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(74) Agent: **BUDDE SCHOU A/S**; Vester Søgade 10,
DK-1601 Copenhagen V (DK).

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(71) Applicant (for all designated States except US):
LITHIUM BALANCE A/S [DK/DK]; Gregersensvej 1A,
DK-2630 Taastrup (DK).

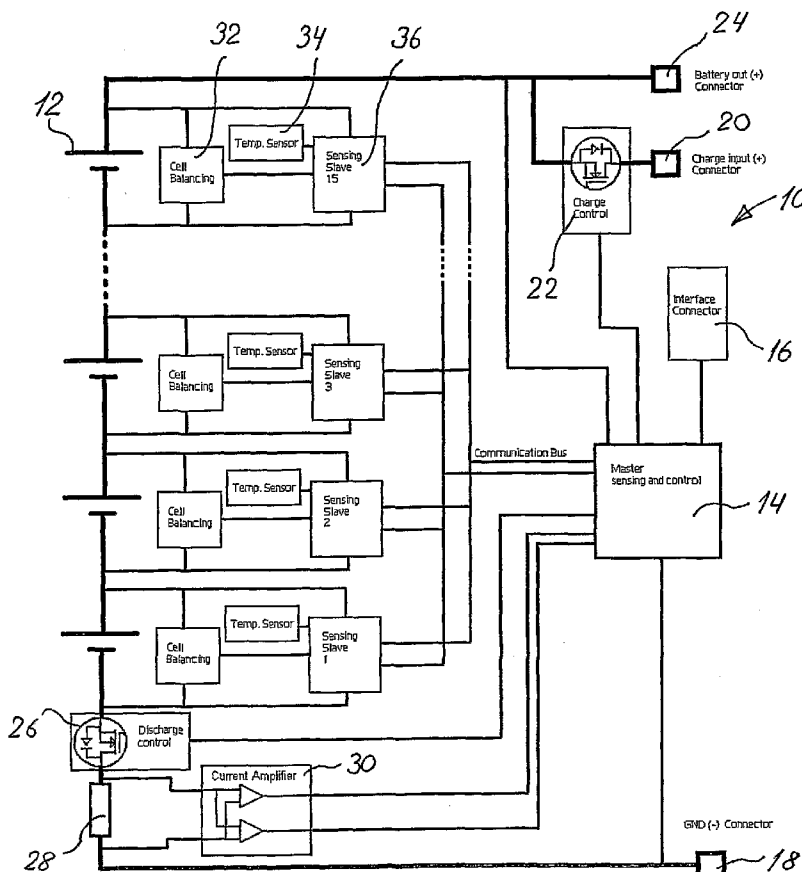
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(72) Inventor; and

(75) Inventor/Applicant (for US only): **LONCAREVIC, Ivan**
[DK/DK]; Havdrupvej 93A, DK-2700 Brønshøj (DK).

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(54) Title: A BATTERY MANAGEMENT SYSTEM



(57) Abstract: A method and apparatus are disclosed for a Battery Management System (BMS) for the controlling of the charging and discharging of a plurality of batteries (12). Each battery has an associated plurality of control circuits (32, 36) which monitor and control the charging of individual battery. These units are controlled by a central microcontroller (14) which shunts current around the battery if fully charged and stops discharge if a battery is fully discharged in order to prevent damage to the batteries.

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A BATTERY MANAGEMENT SYSTEM

TECHNICAL FIELD

The present invention relates to systems and methods for controlling charging and discharging battery cells such as lithium ion cells.

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BACKGROUND OF THE INVENTION

The introduction of rechargeable lithium ion batteries opens new possibilities of performances. Lithium technologies offer several advantages where maximum operating time and battery cycles life is required over wide temperature range, coupled with compact size and minimum weight. This technology needs strict charge and discharge criteria. Protection and detection against abusive conditions is here a demand. A BMS (Battery Management System) is to be developed in order to fulfil these demands.

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SUMMARY OF THE INVENTION

On the above background it is an object of the present invention to provide a battery management system (BMS) that ensures optimal charge and discharge conditions for each of the individual lithium cells and protects the lithium cells from any abusive conditions such as overload and/or short circuit.

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These and other objects and advantages are according to the invention attained by a battery management system (BMS) for the controlling and monitoring of a plurality of lithium ion cells or similar battery cells including lithium molybdenum, nickel, cadmium and PB cells, the BMS including a central controlling microcontroller and a plurality of control circuits connected with a respective battery cell and serving to individually monitoring the charging of the individual respective battery cell and at the time of reaching a maximum charging state establishing a shunt across the individual battery cell for allowing a continued charging of the remaining battery cells and at the same time communicating to the central controlling microcontroller a message representing that the maximum charging state has been reached and serving during discharging of the battery to monitor the state of the individual

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respective battery cell and to inform the central controlling microcontroller in case a minimum charging state has been reached for causing the central controlling microcontroller to disconnect the battery from the load in order to prevent excessive discharging of the individual battery cells.

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According to a specific embodiment of the invention said BMS comprises temperature sensors for continuous monitoring of the temperature in the device, means to shut down the charging / discharging in case of overload / short circuit, current monitoring by means of a shunt resistor, fuse protection of the device in case of overload / short circuit, a power supply for the control unit and a fuel gauge.

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The above and other objects and advantages are furthermore according to the invention attained by a method for controlling and monitoring a plurality of lithium ion cells or similar battery cells including lithium molybdenum, nickel, cadmium and PB cells, the method comprising:

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- during charging of said cells:
 - adjusting the voltage / current with respect to the cell condition to achieve optimum charge performance and bypassing one or more individual cells for allowing continuous charging of the remaining cells when said one or more individual cells has reached the top voltage;
- during discharging of said cells
 - the voltage of each individual cell is monitored until a minimum value has been reached in one or more individual cells at which time all the cells are shut down to prevent the lithium ion cell having reached the minimum voltage level to be ruined by continuous discharging;

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thereby ensuring the highest performance of the battery maximum safety during charging and discharging.

The present invention furthermore relates to a battery management system (BMS) of a modular design, where the system can be adapted to different numbers and physical placements of rechargeable cells. In a modular system according to the invention circuits/functions common to all cells are thus provided centrally, for instance on a single PCB or otherwise, whereas individual cells can be provided

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with corresponding control systems comprising cell balancing means and/or slave sensor means, the individual control systems being either of a type common for all cells in the system or individually adapted to each individual cell. The control systems at the individual cells can communicate with the central circuits of the system by wired connections, e.g. an analogue connection or a digital communication bus according to the specific implementation of the system. It would, however, alternatively be possible to provide communication between the individual cell control systems and the central parts of the system by wireless communication means, hence increasing the flexibility of the entire set-up even further.

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In the following detailed description of the invention the concepts of the invention will be illustrated by reference to two specific embodiments of the invention, but it is understood that the scope of the invention is not limited to those embodiments. Even though the embodiments shown and described in the detailed description of the invention relate to a specific number of cells and to specific voltages over each individual cell and over the entire batter the invention is not limited to these specific numerical values. In fact any number of individual cells may be included in the system and method of the invention.

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BRIEF DESCRIPTION OF THE DRAWINGS

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The present invention will be better understood with reference to the following detailed description of embodiments of the invention taken in conjunction with the figures, where:

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figure 1 shows a schematic block diagram of a first embodiment of a BMS (Battery Management System) according to the present invention,

figure 2 shows a diagrammatic view illustrating the charging of a 14 cells lithium ion battery when using the BMS of Fig. 1,

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figure 3 shows a diagrammatic view similar to the view of Fig. 2 of the discharging of the 14 cells lithium ion battery when using the BMS of Fig. 1.

figure 4 shows a schematic block diagram of a second embodiment of a BMS (Battery Management System) according to the present invention,

5 figure 5 shows a schematic view of a battery switch from the second embodiment of a BMS (Battery Management System) according to the present invention,

figure 6 shows a schematic view of a power supply from the second embodiment of a BMS (Battery Management System) according to the present invention,

10 figure 7 shows a schematic diagram of a start-up of the power supply from figure 6 of the second embodiment of a BMS (Battery Management System) according to the present invention,

15 figure 8 shows a schematic view of a supply part for the communication bus, an internal temperature sensor, an external temperature sensor and an output fuel gauge from the second embodiment of a BMS (Battery Management System) according to the present invention,

20 figure 9 shows a schematic view of a synchronizing and control unit from the second embodiment of a BMS (Battery Management System) according to the present invention,

25 figure 10 shows a schematic view of a cell balancing module and a cell voltage measurement from the second embodiment of a BMS (Battery Management System) according to the present invention,

figure 11 shows a schematic view of a single wire bus from the second embodiment of a BMS (Battery Management System) according to the present invention.

30 DETAILED DESCRIPTION OF THE INVENTION

Referring to figure 1 there is shown a schematic block diagram of a first embodiment of the battery management system or BMS according to the invention, which is

shown connected to a plurality of lithium ion cells, in the embodiment shown in figure 1 a total of 15 lithium ion cells. One of the lithium ion cells is designated the reference numeral 12 and the BMS is in its entirety designated the reference numeral 10.

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The BMS centrally includes a master microcontroller performing the overall sensing and control of the BMS, which central microcontroller is designated the reference numeral 14. The microcontroller 14 is connectable to external equipment such as an external PC through an interface connector 16. The BMS is connected to a common ground connector or terminal 18 and is connected to a charge input connector or terminal 20 through a charge control MOSFET 22 serving to separate the charge input connector from a battery output connector 24 constituting the positive output terminal of the battery system relative to the common ground connector or terminal 18.

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The series configuration of the 15 lithium ion cells defines a positive terminal which is connected to the junction between the battery output terminal or connector 24 and the battery voltage sensor terminal of the charge control MOSFET 22. The negative terminal of the series configuration of the 15 lithium ion cells is connected through a series configuration of a discharge control MOSFET 26 and low ohm resistor to the common ground connector or terminal 18. The voltage across the low ohm resistor 28 is sensed by current amplifier delivering an output voltage in response to an excessive current passing through the low ohm resistor 28 for informing the central master microcontroller 14 of the occurrence of an excessive current load through the series configuration of the 15 lithium ion cells. The discharge controlling MOSFET 26 is controlled by the central master microcontroller 14 and is used for a shut down of the supply of current from the lithium ion cells as will be described below.

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As a particular feature of the BMS according to the present invention each lithium ion cell is connected to a separate monitoring and controlling circuit including for each lithium ion cell a cell balancing circuit 32, a temperature sensor 34 and a communication or sensing slave circuit 36 establishing communication from the cell

balancing circuit 32 and the temperature sensor to and from the central master microcontroller 14. The cell balancing circuit 32 basically serves to monitor the voltage across the lithium ion cell during charging and in case the lithium ion cell connected to the cell balancing circuit in question has reached the top voltage and the master microcontroller 14 is still controlling the BMS into continuous charging of the remaining lithium ion cells, the cell balancing circuit 32 shunts the lithium ion cell for allowing the continuous charging of the remaining lithium ion cells.

The temperature sensor 34 serves to monitor if an excessive temperature is reached in the lithium ion cell and/or in the cell balancing and sensing slave circuits 32 and 36, respectively, and the sensing slave circuit 36 serves during discharging of the lithium ion cell to monitor the discharging of the lithium ion cell to a minimum at which time the sensing slave circuit 36 informs the master microcontroller 14 of the occurrence of a complete discharging of one of the cells causing the master microcontroller 14 to shut down the whole circuitry in order to prevent the lithium ion cell having reached the minimum voltage level to be ruined by continuous discharging of the lithium ion cell.

Referring to figure 2 there is shown a diagram illustrating the advantageous charging of a total of 14 cells by the use of the BMS as shown in figure 1, however, modified into communicating with 14 lithium ion cells rather than 15 lithium ion cells as illustrated in figure 1. From figure 2 it is evident that the individual lithium ion cells are charged simultaneously to the same maximum level of approximately 4.2V.

Referring to figure 3 there is shown a diagram illustrating the advantageous discharging and control of a total of 14 cells by the use of the BMS as shown in figure 1, however, modified into communicating with 14 lithium ion cells rather than 15 lithium ion cells as illustrated in figure 1. From figure 2 it is evident that of each of the individual cells is monitored and the battery as a whole is allowed to be shut down at the time a single lithium ion cell reaches the minimum voltage level of 2.8V.

Referring to figure 4 there is shown a schematic block diagram of a second embodiment of the battery management system or BMS according to the invention,

which is shown connected to a plurality of lithium ion cells, in the embodiment shown in figure 4 a total of 15 lithium ion cells. One of the lithium ion cells is designated the reference numeral 12 and the BMS is in its entirety designated the reference numeral 10.

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The BMS centrally includes a master microcontroller 14 performing the overall sensing and control of the BMS. The master microcontroller 14 is connectable to external equipment such as an external PC through an external device bus 16.

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The BMS is connected to a common battery connector or terminal 24 which is connected to the series configuration of the 15 lithium ion cells 12 and defines a positive terminal. The negative terminal of the series configuration of the 15 lithium ion cells is connected through a low ohm shunt resistor 28. The voltage across the low ohm shunt resistor 28 is sensed by current amplifier 44 delivering an output voltage in response to an excessive current passing through the low ohm shunt resistor 28 during charging or during discharging for informing the central master microcontroller 14 of the occurrence of an excessive current load through the series configuration of the 15 lithium ion cells. In case of a short circuit / overload the threshold of charging currents or discharging currents is reached and the central master microcontroller shuts down the charging / discharging process.

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The low ohm shunt resistor 28 is further connected to a junction between the load enable MOSFET 26 and the charge enable MOSFET 22 serving to separate the load discharging out ground terminal 18 and the charging in ground terminal 20. The load enable MOSFET 26 and the charge enable MOSFET 22 are controlled by the central master microcontroller 14 and is used to connect the lithium ion cells to the load in case of discharging and to the charger in case of charging and to shut down the supply of current in case of short circuit / overload as will be described below.

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As a particular feature of the BMS according to the present invention each lithium ion cell is connected to a separate monitoring and controlling circuit including for each lithium ion cell a cell balancing circuit 32 and a communication and sensing slave circuit 36 establishing communication from the cell balancing circuit 32 to and

from the central master microcontroller 14. The sensing circuit 36 serves to monitor the voltage across the lithium ion cell during charging and in case the lithium ion cell connected to the cell balancing circuit in question has reached the top voltage and the master microcontroller 14 is still controlling the BMS into continuous charging of the remaining lithium ion cells, the cell balancing circuit 32 shunts the lithium ion cell in question which has reached the top voltage for allowing the continuous charging of the remaining lithium ion cells.

The shunting is done by the cell balancing circuit 32 by shorting the positive and the negative pole of the cell through a power resistor and a fast switching transistor. PWM modulation is in an embodiment of the invention done to ensure an adjustable current through the resistor.

The sensing slave circuit 36 serves during discharging of the lithium ion cell to monitor the discharging of the lithium ion cell to a minimum at which time the sensing slave circuit 36 informs the master microcontroller 14 of the occurrence of a complete discharging of one of the cells causing the master microcontroller 14 to shut down the whole circuitry in order to prevent the lithium ion cell having reached the minimum voltage level to be ruined by continuous discharging of the lithium ion cell.

A power supply fed from the battery is used to supply the electronics of the BMS with DC voltage. Switching transistors connected in half bridge configuration and filtered by a low pass filter and further regulated by voltage regulators provide the necessary voltages for the controlling electronics.

An internal temperature sensor 34 serves to monitor and report to the master microcontroller 14 the temperature in the master microcontroller 14 and in case an excessive temperature is reached the master microcontroller 14 the charging / discharging will shut down. A battery temperature sensor 40 serves to monitor and report to the master microcontroller the temperature in the lithium ion cell and/or in the cell balancing and sensing slave circuits 32 and 36, respectively. If an excessive temperature is reached in the lithium ion cell and/or in the cell balancing and

sensing slave circuits 32 and 36 the master microcontroller will shut down the charging / discharging process.

5 A cell communication bus 42 is used for the communication between the master microcontroller and a slave microcontroller provided in each individual slave circuit. The bus is separated from the master microcontroller by an isolation stage and (de)coupling 38. The bus is also used for the fuel gauge where the remaining capacity of the battery is reported.

10 Referring to figure 5 there is shown a detailed schematic description of a discharge enable and charge enable switch and the current sensing shunt resistor. The BMS contains two parallel CMOS switches which serve to separate the charging input ground connector from the battery output ground connector. Each switch is created by a parallel connection of MOSFETs where MOSFET number D1 up to D20 are
15 used for connecting the load during discharging and MOSFET number D52, D55, D68, D64, D65, D67 are used for connecting the charger during charging.

The load is switched to the battery with 'HIGH' level of BATTERY_SW signal, thereby connecting the positive voltage derived from +15V through Q2 and Q1
20 transistors. The charger is switched to the battery with 'HIGH' level of CHARGER_SW signal, thereby connecting the +15V through Q29 and Q28 transistors.

The hardware shutdown is activated by reaching the threshold level derived from
25 the shunt resistor in the case of overload / short circuit. The analogue value of the charge current is derived from the U2B inverter output CHARGE. The analogue value of the load current is done in two ranges where the lower current range is read out from output of U4A and the higher range is read out from the output of U2A opamp where the margins of the lower and higher current interval will vary
30 depending on the application and will be set up by gain determining resistors of non-inverting amplifiers R8, R7, R35. The Q30 transistor enables or disables the supply for charge current sensing opamp for power saving reasons.

In case the melting fuse F2 blows due to short circuit through D61 and D71 MOSFETs to prevent the deep discharging of the battery the "Fuse blow" shutdown is initiated by 2 signals in logical AND function provided by Q16 and Q17 to avoid random triggering of "Fuse blown" shutdown. In case of hardware shut down due to a high current level a 'HIGH' level of the SHUT DOWN signal on the Q4 transistor will result in opening of the Q4 transistor which remains open by positive voltage feedback through R24 resistor. The shutdown can be terminated only by changing the level of the SHUTDOWN_RST signal thereby cutting of the Q5 transistor and disconnecting the positive voltage feedback provided by the R24 resistor.

Referring to figure 6 there is shown a detailed schematic description of a power supply for the control module which is created by D41 and D40 switching transistors connected in halfbridge configuration and driven by U22 halfbridge driver where feedback from the battery voltage is applied through U4B opamp connected in voltage follower configuration in the function as a buffer. The DC output from the control module is created by filtering the pulsing DC voltage from the switching transistors with LC filter L1 and C64 and regulate the voltage by voltage regulators U24 (15V output +15V_ON) and U23 (5V output +5V_ON) and +9V by using D48 Zener diode and +5V by U20 regulator where the 5V output is supplied directly from the battery for supplying the main microcontroller in the sleep mode. The +5V output is disabled by Q25 which opens when the PWM (Pulse-Width Modulation) of the halfbridge is active.

Referring to figure 7 there is a diagram view of the start-up sequence of the power supply where AUX_START signal 'HIGH' after power-up of the master microcontroller (1) provides temporary power supply for the halfbridge. After approx. 100ms the DC voltage is fully developed resulting in ramp up of the +5V_ON voltage (2) and after additionally 100ms the temporary power supply is terminated (3).

Referring to figure 8a there is shown a detailed schematic description of a supply part for the communication from the master microcontroller to the slave

microcontroller communication bus where signal from the master microcontroller to the slave microcontroller TX_CELL is amplified by Q10 transistor.

5 Referring to figure 8b there is shown a detailed schematic description of a supply part for the communication from the slave microcontroller communication bus to the master microcontroller where the signal from the slave microcontroller to the master microcontroller is supplied by a +5V_ON signal and the current is limited by R194 resistor when RX_CELL is switched to ground to provide the "LOW" signal level.

10 Referring to figure 8c there is shown a detailed schematic description of an internal temperature sensor where the internal temperature is sensed by R45 thermistor.

15 Referring to figure 8d there is shown a detailed schematic description of an external temperature sensor where the external or battery temperature sensing is provided by transient voltage suppressor diodes, voltage level adjusting resistors, filtering capacitors and external NTC thermistor.

20 Referring to figure 8e there is shown a detailed schematic description of an analogue output for a fuel gauge where the voltage level is adjusted by a R44 resistor. The fuel gauge use the PWM output (V_OUT) where the duty cycle of the output can be used for deriving the remaining capacity of the battery alternatively the PWM output (V_OUT) can be used to carry binary information for a digital fuel gauge. The fuel gauge is counting all currents going in an out of the battery. A two stage amplifier Q11, Q13, Q12, Q14 is used to improve current carrying capability of
25 the PWM_output. The stages in the two stage amplifier are filtered by parallel RC network and separated by a ISO1 optocoupler from the master microcontroller.

30 Referring to figure 9 there is shown a synchronizing and control unit for the slave microcontroller for controlling shut down, enabling charging or discharging and sensing circuit. Each slave have their own address for the master to recognize them and each slave individually receives synchronise pulse and values for cell balancing from the master and sends voltage measurements and status information to the master. The sensing circuit consists of current sensing of the discharge

current (DISCHARGE_HIGH, DISCHARGE_LOW), sensing of the charging current (CHARGE), sensing of the internal temperature (TEMPSNS_INT), sensing of the external temperature (TEMPSNS_EXT) and sensing of the battery voltage (BATTERY_VOLTAGE). The power supply of the control module is supported at the startup by a START_AUX signal and the switching of the halfbridge is regulated by a PWM_AUX signal and the feedback from the output +5V_ON when the halfbridge is ready to supply its driver from its own output. The 5V_uP can disable the current sensing opamps thereby reducing the power consumption in the sleep mode. The CMOS switch for enabling charging is controlled by CHARGE_SW signal and the CMOS switch for enabling discharging is controlled by BATTERY_SW signal. The 'HIGH' SHUT_DOWN signal will disconnect the +15V from the gates thereby securing open status of the MOSFETs and the almost immediately following 'HIGH' level of the TURN_OFF signal secures the fast discharging of the gates through 12 ohm resistor. The microcontroller provide a shut down status cancelling by a SHUT_DOWN signal at 'LOW' level for at short period of time and the driving signals for OUT_1 and OUT_2: OUT_1_DRIVE and OUT_2_DRIVE. The 'HIGH' level of WAKE_UP signal provides a low signal on the pin 1 of the Microcontroller through grounding the collector of Q8 thereby activating the microcontroller from power save (standby) mode. The cell communication is provided by TX_CELL (transfer to cell) signal and RX_CELL (receiving from cell) signal thereby the charge can be regulated by the BMS by transferring information to the cell by using TX_CELL and receiving information from the cell by using the RX_CELL signal and further diagnostics of the BMS can be made using the appropriate software.

Referring to figure 10a there is shown a cell balancing module where the charging of each individual cell is controlled by its own voltage spike protected microcontroller. Cell balancing is provided by shorting the positive and negative pole of the cell through a power resistor and a fast switching transistor. PWM is used to ensure adjustable current through the resistor. The slave receives a voltage from the master, calculated the difference between the received value and computes the duty cycle for the cell balancing PWM. If the cell voltage is lower than the received voltage from the master the PWM is set to zero.

Referring to figure 10b there is shown a cell voltage measurement module where measurement is done by a voltage divider made of parallel 1k ohm resistors where the analogue value is connected to pin 3 of the microcontroller. The cell balancing is stopped while measuring voltage to avoid a voltage drop in cables. The measurement is transmitted to the master microcontroller. In the sleep mode the voltage sensing is disabled by turning off the NPN transistor resulting in the PNP transistor being cut off as well.

Referring to figure 11a there is shown a single wire bus for communicating the TX and RX signals to a single wire DATA including galvanic isolation from the source and amplifying by D64 transistor.

Referring to figure 11b there is shown a power stage of the output OUTPUT_1

Referring to figure 11c there is shown a protection circuitry of the thermistor monitoring the battery and / or in the cell balancing and sensing and control circuits.

Referring to figure 12 there is shown a cell to master microcontroller communication bus for decoupling the TX_CELL signal to RX1 up to RX15 signals and coupling of the TX1 up to TX15 to RX_CELL signal.

A detailed description of an embodiment of the invention is given with reference to the following annexes, where:

- ANNEX A contains a technical description;
- ANNEX B contains a software description; and
- ANNEX C contains detailed circuit diagrams of portions of the system.

Annex A**System Specification**

Battery Voltage		
Amount of cells		15
Cell voltage		2,8V – 4,2V / cell
Minimum voltage		42 VDC
Maximum voltage		63 VDC
DC Current Handling		
Continuous discharge current		150 A
Peak discharge current (< 8s)		250 A
Max. charge current handling		35 A
Peak charge current (< 1s)		50 A
Measurements / Accuracy		
Single cell voltage		< 1 %
Battery voltage		< 1 %
Δ temperature resolution		< 0,25 °C
Temperature		+/- 3 °C
Cell Balancing		
Maximum bypass current 1A		Adjustable from 0A
BMS Power Consumption		
Standby consumption		< 250 μ A
Active consumption		< 50 mA
Overload		
Discharge > 200 A		Software shutdown
Resting period		10 s, 3 attempts in a row to restart BMS
Custom overload behavior		TBD
Short Circuit		
Battery short circuit activation		Hardware shutdown
Resting period		10s, 3 attempts in a row to restart BMS
Custom Short circuit behavior		TBD
Fuse		
MEGA FUSE from Littelfuse fuse		175A
High Temperature Protection		
Heat sink		Passive
Termination due overload		
Over-voltage		
Battery disconnection response time when overvoltage appears		20 ms
Single cell disconnection in the case of overvoltage		1 s
Under-voltage		
Device shut down		TBD
Operating Conditions		
Minimum ambient temperature		- 20 °C
Maximum ambient temperature		+ 50 °C
Maximum operating temperature		+ 105 °C

Mainboard Description

The BMS module can be in principle described as a high current capacity CMOS switch featured by emergency shut down in the case of short-circuit or overload of the battery. This switch provides connection of the charger to the battery in the case of charging and to the load (motor) during normal operation.

- Battery switch for charger and load controlled by microcontroller featured by hardware shut down in the case of overload or short circuit; current sensing
- Power supply for the control module
- Supply part for the cell communication bus and analogue output reserved for fuel gauge
- Master microcontroller

(See Fig. 5)

Function:

Battery switch for charger and load controlled by microcontroller featured by hardware shut down in the case of overload or short circuit; current sensing. Additionally "fuse blow" shutdown is introduced to prevent the deep discharging of the battery in the case of short circuit of switching MOSFETS.

Description:

The BMS contains two parallel CMOS for connecting the battery to the charger or to the load. Each switch is created by a parallel connection of MOSFETs : Transistors D1 up to D20 for the load connection and the switch for charger connection is created by a parallel combination of D52, D55, D68, D64, D65, D67 transistors.

In the normal mode the load is switch to battery with 'HIGH' level of *BATTERY_SW* signal. This connects the positive voltage derived from +15V through Q2 and Q1 transistors. The connection of the charger is enabled by Q29 through Q28 transistors with 'HIGH' *CHARGER_SW* signal.

The hardware shutdown is activated by reaching the threshold level of currents in the case of overload/short circuit. The current level is derived from the shunt resistor R1, the analogue value of the charge current is derived from the U2B inverter output - *CHARGE*. The readout of the load current is done in two ranges: for the lower current range is read out from output of U4A and the

higher range from the output of U2A opamp. The margins of lower and higher current interval will be various depending on the concrete project and will be set up by a gain determining resistors of a non-inverting amplifiers R8, R7, R35. The Q30 transistor enables or disables the supply for charge current sensing opamp for power saving reasons.

The hardware shut down initiated by a high current level will result the 'HIGH' level of the SHUT DOWN signal on the Q4 transistor resulting the opening the Q4 transistor, which remains open through positive voltage feedback through R24 resistor (note that the level of the *SHUTDOWN_RST* signal is 'HIGH' during normal operation).

Positive voltage of *SHUT DOWN* opening Q6 closes Q2 resulting the cut off of the Q1 transistor which disconnects the +15V source before connecting the gates of the switches to ground to prevent the short circuit of +15V_ON to the ground which could appear when gates of transistors are grounded.

The shutdown can be terminated only by changing the level of the *SHUTDOWN_RST* signal cutting off the Q5 transistor and disconnecting the positive voltage feedback provided by R24 resistor.

The shut down initiated by a microcontroller is done by setting the level of *TURN_OFF* to 'HIGH' level (software shutdown).

The " fuse blow" shutdown is providing by connecting the positive and negative poles of the battery resulting short-circuit through D61 and D71 MOSFETs. The short circuit current will blow the charger fuse F2. The "fuse blow" shutdown is initiated by 2 signals in logical AND function (provided by Q16 and Q17 circuitry) to avoid random triggering of this type of shutdown. The activating of the charger is indicated to processor by "HIGH" *CHARGER_ACTIVE* signal.

(See Fig. 6)

Function:

Power supply of the control module

Description:

The core of the power supply fed from battery and created by a D41 and D40 switching transistors connected in halfbridge configuration driven by a U22 halfbridge driver. Feedback from the supply (battery) voltage is applied through U4B opamp connected in voltage follower configuration in the function as a buffer.

The DC output is created by filtering the pulsing DC voltage with lowpass LC filter (parallel connection of L1 and C64). The regulated voltages are provided by voltage regulators U24 (15V output +15V_ON) and U23 (5V output +5V_ON); +9V by using D48 Zener diode and +5V by U20 regulator. The +5V output is supplied directly from the battery and it is meant only for supplying the main microcontroller in the sleep mode. The +5V output is disabled by Q25

transistor, which opens when the PWM of the halfbridge is active.

Firstly the *AUX_START* signal is 'HIGH' at the startup to ensure the supply VCC voltage for the drive. After some time this signal is set to 'LOW' and the VCC is derived from the *+15V_ON* voltage. The startup of the switching power supply of the control module can be described as shown on Fig.1. After power up of the master microcontroller (1.) the processor sets up the *AUX_START* signal to "HIGH" to provide the temporary supply for the halfbridge driver. After a certain time (approx. 100 ms) the DC voltage is fully developed resulting in the ramp up to the *+5V_ON* voltage (2.). To ensure the correct function of the power supply, the temporary supply is held on for additionally 100 ms and after this it is terminated (3.).

(See Fig. 7)

(See Fig. 8)

Function:

Supply part for the cell communication bus and analogue output reserved for fuel gauge

Description:

The transfer signal from the microcontroller to cells *TX_CELL* is amplified by a Q10 transistor. The signal received from the slave microcontrollers by a master controller is supplied by a +5V_{ON} signal and the current is limited by a R194 when the *RX_CELL* is switched to ground to provide the "LOW" signal level. The internal temperature is sensed by a R45 thermistor and the voltage level for the controller is adjusted by a R44 resistor.

For the fuel gauge is reserved the PWM output (*V_OUT*), where the duty cycle of the output (i.e. the pulse width) can be equal to the remaining capacity of the battery or it is also capable to carry binary information for digital fuel gauge. The current carrying capacity of the output is improved by a two stage amplifier created by Q11,Q13 and Q12,Q14. The stages in cascade connections are filtered by a lowpass filters created by a parallel RC networks. This output is also separated by a ISO1 optocoupler from the master microcontroller.

The circuitry for the external temperature sensing is created by a transient voltage suppressor diodes, voltage level adjusting resistors, filtering capacitors and the external NTC thermistor.

(See Fig. 9)

Function:

Synchronizing and the control of the slave microcontrollers. Controlling of the shut down and enabling of the load and the charger.

Description:

Microcontroller can be programmed and reconfigured by a J32 connector. The signals for synchronizing and controlling can be divided to following groups:

- Sensing circuits
- Control module power supply startup and regulation
- CMOS switch control
- Cell communication
- Charger communication
- Analogue/digital output

The sensing circuitry consists of current sensing of a load current (*DISCHARGE_HIGH* and *DISCHARGE_LOW*) and the charging current (*CHARGE*), sensing of the internal temperature (*TEMPSNS_INT*) and the temperature of the battery (*TEMPSNS_EXT*), sensing of the battery voltage (*BATTERY_VOLTAGE*).

The power supply of the control module is supported at the startup by a *START_AUX* signal and the switching of the halfbridge is regulated by a *PWM_AUX* signal and the feedback from the output *+5V_ON* to notify when the halfbridge is ready to supply its driver from its own output. The *+5V_uP* can disable the supplying the current sensing opamps thus reducing the power consumption in the sleep mode.

The CMOS switch of the charger is switched by *CHARGE_SW* signal and the load switch is controlled by a level of a *BATTERY_SW* signal. In the case of the shut down the positive voltage *SHUT_DOWN* will disconnect the +15V volts from the gates securing the open status of the MOSFETs and almost immediately after that the 'HIGH' level of the *TURN_OFF* signal secures the fast discharging of the gates through 12Ω resistor.

The cell communication is provided by a *TX_CELL* signal (transfer to cells) and *RX_CELL* (receiving from the cells).

During the charging the charge can be regulated by BMS transferring information to a charger using *TX* signal and receiving information from the charger – *RX* signal. These signals can be used for a diagnostic of the BMS with the proper software.

The microcontroller provide a shut down status cancelling by a *SHUT_DOWN* signal at 'LOW' level for a short period of time and the driving signals for outputs *OUT_1* and *OUT_2* : *OUT_1_DRIVE* and *OUT_2_DRIVE*.

The processor is activated from the power save (standby) mode by "HIGH" level of *WAKE_UP* signal which will provide low signal on the pin 1 of the Microcontroller through grounding the collector of the Q8.

Control Module

The main function of the control module is the supervising the charging of the separate cells of the battery and the overall charging by controlling of the charger.

(See Fig. 10)

Function:

Cell balancing

Description:

Each separate cell of the battery is controlled by its own voltage spike protected microcontroller. The cell balancing is provided by shorting the positive and negative pole of the cell through the power resistor. The bypassing is done by a PWM modulation to ensure the adjustable current through the resistor. The cell is bypassed through fast switching transistor. The cell voltage measurement is done by a voltage divider made of parallel $1k\Omega$ resistors, where the analogue value is connected to pin 3 of the slave microcontroller.

In the sleep mode the voltage sensing is disabled by turning off the NPN transistor resulting the cut off the PNP transistor as well.

(See Fig. 11)

Function:

Single wire bus for a charger communication and output interface.

Description:

Converting *TX* and *RX* signals to a single wire *DATA* featured galvanic isolation from the source and amplifying by D64 transistor. The control module also includes power stage of the output *OUTPUT_1*. On control board there is an additional protection circuitry of the thermistor located on the mainboard.

(See Fig. 12)

Function:

Cell to microcontroller communication bus signal coupling/decoupling including galvanic isolation.

Description:

Decoupling the TX_CELL to RX1 up to RX15 signals and coupling of the TX1 up to TX15 to RX_CELL signal.

Software Features

Internal functions:

Analogue measurements

Measurement of the battery voltage, current sensing, temperature sensing is described in the hardware part - *refresh time: 10msec*

Power management

To minimize the power consumption in the sleep mode some power saving features are involved in the design:

- Disconnecting the charger
- Disabling the voltage measuring of the separate cells
- Disable the continuous current sensing (sample monitoring 10 times per second)
- Disabling the power supply for the control circuitry except the master microcontroller

Power supply

Power supply start up voltage ¹	27,78 V
Power supply output voltage	20 V
Power Supply Max PWM duty cycle	90 %

Functions:

Charging

Charging max current (< 1sec) ²	35 A
Charging max current (< 40msec) ³	50 A
Charging shutdown resting time ⁴	10 sec
Shutdowns in a row ⁵	3
Cell voltage max ⁶	4,25 V
Cell voltage max reset	4,15 V
Total voltage max ⁷	58,8 V
Total voltage max reset	58,1 V

Discharging

Discharging max current (<1sec) (see note 2)	200 A
Discharging max current (< 40msec) (see note 3)	250 A
Discharge shutdown resting time (see note 4)	10 sec
Shutdowns in a row (see note 5)	3
Cell voltage min ⁸	2,8 V
Cell voltage min reset ⁹	3,7 V
Discharge re-enable fuel gauge ¹⁰	10 Ah

¹ Minimum overall voltage required to start up the power supply

² Duration longer than 1 second is considered for an overload

³ Duration longer than 40 milliseconds is considered for an overload

⁴ Time interval until next restart attempt

⁵ Maximum number of attempts in a row until definitive shutdown of BMS

⁶ When the highest cell voltage reach this value the charging is stopped and cell balance will equalize the cell voltages.

When the maximum cell voltage falls bellow the value given by *Cell voltage max reset* the charging is re-enabled

⁷ When the battery voltage reach this level the charging is stopped and again re-enabled when the voltage falls below

Total voltage max reset value

⁸ If the lowest cell voltage reach this value the discharge is stopped

⁹ The lowest voltage amongst cell voltages must reach this value to re-enable discharging

¹⁰ The minimum charged remaining capacity of the battery, when the discharge is re-enabled

Cell balancing

When cell balancing is started, the PWM is computed from the cell voltage. The computing is done by adding the differences in cell voltage from the lowest cell voltage, together. After adding all cell voltages, the PWM value to each cell is computed to ensure total maximum power dissipation don't exceed the limit

Cell balance max power ¹¹	27 W
Cell balance start voltage average ¹²	4,10 V
Cell balance peak start voltage ¹³	4,20 V
Cell balance min charge current ¹⁴	0,5 A

Temperature

Battery Temperature cut off high ¹⁵	70 °C
Battery Temperature high reset	60 °C
Battery Temperature cut off low ¹⁶	-20 °C
Battery Temperature low reset	-10 °C
BMS Temperature cut off high ¹⁷	100 °C
BMS Temperature high reset	90 °C

Fuel Gauge (Counting Amp/hours)

Fuel Gauge min input ¹⁸	±0,3 A
Max value ¹⁹	105% of the specified capacity
Self learning ²⁰	1% / cycles

Sleep mode

Enter sleep mode after (< 300 mA)	60 sec
Wakeup current	300 mA
Standby search time	0,1 sec

Interfaces:

Single wire bus (communication with a charger or the diagnostic program)

1 Analogue output

1 Open collector "High" / "Low" level output

¹¹ Maximum overall power dissipation allowed on the cell balancing power resistors

¹² When the average voltage from all the cells reaches this level and the *Cell balance min charge current* condition is fulfilled the cell balancing is triggered

¹³ When the voltage of any of the cells reaches this value the cell balancing is triggered

¹⁴ When the charging current reaches this value and the *Cell balance start voltage average* condition is fulfilled the cell balancing is triggered

¹⁵ When this battery temperature is reached the charging and the discharging is stopped until the temperature fall to *Battery Temperature high reset* and then the functions are re-enabled

¹⁶ When this battery temperature is reached the charging and the discharging is stopped until the temperature rise to *Battery Temperature low reset* and then the functions are re-enabled

¹⁷ When this internal BMS temperature is reached the charging and the discharging is stopped until the temperature does not fall to *BMS Temperature high reset* and then the functions are re-enabled

¹⁸ The value of the charge/discharge current must exceed this value to be relevant for the gauge counting

¹⁹ Maximum value indicated by a fuel gauge related to previously evaluated capacity using self learning

²⁰ When the battery is charged from empty to full the real capacity can be reevaluated in the range of 1% from the previously obtained value in the self learning process

BMS Internal (Cell) Communication

Internal Communication

The master controls and monitors all the slaves by a communication between slaves and master. The master handles the communication and the slaves only respond when asked. The communication is build upon a USART full duplex, running on 5kb with 9bit transmission. When the 9th bit is set, the byte is a command, otherwise its data. When receiving a package, it is stored in a buffer to calculate if the checksum is the same as received. Only if the checksum matches it will use the package.

Start byte / Address

In the beginning of all packages, there has to be a start byte containing the address of the slave witch is receiving or transmitting. It is possible to connect up to 120 slaves to the master. The slaves will have there on address given in production for the master to access them. The addresses of the slaves will start from 1 and up to the number of slaves connected.

List of addresses: (9th bit set)

Value	Address
0	Global address
1-120	Slave address

Command

The master sends packages to the slaves to give inform or give instructions. The command is always the first byte after the start byte.

There are always 3 command bytes in one package (Start byte, Command and Checksum)

List of commands: (9th bit set)

Value	Name	Description
0-120	Start byte	Start byte and address of the slaves
121	Send info to master	Return data to master
122	Info from master	Average battery voltage
123	Error check	Check if one of the slaves has a error
124	Enter sleep-mode	Put the slaves into sleep-mode
125	Sync pulse	The master will transmit a sync pulse
126	Calibration	The Master transmit the real cell voltage and the slaves adjust the measured voltage
128-255	Checksum	

Data

In some of the Packages it is necessary to transfer a few data bytes. When transmitting a data byte, the parity bit has to be low to indicate, it is a data byte and not a command. The receive buffer in the slaves is very small and it is only packages is possible to transmit or receive packages up to 16 bytes of data. When transmitting data values of 2 bytes, LSB is sent first.

Checksum

The checksum is the last byte of the packages and data coming after what is ignored only a new start byte in a new package is accepted. Since the check sum only calculate with 8bits a value

25 is added for each parity bit. Every time the checksum has overflow the checksum is incremented one time. The checksum it self is not added to the checksum and not taken into calculation. The checksum can only have the value from 128 to 255, if the value is out of range two different values is added depending of the checksum value.

Checksum	Value to Add
Parity	25
Each byte	1
Overflow	1
0-122	133 (128+5)
123-127	10
128-255	No add

Ex1:	Ex2:	Ex3:
Start byte: 15	Start byte: 120	Start byte: 15
Command: 121	Command: 121	Command: 122
Data: No	Data: No	Data: 189
Data: No	Data: No	Data: 3
Checksum: <u>186</u>	Checksum: <u>169</u>	Checksum: <u>134</u>

Standard Master package:

Byte count	Name
1	Start byte / Address
1	Command
2	Data (Cell Balance Voltage)
2	Data (PWM Steps / Voltage)
1	Checksum
7	Total bytes

Standard Slave package:

Byte count	Name
1	Start byte / Address
1	Data (Status byte)
1	Data (PWM value)
2	Data (Battery Voltage)
1	Checksum
6	Total Bytes

Annex B

1 Master version 1.03.05

The master is controlling the BMS charger and discharge current and gathering information from the slaves for cell balancing and protection.

1.1 Measurements

The master measures charge current, discharge current, battery voltage, internal temperature and battery temperature. All measurements are computed 100times/sec and average measurements are made each second.

1.2 Internal communication

The master controls the communication between master and all slaves. The following flow chart is repeated all the time in normal operation.

1. The master is sending a synchronisation pulse for the slaves to adjust there clock frequency for drifting over temperature.
2. Information about cell balancing is send from the master to all slaves.
3. The master gathers voltage information from all the slaves.

1.3 Single wire

Information about the status of the BMS and measured voltages of the slave is transmitted each second in normal operation.

Information from master

Bytes	Name	Description
4	Status bytes	Bit information
1	Cell count	Number of cells in the BMS
2	Battery voltage	Measured battery voltage in the BMS
2	Total battery voltage	Slave voltages added together
2	Cell voltage low	The lowest cell voltage
2	Cell voltage average	The average cell voltage
2	Cell voltage high	The highest cell volage
2	Fuel gauge	Fuel gauge counter
2	Discharge current	Discharge current
2	Charge current	Charge current
2	Temperature in	Temperature inside BMS
2	Temperature out	Battery temperature
2	Cell voltage steps	Total amount of cell balancing
2	Cell voltage pwm	Cell balance voltage for pwm

1.4 Power supply

In normal operation the 5 volt and the 16 volt is power supply running and stopped in sleep.

Flow chart when starting up the power supply:

1. Power up the 5 volt power supply and wait 80msec
2. Measure offset on Op amps.
3. Power up AUX_START and wait 100msec to charge the capacitors
4. Start PWM on driver and wait 100msec
5. Stop AUX_START and power supply's are running.

The PWM for the 16volt power supply is computed from the battery voltage and running with a fixed value to maintain an output voltage of 16 volt. The PWM is adjusted each 10msec.

1.5 Charging

The BMS is controlling the charging and protecting against over charging. To control the charging the charge mosfet can be on / off and is only on when charging is active. When connecting a charger and the master detect the charger on CHARGER_ACTIVE pin the mosfet is turn on and charging can begin. If the charge current is below 0.5A for 30sec charging is stopped and the charger has to be disconnected before it is re-enabled.

If the charge current is above limit charging is stopped and will retry 3 times before locking. To unlock, remove wakeup signal and charger for 10 sec.

If battery temperature exceeds limit, charging is stopped until the temperature is 10°C within limits, when automatically restarted.

If the BMS temperature exceeds limit, charging is stopped until the temperature is 10°C within limits, when automatically restarted.

1.6 Discharging

The BMS is controlling discharging and protecting against deep discharge by switching off the discharge mosfet. If one or more cells are discharged, the discharge mosfet is switched of and the master will go into sleep. Discharge is only active if wakeup signal is active and the master will wakeup and power up the control circuits, but only if the cell voltages are within limits discharge is activated. Otherwise the master will go back into sleep again after 30sec.

If the discharge current is above limit discharging is stopped and will rétry 3 times before locking. To unlock, remove wakeup signal and charger for 10 sec.

If battery temperature exceeds limit, discharging is stopped until the temperature is 10°C within limits, when automatically restarted.

If the BMS temperature exceeds limit, discharging is stopped until the temperature is 10°C within limits, when automatically restarted.

1.7 Fuel gauge

The fuel gauge is counting all currents going in and out of the battery. If the measured current value is below 0.3A it is not counted into the fuel gauge. The fuel gauge value is not allowed to go below zero or above 105% of specified capacity.

1.8 Sleep

If wakeup signal and charger has been missing for 30sec the BMS will go into sleep to minimize power consumption. The master wakeups when wakeup signal or charger is connected. If there is under voltage on one or more slaves, the master will only power up the control circuits and check the slave voltages and go back into sleep. To wakeup the master once more, first remove wakeup signal and reconnect.

1.9 Software settings

Power supply settings

Description	Value
Power supply start up voltage	25,55 V
Power supply output voltage	23 V
Power Supply Max PWM Pulse	90 %

Current settings

Description	Value
Charge current max slow	35A
Charge current max slow time	.1 sec
Charge current max fast	50A
Charge current min	0.5A
Discharge current max slow	150A
Discharge current max slow time	8 sec
Discharge current max fast	250A
Fuel gauge min detection	0.3A
Fuel gauge charge efficiency	100%
Battery capacity	80Ah

Voltage settings

Description	Value
Cell voltage min	2.8V
Cell voltage min reset	3.3V
Cell voltage max	4.1V
Cell voltage max reset	4.0V
Cell balance start voltage (single cell)	4.0V
Cell balance start voltage (average)	3.8V
Cell balance total power dispassion.	27W

Temperature settings

Description	Value
BMS internal temperature max	105°C
BMS internal temperature reset	90°C
Battery charging temperature min	-10°C
Battery charging temperature min reset	0°C
Battery charging temperature max	50°C
Battery charging temperature max reset	40°C
Battery discharging temperature min	-20°C
Battery discharging temperature min reset	-10°C
Battery discharging temperature max	70°C
Battery discharging temperature max reset	60°C

2 Slave version 1.03.01

The Slave is measuring the voltage of the cell and controlling the cell balance with information from the master.

2.1 Measurements

The slave measures the cell voltage each 9,5ms and compute an average value after 50 measurements. The cell balancing is stopped while measuring to avoid wrong value caused by voltage drop in cables. The measurement is transmitted to the master. The measurement is calibrated in production via communication.

2.2 Cell balance

The slave is making the cell balancing controlled values received from the master. The slave receives a voltage from the master, the difference between this value and measured value are multiplied and put in second. A fixed computed value is also received from the master and multiplied with the delta voltage used to compute the duty cycle for the cell balance PWM. If the cell voltage is lower than the received voltage fro the master the PWM is set to zero.

2.3 Communication

The slaves each the there own address for the master to recognize them and control the battery. The slave receive synchronise pulse and values for cell balance each second and the master gets voltage measurement and status information each second.

2.4 Sleep

If the communication from the master stops for more than 10sec the slave is put into sleep and waiting for communication to start again.

3 Internal Communication

The master controls and monitors all the slaves by a communication between slaves and master. The master handles the communication and the slaves only respond when asked. The communication is build upon a USART full duplex, running on 5kb with 9bit transmission. When the 9th bit is set, the byte is a command, otherwise its data. When receiving a package, it is stored in a buffer to calculate if the checksum is the same as received. Only if the checksum matches it will use the package.

3.1 Start byte / Address

In the beginning of all packages, there has to be a start byte containing the address of the slave witch is receiving or transmitting. It is possible to connect up to 120 slaves to the master. The slaves will have there on address given in production for the master to access them. The addresses of the slaves will start from 1 and up to the number of slaves connected.

List of addresses: (9th bit set)

Value	Address
0	Global address
1-120	Slave address

3.2 Command

The master sends packages to the slaves to give inform or give instructions. The command is always the first byte after the start byte. There are always 3 commando bytes in one package (Start byte, Command and Checksum)

List of commands: (9th bit set)

Value	Name	Description
0-120	Start byte	Start byte and address of the slaves
121	Send info to master	Return data to master
122	Info from master	Average battery voltage
123	Error check	Check if one of the slaves has a error
124	Enter sleep-mode	Put the slaves into sleep-mode
125	Sync pulse	The master will transmit a sync pulse
126	Calibration	The Master transmit the real cell voltage and the slaves adjust the measured voltage
128-255	Checksum	

3.3 Data

In some of the Packages it is necessary to transfer a few data bytes. When transmitting a data byte, the parity bit has to be low to indicate, it is a data byte and not a command. The receive buffer in the slaves is very small and it is only packages is possible to transmit or receive packages up to 16 bytes of data. When transmitting data values of 2 bytes, LSB is sent first.

3.4 Checksum

The checksum is the last byte of the packages and data coming after what is ignored only a new start byte in a new package is accepted. Since the check sum only calculate with 8bits a value 25 is added for each parity bit. Every time the checksum has overflow the checksum is incremented one time. The checksum it self is not added to the checksum and not taken into calculation. The checksum can only have the value from 128 to 255, if the value is out of range two different values is added depending of the checksum value.

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Parity	25
Each byte	1
Overflow	1
0-122	133 (128+5)
123-127	10
128-255	No add

Ex1:	Ex2:	Ex3:
Start byte: 15	Start byte: 120	Start byte: 15
Command: 121	Command: 121	Command: 122
Data: No	Data: No	Data: 189
Data: No	Data: No	Data: 3
Checksum: <u>186</u>	Checksum: <u>169</u>	Checksum: <u>134</u>

Standard Master package:

Byte count	Name
1	Start byte / Address
1	Command
2	Data (Cell Balance Voltage)
2	Data (PWM Steps / Voltage)
1	Checksum
7	Total bytes

Standard Slave package:

Byte count	Name
1	Start byte / Address
1	Data (Status byte)
1	Data (PWM value)

2	Data (Battery Voltage)
1	Checksum
6	Total Bytes

CLAIMS

1. A battery management system (BMS) for the controlling and monitoring of a plurality of lithium ion cells or similar battery cells including lithium molybdenum, nickel, cadmium and PB cells, the BMS including a central controlling
5 microcontroller (14) and a plurality of control circuits (32, 36) connected with a respective battery cell (12) and serving to individually monitoring the charging of the individual respective battery cell and at the time of reaching a maximum charging state establishing a shunt across the individual battery cell for allowing a continued charging of the remaining battery cells and at the same time communicating to the
10 central controlling microcontroller (14) a message representing that the maximum charging state has been reached and serving during discharging of the battery to monitor the state of the individual respective battery cell and to inform the central controlling microcontroller (14) in case a minimum charging state has been reached for causing the central controlling microcontroller (14) to disconnect the battery from
15 the load in order to prevent excessive discharging of the individual battery cells.
2. A battery management system according to claim 1, where said control circuits comprise cell balancing means (32) and slave sensing means (36).
- 20 3. A battery management system according to claim 1 or 2, where said slave sensing means comprise a microcontroller.
4. A battery management system according to any of the preceding claims, furthermore comprising temperature sensors for continuous monitoring of the
25 temperature of the cells and / or in the cell balancing and sensing and control circuits respectively allowing the central control unit to reduce charging current in case of high temperature.
5. A battery management system according to any of the preceding claims,
30 furthermore comprising means (26, 22) for shut down of the charging / discharging of the cells controlled by said central controlling microcontroller (14) in the case of overload or short circuit of the battery.

6. A battery management system according to any of the preceding claims, furthermore comprising means (28, 30) for monitoring the current through the plurality of cells (12), whereby a shunt resistor located in series with the cells is used.

5

7. A battery management system according to any of the preceding claims, furthermore comprising a fuse for protection in case of overload or short circuit of the battery.

10

8. A battery management system according to any of the preceding claims, furthermore comprising a power supply unit for supplying the control unit.

9. A battery management system according to any of the preceding claims, furthermore comprising a fuel gauge for continuous monitoring of the battery level.

15

10. A method for controlling and monitoring a plurality of lithium ion cells or similar battery cells including lithium molybdenum, nickel, cadmium and PB cells, the method comprising:

20

- during charging of said cells:
 - Adjusting the voltage/current with respect to the cell condition to achieve optimum charge performance and bypassing one or more individual cells for allowing continued charging of the remaining cells when said one or more individual cells has reached the top voltage;

25

- during discharging of said cells:
 - monitoring the voltage of each individual cell until a minimum value has been reached in one or more individual cells at which time all the cells are shut down to prevent said one or more cells having reached the minimum voltage level from being harmed or ruined by continued discharging;

30

thereby ensuring the highest performance of the charging/discharging processes and preventing harm to the individual cells.

11. A method according to claim 10, where the temperature of one or more individual cells and/or or the cell balancing and sensing circuits and/or of further circuits including the central microprocessor are monitored, thereby to reduce charging current in case of an unacceptable high temperature is reached in one or
5 more of said cells and/or circuits.

12. A method according to claim 10 or 11, where charging/discharging of the cells is interrupted in case of overload or short circuit of the battery.

10 13. A modular battery management system comprising a central control system and a plurality of individual cell control systems for controlling and monitoring charging and/or discharging of individual cells, the plurality of individual cell control systems communicating with the central control system through wired analogue or digital
15 communication means or through wireless analogue or digital communication means.

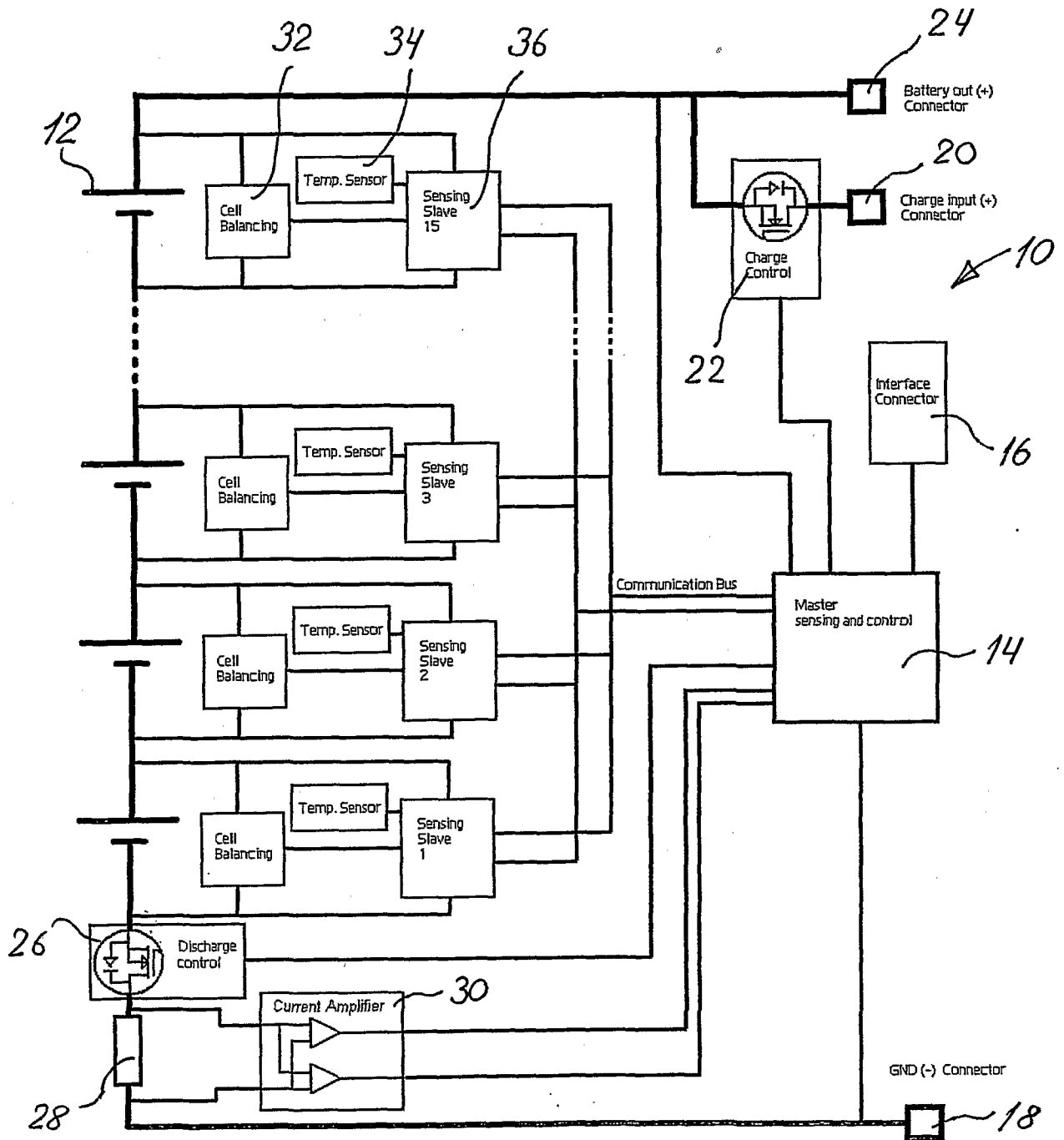


Fig. 1

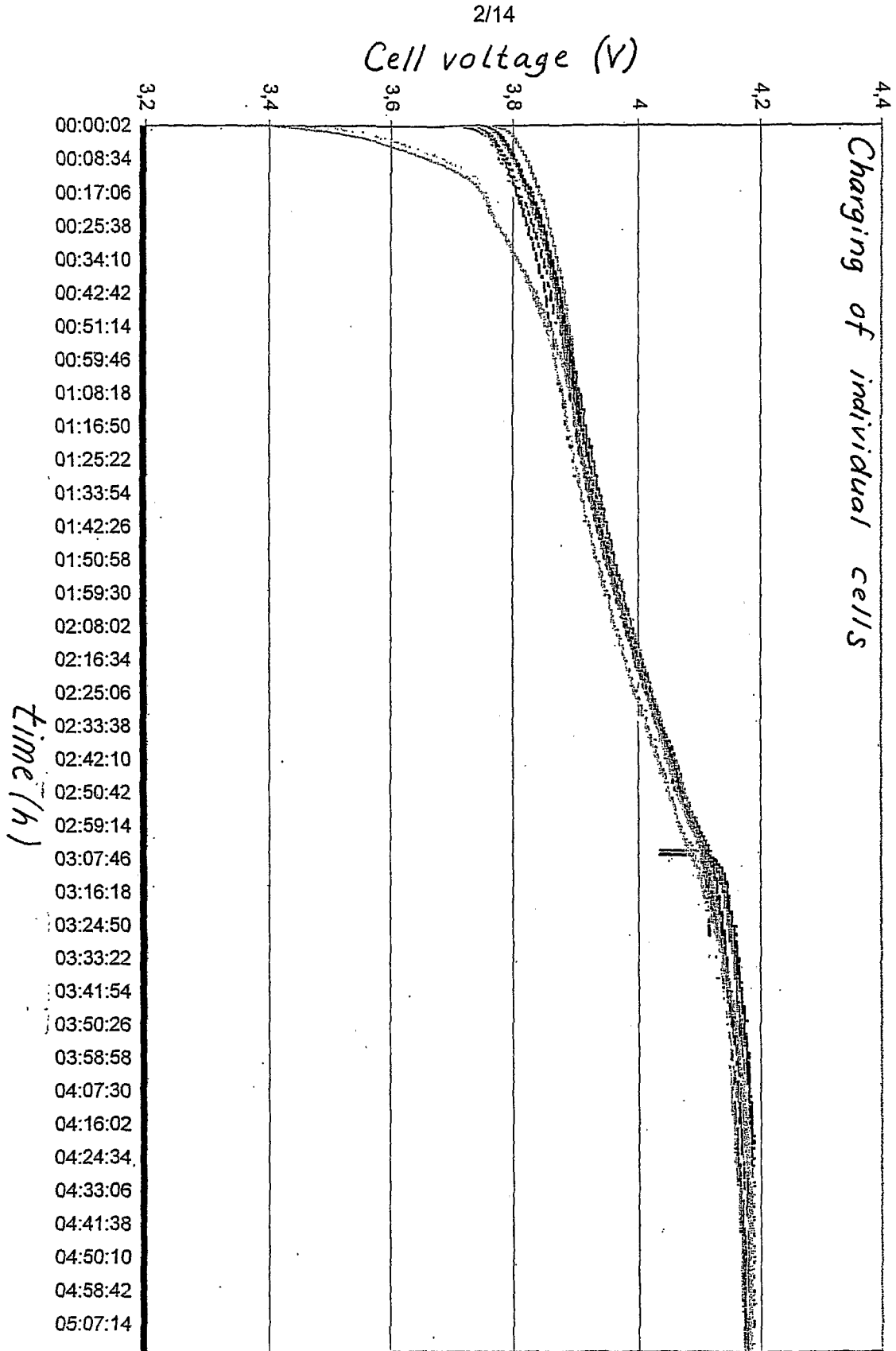
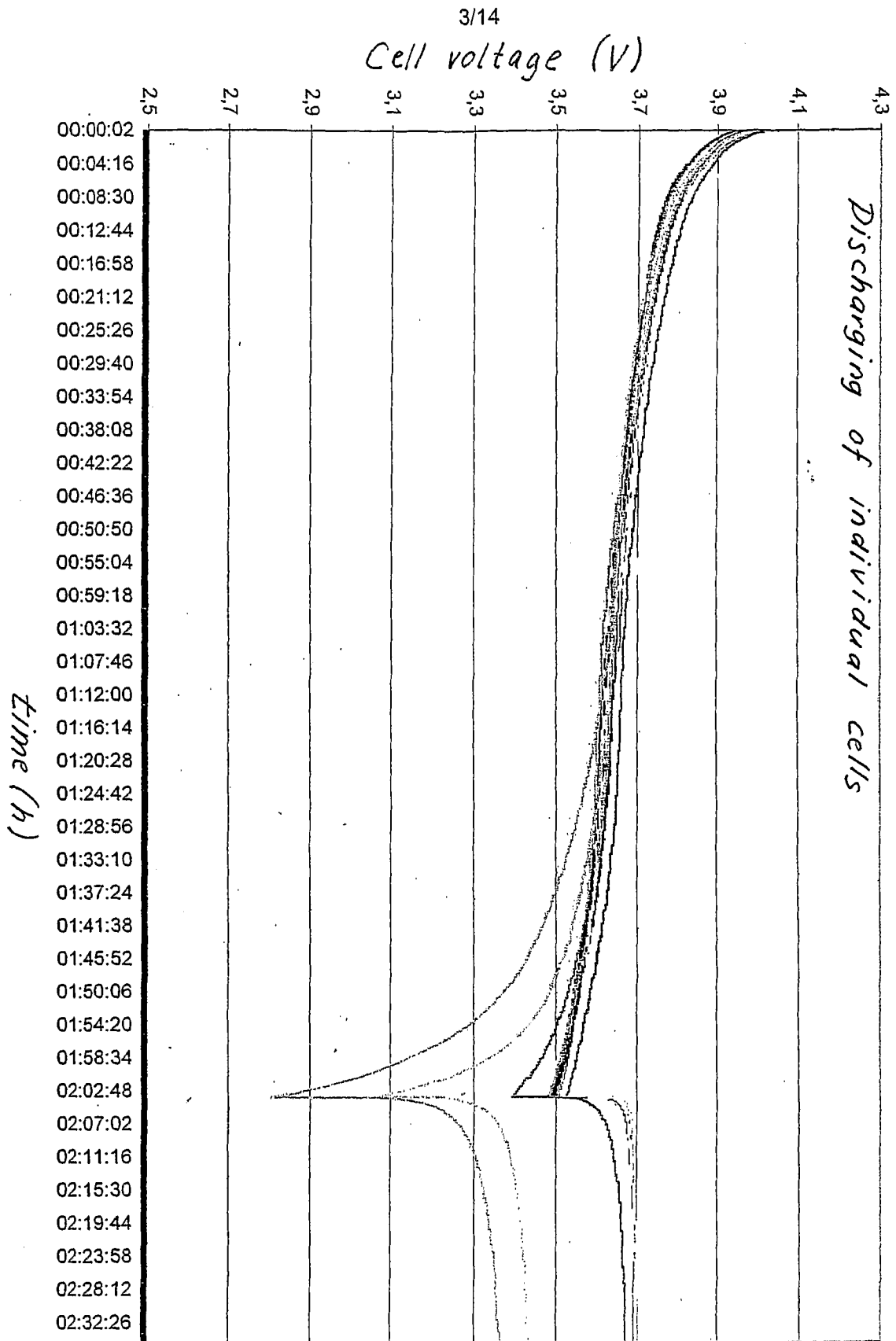


Fig. 2



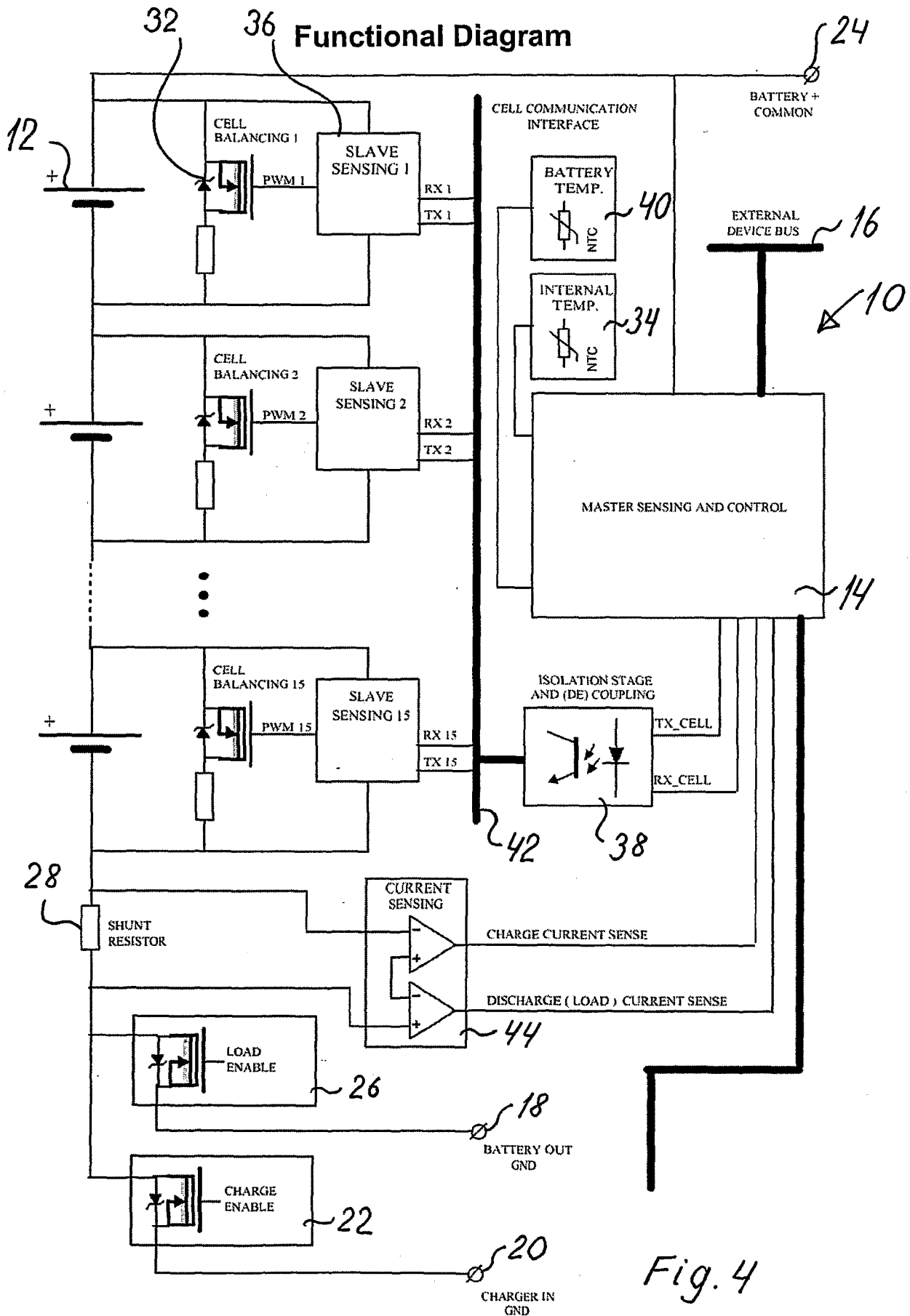


Fig. 4

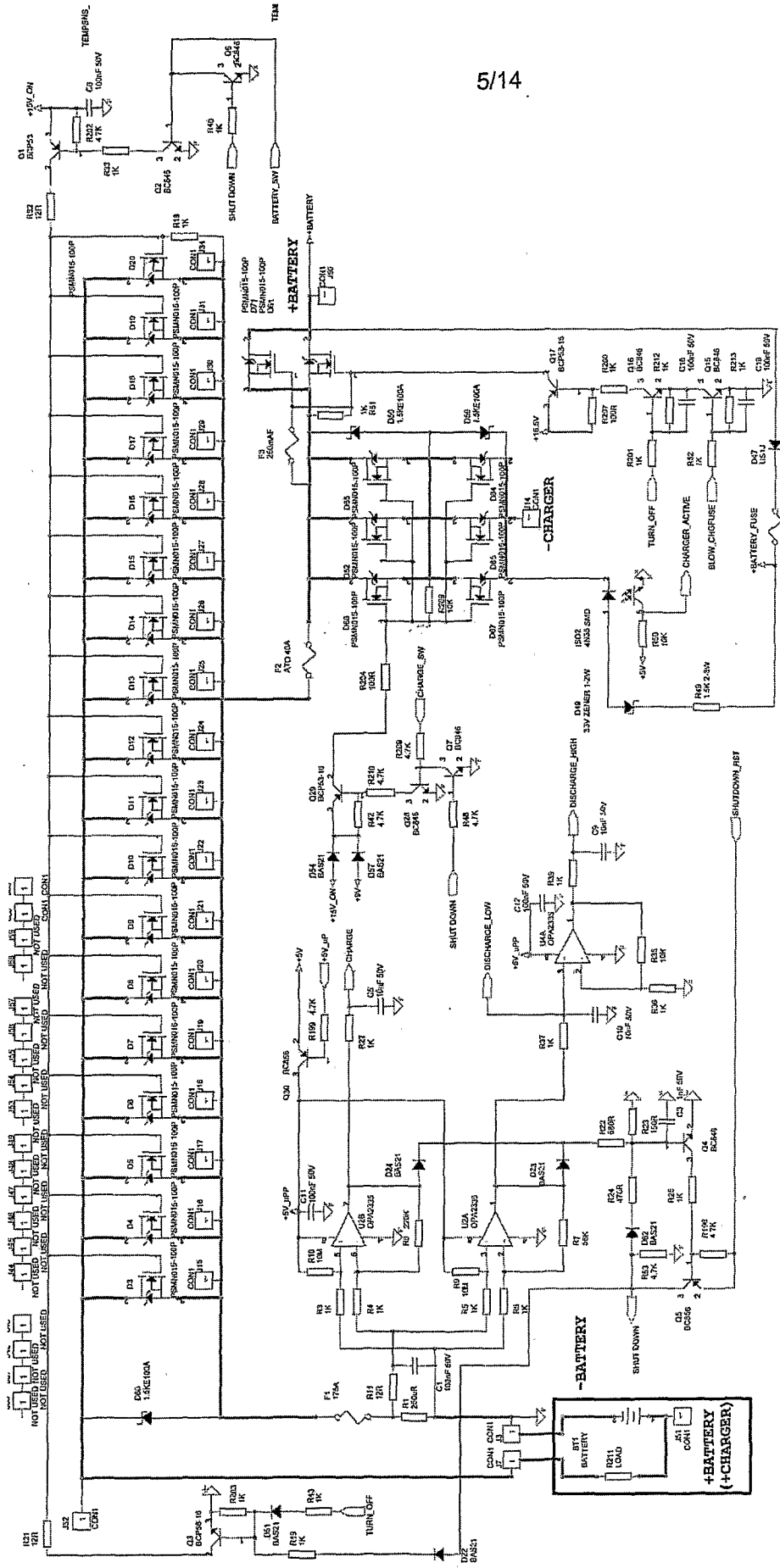


Fig. 5

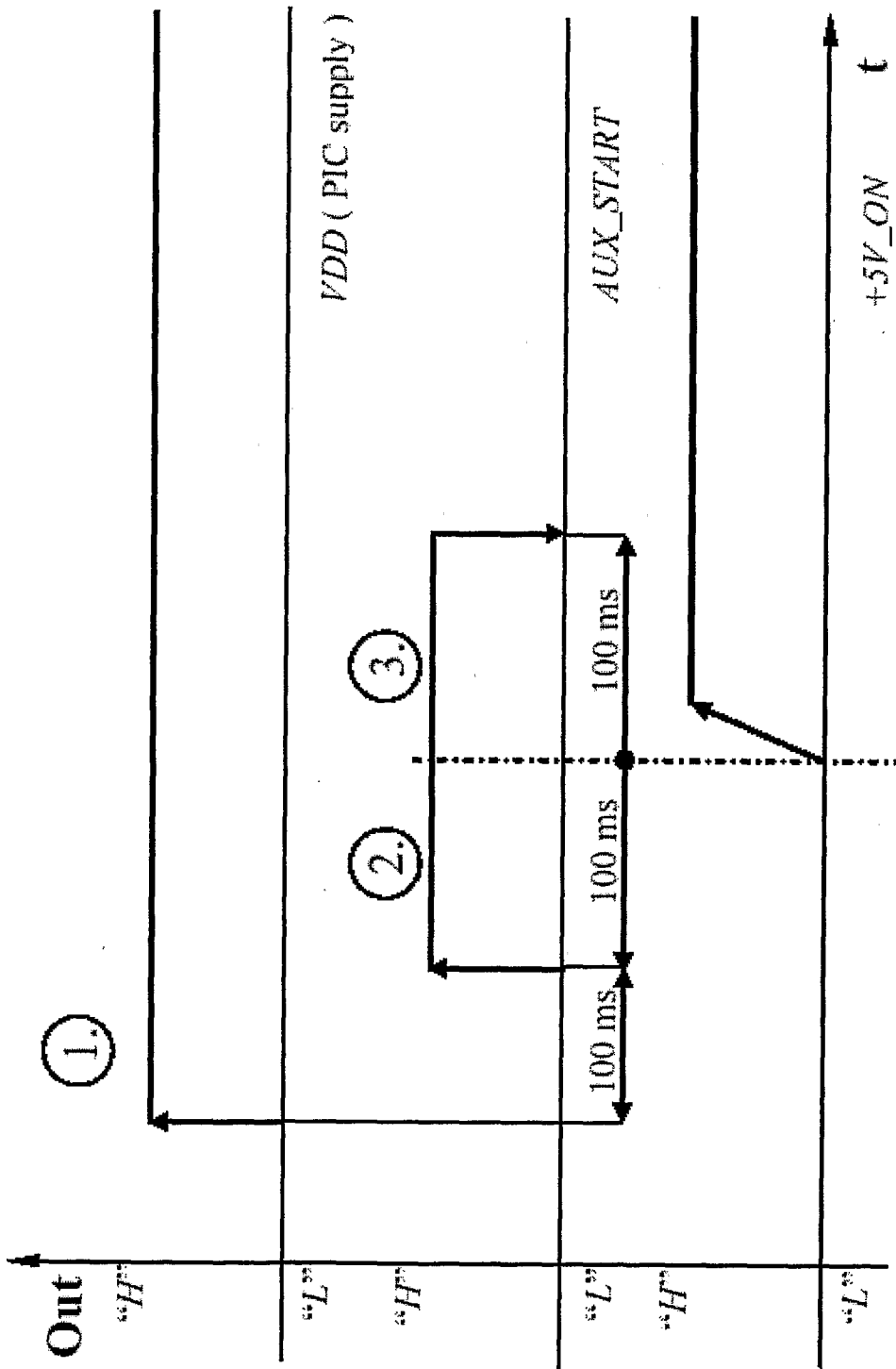


Fig. 7

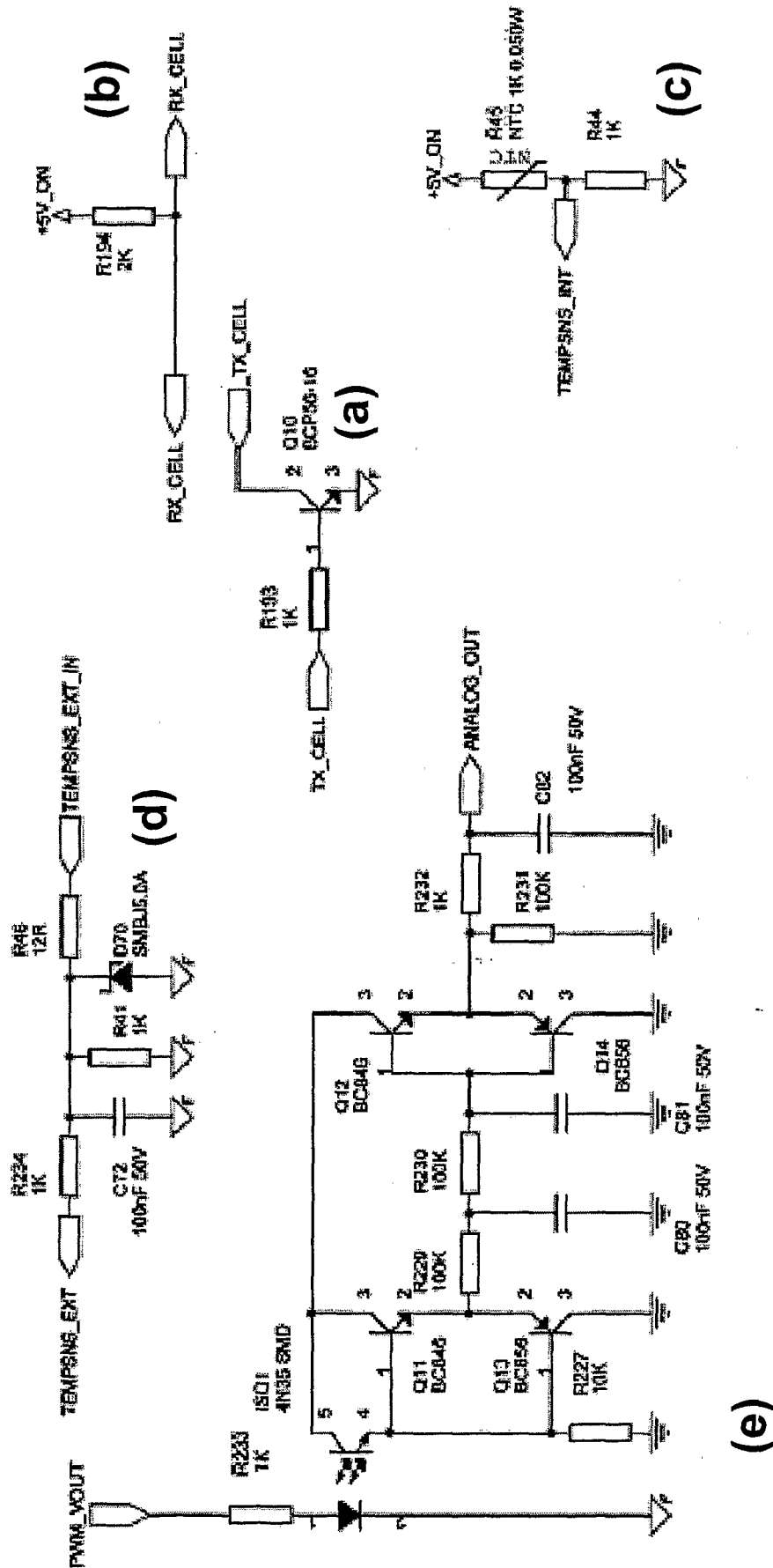


Fig. 8

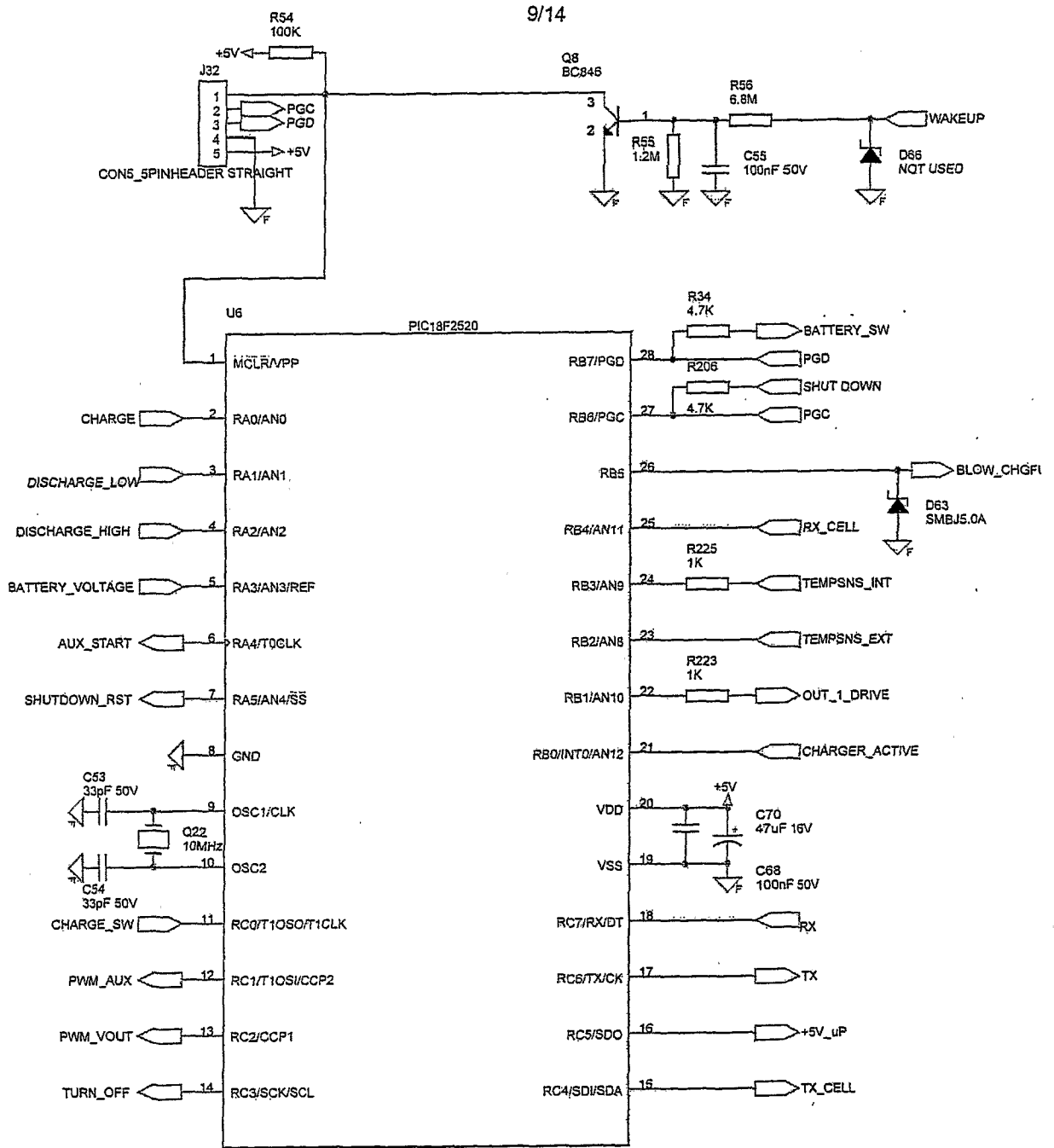


Fig. 9

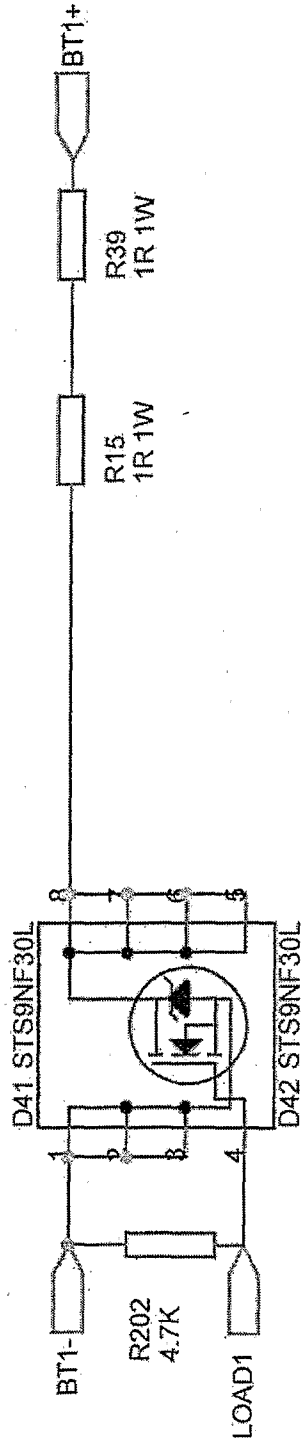


Fig. 10a

11/14

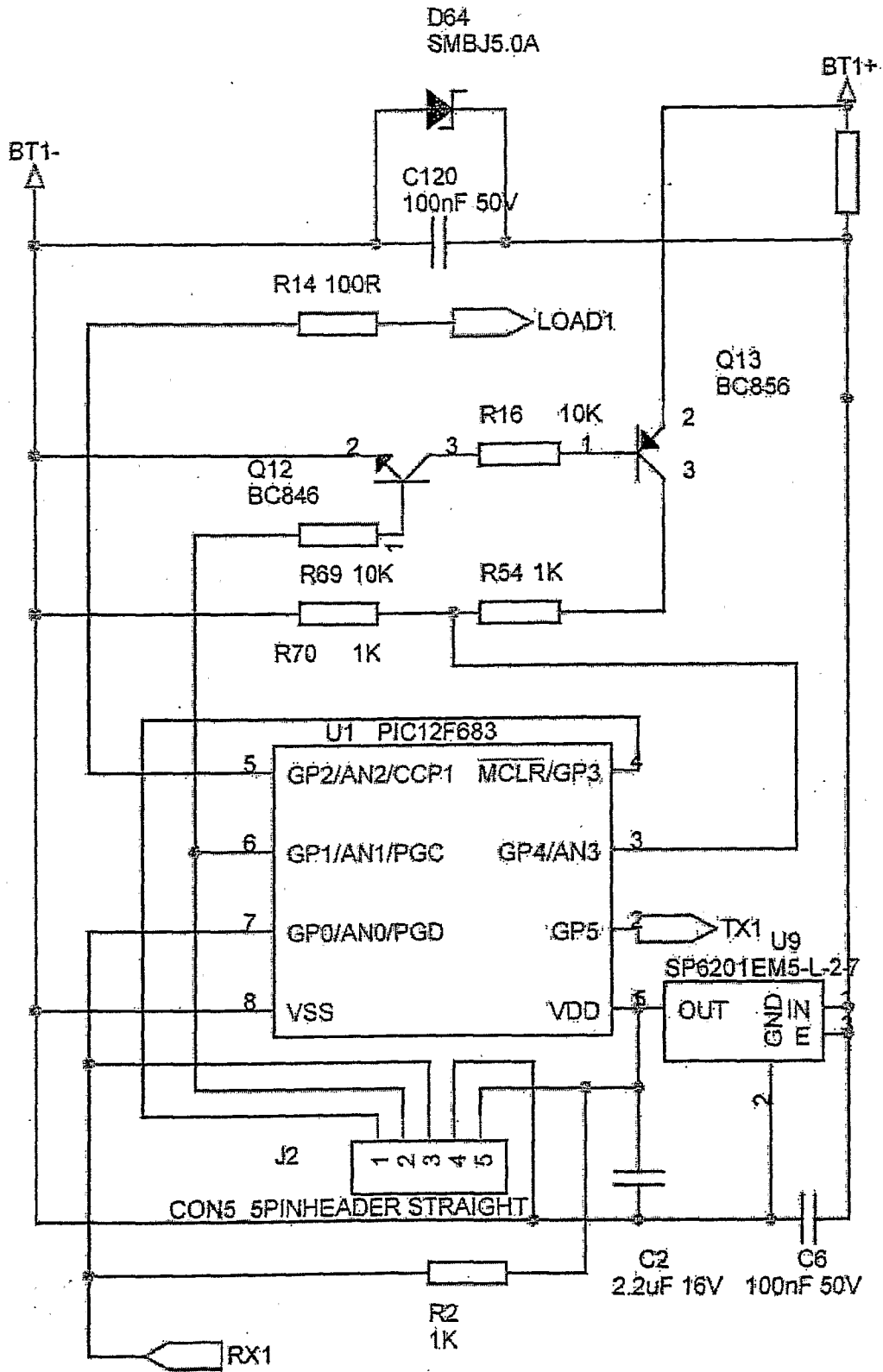


Fig 10 b

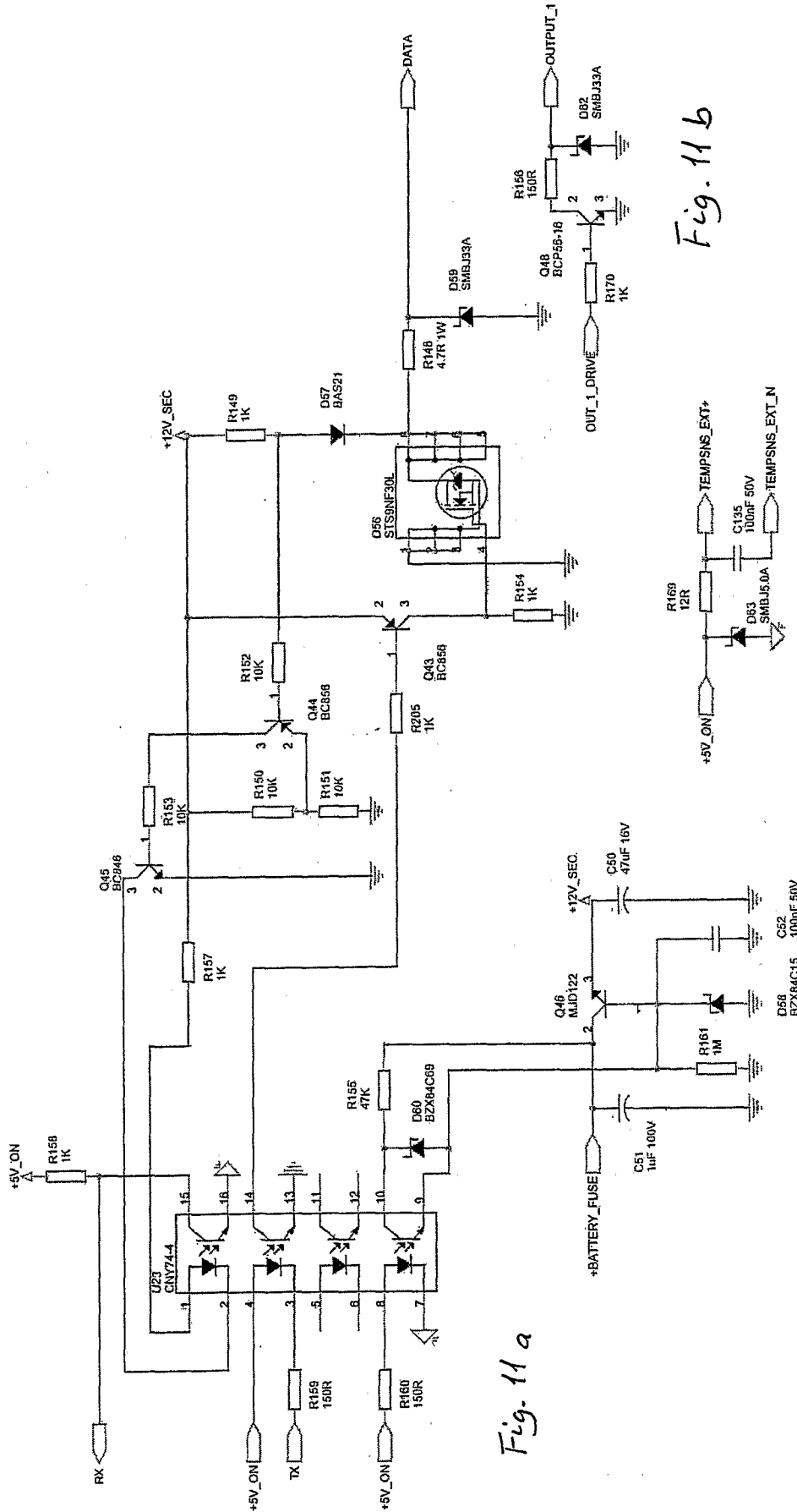


Fig. 11b

Fig. 11c

Fig. 11a

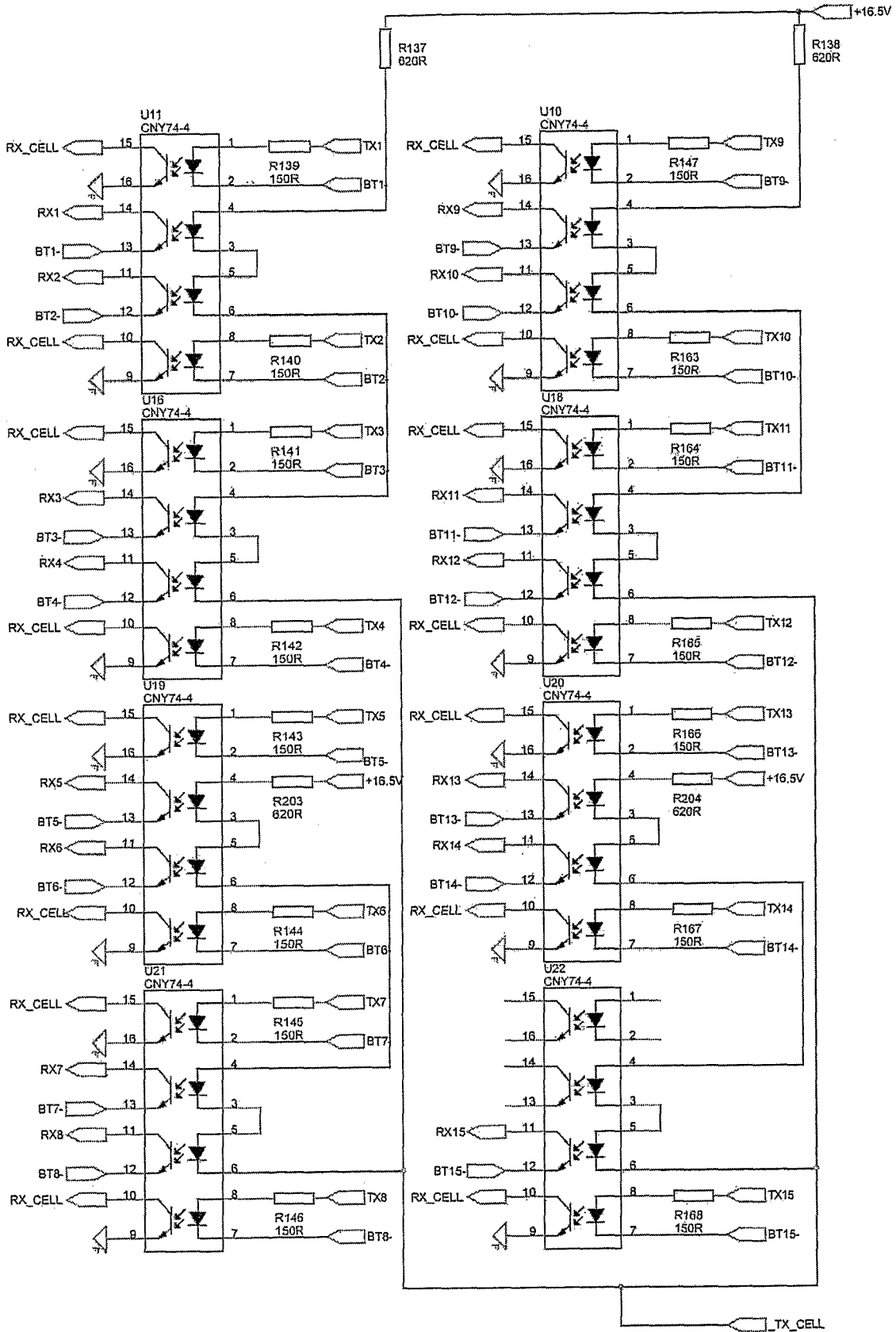


Fig. 12

BMS Main Connectors Layout

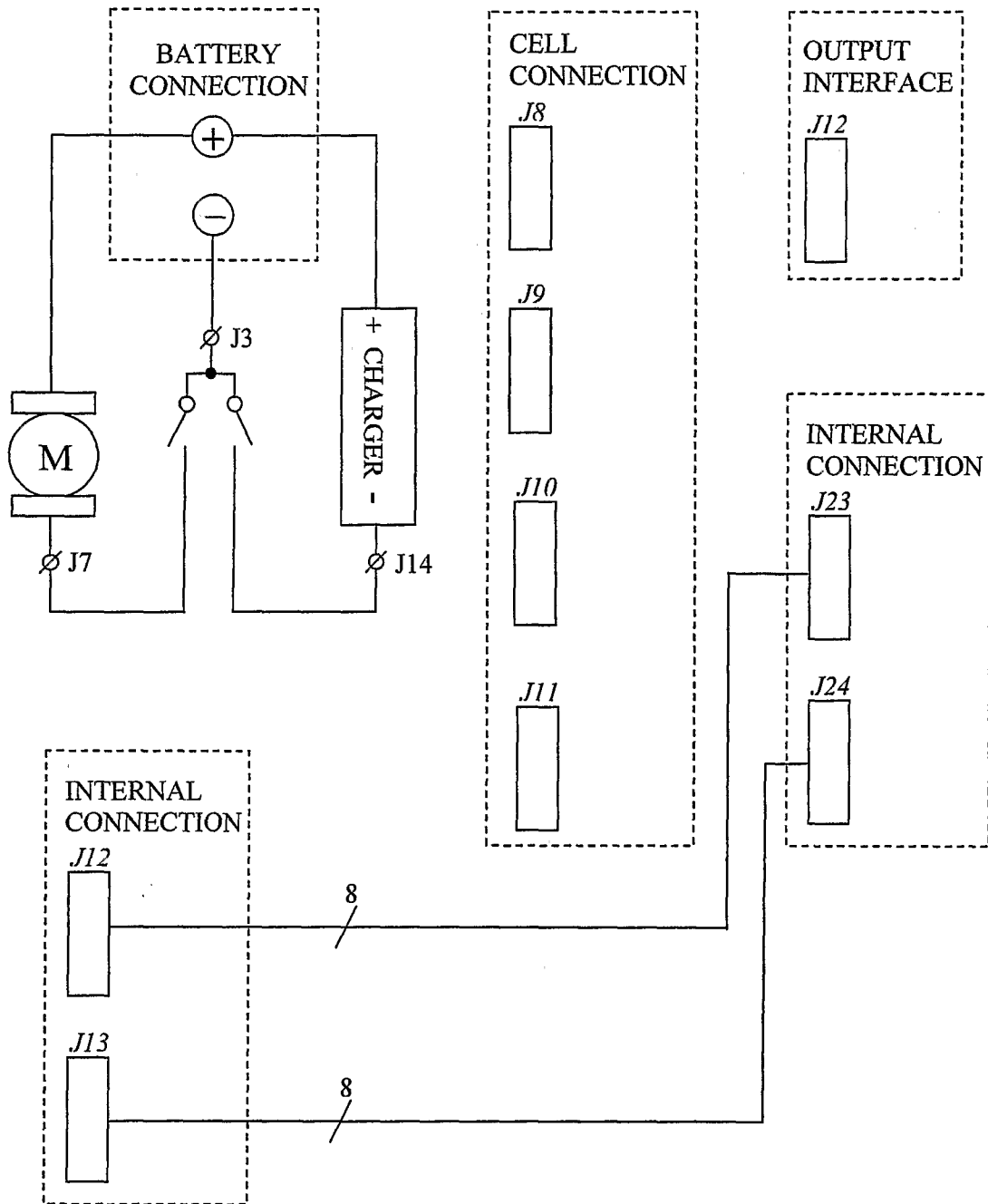


Fig. 13

INTERNATIONAL SEARCH REPORT

International application No
PCT/DK2007/000492

A. CLASSIFICATION OF SUBJECT MATTER
INV. H02J7/00

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
H02J

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

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Y	paragraph [0003] - paragraph [0023]; claims 1,7; figure 2	7-9
Y	GB 2 420 235 A (SANYO ELECTRIC CO [JP]) 17 May 2006 (2006-05-17)	7
Y	paragraph [0036] - paragraph [0038]	
Y	US 2003/042870 A1 (YAU KWOK WONG [HK] ET AL) 6 March 2003 (2003-03-06)	8
Y	figure 2	
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	page 15, paragraph 5	
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Further documents are listed in the continuation of Box C.

See patent family annex.

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Date of the actual completion of the international search

21 February 2008

Date of mailing of the international search report

04/03/2008

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NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
Fax: (+31-70) 340-3016

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International application No
PCT/DK2007/000492

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
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