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(71) Applicant(s)  
**Aker Solutions AS**

(72) Inventor(s)  
**Homstvedt, Gunder;Pedersen, Martin;Bjorgum, Rikhard**

(74) Agent / Attorney  
**Griffith Hack, GPO Box 1285, MELBOURNE, VIC, 3001, AU**

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## (71) Applicant: AKER SUBSEA AS [NO/NO]; P.O. Box 94, N-1325 Lysaker (NO).

## (72) Inventors: HOMSTVEDT, Gunder; 1648 Lakeside Enclave Dr., Houston, Texas 77077 (US). PEDERSEN, Martin; Grimstadgata 23F, N-0464 OSLO (NO). BJØRGUM, Rikhard; Ruglandsveien 140, N-1359 Eiksmarka (NO).

## (74) Agent: PROTECTOR IP CONSULTANTS AS; Oscarsgate 20, NO-0352 Oslo (NO).

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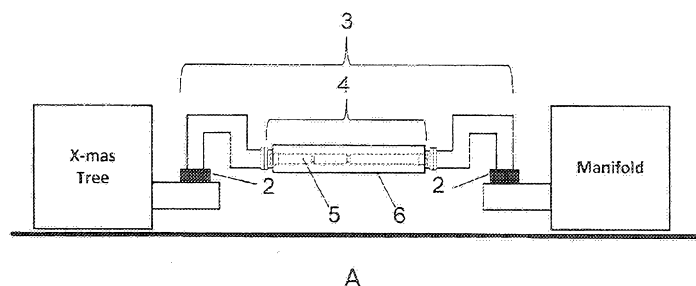


Figure 2

(57) Abstract: System for subsea pumping or compressing, comprising: an ESP (electrical submersible pump), a flowline jumper, a connector part in either end of the flowline jumper, and an arrangement for lifting, the ESP has been arranged in the flowline jumper which has been orientated in substance horizontal, distinctive in that the system further comprises: a stiffening arrangement, ensuring a straight ESP shaft at all times during lifting, installation and operation, and a load limiting arrangement for limiting or eliminating the load on structure and seabed supporting the system.

## SYSTEM FOR SUBSEA PUMPING OR COMPRESSING

### Field of the invention

5 The present invention relates to subsea tie-in, subsea production and subsea pressure boosting of hydrocarbons or other subsea flows handled in the petroleum industry. More specifically, the invention relates to a system for subsea pumping or compressing, comprising an Electric Submersible Pump (ESP).

10

### Background of the invention and prior art

A subsea pump, according to normal terminology in the art, is a pump designed to be operated as located on or close to the seabed. Accordingly, subsea pumping means pumping with subsea pumps arranged on or close to the  
15 seabed. In contrast, an Electric Submerged Pump (ESP) is according to normal terminology in the art a downhole pump to be arranged downhole into a wellbore for downhole pumping. Corresponding terminology can be used for compressors. Correspondingly, a subsea pressure booster is a subsea pump or compressor for subsea pressure boosting.

20

A demand exists for subsea pressure boosting for different applications.

Traditional subsea pumps are designed to handle rather large flow rates and high pressure boosting needs. Such pumps typically require supply of barrier  
25 fluid, extensive monitoring and manifold arrangements, making installations with such pumps complex, large, heavy and costly to fabricate and install.

For cases where there is a need to boost low flow rates, from a single well or a few wells, various attempts to applying downhole pumps – so called Electrical  
30 Submerged Pumps (ESP) - at the seabed have been tried. Such pumps have widespread application for artificial lift from wells as placed down in the wellbore. These pumps are driven by an electric motor powered through a cable clamped to the production tubing. They are mature machines with extensive track records, commercially available from a number of suppliers, Schlumberger

and Baker Hughes being the biggest. Since they are designed to be placed in a slim well bore, they are long and skinny. Length can be up to 40 meter and total installed power can be up to and above 1 MW, typically about 20 m length and about 1 MW installed power.

5

One arrangement of placing ESPs on the seabed is described in US pat. 7 565 932, "Subsea flowline jumper containing ESP" by Baker Hughes Inc. The patent describes the basic concept of installing an ESP in a generally horizontal section of a flowline jumper. Such flowline jumpers are typically used to connect  
10 various units in a subsea production system, the flowline jumpers having a vertical connector in each end. By exchanging the horizontal pipe section of the flowline jumper with an enlarged section containing an ESP, ease of installation can be achieved.

15 In US pat. 7 516 795, "Subsea Petroleum Production System Method of Installation and Use of the Same", by Petrobras, it has been described a subsea pumping system where pipe-mounted ESPs are assembled in a cassette. The ESPs are connected in series and mounted at an angle of up to 5 degrees from horizontal. The cassette is mounted onto a flow base. The cassette and the flow  
20 base can be installed via cable from service vessels in order to reduce time and cost.

Another arrangement is described in the US patent 8 500 419 "Subsea pumping system with interchangeable pumping units", by Schlumberger. This patent  
25 describes a similar arrangement of one or more ESPs in generally horizontal subsea pipe sections. Said patent describes a pumping module containing one or several pumping units mounted on a skid. The pump units, each having electric driven pumps (ESPs) assembled in a tubular section, can be individually retrieved. The pump skid includes a number of additional sub-systems:  
30 controller, sensor, pipe mount, hydraulic/ electrical connectors, isolation valves and at least one fluid by-pass valve.

The US patent 8 083 501 "Subsea pumping system including a skid with mate-able electrical and hydraulic connections", also by Schlumberger, describes a

more generalized version of the system described in patent US 8 500 419. The two patents are filed at the same date. Patent US 8 083 501 has the same arrangement as US 8 083 419, but describes a self-contained horizontal pump module, containing a centrifugal pump driven by an electrical motor. The  
5 description covers electric driven horizontal pumps in general – assembled in a pressure containing housing on a skid.

Pumps that are long and slim due to their intended application in a wellbore, are not ideal for subsea use. Typical subsea pumps are in contrast more compact  
10 and arranged for vertical installation and retrieval. A subsea pump is typically mounted on a flow base having a simple manifold arrangement for the routing of flow in and out of the pump plus allowing for by-pass in case of pump shutdown. US Patents 7 516 795, 8 500 419 and 8 083 501, mentioned above, describe typical subsea arrangement of the respective pumps mounted on a base. Such  
15 base is costly both to fabricate and install. Said pumps are arranged in a structure that adds weight and cost.

Subsea operations are expensive and equipment reliability is therefore one of the most vital selection criteria. Rotating equipment is in need of more frequent  
20 service than stationary equipment and reliability and serviceability should be given high priority in design.

ESPs have limited service life compared to subsea pumps, in part due to the design and in part due to the very challenging down-hole environment where  
25 they normally are installed. Typical interval for retrieval for service is 2-4 years.

However, if the arrangement described in the state of the art publication US patent 7 565 932 could be further enhanced with respect to reliability, robustness, simplicity, cost and installation/retrieval, it would be beneficial for  
30 the petroleum industry and it would increase the use of ESPs subsea, on or close to the seabed.

The present invention may improve the technology of the state of the art, as described in US patent 7 565 932.

Summary of the invention

The invention provides a system for subsea pumping or compressing, comprising:

- 5           a flowline jumper;
- an ESP (electrical submersible pump) arranged in the flowline jumper;
- a connector part in either end of the flowline jumper;
- at least one of a truss structure and a longitudinal rib arrangement
- configured as a stiffening arrangement to ensure a straight ESP shaft during
- 10   lifting, installation, and operation; and
- a load limiting arrangement that comprises buoyancy elements.

The invention also provides a system for subsea pumping or compressing, comprising:

- 15           a flowline jumper;
- an ESP (electrical submersible pump) arranged in the flowline jumper;
- a connector part in either end of the flowline jumper; and
- at least one of a truss structure and a longitudinal rib-arrangement
- configured as a stiffening arrangement to ensure a straight ESP shaft during
- 20   lifting, installation, and operation;
- wherein the stiffening arrangement comprises the longitudinal rib-arrangement.

The invention also provides a system for subsea pumping or compressing, comprising:

- 25           a flowline jumper;
- an ESP (electrical submersible pump) arranged in the flowline jumper;
- a connector part in either end of the flowline jumper;
- at least one of a truss structure and a longitudinal rib-arrangement
- 30   configured as a stiffening arrangement to ensure a straight ESP shaft during
- lifting, installation, and operation; and

at least one extendable support leg configured to extend toward the sea-bottom. The invention also provides a system for subsea pumping or compressing, comprising:

- 5           a flowline jumper;  
          an ESP (electrical submersible pump) arranged in the flowline jumper;  
          a connector part in either end of the flowline jumper;  
          at least one of a truss structure and a longitudinal rib-arrangement  
configured as a stiffening arrangement to ensure a straight ESP shaft during  
10   lifting, installation, and operation; and  
          an intermediate landing structure that can be mounted at locations where  
the flowline jumper in which the ESP is arranged needs to be at an angle  
compared to a separate flowline jumper to allow enough space for installation.
  
- 15   The invention also provides a system for subsea pumping or compressing,  
comprising:
  - an ESP (electrical submersible pump),
  - a flowline jumper,
  - a connector part in either end of the flowline jumper, and
  - 20       an arrangement for lifting, the ESP has been arranged in the flowline  
jumper which has been orientated in substance horizontally,  
wherein the system further comprises:
    - a stiffening arrangement, ensuring a straight ESP shaft at all times during  
lifting, installation and operation, and
    - 25       a load limiting arrangement for limiting or eliminating the load on  
structure and seabed supporting the system,  
          the load limiting arrangement comprising buoyancy elements in the form  
of syntactic foam based buoyancy elements having service life and total  
buoyancy in order to compensate for the added weight of the system compared  
30   to a traditional subsea jumper.

The term ESP means in this context a pump designed and typically used down into wellbores, as previously described. The phrase "flowline jumper which has been orientated in substance horizontal" means a horizontally orientated or

- slightly inclined flowline jumper. Slightly inclined means angle from horizontal orientation to less than 5°, 3°, 2° or 1° from horizontal. “In substance horizontal”, “substantially horizontal” and “generally horizontal” has the same meaning in
- 5 this context. For pressure boosting of liquid with some gas, the gas can be restricted in the flow inlet to the ESP by said inclination, and for pressure boosting of gas with some liquid, the liquid can be restricted. The flowline jumper has increased cross section area and wall thickness due to the ESP inside, compared to an ordinary flowline jumper without ESP. With the phrase “a
- 10 stiffening arrangement, ensuring a straight ESP shaft at all times during lifting, installation and operation”, it is meant sufficient stiffening to avoid shortened service life at lifting in air and lifting in water as in a normal installation procedure, as compared to the design service life without said lifting. With the phrase “a load limiting arrangement for limiting or eliminating the load on
- 15 structure and seabed supporting the connectors”, it is meant that the load is limited to the system having a weight not overloading substructure and soil, as



compared to design load for an ordinary flowline jumper without an ESP and stiffening arrangement. The stiffening arrangement and the load limiting arrangement are arranged to the flowline jumper part of the system for providing straightness of the ESP shaft and load limiting, respectively, or combined as  
5 one structure providing both straightness of the ESP shaft and load limiting.

Preferably, the load limiting arrangement comprises buoyancy elements. Such elements are preferably made from syntactic foam having the required service life. Alternatively, a number of small tanks or pipe sections filled with gas or  
10 foam based buoyancy material can be used as buoyancy elements.

The buoyancy compensation is preferably 4-6 metric tons, since this is a typical additional weight of a system of the invention as compared to an ordinary flowline jumper. The load or weight compensation by the buoyancy material  
15 can however span from resulting in a system of approximately neutral buoyancy as installed and connected and down to 1 metric ton. If near neutral buoyancy is used, such as resulting in a system weight as submerged of less than 500 kg, weight elements can be included in the system during handling and installation, at least as immersed, after which installation the weight elements can be  
20 removed, which represents a preferable embodiment of the invention. Accordingly, a very low load on supporting structure and seabed can be achieved whilst still allowing effective installation.

Preferably, the stiffening arrangement comprises a truss structure or  
25 longitudinal ribs mounted or welded to the pipe containing the ESP, or both a truss structure and longitudinal ribs. At least three longitudinal rib structures arranged 120° apart around the circumference are convenient. An additional or alternative stiffening structure comprises one or more support legs arranged in the mid-section or along the jumper containing the ESP.

30

In a preferable embodiment, the load limiting arrangement and the stiffening arrangement are combined. Parallel gas filled or buoyancy material filled pipe sections or similar structure arranged to the flowline jumper providing stiffening

and buoyancy with one structure is one example.

Preferably, each connector part or connector adapter comprises an isolation valve, to avoid leakage to the environment at installation, replacement or  
5 retrieval of the system.

The system can preferably comprise a separate by-pass line controlled by an electrically operated valve that closes when power is applied to the ESP.

10 The system may comprise an intermediate landing structure that can be mounted at locations where the jumper containing the ESP needs to be at an angle compared to the initial jumper to allow enough space for installation. The intermediate landing structure has preferably been adapted for installation of more than one flowline jumper containing ESPs, preferably the intermediate  
15 landing structure comprises manifolds and valves allowing routing of the flow. The intermediate landing structure preferably comprises one or more of: manifolds and valves allowing at least two ESPs to be run in parallel, manifolds and valves allowing at least two ESPs to be run in series, manifolds and valves for a by-pass pipe, the valves are preferably remotely activated valves.

20 The system of the invention provides subsea pressure boosting whilst eliminating the weight and cost of making a pump skid and enable reliable connection and isolation features. The system of the invention provides a relatively simple and cost effective pressure boosting, allowing use also where  
25 the supporting structure or seabed can tolerate no further loads, which is a very relevant issue in mature areas, often having soft soil seabeds overloaded by old, existing structure.

The system further enhances the application on a variety of subsea fields by  
30 utilizing intermediate, free standing landing structures to which the system can be connected. Connection to such landing structures can be done via flexible hoses, horizontal or vertical connections.

The system can further be used in areas where trawling protection is required

by having the pipe-section located at or close to the sea floor. The system may comprise a protection mat placed above the pipe-section and a local protection structure at the connection hubs. In such areas, a horizontal tie-in and connection method will be used.

5

The system of the invention establishes an enhanced version of a subsea installed ESP based on the basic concept in US pat. 7 565 932 by solving the following key issues:

- 10      ○ The increased weight of the installed ESPs, giving an additional load on the connector supports and other existing subsea structure in each end of the jumper, will be reduced or eliminated
- 15      ○ The risk of bending the pipe containing the ESP (due to the added weight) and thereby challenging the rotor-dynamic stability of the ESP motor-pump assembly, is eliminated
- 20      ○ The original, permanently installed connection hubs will typically lack isolation valves to contain hydrocarbons during installation and retrieval. Such modifications cannot be done to the permanent installed connector hubs. The system of the invention handles this issue.
- 25      ○ If the existing field architecture/arrangement does not have the required horizontal distance between the existing connection hubs to allow installation of the system directly onto those connectors, the installation of the system can be done onto one or two intermediate landing hubs either pre-installed or landed with the jumper on the seabed close to the existing connection points.

25

Contrary to the systems of US patents 7 516 795, 8 500 419 (pipes containing an ESP type pump unit) and 8 083 501 (a more generalized pump unit), all of which are mounted onto subsea skids and being complex, heavy and expensive, the system of the invention can utilize the existing foundations at the connection points, without overloading said connection points or supporting structure or seabed.

30

The system of the invention is lightweight, easy to install with minimum added equipment in, requiring only electric power supply in order to work as a boosting

station. The seabed location provides better cooling of the ESP than downhole location and allows for shorter pumps with larger diameter, running at lower speed than down-hole versions, increasing reliability.

## 5 Figures

Figure 1 gives a presentation of a typical flow-line jumper arrangement, not according to the invention.

Figures Nos. 2A, 2B, 3, 4, 5, 6, 7A-D, 8A-D and 9 illustrate embodiments of the system of the invention, or details thereof, as explained in detail below.

10

### Detailed description

As illustration of background art, not according to the invention, Figure 1 illustrates of a typical flow-line jumper arrangement (1) with vertical connector parts (2) in each end for connecting to a x-mas tree and with a manifold, respectively. Similar arrangement can also be made in a horizontal version. Horizontally made-up connectors will in such case be used instead of the vertical ones. Horizontal arrangements are typically used where trawling activity might be going on. The flowline will in such cases be trenched, located at or close to the seabed. A removable trawling protection mat or similar arrangement will typically be placed on top of the flow-line if it is not trenched.

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Figure 2A illustrates a preferred embodiment of the invention where there is enough space between the connection points to directly replace the existing jumper with the new jumper assembly (3). The new jumper version has the same connector parts (2), but it has a new mid-section (4) that contains the ESP (5) inside a generally horizontal section of the flow-line (6). Figure 2B illustrates a variation of the embodiment as for Figure 2A, wherein each connector part comprises a connector adaptor (7) at each end of the new jumper, between the connector part of original design towards the X-mas tree and manifold, respectively, and the mid-section. This adaptor comprises an isolation valve (8) and a new connector with new connector part (9). The initial connector part is permanently left in place with the isolation valve when the mid-section with new connector parts is retrieved. This allows for closing the flow-line ahead of pulling the jumper to avoid spillage to sea. This solves an

important issue related to replacing an existing jumper with an ESP-Jumper as such isolation valves are typically not in place in the existing system. This arrangement also allows for selecting a new connector that is optimally suited for quick and reliable retrieval and re-installation and standardization of required tooling.

Figure 3 illustrates another preferred embodiment of the invention. This version can be used in cases where there is not enough space between the connection points for direct replacement of the original jumper with a new ESP-jumper assembly (10). At least one intermediate landing structure (12) is in such case located between the original connection points. Figure 3 is showing two such landing structures. Such structures are typically landed at the seabed on a mud-mat or similar foundations. They are having a simple manifold connecting the in and out-going flow. They can be arranged with isolation valves (8) and new connector parts (9) suitable for easy retrieval, re-landing and connecting the ESP-jumper (10). Suitable jumpers (11) are used in connecting the intermediate landing structures with the initial connection hubs. The jumpers 10 and 11 will typically be mounted at an angle to each other allowing more freedom to locate the equipment if the seabed space is limited in the area.

Figure 4 illustrates an embodiment of the invention where the ESP-jumper (10) is equipped with a truss structure (13) to make the generally horizontal section of the jumper containing the ESP (6) stiff enough to avoid significant bending. Vertical connector parts (9) are mounted in each end. Wet-mate connector (14) for electric power feed to the ESP is mounted on the truss structure.

Figure 5 illustrates an alternative embodiment of the invention where the ESP-jumper (10) is equipped with ribs (15) and buoyancy elements (16). Three such ribs are typically located 120 degrees apart to make the generally horizontal section of the jumper containing the ESP stiff enough to avoid significant bending. The ribs are typically covering the entire jumper pipe length and having a size that reduces bending to an acceptable level. Vertical connector parts (9) are mounted in each end. Wet-mate connector (14) for electric power feed to the ESP is mounted on one of the ribs. Buoyancy elements (16) are

mounted between the ribs onto the ESP-pipe. The buoyancy elements are sized to compensate for the added weight by including the ESP and the large diameter pipe containing the pump. In this way the connection points see no significantly added weight compared to the initial loading.

5

Similar buoyancy elements can be mounted inside or attached to the truss structure shown in figure 4 for the same purpose as described here.

As a preferable embodiment, the load limiting of the system of the invention can be enhanced by adding more buoyancy, reducing the weight of the system to a value lower than the initial jumper load without an ESP, thereby increasing the structural integrity. This is particularly feasible for mature fields with overloaded support structure and fields with weak or unstable seabed. Additional weight required for efficient installation can preferably be a part of the lifting arrangement, and be retrieved after installation.

15

Figure 6 illustrates an additional or alternative way of supporting jumpers containing an ESP to avoid sagging. The mid-section of the horizontal pipe comprises at least one supporting adjustable leg (21). The leg comprises a foundation resting on the seabed and can be adjusted to give proper support.

20

Figure 7 illustrates four alternative arrangements of jumpers containing an ESP (5) landed onto two intermediate landing structures (12).

25

In figure 7A a single ESP-jumper is utilized. The isolation valve (8a) is set in open position during operation.

In figure 7B a single ESP-jumper is utilized in parallel with another pipe with no ESP. The pipe with no ESP can be utilized for by-pass if needed. If for example the ESP should be out of operation, the flow can be routed through this bypass pipe. The isolation valve (8a) for the pipe containing an ESP is set in closed position during bypass-operation. The bypass pipe can also allow for pigging through the system.

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In figure 7C two ESP-jumpers are utilized in parallel for increased capacity. The isolation valves connected to the ESP-pipes are set in open position during

operation.

In figure 7D two ESP-jumpers are connected in series for increased pressure boosting capacity. A third pipe, having no ESP, connecting the outlet of the first ESP with the inlet to the second ESP will allow this mode of operation. The  
5 isolation valves are set in open position during pumping.

Figure 8 illustrates an alternative arrangement where the manifolds at the intermediate landing structures are re-arranged to allow for various operation modes by changing valve position. Three pipes (17a, 17b and 17c) are  
10 arranged in parallel. Pipe 17a and 17c contain ESPs and pipe 17b serve as by-pass line. Isolation valves 18a, 18b and 18c are located at the inlet of each of the pipes, while isolation valves 18d, 18e and 18f are located at the respective outlets. Routing valve 19 is located in the inlet cross-connecting header between pipe number one and two (17a and 17b), while valve 20 is located in  
15 the outlet cross-connecting header between the outlets of pipe two and three (17b and 17c). A setup with three ESPs in parallel can also be arranged (not shown). The valves are typically remotely controlled for efficient re-routing of the flow.

20 Figure 8A illustrates a single ESP operation. A second ESP can be installed as back up. The by-pass line and the back-up ESP are closed off. Valves 18a, 18d and 20 are open. The other valves are closed.

Figure 8B illustrates a by-pass operation with no ESPs in operation. The two  
25 ESPs are closed off. Valves 19, 18b, 18e and 20 are open. The others are closed.

Figure 8C illustrates a parallel operation of two ESPs. The by-pass is closed off. Valves 18b and 18e are closed. The other valves are open.

30

Figure 8D illustrates serial operation of two ESPs. The by-pass line is used to connect the two ESPs. Valves 19 and 20 are closed, all other valves are open.

Figure 9 illustrates a pipe support frame (22) typically mounted in each end of

the jumpers illustrated in figures 4 and 5. The frame allows for temperature induced expansion/contraction in the direction of the pipe axis. The frame will however transfer torque and load in the vertical direction onto the connector hub. Side-load (in the horizontal direction) induced typically by any ocean  
5 current at the location, will also be transferred.

With the present invention, the prior art limitations are remedied by one or more of the following changes:

- 10 The weight of the jumper is different in air and submerged in water. The stiffening arrangement and a proper lifting arrangement to secure a straight pipe during lifting will be arranged so that the pipe containing the ESP will see minimal bending during lifting in air and in water, installation and in the landed, operational position. Long pumps, like the ESP type, shall preferably be  
15 operated with a straight shaft. The rotor-dynamic behaviour of this long shaft going through the motor, seal section and pump benefits from the present invention. Minimizing oscillations and vibrations will minimize the wear and tear on bearings and seals and ensure long service life. Such shaft straightness will be achieved by a stiffening arrangement on the ESP-pipe. A truss structure or  
20 fins mounted onto the pipe are two possible arrangements.  
A spreader-bar and wires from this bar connected to lifting points distributed along the jumper allows for keeping the jumper straight also during lifting in air and going through the splash-zone during installation.
- 25 In order to avoid additional weight on the landing structures and vertical connectors beyond the initial loading of these connectors, buoyancy elements are included as a load limiting arrangement. Such buoyancy elements will compensate for the added weight introduced by the ESP and the larger pipe containing it. The buoyancy elements and stiffening devices can be combined  
30 either in a truss structure or with stiffening fins attached to the pipe and embedded in the buoyancy materials, or the same structure can be both stiffening and load limiting.

A subsea jumper arrangement that has a generally horizontal section containing



an ESP will require a certain distance between the connector hubs. If such distance is sufficient, the ESP-jumper can directly replace the existing jumper. If the distance is too short, one or two intermediate landing structures can be installed and the ESP-jumper is installed between the structures. One or two  
5 flow-line jumpers will in such case have to be installed between the initial connection hubs and the intermediate landing structures. The jumpers are installed at an angle to each other in the horizontal plane to allow for flexible routing and enough space for the ESP pipe. In fields where horizontal connector systems are used, the arrangement can be adapted for such connectors.  
10 Trawling protection can be added both on the horizontal pipe section and also for the intermediate landing structures where needed.

Connectors exist in various make requiring relevant subsea tools for installation and retrieval. The ESP-jumper might need more frequent change-out, typically  
15 every 2-4 years, than the pipeline jumper due to required pump service. Installing a quick-connect connector type for the ESP-jumper is therefore preferable, for standardizing and availability of required tools and efficient operation.

20 Isolation of the in- and out-board pipeline ends is vital to contain hydrocarbons from leaking to the environment when the ESP-jumper is retrieved. If the ESP-jumper is landed directly onto the original hubs, a connector adaptor including such isolation valve is preferably used. Such adaptor will typically be a complete connector housing permanently left in place on the existing connection hub and  
25 terminated at the upper end with the standardized vertical connector hub. An isolation valve is included in the adaptor between the connectors. Such valve is typically operated by a Remote Operated Vehicle (ROV). If the ESP-jumper is landed onto one or more intermediate landing structures, a small manifold with isolations valves can be included.

30

Flow by-pass can be achieved by having a pipe arranged in parallel with the ESP-pipe and the flow path controlled by valves. The valves can be ROV operated or remotely controlled by the production control system. The valves can also be electrically operated by the electric power fed to the ESP so that it

will be set in the desired position when the ESP is powered.

The embodiment where the ESP-jumper is arranged onto two intermediate landing structures can accommodate serial or parallel operation of ESPs.

5 Three parallel pipes arranged with valves in each ends of the pipes onto the manifold mounted on the structures can direct flow in various ways. Two pipes will typically be equipped with ESPs while the third is empty. The empty pipe is used for by-pass.

10 For all these embodiments and variations thereof, means are provided to allow for hydrate inhibition. Injection ports are installed at suitable locations for supply of methanol or other inhibitors. This arrangement will also be used for flushing of the unit to remove hydrocarbons prior to retrieval. Supply and control of such injection is typically provided from the associated production system. Valves  
15 and connectors of the system are preferably designed to allow override by ROV in case of control failure.

Condition monitoring of the ESP (pressure, temperature and vibration signals) can be done in several ways:

- 20
- Signals modulated onto the power feed cable, as typically done for ESPs used in wells, can be applied if the data update frequency is not critical
  - Signals can be routed through the production controls system
  - Signals can be routed through a signal line or optical fiber in the ESP power umbilical.

25 As an example of the technical effect of the invention, a case study for a specific field in the Gulf of Mexico can be mentioned. For said field, an installed state of the art subsea pump system comprising 4 flowline jumpers with ESP for pressure boosting weighs about 350 metric tons, including required  
30 substructure. A system of the invention, also comprising 4 flowline jumpers with ESP, providing identical pressure boosting, weighs about 60 metric tons, including required substructure. Accordingly, the weight reduction is about a factor 60/350, resulting in a weight of about 17% of the state of the art system, and it is reason to believe that also the cost reduction and reduced time for

fabrication are accordingly. If comparison is made to traditional subsea pump systems, the technical effect is even more favorable.

5 For subsea fields with overloaded structure or unstable seabed or both, the system of the invention can be the only possible way of providing pressure boosting without building a completely new pressure boosting station for location on the seabed besides the existing structures.

10 The system of the invention may comprise any feature or step as here illustrated or described, in any operative combination, each such operative combination is an embodiment of the present invention.

15 It is to be understood that, if any prior art publication is referred to herein, such reference does not constitute an admission that the publication forms a part of the common general knowledge in the art, in Australia or any other country.

20 In the claims which follow and in the preceding description of the invention, except where the context requires otherwise due to express language or necessary implication, the word "comprise" or variations such as "comprises" or "comprising" is used in an inclusive sense, i.e. to specify the presence of the stated features but not to preclude the presence or addition of further features in various embodiments of the invention.

## CLAIMS

1. A system for subsea pumping or compressing, comprising:  
a flowline jumper;  
5 an ESP (electrical submersible pump) arranged in the flowline jumper;  
a connector part in either end of the flowline jumper;  
at least one of a truss structure and a longitudinal rib arrangement  
configured as a stiffening arrangement to ensure a straight ESP shaft during  
lifting, installation, and operation; and  
10 a load limiting arrangement that comprises buoyancy elements.
2. The system according to claim 1, further comprising at least one isolation  
valve arranged in the connector part and configured to avoid leakage to the  
environment at installation, replacement or retrieval of the flowline jumper.  
15
3. The system according to claim 1 or 2, further comprising a separate by-pass  
pipe controlled by a valve that closes when power is applied to the ESP.
4. The system according to any of claims 1 to 3, wherein the stiffening  
20 arrangement and the load limiting arrangement together comprise a common  
structure.
5. The system according to any of claims 1 to 4, wherein the flowline jumper is  
orientated in a position that is within 5 degrees of horizontal.  
25
6. The system according to any of claims 1 to 5, wherein the buoyancy  
elements comprise syntactic foam.
7. The system according to any of claim 1 to 6, wherein the buoyancy elements  
30 comprise at least one of a gas-filled tank, a buoyancy material filled tank, a gas  
filled pipe parallel to and arranged to the flowline jumper, and a buoyancy  
material filled pipe parallel to and arranged to the flowline jumper.

8. System for subsea pumping or compressing, comprising:

an ESP (electrical submersible pump),

a flowline jumper,

a connector part in either end of the flowline jumper, and

5 an arrangement for lifting, the ESP has been arranged in the flowline jumper which has been orientated in substance horizontally,

wherein the system further comprises:

a stiffening arrangement, ensuring a straight ESP shaft at all times during lifting, installation and operation, and

10 a load limiting arrangement for limiting or eliminating the load on structure and seabed supporting the system,

the load limiting arrangement comprising buoyancy elements in the form of syntactic foam based buoyancy elements having service life and total buoyancy in order to compensate for the added weight of the system compared  
15 to a traditional subsea jumper.

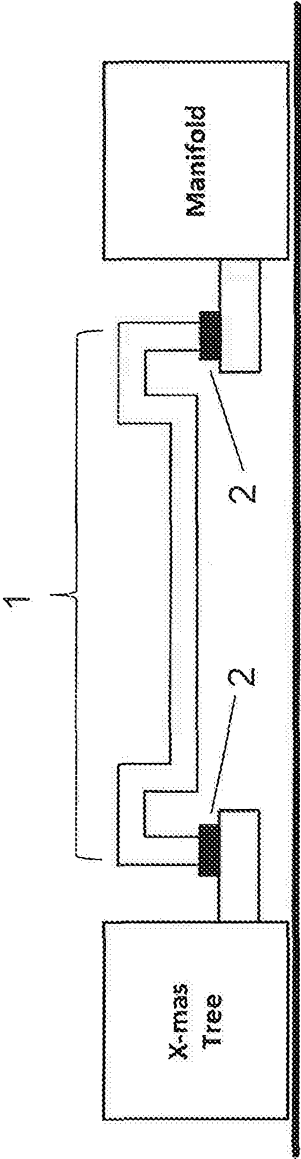


Figure 1

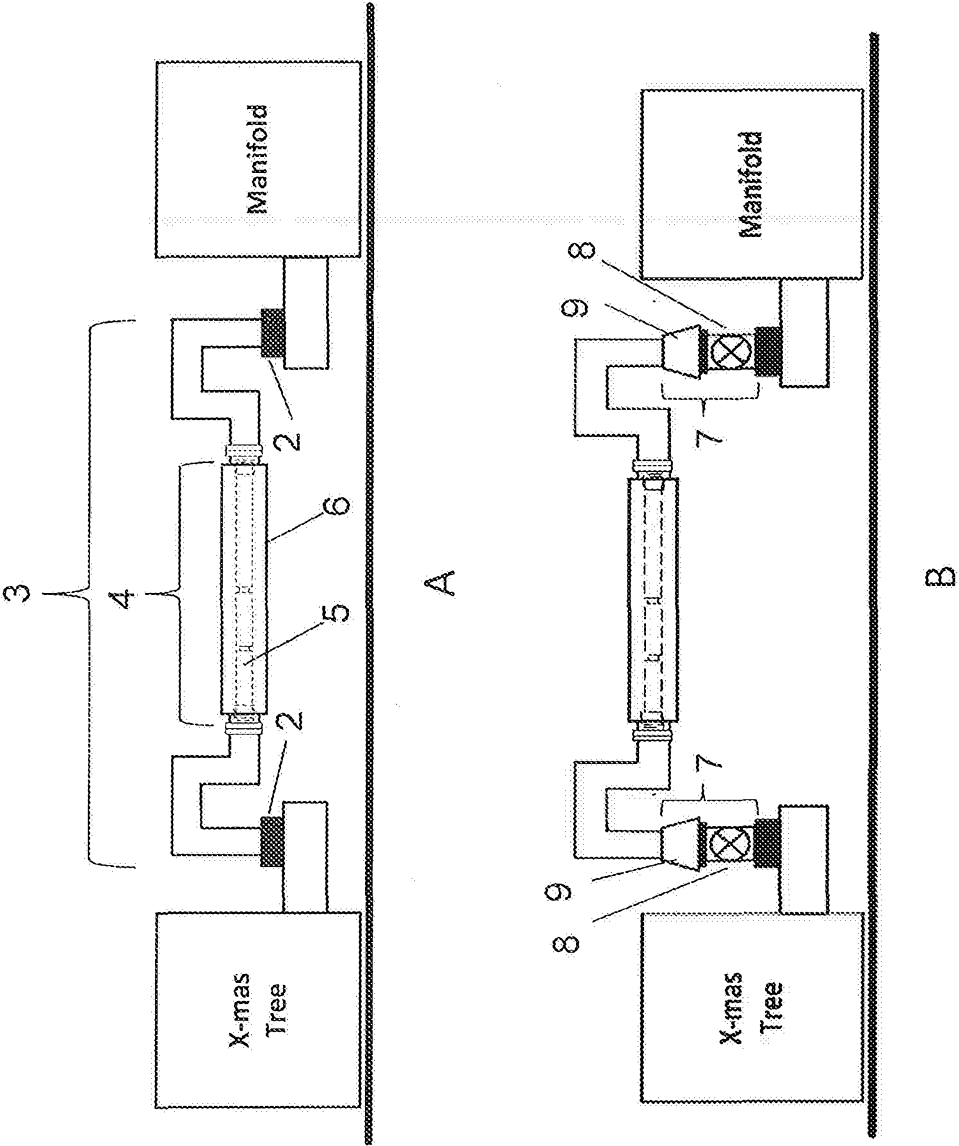


Figure 2

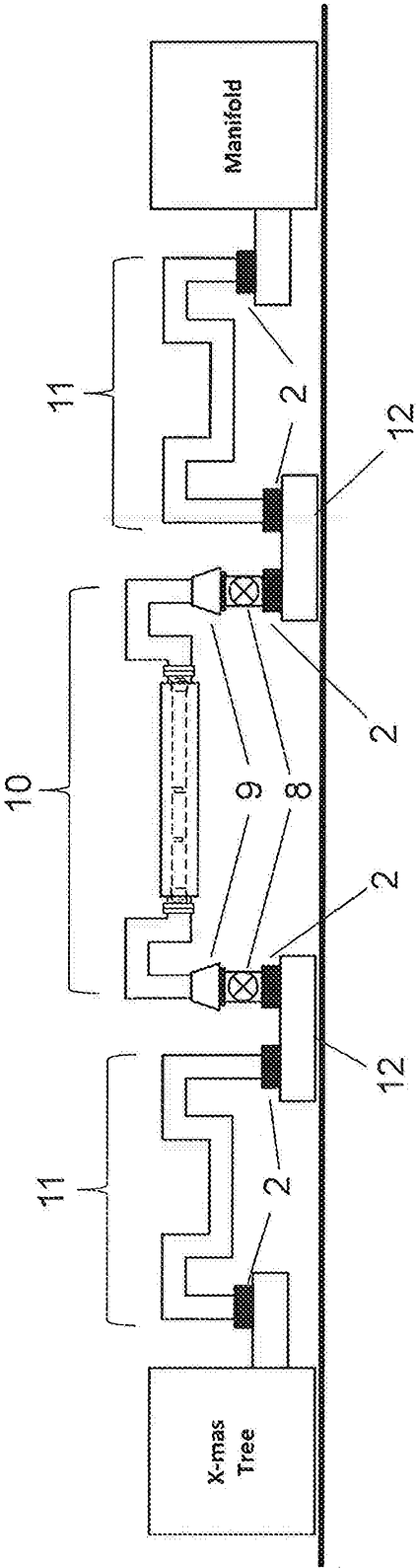


Figure 3



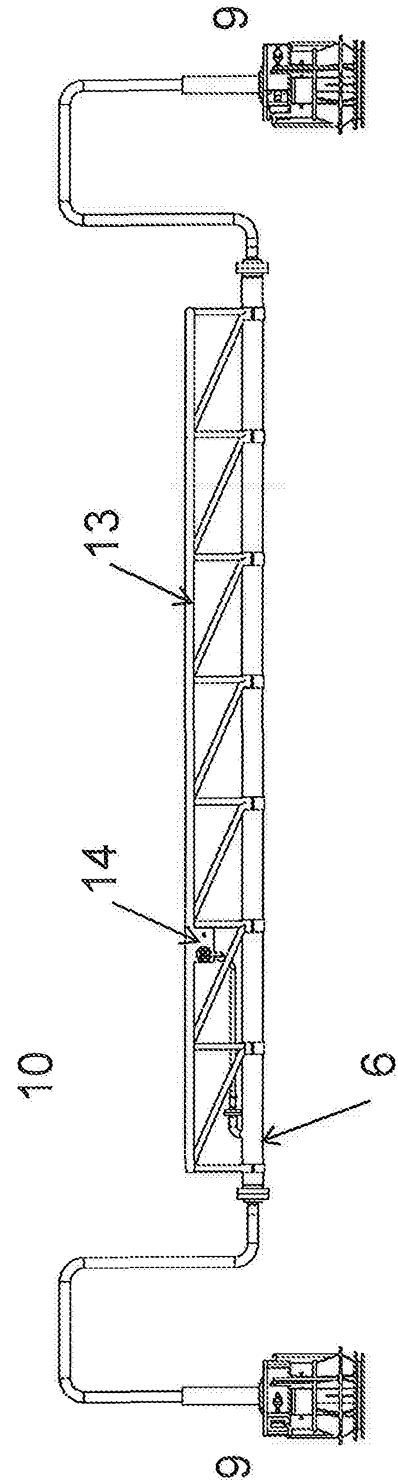


Figure 4

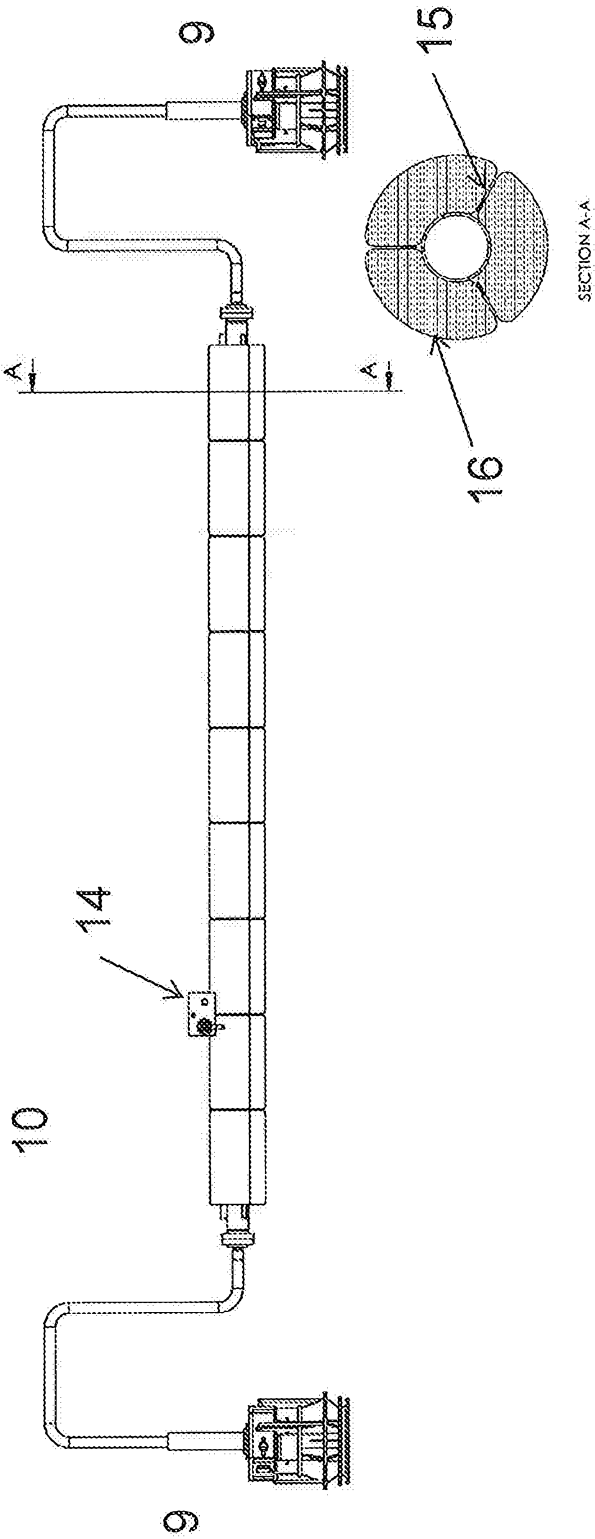


Figure 5

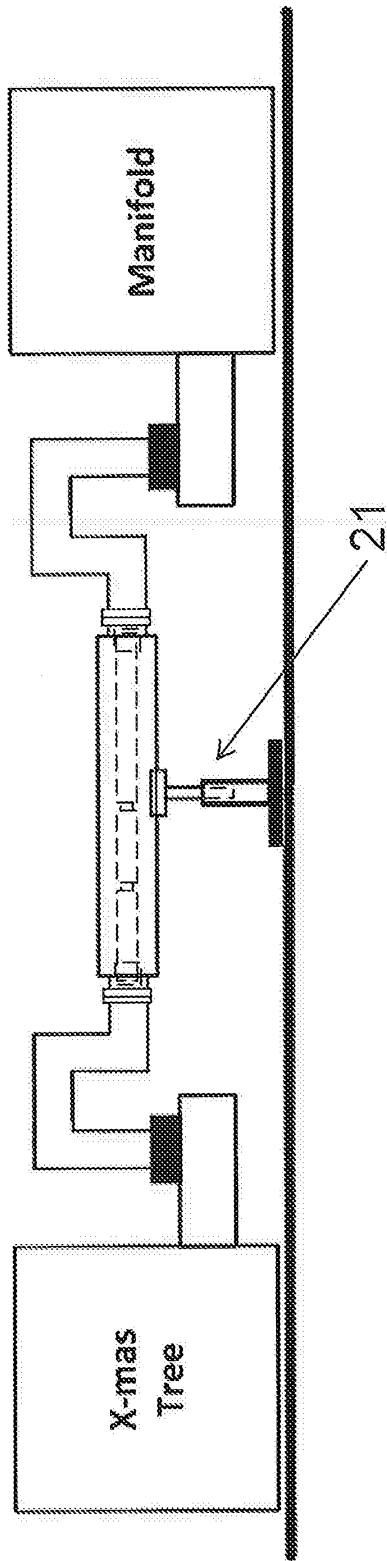


Figure 6

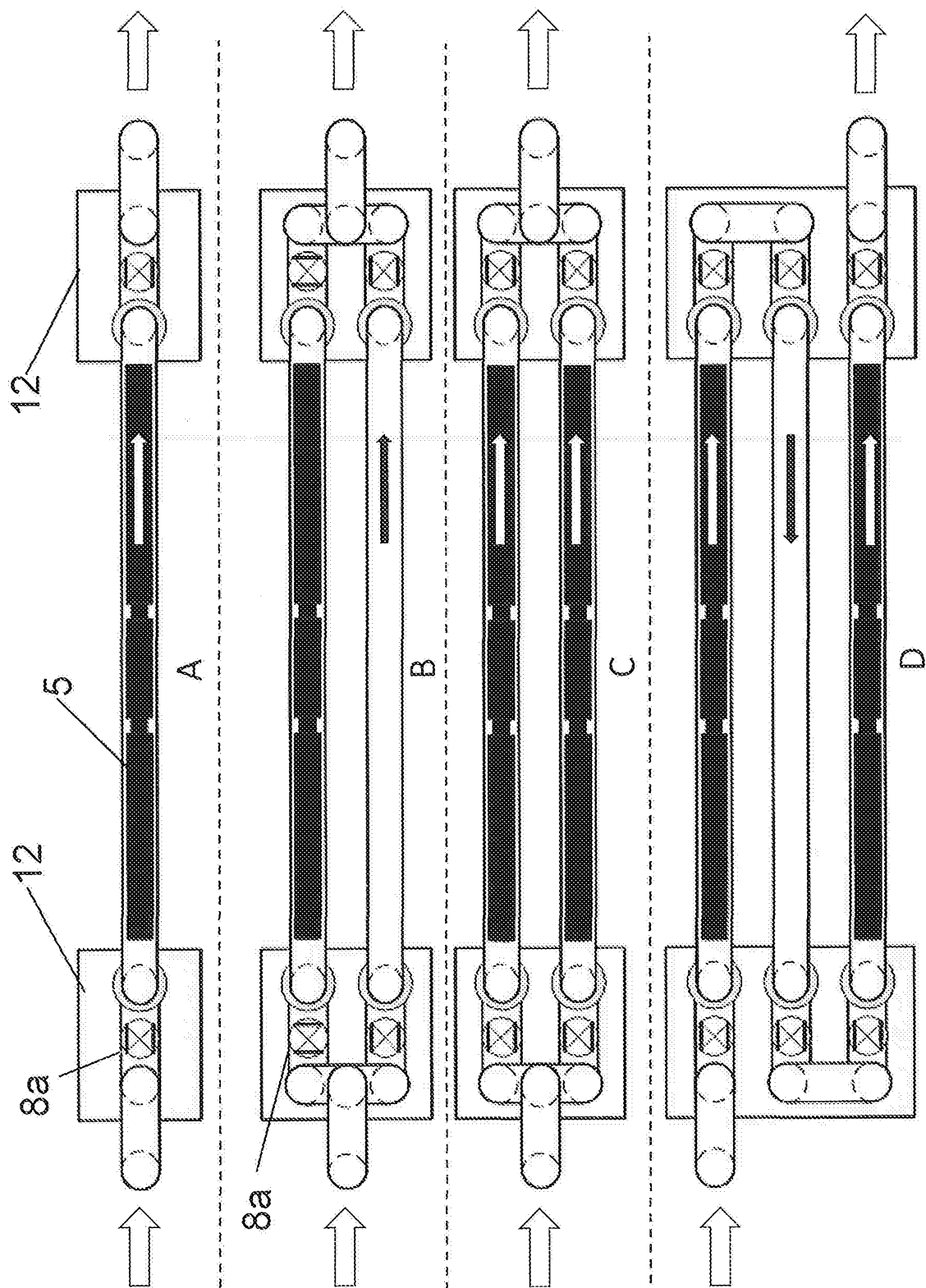
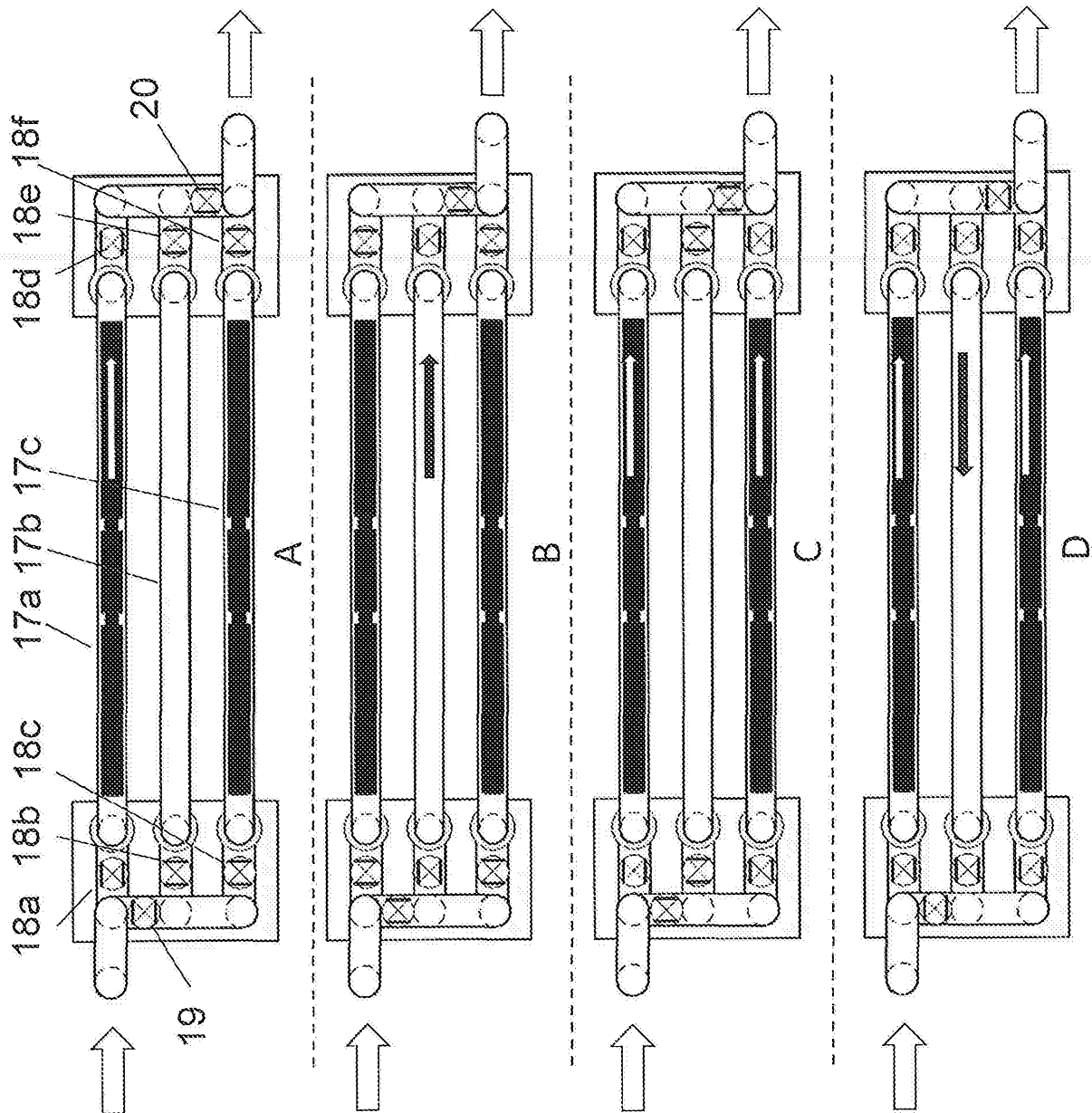


Figure 7



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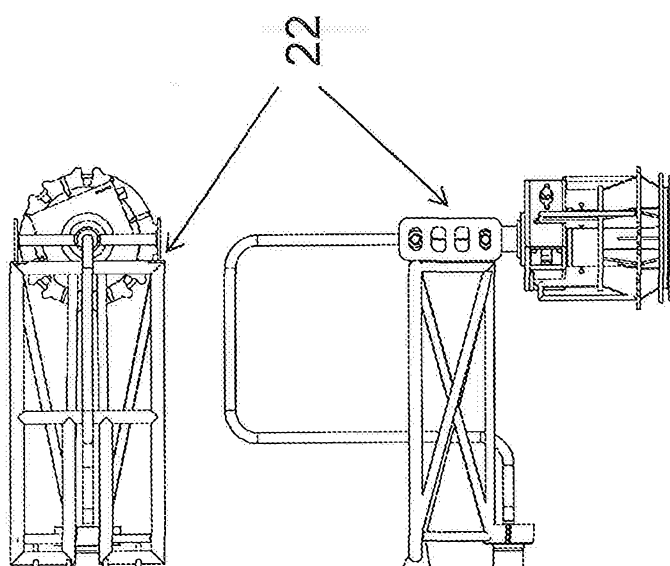


Figure 9