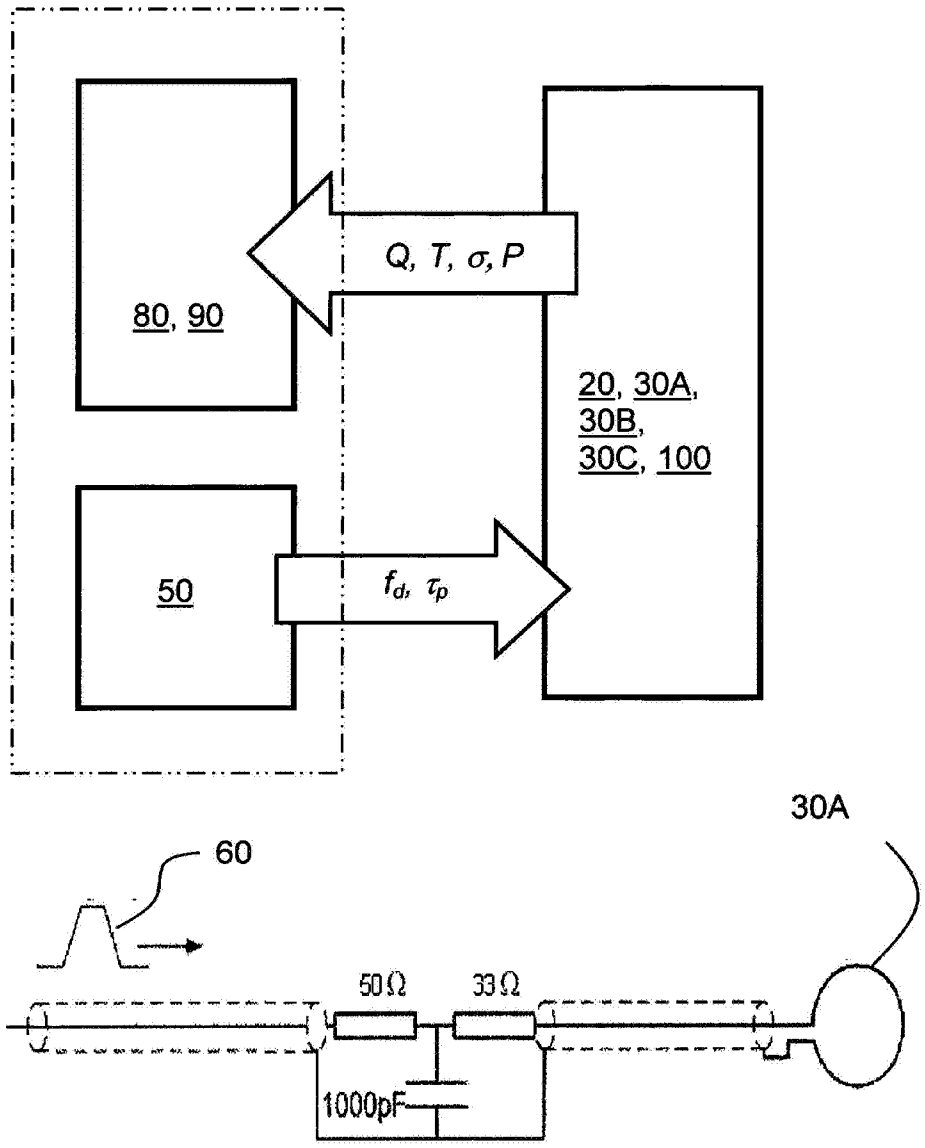


FIG. 2

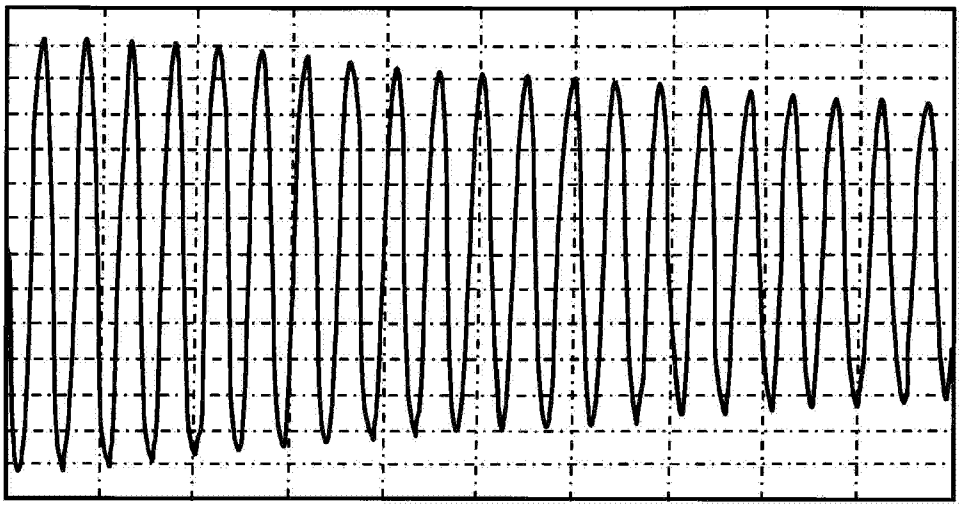


FIG. 3A

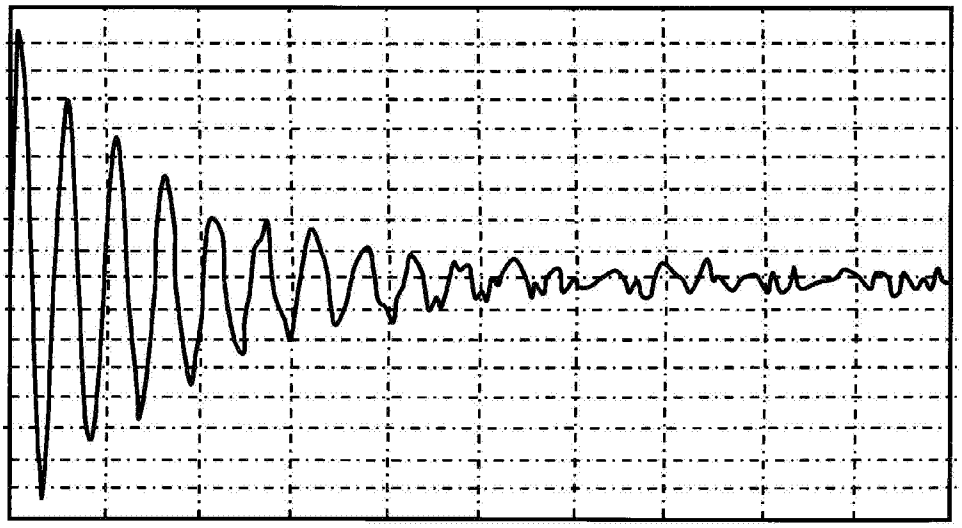


FIG. 3B

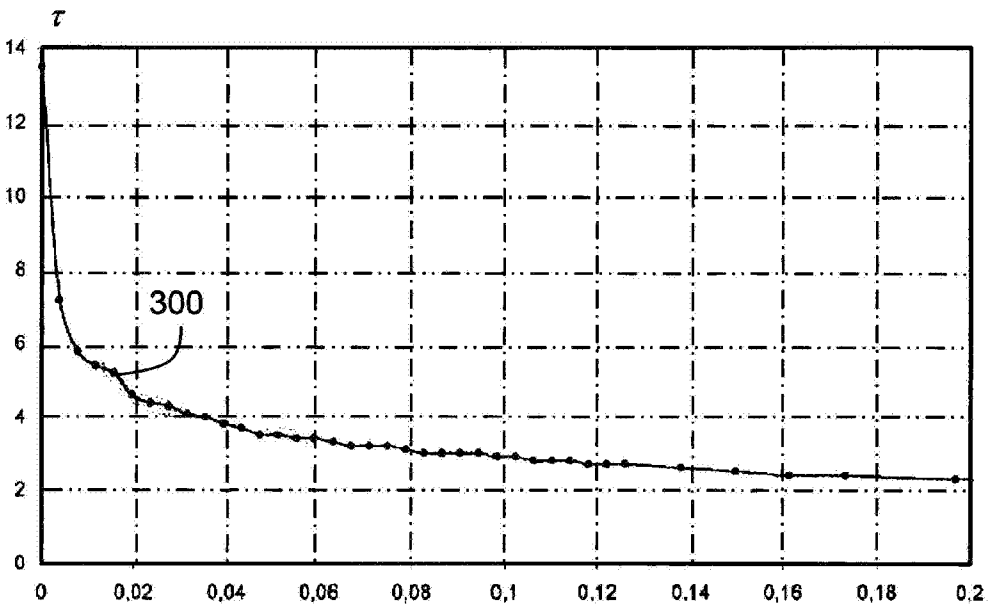


FIG. 4

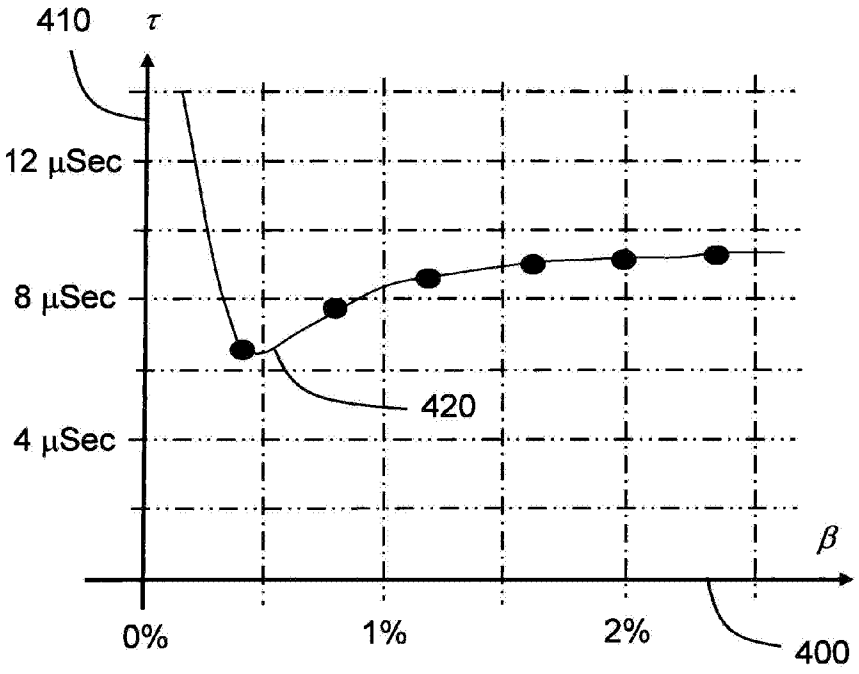


FIG. 5

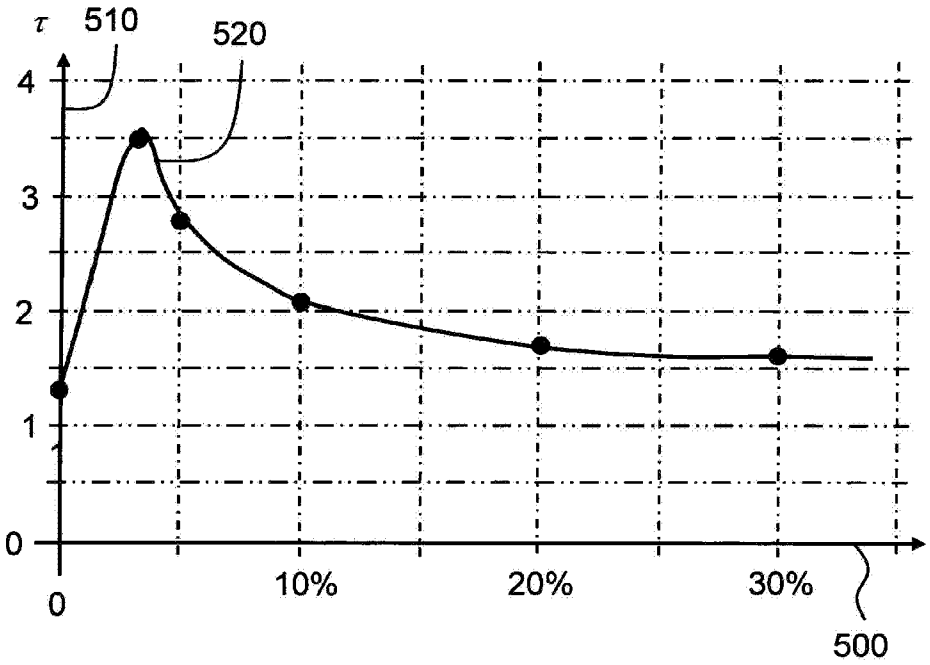


FIG. 6

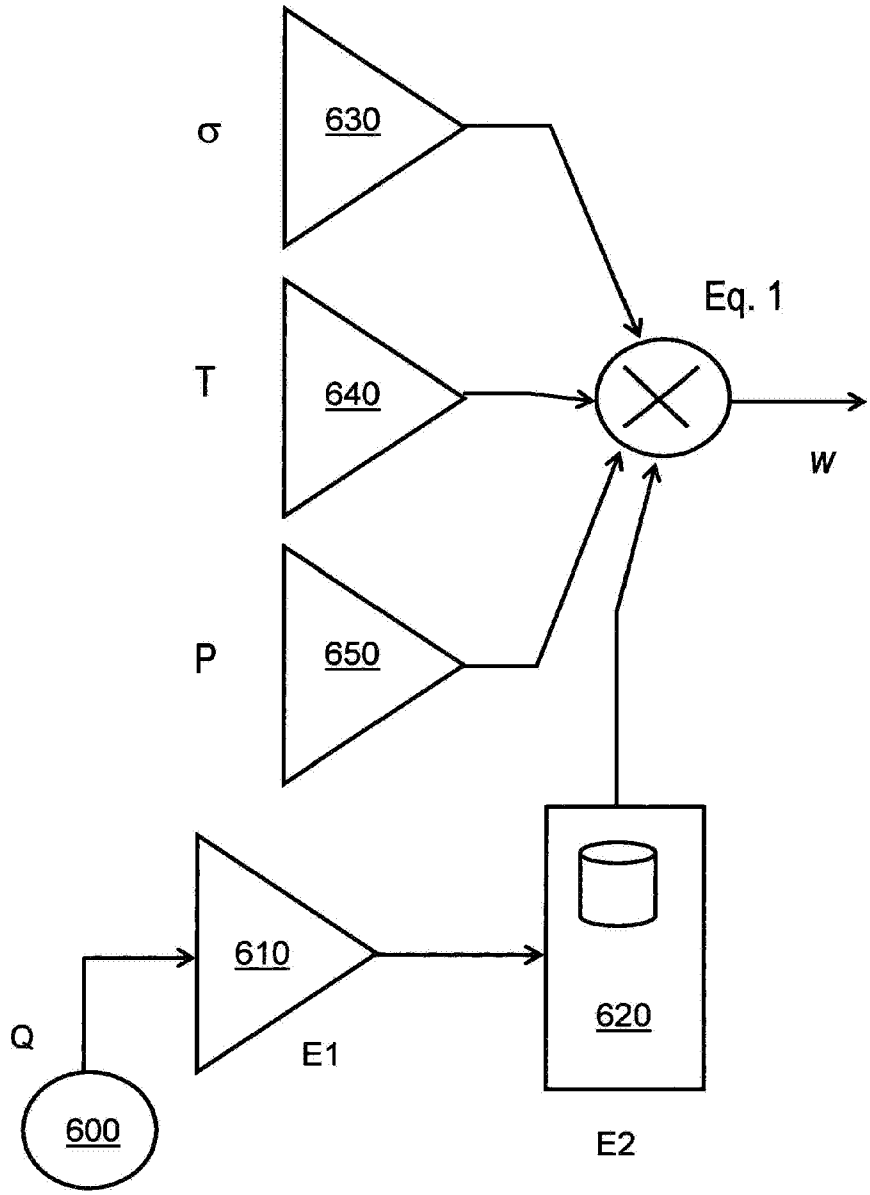
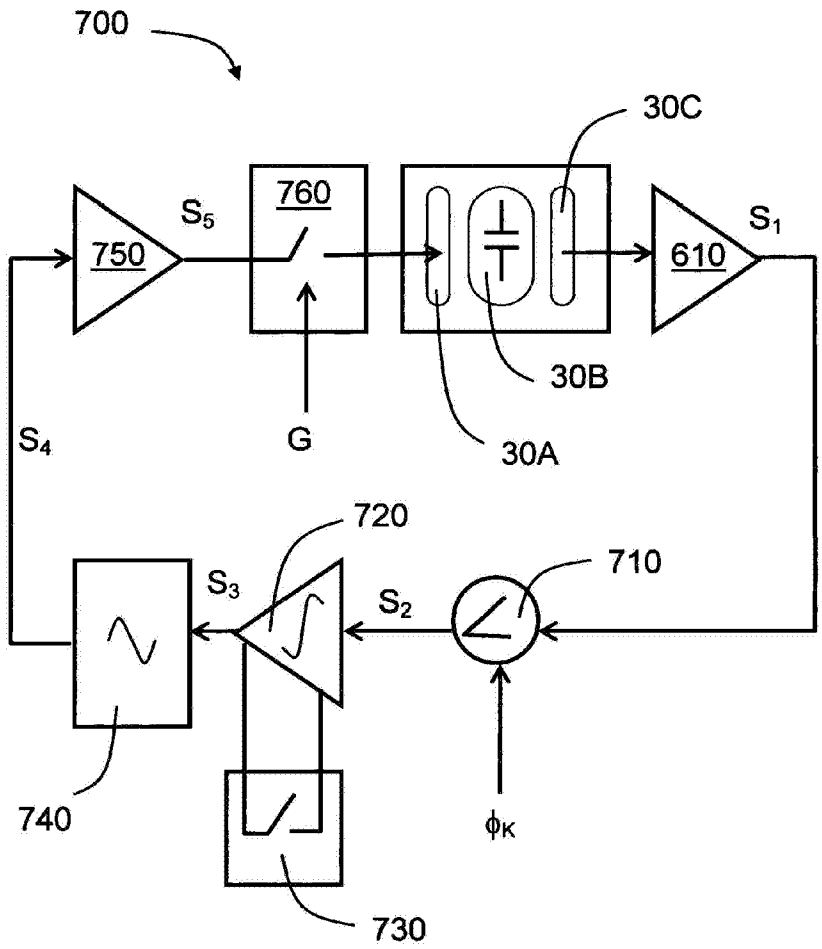


FIG. 7


700
30C
760
S5
750
610
S1
30B
G
30A
S4
720
710
S3
S2
740
ϕK
730

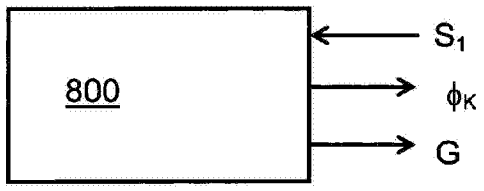

800
S1
ϕK
G

FIG. 8

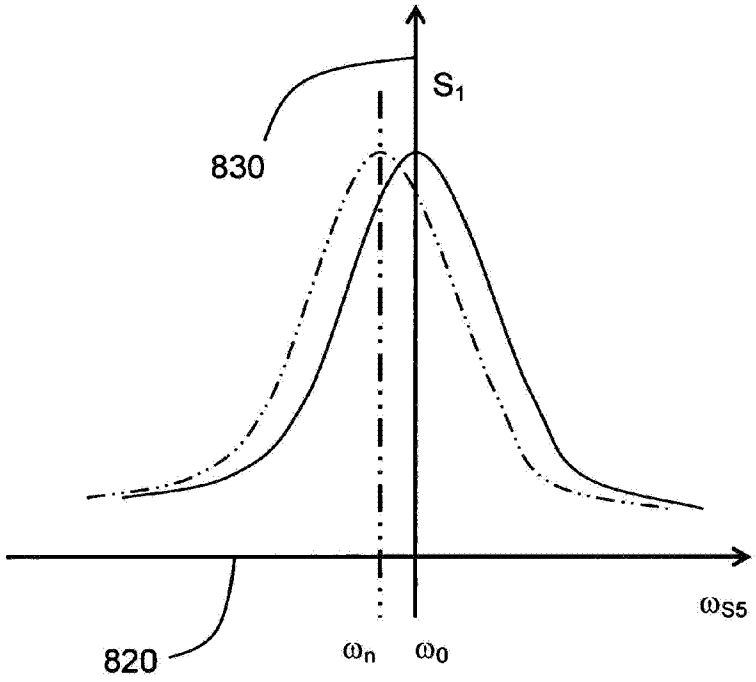


FIG. 9

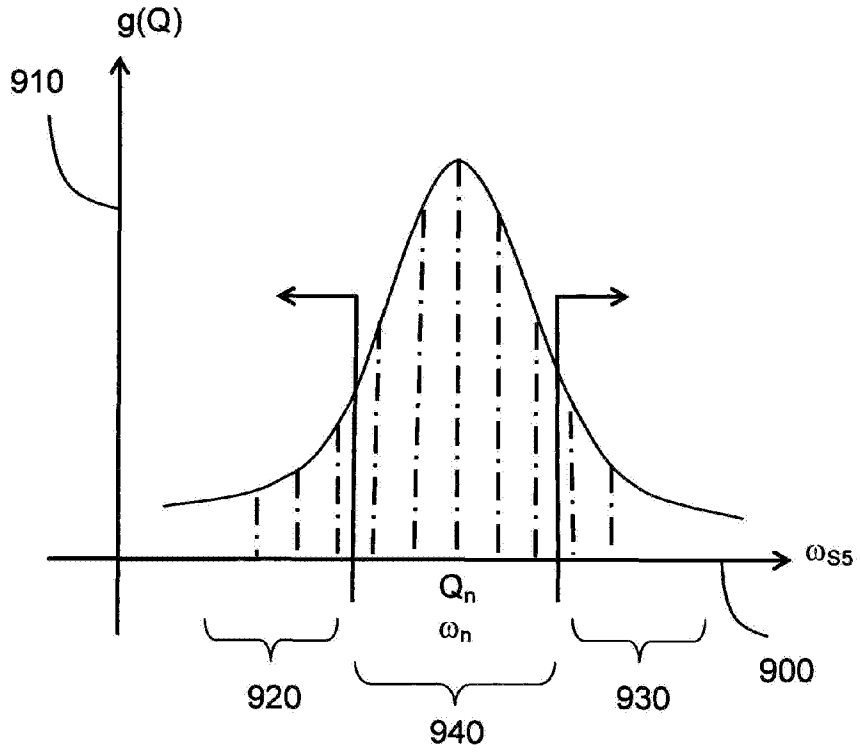


FIG. 10

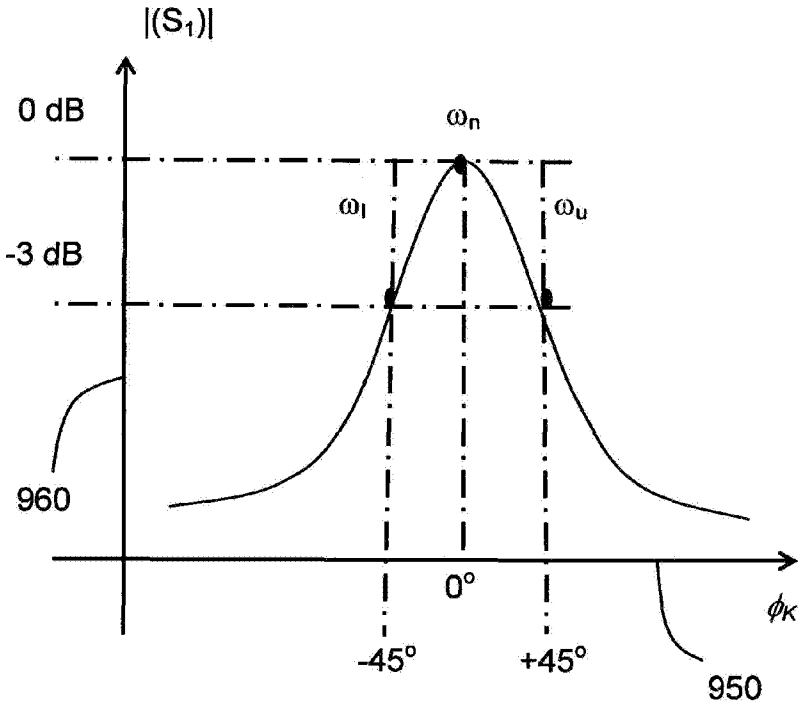


FIG. 11