Abstract:

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POLYETHYLENE COMPOSITION HAVING HIGH SWELL RATIO

The present invention provides a polyethylene composition suitable for preparing various kinds of formed articles. In particular, due to its enhanced processability, high die-swell with high-quality surface and dimension stability of final article, environmental stress cracking resistance (FNCT) and impact resistance, the present composition is suitable for making extrusion blow-moulded hollow articles, such as drums, containers and gasoline storage tanks.

The present invention also relates to a multi-stage polymerization process for preparing the said polyethylene composition.

An additional and important advantage of the polyethylene composition of the present invention is that it can be melt-processed at unusually high shear rate values, which mean high processing speeds and/or reduced melt-processing temperatures, without encountering flow-instabilities which generally produce unacceptable defects in the formed articles (e.g. shark skin or melt-fracture), even in the absence of processing aids.

Moreover, the fast crystallization kinetics of the present composition, which provides a critical contribution to its superior process-ability, also provides an unusually reduced shrinkage of the formed articles, thus allowing achieving a remarkable dimensional stability.

Thus the composition of the present invention provides an unmatched balance of mechanical properties and process-ability with respect to the known polyethylene compositions for the same use, as disclosed in particular in US6201078.

In fact, the polymers disclosed in US6201078 achieve a relatively low balance of swell ratio and environmental stress cracking resistance, as shown in the examples.

The problem of achieving a high impact resistance, reducing the flow-instabilities and improving the dimensional stability (lowering shrinkage) is not mentioned in such document.

Thus the present invention provides a polyethylene composition having the following features:

1) density from 0.945 to less than 0.952 g/cm³, preferably from 0.948 to 0.951 g/cm³, determined according to ISO 1183 at 23°C;

2) ratio MIF/MIP from 15 to 30, in particular from 17 to 29, where MIF is the melt flow index at 190°C with a load of 21.60 kg, and MIP is the melt flow index at 190°C with a load of 5 kg, both determined according to ISO 1133;
3)  SIC Index from 2.5 to 5.5, preferably from 2.5 to 4.5, more preferably from 3.2 to 3.9;

wherein the SIC Index is the Shear-Induced Crystallization Index, determined according to the following relation:

\[
\text{SIC Index} = \frac{(t_{\text{onset}, \text{sic}} \times 1000 \times t_{\text{onset}, \text{quiescent}})}{(\text{HLMI})}
\]

where \( t_{\text{onset}, \text{sic}} \) is measured in seconds and is the time required for a crystallization onset under shear rate of 1000 s\(^{-1}\), the \( t_{\text{onset}, \text{quiescent}} \) is measured in seconds and is the crystallization onset time at temperature of 125°C under no shear, determined in isothermal mode by differential scanning calorimetry (DSC); HLMI is the melt flow index determined at 190°C with a load of 21.6 kg, according to ISO 1133.

The expression "polyethylene composition" is intended to embrace, as alternatives, both a single ethylene polymer and an ethylene polymer composition, in particular a composition of two or more ethylene polymer components, preferably with different molecular weights, such composition being also called "bimodal" or "multimodal" polymer in the relevant art.

Typically the polyethylene composition of the present invention consists of or comprises one or more ethylene copolymers.

All the features herein defined, comprising the previously defined features 1) to 3), are referred to the said ethylene polymer or ethylene polymer composition. The addition of other components, like the additives normally employed in the art, can modify one or more of said features.

The ratio MIF/MIP provides a rheological measure of molecular weight distribution.

Another measure of the molecular weight distribution is provided by the ratio Mw/Mn, where Mw is the weight average molar mass and Mn is the number average molar mass, both measured by GPC (Gel Permeation Chromatography), as explained in the examples.

Preferred Mw/Mn values for the polyethylene composition of the present invention range from 20 to 30.

Moreover the polyethylene composition of the present invention has preferably at least one of the following additional features.

- Mw equal to or greater than 250000 g/mol, more preferably equal to or greater than 280000 g/mol, in particular equal to or greater than 300000 g/mol;
- Long Chain Branching index (LCB) determined as described in the examples, equal to or greater than 0.70, more preferably equal to or greater than 0.72, in particular equal to or greater than 0.80;
- MIP: 0.05 - 0.5 g/10 min.;
- MIF: 1 - 15 g/10 min;
- Comonomer content equal to or less than 1% by weight, in particular from 0.05 to 1% by weight, with respect to the total weight of the composition.

The comonomer or comonomers present in the ethylene copolymers are generally selected from olefins having formula CH$_2$=CHR wherein R is an alkyl radical, linear or branched, having from 1 to 10 carbon atoms.

Specific examples are propylene, butene-1, pentene-1, 4-methylpentene-1, hexene-1, octene-1 and decene-1. A particularly preferred comonomer is hexene-1.

In particular, in a preferred embodiment, the present composition comprises:

A) 30 - 50% by weight of an ethylene homopolymer or copolymer (the homopolymer being preferred) with density equal to or greater than 0.960 g/cm$^3$ and melt flow index MIE at 190°C with a load of 2.16 kg, according to ISO 1133, of 10 - 35 g/10 min.;

B) 50 - 70% by weight of an ethylene copolymer having a MIE value lower than the MIE value of A), preferably lower than 0.5 g/10 min.

The above percent amounts are given with respect to the total weight of A) + B).

The amount of comonomer in B) is preferably from 0.1 to 2% by weight, with respect to the total weight of B).

As previously said, the present polyethylene composition can be advantageously used in the preparation of extrusion blow-moulded hollow articles, in particular large blow moulded articles such as open-top-drums (OTD) or industrial-bulk-containers (IBC), thanks to its valuable mechanical properties.

In fact it is preferably characterized by the following properties.
- FNCT equal to or greater than 10 hours, more preferably equal to or greater than 100 hours, in particular equal to or greater than 150 hours, measured at 4 MPa, 80°C;
- Notch Tensile Impact (-30°C) equal to or greater than 100 kJ/m$^2$;
- Critical shear-rate for shark skin (190°C) equal to or greater than 250 s$^{-1}$;
- Die swell-ratio equal to or greater than 150%;
- Shrinkage at 1500 s$^{-1}$ (190°C) equal to or smaller than 17%. 

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The details of the test methods are given in the examples. In particular the shark skin test (critical shear rate for shark skin) provides an indication of the shear rate at which flow-instabilities start due to pressure oscillations, thus of the melt processing conditions, and consequently of the extrusion throughput, at which irregularities on the surface of the extruded piece become visible. Such irregularities strongly reduce surface gloss and smoothness, thus lowering the quality of the extruded article to an unacceptable level.

As previously mentioned, the polyethylene composition of the present invention can be melt-processed at surprisingly high values of shear rate, still without undergoing pressure oscillations and flow-instabilities.

While no necessary limitation is known to exist in principle on the kind of polymerization processes and catalysts to be used, it has been found that the polyethylene composition of the present invention can be prepared by a gas phase polymerization process in the presence of a Ziegler-Natta catalyst.

A Ziegler-Natta catalyst comprises the product of the reaction of an organometallic compound of group 1, 2 or 13 of the Periodic Table of elements with a transition metal compound of groups 4 to 10 of the Periodic Table of Elements (new notation). In particular, the transition metal compound can be selected among compounds of Ti, V, Zr, Cr and Hf and is preferably supported on MgCl₂.

Particularly preferred catalysts comprise the product of the reaction of said organometallic compound of group 1, 2 or 13 of the Periodic Table of elements, with a solid catalyst component comprising a Ti compound and an electron donor compound (ED) supported on MgCl₂.

Preferred organometallic compounds are the organo-Al compounds.

Thus in a preferred embodiment, the polyethylene composition of the present invention is obtainable by using a Ziegler-Natta polymerization catalyst, more preferably a Ziegler-Natta catalyst supported on MgCl₂, even more preferably a Ziegler-Natta catalyst comprising the product of reaction of:

a) a solid catalyst component comprising a Ti compound and an electron donor compound ED supported on MgCl₂;

b) an organo-Al compound; and optionally

c) an external electron donor compound ED_ext.
Preferably in component a) the ED/Ti molar ratio ranges from 1.5 to 3.5 and the Mg/Ti molar ratio is higher than 5.5, in particular from 6 to 80.

Among suitable titanium compounds are the tetrahalides or the compounds of formula \( \text{TiX}_n(\text{OR'})_m \), where \( 0 \leq n < 3 \), \( X \) is halogen, preferably chlorine, and \( R' \) is \( \text{Ci-C}1_{10} \) hydrocarbon group. The titanium tetrachloride is the preferred compound.

The ED compound is generally selected from alcohol, ketones, amines, amides, nitriles, alkoxy silanes, aliphatic ethers, and esters of aliphatic carboxylic acids

Preferably the ED compound is selected among, amides, esters and alkoxy silanes.

Excellent results have been obtained with the use of esters which are thus particularly preferred as ED compound. Specific examples of esters are the alkyl esters of C1-C20 aliphatic carboxylic acids and in particular C1-C8 alkyl esters of aliphatic mono carboxylic acids such as ethyl acetate, methyl formiate, ethyl formate, methyl acetate, propyl acetate, i-propyl acetate, n-butyl acetate, i-butyl acetate. Moreover, are also preferred the aliphatic ethers and particularly the C2-C20 aliphatic ethers, such as tetrahydrofuran (THF) or dioxane.

In the said solid catalyst component the MgCl\(_2\) is the basic support, even if minor amount of additional carriers can be used. The MgCl\(_2\) can be used as such or obtained from Mg compounds used as precursors that can be transformed into MgCl\(_2\) by the reaction with halogenating compounds. Particularly preferred is the use of MgCl\(_2\) in active form which is widely known from the patent literature as a support for Ziegler-Natta catalysts. Patents USP 4,298,718 and USP 4,495,338 were the first to describe the use of these compounds in Ziegler-Natta catalysis. It is known from these patents that the magnesium dihalides in active form used as support or co-support in components of catalysts for the polymerization of olefins are characterized by X-ray spectra in which the most intense diffraction line that appears in the ASTM-card reference of the spectrum of the non-active halide is diminished in intensity and broadened. In the X-ray spectra of preferred magnesium dihalides in active form said most intense line is diminished in intensity and replaced by a halo whose maximum intensity is displaced towards lower angles relative to that of the most intense line.

Particularly suitable for the preparation of the polyethylene composition of the present invention are the catalysts wherein the solid catalyst component a) is obtained by first contacting the titanium compound with the MgCl\(_2\), or a precursor Mg compound, optionally in the presence of an inert medium, thus preparing an intermediate product a') containing a titanium compound supported on MgCl\(_2\), which intermediate product a') is then contacted
with the ED compound which is added to the reaction mixture alone or in a mixture with other compounds in which it represents the main component, optionally in the presence of an inert medium.

With the term "main component" we intend that the said ED compound must be the main component in terms of molar amount, with respect to the other possible compounds excluded inert solvents or diluents used to handle the contact mixture. The ED treated product can then be subject to washings with the proper solvents in order to recover the final product. If needed, the treatment with the ED compound desired can be repeated one or more times.

As previously mentioned, a precursor of MgCl₂ can be used as starting essential Mg compound. This can be selected for example among Mg compound of formula MgR'₂ where the R' groups can be independently C₁-C₂₀ hydrocarbon groups optionally substituted, OR groups, OCOR groups, chlorine, in which R is a C₁-C₂₀ hydrocarbon groups optionally substituted, with the obvious proviso that the R' groups are not simultaneously chlorine. Also suitable as precursors are the Lewis adducts between MgCl₂ and suitable Lewis bases. A particular and preferred class being constituted by the MgCl₂ (R"OH)ₘ adducts in which R" groups are C₁-C₂₀ hydrocarbon groups, preferably C₁-C₁₀ alkyl groups, and m is from 0.1 to 6, preferably from 0.5 to 3 and more preferably from 0.5 to 2. Adducts of this type can generally be obtained by mixing alcohol and MgCl₂ in the presence of an inert hydrocarbon immiscible with the adduct, operating under stirring conditions at the melting temperature of the adduct (100-130°C). Then, the emulsion is quickly quenched, thereby causing the solidification of the adduct in form of spherical particles. Representative methods for the preparation of these spherical adducts are reported for example in USP 4,469,648, USP 4,399,054, and WO98/44009. Another useful method for the spherulization is the spray cooling described for example in USP 5,100,849 and 4,829,034.

Particularly interesting are the MgCl₂(EtOH)ₘ adducts in which m is from 0.15 to 1.7 obtained subjecting the adducts with a higher alcohol content to a thermal dealcoholation process carried out in nitrogen flow at temperatures comprised between 50 and 150°C until the alcohol content is reduced to the above value. A process of this type is described in EP 395083.

The dealcoholation can also be carried out chemically by contacting the adduct with compounds capable to react with the alcohol groups.
Generally these dealcoholated adducts are also characterized by a porosity (measured by mercury method) due to pores with radius up to 0.1 \( \mu \)m ranging from 0.15 to 2.5 cm\(^3\)/g preferably from 0.25 to 1.5 cm\(^3\)/g.

It is preferred that the dealcoholation reaction is carried out simultaneously with the step of reaction involving the use of a titanium compound. Accordingly, these adducts are reacted with the TiX\(_3\)OR\(_2\) compound (or possibly mixtures thereof) mentioned above which is preferably titanium tetrachloride. The reaction with the Ti compound can be carried out by suspending the adduct in TiCl\(_4\) (generally cold). The mixture is heated up to temperatures ranging from 80-130°C and kept at this temperature for 0.5-2 hours. The treatment with the titanium compound can be carried out one or more times. Preferably it is repeated twice. It can also be carried out in the presence of an electron donor compound as those mentioned above. At the end of the process the solid is recovered by separation of the suspension via the conventional methods (such as settling and removing of the liquid, filtration, centrifugation) and can be subject to washings with solvents. Although the washings are typically carried out with inert hydrocarbon liquids, it is also possible to use more polar solvents (having for example a higher dielectric constant) such as halogenated hydrocarbons.

As mentioned above, the intermediate product is then brought into contact with the ED compound under conditions able to fix on the solid an effective amount of donor. Due to the high versatility of this method, the amount of donor used can widely vary. As an example, it can be used in molar ratio with respect to the Ti content in the intermediate product ranging from 0.5 to 20 and preferably from 1 to 10. Although not strictly required the contact is typically carried out in a liquid medium such as a liquid hydrocarbon. The temperature at which the contact takes place can vary depending on the nature of the reagents. Generally it is comprised in the range from -10° to 150°C and preferably from 0° to 120°C. It is plain that temperatures causing the decomposition or degradation of any specific reagents should be avoided even if they fall within the generally suitable range. Also the time of the treatment can vary in dependence of other conditions such as nature of the reagents, temperature, concentration etc. As a general indication this contact step can last from 10 minutes to 10 hours more frequently from 0.5 to 5 hours. If desired, in order to further increase the final donor content, this step can be repeated one or more times. At the end of this step the solid is recovered by separation of the suspension via the conventional methods (such as settling and removing of the liquid, filtration, centrifugation) and can be subject to washings with solvents.
Although the washings are typically carried out with inert hydrocarbon liquids, it is also possible to use more polar solvents (having for example a higher dielectric constant) such as halogenated or oxygenated hydrocarbons.

As previously mentioned, the said solid catalyst component is converted into catalysts for the polymerization of olefins by reacting it, according to known methods, with an organometallic compound of group 1, 2 or 13 of the Periodic Table of elements, in particular with an Al-alkyl compound.

The alkyl-Al compound is preferably chosen among the trialkyl aluminum compounds such as for example triethylaluminum, triisobutylaluminum, tri-n- butylaluminum, tri-n-hexylaluminum, tri-n-octylaluminum. It is also possible to use alkylaluminum halides, alkylaluminum hydrides or alkylaluminum sesquichlorides such as AlEt₂Cl and Al₂Et₃O optionally in mixture with said trialkyl aluminum compounds.

The external electron donor compound EDₜₐₓ optionally used to prepare the said Ziegler-Natta catalysts can be equal to or different from the ED used in the solid catalyst component a). Preferably it is selected from the group consisting of ethers, esters, amines, ketones, nitriles, silanes and their mixtures. In particular it can advantageously be selected from the C2-C20 aliphatic ethers and in particulars cyclic ethers preferably having 3-5 carbon atoms such as tetrahydrofurane and dioxane.

Specific examples of the above described Ziegler-Natta catalysts and of methods for their preparation are provided in WO2004106388. However, the therein described prepolymerization of the solid catalyst component containing the Ti compound and the electron donor compound ED (solid catalyst component a)) is not comprised in the preferred embodiments according to the present invention.

In particular, the polyethylene composition of the present invention is obtainable by a process wherein all the polymerization steps are carried out in the presence of the said catalyst.

In fact it has been found that by using the above described polymerization catalyst, the polyethylene composition of the present invention can be prepared in a process comprising the following steps, in any mutual order:

a) polymerizing ethylene, optionally together with one or more comonomers, in a gas-phase reactor in the presence of hydrogen;

b) copolymerizing ethylene with one or more comonomers in another gas-phase reactor in the presence of an amount of hydrogen less than step a);
where in at least one of said gas-phase reactors the growing polymer particles flow upward through a first polymerization zone (riser) under fast fluidization or transport conditions, leave said riser and enter a second polymerization zone (downcomer) through which they flow downward under the action of gravity, leave said downcomer and are reintroduced into the riser, thus establishing a circulation of polymer between said two polymerization zones. In the first polymerization zone (riser), fast fluidization conditions are established by feeding a gas mixture comprising one or more olefins (ethylene and comonomers) at a velocity higher than the transport velocity of the polymer particles. The velocity of said gas mixture is preferably comprised between 0.5 and 15 m/s, more preferably between 0.8 and 5 m/s. The terms "transport velocity" and "fast fluidization conditions" are well known in the art; for a definition thereof, see, for example, "D. Geldart, Gas Fluidisation Technology, page 155 et seq., J. Wiley & Sons Ltd., 1986".

In the second polymerization zone (downcomer), the polymer particles flow under the action of gravity in a densified form, so that high values of density of the solid are reached (mass of polymer per volume of reactor), which approach the bulk density of the polymer.

In other words, the polymer flows vertically down through the downcomer in a plug flow (packed flow mode), so that only small quantities of gas are entrained between the polymer particles.

Such process allows to obtain from step a) an ethylene polymer with a molecular weight lower than the ethylene copolymer obtained from step b).

Preferably, the polymerization of ethylene to produce a relatively low molecular weight ethylene polymer (step a) is performed upstream the copolymerization of ethylene with a comonomer to produce a relatively high molecular weight ethylene copolymer (step b). To this aim, in step a) a gaseous mixture comprising ethylene, hydrogen and an inert gas is fed to a first gas-phase reactor, preferably a gas-phase fluidized bed reactor. The polymerization is carried out in the presence of the previously described Ziegler-Natta catalyst. Preferably, no comonomer is fed to said first gas phase reactor and a highly crystalline ethylene homopolymer is obtained in step a). However, a minimal amount of comonomer may be fed with the proviso that the degree of copolymerization in step a) is limited so that the density of the ethylene polymer obtained in step a) is not less than 0.960 g/cm³.

Hydrogen is fed in an amount depending on the specific catalyst used and, in any case, suitable to obtain in step a) an ethylene polymer with a melt flow index MIE from 10 to 35 g/10 min. In order to obtain the above MIE range, in step a) the hydrogen/ethylene molar
ratio is indicatively from 0.5 to 2, the amount of ethylene monomer being from 5 to 50% by volume, preferably from 5 to 30% by volume, based on the total volume of gas present in the polymerization reactor. The remaining portion of the feeding mixture is represented by inert gases and one or more comonomers, if any. Inert gases which are necessary to dissipate the heat generated by the polymerization reaction are conveniently selected from nitrogen or saturated hydrocarbons, the most preferred being propane.

The operating temperature in the reactor of step a) is selected between 50 and 120°C, preferably between 65 and 100°C, while the operating pressure is between 0.5 and 10 MPa, preferably between 2.0 and 3.5 MPa.

In a preferred embodiment, the ethylene polymer obtained in step a) represents from 30 to 50% by weight of the total ethylene polymer produced in the overall process, i.e. in the first and second serially connected reactors.

The ethylene polymer coming from step a) and the entrained gas are then passed through a solid/gas separation step, in order to prevent the gaseous mixture coming from the first polymerization reactor from entering the reactor of step b) (second gas-phase polymerization reactor). Said gaseous mixture can be recycled back to the first polymerization reactor, while the separated ethylene polymer is fed to the reactor of step b). A suitable point of feeding of the polymer into the second reactor is on the connecting part between the downcomer and the riser, wherein the solid concentration is particularly low, so that the flow conditions are not negatively affected.

The operating temperature in step b) is in the range of 65 to 95°C, and the pressure is in the range of 1.5 to 4.0 MPa. The second gas-phase reactor is aimed to produce a relatively high molecular weight ethylene copolymer by copolymerizing ethylene with one or more comonomers. Furthermore, in order to broaden the molecular weight distribution of the final ethylene polymer, the reactor of step b) can be conveniently operated by establishing different conditions of monomers and hydrogen concentration within the riser and the downcomer.

To this purpose, in step b) the gas mixture entraining the polymer particles and coming from the riser can be partially or totally prevented from entering the downcomer, so to obtain two different gas composition zones. This can be achieved by feeding a gas and/or a liquid mixture into the downcomer through a line placed at a suitable point of the downcomer, preferably in the upper part thereof. Said gas and/or liquid mixture should have a suitable composition, different from that of the gas mixture present in the riser. The flow of said gas
and/or liquid mixture can be regulated so that an upward flow of gas counter-current to the flow of the polymer particles is generated, particularly at the top thereof, acting as a barrier to the gas mixture entrained among the polymer particles coming from the riser. In particular, it is advantageous to feed a mixture with low content of hydrogen in order to produce the higher molecular weight polymer fraction in the downcomer. One or more comonomers can be fed to the downcomer of step b), optionally together with ethylene, propane or other inert gases.

The hydrogen/ethylene molar ratio in the downcomer of step b) is comprised between 0.005 and 0.2, the ethylene concentration being comprised from 1 to 20%, preferably 3-10%, by volume, the comonomer concentration being comprised from 0.2 to 1 % by volume, based on the total volume of gas present in said downcomer. The rest is propane or similar inert gases. Since a very low molar concentration of hydrogen is present in the downcomer, by carrying out the process of the present invention is possible to bond a relatively high amount of comonomer to the high molecular weight polyethylene fraction.

The polymer particles coming from the downcomer are reintroduced in the riser of step b). Since the polymer particles keep reacting and no more comonomer is fed to the riser, the concentration of said comonomer drops to a range of 0.1 to 0.5 % by volume, based on the total volume of gas present in said riser. In practice, the comonomer content is controlled in order to obtain the desired density of the final polyethylene. In the riser of step b) the hydrogen/ethylene molar ratio is in the range of 0.05 to 0.3, the ethylene concentration being comprised between 5 and 15 % by volume based on the total volume of gas present in said riser. The rest is propane or other inert gases.

More details on the above described polymerization process are provided in W09412568.

The following examples are given to illustrate, without limiting, the present invention.

Unless differently stated, the following test methods are used to determine the properties reported in the detailed description and in the examples.

- **Density**
  Determined according to ISO 1183 at 23°C.

- **Molecular Weight Distribution Determination**
  The determination of the molar mass distributions and the means Mn, Mw and Mw/Mn derived therefrom was carried out by high-temperature gel permeation chromatography using a method described in ISO 16014-1, -2, -4, issues of 2003. The specifics according to the mentioned ISO standards are as follows: Solvent 1,2,4-
trichlorobenzene (TCB), temperature of apparatus and solutions 135°C and as concentration detector a PolymerChar (Valencia, Paterna 46980, Spain) IR-4 infrared detector, capable for use with TCB. A WATERS Alliance 2000 equipped with the following pre-column SHODEX UT-G and separation columns SHODEX UT 806 M (3x) and SHODEX UT 807 (Showa Denko Europe GmbH, Konrad-Zuse-Platz 4, 81829 Muenchen, Germany) connected in series was used. The solvent was vacuum destilled under Nitrogen and was stabilized with 0.025% by weight of 2,6-di-tert-butyl-4-methylphenol. The flowrate used was 1 ml/min, the injection was 500µl and polymer concentration was in the range of 0.01% < cone. < 0.05% w/w. The molecular weight calibration was established by using monodisperse polystyrene (PS) standards from Polymer Laboratories (now Agilent Technologies, Herrenberger Str. 130, 71034 Boeblingen, Germany) in the range from 580g/mol up to 11600000g/mol and additionally with Hexadecane. The calibration curve was then adapted to Polyethylene (PE) by means of the Universal Calibration method (Benoit H., Rempp P. and Grubisic Z., & in J. Polymer Sci., Phys. Ed., 5, 753(1967)). The Mark-Houwing parameters used herefore were for PS: kPS= 0.000121 dl/g, aPS=0.706 and for PE kPE= 0.000406 dl/g, aPE=0.725, valid in TCB at 135°C. Data recording, calibration and calculation was carried out using NTGPC_Control_V6.02.03 and NTGPC_V6.4.24 (hs GmbH, Hauptstrasse 36, D-55437 Ober-Hilbersheim, Germany) respectively.

Shear-induced crystallization test

This method is utilized to determine the onset time of shear-induced crystallization (SIC) of the polymer, t_onset,sic. Samples are melt-pressed at 210 °C, 4 min, under 200 bar in a lab press to 1mm thick-plaques. Disc specimens are cut-out with a diameter of 25 mm. The samples are inserted in the plate-plate oscillatory-shear rheometer. A Physica MCR 301 rotational rheometer from AntonPaar is used. The sample is then molten inside the test-geometry at 190 °C for 4 min, cooled down with ~10K/min to the test temperature, T = 125 °C, and annealed for 5 min. Consequently, steady-shear under constant shear rate is applied and the shear viscosity is monitored as a function of time. The experiment is repeated applying each time a different shear-rate ranging from 0.05 to 0.5 s⁻¹. The onset time for SIC, t_onset,sic, is taken at the point where the viscosity has increased at 50% of its steady-state value |η|@125°C. The steady-state value is the average of the steady-shear melt viscosity measured at the specific temperature.
The plot of log(t_{onset,sic}) vs. log shear-rate provides a linear function (of type y=Ax+B) which is extrapolated to a shear rate of 1000 s\(^{-1}\) (process-relevant) to determine the value of t_{onset,sic}@1000.

The SIC Index is then calculated according to the following relation:

\[
\text{SIC Index} = \frac{(t_{onset,sic @ 1000} \times t_{onset,quiescent})}{\text{HLMI}}
\]

The \(t_{onset,quiescent}\) (in sec) is the crystallization onset at temperature of 125 °C under quiescent conditions, i.e. no shear, measured in isothermal mode in a differential-scanning-calorimetry apparatus, DSC, as hereinafter explained.

HLMI is the melt flow index (g/10min) measured at T = 190 °C with 21.6 kg load, according to ISO 1133.

The same protocol is described in the following documents.


- **Isothermal DSC**

The \(t_{onset,quiescent}\), the onset time when no deformation is applied at 125 °C, is determined by the iso-DSC (isothermal Differential Scanning Calorimetry) method. It is measured at 125 °C in a TA Instruments Q2000 DSC apparatus. The determination of the \(t_{onset,quiescent}\) is performed utilizing the commercially available software TA Universal Analysis 2000. The sample preparation and set-up follows the DIN EN ISO 11357-1:2009 and ISO 11357-3:1999.

- **Melt flow index**

Determined according to ISO 1133 at 190°C with the specified load.

- **Long Chain Branching index (LCB)**

The LCB index corresponds to the branching factor \(g'\), measured for a molecular weight of 10^6 g/mol. The branching factor \(g'\), which allows determining long-chain branches at high Mw, was measured by Gel Permeation Chromatography (GPC) coupled with Multi-Angle Laser-Light Scattering (MALLS), as described in the
following. The parameter g' is the ratio of the measured mean square radius of gyration to that of a linear polymer having the same molecular weight. Linear molecules show g’ of 1, while values less than 1 indicate the presence of LCB. Values of g’ as a function of mol. weight, M, were calculated from the equation:
\[
g'(M) = \frac{\langle R_g^2 \rangle_{\text{sample}, M}}{\langle R_g^2 \rangle_{\text{linear ref}, M}}
\]
where \( \langle R_g^2 \rangle_{\text{M}} \) is the root-mean-square radius of gyration for the fraction of mol. weight M.

The radius of gyration for each fraction eluted from the GPC (as described above but with a flow-rate of 0.6 ml/min and a column packed with 30μm particles) is measured by analyzing the light scattering at the different angles. Therefore, from this MALLS setup it is possible to determine mol. weight M and \( \langle R_g^2 \rangle_{\text{sample}, M} \) and to define a g’ at a measured \( M = 10^6 \) g/mol. The \( \langle R_g^2 \rangle_{\text{linear ref}, M} \) is calculated by the established relation between radius-of-gyration and molecular weight for a linear polymer in solution (Zimm and Stockmayer WH 1949)) and confirmed by measuring a linear PE reference with the same apparatus and methodology described.

The same protocol is described in the following documents.


Rubinstein M., Colby RH. (2003), *Polymer Physics*, Oxford University Press

- **Comonomer content**

  The comonomer content is determined by means of IR in accordance with ASTM D 6248 98, using an FT-IR spectrometer Tensor 27 from Bruker, calibrated with a chemometric model for determining ethyl- or butyl- side-chains in PE for butene or hexene as comonomer, respectively.

- **Swell ratio**

  The Swell-ratio of the studied polymers is measured utilizing a capillary rheometer, Gottfert Rheotester2000 and Rheograph25, at T = 190°C, equipped with a commercial 30/2/2/20 die (total length 30 mm, Active length=2 mm, diameter = 2 mm, L/D=2/2 and 20° entrance angle) and an optical device (laser-diod from Gottfert) for measuring the extruded strand thickness. Sample is molten in the capillary barrel at 90°C for 6 min and extruded with a piston velocity corresponding to a resulting shear-rate at the die of 1440 s⁻¹. The extrudate is cut (by an automatic cutting device from Gottfert) at a distance of 150 mm from the die-exit, at the moment the piston reaches a position of
96 mm from the die-inlet. The extrudate diameter is measured with the laser-diod at a distance of 78 mm from the die-exit, as a function of time. The maximum value corresponds to the $D_{\text{extrudate}}$. The swell-ratio is determined from the calculation: 

$$SR = \frac{(D_{\text{extrudate}} - D_{\text{die}})}{D_{\text{die}}} \times 100\%$$

where $D_{\text{die}}$ is the corresponding diameter at the die exit, measured with the laser-diod.

**Shrinkage rate**

This method is applied in order to determine the shrinkage of the final product of polyethylene after melt-extrusion, or in other words the dimensional stability potential of a grade. The method is recommended for homogeneous PE in granulate form. Samples in powder can be measured, only after stabilizing and melt-homogenization (typically in a lab-plasticizer-kneader). However in the latter case, one should expect a significant effect on the results, mainly due to the fact that the sample is more sensitive to degradation and air-bubbles in the extrudate.

The samples in granulate form can be used directly and approximately 20 g of sample are needed for filling the capillary barrel. The utilized capillary rheometer is a Gottfert Rheotester 2000, with a 15 mm diameter barrel and applicable pressure range 0-2000 bar, temperatures 25-400 °C, equipped with a 30/2/2/20 die, with total length 30mm, $L/D=2/2$ and $20^\circ$ entrance angle. The recommended test temperature for polyethylene is 210 °C.

The piston speed is set in order to have the required apparent shear rate at the die exit. The test is performed at shear rates 50 s$^{-1}$, 1000 s$^{-1}$, 1500 s$^{-1}$ and 2500 s$^{-1}$.

The extrudate is marked and pieces of 40 mm length each are punched/stamped, while still in the molten-state, and left to cool at room temperature. At least 3 parts of 40 mm must be marked in this way. A pinch-off metal-tool is utilized to stamp the extrudate after the die-exit in the parts to be measured, with a length of 40 mm (initial length for each part, $L_{\text{o}}$) and typically 10 mm wide.

The whole extrudate is cut and left on a lab table to crystallize and cool down at room temperature for at least 15 min. The parts are cut at the marks and measured in length. The resulting length, $L_i$, in mm is recorded for each part $i$ and averaged for 4 parts.

$$\text{Shrinkage} = \frac{L_i - L_{\text{r}}}{L_{\text{r}}} \times 100\% = \frac{\Delta L_i}{L_{\text{r}}} \times 100\%$$
The procedure is undertaken for each applied shear-rate and the measurement of shrinkage for each shear-rate is repeated at least two times.

Remark: Deviations of the shrinkage along the extrudate length are expected, i.e. due to varying cooling time after exiting the die for each part and sagging (the punched part leaving last the die will be less time exposed to room temperature and "stretched" due to the extrudate weight).

Critical shear rate for sharkskin (sharkskin test)

The sharkskin test is a method to quantify the flow-instabilities and surface defects occurring during extrusion of polymer melts. Specifically, the commercial sharkskin-option with the Rheotester2000 capillary rheometer from Gottfert is used. The sharkskin-option is a slit-die of 30 x 3 x 0.3 mm with three pressure transducers distributed along the die (at die-entry, middle and before die-exit). The pressure is recorded and analyzed (Fourier-transformation) using the available commercial Gottfert WebRheo software.

The polymer is extruded at 190°C applying the following shear-rates in this specific order: 100-150-200-250-300-400-450-500 s⁻¹. The extrudate is consequently visually inspected for surface defects. The critical shear-rate for sharkskin instability is the applied shear-rate for which the sharkskin instability first occurs (high frequency pressure oscillations and visually detectable periodic surface distortions).

The same protocol is described in the following documents.

- Notched Tensile Impact Test
The tensile-impact strength is determined using ISO 8256:2004 with type 1 double notched specimens according to method A. The test specimens (4 x 10 x 80 mm) are cut form a compression molded sheet which has been prepared according ISO 1872-2 requirements (average cooling rate 15 K/min and high pressure during cooling phase). The test specimens are notched on two sides with a 45\(^\circ\) V-notch. Depth is 2 ± 0.1 mm and curvature radius on notch dip is 1.0 ± 0.05 mm. The free length between grips is 30 ± 2 mm. Before measurement, all test specimens are conditioned at a constant temperature of -30°C over a period of from 2 to 3 hours. The procedure for measurements of tensile impact strength including energy correction following method A is described in ISO 8256.

- **Environmental stress crackin2 resistance accordin2 to full notch creep test (FNCT)**

The environmental stress cracking resistance of polymer samples is determined in accordance to international standard ISO 16770 (FNCT) in aqueous surfactant solution. From the polymer sample a compression moulded 10 mm thick sheet has been prepared. The bars with squared cross section (10x10x100 mm) are notched using a razor blade on four sides perpendicularly to the stress direction. A notching device described in M. Fleissner in Kunststoffe 77 (1987), pp. 45 is used for the sharp notch with a depth of 1.6 mm. The load applied is calculated from tensile force divided by the initial ligament area. Ligament area is the remaining area = total cross-section area of specimen minus the notch area. For FNCT specimen: 10x10 mm\(^2\) - 4 times of trapezoid notch area = 46.24 mm\(^2\) (the remaining cross-section for the failure process / crack propagation). The test specimen is loaded with standard condition suggested by the ISO 16770 with constant load of 4 MPa at 80°C in a 2\% (by weight) water solution of non-ionic surfactant ARKOPAL N100. Time until rupture of test specimen is detected.

- **Charpy aFM**

Fracture toughness determination by an internal method on test bars measuring 10 x 10 x 80 mm which had been sawn out of a compression molded sheet with a thickness of 10 mm. Six of these test bars are notched in the center using a razor blade in the notching device mentioned above for FNCT. The notch depth is 1.6 mm. The measurement is carried out substantially in accordance with the Charpy measurement method in accordance with ISO 179-1, with modified test specimens and modified
impact geometry (distance between supports). All test specimens are conditioned to the measurement temperature of 0°C over a period of from 2 to 3 hours. A test specimen is then placed without delay onto the support of a pendulum impact tester in accordance with ISO 179-1. The distance between the supports is 60 mm. The drop of the 2 J hammer is triggered, with the drop angle being set to 160°, the pendulum length to 225 mm and the impact velocity to 2.93 m/s. The fracture toughness value is expressed in kJ/m² and is given by the quotient of the impact energy consumed and the initial cross-sectional area at the notch, aFM. Only values for complete fracture and hinge fracture can be used here as the basis for a common meaning (see suggestion by ISO 179-1).

Examples 1, 2 and Comparative Examples 1 and 2

- Process Setup

In Examples 1-2 the process of the invention was carried out under continuous conditions in a plant comprising two serially connected gas-phase reactors, as shown in Figure 1. Comparative Example 1 is carried out in the same plant under continuous conditions as well.

Example 1

- The solid catalyst component was prepared as described in Example 13 of WO2004106388. The AcOEt/Ti molar ratio was of 8.
- Polymerization

7 g/h of the solid catalyst component prepared as described above were fed, using 5 kg/h of liquid propane, to a precontacting apparatus, in which also a mixture of triisobuthylalumium (TIBA) and diethylaluminum chloride (DEAC) as well tetrahydrofuran (THF) were dosed. The weight ratio between TIBA and DEAC was 7:1. The weight ratio between aluminum alkyl and solid catalyst component was 10:1. The weight ratio between aluminum alkyl and THF was 70. The precontacting step was carried out under stirring at 50°C with a total residence time of 70 minutes.

The catalyst enters the first gas-phase polymerization reactor 1 of Fig. 1 via line 10. In the first reactor ethylene was polymerized using H₂ as molecular weight regulator and in the presence of propane as inert diluent. 35 kg/h of ethylene and 62 g/h of hydrogen were fed to the first reactor via line 9. No comonomer was fed to the first reactor.

The polymerization was carried out at a temperature of 75 °C and at a pressure of 2.5 MPa. The polymer obtained in the first reactor was discontinuously discharged via line 11, separated from the gas into the gas/solid separator 12, and reintroduced into the second gas-phase reactor via line 14.
The polymer produced in the first reactor had a melt index MIE of about 25 g/10 min and a density of 0.966 kg/dm$^3$.

The second reactor was operated under polymerization conditions of about 80 °C, and a pressure of 2.5 MPa. 14 kg/h of ethylene and 0.75 kg/h of 1-hexene were introduced in the downcomer 33 of the second reactor via line 46. 5 kg/h of propane, 28.5 kg/h of ethylene and 3.1 g/h of hydrogen were fed through line 45 into the recycling system.

In order to broaden the molecular weight distribution of the final ethylene polymer, the second reactor was operated by establishing different conditions of monomers and hydrogen concentration within the riser 32 and the downcomer 33. This is achieved by feeding via line 52, 330 kg/h of a liquid stream (liquid barrier) into the upper part of the downcomer 33. Said liquid stream has a composition different from that of the gas mixture present in the riser. Said different concentrations of monomers and hydrogen within the riser, the downcomer of the second reactor and the composition of the liquid barrier are indicated in Table 1. The liquid stream of line 52 comes from the condensation step in the condenser 49, at working conditions of 52°C and 2.5 MPa, wherein a part of the recycle stream is cooled and partially condensed. As shown in the figure, a separating vessel and a pump are placed, in the order, downstream the condenser 49. The final polymer was discontinuously discharged via line 54.

The polymerization process in the second reactor produced relatively high molecular weight polyethylene fractions. In Table 1 the properties of the final product are specified. It can be seen that the melt index of the final product is decreased as compared to the ethylene resin produced in the first reactor, showing the formation of high molecular weight fractions in the second reactor.

The first reactor produced around 44.5 % by weight (split wt %) of the total amount of the final polyethylene resin produced by both first and second reactors. At the same time, the obtained polymer is endowed with a relatively broad molecular weight distribution as witnessed by a ratio MIF/MIP equal to 23.7.

**Example 2**

The process of the invention was carried out with the same setup and the same polymerization catalyst of Example 1. Also the process conditions and consequently the obtained polymer properties of the first reactor were the same.

The second reactor was operated under polymerization conditions of about 80 °C, and a pressure of 2.5 MPa. 14 kg/h of ethylene and 0.86 kg/h of 1-hexene were introduced in the
downcomer of the second reactor via line 46. 5 kg/h of propane, 27.4 kg/h of ethylene and 3.6 g/h of hydrogen were fed through line 45 into the recycling system. In order to broaden again the molecular weight distribution of the final ethylene polymer, the second reactor was operated by establishing different conditions of monomers and hydrogen concentration within the riser 32 and the downcomer 33. Again 330 kg/h of barrier liquid were fed via line 52. The gas compositions of the riser, the downcomer and the liquid barrier are indicated in Table 1. The liquid stream of line 52 comes from the condensation step in the condenser 49, at working conditions of 51°C and 2.5 MPa, wherein a part of the recyle stream is cooled and partially condensed.

The first reactor produced around 45 % by weight (split wt %) of the total amount of the final polyethylene resin produced by both first and second reactors. At the same time, the obtained polymer is endowed with a relatively broad molecular weight distribution as witnessed by a ratio MIF/MIP equal to 22.5.

Comparative Example 1

The polymerization was carried out using the same setup of Examples 1 and 2, but the polymerization catalyst was the same as used in example 6 of WO2005019280. 8 g/h of the solid catalyst component prepared as described above were fed, using 5 kg/h of liquid propane, to a precontacting apparatus, in which triethylaluminum (TEA) as well tetrahydrofuran (THF) were dosed. The weight ratio between aluminum alkyl and solid catalyst component was 5:1. The weight ratio between aluminum alkyl and THF was 44. The precontacting step was carried out under stirring at 50°C with a total residence time of 70 minutes. The catalyst enters the first gas-phase polymerization reactor 1 of Fig. 1 via line 10. In the first reactor ethylene was polymerized using H₂ as molecular weight regulator and in the presence of propane as inert diluent. 40 kg/h of ethylene and 75 g/h of hydrogen were fed to the first reactor via line 9. No comonomer was fed to the first reactor. The polymerization was carried out at a temperature of 80 °C and at a pressure of 2.4 MPa. The polymer obtained in the first reactor was discontinuously discharged via line 11, separated from the gas into the gas/solid separator 12, and reintroduced into the second gas-phase reactor via line 14. The polymer produced in the first reactor had a melt index MIE of about 100 g/10 min and a density of 0.968 kg/dm³.
The second reactor was operated under polymerization conditions of about 80 °C, and a pressure of 2.1 MPa. 12 kg/h of ethylene and 1.5 kg/h of 1-hexene were introduced in the downcomer 33 of the second reactor via line 46. 5 kg/h of propane, 26.5 kg/h of ethylene and 1.2 g/h of hydrogen were fed through line 45 into the recycling system.

In order to broaden the molecular weight distribution of the final ethylene polymer, the second reactor was operated by establishing different conditions of monomers and hydrogen concentration within the riser 32 and the downcomer 33. This is achieved by feeding via line 52, 200 kg/h of a liquid stream (liquid barrier) into the upper part of the downcomer 33. Said liquid stream has a composition different from that of the gas mixture present in the riser. Said different concentrations of monomers and hydrogen within the riser, the downcomer of the second reactor and the composition of the liquid barrier are indicated in Table 1. The liquid stream of line 52 comes from the condensation step in the condenser 49, at working conditions of 53°C and 2.1 MPa, wherein a part of the recycle stream is cooled and partially condensed. As shown in the figure, a separating vessel and a pump are placed, in the order, downstream the condenser 49. The final polymer was discontinuously discharged via line 54.

The polymerization process in the second reactor produced relatively high molecular weight polyethylene fractions. In Table 1 the properties of the final product are specified. It can be seen that the melt index of the final product is decreased as compared to the ethylene resin produced in the first reactor, showing the formation of high molecular weight fractions in the second reactor.

The first reactor produced around 50 % by weight (split wt %) of the total amount of the final polyethylene resin produced by both first and second reactors. At the same time, the obtained polymer is endowed with a relatively broad molecular weight distribution as witnessed by a ratio MIF/MIP equal to 38.8

Comparative Example 2

The polymer of this comparative example is a prior-art polyethylene composition prepared with a Cr-catalyst, in a single gas-phase reactor.
Table 1

<table>
<thead>
<tr>
<th>Table 1</th>
<th>Ex. 1</th>
<th>Ex. 2</th>
<th>Comp. 1</th>
<th>Comp. 2</th>
</tr>
</thead>
<tbody>
<tr>
<td>Operative conditions first reactor</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>H₂/C₂H₄ Molar ratio</td>
<td>1.9</td>
<td>1.9</td>
<td>1.7</td>
<td></td>
</tr>
<tr>
<td>C₂H₄%</td>
<td>12.1</td>
<td>12.4</td>
<td>14</td>
<td></td>
</tr>
<tr>
<td>Split (wt%)</td>
<td>44.5</td>
<td>45</td>
<td>50</td>
<td></td>
</tr>
<tr>
<td>Operative conditions second reactor</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>H₂/C₂H₄ Molar ratio riser</td>
<td>0.157</td>
<td>0.203</td>
<td>0.038</td>
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<tr>
<td>C₂H₄% riser</td>
<td>11.3</td>
<td>11.4</td>
<td>15</td>
<td></td>
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<tr>
<td>C₆H₁₂ riser</td>
<td>0.56</td>
<td>0.65</td>
<td>1.2</td>
<td></td>
</tr>
<tr>
<td>H₂/C₂H₄ Molar ratio downcomer</td>
<td>0.069</td>
<td>0.086</td>
<td>0.04</td>
<td></td>
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<tr>
<td>C₂H₄% downcomer</td>
<td>2.6</td>
<td>2.8</td>
<td>5.4</td>
<td></td>
</tr>
<tr>
<td>C₆H₁₂ downcomer</td>
<td>0.60</td>
<td>0.71</td>
<td>2.2</td>
<td></td>
</tr>
<tr>
<td>H₂/C₂H₄ Molar ratio barrier</td>
<td>0.013</td>
<td>0.015</td>
<td>0.01</td>
<td></td>
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<tr>
<td>C₂H₄% barrier</td>
<td>6.8</td>
<td>7.1</td>
<td>6.5</td>
<td></td>
</tr>
<tr>
<td>C₆H₁₂ barrier</td>
<td>0.93</td>
<td>1.17</td>
<td>2.7</td>
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</tbody>
</table>

Final Polymer properties

<table>
<thead>
<tr>
<th>Final Polymer properties</th>
<th>Ex. 1</th>
<th>Ex. 2</th>
<th>Comp. 1</th>
<th>Comp. 2</th>
</tr>
</thead>
<tbody>
<tr>
<td>MIP [5 kg] (g/10 min.)</td>
<td>0.2</td>
<td>0.29</td>
<td>0.21</td>
<td>0.31</td>
</tr>
<tr>
<td>MIF [21.6 kg] (g/10 min.)</td>
<td>4.8</td>
<td>6.5</td>
<td>8.15</td>
<td>6.25</td>
</tr>
<tr>
<td>MIF/MIP</td>
<td>23.7</td>
<td>22.5</td>
<td>38.8</td>
<td>20.16</td>
</tr>
<tr>
<td>Density (kg/dm³)</td>
<td>0.9509</td>
<td>0.9496</td>
<td>0.9487</td>
<td>0.947</td>
</tr>
<tr>
<td>Mw [g/mol]</td>
<td>3.5E+5</td>
<td>3.8E+5</td>
<td>3.6E+5</td>
<td>3.9E+5</td>
</tr>
<tr>
<td>Mz [g/mol]</td>
<td>2.0E+6</td>
<td>8.3E+6</td>
<td>5.0E+6</td>
<td>3.5E+6</td>
</tr>
<tr>
<td>Mw/Mn</td>
<td>25</td>
<td>27</td>
<td>52</td>
<td>25</td>
</tr>
<tr>
<td>LCB</td>
<td>0.89</td>
<td>0.84</td>
<td>0.69</td>
<td>0.99</td>
</tr>
<tr>
<td>Commonomer content IR [% by weight]</td>
<td>0.7% ±0.1 (C₆H₁₂)</td>
<td>0.7% ±0.1 (C₆H₁₂)</td>
<td>1.6 (C₆H₁₂)</td>
<td>1.6 (C₆H₁₂)</td>
</tr>
<tr>
<td>SIC index</td>
<td>3.8</td>
<td>3.3</td>
<td>1.9</td>
<td>6.1</td>
</tr>
<tr>
<td>Swell ratio (%)</td>
<td>179</td>
<td>171</td>
<td>120</td>
<td>210</td>
</tr>
<tr>
<td>Shrinkage@1500 s⁻¹, T = 190°C [%]</td>
<td>15</td>
<td>12</td>
<td>-</td>
<td>23</td>
</tr>
<tr>
<td>Critical shear-rate for sharkskin, T = 190°C, [1/s]</td>
<td>300</td>
<td>300</td>
<td>-</td>
<td>200</td>
</tr>
<tr>
<td>Notched-Tensile Impact test, T = -30°C [kJ/m²]</td>
<td>164</td>
<td>155</td>
<td>93</td>
<td>145</td>
</tr>
<tr>
<td>FNCT 4 MPa/80°C (hours)*</td>
<td>329</td>
<td>20</td>
<td>&gt;2000</td>
<td>4</td>
</tr>
<tr>
<td>Charpy aFM, T = 0°C [kJ/m²]</td>
<td>-</td>
<td>-</td>
<td>8.9</td>
<td></td>
</tr>
</tbody>
</table>

Notes: C₂H₄ = ethylene; C₆H₁₂ = hexene; *aqueous solution of 2% Arkopal N100
CLAIMS

1. Polyethylene composition having the following features:
   1) density from 0.945 to less than 0.952 g/cm³, preferably from 0.948 to 0.951 g/cm³, determined according to ISO 1183 at 23°C;
   2) ratio MIF/MIP from 15 to 30, in particular from 17 to 29, where MIF is the melt flow index at 190°C with a load of 21.60 kg, and MIP is the melt flow index at 190°C with a load of 5 kg, both determined according to ISO 1133;
   3) SIC Index from 2.5 to 5.5, preferably from 2.5 to 4.5, more preferably from 3.2 to 3.9;

   wherein the SIC Index is the Shear-Induced Crystallization Index, determined according to the following relation:

   \[
   \text{SIC Index} = \left( t_{\text{onset,sic}@1000} \times t_{\text{onset,quiescent}} \right) / (\text{HLMI})
   \]

   where \( t_{\text{onset,sic}@1000} \) is measured in seconds and is the time required for crystallization onset under shear rate of 1000 s\(^{-1}\), the \( t_{\text{onset,quiescent}} \) is measured in seconds and is the crystallization onset time at temperature of 125°C under no shear, determined in isothermal mode by differential scanning calorimetry; HLMI is the melt flow index determined at 190°C with a load of 21.6 kg, according to ISO 1133.

2. The polyethylene composition of claim 1, consisting of or comprising one or more ethylene copolymers.

3. The polyethylene composition of claim 2, having a comonomer content equal to or less than 1% by weight.

4. The polyethylene composition of claims 2 and 3, wherein the comonomer or comonomers present in the ethylene copolymers are selected from olefins having formula \( \text{CH}_2=\text{CHR} \) wherein \( R \) is an alkyl radical, linear or branched, having from 1 to 10 carbon atoms.

5. The polyethylene composition of claims 1 and 2, obtainable by using a Ziegler-Natta polymerization catalyst.

6. The polyethylene composition of claim 1, having at least one of the following additional features:
   - \( M_w \) equal to or greater than 250000 g/mol, in particular equal to or greater than 280000 g/mol;
   - \( M_w/M_n \) from 20 to 30;
- Long Chain Branching index equal to or greater than 0.70, in particular equal to or greater than 0.72;
- MIP: 0.05 - 0.5 g/10 min.;
- MIF: 1 - 15 g/10 min.

7. The polyethylene composition of claim 1, comprising:
   A) 30 - 50 % by weight of an ethylene homopolymer or copolymer with density equal to or greater than 0.960 g/cm³ and melt flow index MIE at 190°C with a load of 2.16 kg, according to ISO 1133, of 10 - 35 g/10 min.;
   B) 50 - 70 % by weight of an ethylene copolymer having a MIE value lower than the MIE value of A), preferably lower than 0.5 g/10 min.

8. Manufactured articles comprising the polyethylene composition of claim 1.

9. Manufactured articles according to claim 8, in form of blow-moulded articles.

10. Process for preparing the polyethylene composition of claim 1, wherein all the polymerization steps are carried out in the presence of a Ziegler-Natta polymerization catalyst supported on MgCl₂.

11. The process of claim 10, comprising the following steps, in any mutual order:
   a) polymerizing ethylene, optionally together with one or more comonomers, in a gas-phase reactor in the presence of hydrogen;
   b) copolymerizing ethylene with one or more comonomers in another gas-phase reactor in the presence of an amount of hydrogen less than step a);

where in at least one of said gas-phase reactors the growing polymer particles flow upward through a first polymerization zone under fast fluidization or transport conditions, leave said riser and enter a second polymerization zone through which they flow downward under the action of gravity, leave said second polymerization zone and are reintroduced into the first polymerization zone, thus establishing a circulation of polymer between said two polymerization zones.
INTERNATIONAL SEARCH REPORT

A. CLASSIFICATION OF SUBJECT MATTER

 According to International Patent Classification (IPC) and to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

C08L B29C

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

<table>
<thead>
<tr>
<th>Category*</th>
<th>Citation of document, with indication, where appropriate, of the relevant passages</th>
<th>Relevant to claim No.</th>
</tr>
</thead>
</table>

* Special categories of cited documents:

- "A" document defining the general state of the art which is not considered to be of particular relevance
- "E" earlier application or patent but published on or after the international filing date
- "L" document which may throw doubts on priority claim(s) one of which is cited to establish the publication date of another citation or other special reason (as specified)
- "O" document referring to an oral disclosure, use, exhibition or other means
- "P" document published prior to the international filing date but later than the priority date claimed

"I" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to be the same inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to be the same inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"A" document member of the same patent family

Date of the actual completion of the international search: 6 December 2013

Date of mailing of the international search report: 18/12/2013

Name and mailing address of the ISA:

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Authorized officer

Knutzen-Mi es, Karen

Form PCT/ISA/210 (second sheet) (April 2005)
<table>
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<tr>
<th>Patent document cited in search report</th>
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