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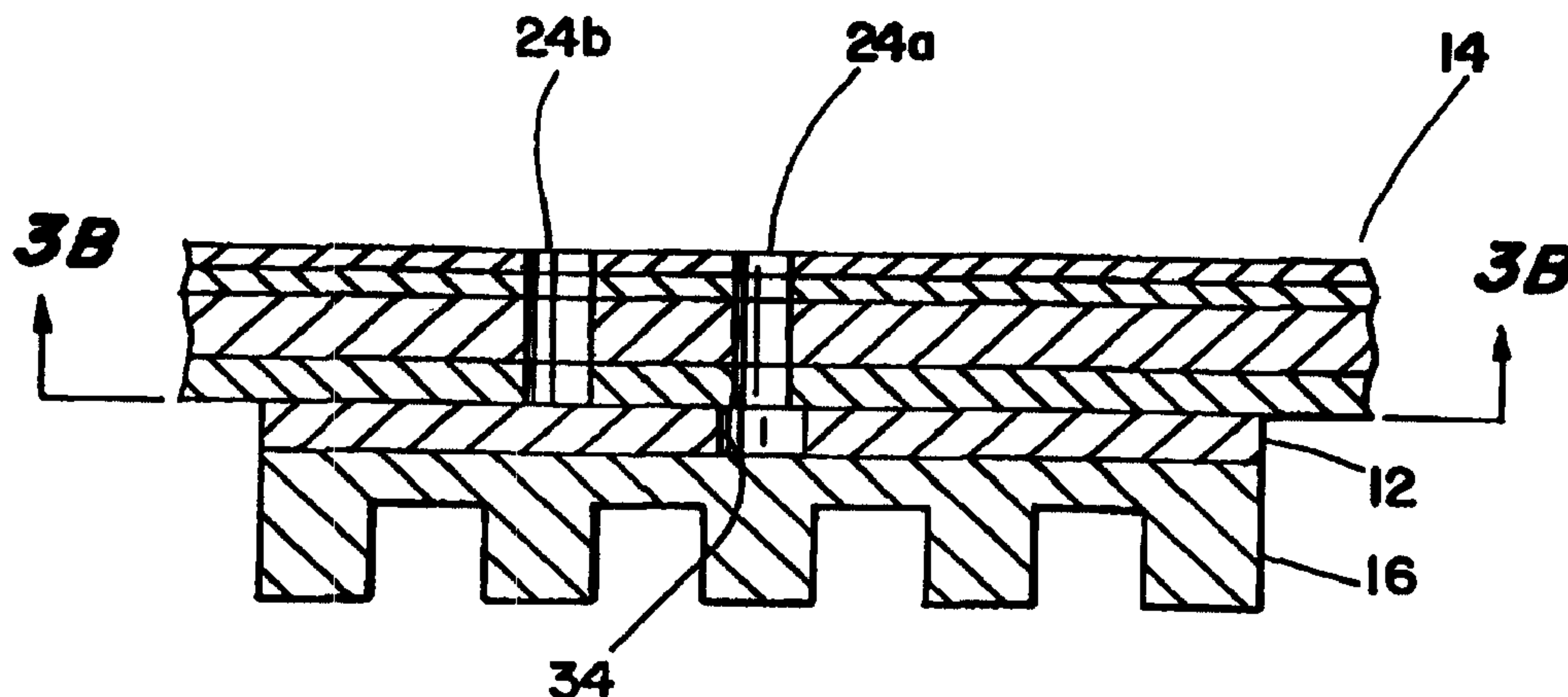
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(54) **BOITIERS MICRO-ELECTRONIQUES ET PROCEDES
D'ENCAPSULATION COMPRENANT UNE PLAGE THERMO
ET ELECTROCONDUTRICE**

(54) **MICROELECTRONIC PACKAGES AND PACKAGING
METHODS INCLUDING THERMALLY AND ELECTRICALLY
CONDUCTIVE PAD**



(57) La présente invention concerne une plage thermo et électroconductrice disposée entre une carte de circuit électronique (PCB) et un puits de chaleur, dans une station de base de téléphone cellulaire. La plage comprend au moins un orifice qui recouvre une ou plusieurs traversées de signal sur un plan de masse de la PCB. Les ouvertures de la plage sont plus grandes que chacune des traversées sous-jacentes de signal de façon à isoler électriquement, du matériau conducteur de la plage et du puits de chaleur, les traversées de signal. La plage permet au traversées mises à la masse sur un plan de masse de PCB de mettre le puits de chaleur à la masse.

(57) A thermally and electrically conductive (TEC) pad is disposed between a PCB and a heat sink in a cellular telephone base station. The TEC pad includes at least one aperture that overlies one or more signal vias on a ground plane of the PCB. The TEC pad apertures are larger than any underlying signal vias in order to electrically isolate the signal vias from the conductive material of the pad and the heat sink. The TEC pad allows ground vias on a PCB ground plane to ground to the heat sink.

ABSTRACT OF THE DISCLOSURE

A method and a system for measuring the mechanical vibrations of an object. In order to simplify the electronic circuit necessary for the measurement chain and to reduce
5 its costs, this method and this system are characterized in that they comprise the processing of an input signal, representative of an acceleration or of a velocity related to a mechanical vibration of said object, said input signal having a frequency spectrum comprising a so-called low
10 frequency band, situated below a so-called transition frequency, and a so-called high frequency band, situated above said transition frequency, said method and system carrying out said processing of said input signal by means of an electronic circuit for producing an output signal
15 which, in said low frequency band, corresponds to the mathematical integral over the time of said input signal, and, in said high frequency band, corresponds to said input signal.

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20 (FIG. 1)

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METHOD AND SYSTEM FOR COMBINED VIBRATION MEASUREMENTSBACKGROUND OF THE INVENTION

5 1. Field of the Invention

The present invention is related to a method for measuring mechanical vibrations of an object. Furthermore, the invention is related to a system for measuring such vibrations of an object.

10 2. Description of the Prior Art

The frequency spectrum of a signal representative of the vibrations of, e.g., an axial compressor or any other rotational industrial or aeronautical machine shows generally two rather different domains:

15 1) At low frequencies, for example in a frequency range lower than 1000 or 2000 Hertz, the vibration signal has a rather low level in terms of acceleration and is for example inferior to 1 m/s².

20 In the fields of aeronautics and industry, a low frequency vibration signal is transformed or measured in terms of vibration velocity which is representative of the vibration energy, often destructive, which acts on a rotary machine.

25 The ranges of low frequencies and the levels of acceptable vibration signals in these ranges are broadly standardized in function of the machine, for example:

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- according to ISO standard No. 2954/VDI2056, between 10 and 1000 Hertz;
- according to API standard No. 670, between 10 and 2500 Hertz, etc.

5 At low frequencies, the level of a vibration signal at the
fundamental rotational frequency constitutes a particular
interest in counterbalancing principal rotors (for example
in the case of a blower, a compressor and a turbine, a
propeller, etc.). The level of the vibration signal at
10 harmonics at low frequencies has also a certain interest in
certain analyses.

2) At medium and high frequencies (for example at
frequencies higher than 1000 Hertz), lines corresponding for
example to gearing vibrations, to multiples and modulation
15 of such lines, lines corresponding to the passage of turbine
blades, to signatures of rolling bearings, etc., can be
found in the frequency spectrum of a signal representative
of the vibrations of an object.

- In the field of industry, a vibration signal of
20 medium and high frequencies is measured in terms of
the vibration acceleration, and its level is
relatively high and often greater than to 10 m/s².
- In the fields of civil and, above all, military
aeronautics, the vibration acceleration at high
25 frequencies may attain 10,000 m/s²; such vibrations
can provoke saturation of the first amplification
stage in the measurement chain.

The above-indicated strongly pronounced differences between
the features of a low frequency vibration signal and the

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features of the same signal at medium and high frequencies result in the necessity, for certain applications as, for example, the measurement of vibrations acting upon a turbo-propeller group of an aircraft, to install two different
5 measurement chains, namely a first measurement chain for monitoring the low frequency component of the vibrating signal corresponding to the vibrations related to the rotation of the propeller, and a second measurement chain for monitoring, in the field of high frequencies, the
10 component of the vibrating signal corresponding to the vibrations of the reduction gear. Such a solution has certain disadvantages, namely not only the price increase of the measurement system but also a lower reliability of such a system, since it is more complex and, as a consequence,
15 the probability of defects is higher.

SUMMARY OF THE INVENTION

Therefore, the aim of the present invention is to provide a method and a system for measuring mechanical vibrations which allows to overcome the above-discussed drawbacks.

20 According to a first aspect of the invention this aim is attained with a method for measuring the mechanical vibrations of an object, comprising
electronically processing an input signal,
representative of an acceleration related to a mechanical
25 vibration of said object and having a frequency spectrum comprising a low-frequency band situated below a transition frequency and a high frequency band situated above said transition frequency,
said processing being carried out by means of an
30 electronic circuit which is adapted to provide an output signal which

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within said low-frequency band corresponds to the mathematical integral over the time of said input signal, i.e. to the vibration velocity of said object, and

within said high-frequency band corresponds to the input signal, i.e. to the vibration acceleration of said object.

According to a second aspect of the invention, the above mentioned aim is attained with a method for measuring the mechanical vibrations of an object, comprising

electronically processing an input signal, representative of a velocity related to a mechanical vibration of said object and having a frequency spectrum comprising a low-frequency band situated below a transition frequency and a high frequency band situated above said transition frequency,

said processing being carried out by means of an electronic circuit which is adapted to provide an output signal which

within said low-frequency band corresponds to the mathematical integral over the time of said input signal, i.e. to the vibration displacement of said object, and

within said high-frequency band corresponds to the input signal, i.e. to the vibration velocity of said object.

According to a third aspect of the invention, the above mentioned aim is attained with a system for measuring mechanical vibrations of an object, comprising

(a) a transducer mounted on said object and being capable of providing at its output an input signal which is representative of an acceleration related to a mechanical vibration of said object, said input signal comprising a low-frequency band situated below a transition frequency and a high frequency band situated above said transition

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frequency, and

(b) an electronic circuit having an input port, connected to the output of said transducer, and an output port, said circuit being adapted to process said input
5 signal to yield an output signal which within said low-frequency band corresponds to the mathematical integral over the time of said input signal, and which within said high-frequency band corresponds to said input signal.

According to a fourth aspect of the invention, the above
10 mentioned aim is attained with a system for measuring mechanical vibrations of an object, comprising

(a) a transducer mounted on said object and being capable of providing at its output an input signal which is representative of a velocity related to a mechanical
15 vibration of said object, said input signal comprising a low-frequency band situated below a transition frequency and a high frequency band situated above said transition frequency, and

(b) an electronic circuit having an input port,
20 connected to the output of said transducer, and an output port, said circuit being adapted to process said input signal to yield an output signal which within said low-frequency band corresponds to the mathematical integral over the time of said input signal, and which within said high-
25 frequency band corresponds to said input signal.

The main advantage of the invention is that it allows to obtain, by means of a sole transducer and a sole measurement chain, a single output signal which, in the range of low frequencies, corresponds to the vibration velocity, and in
30 the range of medium and high frequencies, to the vibration acceleration. The information thus obtained on the vibration velocity may be used to quantify the severity of vibrations

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at low frequencies and to take the necessary measures for the protection of the machine, whereas the information obtained on the vibration acceleration may be used above all for the diagnostic and the health of mechanical components
5 such as bearings, blade arrays and gearings which generate in particular the high frequency vibrations when their mechanical condition degrades.

Furthermore, the invention offers the following advantage:

It permits either to increase the level of the signal at low
10 frequencies where the problem of background noise often limits the behavior of the measurement chains, or to decrease the amplitudes at high frequencies which could provoke the saturation in the following stages of the measurement chain. In both cases, this advantage provides an
15 optimization of the signal dynamics. In a simple example of an industrial turbo-generator, it has been calculated that the necessary dynamic was optimized by about 30 dB. This great improvement reduces the performance requirements downstream the collecting chains and allows for example

20 - to simplify the attenuators or amplifiers at the input port of the signal processing unit, and

- to reduce the resolution performance of the analog-digital converters (ADC) in terms of required bits.

The invention thus allows to reach simultaneously two goals,
25 namely, on one hand, an improvement of the dynamics in the processing of the measurement signal, and, on the other hand, the supply of two physical quantities of current use in vibration analysis, namely acceleration and velocity, and this on a single output signal stemming from a sole
30 transducer.

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Still another advantage of the invention is the fact that it allows to increase the productivity of measurements which can be carried out by means of a system for measuring mechanical vibrations. In fact, for dynamic reasons during
5 the signal processing, it has been necessary until now to carry out two separated analyses: one within the range of low frequencies, and the other in the range of medium and high frequencies. Each one of these analyses consists in a type FFT (Fast Fourier Transformation) processing which is a
10 long-lasting one for the operators and the processor. Since the present invention allows to modify or adapt the signal dynamics, the analysis of the measurement signal can be carried out in a single run, resulting in a gain of time and in a simplification in the management of the vibration
15 database.

It is possible, through a repeated application of the method according to the invention, to obtain a single output signal carrying information on three physical quantities such as displacement, velocity and acceleration. The applications of
20 this variant are, however, more limited.

Embodiments of the invention will now be described by way of Examples in referring to the attached drawings.

BRIEF DESCRIPTION OF THE DRAWING

In the drawings,

25 FIGURE 1 shows the block diagram of a first system according to the invention,

FIGURE 2 shows a block diagram of a first embodiment of a system whose block diagram is shown in FIG. 1,

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FIGURE 3 shows a block diagram of a second embodiment of a system whose block diagram is shown in FIG. 1,

FIGURE 4 shows a block diagram of a third embodiment of a system whose block diagram is shown in FIG. 1,

5 FIGURE 5 shows a block diagram of a second system according to the invention,

FIGURE 6 shows a block diagram of a first embodiment of a system whose block diagram is shown in FIG. 5,

10 FIGURE 7 shows a block diagram of a second embodiment of a system whose block diagram is shown in FIG. 5,

FIGURE 8 shows the typical frequency response curve of a system according to the invention.

DETAILED DESCRIPTION OF THE INVENTION

15 EXAMPLES OF A FIRST SYSTEM AND OF A FIRST METHOD ACCORDING TO THE INVENTION

As it has been shown in the block diagram of FIG. 1, a first system according to the invention for the measurement of mechanical vibrations of an object comprises a transducer 11 which is mounted on an object subjected to vibrations, and
20 an electronic circuit 13.

The transducer 11 has an output port 12 on which it supplies a signal representative of the acceleration of the vibration movement of the object. This signal has a frequency spectrum comprising a band called low frequency band situated below a
25 frequency called transition frequency, and a second band called high frequency band, situated above said transition frequency.

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The electronic circuit 13 has an input port 14, connected to the output port 12 of the transducer 11, and an output port 15. The circuit 13 is used to process the signal supplied by the transducer 11 at its output port 12. The circuit 13
5 supplies an output signal at its output port 15 which, in said low frequency band, corresponds to the mathematical integral over the time function of the output signal of the transducer 11, and within said high frequency band, corresponds to said output signal of the transducer 11. The
10 output signal supplied at the output port 15 of the electronic circuit 13 is therefore composed in such a manner that, within said low frequency band, it corresponds to the velocity of the vibration movement of the object, and within said high frequency band, it corresponds to the acceleration
15 of the vibration movement of the object.

The measurement system according to FIG. 1 thus allows the implementation of a first method according to the invention, characterized in that it comprises:

the processing of an input signal, representative of an
20 acceleration related to a mechanical vibration of the examined object, said input signal having a frequency spectrum comprising a so-called low-frequency band situated below a transition frequency, and a so-called high frequency band situated above said transition frequency, said method
25 carrying out said signal processing in an electronic circuit for producing an output signal such as the signal supplied at the output port 15 of the electronic circuit 13, said output signal corresponding, within said low-frequency band, to the mathematical integral over the time of said input
30 signal, i.e. to the vibration velocity of said object, and corresponding, within said high-frequency band, to the input signal, i.e. to the vibration acceleration of said object.

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FIRST EXAMPLE OF A SYSTEM ACCORDING TO FIG. 1

FIG. 2 shows the block diagram of a first example of a measurement system whose block diagram is shown in FIG. 1. The system represented in Fig. 2 comprises a transducer 31
5 mounted on an object which is subjected to vibrations (this object is not shown in Fig. 2), and an electronic circuit 33 for the processing of the output signal supplied by the transducer 31.

The transducer 31 is arranged as an accelerometer and
10 supplies an electric charge Q as an output signal on line 32. This charge Q is proportional to the acceleration of the object over the entire interesting frequency range.

The electronic circuit for processing the output signal, supplied by the transducer 31 on line 32, comprises two
15 branches 33, 34. Each one of these branches contains a charge divider C_1 and, respectively, C_2 allowing to optimize the distribution of the signal dynamic, followed by a charge amplifier 35 and 36, respectively. Negative feedback capacitors C_{f1} and C_{f2} , respectively, allow to control the
20 gain of charge amplifiers 35 and 36, respectively. The frequency bands transmitted by these amplifiers can be limited. In the first branch 33, the amplifier 35 is followed by an integrator 37 which transforms the signal corresponding to acceleration, supplied at the output of
25 amplifier 35, to a signal corresponding to velocity. The integrator 37 is followed by a low-pass filter 38 whose passing band extends from f_0 to f_1 where f_0 is the lowest frequency of interest and f_1 is the so-called transition frequency. In the second branch 34, the amplifier 36 is
30 directly followed by a high-pass filter 39 whose passing band extends from f_1 to f_2 where f_2 is the highest frequency

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of interest. The output signals of the two branches 33 and 34 are applied to the inputs of a summing integrator 40 that supplies an output signal E_s whose mathematical expression is:

$$5 \quad E_s = dx/dt = x' \quad \text{in the interval } [f_0; f_1]$$

$$E_s = d^2x/dt^2 = x'' \quad \text{in the interval } [f_1; f_2]$$

$$\text{thus: } E_s = (x'[f_0; f_1]) \oplus (x'' [f_1; f_2])$$

The variable x represents the vibration displacement.

10 SECOND EXAMPLE OF A SYSTEM ACCORDING TO FIG. 1

FIG. 3 shows the block diagram of a second example of a measurement system whose block diagram is shown in FIG. 1. The system represented in Fig. 3 comprises a transducer 51 mounted on an object which is subjected to vibrations (this object is not shown in Fig. 3), and an electronic circuit for the processing of the output signal supplied by the transducer 51.

The transducer 51 is arranged as an accelerometer and supplies an electric charge Q as an output signal, the charge Q being proportional to the acceleration of the object over the entire interesting frequency range.

The transducer 51 is followed by a charge amplifier 52 having a dynamic that is adapted to the entire range of useful frequencies. The charge amplifier 52 is followed by two branches 53, 54 for the processing of its output signal which corresponds to the acceleration of the object.

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The branch 53 comprises an integrator 55 that transforms the signal supplied at the output of amplifier 52 and corresponding to acceleration, into a signal corresponding to velocity. The integrator 55 is followed by an adjustable
5 gain amplifier 56 and then by a low-pass filter 57 whose passing band extends from f_0 to f_1 .

The branch 54 comprises an adjustable gain amplifier 58 followed by a high-pass filter 59 whose passing band extends from f_1 to f_2 .

10 The adjustable gain amplifiers 56 and 58 permit to control the two sensibilities of velocity and acceleration.

The output signals of the two branches 53 and 54 are applied to the inputs of a summing integrator 60 that supplies an output signal E_s whose mathematical expression is the same
15 as that in the preceding Example related to FIG. 2:

$$E_s = dx/dt = x' \quad \text{in the interval } [f_0; f_1]$$

$$E_s = d^2x/dt^2 = x'' \quad \text{in the interval } [f_1; f_2]$$

thus: $E_s = (x'[f_0; f_1]) \oplus (x'' [f_1; f_2])$

20 The variable x represents the vibration displacement.

THIRD EXAMPLE OF A SYSTEM ACCORDING TO FIG. 1

FIG. 4 shows the block diagram of a third example of a measurement system whose block diagram is shown in FIG. 1. The system represented in Fig. 4 comprises a transducer 71
25 mounted on an object which is subjected to vibrations (this object is not shown in Fig. 4), and an electronic circuit 73

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for the processing of the output signal supplied by the transducer 71.

The transducer 71 is arranged as an accelerometer and supplies an electric charge Q as an output signal, the charge Q being proportional to the acceleration of the object over the entire interesting frequency range.

The transducer 71 is followed by a charge amplifier 72 having a dynamic that is adapted to the entire range of useful frequencies. The charge amplifier 72 is followed by a circuit 73 for the processing of its output signal which corresponds to the acceleration of the object. The circuit 73 is in turn followed by an adjustable gain amplifier 74.

The circuit 73 is a limited I/P integrator having the structure shown in FIG. 4. In the circuit 73, the output signal supplied by the amplifier 72 is subjected, as to the electronic meaning, to a so-called "limited" I/P integration. The term "limited" integration is justified by the fact that the I/P circuit acts as a mathematical integrator in the range of low frequencies until the so-called transition frequency f_1 , in which field the impedance of the feedback of the amplifier that is part of the I/P integrator, is essentially capacitive and becomes resistive for the range of high frequencies. The transition frequency f_1 responds to the relation

$$f_1 = 1/2 \pi R_1 C_1.$$

The output signal supplied by the circuit 73 is amplified in the adjustable gain amplifier 74.

The adjustable gain amplifier 74 supplies an output signal E_s whose mathematical expression is the same as that in the preceding Examples described with regard to FIG. 2 and 3:

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$$E_s = dx/dt = x' \quad \text{in the interval } [f_0; f_1]$$

$$E_s = d^2x/dt^2 = x'' \quad \text{in the interval } [f_1; f_2]$$

$$\text{thus: } E_s = (x'[f_0; f_1]) \oplus (x'' [f_1; f_2])$$

5 The variable x represents the vibration
displacement.

In the present Example, the output signal E_s fulfills the
function

$$E_s = (x'[f_0; f_1]) \oplus (x'' [f_1; f_2])$$

10 precisely at the asymptotes, namely near the frequencies f_0
and f_2 and with a certain error around the transition
frequency f_1 .

EXAMPLES OF A SECOND SYSTEM AND A SECOND METHOD ACCORDING TO THE INVENTION

15 As it is represented in the block diagram of FIG. 5, a
second system according to the invention for the measurement
of mechanical vibrations of an object comprises a transducer
21 which is mounted on an object subjected to vibrations,
and an electronic circuit 23.

20 The transducer 21 has an output port 22 on which it supplies
a signal representative of the velocity of the vibration
movement of the object. This signal comprises a frequency
spectrum comprising a band called low frequency band
situated below a frequency called transition frequency, and
a second band called high frequency band, situated above
25 said transition frequency.

The electronic circuit 23 has an input port 24, connected to
the output port 22 of the transducer 21, and an output port
25. The circuit 23 is used to process the signal supplied by

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the transducer 21 at its output port 22. The circuit 23 supplies an output signal at its output port 25 which, in said low frequency band, corresponds to the mathematical integral over the time function of the output signal of the transducer 21, and within said high frequency band, corresponds to said output signal of the transducer 21. The output signal supplied at the output port 25 of the electronic circuit 23 is therefore composed in such a manner that, within said low frequency band, it corresponds to the displacement associated to the vibration movement of the object, and within said high frequency band, it corresponds to the velocity of the vibration movement of the object.

The measurement system according to FIG. 5 thus allows the implementation of a second method according to the invention, characterized in that it comprises:

the processing of an input signal, representative of a velocity related to a mechanical vibration of the examined object, said input signal having a frequency spectrum comprising a so-called low-frequency band situated below a transition frequency, and a so-called high frequency band situated above said transition frequency, said method carrying out said signal processing in an electronic circuit for producing an output signal such as the signal supplied at the output port 25 of the electronic circuit 23, said output signal corresponding, within said low-frequency band, to the mathematical integral over the time of said input signal, i.e. to the vibration displacement of said object, and corresponding, within said high-frequency band, to the input signal, i.e. to the vibration velocity of said object.

FIRST EXAMPLE OF A SYSTEM ACCORDING TO FIG. 5

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FIG. 6 shows the block diagram of a first embodiment of a measurement system whose block diagram is shown in FIG. 5. The system represented in FIG. 6 comprises a transducer 81 mounted on an object which is subjected to vibrations (this object is not shown in Fig. 6), and an electronic circuit 83 for the processing of the output signal supplied by the transducer 81.

The transducer 81 is arranged as a velocimeter and supplies an electric voltage as an output signal, this voltage being proportional to the vibration velocity of the object over the entire interesting frequency range.

The transducer 81 is followed by an amplification step 82 which may contain correction elements or not.

The amplifier 82 is followed by two branches 83, 84 for the processing of its output signal which represents the vibration velocity of the object.

The branch 83 comprises an integrator 85 that transforms the signal supplied at the output of the amplifier 82, corresponding to the velocity of the vibration, into a signal which corresponds to the vibration displacement. The integrator 85 is followed by an adjustable gain amplifier 86, followed in turn by a low-pass filter 87 whose passing band extends from f_0 to f_1 .

The branch 84 contains an adjustable gain amplifier 88 followed by a high-pass filter 89 whose passing band extends from f_1 to f_2 .

The adjustable gain amplifiers 86 and 88 allow to control the two sensibilities, namely that of the vibration displacement and of the vibration velocity.

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The output signals of the two branches 83 and 84 are added by means of a summing integrator 90 that supplies an output signal E_s whose mathematical expression is the following:

$$E_s = x \quad \text{in the interval } [f_0; f_1]$$

$$5 \quad E_s = dx/dt = x' \quad \text{in the interval } [f_1; f_2]$$

$$\text{thus: } E_s = (x[f_0; f_1]) \oplus (x' [f_1; f_2])$$

The variable x represents the vibration displacement.

SECOND EXAMPLE OF A SYSTEM ACCORDING TO FIG. 5

10 FIG. 7 shows the block diagram of a second embodiment of a measurement system whose block diagram is shown in FIG. 5. The system represented in FIG. 7 comprises a transducer 91 mounted on an object which is subjected to vibrations (this object is not shown in Fig. 7), and an electronic circuit
15 for the processing of the output signal supplied by the transducer 91.

The transducer 91 is arranged as a velocimeter and supplies an electric voltage as an output signal, this voltage being proportional to the vibration velocity of the object over
20 the entire interesting frequency range.

The transducer 91 is followed by an amplifier 92 having a dynamic that is adapted to the entire range of useful frequencies. The amplifier 92 is followed by a circuit 93 for the processing of its output signal. The circuit 93 is
25 in turn followed by an adjustable gain amplifier 94.

The circuit 93 is a limited I/P integrator having the structure shown in FIG. 7. In the circuit 93, the output

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signal supplied by the amplifier 92 is subjected, as to the electronic meaning, to a so-called "limited" I/P integration. The term "limited" integration is justified by the fact that the I/P circuit acts as a mathematical

5 integrator in the range of low frequencies until the so-called transition frequency f_1 , in which field the impedance of the feedback of the amplifier that is part of the I/P integrator, is essentially capacitive and becomes resistive for the range of high frequencies. The transition frequency

10 f_1 responds to the relation

$$f_1 = 1/2 \pi R_1 C_1.$$

The output signal supplied by the circuit 93 is amplified in the adjustable gain amplifier 94.

The adjustable gain amplifier 94 supplies an output signal

15 E_s whose mathematical expression is the same as that in the foregoing Example, described with regard to FIG. 6:

$$E_s = x \quad \text{in the interval } [f_0; f_1]$$

$$E_s = dx/dt = x' \quad \text{in the interval } [f_1; f_2]$$

thus: $E_s = (x[f_0; f_1]) \oplus (x' [f_1; f_2])$

20 The variable x represents the vibration displacement.

In the present Example, the output signal E_s fulfills the function

$$E_s = (x [f_0; f_1]) \oplus (x' [f_1; f_2])$$

25 precisely at the asymptotes, namely near the frequencies f_0 and f_2 and with a certain error around the transition frequency f_1 .

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GENERAL REMARKS REGARDING THE STRUCTURE OF A SYSTEM
ACCORDING TO THE INVENTION

Within the scope of the invention, no limitation whatsoever is requested regarding the choice of the type of the
5 transducer to be used. The above-mentioned transducers are to be regarded as examples only. Other transducers may still be cited, such as piezoelectric accelerometers with integrated electronic supplying a voltage modulated output signal, piezoelectric accelerometers with integrated
10 electronic supplying a current modulated output signal, piezoresistive accelerometers supplying a voltage output signal, etc. All these types of transducers may be used indifferently with the electronic circuits shown in FIG: 3 and 4. Optical velocimeters may be used with the circuits
15 represented in FIG. 6 and 7.

The electronic circuit which processes the signal supplied by the transducer may be incorporated into the transducer casing or arranged outside. In the first case, the device is a transducer with integrated electronic where the output
20 port 12 and the connector 14 in FIG. 1 are physically identical. In the second case, the outside electronic is mounted in a conditioning cabinet disposed distantly from the pickup or the transducer.

For sake of simplification of this description, the
25 following components have not been represented in the block diagrams shown by the attached drawings; these components are however necessary, and their use are well known to the one skilled in the art:

- a high-pass filter for attenuate the very low
30 frequencies is mounted upstream those parts of the circuit which carry out mathematical integration operations;

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a low-pass filter is also used for the rejection of high frequencies or undesired parasites.

In each one of the above circuits described with reference to the figures, the output signal E_s can be transmitted as
5 an electric voltage or through a voltage-to-current converter, or even in any other transmission form (optical, amplitude modulated radiofrequency, frequency modulated radiofrequency, etc.).

10 FREQUENCY RESPONSE CURVE OF A MEASUREMENT SYSTEM ACCORDING TO THE INVENTION

FIG. 8 shows an example of a frequency response curve of a system according to the invention, drafted on a log-log scale, the frequency being expressed in kHz on the abscissa and the acceleration in m/s^2 on the ordinate. This curve
15 gives the transfer function between a vibration excitation signal of an acceleration at a constant level of 1 m/s^2 over the entire interesting frequency band (from 10 Hz to 50 kHz), and the output signal of the measurement system in said interesting frequency band.

20 The sensitivity of the measurement chain in this Example is $A_s = 1.26 \text{ mV}/(\text{m/s}^2)$, representative of the acceleration of the vibration movement within the frequency band of from $f_1 = 500 \text{ Hz}$ to $f_2 = 50 \text{ kHz}$, and $V_s = 3.94 \text{ mV}/(\text{mm/s})$, representative of the vibration velocity within the
25 frequency band of from $f_0 = 10 \text{ Hz}$ to $f_1 = 500 \text{ Hz}$. The frequency response curve according to FIG. 8 shows two branches:

- the low frequency branch represents the mathematical integration

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$$v(t) = \int a(t) dt \qquad v(f) = \frac{a(f)}{2 \cdot \pi \cdot f}$$

$$\text{or} \quad \delta(t) = \int v(t) dt \qquad \delta(f) = \frac{v(f)}{2 \cdot \pi \cdot f}$$

wherein: δ or x are the vibration displacement,

v or $\dot{x}$ are the vibration velocity, and

5 a or $\ddot{x}$ are the vibration acceleration,

the curve having a slope of -6 dB/octave; and

- the medium and high frequency branch represents a constant sensitivity.

In the example of representation of the frequency response
 10 curve shown by FIG. 8, the limits at very low frequencies
 (frequencies lower than f_0) given by the high-pass filter
 has been excluded. The high-pass filter is necessary before
 the operation of the mathematical integration. The limit at
 very high frequencies (higher than f_2) has been excluded as
 15 well. It is given by a low-pass filter, the role of which is
 to eliminate undesired signals or parasites.

The two branches converge at a so-called transition
 frequency f_1 . If the continuity of the curve in f_1 should be
 respected, the velocity sensitivity V_s and the acceleration
 20 sensitivity A_s follow the relation: $A_s = (1/(2\pi f_1))V_s$, and
 the sensitivities of the displacement D_s and of the velocity
 V_s follow the same relation: $V_s = (1/(2\pi f_1))D_s$.

In the Example of the representation of the frequency
 response curve in FIG. 8, the transition frequency is $f_1 =$
 25 500 Hz, the lower limit of the so-called low frequency band

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is $f_0 = 10$ Hz, and the upper limit of the so-called high frequency band is $f_2 = 50$ kHz.

Although preferred embodiments of the invention have been described using specific terms, such description is for
5 illustrative purposes only, and it is to be understood that changes and variations may be made without departing from the spirit or scope of the invention defined by the following claims.

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CLAIMS

1. A method for measuring the mechanical vibrations of an object, comprising

electronically processing an input signal,
5 representative of an acceleration related to a mechanical vibration of said object and having a frequency spectrum comprising a low-frequency band situated below a transition frequency and a high frequency band situated above said transition frequency,

10 said processing being carried out by means of an electronic circuit which is adapted to provide an output signal which

within said low-frequency band corresponds to the mathematical integral over the time of said input signal,
15 i.e. to the vibration velocity of said object, and
within said high-frequency band corresponds to the input signal, i.e. to the vibration acceleration of said object.

2. A method for measuring the mechanical vibrations of an
20 object, comprising

electronically processing an input signal,
representative of a velocity related to a mechanical vibration of said object and having a frequency spectrum comprising a low-frequency band situated below a transition
25 frequency and a high frequency band situated above said transition frequency,

said processing being carried out by means of an electronic circuit which is adapted to provide an output signal which

30 within said low-frequency band corresponds to the mathematical integral over the time of said input signal, i.e. to the vibration displacement of said object, and

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within said high-frequency band corresponds to the input signal, i.e. to the vibration velocity of said object.

3. A system for measuring mechanical vibrations of an object, comprising

5 (a) a transducer mounted on said object and being capable of providing at its output an input signal which is representative of an acceleration related to a mechanical vibration of said object, said input signal comprising a low-frequency band situated below a transition frequency and
10 a high frequency band situated above said transition frequency, and

(b) an electronic circuit having an input port, connected to the output of said transducer, and an output port, said circuit being adapted to process said input signal to yield
15 an output signal which within said low-frequency band corresponds to the mathematical integral over the time of said input signal, and which within said high-frequency band corresponds to said input signal.

4. A system for measuring mechanical vibrations of an
20 object, comprising

(a) a transducer mounted on said object and being capable of providing at its output an input signal which is representative of a velocity related to a mechanical vibration of said object, said input signal comprising a
25 low-frequency band situated below a transition frequency and a high frequency band situated above said transition frequency, and

(b) an electronic circuit having an input port, connected to the output of said transducer, and an output port, said

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circuit being adapted to process said input signal to yield an output signal which within said low-frequency band corresponds to the mathematical integral over the time of said input signal, and which within said high-frequency band
5 corresponds to said input signal.

5. The system of claim 3, wherein said electronic circuit comprises two branches:

a first branch containing the connection in series of a charge divider, a charge amplifier, an integrator and a low-
10 pass filter, and

a second branch containing the connection in series of a charge divider, a charge amplifier and a high-pass filter,

the outputs of the two branches being connected to the input ports of a summing device .

15 6. The system of claim 3, wherein said electronic circuit comprises a conditioner for the signal supplied by the transducer, said conditioner being followed by two branches:

a first branch containing the connection in series of an integrator, an adjustable gain amplifier and a low-pass
20 filter, and

a second branch containing the connection in series of an adjustable gain amplifier and a high-pass filter,

the outputs of the two branches being connected to the input ports of a summing device .

25 7. The system of claim 3, wherein the electronic circuit comprises a conditioner for the signal supplied by the transducer, said conditioner being followed by a connection in series of a limited integrator and an adjustable gain amplifier .

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8. The system of claim 4, wherein said electronic circuit comprises a conditioner for the signal supplied by the transducer, said conditioner being followed by two branches:

5 a first branch containing the connection in series of an integrator, an adjustable gain amplifier and a low-pass filter, and

a second branch containing the connection in series of an adjustable gain amplifier and a high-pass filter,

10 the outputs of the two branches being connected to the input ports of a summing device .

9. The system of claim 4, wherein the electronic circuit comprises a conditioner for the signal supplied by the transducer, said conditioner being followed by a connection in series of a limited integrator and an adjustable gain
15 amplifier .

10. The system according to claim 3 or claim 4, wherein said object is an object subjected to vibrations, and in particular a rotary machine or a rotary piece connected to such machine.

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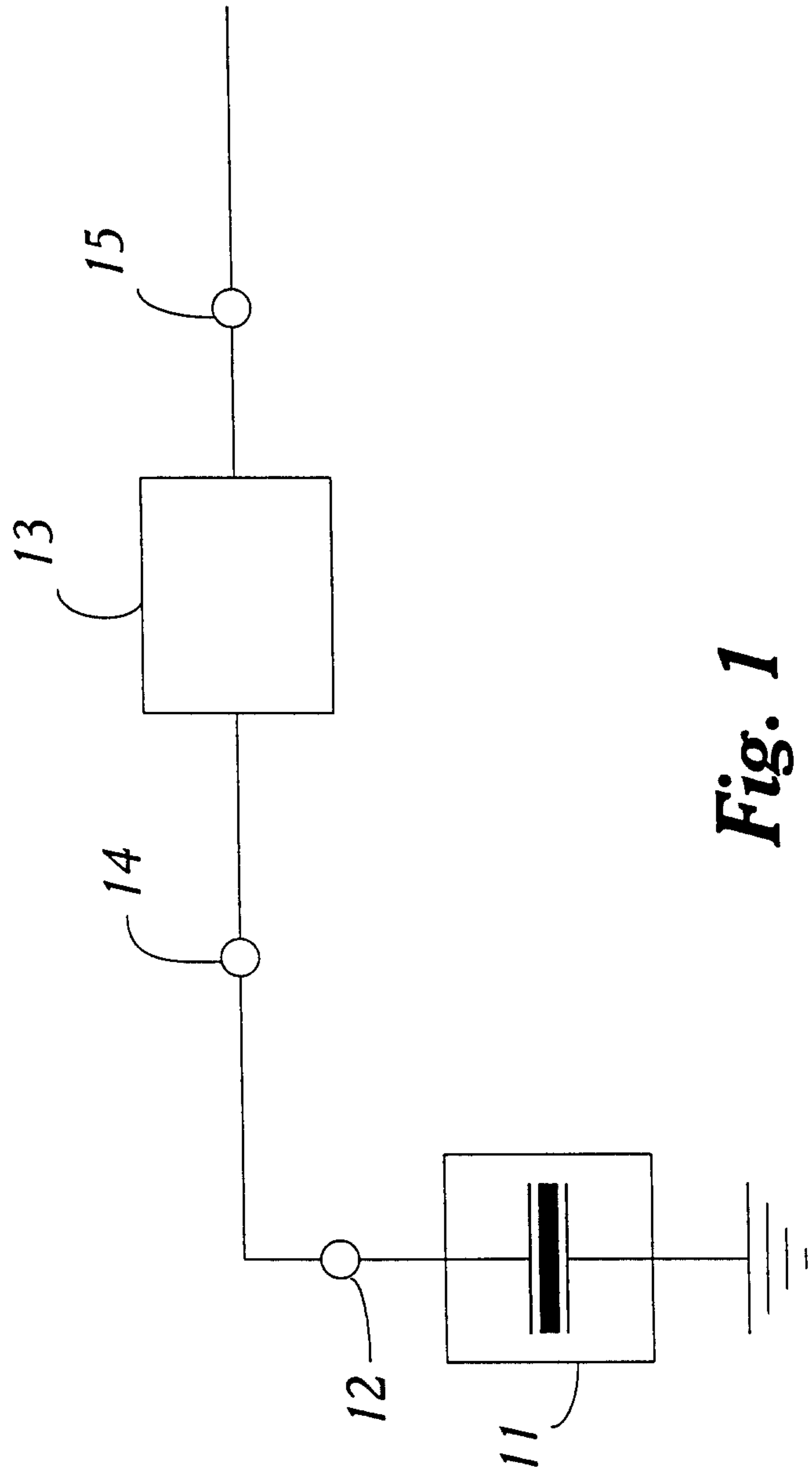


Fig. 1

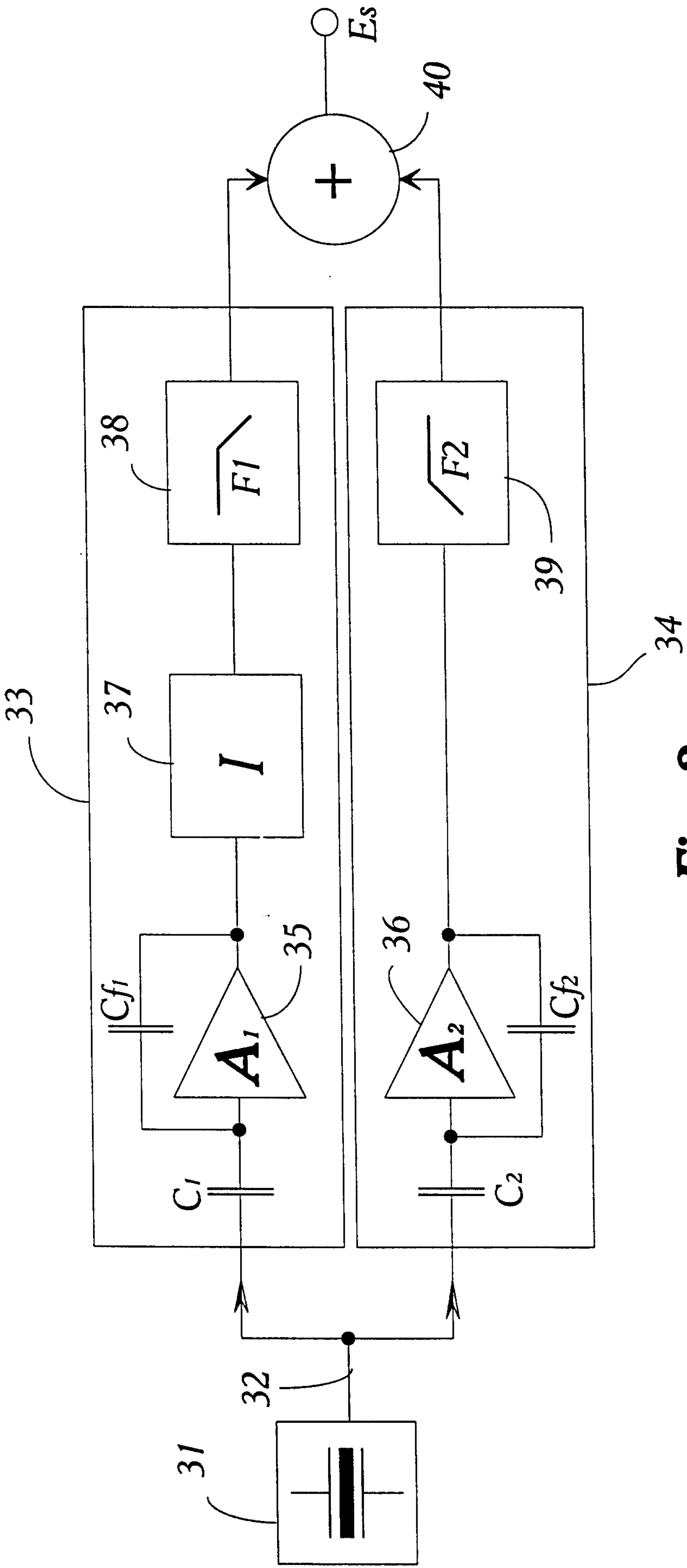


Fig. 2

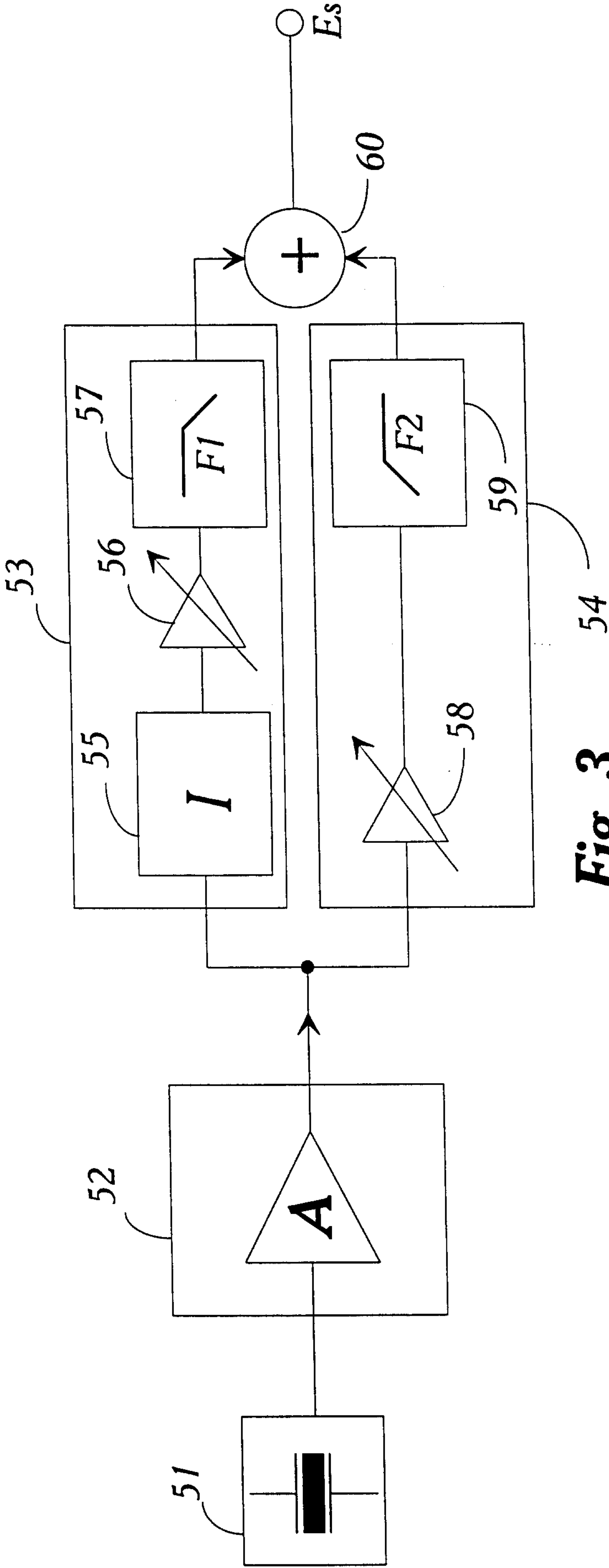


Fig. 3

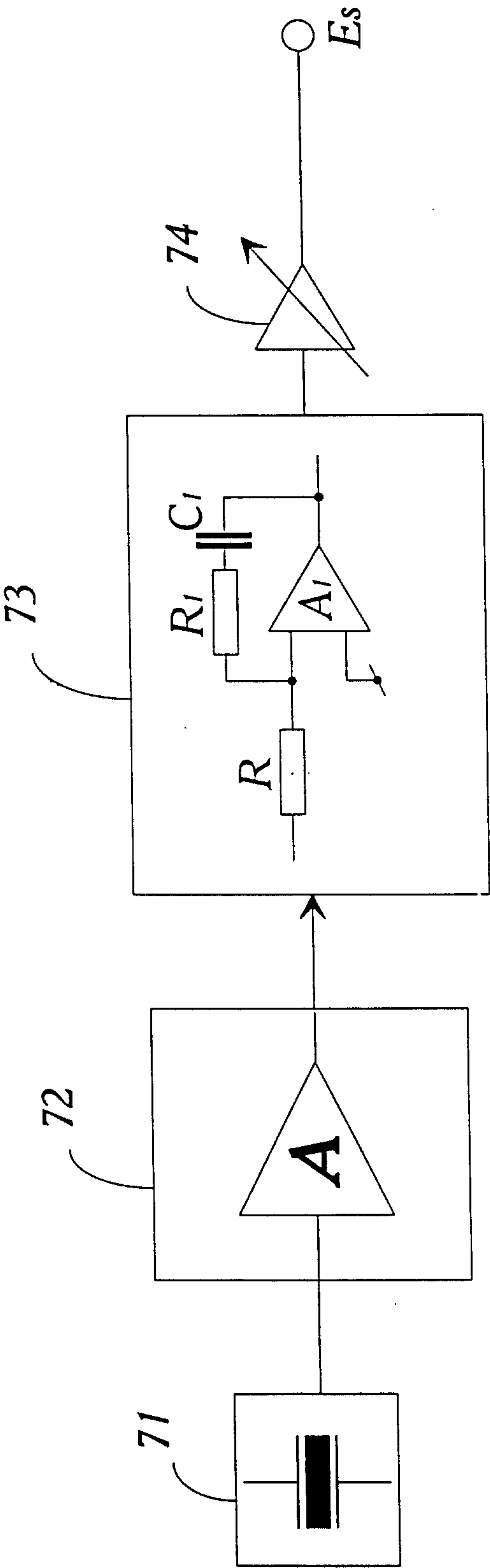


Fig. 4

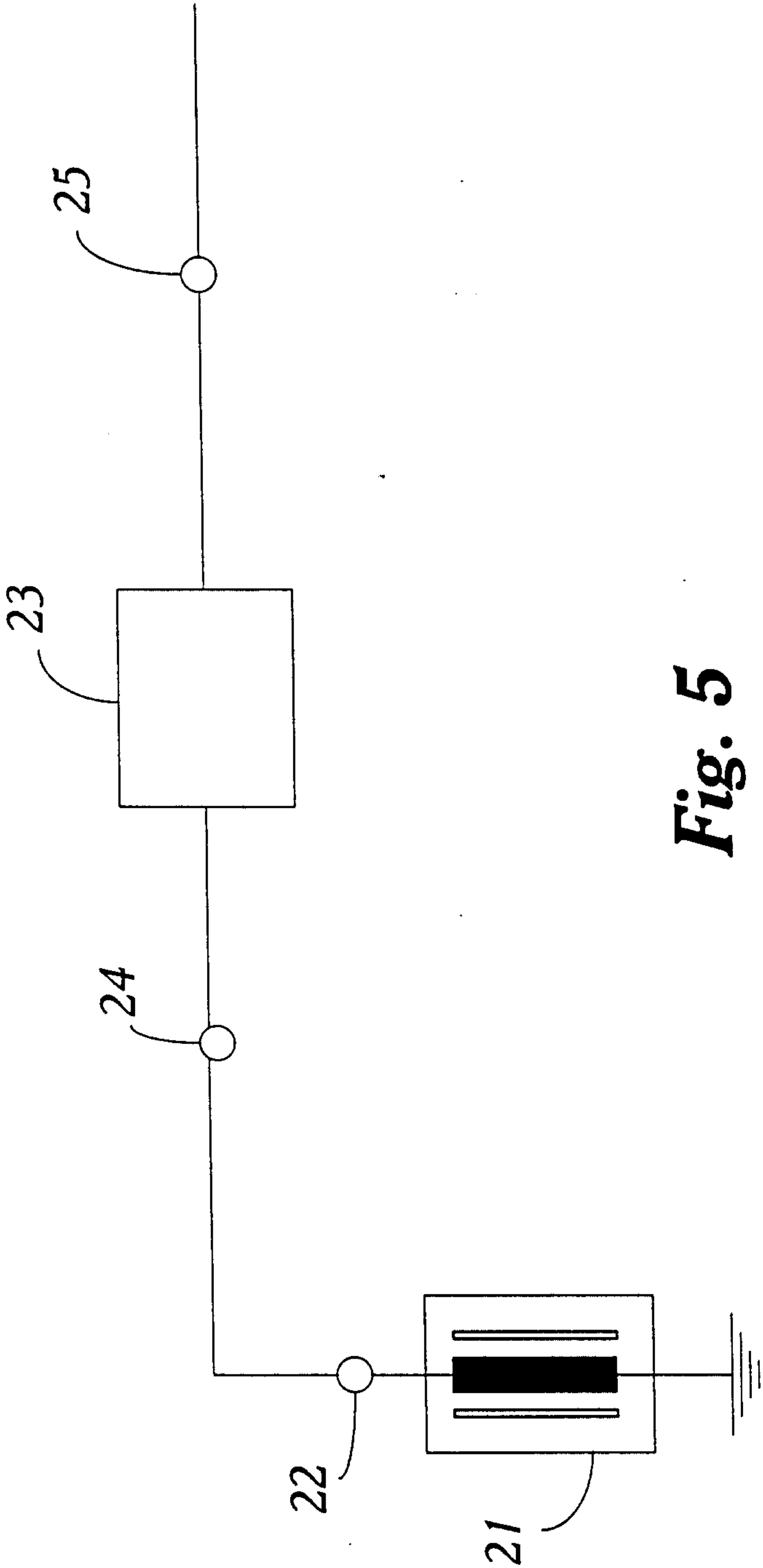


Fig. 5

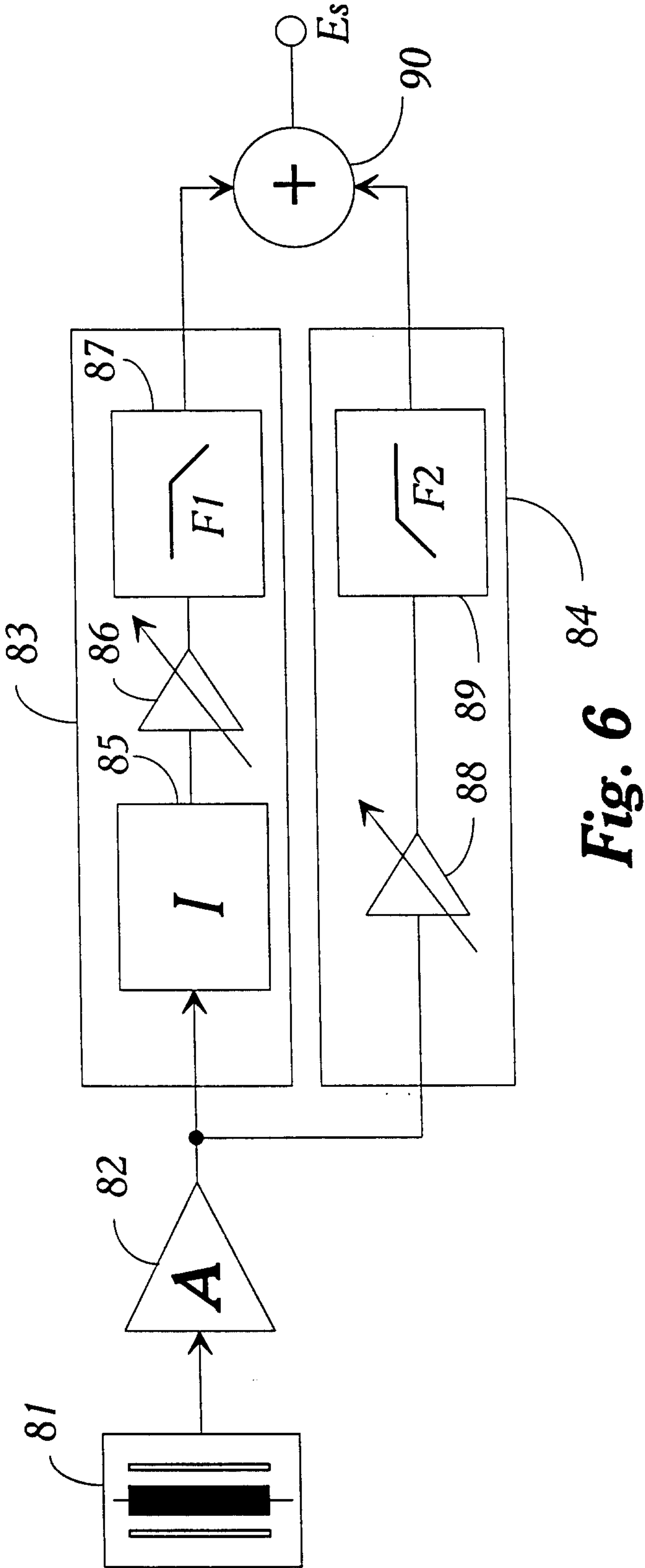


Fig. 6

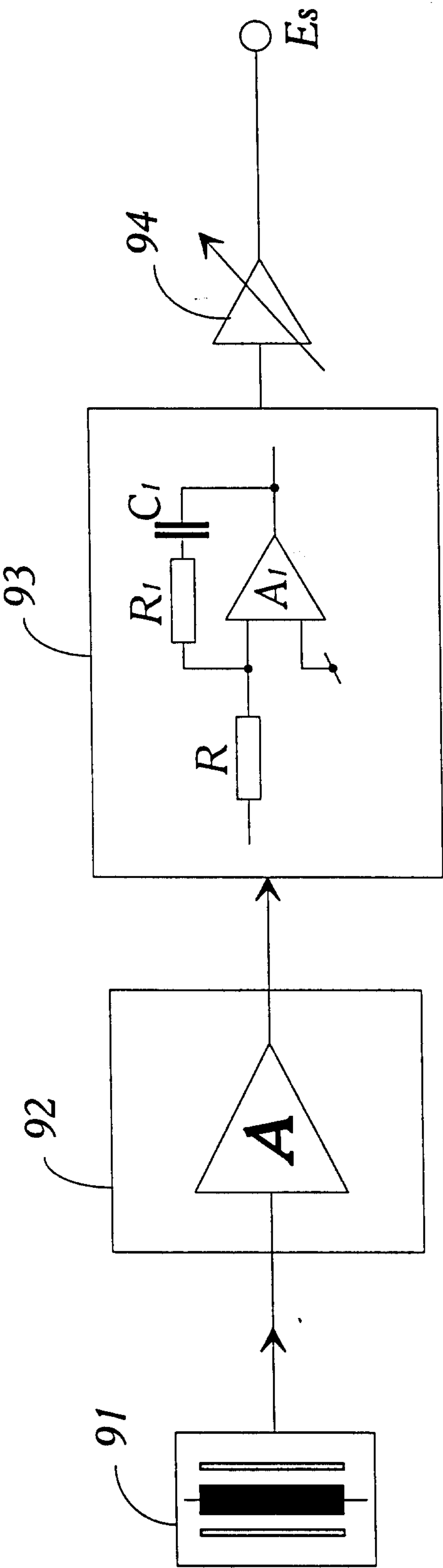


Fig. 7

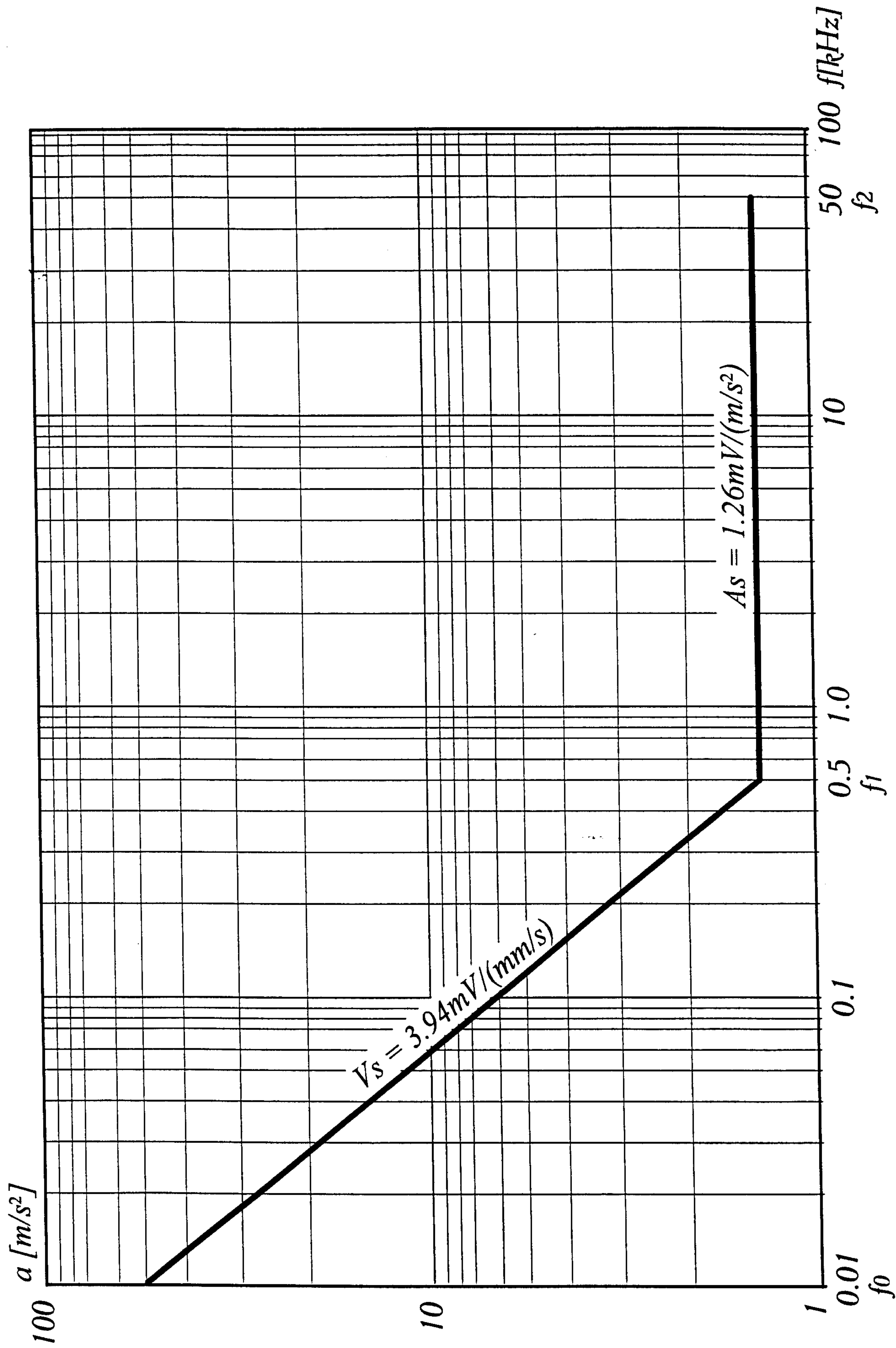


Fig. 8