

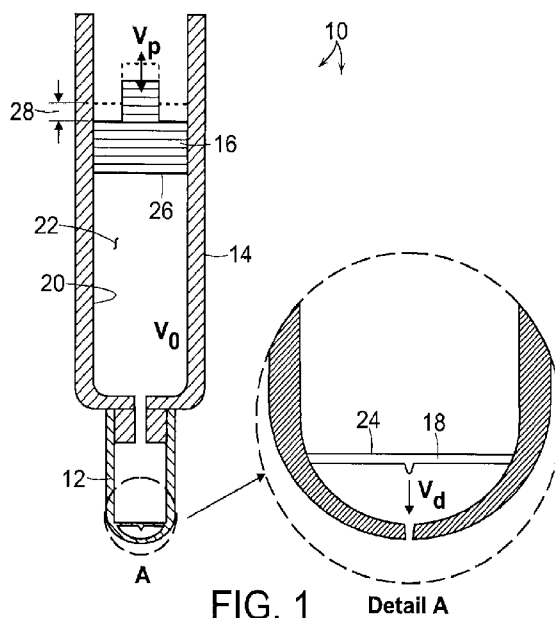
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(54) Title: NANOLITER PIPETTING DEVICE

(57) **Abstract:** Nanoliter pipette assembly. The assembly includes a housing containing a working fluid in a working fluid chamber therein and includes a moveable piston within the housing, the piston moveable by a linear actuation mechanism for contact with the working fluid. A tip portion is provided that includes a diaphragm deformable to engage an inner portion of the tip. It is preferred that the diaphragm have a projecting three-dimensional structure for direct contact with a liquid.

Published:

— *with international search report (Art. 21(3))*

Nanoliter Pipetting Device

This application claims priority to U.S. Application Serial Number 15/590,131 filed May 9, 2017 and U.S. Provisional Application Serial Number 62/334,709 filed on May 11, 5 2016, the contents of which are incorporated herein by reference in their entirety.

Background of the Invention

10 This invention relates to a pipetting device for drawing and dispensing small liquid volumes from approximately 1-1000 nanoliters.

Handheld pipettes are a ubiquitous tool; they are found across industry and academia in essentially all wet laboratories, and are essential to accurate laboratory work in the fields of chemistry, biology, and medicine. They are used for manipulating small volumes of fluid, 15 and still make up the largest percentage of the US liquid handling market. Hand held pipettes offer the convenience, flexibility, ease of use, and low cost that more complex liquid handling solutions cannot offer.

20 Handheld pipettes operate under very simple physical principles. They consist of several main components: an internal piston, a spring loaded plunger, a disposable tip, an adjustable stop, and a fixed stop. The pipette is held in one hand by the user, and a volume is selected by moving the adjustable stop. The user then presses the plunger down to the adjustable stop. This causes the piston to displace a volume, V_p . The pipette is then lowered 25 into the fluid and the plunger is slowly released. As the spring forces the piston to move back to its initial position, the pressure in the tip lowers and a volume, V_p , of fluid is drawn into the tip. The fluid can then be dispensed into another container by depressing the plunger to the second stop.

30 As previously mentioned, their ease of use and low cost has led to their widespread adoption; however, there are several important limitations of current handheld pipettes. Pipetting volumes smaller than 1000 nanoliters is challenging and typically imprecise (accuracy ~25%). Volumes smaller than 100 nanoliters is currently inaccessible. Under the current pipette operating principles, in order to achieve such small volumes, extremely small

piston diameters must be used, which are in most cases not manufacturable. Because the piston diameter is fixed, the range of volumes a given pipette can dispense is limited by the piston range. As a result, labs will often have to purchase a variety of pipettes to dispense volumes in every range they may need. Pipette volume resolution is determined by the positional resolution of the hard stop and the diameter of the piston. When purchasing a pipette there is often a tradeoff between resolution and range.

Therefore, current pipetting technology is not suitable for manipulating smaller volumes. Reducing the volumes that a pipette can aspirate and dispense will allow labs to conserve resources, lower their costs, and perform more experiments.

Summary of the Invention

The nanoliter pipette assembly according to the invention includes a housing containing a working fluid in a working fluid chamber therein. A piston is provided that is moveable within the housing by a linear actuation mechanism for contact with the working fluid. A tip portion is provided having a diaphragm therein, the diaphragm deformable to engage an inner portion of the tip. The diaphragm and tip portion each include an orifice for aspirating and dispensing a selected fluid wherein the linear actuating mechanism, diaphragm properties and housing properties are selected so that the piston displaces a first volumetric amount of the working fluid on one side of the diaphragm and in which the diaphragm displaces a second volumetric amount of the selected fluid on the opposite side of the diaphragm via direct contact with the selected fluid. The second volumetric amount is less than the first volumetric amount providing a deamplification ratio. In a preferred embodiment, the diaphragm orifice includes a projection that mates with an orifice in the tip. The diaphragm, projection and internal surface of the tip portion are wetted by the selected fluid. A suitable working fluid is a compressible gas such as air.

In another preferred embodiment, the adjustable diaphragm parameters include diaphragm radius, diaphragm thickness, diaphragm shear modulus and diaphragm pre-stretch. In yet another preferred embodiment, the linear actuation mechanism includes a series of cams to provide repeatability and adjustability of the selected fluid volumes.

It is also preferred that the liquid to be drawn completely wets an exterior side of the diaphragm and an inner surface of the tip in such a manner that when the liquid is drawn there is no air, and thereby no liquid-air interface inside the pipette tip. It is also preferred that the projection on the diaphragm (nipple) protrudes through the orifice in the tip to provide direct contact with the liquid, so as to prevent the volume of drawn liquid from being influenced by capillary pressure that is a primary limitation to pipetting smaller volumes with current handheld pipettes. It is also preferred that the outer surface of the pipette tip be non-wetting so that liquid does not stick to it. It is further preferred that the orifice be small, on the order or tens of microns in lateral dimension to minimize volume loss due to evaporation for volatile liquids.

It is also preferred that the diaphragm is elastic and that the working fluid is a compressible gas such as air. The invention disclosed herein allows the volume displacement of the diaphragm to be a scaled amount of the piston's displacement based on the diaphragm's stiffness and air's compressibility.

Brief Description of the Drawing

Fig. 1 is a cross-sectional view, along with detail, of an embodiment of the invention disclosed herein.

Figs. 2a, 2b, 2c and 2d are cross-sectional views of device tips showing a sequence of diaphragm positions.

Fig. 3 is a cross-sectional view of a tip portion and diaphragm according to an embodiment of the invention.

Fig. 4 is an exterior, schematic view of a nanoliter pipette tip according to an embodiment of the invention.

Fig. 5 is a cross-sectional view of another nanoliter pipette tip suitable for practice of the invention.

Fig. 6 is a cutaway, exploded, view of the device showing details of a tip suitable for use in the invention.

Fig. 7 is a cross-sectional view of the tip portion of another embodiment of the invention.

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Figs. 8, 9 and 10 are graphs of a calculated relationship of relevant volumes in embodiments of the invention.

Fig. 11 illustrates a pressure relief system used to calibrate the pipette of the invention before use or adjustment.

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Fig. 12 is a cross-sectional view showing the specifics of a piston cam mechanism according to a preferred embodiment of the invention.

Figs. 13a – 13h are perspective views illustrating an eight-step breakdown of the cam mechanism disclosed herein.

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Description of the Preferred Embodiment

As will become apparent from the following disclosure, a pipette tip, including a diaphragm, in combination with a novel piston linear actuation mechanism, may be configured as part of a high-resolution pipette assembly, that can dispense volumes of fluid as small as one nanoliter. The components function via a volume deamplification concept in which a pipette piston displaces a volumetric amount of a working fluid on one side of the diaphragm placed in the tip and in which the diaphragm displaces a smaller volumetric amount of fluid at an opposite side of the diaphragm via direct contact with the fluid. This displacement reduction from one side of the diaphragm to the other may be characterized by a deamplification ratio that can span multiple orders of magnitude. One or more portions of a fluid chamber that encloses the working fluid may undergo elastic deformation to facilitate the deamplification. Additionally or alternatively, the working fluid may be compressible to contribute to the deamplification. The deamplification ratio and resolution may also be adjustable.

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Referring to Fig 1, a schematic cross-sectional view of the nanoliter pipette is shown. The pipette assembly **10** consists of a tip **12**, a housing, **14**, a piston and accompanying mechanism **16**, and a diaphragm **18** constrained in the tip. The piston and diaphragm define an adjustable fluid chamber, **20**. The working fluid **22** is in contact with the piston **16** and the chamber side **24** of the diaphragm. The piston **16** is movable and displaces the working fluid **22** within the chamber **20**. The illustrated embodiment is not to scale. The tip **12** consists of several separate pieces that are used to form a fluid tight seal with the diaphragm **18** and the housing **14**, using sealing methods known to those skilled in the art.

In operation, still referring to Fig 1, the piston **16** moves to displace a volumetric amount of working fluid **22** within the fluid chamber **20**. The volume displaced, V_p , by the piston **16** is equal to the product of the surface area of surface **26** and the distance **28** the piston has moved. The piston **16** is shown in this displaced position after being moved from its initial position shown in dashed lines. The volume displacement, V_p , causes a corresponding volume displacement, V_d , by the diaphragm **18**.

Due to the small volumes the tip **12** will be handling, a novel piston and accompanying mechanism **16** has been designed. Details of how the piston and piston mechanism **16** deflect the diaphragm **18** to aspirate and dispense fluid can be seen in Figs. 2a-2d, cross-sectional schematics of the pipette tip. In step 1 in Fig. 2a, **30**, the operator sets the stop to determine volume to dispense, V_d . In step 2 in Fig. 2b, **32**, the operator depresses the piston **16** to the bottom of its stroke, deflecting the diaphragm **18** to its maximum position. At this point, a three dimensional feature **34** contacts the fluid. Because the pipette is dispensing fluids as small as 1 nL, evaporation becomes a concern. If proper design considerations are not made, a large percentage of aspirated fluid can evaporate in the time it takes to aspirate the fluid and dispense it in the appropriate container. An orifice **36** on the pipette tip **12** was designed to be extremely small, limiting evaporation. However, as this orifice **36** becomes smaller and smaller, the more difficult it becomes to aspirate and dispense fluid accurately due to an increase in capillary pressure. Therefore, the fluid facing surface of the diaphragm **18** is designed with a three dimensional feature **34**. During step 2 (Fig. 2b), **32** of the pipetting process, this feature comes in contact with the working fluid. The diaphragm **18**, the three dimensional feature **34** and the interior cavity of the tip **12** are configured to be wetting such that retraction of the diaphragm to a controlled position allows fluid to fill the cavity

defined by the deflection of the diaphragm **18** and the retraction of the piston mechanism **16**. This is the motivation behind the design of the piston mechanism **16**. The diaphragm **18** must be deflected to its maximum position **32** first in order to come in contact with the fluid. Then in step 3, Fig. 2c, **38**, the piston **16** is retracted to the position shown in order to aspirate fluid volume, V_d . In Step 4, Fig. 2d, **40**, the diaphragm **18** is once again deflected to its maximum position to dispense all the fluid.

The working fluid **20** may be a compressible fluid such as air or some other gas. The compressible working fluid **22** compresses when the piston **16** moves against the working fluid **22** to displace it, resulting in an increased fluid chamber pressure. Here, the working fluid acts to temporarily store a portion of the work energy transferred thereto by the piston. In one embodiment, the diaphragm **18** undergoes elastic deformation and the working fluid is compressed when the piston **16** moves against the working fluid **22** to displace it. Thus, diaphragm elasticity and working fluid compressibility may be used in various combinations to arrive at the desired deamplification ratio.

A set of three nanoliter pipette tips **12** has been designed to exhibit the configuration stated above. Each tip **12** possesses different dimensions and initial conditions. Fig. 3 illustrates which dimensions can be varied. The diaphragm radius, **42**, the diaphragm thickness, **44**, the diaphragm shear modulus, **46**, the diaphragm pre-stretch, **48**, and the size of the fluid chamber **20**. Changing the dimensions allows the pipette assembly **10** to behave differently based on which tip **12** is selected by the operator. Different tips can cause the pipette **10** to have different volume ranges and resolutions.

Figs. 4-7 illustrate our initial embodiment of the nanoliter pipette tip **12**. This tip can dispense volumes ranging from 1-10 nl. Fig 4 is a front view of the tip **12**. The tip **12** will screw onto the housing **14** and form a fluid tight seal. Fig 5 is a cross section of the 10 nl tip **12**. The tip **12** is composed of several key components, all critical to the assembly and functionality of the tip. The tip **12** is composed of two main pieces, tip bottom **50** and tip top **52**. An exploded view of tip bottom **50** and its mating components can be seen in Fig 6. The diaphragm **18** is secured to the membrane clamp **54** via adhesive **56**. The adhesive makes assembly easier and holds the diaphragm pre-stretch **48**. A detailed view of tip bottom **50**, membrane clamp **54**, the diaphragm **18**, the adhesive **56**, and the three dimensional

diaphragm feature 34 can be seen in Fig 7. In one embodiment, the raised feature 34 on the diaphragm is a glass microsphere that will be secured to the diaphragm via an adhesive, or can be formed as a monolithic feature of the diaphragm such as by a molding technique. Fig 5 also features many other components in an example embodiment. A machined nut 58 secures the assembly and provides pre-load by compressing a spring 60. The preload allows for fine tuning of the compressive forces on the membrane 18. A PET washer 62 acts as a thrust bearing to prevent any torsional stress from getting to the membrane 18 via the nut 58. A gasket 64 acts to seal tip top 52 and tip bottom 50.

Figure 12 delineates the specifics of the piston cam mechanism 92-98 and the chamber 78, which corresponds with the housing 14 in Fig. 1. The chamber 78 holds a sealed working volume, V_o , that comes in direct contact with the diaphragm 18 in the tip 12. V_o can be adjusted to the correct volume via a side screw 76. The side screw 76 is preloaded via the side spring 74 to ensure that the screw does not move during operation. Additionally, a side o-ring 66 provides a fluid seal to ensure that there is no leakage in the system. The chamber 78 is connected to the tip 12 and the exterior body 86 via threads, M6 and $\frac{7}{8}$ "-14 respectively. Similarly to the side screw 76, the tip 12 is sealed via a gasket 64 and the exterior body is sealed via the top o-ring 80. Above the chamber is the dynamic portion of the mechanism as parts 82, 84, 88, 90, 92, 94 and 104 are all in motion, both vertical and rotational. The piston 82 fits into the chamber 78 and when its motion is directly coupled to that of V_p . It is also press fit into the interior cap 88.

Around the piston 82, is the piston spring 84. The piston spring 84, compresses during operation and provides an upward bias to the cams, 92 & 94, via the interior cap 88 and lead screw 104. The lead screw 104 is fitted into the top of interior cap 88 and is mated with the threaded bushing 90. The threaded bushing 90 is press fit into the variable cam 92. The motion and dynamics of four cams mechanisms, 92-98 are described below. The exterior cams 96 & 98 are held in place via a shoulder in the exterior body 86 and a top spacer 100. The top spacer is bolted into the exterior body 86 via four 4-40 screws of length .3125" 102. The thumb push 110 is coupled to the thumb connector 106 via a bearing 108 that is press fit onto both pieces.

In the exterior body **86** rests the cam mechanisms **92-98**, which along with the actual piston **82** correspond to **16** in Fig. 1. These series of cams provide the repeatability and adjustability required to handle the small volumes of fluid. The cam mechanisms are made up of the exterior cam top **98**, exterior cam bottom **96**, interior cam **94** and the variable cam **92**. The exterior cams **96, 98** fit together with mirrored offsets and rest on a shoulder in the exterior body **86**. These two cams do not move during the pipetting process. During operation the interior cam **94** and variable cam **92** move up and down and rotate about the vertical axis. Before operation, the two cams can move independent of each other through the use of the lead screw **104** and the threaded bushing **90**. Rotation of the lead screw, which is done manually by turning the thumb connector **106**, moves the variable cam **92** up and down relative to the interior cam **94**.

Figs. 13a-13-h show an 8-step breakdown of the cam mechanism in operation. The interior and variable cams **92, 94** start in position 1) continue as follows: 1) the thumb push **110** is depressed causing the interior and variable cams **92, 94** to move down until the top face of the exterior cam **96** comes in to contact with the face of the interior cam **94** 2) the interior and variable cams **92, 94** continue to move down and rotate 22.5 degrees due to the angular face mate to arrive at position C, 3) the thumb push **110** is released and the bottom face of the exterior cam **96** comes in to contact with the face of the variable cam **92**, 4) the interior and variable cams **92, 94** continue to move up and rotate another 22.5 degrees to arrive at position E, 5) the thumb push **110** is again depressed and the interior and variable cams **92, 94** move down until the top face of the exterior cam **96** comes in to contact with the face of the interior cam **94**, 6) the interior and variable cams **92, 94** continue to move down and rotate 22.5 degrees due to the angular face mate to arrive at position G, 7) the thumb push **110** is released and the bottom face of the exterior cam **96** comes in to contact with the face of the interior cam **92**, 8) the interior and variable cams **92, 94** continue to move up and rotate another 22.5 degrees to arrive back at position 1). Note: all rotation is counterclockwise.

Figure 11 shows the pressure relief system that is used to calibrate the pipette before every use or adjustment. It is necessary for the pipette to have this capability so that the desired deamplification ratio can be achieved. The relief slider **68** can be easily pulled down to expose a relief cavity that connects directly to the inside of the sealed working fluid **20** in the chamber **78**. This relief cavity is sealed by an o-ring that is not pictured in the figures.

The relief slider **68** is held in place by a thin shim **70** that is mounted to the chamber **78** via two 4-40 screws with a length of .25" **72**.

The volume deamplification principles described above and the design of a pipette tip **12** and piston mechanism **16** in accordance with the present teachings is guided by a mathematical model detailed in our earlier patent application US20130283884 A1. Using this model, pipette tip values can be selected to achieve desired pipetting performance.

Example

Three different pipette tips have been designed and manufactured. All three tips are compatible with the same chamber **78** and piston/cam mechanism **82, 92-98**. The first tip has the ability to dispense fluids in the range of 1-10 nl. A graph of the calculated relationship V_d vs V_p can be seen in Fig. 8. It has a volume deamplification ratio $V_d/V_p = 49600$. The second tip was designed to dispense volumes within the range of 10-100 nl. Its graph can be seen in Fig. 9. It has a volume deamplification ratio $V_d/V_p = 4960$. Finally, Fig. 10 presents the final pipette tip which can dispense volumes of 100-1000 nl. It possesses a volume deamplification ratio of $V_d/V_p = 496$. As can be seen in the Figs. 8-10, the function $V_d(V_p)$ is most accurately modeled as a third order polynomial, but with careful selection of pipette tip parameters, the diaphragm radius **42**, the diaphragm thickness **44**, the diaphragm shear modulus **46**, the diaphragm pre-stretch **48**, and the initial volume of the fluid chamber **20**, $V_d(V_p)$ acts approximately linear over the entire stroke of the pipette. Linearity of this function is crucial to making the pipette intuitive to use, simplifying mechanical design, and thus lower costs.

It can be appreciated that, based on the principles above and using suitable fabrication methods known to those skilled in the art, the design may be scaled to manipulate volumes smaller or larger than ~1-1000 nl. The pipette device could also be used to manipulate materials other than liquids, or liquids containing soft solids, for example biological cells. Other considerations may include electrical contact to the diaphragm and/or tip, such that electrical signals can be applied when the tip is in contact with solids and/or liquids. The design may also be employed in other configurations, such that multiple tips are arrayed in close proximity, driven by one or more piston mechanisms, which may be manual or motorized. In one example, an array of diaphragms, each within its own tip, is in contact

with a single piston via a common volume of working fluid. The characteristics of the diaphragms within the array may be chosen to be the same, or to vary in a prescribed manner.

Additional information about the present invention may be found in “Universal
5 Handheld Micropipette” Review of Scientific Instruments 87,115112(2016) and in United
States published patent application US2013/0283884. The contents of both of these
references are incorporated herein by reference in their entirety.

It is recognized that modifications and variations of the present invention will be
10 apparent to those of ordinary skill in the art and it is intended that all such modifications and
variations be included within the scope of the appended claims.

What is claimed is:

What is claimed is:

- 1 1. Nanoliter pipette assembly comprising:
2
3 a housing containing a working fluid in a working fluid chamber therein;
4
5 a piston moveable within the housing by a linear actuation mechanism for
6 contact with the working fluid; and
7
8 a tip portion including a diaphragm therein, the diaphragm deformable to
9 engage an inner portion of the tip, wherein the diaphragm and tip portion each include
10 an orifice for aspirating and dispensing a selected fluid, wherein the linear actuating
11 mechanism, diaphragm properties and housing properties are selected so that the
12 piston displaces a first volume amount of the working fluid on one side of the
13 diaphragm and in which the diaphragm displaces a second volumetric amount of the
14 selected fluid on the opposite side of the diaphragm via direct contact with the
15 selected fluid, wherein the second volumetric amount is less than the first volumetric
16 amount providing a deamplification ratio.

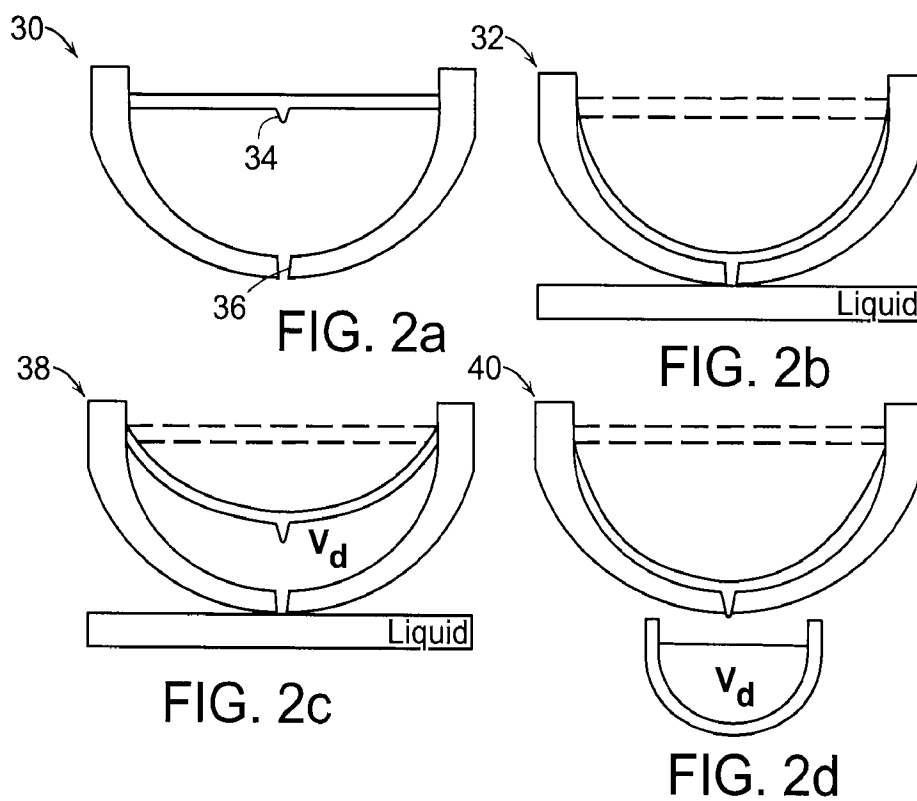
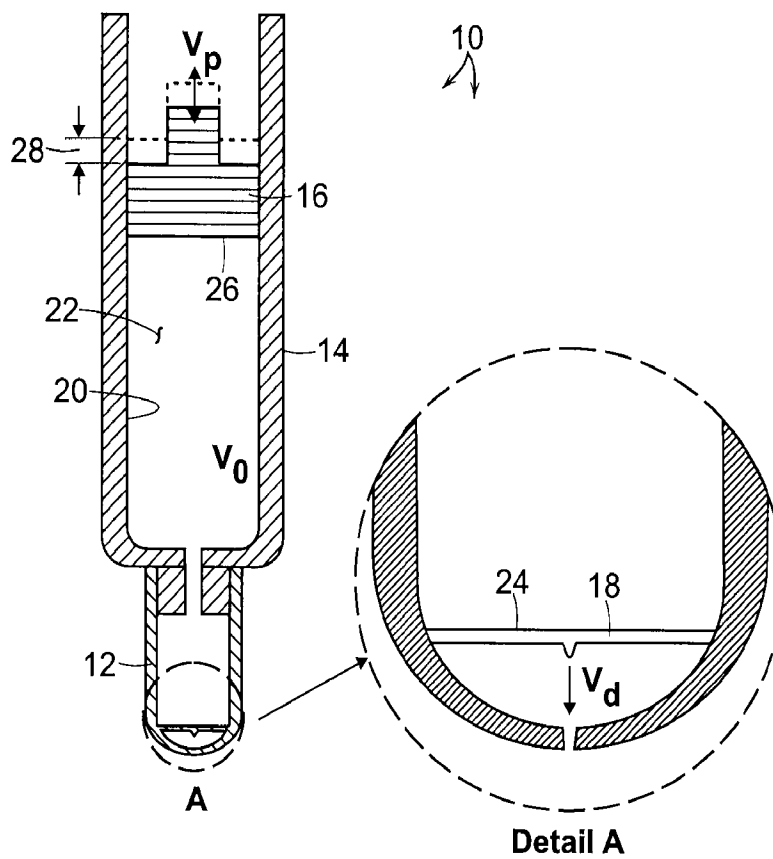
- 1 2. The nanoliter pipette assembly of claim 1 wherein the diaphragm orifice forms a
2 projection that mates with a depression in the tip.

- 1 3. The nanoliter pipette assembly of claim 1 wherein the diaphragm, projection and
2 interior of the tip portion are wetted by the selected fluid.

- 1 4. The nanoliter pipette assembly of claim 1 wherein the working fluid is a compressible
2 gas.

- 1 5. The nanoliter pipette assembly of claim 1 wherein the selected diaphragm properties
2 include diaphragm radius, diaphragm thickness, diaphragm elasticity and diaphragm
3 pre-stretch/load.
- 1 6. The nanoliter pipette assembly of claim 1 wherein the linear actuation mechanism
2 includes a series of cams to provide repeatability and adjustability of selected fluid
3 volumes.
- 1 7. The nanoliter pipette assembly of claim 1 wherein the linear actuation mechanism
2 includes a stop to set a desired dispense volume of the selected fluid; depresses the
3 piston to the bottom of its stroke bringing a projection on the diaphragm into contact
4 with the selected fluid; retracting the piston to aspirate the desired dispense volume
5 and deflecting the diaphragm again to its maximum position to dispense the fluid.
- 1 8. The nanoliter pipette assembly of claim 6 further including a thumb push button
2 coupled to the series of cams providing an eight step operation of the pipette assembly
3 to aspirate and then dispense the selected fluid providing an adjustable-range click-
4 pen-type mechanism.

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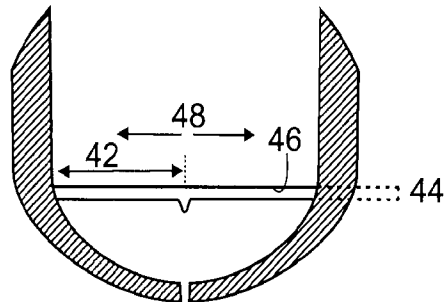


FIG. 3

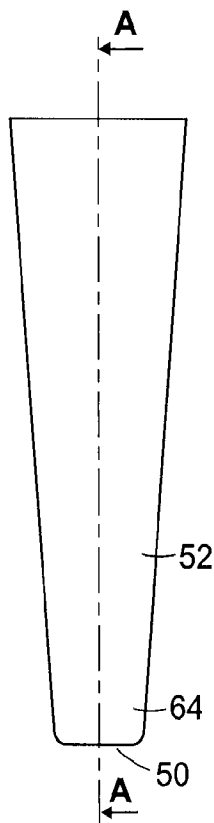
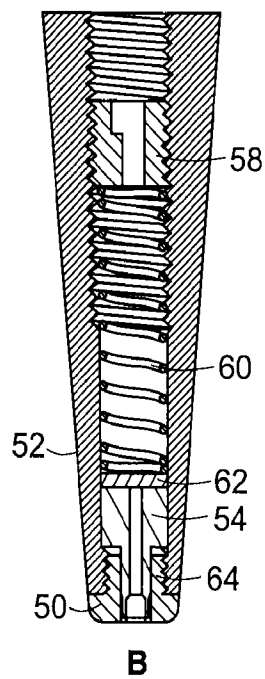


FIG. 4



Section AA

FIG. 5

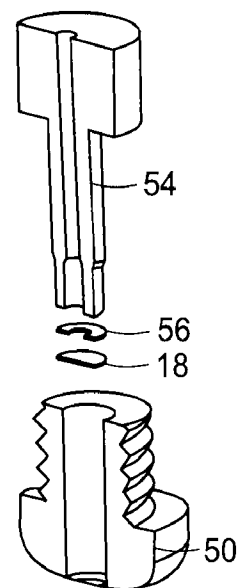


FIG. 6

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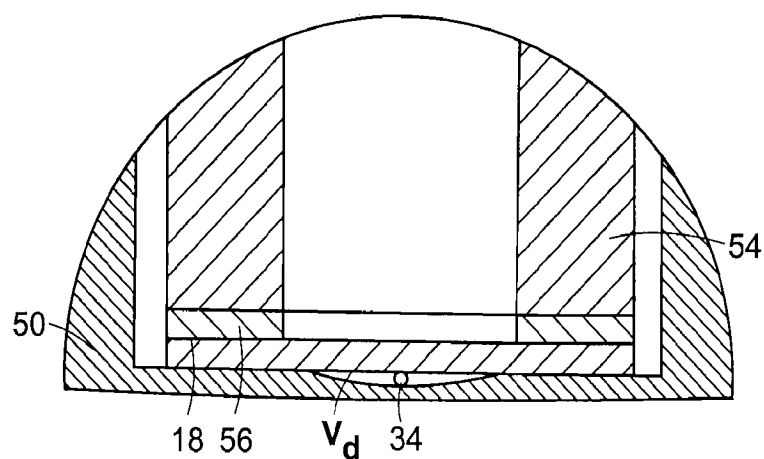


FIG. 7

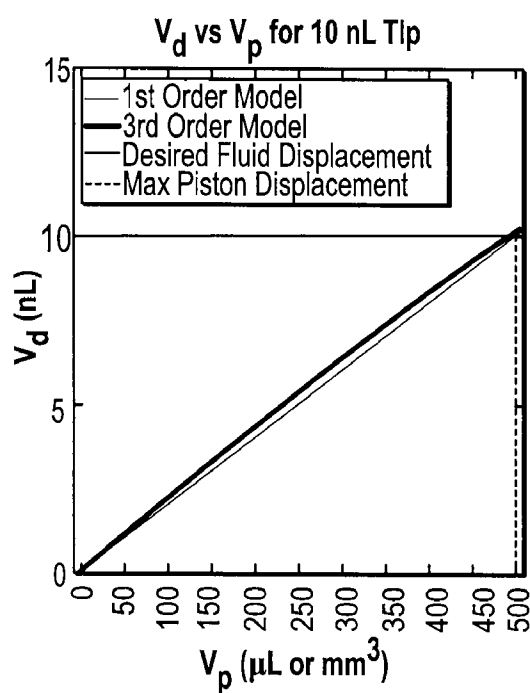


FIG. 8

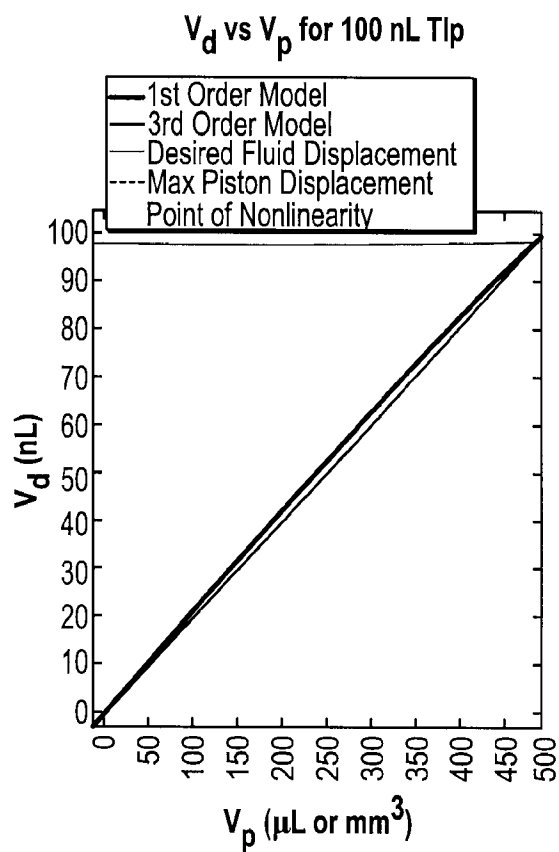


FIG. 9

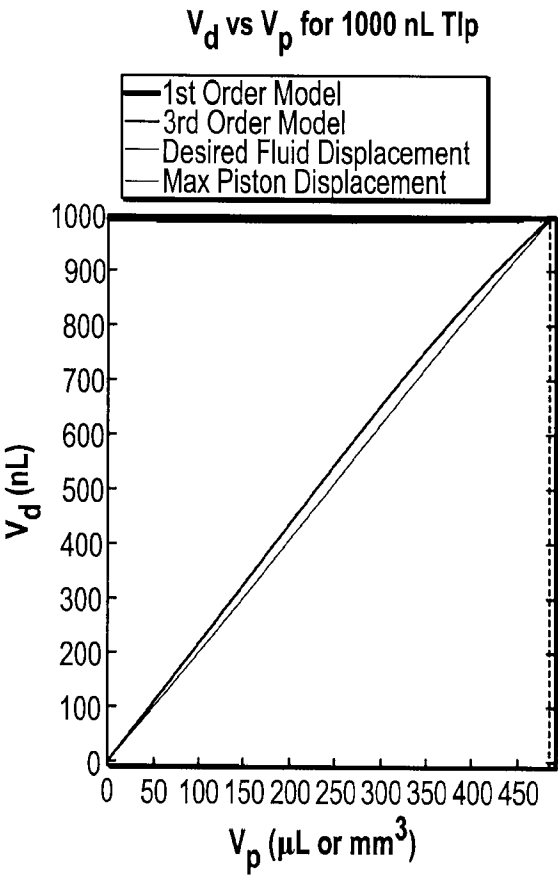


FIG. 10

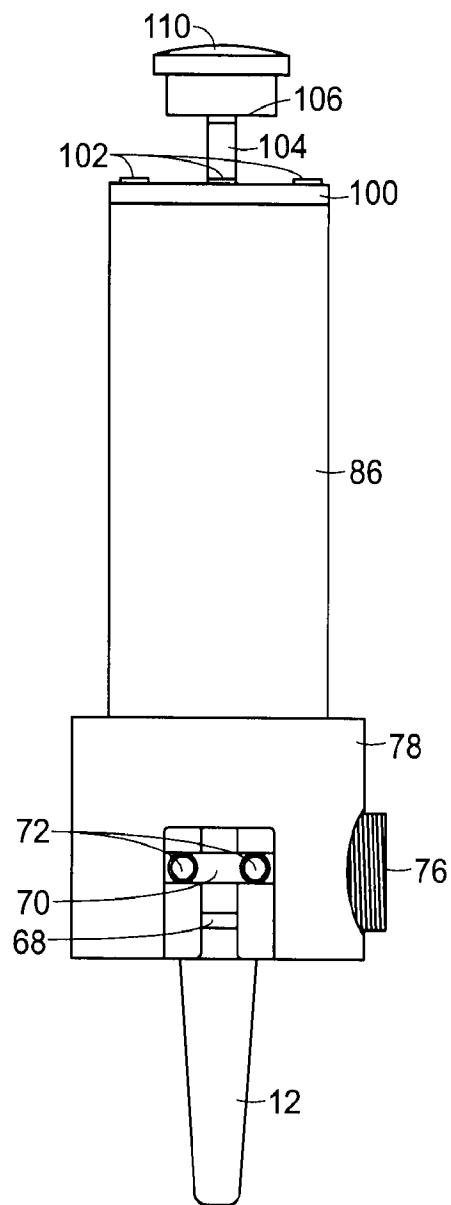


FIG. 11

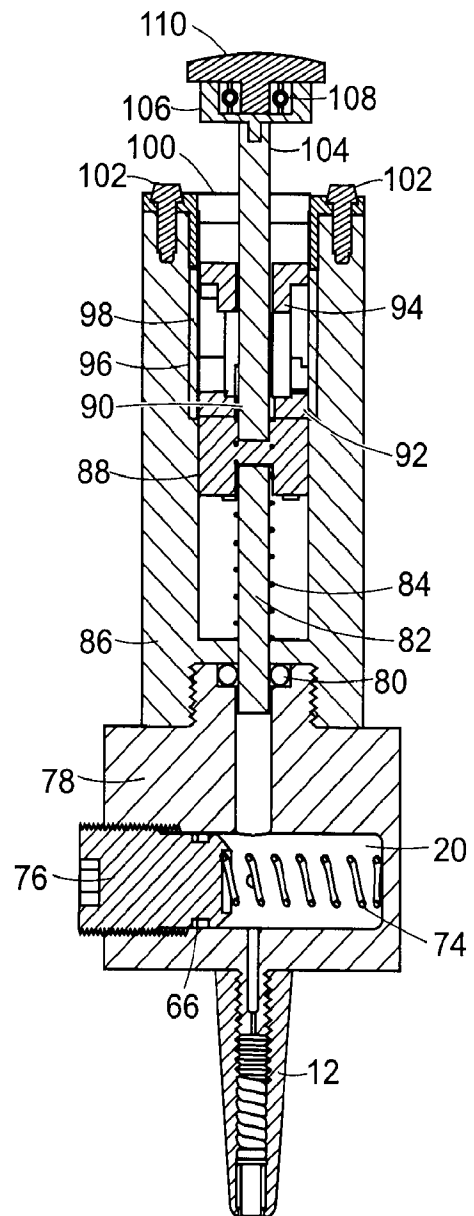
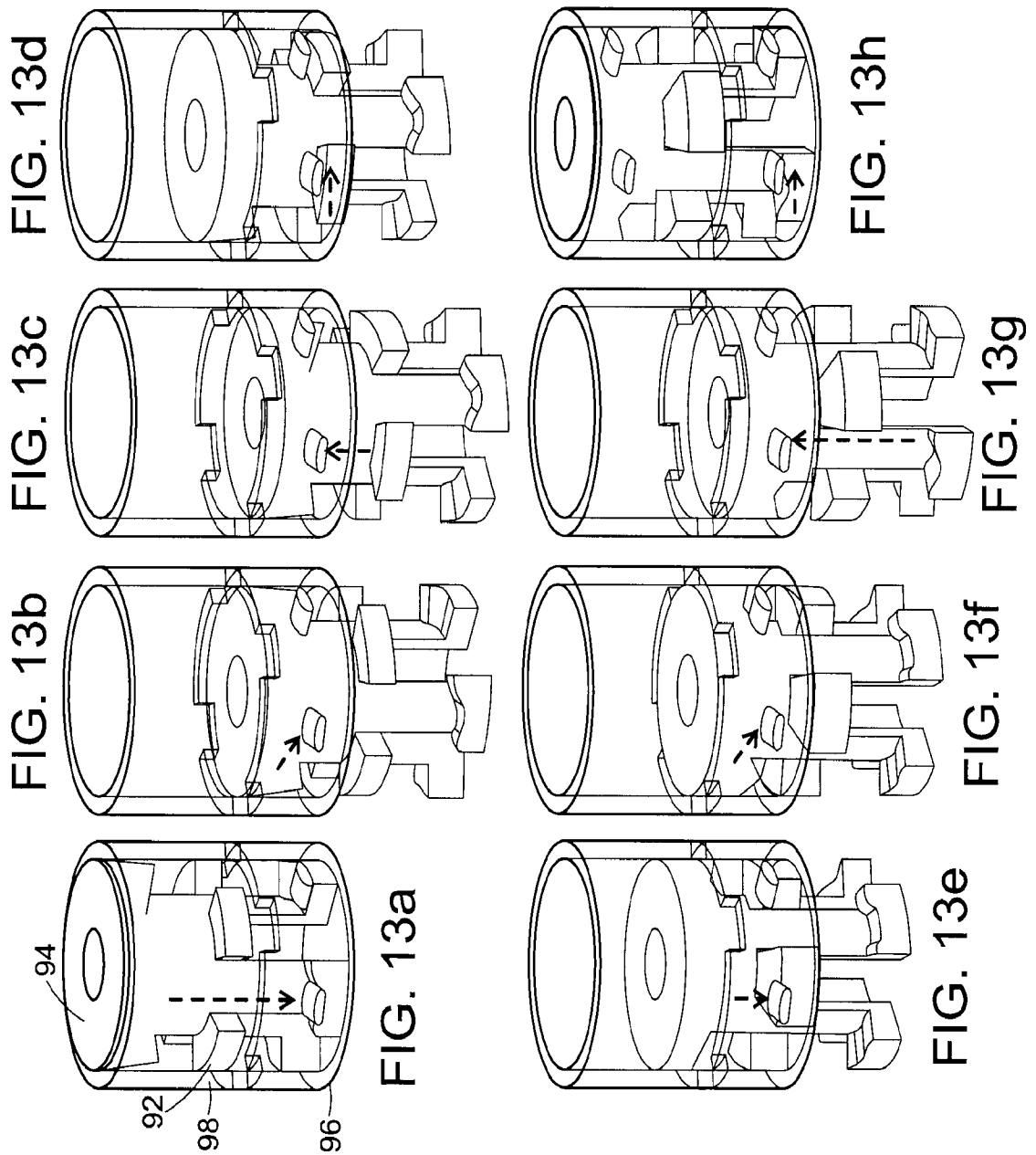


FIG. 12



INTERNATIONAL SEARCH REPORT

International application No.

PCT/US 17/31891

A. CLASSIFICATION OF SUBJECT MATTER

IPC(8) - B01L 3/02 (2017.01)

CPC - B01L 3/021, 3/0217, 3/02, 3/022, 3/0224, 3/0293, 2400/0478, 2400/0481

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

See Search History Document

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

See Search History Document

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

See Search History Document

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X ---	US 2013/0283884 A1 (Beroz et al.) 31 October 2013 (31.10.2013), Figs. 1-2, para [0034]-[0039]	1 and 4-5 ---
Y		2-3 and 6-8
Y	DE 102010045452 A1 (Hamilton Robotics GmbH) 15 March 2012 (15.03.2012), Fig. 1	2-3 and 7
Y	US 5,747,709 A (Oshikubo) 05 May 1998 (05.05.1998), col. 2, ln. 35-46, col. 3, ln. 23-60	6 and 8
A	US 2005/0119618 A1 (Gonnelli) 02 June 2005 (02.06.2005), Figs. 4A-4B, para [0076]-[0077]	1-8
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☐ Further documents are listed in the continuation of Box C.☐ See patent family annex.

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05 July 2017

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