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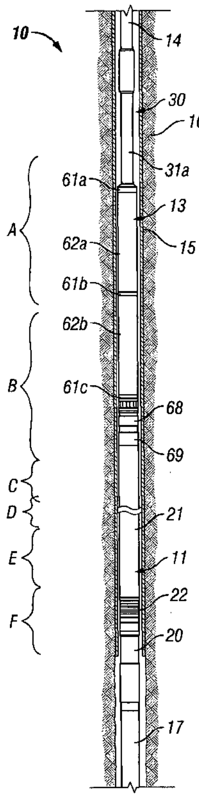


**FIG. 1A**

**(57) Abstract**: Novel hydraulic actuators and hydraulic setting assemblies are provided for use in downhole, oil and gas well tools. The novel hydraulic actuators include a cylindrical mandrel and an annular stationary sealing member connected to the mandrel. A hydraulic cylinder is slidably supported on the mandrel and stationary sealing member and is releasably fixed in position on the mandrel. The stationary sealing member divides the interior of the cylinder into a bottom hydraulic chamber and a top hydraulic chamber. An inlet port provides fluid communication into the bottom hydraulic chamber, and an outlet port provides fluid communication into the top hydraulic chamber. A balance piston is slidably supported within the top hydraulic chamber of the actuator. The piston includes an axially extending passageway. Fluid communication through the piston and between its upper and lower sides is controlled by a normally shut valve in the passageway. In the absence of relative movement between the mandrel and cylinder, the balance piston is able to slide in response to a difference in hydrostatic pressure between the outlet port, which is on one side of the piston, and the portion of the top hydraulic chamber that is on the bottom side of the piston.

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— *as to applicant's entitlement to apply for and be granted a patent (Rule 4.17(ii))*

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# ANCHOR AND HYDRAULIC SETTING ASSEMBLY

## FIELD OF THE INVENTION

The present invention relates to downhole tools used in oil and gas well drilling operations and, more particularly, to a hydraulic setting assembly which may be used to actuate anchors for well liners and other downhole tools and to tools and methods utilizing the novel hydraulic setting assembly.

## BACKGROUND OF THE INVENTION

Hydrocarbons, such as oil and gas, may be recovered from various types of subsurface geological formations. The formations typically consist of a porous layer, such as limestone and sands, overlaid by a nonporous layer. Hydrocarbons cannot rise through the nonporous layer, and thus, the porous layer forms a reservoir in which hydrocarbons are able to collect. A well is drilled through the earth until the hydrocarbon bearing formation is reached. Hydrocarbons then are able to flow from the porous formation into the well.

In what is perhaps the most basic form of rotary drilling methods, a drill bit is attached to a series of pipe sections referred to as a drill string. The drill string is suspended from a derrick and rotated by a motor in the derrick. As the drilling progresses downward, the drill string is extended by adding more pipe sections.

A drilling fluid or "mud" is pumped down the drill string, through the bit, and into the well bore. This fluid serves to lubricate the bit and carry cuttings from the drilling process back to the surface. As a well bore is drilled deeper and passes through hydrocarbon producing formations, however, the production of hydrocarbons must be controlled until the well is completed and the necessary production equipment has been installed. The drilling fluid also is used to provide that control. That is, the hydrostatic pressure of drilling fluid in the well bore relative to the hydrostatic pressure of hydrocarbons in the formation is adjusted by varying the density of the drilling fluid, thereby controlling the flow of hydrocarbons from the formation.

When the drill bit has reached the desired depth, larger diameter pipes, or casings, are placed in the well and cemented in place to prevent the sides of the borehole from caving in. The casing then is perforated at the level of the oil bearing formation so oil can enter the cased well. If necessary, various completion processes are performed to enhance the ultimate flow of oil from the formation. The drill string is withdrawn and replaced with a production string. Valves and other production equipment are installed in the well so that the hydrocarbons may flow in a controlled manner from the formation, into the cased well bore, and through the production string up to the surface for storage or transport.

This simplified drilling process, however, is rarely possible in the real world. For various reasons, a modern oil well will have not only a casing extending from the surface, but also one or more pipes, *i.e.*, casings, of smaller diameter running through all or a part of the casing. When those "casings" do not extend all the way to the surface, but instead are mounted in another casing, they are referred to as "liners." Regardless of the terminology, however, in essence the modern oil well typically includes a number of tubes wholly or partially within other tubes.

Such "telescoping" tubulars, for example, may be necessary to protect groundwater from exposure to drilling mud. A liner can be used to effectively seal the aquifer from the borehole as drilling progresses. Also, as a well is drilled deeper, especially if it is passing through previously depleted reservoirs or formations of differing porosities and pressures, it becomes progressively harder to control production throughout the entire depth of the borehole. A drilling fluid that would balance the hydrostatic pressure in a formation at one depth might be too heavy or light for a formation at another depth. Thus, it may be necessary to drill the well in stages, lining one section before drilling and lining the next section. Portions of existing casing also may fail and may need to be patched by installing liners within damaged sections of the casing.

The traditional approach to installing a liner in an existing casing has been to connect or "tie" the liner into an anchor, that is, a "liner hanger." Conventional anchors have included various forms of mechanical slip mechanisms that are connected to the liner. The slips themselves typically are in the form of cones or wedges having teeth or roughened surfaces. The typical hanger will include a relatively large number of slips, as many as six or more. A running and/or setting tool is used to position the anchor in place and drive the slips from their initial, unset position, into a set position where they are able to bite into and engage the existing casing. The setting mechanisms typically are either hydraulic, which are actuated by increasing the hydraulic pressure within the tool, or mechanical, which are actuated by rotating, lifting, or lowering the tool, or some combination thereof.

Such mechanical slip hangers may be designed to adequately support the weight of long liners. In practice, however, the wedges, cones, and the like that are intended to grip the existing casing may partially extend as the tool is run through existing casing and can cause the hanger to get stuck. They also may break off and interfere with other tools already in the well or make it difficult to run other tools through the casing at a later time. Moreover, separate "packers" must be used with such anchors if a seal is required between the liner and the existing casing.

One approach to avoiding such problems has been to eliminate in a sense the anchor entirely. That is, instead of tying a liner into an anchor, a portion of the liner itself is expanded into contact with an existing casing, making the liner essentially self-supporting and self-sealing. Thus, the liner conduit is made of sufficiently ductile metal to allow radial expansion of the liner, or more commonly, a portion of the liner into contact with existing casing. Various mechanisms, both hydraulic and mechanical, are used to expand the liner. Such approaches, however, all rely on direct engagement of, and sealing between the expanded liner and the existing casing.

For example, U.S. Pat. 6,763,893 to B. Braddick discloses a patch liner assembly that is used, for example, to repair existing casing. The patch assembly comprises a pair of expandable conduits, that is, an upper expandable liner and a lower expandable liner. The expandable liners are connected to the ends of a length of "patch" conduit. The patch assembly is set within the casing by actuating sets of expanding members that radially expand a portion of each expandable liner into engagement with the casing. Once expanded, the expanded portion of the liners provide upper and lower seals that isolate the patched portion of the existing casing. The expanded liners, together with the patch conduit, thereafter provide a passageway for fluids or for inserting other tubulars or tools through the well.

U.S. Pat. 6,814,143 to B. Braddick and U.S. Pat. 7,278,492 to B. Braddick disclose patch liner assemblies which, similar to Braddick '893, utilize a pair of expandable liners connected via a length of patch conduit. The upper and lower liners are expanded radially outward via a tubular expander into sealing engagement with existing casing. Unlike the expanding members in Braddick '893, however, the tubular expanders disclosed in Braddick '143 and '492 are not withdrawn after the liner portions have been expanded. They remain in the expanded, set liner such that they provide radial support for the expanded portions of the liner.

U.S. Pat. 7,225,880 to B. Braddick discloses an approach similar to Braddick '143 and '492, except that it is applied in the context of extension liners, that is, a smaller diameter liner extending downward from an existing, larger diameter casing. An expandable liner is expanded radially outward into sealing engagement with the existing casing via a tubular expander. The tubular expander is designed to remain in the liner and provide radial support for the expanded liner.

U.S. Pat. 7,387,169 to S. Harrell *et al.* also discloses various methods of hanging liners and tying in production tubes by expanding a portion of the tubular via, *e.g.*, a rotating expander tool. All such methods rely on creating direct contact and seals between the expanded portion of the tubular and the existing casing.

Such approaches have an advantage over traditional mechanical hangers. The external surface of the liner has no projecting parts and generally may be run through existing conduit more reliably than mechanical liner hangers. The expanded liner portion also not only provides an anchor for the rest of the liner, but it also creates a seal between the liner and the existing casing, thus reducing the need for a separate packer. Nevertheless, they suffer from significant drawbacks

First, because part of it must be expandable, the liner is necessarily is fabricated from relatively ductile metals. Such metals typically have lower yield strengths, thus limiting the amount of weight and, thereby, the length of liner that may be supported in the existing casing. Shorter liner lengths, in deeper wells, may require the installation of more liner sections, and thus, significantly greater installation costs. This problem is only exacerbated by the fact that expansion creates a weakened area between the expanded portion and the unexpanded portion of the liner. This weakened area is a potential failure area which can damage the integrity of the liner.

Second, it generally is necessary to expand the liner over a relatively long portion in order to generate the necessary grip on the existing casing. Because it must be fabricated from relatively ductile metal, once expanded, the liner portion tends to relax to a greater degree than if the liner were made of harder metal. This may be acceptable when the load to be supported is relatively small, such as a short patch section. It can be a significant limiting factor, however, when the expanded liner portion is intended to support long, heavy liners.

Thus, some approaches, such as those exemplified by Braddick '143 and '492, utilize expanders that are left in the liner to provide radial support for the expanded portion of the liner. Such designs do offer some benefits, but the length of liner which must be expander still can be substantial, especially as the weight of the liner string is increased. As the length of the area to be expanded increases the forces required to complete the expansion generally increase as well. Thus, there is progressively more friction between the expanding tool and the liner being expanded and more setting force is required to overcome that increasing friction. The need for greater setting forces over longer travel paths also can increase the chances that liner will not be completely set.

Moreover, the liner necessarily must have an external diameter smaller than the internal diameter of the casing into which it will be inserted. This clearance, especially for deep wells where a number of progressively smaller liners will be hung, preferably is as small as possible so as to allow the greatest internal diameter for the liner. Nevertheless, if the tool is to be passed reliably through existing casing, this clearance is still relatively large, and therefore, the liner portion is expanded to a significant degree.

Thus, it may not be possible to fabricate the liner from more corrosion resistant alloys. Such alloys typically are harder and less ductile. In general, they may not be expanded, or expanded only with much higher force, to a degree sufficient to close the gap and grip the existing casing.

Another reality facing the oil and gas industry is that most of the known shallow reservoirs have been drilled and are rapidly being depleted. Thus, it has become necessary to drill deeper and deeper wells to access new reserves. Many operations, such as mounting a liner, can be practiced with some degree of error at relatively shallow depths. Similarly, the cost of equipment failure is relatively cheap when the equipment is only a few thousand feet from the surface.

When the well is designed to be 40,000 feet or even deeper, such failures can be costly in both time and expense. Apart from capital expenses for equipment, operating costs for modern offshore rigs can be $500,000 or more a day. There is a certain irony too in the fact that failures are not only more costly at depth, but that avoiding such failures is also more difficult. Temperature and pressure conditions at great depths can be extreme, thus compounding the problem of designing and building tools that can be installed and will function reliably and predictably.

In particular, hydraulic actuators are commonly employed in downhole tools to generate force and movement, especially linear movement within the tool as may be required to operate the tool. They typically include a mandrel which is connected to a work string. A stationary piston is connected to the mandrel, and a hydraulic cylinder is mounted on, and can slide over the mandrel and the stationary piston. The stationary piston divides the interior of the cylinder into two hydraulic chambers, a top chamber and a bottom chamber. An inlet port allows fluid to flow through the mandrel into the bottom hydraulic chamber, which in turn urges the cylinder downward and away from the stationary piston. As the cylinder moves downward, fluid is able to flow out of the top hydraulic chamber via an outlet port. The movement of the cylinder then may be used to actuate other tool components.

Hydraulic actuators, therefore, can provide an effective mechanism for creating relative movement within a tool, and they are easily actuated from the surface simply by increasing the hydraulic pressure within the tool. Such actuators, however, can be damaged by the hostile environment in which they must operate. The hydrostatic pressures encountered in a well bore can be extreme and imbalances between the pressure in the mandrel and outside the actuator are commonly encountered. If the ports are closed while the tool is being run into a well, such pressure differentials will not cause unintended movement of the actuator, but they can impair subsequent operation of the actuator by deforming the actuator cylinder. Such problems can be avoided by immobilizing the cylinder through other means and simply leaving the ports open to avoid any imbalance of hydrostatic pressure that might deform the actuator cylinder. Fluids in a well bore, however, typically carry a large amount of gritty, gummy debris. The ports and hydraulic chambers in the actuator, therefore, typically are filled with heavy grease before they are run into the well. Nevertheless, the tool may be exposed to wellbore fluid for prolonged periods and under high pressure, and debris still can work its way into conventional actuators and impair their operation.

The increasing depth of oil wells also means that the load capacity of a connection between an existing casing and a liner, whether achieved through mechanical liner hangers or expanded liners, is increasingly important. Higher load capacities may mean that the same depth may be reached with fewer liners. Because operational costs of running a drilling rig can be so high, significant cost savings may be achieved if the time spent running in an extra liner can be avoided.

Ever increasing operational costs of drilling rigs also has made it increasingly important to combine operations so as to reduce the number of trips into and out of a well. For example, especially for deep wells, significant savings may be achieved by drilling and lining a new section of the well at the same time. Thus, tools for setting liners have been devised which will transmit torque from a work string to a liner. A drill bit is attached to the end of the liner, and the liner is rotated.

Torque is typically transmitted through the tool by a serious of tubular sections threaded together via threaded connectors. The rotational forces transmitted through the tool, however, can be substantial and can damage threaded connections by over-tightening the threads. In addition, it often is useful to rotate opposite to the threads. Such reverse, or "left-handed" rotation may be useful in the actuation and operation of various mechanisms, but it can loosen the connection. In either event, if connections in the torque transmitting components are impaired, it may be difficult or impossible to operate the tool. Set screws, pins, keys, and the like, therefore, have been used to secure a connector, but such approaches are susceptible to failure.

Such disadvantages and others inherent in the prior art are addressed by the subject invention, which now will be described in the following detailed description and the appended drawings.

## SUMMARY OF THE INVENTION

The subject invention provides for novel hydraulic actuators and hydraulic setting assemblies which may be used in downhole, oil and gas well tools. The novel hydraulic actuators include a cylindrical mandrel and an annular stationary sealing member connected to the mandrel. A hydraulic cylinder is slidably supported on the mandrel and stationary sealing member and is releasably fixed in position on the mandrel. The stationary sealing member divides the interior of the cylinder into a bottom hydraulic chamber and a top hydraulic chamber. An inlet port provides fluid communication into the bottom hydraulic chamber, and an outlet port provides fluid communication into the top hydraulic chamber.

The novel actuators further include a balance piston. The balance piston is slidably supported within the top hydraulic chamber of the actuator, preferably on the mandrel. The balance piston includes a passageway extending axially through the balance piston. Fluid communication through the piston and between its upper and lower sides is controlled by a normally shut valve in the passageway. Thus, in the absence of relative movement between the mandrel and the cylinder, the balance piston is able to slide in response to a difference in hydrostatic pressure between the outlet port, which is on one side of the balance piston, and the portion of the top hydraulic chamber that is on the bottom side of the balance piston. The novel actuators, therefore, are less susceptible to damage caused by differences in the hydrostatic pressure inside and outside of the actuator. Moreover, the balance piston of the novel actuators is able to prevent the ingress of debris into the actuator.

The normally shut valve in the novel actuators preferably is a rupturable diaphragm. Other preferred embodiments include a pressure release device allowing controlled release of pressure from the top hydraulic cylinder.

In other aspects, the subject invention provides for anchor assemblies that are intended for installation within an existing conduit. The novel anchor assemblies comprise a nondeformable mandrel, an expandable metal sleeve, and a swage. The expandable metal sleeve is carried on the outer surface of the mandrel. The swage is supported for axial movement across the mandrel outer surface from a first position axially proximate to the sleeve to a second position under the sleeve. The movement of the swage from the first position to the second position expands the sleeve radially outward into contact with the existing conduit.

Preferably, the swage of the novel anchor assemblies has an inner diameter substantially equal to the outer diameter of the mandrel and an outer diameter greater than the inner diameter of the expandable metal sleeve. The mandrel of the novel anchor assemblies preferably is fabricated from high yield metal alloys and, most preferably, from corrosion resistant high yield metal alloys.

The novel anchor assemblies preferably have a load capacity of at least 100,000 lbs, more preferably, a load capacity of at least 250,000 lbs, and most preferably a load capacity of at least 500,000 lbs. The novel anchors thus are able to support the weight of liners and other relative heavy downhole tools and well components.

The novel anchor assemblies are intended to be used in combination with a tool for installing the anchor in a tubular conduit. The anchor and tool assembly comprises the anchor assembly, a running assembly, and a setting assembly. The running assembly releasably engages the anchor assembly. The setting assembly is connected to the running assembly and engages the swage and moves it from its first position to its second position.

As will become more apparent from the detailed description that follows, once the sleeve is expanded, the mandrel and swage provide radial support for the sleeve, thereby enhancing the load capacity of the novel anchors. Conversely, by enhancing the radial support for the sleeve, the novel anchors may achieve, as compared to expandable liners, equivalent load capacities with a shorter sleeve, thus reducing the amount of force required to set the novel anchors. Moreover, unlike expandable liners, the mandrel of the novel anchor assemblies is substantially nondeformable and may be made from harder, stronger, more corrosion resistant metals.

In yet other aspects the subject invention provides for novel clutch mechanisms which may be and preferably are used in the mandrel of the novel anchor and tool assemblies and in other sectioned conduits and shafts used to transmit torque. They comprise shaft sections having threads on the ends to be joined and prismatic outer surfaces adjacent to their threaded ends. A threaded connector joins the threaded ends of the shaft sections. The connector has axial splines. A pair of clutch collars is slidably supported on the prismatic outer surfaces of the shaft sections. The clutch collars have prismatic inner surfaces that engage the prismatic outer surfaces of the shaft sections and axial splines that engage the axial splines on the threaded connector. Preferably, the novel clutch mechanisms also comprise recesses adjacent to the mating prismatic surfaces that allow limited rotation of the clutch collars on the prismatic shaft sections to facilitate engagement and disengagement of the mating prismatic surfaces. Thus, as will become more apparent from the detailed description that follows, the novel clutch mechanisms provide reliable transmission of large amounts of torque through sectioned conduits and other drive shafts without damaging the threaded connections.

Those and other aspects of the invention, and the advantages derived therefrom, are described in further detail below.

## BRIEF DESCRIPTION OF THE DRAWINGS

**FIGURE 1A** is a perspective view of a preferred embodiment **10** of the tool and anchor assemblies of the subject invention showing liner hanger tool **10** and liner hanger **11** at depth in an existing casing **15** (shown in cross-section);

**FIG. 1B** is a perspective view similar to **FIG. 1A** showing preferred liner hanger **11** of the subject invention after it has been set in casing **15** by various components of tool **10** and the running and setting assemblies of tool **10** have been retrieved from casing **15**;

**FIG. 2A** is an enlarged quarter-sectional view generally corresponding to section **A** of tool **10** shown in **FIG. 1A** showing details of a preferred embodiment **13** of the setting assemblies of the subject inventions showing setting tool **13** in its run-in position;

**FIG. 2B** is a quarter-sectional view similar to **FIG. 2A** showing setting tool **13** in its set position;

**FIG. 3A** is an enlarged quarter-sectional view generally corresponding to section **B** of tool **10** shown in **FIG. 1A** showing additional details of setting tool **13** and portions of liner hanger **11** in their run-in position;

**FIG. 3B** is a view similar to **FIG. 3A** showing setting tool **13** and liner hanger **11** in their set position;

**FIG. 4A** is an enlarged quarter-sectional view generally corresponding to section **C** of tool **10** shown in **FIG. 1A** showing further details of setting tool **13** and portions of liner hanger **11** in their run-in position;

**FIG. 4B** is a view similar to **FIG. 4A** showing setting tool **13** and liner hanger **11** in their set position;

**FIG. 5A** is an enlarged quarter-sectional view generally corresponding to section **D** of tool **10** shown in **FIG. 1A** showing additional details of setting tool **13** and portions of liner hanger **11** in their run-in position;

**FIG. 5B** is a view similar to **FIG. 5A** showing setting tool **13** and liner hanger **11** in their set position;

**FIG. 6A** is an enlarged quarter-sectional view generally corresponding to section **E** of tool **10** shown in **FIG. 1A** showing details of a preferred embodiment of the running assemblies of the subject invention showing running tool **12** and liner hanger **11** in their run-in position;

**FIG. 6B** is a view similar to **FIG. 6A** showing running tool **12** and liner hanger **11** in their set position;

**FIG. 6C** is a view similar to **FIGS. 6A** and **6B** showing running tool **12** and liner hanger **11** in their release position;

**FIG. 7A** is an enlarged quarter-sectional view generally corresponding to section **F** of tool **10** shown in **FIG. 1A** showing additional details of liner hanger **11** and running tool **12** in their run-in position;

**FIG. 7B** is a view similar to **FIG. 7A** showing liner hanger **11** and running tool **12** in their set position;

**FIG. 7C** is a view similar to **FIGS. 7a** and **7B** showing liner hanger **11** and running tool **12** in their release position;

**FIG. 8A** is a partial, quarter-sectional view of a tool mandrel **30** of tool **10** shown in **FIG. 1A** (that portion located generally in section **A** of **FIG. 1A)** showing details of a preferred embodiment **32** of novel clutch mechanisms of the subject invention;

**FIG. 8B** is a view similar to **FIG. 7A** showing connector assembly **32** in an uncoupled position;

**FIG. 9A** is a cross-sectional view taken along line **9A-9A** of **FIG. 8A** of connector assembly **32**; and

**FIG. 9B** is a view similar to **FIG. 8A** taken along line **9B-9B** of **FIG. 8B** showing connector assembly **32** in an uncoupled position.

Those skilled in the art will appreciate that line breaks along the vertical length of the tool may eliminate well known structural components for inter connecting members, and accordingly the actual length of structural components is not represented.

## DESCRIPTION OF ILLUSTRATIVE EMBODIMENTS

The anchor assemblies of the subject invention are intended for installation within an existing conduit. They comprise a nondeformable mandrel, an expandable metal sleeve, and a swage. The expandable metal sleeve is carried on the outer surface of the mandrel. The swage is supported for axial movement across the mandrel outer surface from a first position axially proximate to the sleeve to a second position under the sleeve. The movement of the swage from the first position to the second position expands the sleeve radially outward into contact with the existing conduit.

The novel anchor assemblies are intended to be used in combination with a tool for installing the anchor in a tubular conduit. The anchor and tool assembly comprises the anchor assembly, a running assembly, and a setting assembly. The running assembly releasably engages the anchor assembly. The setting assembly is connected to the running assembly and engages the swage and moves it from its first position to its second position.

The anchor and tool assembly is used, for example, in drilling oil and gas wells and to install liners and other well components. It is connected to a work string which can be raised, lowered, and rotated as desired from the surface of the well. A liner or other well component is attached to the anchor assembly mandrel. The assembly then is lowered into the well through an existing conduit to position the anchor assembly at the desired depth. Once the anchor assembly is in position, the swage is moved axially over the mandrel outer surface by a setting assembly. More particularly, the swage is moved from a position proximate to the expandable metal sleeve to a position under the sleeve, thereby expanding the sleeve radially outward into contact with the existing conduit. Once the metal sleeve has been expanded, the tool is manipulated to release the running assembly from the anchor assembly, and the running and setting assemblies are retrieved from the conduit to complete installation of the liner or other well component.

For example, **FIG. 1A** shows a preferred liner hanger tool **10** of the subject invention. Tool **10** includes a preferred embodiment **11** of the novel liner hangers which is connected to a running tool **12** (not shown) and a setting tool **13**. Tool **10** is connected at its upper end to a work string **14** assembled from multiple lengths of tubular sections threaded together through connectors. Work string **14** may be raised, lowered, and rotated as needed to transport tool **10** through an existing casing **15** cemented in a borehole through earth **16**. Work string **14** also is used to pump fluid into tool **10** and to manipulate it as required for setting hanger **11**.

***Hanger Assembly***

Hanger 11 includes a hanger mandrel **20**, a swage **21**, and a metal sleeve **22**. A liner **17** is attached to the lower end of tool **10**, more specifically to hanger mandrel **20** of hanger **11**. Liner **17** in turn is assembled from multiple lengths of tubular sections threaded together through connectors. In addition, liner **17** typically will have various other components as may be need to perform various operations in the well, both before and after setting hanger **11**. For example, liner **17** typically will be cemented in place. Thus, tool **10** also will include, or the liner **17** will incorporate various well components used to perform such cementing operations, such as a slick joint, cement packoffs, plug landing collars, and the like (not shown). Operation of tool **10**, as discussed in detail below, is accomplished in part by increasing hydraulic pressure within tool **10**. Thus, when liner **17** is not cemented in place, tool **10** or liner **17** preferably incorporate some mechanism to allow pressure to be built up in work string **14**, such as a seat (not shown) onto which a ball may be dropped. Importantly, liner **17** also may include a drill bit (not shown) so that the borehole may be drilled and extended as liner **17** and tool **10** are lowered through existing casing **15**.

It will be appreciated, however, that in its broadest embodiments, the anchor and tool assemblies of the subject invention do not comprise any specific liner assemblies or a liner. The anchor assemblies may be used to install a variety of liner assemblies, and in general, may be used to install any other downhole tool or component that requires anchoring within a conduit, such as whipstocks, packers, bridge plugs, cement plugs, frac plugs, slotted pipe, and polished bore receptacles (PBRs). Similarly, while preferred liner hanger tool **10** is exemplified by showing a liner suspended in tension from the anchor assembly, the novel anchor assemblies may also be used to support liners or other well components extending above the anchor assembly, or to secure such components in resistance to torsional forces.

Moreover, as used in industry, a "casing" is generally considered to be a tubular conduit lining a well bore and extending from the surface of the well. Likewise, a "liner" is generally considered to be a tubular conduit that does not extend from the surface of the well, and instead is supported within an existing casing or another liner. In the context of the subject invention, however, it shall be understood that "casing" shall refer to any existing conduit in the well into which the anchor assembly will be installed, whether it extends to the surface or not, and "liner" shall refer to a conduit having an external diameter less than the internal diameter of the casing into which the anchor assembly is installed.

Even more broadly, it will be appreciated that the tool has been exemplified in the context of casings and liners used in drilling oil and gas wells. The invention, however, is not so limited in its application. The novel tool and anchor assemblies may be used advantageously in other conduits where it is necessary to install an anchor by working a tool through an existing conduit to install other tools or smaller conduits.

It also will be appreciated that the figures and description refer to tool **10** as being vertically oriented. Modern wells, however, often are not drilled vertically and, indeed, may extend horizontally through the earth. The novel tool and anchor assemblies also may be used in horizontal wells. Thus, references to up, down, upward, downward, above, below, upper, lower, and the like shall be understood as relative terms in that context.

In **FIG. 1A**, liner hanger tool **10** is shown in its "run-in" position. That is, it has been lowered into existing casing **15** to the depth at which hanger **11** will be installed. Hanger **11** has not yet been "set" in casing **15**, that is, it has not been installed. **FIG. 1B** shows hanger **11** after it has been installed, that is, after it has been set in casing **15** and running tool **12** and setting tool **13** have been retrieved from the well. It will be noted in comparing the two figures that hanger mandrel **20** has remained in substantially the same position relative to casing **15**, that swage **21** has travelled down tool **10** approximately the length of sleeve **22**, and that sleeve **22** has been expanded radially outward into contact with casing **15**.

Further details regarding liner hanger **11** may be seen in **FIGS. 7**, which show liner hanger **11** and various components of running tool **12**. **FIG. 7A** shows hanger **11** in its "run-in" position, **FIG. 7B** shows hanger **11** after it has been "set," and **FIG. 7C** shows hanger tool **11** after it has been "released" from running tool **12**.

As may be seen therefrom, hanger mandrel **20** is a generally cylindrical body providing a conduit. It provides a connection at its lower end to, *e.g.*, a liner string (such as liner **17** shown in **FIGS. 1**) through threaded connectors or other conventional connectors. Other liners, such as a patch liner, and other types of well components or tools, such as a whipstock, however, may be connected to mandrel **20**, either directly or indirectly. Thus, while described herein as part of liner hanger **11**, it also may be viewed as the uppermost component of the liner or other well component that is being installed. As will be described in further detail below, mandrel **20** also is releasably engaged to running tool **12**.

As may be seen from **FIG. 7A**, in the run-in position the upper portion of mandrel **20** provides an outer surface on which are carried both swage **21** and expandable metal sleeve **22**. Swage **21** and expandable metal sleeve **22**, like mandrel **20**, also are generally cylindrical bodies.

Swage **21** is supported for axial movement across the outer surface of mandrel **20**. In the run-in position, it is proximate to expandable metal sleeve **22**, *i.e.*, it is generally axially removed from sleeve **22** and has not moved into a position to expand sleeve **22** into contact with an existing casing. In theory it may be spaced some distance therefrom, but preferably, as shown in **FIG. 7A**, swage **21** abuts metal sleeve **22**. Sleeve **22** also is carried on the outer surface of mandrel **20**. Preferably, sleeve **22** is restricted from moving upward on mandrel **20** by swage **21** as shown and restricted from moving downward by its engagement with annular shoulder **23** on mandrel **20**. It may be restricted, however, by other stops, pins, keys, set screws and the like as are known in the art.

By comparing **FIG. 7A** and **FIG. 7B**, it may be seen that hanger **11** is set by actuating swage **21**, as will be described in greater detail below, to move across the outer surface of mandrel **20** from its run-in position, where it is proximate to sleeve **22**, to its set position, where it is under sleeve **22**. This downward movement of swage **21** causes metal sleeve **22** to expand radially into contact with an existing casing (such as casing **15** shown in **FIGS 1**).

Movement of swage **21** under sleeve **22** preferably is facilitated by tapering the lower end of swage **21** and the upper end of sleeve **22**, as seen in **FIG. 7A**. Preferably, the facing surfaces of mandrel **20**, swage **21**, and sleeve **22** also are polished smooth and/or are provided with various structures to facilitate movement of swage **21** and to provide seals therebetween. For example, outer surface of mandrel **20** and inner surface of sleeve **22** are provided with annular bosses in the areas denoted by reference numeral **24**. Those bosses not only reduce friction between the facing surfaces as swage **21** is being moved, but when swage **21** has moved into place under sleeve **22**, though substantially compressed and/or deformed, they also provide metal-to-metal seals between mandrel **20**, swage **21**, and sleeve **22**. It will be understood, however, that annular bosses may instead be provided on the inner and outer surfaces of swage **21**, or on one surface of swage **21** in lieu of bosses on either mandrel **20** or sleeve **22**. Coatings also may be applied to the facing surfaces to reduce the amount of friction resisting movement of swage **21** or to enhance the formation of seals between facing surfaces.

The outer surface of swage **21**, or more precisely, that portion of the outer surface of swage **21** that will move under sleeve **22** preferably is polished smooth to reduce friction therebetween. Likewise, the inner surface of swage **21** preferably is smooth and polished to reduce friction with mandrel **20**. Moreover, once hanger **11** is installed in an existing casing, the upper portion of swage **21** is able to provide a polished bore receptacle into which other well components may be installed.

Preferably, the novel anchor assemblies also include a ratchet mechanism that engages the mandrel and swage and resists reverse movement of the swage, that is, movement of the swage back toward its first position, in which it is axially proximate to the sleeve, and away from its second position, where it is under the sleeve. Liner hanger **11**, for example, is provided with a ratchet ring **26** mounted between mandrel **20** and swage **21**. Ratchet ring **26** has pawls that normally engage corresponding detents in annular recesses on, respectively, the outer surface of mandrel **20** and the inner surface of swage **21**. Ratchet ring **26** is a split ring, allowing it to compress circumferentially, depressing the pawls and allowing them to pass under the detents on swage **21** as swage **21** travels downward in expanding sleeve **22**. The pawls on ring **26** are forced into engagement with the detents, however, if there is any upward travel of swage **21**. Thus, once set, relative movement between mandrel **20**, swage **21**, and sleeve **22** is resisted by ratchet ring **26** on the one hand and mandrel shoulder **23** on the other.

It will be appreciated from the foregoing that in the novel anchor assemblies, or at least in the area of travel by the swage, the effective outer diameter of the mandrel and the effective inner diameter of the swage are substantially equal, whereas the effective outer diameter of the swage is greater than the effective inner diameter of sleeve. Thus, for example and as may be seen in **FIG. 7B**, swage **21** acts to radially expand sleeve **22** and, once sleeve **22** is expanded, mandrel **20** and swage **21** concentrically abut and provide radial support for sleeve **22**, thereby enhancing the load capacity of hanger **11**. Conversely, by enhancing the radial support for sleeve **22**, hanger **11** may achieve equivalent load capacities with a shorter sleeve **22**, thus reducing the amount of force required to set hanger **11**.

By effective diameter it will be understood that reference is made to the profile of the part as viewed axially along the path of travel by swage **21**. In other words, the effective diameter takes into account any protruding structures such as annular bosses which may project from the nominal surface of a part. Similarly, when projections such as annular bosses are provided on mandrel **20** or swage **21**, the outer diameter of mandrel **20** will be slightly greater than the inner diameter of swage **21** so that a seal may be created therebetween. “Substantially equal” is intended to encompass such variations, and other normal tolerances in tools of this kind.

Moreover, since hanger mandrel **20** is in a sense the uppermost component of liner **17** to be installed, it will be appreciated that its inner diameter preferably is at least as great as the inner diameter of liner **17** which will be installed. Thus, any further constriction of the conduit being installed in the well will be avoided. More preferably, however, it is substantially equal to the inner diameter of liner **17** so that mandrel **20** may be made as thick as possible.

It also will be appreciated that the mandrel of the novel anchor assemblies is substantially nondeformable, *i.e.*, it resists significant deformation when the swage is moved over its outer surface to expand the metal sleeve. Thus, expansion of the sleeve is facilitated and the mandrel is able to provide significant radial support for the expanded sleeve. It is expected that some compression may be tolerable, on the order of a percent or so, but generally compression is kept to a minimum to maximize the amount of radial support provided. Thus, the mandrel of the novel anchors preferably is fabricated from relatively hard ferrous and non-ferrous metal alloys and, most preferably, from such metal alloys that are corrosion resistant. Suitable ferrous alloys include nickel-chromium-molybdenum steel and other high yield steel. Non-ferrous alloys include nickel, iron, or cobalt superalloys, such as Inconel, Hastelloy, Waspaloy, Rene, and Monel alloys. The superalloys are corrosion resistant, that is, they are more resistant to the chemical, thermal, pressure, and other corrosive conditions commonly encountered in oil and gas wells. Thus, superalloys or other corrosion resistant alloys may be preferable when corrosion of the anchor is a potential problem.

The swage of the novel anchors also is preferably fabricated from such materials. By using such high yield alloys, not only is expansion of the sleeve facilitated, but the mandrel and swage also are able to provide significant radial support for the expanded sleeve and the swage may be made more resistant to corrosion as well.

On the other hand, the sleeve of the novel anchor assemblies preferably is fabricated from ductile metal, such as ductile ferrous and non-ferrous metal alloys. The alloys should be sufficiently ductile to allow expansion of the sleeve without creating cracks therein. Examples of such alloys include ductile aluminum, brass, bronze, stainless steel, and carbon steel. Preferably, the metal has an elongation factor of approximately 3 to 4 times the anticipated expansion of the sleeve. For example, if the sleeve is required to expand on the order of 3%, it will be fabricated from a metal having an elongation factor of from about 9 to about 12%. In general, therefore, the material used to fabricate the sleeve should have an elongation factor of at least 10%, preferably from about 10 to about 20%. At the same time, however, the sleeve should not be fabricated from material that is so ductile that it cannot retain its grip on an existing casing.

It also will be appreciated that the choice of materials for the mandrel, swage, and sleeve should be coordinated to provide minimal deformation of the mandrel, while allowing the swage to expand the sleeve without creating cracks therein. As higher yield materials are used in the mandrel and swage, it is possible to use progressively less ductile materials in the sleeve. Less ductile materials may provide the sleeve with greater gripping ability, but of course will require greater expansion forces.

Significantly, however, by using a ductile, expandable metal seal, and a nondeformable mandrel, it is possible to provide a strong, reliable seal with an existing casing, while avoiding the complexities of other mechanical hangers and the significant disadvantages of expandable liners. More specifically, the novel hangers do not have a weakened area such as exists at the junction of expanded and unexpanded portions of expandable liners. Thus, other factors being equal, the novel hangers are able to achieve higher load ratings.

In addition, expandable liners must be made relatively thick in part to compensate for the weakened area created between the expanded and unexpanded portions. The expandable sleeves of the novel hangers, however, are much thinner. Thus, other factors being equal, the expandable sleeves may be expanded more easily, which in turn reduces the amount of force that must be generated by the setting assembly.

Ductile alloys, from which both conventional expandable liners and the expandable sleeves of the novel hangers may be made, once expanded, can relax and cause a reduction in the radial force applied to an existing casing. Conventional tools have provided support for expanded liner portions by leaving the swage or other expanding member in the well. The nondeformable mandrel of the novel liner hangers, however, has substantially the same outer diameter as the internal diameter of the swage. Thus, both the mandrel and the swage are able to provide radial support for the expanded sleeve. Other factors being equal, that increased radial support reduces “relaxation” of the expanded, relatively ductile sleeve and, in turn, tends to increase the load capacity of the anchor. At the same time, the mandrel is quite easily provided with an internal diameter at least as great as the liner which will be installed, thus avoiding any further constriction of the conduit provided through the well.

Expandable liner hangers, since they necessarily are fabricated from ductile alloys which in general are less resistant to corrosion, are more susceptible to corrosion and may not be used, or must be used with the expectation of a shorter service life in corrosive environments. The mandrel of the novel hangers, however, may be made of high yield alloys that are much more resistant to corrosion. The expandable sleeve of the novel hangers are fabricated from ductile, less corrosion resistant alloys, but it will be appreciated that as compared to a liner, only a relatively small surface area of the sleeve will be exposed to corrosive fluids. The length of the seal formed by the sleeve also is much greater than the thickness of a liner, expanded or otherwise. Thus, the novel hangers may be expected to have longer service lives in corrosive environments.

The expandable sleeve of the novel anchor assemblies also preferably is provided with various sealing and gripping elements to enhance the seal between the expanded sleeve and an existing casing and to increase the load capacity of the novel hangers. For example, as may be seen in **FIGS. 7**, sleeve **22** is provided with annular seals **27** and radially and axially spaced slips **28** provided on the outer surface thereof. Annular seals may be fabricated from a variety of conventional materials, such as wound or unwound, thermally cured elastomers and graphite impregnated fabrics. Slips may be provided by conventional processes, such as by machining slips into the sleeve, or by soldering crushed tungsten-carbide steel or other metal particles to the sleeve surface with a thin coat of high nickel based solder or other conventional solders. When such seals and slips are used the sleeve also preferably is provided with gage protection to minimize contact between such elements and the casing wall as the anchor assembly is run into the well.

As will be appreciated by those skilled in the art, the precise dimensions of the expandable sleeve may be varied so as to, other factors being equal, to provide greater or lesser load capacity and to allow for greater or lesser expansion forces. The external diameter of the sleeve necessarily will be determined primarily by the inner diameter of the liner into which the anchor will be installed and the desired degree of expansion. The thickness of the sleeve will be coordinated with the tensile and ductile properties of the material used in the sleeve so as to provide the desired balance of load capacity and expandability. In general, the longer the sleeve, the greater the load capacity. Thus, the sleeve typically will have a length at least equal to its diameter, and preferably a length of at least 150% of the diameter, so as to provide sufficient surface area to provide load capacities capable of supporting relatively heavy liners and other downhool tools and well components. The novel anchor assemblies thus may be provided with load capacities of at least 100,000 lbs, more preferably, at least 250,000 lbs, and most preferably, at least 500,000 lbs.

***Clutch Mechanism***

As noted above, the novel anchor assemblies are intended to be used in combination with a tool for installing the anchor in a tubular conduit. For example, running tool **12** is used to releasably engage hanger **11** and setting tool **13** is used to actuate swage **21** and set sleeve **22**. There are a variety of mechanisms which may be incorporated into tools to provide such releasable engagement and actuation. In this respect, however, the subject invention does not encompass any specific tool or mechanism for releasably engaging, actuating, or otherwise installing the novel anchor assemblies. Preferably, however, the novel anchors are used with the tools disclosed herein. Those tools are capable of installing the novel anchors easily and reliably. Moreover, as now will be discussed in further detail, they incorporate various novel features and represent other embodiments of the subject invention.

Running tool **12** and setting tool **13**, as will be appreciated by comparing **FIGS. 2-7**, share a common tool mandrel **30**. Tool mandrel **30** provides a base structure to which the various components of liner hanger **11**, running tool **12**, and setting tool **13** are connected, directly or indirectly.

Tool mandrel **30** is connected at its upper end to a work string **14** (see **FIG. 1A**). Thus, it provides a conduit for the passage of fluids from the work string **14** that are used to balance hydrostatic pressure in the well and to hydraulically actuate setting tool **13** and, ultimately, swage **21**. Mandrel **30** also provides for transmission of axial and rotational forces from work string **14** as are necessary to run in the hanger **11** and liner **17**, drill a borehole during run-in, set the hanger **11**, and release and retrieve the running tool **12** and setting tool **13**, all as described in further detail below.

Tool mandrel **30** is a generally cylindrical body. Preferably, as illustrated, it comprises a plurality of tubular sections **31** to facilitate assembly of tool **10** as a whole. Tubular sections **31** may be joined by conventional threaded connectors. Preferably, however, the sections **31** of tool mandrel **30** are connected by novel clutch mechanisms of the subject invention.

The novel clutch mechanisms comprise shaft sections having threads on the ends to be joined. The shaft sections have prismatic outer surfaces adjacent to their threaded ends. A threaded connector joins the threaded ends of the shaft sections. The connector has axial splines. A pair of clutch collars is slidably supported on the prismatic outer surfaces of the shaft sections. The clutch collars have prismatic inner surfaces that engage the prismatic outer surfaces of the shaft sections and axial splines that engage the axial splines on the threaded connector. Preferably, the novel clutch mechanisms also comprise recesses adjacent to the mating prismatic surfaces that allow limited rotation of the clutch collars on the prismatic shaft sections to facilitate engagement and disengagement of the mating prismatic surfaces.

Accordingly, mandrel **30** of tool **10** includes a preferred embodiment **32** of the novel clutch mechanisms. More particularly, mandrel **30** is made up of a number of tubular sections **31** joined by novel connector assemblies **32**. Connector assemblies **32** include threaded connectors **33** and clutch collars **34**. **FIGS. 8-9** show the portion of mandrel **30** and connector assembly **32a** which is seen in **FIGS. 2** and which is representative of the connections used to make up mandrel **30**. As may be seen in those figures, lower end of tubular section **31a** and upper end of tubular section **31b** are threaded into and joined by threaded connector **33a**. The threads, as is common in the industry, are right-handed threads, meaning that the connection is tightened by rotating the tubular section to the right, *i.e.*, in a clockwise rotation. The novel clutch mechanisms, however, may be also be used in left-handed connections. Clutch collars **34a** and **34b** are slidably supported on tubular sections **31a** and **31b**, and when in their coupled or "made-up" position as shown in **FIG. 8A**, abut connector **33a**. Connector **33a** and collars **34a** and **34b** have mating splines which provide rotational engagement therebetween.

Tubular sections **31** have prismatic outer surfaces **35** adjacent to their threaded ends. That is, the normally cylindrical outer surfaces of tubular sections **31** have been cut to provide a plurality of flat surfaces extending axially along the tubular section such that, when viewed in cross section, flat surfaces define or can be extended to define a polygon. For example, as seen best in **FIG. 9A**, tubular section **31a** has octagonal prismatic outer surfaces **35**. The inner surface of clutch collar **34a** has mating octagonal prismatic inner surfaces **36**. Clutch collar **34b** is of similar construction. Thus, when in their coupled positions as shown in **FIG. 9A**, prismatic surfaces **35** and **36** provide rotational engagement between sections **31a** and **31b** and collars **34a** and **34b**. It will be appreciated, therefore, that torque may be transmitted from one tubular section **31** to another tubular section **31**, via collars **34** and connectors **33**, without applying torque to the threaded connections between the tubular sections **31**.

**FIGS. 8B** and **9B** show connector assembly **32a** in uncoupled states. It will be noted that prismatic surfaces **35** extend axially on tubular sections **31a** and **31b** and allow the splines on collars **34a** and **34b** to slide into and out of engagement with the splines on connector **33a**, as may be appreciated by comparing **FIGS. 8A** and **8B**. Recesses preferably are provided adjacent to the mating prismatic surfaces to facilitate that sliding. For example, as may be seen in **FIGS. 9**, recesses **37** are provided adjacent to prismatic surfaces **36** on collar **34a**. Those recesses allow collar **34a** to rotate to a limited degree on tubular sections **31a**. When rotated to the left, as shown in **FIG. 9B**, surfaces **35** and **36** are disengaged, and collar **34a** may slide more freely on tubular section **31a**. Thus, collars **34** may be more easily engaged and disengaged with connectors **33**. Once collars **34** have been moved into engagement with connectors **33**, collars **34** and connectors **33** may be rotated together in a clockwise direction to complete make-up of the connection. Preferably, set screws, pins, keys, or the like (not shown) then are installed to secure collars **34** and prevent them from moving axially along tubular sections **31**. Alternately, annular recesses (not shown) may be provided on the exterior surface of the splines on connectors **33** and on the splines of their associated collars **34**. Those recesses are situated such that when the connectors **33** and collars **34** are in their made-up position (as shown in **FIG. 8A**) they form a recess that extends around the circumference of the connection into which a snap-ring (not shown) may be placed. The recesses and snap ring arrangement also will effectively prevent the collars **34** from moving axially along tubular sections **31**.

It will be appreciated, therefore, that the novel clutch mechanisms provide for reliable and effective transmission of torque in both directions through a sectioned conduit, such as tool mandrel **30**. In comparison to conventional set screws and the like, mating prismatic surfaces and splines on the connector and collars provide much greater surface area through which right-handed torque is transmitted. Thus, much greater rotational forces, and forces well in excess of the torque limit of the threaded connection, may be transmitted in a clockwise direction through a sectioned conduit and its connector assemblies without risking damage to threaded connections. The novel clutch mechanisms, therefore, are particularly suited for tools used in drilling in a liner and other applications that subject the tool to high torque. In addition, because the collars cannot rotate in a counterclockwise direction, or if recesses are provided can rotate in a counterclockwise direction only to a limited degree, left-handed torque may be applied to a tool mandrel without risk of significant loosening or of unthreading the connection. Thus, the tool may be designed to utilize reverse rotation, such as may be required for setting or release of a liner or other well component, without risking disassembly of the tool in a well bore.

At the same time, however, it will be appreciated that mandrel **30** may be made up with conventional connections. Moreover, the novel liner hangers may be used with tools having a conventional mandrel, and thus, the novel clutch mechanisms form no part of that aspect of the subject invention. It also will be appreciated that the novel clutch mechanisms may be used to advantage in making up any tubular strings, in mandrels for other tools, or in other sectioned conduits or shafts, or any other threaded connection where threads must be protected from excessive torque.

***Running Assembly***

Running tool **12** includes a collet mechanism that releasably engages hanger mandrel **20** and which primarily bears the weight of liner **17** or other well components connected directly or indirectly to hanger mandrel **20**. Running tool **12** also includes a releasable torque transfer mechanism for transferring torque to hanger mandrel **20** and a releasable dog mechanism that provides a connection between running tool **12** and tool mandrel **30**.

Tubular section **31g** of mandrel **30** provides a base structure on which the various other components of running tool **12** are assembled. As will be appreciated from the discussion follows, most of those other components are slidably supported, directly or indirectly, on tubular section **31g**. During assembly of tool **10** and to a certain extent in their run-in position, however, they are fixed axially in place on tubular section **31g** by the dog mechanism, which can be released to allow release of the collet mechanism engaging hanger mandrel **20**.

More particularly, as seen best in **FIGS. 7**, running tool **12** includes a collet **40** which has an annular base slidably supported on mandrel **30**. A plurality of fingers extends axially downward from the base of collet **40**. The collet fingers have enlarged ends **41** which extend radially outward and, when tool **10** is in its run-in position as shown in **FIG. 7A**, engage corresponding annular recesses **29** in hanger mandrel **20**. A bottom collar **42** is threaded onto the end of tool mandrel **30**, and its upper beveled end provides radial and axial support for the ends **41** of collet **40**. Thus, collet **40** is able to bear the weight of mandrel **20**, liner **17**, and any other well components that may be connected directly or indirectly thereto. Although not shown in the figures, it will be appreciated that bottom collar **42** also may provide a connection, *e.g.*, via a threaded lower end, to a slick joint or other well components.

As may be seen best in **FIGS. 6-7**, collet **40**, or more precisely, its annular base is slidably supported on mandrel **30** within an assembly including a sleeve **43**, an annular collet cap **46**, an annular sleeve cap **44**, and annular thrust cap **45**. Sleeve **43** is generally disposed within hanger mandrel **20** and slidably engages the inner surface thereof. Sleeve cap **44** is threaded to the lower end of sleeve **43** and is slidably carried between hanger mandrel **20** and collet **40**. Thrust cap **45** is threaded to the upper end of sleeve **43** and is slidably carried between swage **21** and tubular section **31g**. Collet cap **46** is threaded to the upper end of collet **40** and is slidably carried between sleeve **43** and tubular section **31g**. The collet **40** and cap **46** subassembly is spring loaded within sleeve **43** between sleeve cap **44** and thrust cap **45**.

As may be appreciated from **FIGS. 6**, thrust cap **45** abuts at its upper end an annular dog housing **47** and abuts hanger mandrel **20** at its lower end. Hanger mandrel **20** and thrust cap **45** rotationally engage each other via mating splines, similar to those described above in reference to the connector assemblies **32** joining tubular sections **31**. In addition, though not shown in any detail, tubular section **31g** is provided with lugs, radially spaced on its outer surface, which rotationally engage corresponding slots in thrust cap **45**. The slots extend laterally and circumferentially away from the lugs to allow, for reasons discussed below, tubular section **31g** to move axially downward and to rotate counterclockwise a quarter-turn. Otherwise, however, when tool **10** is in its run-in position the engagement between those lugs and slots provide rotational engagement in a clockwise direction between tubular section **31g** and thrust cap **45**, thus ultimately allowing clockwise torque to be transmitted from tool mandrel **30** to hanger mandrel **20**. Running tool **12**, therefore, may be used to drill in a liner. That is, a drill bit may be attached to the end liner **17** and the well bore extended by rotating work string **14**.

Although not shown in their entirety or in great detail, it will be appreciated that dog housing **47** and tubular section **31g** of mandrel **30** have cooperating recesses that entrap a plurality of dogs **48** as is common in the art. Those recesses allow dogs **48** to move radially, that is, in and out to a limited degree. It will be appreciated that the inner ends (in this sense, the bottom) of dogs **48** are provided with pawls which engage the recess in tubular section **31g**. The annular surfaces of those pawls and recesses are coordinated such that downward movement of mandrel **30** relative to dog housing **47**, for reasons to be discussed below, urges dogs **48** outward. In the run-in position, as shown in **FIG. 6A**, however, a locking piston **50**, which is slidably supported on tubular section **31g**, overlies dog housing **47** and the tops of the cavities in which dogs **48** are carried. Thus, outward radial movement of dogs **48** is further limited and dogs **48** are held in an inward position in which they engage both dog housing **47** and tubular section **31g**.

Thus, dogs **48** are able to provide a translational engagement between mandrel **30** and running tool **12** when tool **10** is in the run-in position. This engagement is not typically loaded with large amounts of force when the tool is in its run-in position, as the weight of tool **10** and liner **17** is transmitted to tool mandrel **30** primarily through collet ends **41** and bottom collar **41** and torque is transmitted from mandrel **30** through thrust cap **45** and hanger mandrel **20**. The engagement provided by dogs **48**, however, facilitates assembly of tool **10** and will bear any compressive load inadvertently applied between hanger **11** and tool mandrel **30**. Thus, dogs **48** will prevent liner hanger **11** and running tool **12** from moving upward on mandrel **30** such as might otherwise occur if tool **10** gets hung up as it is run into an existing casing.. Release of dogs **48** from that engagement will be described in further detail below in the context of setting hanger **11** and release of running tool **12**.

It will be appreciated that running tool **12** described above provides a reliable, effective mechanism for releasably engaging liner hanger **11**, for securing liner hanger from moving axially on mandrel **30**, and for transmitting torque from mandrel **30** to hanger mandrel **20**. Thus, it is a preferred tool for use with the liner hangers of the subject invention. At the same time, however, other conventional running mechanisms, such as mechanisms utilizing a left-handed threaded nut or dogs only, may be used, particularly if it is not necessary or desirable to provide for the transmission of torque through the running mechanism. The subject invention is in no way limited to a specific running tool.

***Setting Assembly***

Setting tool **13** includes a hydraulic mechanism for generating translational force, relative to the tool mandrel and the work string to which it is connected, and a mechanism for transmitting that force to swage **21** which, upon actuation, expands metal sleeve **22** and sets hanger **11**. It is connected to running tool **12** through their common tool mandrel **30**, with tubular sections **31a-f** of mandrel **30** providing a base structure on which the various other components of setting tool **13** are assembled.

As will be appreciated from **FIGS. 2-5**, the hydraulic mechanism comprises a number of cooperating hydraulic actuators **60** supported on tool mandrel **30**. Those hydraulic actuators are linear hydraulic motors designed to provide linear force to swage **21**. Those skilled in the art will appreciate that actuators **60** are interconnected so as to "stack" the power of each actuator **60** and that their number and size may be varied to create the desired linear force for expanding sleeve **22**.

As is common in such actuators, they comprise a mandrel. Though actuators for other applications may employ different configurations, the mandrel in the novel actuators, as is typical for oil well tools and components, preferably is a generally cylindrical mandrel. A stationary sealing member, such as a piston, seal, or an extension of the mandrel itself, extends continuously around the exterior of the mandrel. A hydraulic barrel or cylinder is slidably supported on the outer surfaces of the mandrel and the stationary sealing member. The cylinder includes a sleeve or other body member with a pair of dynamic sealing members, such as pistons, seals, or extensions of the body member itself, spaced on either side of the stationary sealing member and slidably supporting the cylinder. The stationary sealing member divides the interior of the cylinder into two hydraulic chambers, a top chamber and a bottom chamber. An inlet port provides fluid communication into the bottom hydraulic chamber. An outlet port provides fluid communication into the top hydraulic chamber. Thus, when fluid is introduced into the bottom chamber, relative linear movement is created between the mandrel and the cylinder. In setting tool **13**, this is downward movement of the cylinder relative to mandrel **30**.

For example, what may be viewed as the lowermost hydraulic actuator **60e** is shown in **FIGS. 4**. This lowermost hydraulic actuator **60e** comprises floating annular pistons **61e** and **61f**. Floating pistons **61e** and **61f** are slidably supported on tool mandrel **30**, or more precisely, on tubular sections **31e** and **31f**, respectively. A cylindrical sleeve **62e** is connected, for example, by threaded connections to floating pistons **61e** and **61f** and extends therebetween. An annular stationary piston **63e** is connected to tubular section **31f** of tool mandrel **30**, for example, by a threaded connection. Preferably, set screws, pins, keys, or the like are provided to secure those threaded connections and to reduce the likelihood they will loosen.

In the run-in position shown in **FIG. 4A**, floating piston **61f** is in close proximity to stationary piston **63e**. A bottom hydraulic chamber is defined therebetween, either by spacing the pistons or by providing recesses in one or both of them, and a port is provided through the mandrel to allow fluid communication with the bottom hydraulic chamber. For example, floating piston **61f** and stationary piston **63e** are provided with recesses which define a bottom hydraulic chamber **64e** therebetween, even if pistons **61f** and **63e** abut each other. One or more inlet ports **65e** are provided in tubular section **31f** to provide fluid communication between the interior of tool mandrel **30** and bottom hydraulic chamber **64e**.

Floating piston **61e**, on the other hand, is distant from stationary piston **63e**, and a top hydraulic chamber **66e** is defined therebetween. One or more outlet ports 67e are provided in floating piston **61e** to provide fluid communication between top hydraulic chamber **66e** and the exterior of cylinder sleeve **62e**. Alternately, outlet ports could be provided in cylinder sleeve **62e**, and it will be appreciated that the exterior of cylinder sleeve **62e** is in fluid communication with the exterior of the tool, *i.e.*, the well bore, via clearances between cylinder sleeve **62e** and swage **21**. Thus, fluid flowing through inlet ports **65e** into bottom hydraulic chamber **64e** will urge floating piston **61f** downward, and in turn cause fluid to flow out of top hydraulic chamber **66e** through outlet ports **67e** and allow actuator **60e** to travel downward along mandrel **30**, as may be seen in **FIG. 4B**.

Setting tool **13** includes another actuator **60d** of similar construction located above actuator **60e** just described. Parts of actuator **60d** are shown in **FIGS. 3** and **4.**

Setting tool **13** engages swage **21** of liner hanger **11** via another hydraulic actuator **60c** which is located above hydraulic actuator **60d**. More particularly, as may be seen in **FIGS. 3**, engagement actuator **60c** comprises a pair of floating pistons **61c** and **61d** connected by a sleeve **62c**. Floating pistons **61c** and **61d** are slidably supported, respectively, on tubular sections **31c** and **31d** around stationary piston **63c**. One or more inlet ports **65c** are provided in tubular section **31c** to provide fluid communication between the interior of tool mandrel **30** and bottom hydraulic chamber **64c**. One or more outlet ports **67c** are provided in cylinder sleeve **62c** to provide fluid communication between top hydraulic chamber **66c** and the exterior of actuator **60c**.

It will be noted that the upper portion of sleeve **62c** extends above swage **21** while its lower portion extends through swage **21**, and that upper end of sleeve **62c** is enlarged relative to its lower portion. An annular adjusting collar **68** is connected to the reduced diameter portion of sleeve **62c** via, *e.g.*, threaded connections. An annular stop collar **69** is slidably carried on the reduced diameter portion of sleeve **62c** spaced somewhat below adjusting collar **68** and just above and abutting swage **21**. Adjusting collar **68** and stop collar **69** are tied together by shear pins (not shown) or other shearable members. It will be appreciated that in assembling tool **10**, rotation of adjusting collar **68** and stop collar **69** allows relative movement between setting tool **13** and running tool **12** on the one hand and liner hanger **11** on the other, ultimately allowing collet ends **41** of running tool **12** to be aligned in annular recesses **29** of hanger mandrel **20**.

Setting tool **13** includes what may be viewed as additional drive actuators **60a** and **60b** located above engagement actuator **60c** shown in **FIGS. 3**. As with the other hydraulic actuators **60**, and as may be seen in **FIGS. 2**, the uppermost hydraulic actuator **60a** comprises a pair of floating pistons **61a** and **61b** connected by a sleeve **62a** and slidably supported, respectively, on tubular sections **31a** and **31b** around stationary piston **63a**. One or more inlet ports **65a** are provided in tubular section **31a** to provide fluid communication between the interior of tool mandrel **30** and bottom hydraulic chamber **64a**. One or more outlet ports **67a** are provided in floating piston **61a** to provide fluid communication between top hydraulic chamber **66a** and the exterior of actuator **60a**. (It will be understood that actuator **60b**, as shown in part in **FIGS. 2** and **3**, is constructed in a fashion similar to actuator **60a**.)

It will be appreciated that hydraulic actuators **60** preferably are immobilized in their run-in position. Otherwise, they may be actuated to a greater or lesser degree by differences in hydrostatic pressure between the interior of mandrel **30** and the exterior of tool **10**. Thus, setting tool **13** preferably incorporates shearable members, such as pins, screws, and the like, or other means of releasably fixing actuators **60** to mandrel **30**.

The setting tool **13** preferably incorporates the hydraulic actuators of the subject invention. The novel hydraulic actuators include a balance piston. The balance piston is slidably supported within the top hydraulic chamber of the actuator, preferably on the mandrel. The balance piston includes a passageway extending axially through the balance piston. Fluid communication through the piston and between its upper and lower sides is controlled by a normally shut valve in the passageway. Thus, in the absence of relative movement between the mandrel and the cylinder, the balance piston is able to slide in response to a difference in hydrostatic pressure between the outlet port, which is on one side of the balance piston, and the portion of the top hydraulic chamber that is on the bottom side of the balance piston.

For example, as may be seen in **FIGS. 2**, actuator **60a** includes balance piston **70a**. Balance piston **70a** is slidably supported on tubular section **31a** of mandrel **30** in top hydraulic chamber **66a** between floating piston **61a** and stationary piston **63a**. When tool **10** is in its run-in position, as shown in **FIG. 2A**, balance piston **70a** is located in close proximity to floating piston **61a**. A hydraulic chamber is defined therebetween, either by spacing the pistons or by providing recesses in one or both of them, and a port is provided through the mandrel to allow fluid communication with the hydraulic chamber. For example, floating piston **61a** is provided with a recess which defines a hydraulic chamber **71a** therebetween, even if pistons **61a** and **70a** abut each other.

Balance piston **70a** has a passageway **72a** extending axially through its body portion, *i.e.*, from its upper side to its lower side. Passageway **72a** is thus capable of providing fluid communication through balance piston **70a**, that is, between hydraulic chamber **71a** and the rest of top hydraulic chamber **66a**. Fluid communication through passageway **72a**, however, is controlled by a normally shut valve, such as rupturable diaphragm **73a**. When diaphragm **73a** is in its closed, or unruptured state, fluid is unable to flow between hydraulic chamber **71a** and the rest of top hydraulic chamber **66a**.

Actuator **60b** also includes a balance piston **70b** identical to balance piston **70a** described above. Thus, when tool **10** is in its run-in position shown in **FIG. 2A**, balance pistons **70a** and **70b** are able to equalize pressure between the top hydraulic chambers **66a** and **66b** and the exterior of actuators **60a** and **60b** such as might develop, for example, when tool **10** is being run into a well. Fluid is able to enter outlet ports **67a** and **67b** and, to the extent that such exterior hydrostatic pressure exceeds the hydrostatic pressure in top hydraulic chambers **66a** and **66b**, balance pistons **70a** and **70b** will be urged downward until the pressures are balanced. Such balancing of internal and external pressures is important because it avoids deformation of cylinder sleeves **62a** and **62b** that could interfere with travel of sleeves **62a** and **62b** over stationary pistons **63a** and **63b**.

Moreover, by not allowing ingress of significant quantities of fluid from a well bore as tool **10** is being run into a well, balance pistons **70a** and **70b** further enhance the reliability of actuators **60a** and **60b**. That is, balance pistons **70a** and **70b** greatly reduce the amount of debris that can enter top hydraulic chambers **66a** and **66b**, and since they are located in close proximity to outlet ports **67a** and **67b**, the substantial majority of the travel path is maintained free and clear of debris. Hydraulic chambers **66a** and **66b** preferably are filled with clean hydraulic fluid during assembly of tool **10**, thus further assuring that when actuated, floating pistons **61a** and **61b** and sleeves **62a** and **62b** will slide cleanly and smoothly over, respectively, tubular sections **31a** and **31b** and stationary pistons **63a** and **63b**.

It will be appreciated that for purposes of balancing the hydrostatic pressure between the top hydraulic chamber and a well bore the exact location of the balance piston in the top hydraulic chamber of the novel actuators is not critical. It may be spaced relatively close to a stationary piston and still provide such balancing. In practice, the balance piston will not have to travel a great distance to balance pressures and, therefore, it may be situated initially at almost any location in the top hydraulic chamber between the external opening of the outlet port and the stationary piston.

Preferably, however, the balance piston in the novel actuators is mounted as close to the external opening of the outlet port as practical so as to minimize exposure of the inside of the actuator to debris from a well bore. It may be mounted within a passageway in what might be termed the "port," such as ports **67a** shown in the illustrated embodiment **60a**, or within what might otherwise be termed the "chamber,' such as top hydraulic chamber **66a** shown in the illustrated embodiment **60a**. As understood in the subject invention, therefore, when referencing the location of a balance piston, the top hydraulic chamber may be understood as including all fluid cavities, chambers, passageways and the like between the port exit and the stationary piston. If mounted in a relatively narrow passageway, such as the outlet ports **67a**, however, the balance piston will have to travel greater distances to balance hydrostatic pressures. Thus, in the illustrated embodiment **60a** the balance piston **70a** is mounted on tubular sections **31a** in the relatively larger top hydraulic chamber **66a**.

It also will be appreciated that, to provide the most effective protection from debris, the normally shut valves in the balance position should be selected such that they preferably are not opened to any significant degree by the pressure differentials they are expected to encounter prior to actuation of the actuator. At the same time, as will be appreciated from the discussion that follows, they must open, that is, provide release of increasing hydrostatic pressure in the top hydraulic chamber when the actuator is actuated. Most preferably, the normally shut valves remain open once initially opened. Thus, rupturable diaphragms are preferably employed because they provide reliable, predictable release of pressure, yet are simple in construction and can be installed easily. Other normally shut valve devices, such as check valves, pressure relief valves, and plugs with shearable threads, however, may be used in the balance piston on the novel actuators.

As will be appreciated by workers in the art, the actuator includes stationary and dynamic seals as are common in the art to seal the clearances between the components of the actuator and to provide efficient operation of the actuator as described herein. In particular, the clearances separating the balance piston from the mandrel and from the sleeve, that is, the top hydraulic chamber, preferably are provided with dynamic seals to prevent unintended leakage of fluid around the balance piston. The seals may be mounted on the balance piston or on the chamber as desired. For example, balance pistons **70a** and **70b** may be provided with annular dynamic seals (not shown), such as elastomeric O-rings mounted in grooves, on their inner surface abutting tubular sections **31a** and **31b** and on their outer surfaces abutting sleeves **62a** and **62b**, respectively. Alternatively, one or both of the seals may be mounted on the top hydraulic chambers **66a** and **66b**, for example, in grooves on tubular sections **31a** and **31b** or sleeves **62a** and **62b.**

As noted above, prior to actuation, the balance pistons essentially seal the top hydraulic chambers and prevent the incursion of debris. Under certain conditions, however, such as increasing downhole temperatures, pressure within the top hydraulic chambers can increase beyond the hydrostatic pressure in the well bore. The balance pistons will be urged upward until pressure in the top hydraulic chambers is equal to the hydraulic pressure in the well bore. In the event that a balance piston "bottoms" out against the outlet port, however, pressure within the top hydraulic chamber could continue to build, possibly to the point where a diaphragm would be ruptured, thereby allowing debris laden fluid from the well bore to enter the chamber. Thus, the novel actuators preferably incorporate a pressure release device allowing release of potentially problematic pressure from the top hydraulic chamber as might otherwise occur if the balance pistons bottom out.

For example, instead of using rupturable diaphragms **73a** and **73b**, check valves or pressure relief valves may be mounted in passageways **72a** and **72b**. Such valves, if used, should also allow a desired level of fluid flow through passageways **72a** and **72b** during actuation. Alternately, an elastomeric burp seal (not shown) may be mounted in one or both of the clearances separating the balance pistons **70a** and **70b** from, respectively, tubular sections **31a** and **31b** and sleeves **62a** and **62b**. Such burp seals would then allow controlled release of fluid from top hydraulic chambers **66a** and **66b** to, respectively, hydraulic chambers **71a** and **71b** if balance pistons **70a** and **70b** were to bottom out against, respectively, floating pistons **61a** and **61b**. Such burp valves would, of course, be designed with a release pressure sufficiently below the pressure required to open the rupturable diaphragm or other normally shut valve.

Preferably, however, the pressure relief device is provided in the cylindrical mandrel. For example, a check or pressure release valve (not shown) may be mounted in tubular sections **31a** and **31b** so as to allow controlled release of fluid from top hydraulic chambers **66a** and **66b** to the interior of mandrel **30**. Such an arrangement has an advantage over a burp seal as described above in that it would be necessary to overcome flow through a burp seal in order to build up sufficient pressure to rupture a diaphragm or otherwise to open a normally shut valve device. If a pressure relief device is provided in the cylindrical mandrel, pressure in the top hydraulic chamber will be equal to pressure within the interior of the mandrel, and there will be no flow through the pressure release device that must be overcome.

The setting assemblies of the subject invention also preferably include some means for indicating whether the swage has been fully stroked into position under the expandable metal sleeve. Thus, as shown in **FIG. 5**, setting tool **13** includes a slidable, indicator ring **75** supported on tubular section **31f** just below actuator **60e** described above. When tool **10** is in its set position, indicator ring **75** is fixed to tubular section **31f** via a shear member, such as a screw or pin (not shown). It is positioned on section **31f** relative to floating piston **61f**, however, such that when floating piston **61f** has reached the full extent of its travel, it will impact indicator ring **75** and shear the member fixing it to section **31f**. Thus, indicator ring **75** will be able to slide freely on mandrel **30** and, when the tool is retrieved from the well, it may be readily confirmed that setting tool **13** fully stroked and set metal sleeve **22**.

It will be appreciated that setting tool **13** described above provides a reliable, effective mechanism for actuating swage **21**, and it incorporates novel hydraulic actuators providing significant advantages over the prior art. Thus, it is a preferred tool for use with the anchor assemblies of the subject invention. At the same time, however, there are a variety of hydraulic and other types of mechanisms which are commonly used in downhole tools to generate linear force and motion, such as hydraulic jack mechanisms and mechanisms actuated by explosive charges or by releasing weight on, pushing, pulling, or rotating the work string. In general, such mechanism may be adapted for use with the novel anchor assemblies, and it is not necessary to use any particular setting tool or mechanism to set the novel anchor assemblies.

Moreover, it will be appreciated that the novel setting assemblies, because they include hydraulic actuators having a balance piston, are able to balance hydraulic pressures that otherwise might damage the actuator and are able to keep the actuator clear of debris that could interfere with its operation. Such improvements are desirable not only in setting the anchor assemblies of the subject invention, but also in the operation of other downhole tools and components where hydraulic actuators or other means of generating linear force are required. Accordingly, the subject invention in this aspect is not limited to use of the novel setting assemblies to actuate a particular anchor assembly or any other downhole tool or component. They may be used to advantage in the setting assemblies of many other downhole tools, such as expandables, expandable liner hangers, liner hangers, whipstocks, packers, bridge plugs, cement plugs, frac plugs, slotted pipe, and polished bore receptacles (PBRs).

***Operation of Anchor and Tool Assembly***

The description of running tool **12** and setting tool **13** thus far has focused primarily on the configuration of those tools in their run-in position. When in its run-in position, tool **10** tool may be lowered into an existing casing, with our without rotation. If a liner is being installed, however, a drill bit preferably is attached to the end of the liner, as noted above, so that the liner may be drilled in. It also will be appreciated that tool mandrel **30** provides a conduit for circulation of fluids as may be needed for drilling or other operations in the well. Once tool **10** has been positioned at the desired depth, the liner hanger **11** will be set and released, and running tool **12** and setting tool **13** will be retrieved from the well, as now will be described in greater detail.

In general, liner hanger **11** is set by increasing the fluid pressure within mandrel **30**. Increased fluid pressure actuates setting tool **13**, which urges swage **21** downward and under expandable sleeve **22**. At the same time, increasing fluid pressure in mandrel **30** causes a partial release of running tool **12** from mandrel **30**. Once tool **10** is in this set position, running tool **12** may be released from liner hanger **11** by releasing weight on mandrel **30** through work string **14**. Alternately, in the event that release does not occur, running tool **12** may be released from liner hanger **11** by rotating mandrel **30** a quarter-turn counterclockwise prior to releasing weight.

More particularly, once tool **10** has been run in to the desired depth, liner **17** may be cemented in place. The cementing operation will allow fluid pressure to be built up within work string **14** and mandrel **30**. If a cementing operation will not first be performed, for whatever reason, it will be appreciated that other means will be provided, such as a ball seat, for allowing pressure to be built up.

As fluid pressure in mandrel **30** is increased to set tool **10**, fluid enters bottom hydraulic chambers **64** of actuators **60** through inlet ports **65**. The increasing fluid pressure in bottom hydraulic chambers **64** urges floating pistons **61b** through **61f** downward. Because floating pistons **61** and sleeves **62** are all interconnected, that force is transmitted throughout all actuators **60**, and whatever shear members have been employed to immobilize actuators **60** are sheared, allowing actuators **60** to begin moving downward. That downward movement in turn causes an increase in pressure in top hydraulic chambers **66** which eventually ruptures diaphragms **73**, allowing fluid to flow through balance pistons **70**. Continuing flow of fluid into bottom hydraulic chambers **64** causes further downward travel of actuators **60**. Since fluid communication has been established in passageways **72**, balance pistons **70** are urged downward along mandrel **30** with floating pistons **61**, as may be seen by comparing **FIGS. 2A** and **2B**.

As actuators **60** continue traveling downward along mandrel **30**, as best seen by comparing **FIGS. 3A** and **3B**, the shear pins connecting adjusting collar **68** and stop collar **69** are sheared. The lower end of adjusting collar **68** then moves into engagement with the upper end of stop collar **69**, which in turn abuts swage **21**. Thus, downward force generated by actuators **60** is brought to bear on swage **21**, causing it to move downward and, ultimately, to expand metal sleeve **22** radially outward into contact with an existing casing. It will be appreciated that ideally there is little or no movement of liner hanger **11** relative to the existing casing as it is being set. Thus, a certain amount of weight may be released on mandrel **30** to ensure that it is not pushed up by the resistance encountered in expanding sleeve **22**.

Finally, as noted above, the increasing fluid pressure within mandrel **30** not only causes setting of liner hanger **11**, but also causes a partial release of running tool **12** from mandrel **30**. More specifically, as understood best by comparing **FIGS. 6A** and **6B**, increasing fluid pressure in mandrel **30** causes fluid to pass through one or more ports **51** in tubular section **31g** into a small hydraulic chamber **52** defined between locking piston **50** and annular seals **53** provided between piston **50** and section **31g**. As fluid flows into hydraulic chamber **52**, locking piston **50** is urged upward along tubular section **31g** and away from dog housing **47**.

That movement of locking piston **50** uncovers recesses in dog housing **47**. As discussed above, dogs **48** are able to move radially (to a limited degree) within those recesses. Once uncovered, however, dogs **48** will be urged outward and out of engagement with tubular section **31g** if mandrel **30** is moved downward. Thus, running tool **12** is partially released from mandrel **30** in the sense that mandrel **30**, though restricted from relative upward movement, is now able to move downward relative to running tool **12**. Other mechanisms for setting and releasing dogs, such as those including one or a combination of mechanical or hydraulic mechanisms, are known, however, and may be used in running tool **12**.

Once liner hanger **11** has been set and any other desired operations are completed, running and setting tools **12** and **13** are retrieved from the well by first moving tool **10** to a "release" position. **FIGS. 6C** and **7C** show the lower sections of tool **10** in their release positions. As will be appreciated therefrom, in general, running tool **12** is released from hanger **11** by releasing weight onto mandrel **30** via work string **14** while fluid pressure within mandrel **30** is reduced. Thus, as weight is released onto mandrel **30** it begins to travel downward and setting tool **13**, which is held stationary by its engagement through stop collar **69** with the upper end of swage **21**, is able to ride up mandrel **30**.

As best seen by comparing **FIG. 6B** and **FIG. 6C**, at the same time dogs **48** now are able to move radially out of engagement with tubular section **31g** as discussed above, and as weight is released onto tool **10** mandrel **30** is able to move downward relative to running tool **12**. An expanded C-ring **54** is carried on the outer surface of tubular section **31g** in a groove in dog housing **47**. As mandrel **30** travels downward, expanded C-ring **54** encounters and is able to relax somewhat and engage another annular groove in tubular section **31g**, thus laterally re-engaging running tool **12** with tool mandrel **30**. The downward travel of mandrel **30** preferably is limited to facilitate this re-engagement. Thus, an expanded C-ring and cover ring assembly **55** is mounted on tubular section **31g** such that it will engage the upper end of dog housing **47**, stopping mandrel **30** and allowing expanded C-ring **54** to engage the mating groove in tubular section **31g**.

Finally, as best seen by comparing **FIGS. 7B** and **7C,** downward travel of mandrel **30** will cause bottom collar **42** to travel downwards as well, thereby removing radial support for collet ends **41**. Running and setting tools **12** and **13** then may be retrieved by raising mandrel **30** via work string **14**. As noted, running tool **12** has been re-engaged with tool mandrel **30**. When mandrel **30** is raised, therefore, collet **40** is raised as well. Collet ends **41** are tapered such that they will be urged radially inward as they come into contact with the upper edges of annular recesses **29** in hanger mandrel **20**, thereby releasing running tool **12** from hanger **11**. Setting tool **13** is carried along on mandrel **30**.

In the event running tool **12** is not released from mandrel **30** as tool **10** is set, it will be appreciated that it may be released by rotating mandrel **30** a quarter-turn counterclockwise and then releasing weight on mandrel **30**. That is, left-handed "J" slots (not shown) are provided in tubular section **31g**. Such "J" slots are well known in the art and provide an alternate method of releasing running tool **12** from hanger mandrel **20**. More specifically, dogs **48** may enter lateral portions of the "J" slots by rotating mandrel **30** a quarter-turn counterclockwise. Upon reaching axial portions of the slots, weight may be released onto mandrel **30** to move it downward relative to running tool **12**. That downward movement will re-engage running tool **12** and remove radial support for collet ends **41** as described above. Preferably, shear wires or other shear members are provided to provide a certain amount of resistance to such counterclockwise rotation in order to minimize the risk of inadvertent release.

While this invention has been disclosed and discussed primarily in terms of specific embodiments thereof, it is not intended to be limited thereto. Other modifications and embodiments will be apparent to the worker in the art.

**WHAT IS CLAIMED IS:**

1. An anchor assembly for installation within a tubular conduit, said anchor assembly comprising:
    a. a nondeformable cylindrical mandrel;
    b. an expandable metal sleeve carried on the outer surface of said mandrel; and
    c. a cylindrical swage supported for axial movement across said mandrel outer surface from a first position axially proximate to said sleeve to a second position under said sleeve; said movement of said swage expanding said sleeve radially outward.
2. The anchor assembly of claim 1, wherein said swage has an inner diameter substantially equal to the outer diameter of said mandrel and an outer diameter greater than the inner diameter of said expandable metal sleeve.
3. The anchor assembly of claim 1 or 2, wherein said assembly comprises a ratchet mechanism engaging said mandrel and said swage, said ratchet mechanism resisting axial movement of said swage away from said second position.
4. The anchor assembly of claim 3, wherein said ratchet assembly comprises annular detents on the inner surface of said swage and on the outer surface of said mandrel and a split ratchet ring mounted therebetween.
5. The anchor assembly of any one of claims 1 to 4, wherein said sleeve comprises an elastomeric sealing ring mounted on the outer surface thereof.
6. The anchor assembly any one of claims 1 to 5, wherein said sleeve comprises a slip mounted on the outer surface thereof.
7. The anchor assembly of claim 6, wherein said slip comprises metal particles soldered to said sleeve outer surface.
8. The anchor assembly of claim 6, wherein said slip is machined into the outer surface of said sleeve.
9. The anchor assembly any one of claims 1 to 8, wherein said mandrel comprises an annular boss on the outer surface thereof, said boss engaging the inner surface of said swage when said swage is in said second position.
10. The anchor assembly any one of claims 1 to 9, wherein said swage comprises an annular boss on the inner surface thereof, said boss engaging the outer surface of said mandrel when said swage is in said second position.

11. The anchor assembly any one of claims 1 to 9, wherein said swage comprises an annular boss on the outer surface thereof, said boss engaging the inner surface of said sleeve when said swage is in said second position.

12. The anchor assembly any one of claims 1 to 11, wherein said sleeve comprises an annular boss on the inner surface thereof, said boss engaging the outer surface of said swage when said swage is in said second position.

13. The anchor assembly any one of claims 1 to 12, wherein said sleeve is composed of ductile ferrous and non-ferrous metal alloys.

14. The anchor assembly of claim 14, wherein said sleeve is composed of metal alloys selected from the group consisting of ductile aluminum, brass, bronze, stainless steel, and carbon steel,

15. The anchor assembly any one of claims 1 to 14, wherein said sleeve is composed of metal alloys having an elongation factor of at least 10%.

16. The anchor assembly of claim 15, wherein said sleeve is composed of metal alloys having an elongation factor of from about 10 to about 20%.

17. The anchor assembly any one of claims 1 to 16, wherein said mandrel is composed of high yield ferrous and non-ferrous alloys.

18. The anchor assembly of claim 17, wherein said mandrel is composed of high yield, corrosion resistant ferrous and non-ferrous alloys.

19. The anchor assembly any one of claims 1 to 16, wherein said mandrel is composed of metal alloys selected from the group consisting of high yield steel and superalloys.

20. A method for installing an anchor in a tubular conduit, said method comprising:

   a. positioning an anchor assembly inside said conduit, said anchor assembly comprising;

      i. a nondeformable cylindrical mandrel;

      ii. an expandable metal sleeve carried on the outer surface of said mandrel; and

      iii. a cylindrical swage supported on said outer surface of said mandrel for axial movement thereon;

   b. moving said swage axially across said mandrel outer surface from a position proximate to said sleeve to a position under said sleeve; whereby said sleeve is expanded radially outward into contact with the inner wall of said conduit.

21. The method of claim 20, wherein said swage is moved by a hydraulic assembly.

22. A conduit assembly comprising:

a. a tubular conduit;

b. a hollow cylindrical mandrel disposed concentrically within said conduit;

c. a cylindrical swage engaging the outer surface of said mandrel; and

d. an expanded metal sleeve engaging the outer surface of said swage and the inner wall of said conduit.

23. The conduit assembly of claim 22, wherein said conduit assembly comprises a first tubular conduit and a second tubular conduit, said mandrel, swage, and sleeve being disposed within said first conduit and said second conduit being connected to one end of said mandrel.

24. The conduit assembly of claim 23, wherein said second tubular conduit has an outer diameter less than the inner diameter of said first conduit.

25. An assembly comprising an anchor and a tool for installing said anchor in a tubular conduit, said anchor and tool assembly comprising:

a. an anchor assembly, said anchor assembly comprising;

i. a nondeformable cylindrical mandrel;

ii. an expandable metal sleeve carried on the outer surface of said mandrel; and

iii. a cylindrical swage supported for axial movement across said mandrel outer surface from a first position axially proximate to said sleeve to a second position under said sleeve; said movement of said swage expanding said sleeve radially outward;

b. a running assembly releasably engaging said anchor assembly; and

c. a setting assembly connected to said running assembly, said setting assembly engaging said swage and being adapted to move said swage from said first position to said second position.

26. The anchor and tool assembly of claim 25, wherein said setting assembly comprises a hydraulic assembly which actuates said movement of said swage.

27. The anchor and tool assembly of claim 25 or 26, wherein said setting assembly comprises a hydraulic actuator comprising:

a. a cylindrical mandrel;

b. an annular stationary sealing member connected to said mandrel;

c. a hydraulic cylinder slidably supported on said mandrel and said stationary sealing member, said cylinder being releasably fixed in position on said mandrel;

d. said stationary sealing member dividing the interior of said cylinder into a bottom hydraulic chamber and a top hydraulic chamber;

e. an inlet port providing fluid communication into said bottom hydraulic chamber;

f. an outlet port providing fluid communication into said top hydraulic chamber;

g. an annular balance piston slidably supported within said top hydraulic chamber between said outlet port and said stationary sealing member, said balance piston comprising a passageway extending axially through said piston wherein fluid communication between the sides of said balance piston through said passageway is controlled by a normally shut valve;

h. whereby, when said cylinder is fixed in position on said mandrel, said balance piston slides in response to a differential in hydrostatic pressure between said outlet port and said top hydraulic chamber.

28. The anchor and tool assembly of claim 27, wherein said balance piston is slidably supported on said mandrel.

29. The anchor and tool assembly of claim 27 or 28, wherein said hydraulic cylinder comprises first and second annular floating pistons slidably supported on said mandrel and a cylindrical sleeve extending between said floating pistons.

30. The anchor and tool assembly any one of claims 27 to 29, wherein the introduction of fluid into said bottom chamber causes an increase in hydrostatic pressure in said top chamber sufficient to open said normally shut valve in said balance piston.

31. The anchor and tool assembly any one of claims 27 to 30, wherein said normally shut valve in said balance piston is a rupturable diaphragm.

32. The anchor and tool assembly any one of claims 25 to 31, wherein said running assembly or said setting assembly comprises a mandrel supporting said assembly, wherein said assembly mandrel comprises a pair of tubular sections joined by a clutch mechanism, and wherein said clutch mechanism comprises:

a. tubular sections having threads on the end to be joined and prismatic outer surfaces adjacent to said threaded ends;

b. a threaded connector joining said threaded ends of said tubular sections, the ends of said connector having axial splines;

c. a pair of clutch collars slidably supported on said outer surface of said tubular sections at their joined ends, said collars having axial splines engaging said connector splines and prismatic inner surfaces engaging said prismatic surfaces on said tubular sections.

33. The anchor and tool assembly of claim 32, wherein said clutch mechanism comprises recesses adjacent to said mating prismatic surfaces, said recesses allowing rotation of said clutch collars on said tubular sections such that said prismatic surfaces may be engaged and disengaged from each other.

34. The anchor and tool assembly of claim 32 or 33, wherein said clutch collars have recesses adjacent to said prismatic surfaces.

35. A hydraulic actuator for a setting assembly of a tool for use in oil and gas wells, said hydraulic actuator comprising:

a. a cylindrical mandrel;

b. an annular stationary sealing member connected to said mandrel;

c. a hydraulic cylinder slidably supported on said mandrel and said stationary sealing member, said cylinder being releasably fixed in position on said mandrel;

d. said stationary sealing member dividing the interior of said cylinder into a bottom hydraulic chamber and a top hydraulic chamber;

e. an inlet port providing fluid communication into said bottom hydraulic chamber;

f. an outlet port providing fluid communication into said top hydraulic chamber;

g. an annular balance piston slidably supported within said top hydraulic chamber between said outlet port and said stationary sealing member, said balance piston comprising a passageway extending axially through said piston wherein fluid communication between the sides of said balance piston through said passageway is controlled by a normally shut valve;

h. whereby, when said cylinder is fixed in position on said mandrel, said balance piston slides in response to a differential in hydrostatic pressure between said outlet port and said top hydraulic chamber.

36. The actuator of claim 35, wherein said balance piston is slidably supported on said mandrel.

37. The actuator of claim 35 or 36, wherein said hydraulic cylinder comprises first and second annular floating pistons slidably supported on said mandrel and a cylindrical sleeve extending between said floating pistons.

38. The actuator any one of claims 35 to 37, wherein the introduction of fluid into said bottom chamber causes an increase in hydrostatic pressure in said top chamber sufficient to open said normally shut valve in said balance piston.

39. The actuator any one of claims 35 to 38, wherein said normally shut valve in said balance piston is a rupturable diaphragm.

40. The actuator any one of claims 35 to 39, wherein said actuator comprises a pressure release device allowing release of pressure from said top hydraulic cylinder.

41. The actuator of claim 40, wherein said pressure release device is a burp seal mounted in the clearance between said balance piston and said top hydraulic cylinder.

42. The actuator of claim 40, wherein said pressure release device is a check valve or pressure release valve mounted in said mandrel.

43. A setting assembly for a tool for use in oil and gas wells, said setting assembly comprising the actuator any one of claims 35 to 42.

44. A tool for use in oil and gas wells, said tool comprising the actuator any one of claims 35 to 42.

45. An assembly comprising an anchor and a tool for installing said anchor in a tubular conduit, said anchor and tool assembly comprising:

a. an anchor assembly;

b. a running assembly; and

c. a setting assembly comprising the actuator of any one of claims 35 to 42.

46. The anchor and tool assembly of claim 45, wherein said anchor assembly comprises:

a. a nondeformable cylindrical mandrel;

b. an expandable metal sleeve carried on the outer surface of said mandrel; and

c. a cylindrical swage supported for axial movement across said mandrel outer surface from a first position axially proximate to said sleeve to a second position under said sleeve; said movement of said swage expanding said sleeve radially outward.

47. The anchor and tool assembly of claim 46, wherein said sleeve is composed of ductile ferrous and non-ferrous metal alloys.

48. The anchor and tool assembly of claim 46 or 47, wherein said sleeve is composed of metal alloys having an elongation factor of at least 10%.

49. The anchor and tool assembly any one of claims 46 to 48, wherein said anchor assembly mandrel is composed of high yield ferrous and non-ferrous alloys.

50. The anchor and tool assembly of any one of claims 45 to 49, wherein said running assembly or said setting assembly comprises a mandrel supporting said assembly, wherein said assembly mandrel comprises a pair of tubular sections joined by a clutch mechanism, and wherein said clutch mechanism comprises:

a. tubular sections having threads on the end to be joined and prismatic outer surfaces adjacent to said threaded ends;

b. a threaded connector joining said threaded ends of said tubular sections, the ends of said connector having axial splines;

c. a pair of clutch collars slidably supported on said outer surface of said tubular sections at their joined ends, said collars having axial splines engaging said connector splines and prismatic inner surfaces engaging said prismatic surfaces on said tubular sections.

51. The anchor and tool assembly of claim 50, wherein said clutch mechanism comprises recesses adjacent to said mating prismatic surfaces, said recesses allowing rotation of said clutch collars on said tubular sections such that said prismatic surfaces may be engaged and disengaged from each other.

52. The anchor and tool assembly of claim 50 or 51, wherein said clutch collars have recesses adjacent to said prismatic surfaces.

53. An assembly comprising a pair of tubular sections joined by a clutch mechanism, wherein said clutch mechanism comprises:

a. tubular sections having threads on the end to be joined and prismatic outer surfaces adjacent to said threaded ends;

b. a threaded connector joining said threaded ends of said tubular sections, the ends of said connector having axial splines;

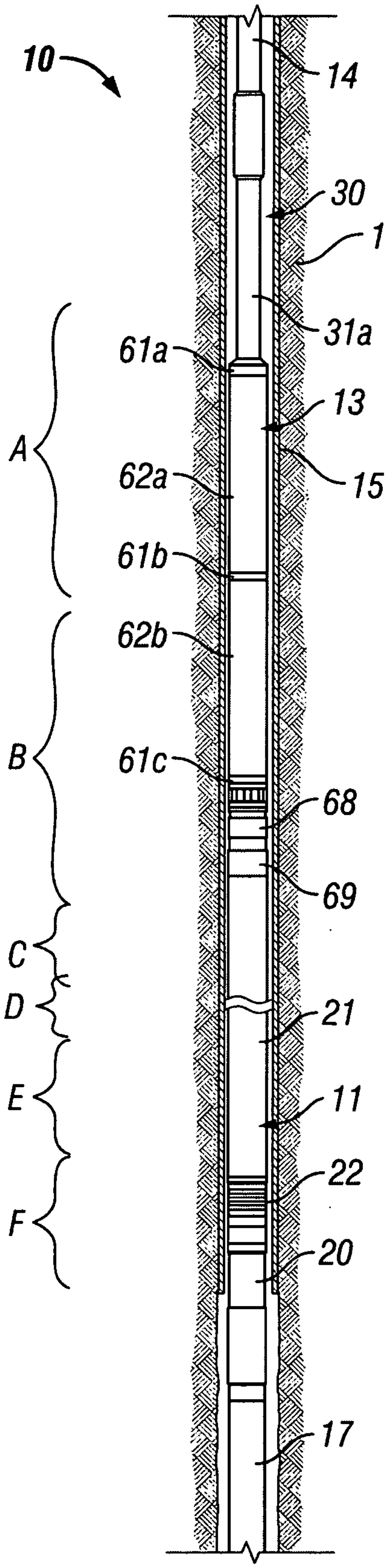
c. a pair of clutch collars slidably supported on said outer surface of said tubular sections at their joined ends, said collars having axial splines engaging said connector splines and prismatic inner surfaces engaging said prismatic surfaces on said tubular sections.

54. The tubular assembly of claim 53, wherein said clutch mechanism comprises recesses adjacent to said mating prismatic surfaces, said recesses allowing rotation of said clutch collars on said tubular sections such that said prismatic surfaces may be engaged and disengaged from each other.

55. The tubular assembly of claim 53 or 54, wherein said clutch collars have recesses adjacent to said prismatic surfaces.

56. A downhole tool for use in drilling operations having a mandrel, wherein said mandrel comprises the tubular assembly any one of claims 53 to 55.

57. A setting assembly for use in drilling operations having a hydraulic actuator comprising a mandrel, wherein said mandrel comprises the tubular assembly any one of claims 53 to 55.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17

FIG. 1A

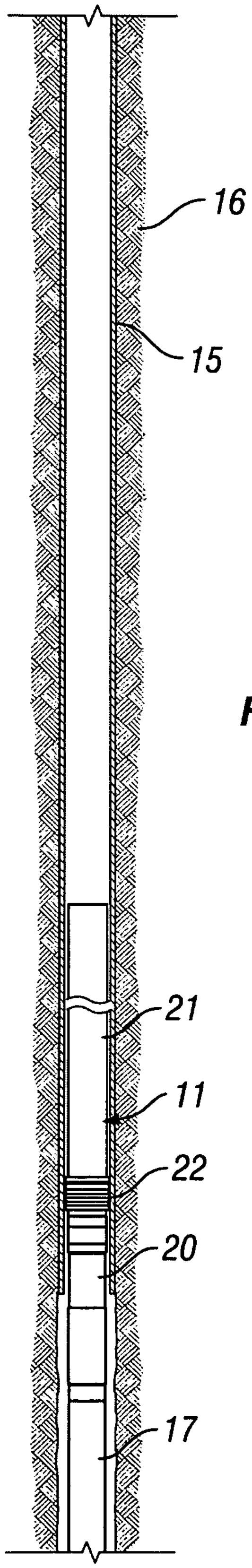
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FIG. 1B

2/11

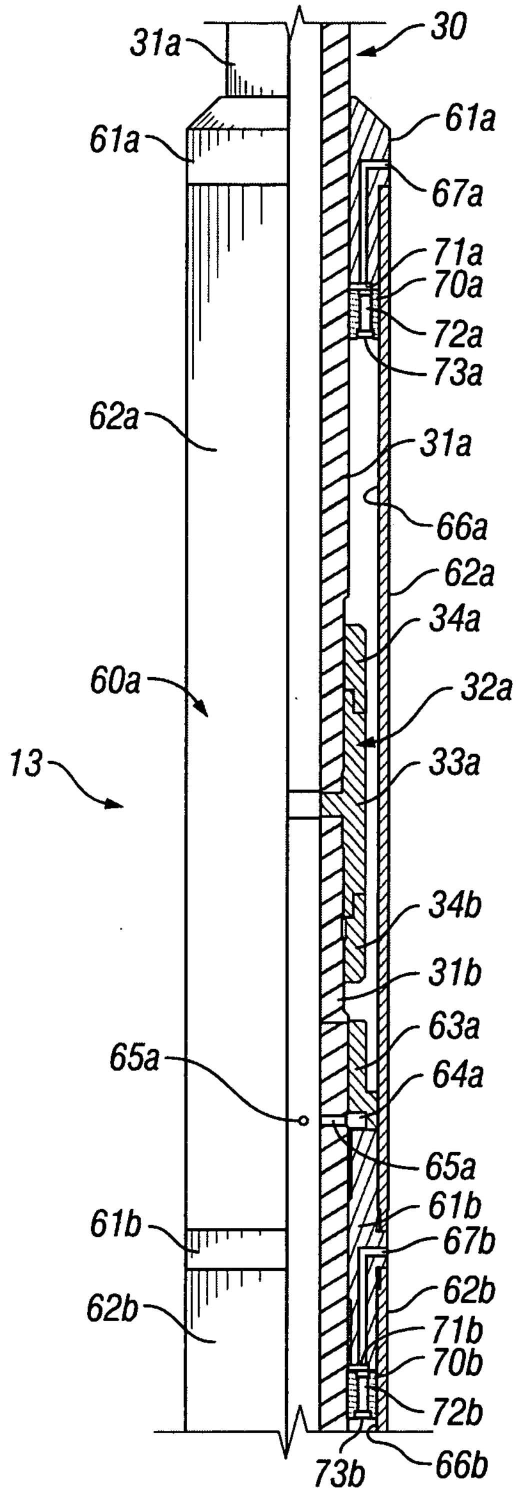



FIG. 2A

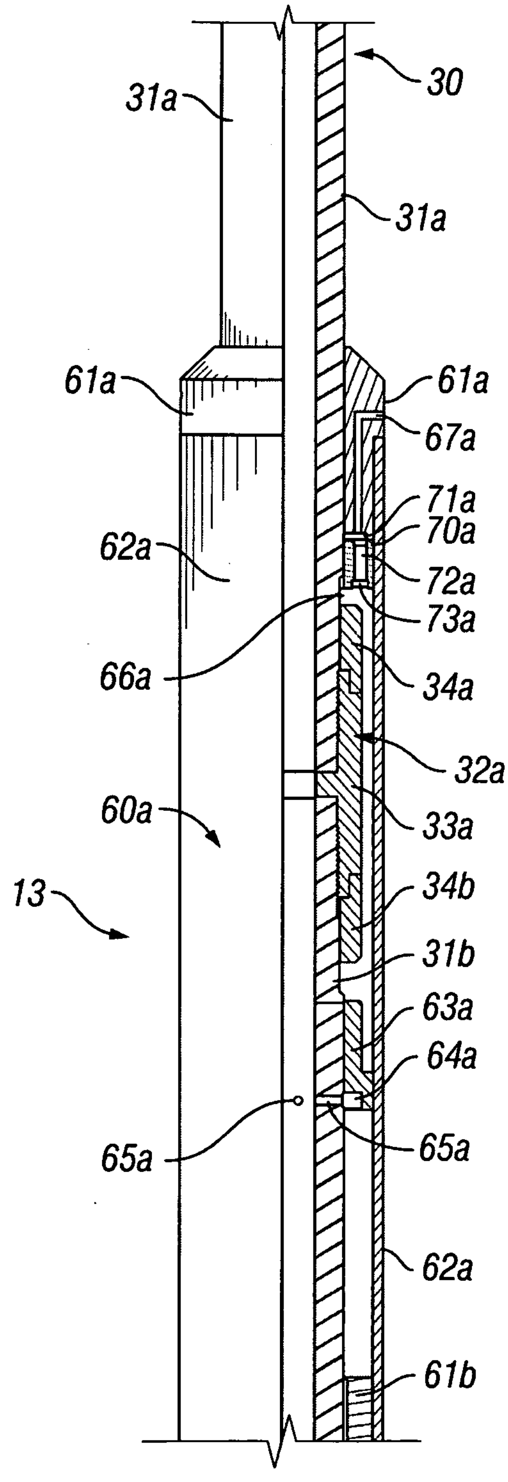



FIG. 2B

3/11

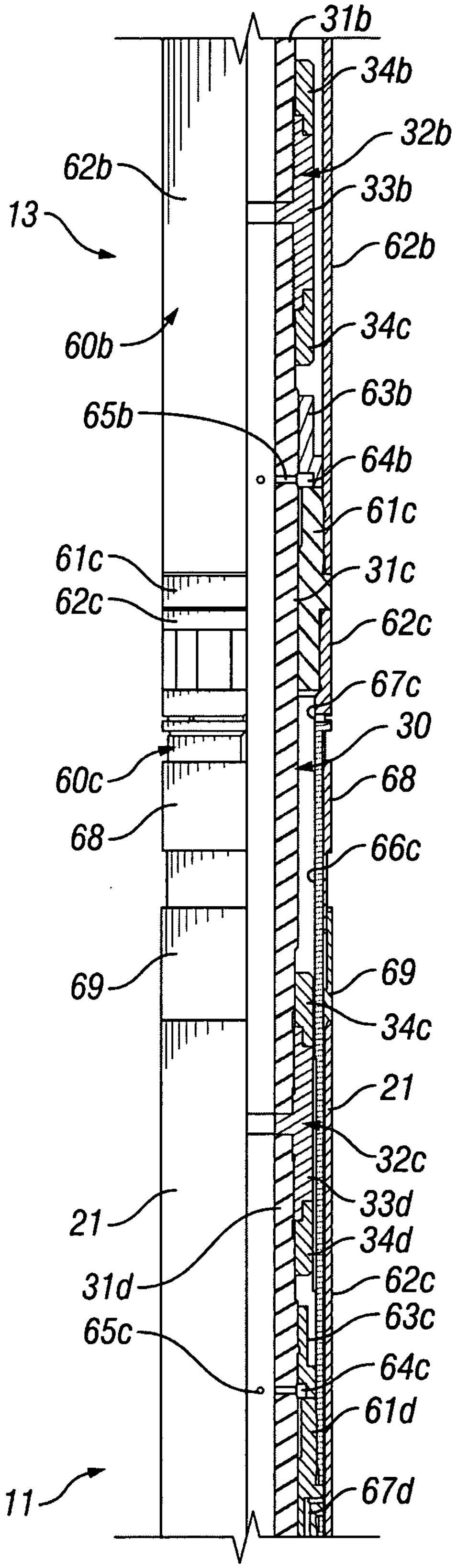



FIG. 3A

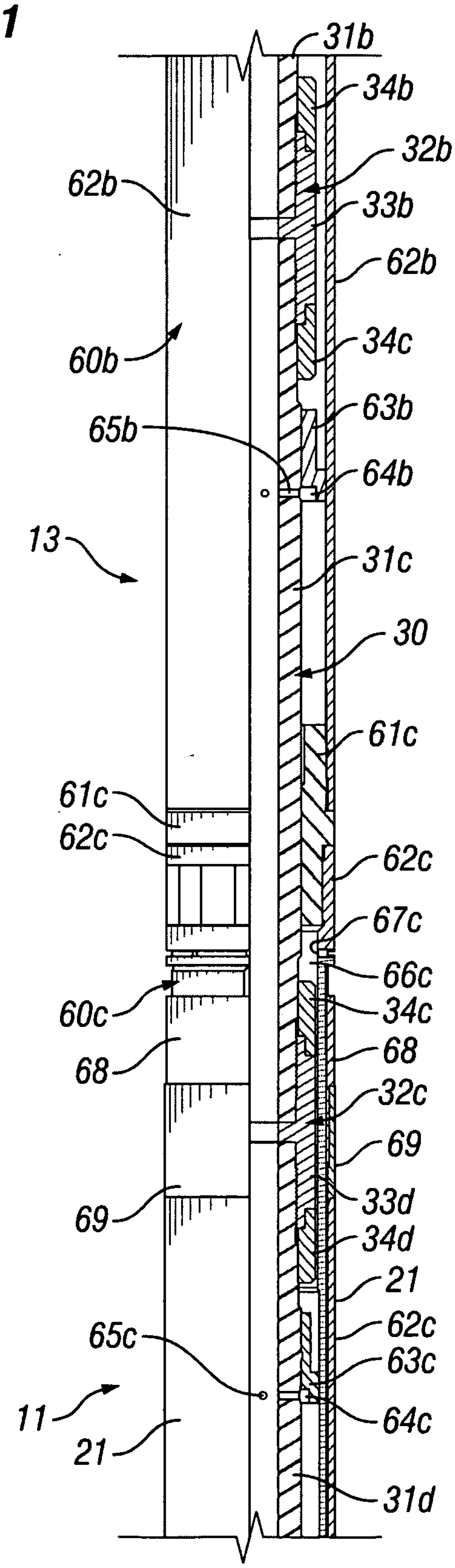
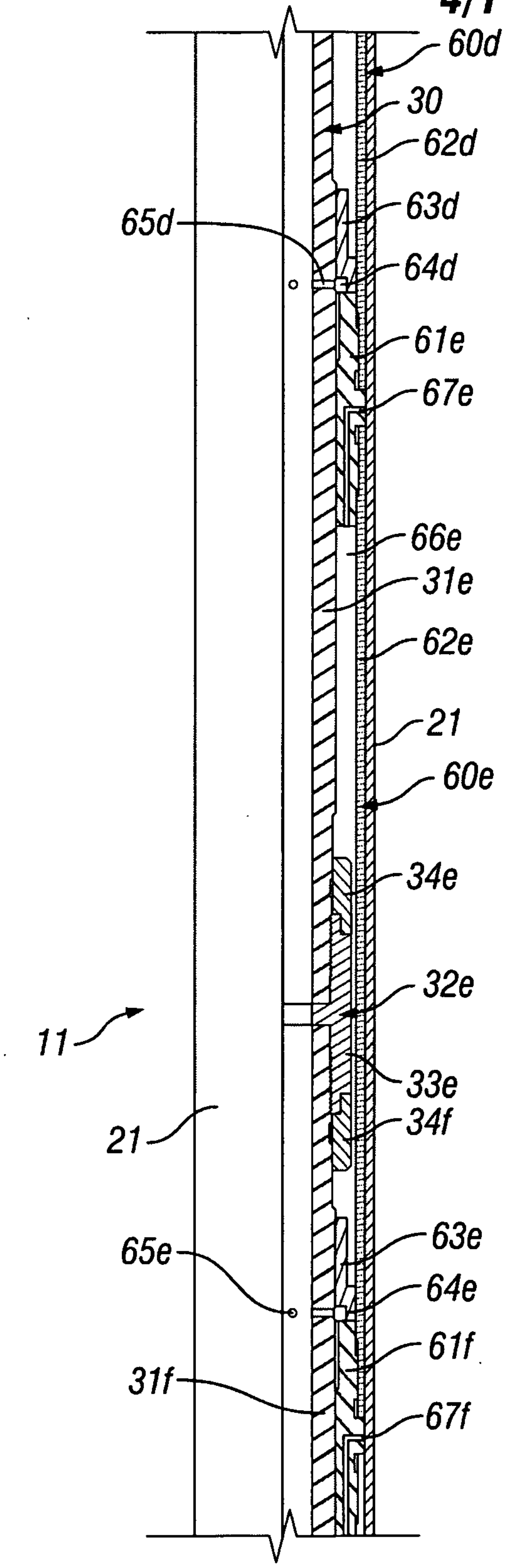



FIG. 3B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64e
61f
31f
67f

FIG. 4A

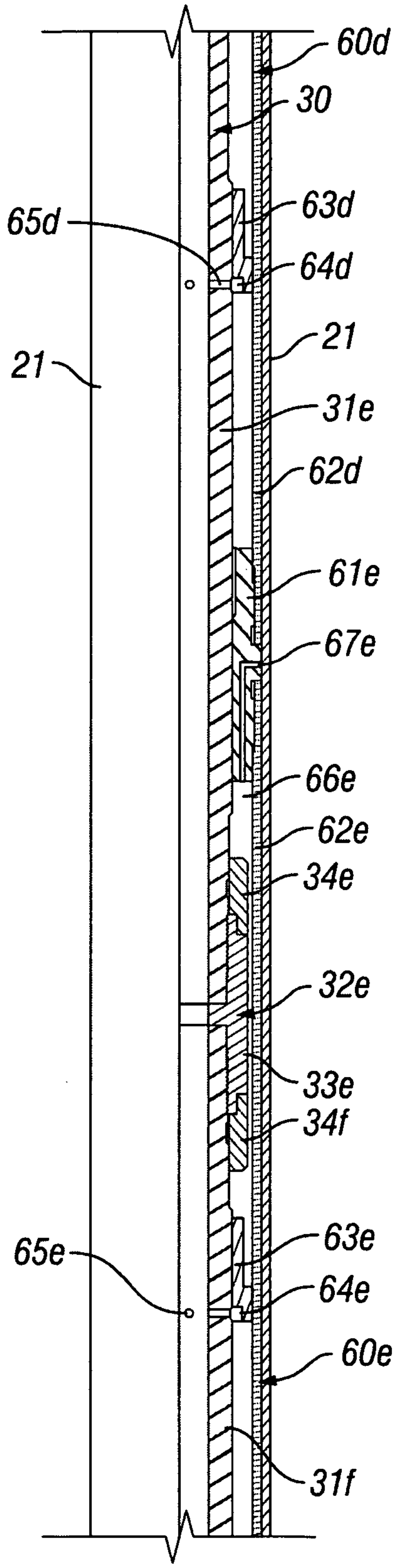
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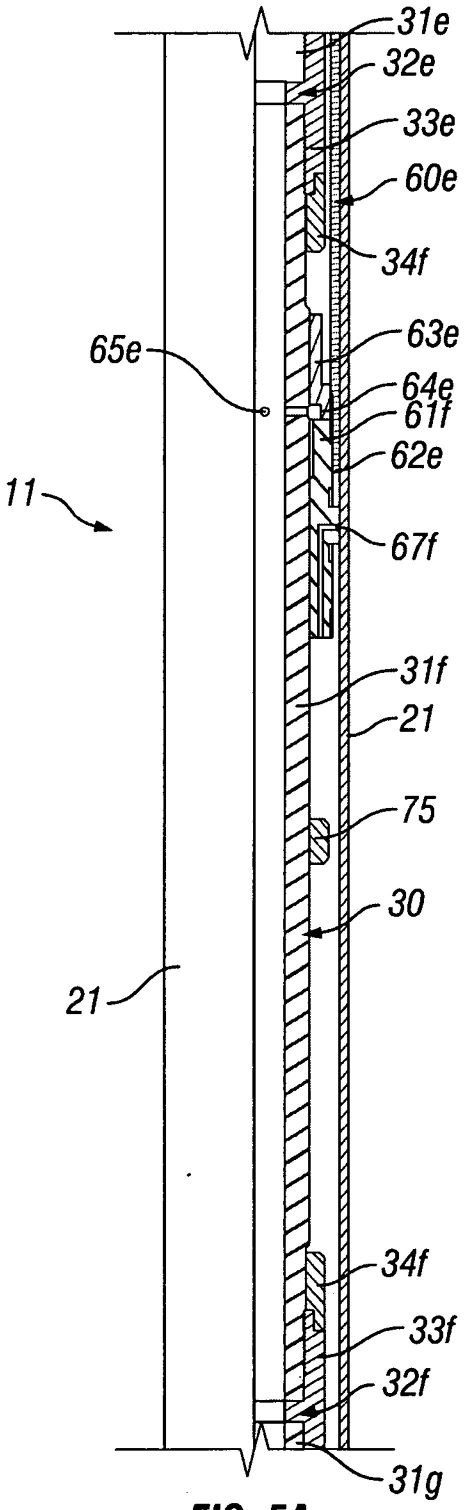
FIG. 4B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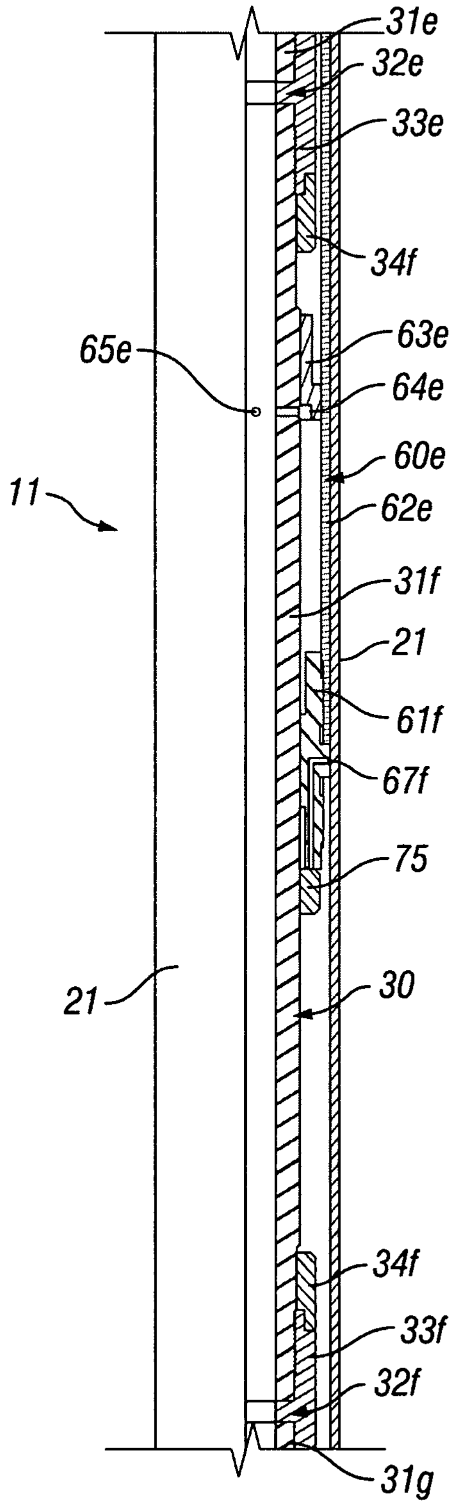
34f
33f
32f
31g

FIG. 5A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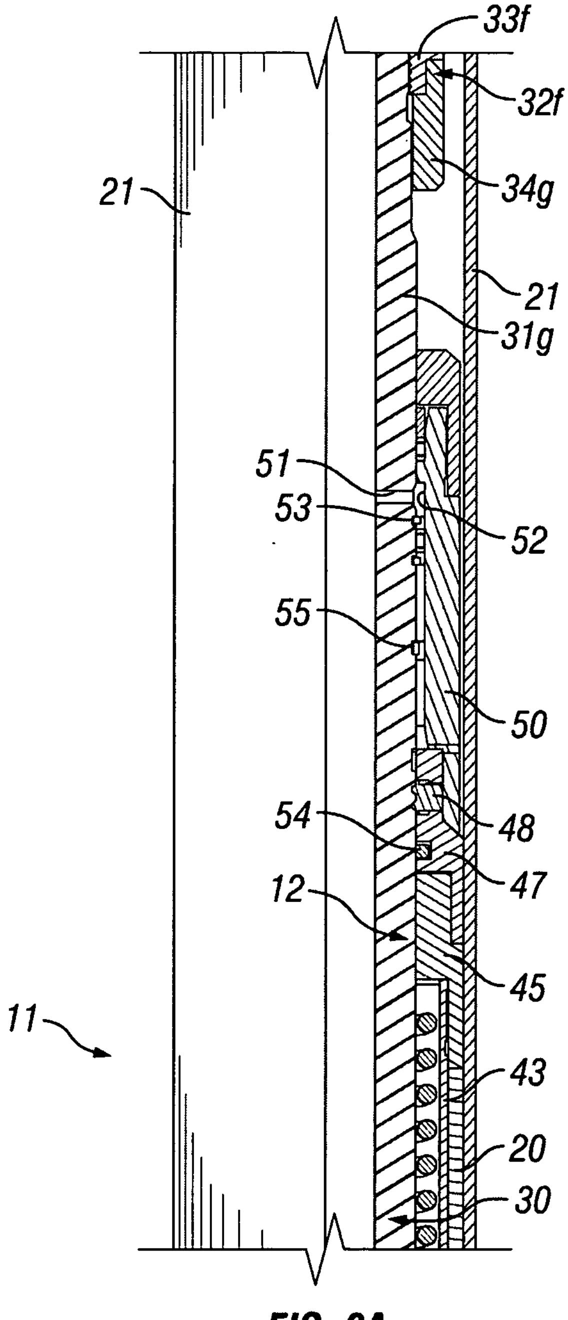
33f
32f
31g

FIG. 5B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30

FIG. 6A

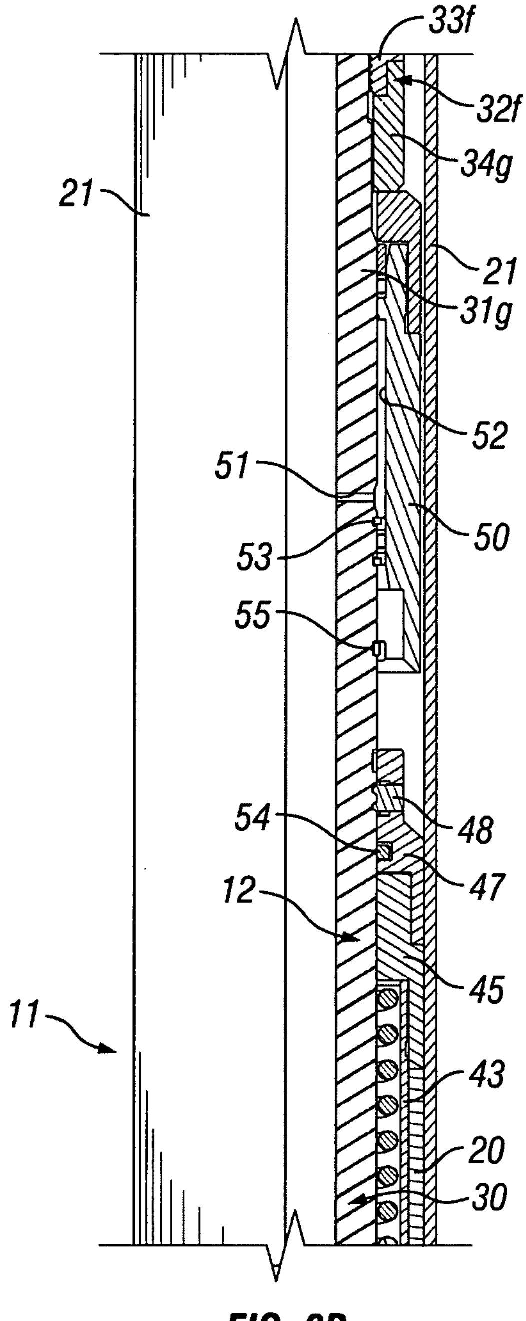
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FIG. 6B

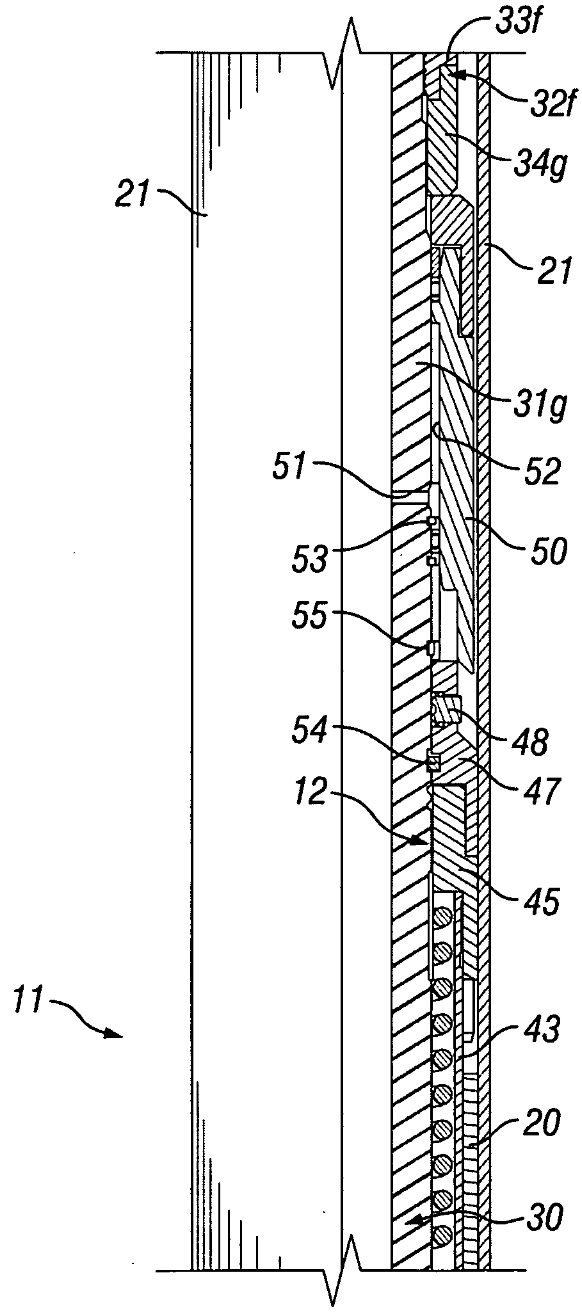


FIG. 6C

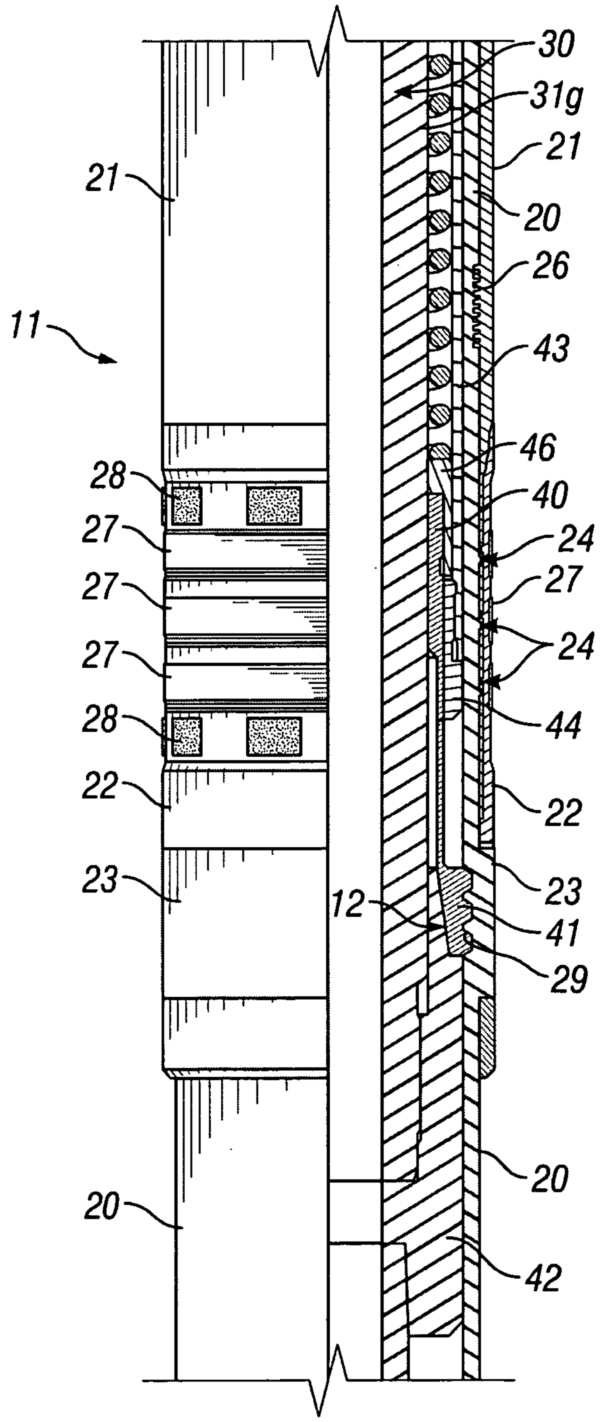
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FIG. 7A

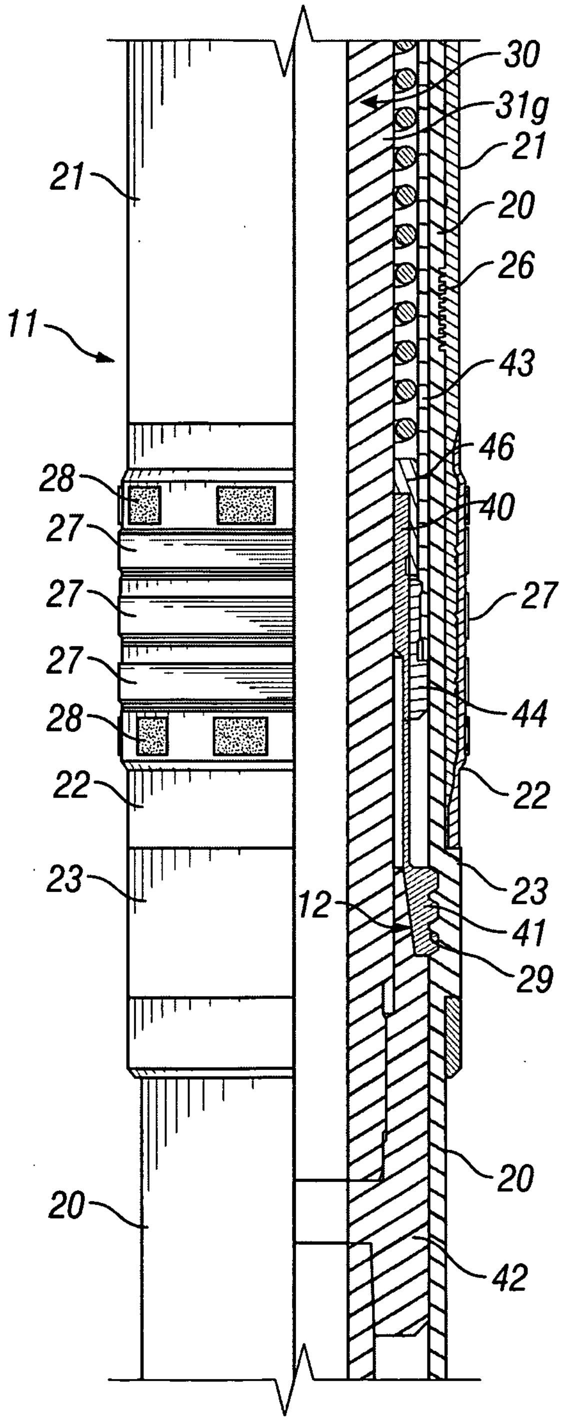
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FIG. 7B

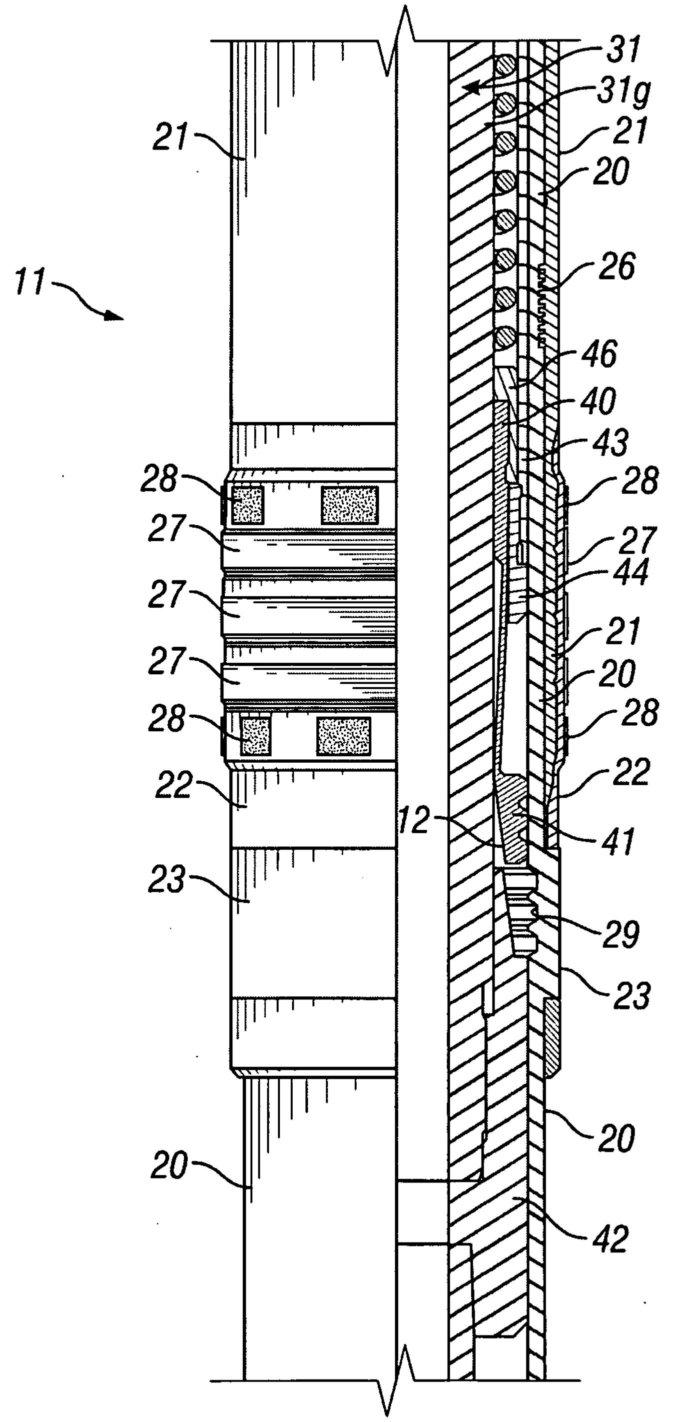
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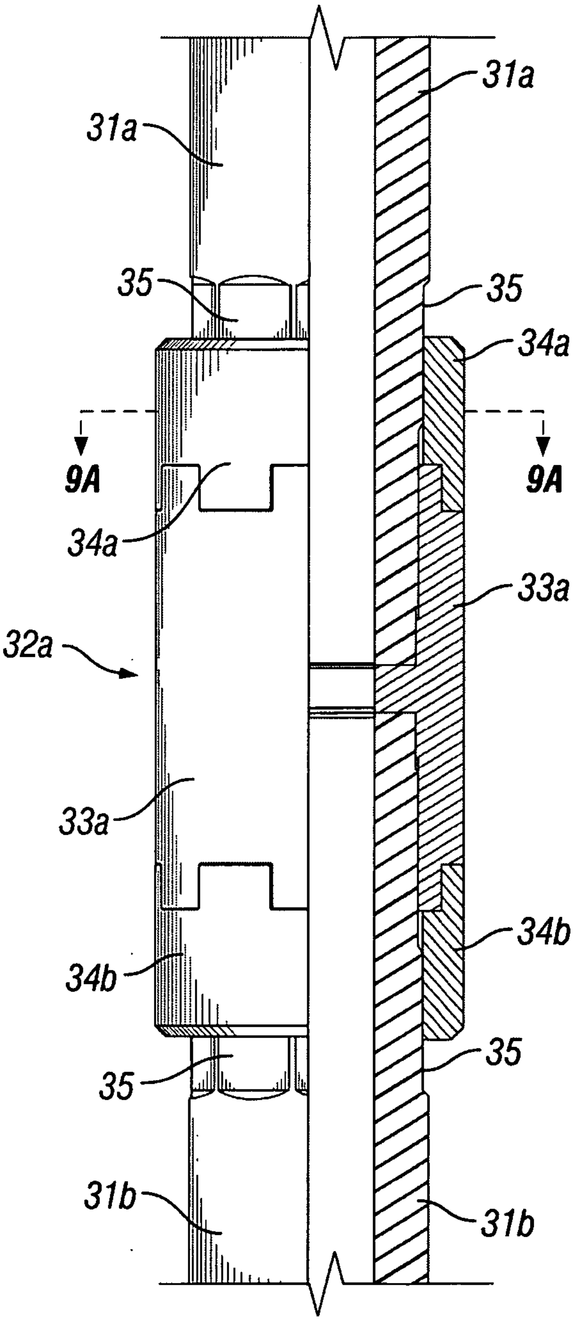
FIG. 7C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31b
31b

FIG. 8A

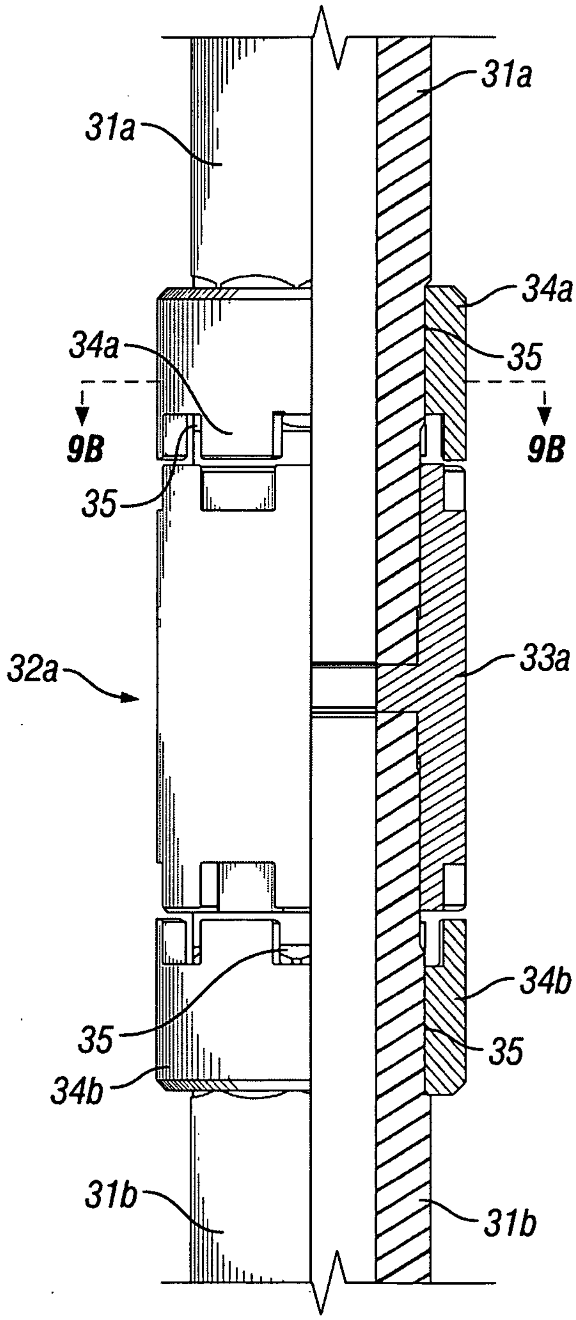
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FIG. 8B

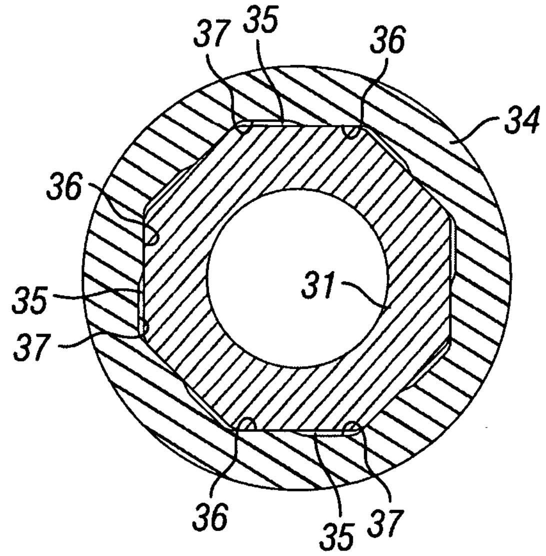


FIG. 9A

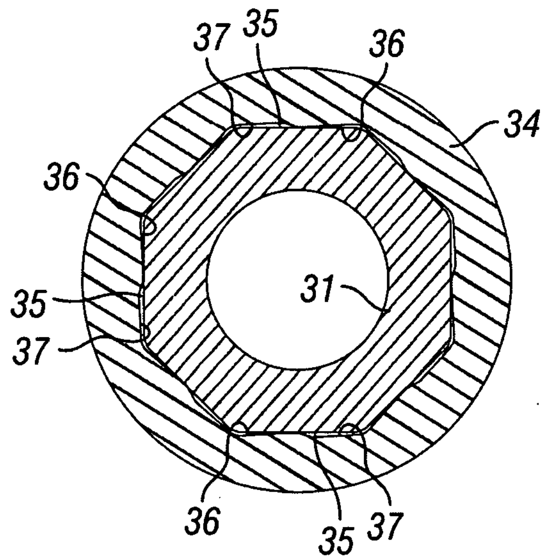


FIG. 9B