

**(19) AUSTRALIAN PATENT OFFICE**

(54) Title  
Method and apparatus for leak testing closed containers

(51) <sup>6</sup> International Patent Classification(s)  
G01M 3/00 060101BHAU  
(2006.01) PCT/CH00/0052  
G01M 3/00 6  
20060101AFI20

(21) Application No: 2000272661 (22) Application Date: 2000.09.26

(87) WIPO No: W000/73760

(43) Publication Date : 2000.12.18  
(43) Publication Journal Date : 2001.03.01

(71) Applicant(s)  
Martin Lehmann

(72) Inventor(s)  
Lehmann, Martin

(74) Agent/Attorney  
Spruson & Ferguson, Level 35 St Martins Tower 31 Market  
Street, Sydney, NSW, 2000

(56) Related Art  
WO 98/54560  
US 3837215  
US 4756184  
EP 619015

CORRECTED VERSION

(19) World Intellectual Property Organization  
International Bureau



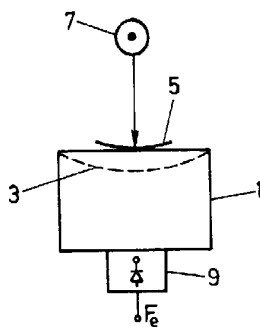
(43) International Publication Date  
7 December 2000 (07.12.2000)

PCT

(10) International Publication Number  
WO 00/073760 A3

- (51) International Patent Classification<sup>7</sup>: G01M 3/36
- (21) International Application Number: PCT/CH00/00526
- (22) International Filing Date:  
26 September 2000 (26.09.2000)
- (25) Filing Language: English
- (26) Publication Language: English
- (71) Applicant and  
(72) Inventor: LEHMANN, Martin [CH/CH]; Obere Farn-  
bühlstrasse 1, CH-5610 Wohlen 1 (CH).
- (74) Agent: TROESCH SCHEIDEGGER WERNER AG;  
Schwänzenmos 14, CH-8126 Zumikon (CH).
- (84) Designated States (*regional*): ARIPO patent (GI, GM,  
KI, LS, MW, MZ, SD, SI, SZ, TZ, UG, ZW), Eurasian  
patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European  
patent (AT, BF, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE,  
IT, LU, MC, NL, PT, SI), OAPI patent (BJ, BJ, CI, CG,  
CI, CM, GA, GN, GW, ML, MR, NE, SN, TD, TG).
- Published:  
*with international search report  
upon request of the applicant, before the expiration of the  
time limit referred to in Article 21(2)(a)*
- (88) Date of publication of the international search report:  
25 October 2001
- (48) Date of publication of this corrected version:  
6 September 2002
- (81) Designated States (*national*): AE, AG, AL, AM, AT, AU,  
AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CR, CU, CZ,  
DE, DK, DM, DZ, EE, ES, FI, GB, GD, GE, GH, GM, HR,  
HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR,  
LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ,  
NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM,  
TR, TT, TZ, UA, UG, US, UZ, VN, YU, ZA, ZW.
- (15) Information about Correction:  
see PCT Gazette No. 36/2002 of 6 September 2002, Sec-  
tion II
- For two-letter codes and other abbreviations, refer to the "Guid-  
ance Notes on Codes and Abbreviations" appearing at the begin-  
ning of each regular issue of the PCT Gazette.*

(54) Title: METHOD AND APPARATUS FOR LEAK TESTING CLOSED CONTAINERS



(57) Abstract: Method and apparatus for leak testing a closed container with at least one flexible wall area. A biasing member is moved towards and onto the flexible wall area in order to apply a predetermined force and the reaction forces are monitored over time.

WO 00/073760 A3

**Method and apparatus for leak testing closed containers**

The present invention is directed to a method for leak testing closed containers with at least one flexible wall area and to a leak testing apparatus for leak testing a closed container with such flexible wall area, irrespective whether such container is filled with a product or not.

- When testing closed containers one known technique is to arrange a container to be tested into a test cavity which is then sealingly closed, then to evacuate the interior space of the test cavity around the container to be tested and to evaluate the time behaviour of the pressure in the surrounding of the container after evacuation has been stopped at a predetermined level. Although this technique is of very high accuracy it necessitates utmost care for reaching such high accuracy. The volume of the test cavity and its shape must snugly fit the outside shape of the container to be tested. On one hand minimising this volume leads to respectively short evacuation time, on the other hand the degree of this minimising largely governs the detection accuracy reached. As a change in pressure in the surrounding of the container is detected as leak indication entity, the smaller than the volume is in which, through a leak, pressure is affected, the higher will be the detection accuracy.
- Further, accuracy is largely influenced by the degree of vacuum which is established in the surrounding of the container, which makes it necessary, for high accuracy, to provide relatively expensive vacuum pumps, possibly even

CONFIRMATION COPY

multiple stage vacuum pumps, if vacuum is to be established down to the level as only reached with turbo vacuum pumps.

#### SUMMARY

5 A need exists to provide for a method and apparatus as mentioned above, which remedies for the drawbacks of state of the art leak testing technique using pressure monitoring. Disclosed is a method of leak testing as mentioned above, comprising the steps of relatively moving a biasing member  
10 towards and onto the flexible wall area of the container, stopping such moving and monitoring a biasing force on said container. The biasing force monitored is sampled at a first point in time resulting in a first force measuring signal and is sampled at least one second subsequent point  
15 in time, resulting in a second force measuring signal. There is further generated a difference signal in dependency of said two measuring signals as a leak indicative signal.

Thereby, the present invention departs from the recognition  
20 that if a container to be tested is biased, leading to either compression or expansion of such container, biasing forces will apply to surfaces applied externally to the wall of the container as reaction forces of the expanded or the compressed container. Such reaction forces may easily be  
25 monitored. If such biasing is installed to a predetermined level and then stopped, a tight container will lead to monitoring a constant reaction force according to the biasing level reached. If the container is leaky, there will occur an exchange of medium between the surrounding of  
30 the container and its inside, leading to a decrease of the reaction force monitored over time.

Thereby, the accuracy of such a technique is largely independent from the volume surrounding the container under test, and is further primarily given by the degree of biasing and the force detecting surface towards which the  
5 biased container reacts.

In a preferred embodiment of the inventive method, biasing is installed up to a predetermined biasing force.

Having reached such predetermined biasing force, it is further proposed to wait for a time span before by sampling  
10 the respective first and second force measuring signals are generated, in dependency of which the difference signal is generated. Thereby, in this time span the biased container can stabilise its shape. In one operating embodiment biasing of the container under test is controlled as a  
15 function of the difference signal generated, so as to hold said difference signal on a predetermined value and exploiting the action of the biasing member as a leak indication. Thereby, a negative feedback loop is established, where the biasing member controllably  
20 counteracts a change of force monitored due to leakage, so that in extreme no change of force will occur due to the fact that the biasing member maintains by appropriate action a constant reaction force.

In a most preferred embodiment biasing the container is not  
25 established by relatively moving external surfaces onto the wall of the container, but in that a pressure difference is installed between the inside of the container and its surrounding. Thereby, the pressure difference is in a most preferred embodiment established by evacuating the  
30 surrounding of the container. The flexible wall area of the

container has then the tendency of bowing outwards, and if this bowing outwards is barred by stationary surfaces outside the container, the container will act with a respective force on such surfaces. This force is monitored.

- 5 So as to avoid that due to the inventively exploited biasing, an existing leak in a container is clogged by the wall area with such leak being urged onto an external surface, it is proposed to provide surface areas contacted by the wall of the container, as it is biased, with a  
10 structure. Such a structure may be realised by interposing a mesh- or grid-like member between wall area of the container and such an external surface or, and preferably, by roughening such surface as by etching or machining.

- In a further preferred embodiment the first force measuring  
15 signal is stored and the difference signal is generated in dependency of the stored first force measuring signal and the second measuring signal.

- In a further preferred mode of operation, already in the first point in time there is generated the difference  
20 signal namely from the first force measuring signal stored, and the first force measuring signal unstored. The resulting difference signal, as a zero offset signal, is stored and zero offset of latter generated difference signal is compensated by the stored zero offset signal.

- 25 So as to early detect large leaks, then smaller leaks, it is further proposed to compare the biasing force monitored with at least one predetermined threshold value, at the latest when sampling at said first point in time, which leads to identifying very large leaks and further

preferably to compare the difference signal with at least one predetermined threshold value.

The leak testing apparatus according to the present invention comprises a biasing arrangement for compressing  
5 or expanding a container under test, further a force detector applicable to the wall of the container under test and generating an electric output signal. The output of the force detector is operationally connected to a storing unit, the output of the storing unit operationally  
10 connected to a comparator unit. The second input of the comparator unit is operationally connected to the output of the force detector.

The invention is especially suited for leak testing so-called pouches, all around flexible wall containers, filled  
15 e.g. with pasty material.

Further preferred forms of realising the inventive method and the inventive apparatus will be become apparent to the skilled artisan reading the following detailed description as well as the claims.

20 By way of examples the following figures show:

Fig. 1 schematically, a first embodiment of an inventive apparatus operating according to the inventive method, whereat a container under test is biased by compression, biasing member and force detector  
25 being arranged on opposite sides of the container;

Fig. 2 in a representation according to fig. 1, an embodiment whereat the container resides on a support and biasing member as well as force

detector are arranged on the opposite side of such support;

- Fig. 3 in a schematic representation according to those of figs. 1 and 2, a further and preferred embodiment of the inventive apparatus and method, whereat biasing the container is realised by evacuating the surrounding of the container under test;
- Fig. 4 a qualitative force versus time diagram explaining the inventive method as performed by an inventive apparatus;
- Fig. 5 by means of a schematic and simplified functional block/signal-flow diagram, an embodiment of the inventive apparatus operating according to the inventive method;
- Fig. 6 schematically and in a simplified form a preferred realisation of storing and comparing units as preferably used in the inventive apparatus;
- Figs. 7 and 8 schematically and in a perspective view, a test chamber for realising the invention as shown in fig. 3 and for testing pouches;
- Figs. 9 and 10 schematically, further preferred features at a test cavity operated according to fig. 3;
- Figs 11a



to 11c force-signal versus time diagrams showing a preferred realisation form of the inventive method by an inventive apparatus;

5 Fig. 12 by means of a signal flow/functional block diagram the embodiment of the inventive apparatus performing measurements as explained with the help of the figures 11a to 11c;

10 Fig. 13 a force signal versus time diagram showing the statistic distribution of biasing force reached after a predetermined time of biasing at unleaky containers of the same type due e.g. to manufacturing tolerances;

15 Fig. 14 a simplified functional block/signal-flow diagram showing a further preferred feature of the inventive apparatus and method for generating an adaptive threshold value at the embodiment according to fig. 12;

20 Fig. 15 over time, qualitatively time courses of adaptively varied threshold values of the inventive apparatus and method as realised by the embodiment of figs. 14 and 16, where

25 Fig. 16 shows an embodiment for adaptively adjusting a further reference or threshold value for the inventive method and as realised at the preferred apparatus, and

Fig. 17 schematically shows an inline plant for inline assembling and testing containers.

Fig. 1 shows schematically one principle according to the present invention. A container to be leak tested, 1, has an area of its wall 3 which is flexible. The principle of the present invention resides in the fact that for leak testing  
5 container 1 a biasing member 5 is moved by means of a drive 7 towards and onto the wall of the container 1 and a force detector 9 monitors the reaction force  $F$  and generates an electric signal  $F_{e1}$  according to that force  $F$ . As shown in fig. 2 in a preferred mode the force detector 9 is directly  
10 coupled to the biasing member 5 and both are driven relative to and onto the flexible area 3 of the wall of the container 1, which latter resides e.g. on a base plate 11.

In a still further preferred embodiment and as shown in fig. 3 the drive 7, which moves one of the biasing member  
15 5, of force detector 9 or of a combined force detector and biasing member 5/9 arrangement with respect to the flexible area 3 of the wall of container 1, is in fact realised as a pneumatic drive. Force detector 9 and biasing member 5 are kept stationary in a test chamber 13.

20 By means of an evacuation pump 15 the test chamber 13 is evacuated, thereby generating a pressure difference  $\Delta p$  between the surrounding of the container 1 and its interior, which is directed from the inside to the outside of the container. Thereby, the flexible wall portion 3 is  
25 bent outwards and moved towards and onto the force detector 9, which here and as a preferred embodiment simultaneously acts as biasing member and as force detector. As shown in dotted lines, it is also possible to pressurise the container 1 e.g. with a source 16 of pressurised gas, and

dependent on the wall structure of container 1, to have area 3 bowing outwards.

Irrespective of the technique, which is inventively exploited and with respect to where the biasing member 5, where the force detector 9 are arranged and how the drive 7 is realised, as a mechanical drive as shown in fig. 1 or 2 or by a pressure difference applied as shown in fig. 3, biasing container 1 by relatively moving biasing member 5 towards and onto container 1 leads to force detector 9 detecting a rising force  $F$  as the container 1 is urged together in the embodiments according to fig. 1 or 2 or is expanded according to the preferred embodiment of fig. 3. According to fig. 4, as soon as biasing member 5 contacts the wall  $t_0$  of container 1, the reaction force  $F$  rises as biasing member 5 is further urged onto the wall of container 1. After a predetermined time  $t_1$  the relative movement of container wall 1 and biasing member 5 is stopped. This leads to a constant reaction force  $F_0$ , if the container is unleaky and its wall does not further react up to achieving equilibrium of shape.

If the container under stress has a large leak  $LL$  according to course (b), then the biasing movement of the biasing member will not lead to a reaction force  $F$  achieving  $F_0$  at all, but after the time span according to  $t_1 - t_0$  a considerably smaller force  $F_{LL}$  will be measured or monitored by the force detector 9.

Thus, a large leak  $LL$  is inventively already detected if the biasing member is moved at a predetermined rate or speed towards and onto the container wall and after a

predetermined time span as of  $t_1 - t_0$  a predetermined force, as of  $F_0$ , is not reached.

- Preferably such a behaviour of the container is already detected after a time span which is shorter than  $t_1 - t_0$ ,  
5 so as to become able to stop biasing of the container early enough and before pressing or suctioning a product contained in the container to and into its surrounding. Thus, preferably, there is installed a shorter time span  $t_{LL} - t_0$  and after this time span of increased biasing it is  
10 checked whether a predetermined threshold force, according to fig. 4 as of  $F_{LL}$ , is reached or not. If it is not reached according to the biasing course (b) further biasing is stopped and the heavily leaky container is freed of any bias as quickly as possible.
- 15 If the container 1 is not heavily leaky, the reaction force monitored,  $F$ , will reach after the predetermined time span of increasing biasing,  $t_1 - t_0$ , the threshold value as of  $F_0$  as required and leakage behaviour of the container will only be detected afterwards.
- 20 After having checked for large leaks  $LL$  and having disabled further biasing of the container as at time  $t_1$ , preferably a predetermined time span  $t_2 - t_1$  up to  $t_2$  is installed, during which the system consisting of container 1, biasing member 5 and force detector 9 is left for attaining  
25 equilibrium e.g. of the shape of the container.

Thereby, in a preferred mode,  $t_2$  is set on the maximum value according to  $t_{max}$ , thus there is valid  $t_2 = t_{max}$ . This is especially done if the container under test does not experience e.g. a volume change under the stress of the

bias, which leads to a decrease of reaction force in a transient phase which decrease is not due to leakage.

At or after reaching  $t_2$  the monitored reaction force  $F$ , then prevailing,  $F_2$ , is sampled and stored. After lapse of  
5 a further time span  $t_3 - t_2$  up to  $t_3$  again the monitored reaction force  $F$  is sampled as  $F_3$  and is compared with reaction force  $F_2$  as was stored. Thus, the difference  $\Delta F$  of  $F_3$  and  $F_2$  is principally evaluated as leak indicative signal.

10 As further shown in fig. 4 it is also possible to sample and store force  $F_2$  on the rising slope of biasing the container 1 and to wait the force  $F$  monitored to re-reach in the falling slope of  $F$ , after having stopped further biasing -  $t_1$  - the value according to  $F_2$ , thereby  
15 indicating that the system has in fact stabilised. In this case time moment  $t_2$  will be defined by the force  $F$  as monitored re-reaching the preset and stored value  $F_2$ .

In fig. 5 the inventive apparatus in its principle form which performs the procedure as explained with the help of  
20 fig. 4 is schematically shown. Thereby, the same reference numbers are used as in the previous figures with respect to features already described. In the test chamber 13, which is vacuum tight, the container 1 to be tested is deposited. The vacuum pump 15 is operated controlled by a timing unit  
25 17. Pump 15 evacuates chamber 13 preferably at a constant and adjustable rate.

Combined biasing member and force detector 9/5 is rigidly mounted within chamber 13 and preferably opposite and adjacent to the area 3 of flexible wall of container 1. The  
30 force detector 9 generates electrical signal  $S(F)$  as a

function of the force acting between area 3 and contact area of the biasing/force detector assembly 9/5, which is as schematically shown provided with a surface structure 19 to prevent that surface shutting a leak of area 3

- 5 incidentally just happening to be located there, where area 3 is or is going to contact the assembly 9/5. The same structuring 19a is preferably provided at the bottom surface of chamber 13.

- 10 The signal  $S(F)$  is fed at a time  $t_{LL}$ , controlled by timing unit 17 as schematically shown and by switch unit  $SW_1$ , to a comparator unit 21, where at time moment  $t_{LL}$  the output signal  $S(F)$  is compared with the large leak indicative threshold value  $S_0(F_{LL})$  as preset at unit 23.

- 15 Whenever at moment  $t_{LL}$ ,  $S_0(F_{LL})$  is not reached by the force signal  $S(F)$ , switching unit  $SW_2$ , the input thereof being connected to  $S(F)$ , is opened disabling via a control unit 25 further biasing e.g. by pump 15. If the threshold value  $S(F_{LL})$  is at least reached by  $S(F)$  at the moment  $t_{LL}$ , then signal  $S(F)$  is led to a further switching unit  $SW_3$ , where, 20 controlled from timing unit 17 at moment  $t_2$ , the prevailing signal is in fact sampled and stored in storing unit 27. Thus, in unit 27 there is stored a value according to force  $F_2$  of fig. 4. The output of the storing unit 27 is fed to a comparing unit 28, to which, again controlled from timing 25 unit 17, at moment  $t_3$  signal  $S(F)$  is additionally fed according to the then prevailing value  $F_3$ . Thus, comparing unit 28 compares the force value at moment  $t_2$  with the value of that force prevailing at moment  $t_3$ . The output  $\Delta F$  of comparator unit 28 is indicative of leak behaviour of

container 1 under test beside of a large leak prevailing, which has been previously detected.

Instead of evaluating directly the output signal of comparator unit 28 it is possible to control biasing as a function of the output signal of comparator unit 28. Thereby, a negative feedback control loop is installed (not shown), wherein the comparator unit 28 compares a rated value according to the stored signal in storing unit 27 with an instantaneously prevailing signal,  $S(F)$  and as an adjusting unit in the negative feedback control loop a biasing member is operated to minimize the output signal of comparator unit 28. Thereby, the control signal of such biasing member 15 is exploited as leak indicative signal.

In Fig. 6 a most preferred realisation of storing unit 27 and comparator unit 28, schematically shown in fig. 5, is depicted.

The output signal of the force detector 9 in assembly 9/5 is input to a conversion unit 121, which comprises, as an input stage, an analogue to digital converter 121a, followed by a digital to analogue converter 121b. The output of the converter stage 121 is fed to a difference amplifier unit 123, which additionally receives directly the output signal from force detector 9. The output of the difference amplifier 123 according to the comparator unit 28 of fig. 5, acts on a further amplifier unit 125, the output of which being superimposed at 128 to its input via storage unit 127. The input of the storage unit 127 is fed from the output of unit 125. A timer unit 129, as timer unit 17 of fig. 5, controls the arrangement. For storing the signal according to the force value  $F_2$  as of fig. 5, at

time  $t_2$  the timer unit 129 enables a conversion cycle at unit 121, so that a reconverted analogue output signal  $el_o(F_2)$  appears at the analogue output.

Simultaneously the substantially same signal  $S(F)$  from  
5 force detector 9 is applied as a signal  $el(F_2)$  to the  
second input of unit 123. Thus, at the output unit 125, a  
zero signal should appear. Nevertheless, in general a zero  
offset signal will appear at the output of unit 125, which  
signal is stored in the storing unit 127, enabled by the  
10 timing unit 129, according to unit 17 of fig. 5. At time  $t_3$   
(fig. 5) no conversion is triggered at the unit 121, so  
that there appears at the input of amplifier 123 directly  
from force detector 9 the signal according to the force  
value  $F_3$  prevailing at  $t_3$ , and from stage 121 the stored  
15 signal according to force value  $F_2$ , which was prevailing at  
 $t_2$ . Further, the zero offset signal, which was stored to  
unit 127, is now superimposed as an offset compensating  
signal to the output of unit 123, so that the resulting  
signal at the output of amplifier unit 125 is zero offset  
20 compensated. This allows a very accurate measurement of the  
force difference  $\Delta F$  as of fig. 4.

When looking at either of the figs. 1, 2 or 3 it becomes  
clear that even if vacuum is used to bias the container's  
wall towards and onto the force detector, the volume of the  
25 test chamber 13 is not very critical with respect to the  
volume of the container to be tested. Whereas in evaluating  
a pressure as is done in prior art leak testers, here  
inventively a force is evaluated. When evaluating a  
pressure as e.g. the pressure prevailing in the surrounding  
30 of a container to be tested, then accuracy of measurement



is largely dependent on the remaining volume between the wall of the test chamber and that of the container, because leakage will affect the pressure in that intermediate volume the more the smaller than said intermediated volume  
5 is selected. According to the present invention by providing biasing a wall portion of the container a wall portion of the container is urged against the force detector. Leakage to the surrounding will affect such force irrespective of the surrounding volume and thus of the  
10 relative volume of the test chamber with respect to the container to be tested.

Nevertheless, under the aspect of shortening testing cycles it is recommended to provide testing chambers which are minimum in volume with respect to the containers to be  
15 tested therein, if biasing is performed by vacuumising according to fig. 3.

By selecting the established biasing according to  $F_0$  of fig. 4 and thereby the force and thus signal  $S(F)$ , the level of measuring is set and may be selected. As the  
20 flexible wall portion in its bowing action will reside along a successively larger contact area on the force detector and/or the biasing member with an eye on the embodiment of fig. 3, establishing a larger biasing pressure difference  $\Delta p$  will lead to an overproportionally  
25 rising biasing force  $F$ . This accords to an amplification of the signal  $\Delta F$  according to fig. 4 to be exploited. This again significantly improves accuracy of the overall measuring system and makes it easy to establish the range of evaluation signals.

In a preferred embodiment operating according to fig. 3 pouches filled with a product are tested. In fig. 7 and 8 there is shown, in a simplified representation, two halves of a test chamber or test cavity according to chamber 13 of  
5 fig. 3, tailored for testing pouches.

According to fig. 7 there is provided in a basis 30 a recess 32 substantially shaped according to pouch 34 (dashed lines) to be tested therein. For instance in the base plate 30 there is applied one or more than one  
10 suctioning line 36 to be connected to an evacuating pump according to pump 15.

The top plate 37 as of fig. 8, which is conceived similarly to the bottom plate 30, has a recess 38, which, once the top plate 37 is deposited upon the base plate 30, defines  
15 with recess 32 the test chamber or test cavity. The bottom surface 40b and the top surface 40a of the two plates 30 and 37 do snugly and vacuum tightly fit and are thereby, if necessary, provided with respective sealing members all around the recesses 32/38. In one (or possibly in both) of  
20 the plates 30, 37 there is installed a force detector arrangement 42 with a large detection surface 44 fitted to the shape of the test cavity. The force detector arrangement 42 preferably operates on the principle of resistance gauge, i.e. pressurising the surface 44 will  
25 generate a force according to pressure multiplied by contact surface, which will slightly bend the resistance gauge element, thereby generating the electric signal S(F) according to fig. 5.

Nevertheless, other force detectors operating on different  
30 physical principles may clearly be used, thereby preferably

force detectors, which operate on minimum mechanical movement. Thus, e.g. a piezo force detector may be used.

Especially when the test cavity as formed by the two recesses 32 and 38 of fig. 7 and 8 for testing pouches is made to snugly fit the shape of a container 1 (a pouch) to be tested therein, it is possible to get additional information especially about large leaks by measuring the electric impedance outside the container under test, which is changed whenever e.g. a liquid content of a leaky container is urged or suctioned out of such container. As shown only in the bottom plate 30 of fig. 7 and not in the top plate 37 of fig. 8, the inner surface of the test cavity may be subdivided in electrically conductive electrodes 44. Every second electrode 44 is connected to one input connector 46 to an impedance measuring unit 48, every electrode in-between to input connector 49. Impedance measuring unit 48 may measure AC and/or DC impedance, preferably DC impedance. Thus, whenever the container, as pouch 34, is biased and a liquid or pasty content is pressed into the test cavity, irrespective of large leak measurement according to figs. 4 and 5 as was discussed above, a change in impedance measured at the unit 48 will indicate such a leak, and the output signal of the impedance measuring unit 48 will stop further biasing of the container.

For cleaning a test cavity e.g. in case content of a leaky container has been pouring out into the test cavity, further (not shown) lines or pipes may be provided abutting in the test cavity and connected to liquid and/or gaseous cleaning media as to a source of air or, and preferably,

nitrogen and/or of pressurised liquid flushing medium and further (not shown) a heater may be incorporated into the walls of the test cavity to dry and additionally clean a spoiled test cavity.

- 5 A most important feature, which is preferably provided irrespective whether the system operates according to fig. 1 or 2 or according to fig. 3, shall now be described with the help of fig. 9 and 10.

Whenever a container 1 to be tested is biased, be it  
10 according to the teaching of the fig. 1 or 2, to which fig. 10 is directed or according to fig. 3, to which fig. 9 is directed, at least two wall portions of the container, which are disposed one opposite the other, denoted in the  
15 figs. 9 and 10 as 51a and 51b, will be firmly pressed onto the biasing member/force detector arrangement or more generically to surfaces. Whenever there happens a leak to be in such an area of container's wall, such a leak might be clogged by such a surface. Therefore and as  
20 schematically shown in figs. 9 and 10 there is provided at all surface areas to which, during biasing the container, a wall area thereof is pressed, a surface structure, so that such a surface does only contact the wall of the container 1 at distinct contact areas, leaving substantial parts of  
25 such wall portion uncontacted. This may be realised by providing a mesh- or grid-like member between the respective surfaces and wall portions of container 1 or by roughening such surfaces by machining such as by etching or sand-blasting. Mechanical abutments 53 as schematically  
30 shown in the figs. 9 and 10, which contact respective distinct areas of container's wall are formed by such

microstructuring of the respective surface. With an eye on the embodiment according to figs. 7 and 9 it is therefore recommended to have the surface of the respective plates 30 and 37, which form the recesses 32 and 38, mechanically  
5 machined to have a roughened microstructure. Thereby, it is prevented that any leak in the wall of the container may be clogged by the wall area of the container having such leak being urged onto a surface of the system, be it the biasing member surface, the force detector surface or another part  
10 of the test cavity's surface.

Force versus time courses as measured according to the inventive method and with an inventive apparatus in preferred mode are shown in fig. 11a for very large and large leaks VGL, in fig. 11b for small leaks and for  
15 unleaky containers in fig. 11c. These figs. shall be discussed in connection with fig. 12, which shows a preferred monitoring and control unit.

According to fig. 11a the timing unit 201 of fig. 12 initiates at time  $t_{10}$  biasing of a container 1 under test,  
20 be it according to the embodiment of fig. 1 or 2 or 3. According to the embodiment of fig. 3, thus the timing unit 201 initiates evacuation of the test cavity 13.

This is shown in fig. 12 by the biasing start signal BIST/ $t_{10}$ .

25 After a fixed predetermined amount of time  $\Delta T$  the output signal of the force detector S(F) becomes compared with a first reference signal preset at a presetting source 107, RFLVGL. To this target, comparator unit 102 is enabled by timer unit 201 at  $t_{10} + \Delta T$ .

If after time span  $\Delta T$  the actual monitored force according to the electric signal  $S(F)$  of fig. 12 has not reached the value of RFVGL according to course I of fig. 11a, this means that a very large leak VGL is present. This is  
5 detected at comparator 109 generating the output signal VGL. If according to the characteristics shown in the block 109 of fig. 12 the output signal of this comparator unit enabled at  $t_{11} = t_{10} + \Delta T$  is e.g. still at a high value, indicating presence of a VGL, this is output at the VGL  
10 output. If the biasing force  $F$  has reached and crossed the reference level RFVGL according to course II of fig. 11a the VGL output signal is not generated.

The VGL signal preferably stops the biasing cycle, because this would lead just to pressing content of the container  
15 under test into the surrounding.

As shown by the course II of fig. 11a as VGL does not occur, biasing of the container under test continues up to a further moment of time  $t_{13}$ . At the time  $t_{13}$  the timer unit 201 disables biasing drive, be it the mechanical drive 7  
20 according to the embodiments of the figs. 1 and 2, or the evacuation pump 15 as of the embodiment of fig. 3.

Further, position of timer unit 201 enables comparator unit 111, to which a further reference value RFGL is led, generated by a reference signal source 113. If at time  $t_{13}$   
25 the force detected by the force detector has not reached RFGL, then comparator unit 111 generates an output signal GL indicating that the container under test has a large leak GL. Here again, some reactions are taken with respect to further operation of the testing system.

If either of the signals VGL or GL are initiated by the respective comparators 109, 111 the timer unit 201 is principally reset because the testing has been completed and the quality of the instantaneously tested container 1  
5 established has been identified. This is schematically shown in fig. 12 by the signal  $RS_{201}$ . If not reset shortly after  $t_{13}$  the value  $S(F)(t_{13})$  of the force detected by the force detector is stored in a holding or storing unit 117. The output of the holding or storing unit 117 is led to one  
10 input of the difference forming unit 119, whereas the second input of this unit 119 is connected to the output  $S(F)$  of the force detector. After a presettable test cycle time  $T_T$  starting at  $t_{13}$  or at the moment of storing data in storing unit 117, as schematically shown by unit 121 of  
15 fig. 12 the force difference  $\Delta F$ -signal is fed to a further comparator unit 125 enabled at the lapse of testing time  $T_T$ .

By means of a further reference value source 127 the reference value  $\Delta F_{REF}$  is fed to the comparator unit 125. As  
20 will be explained later the value of  $\Delta F_{REF}$  may controllably be varied in time and/or a reference value  $\phi_R$ , to which  $\Delta F_{REF}$  is referred to, may also controllably be varied in time.

If the  $\Delta F$ -signal at time  $t_{13} + T_T$  is larger than the  
25 reference value  $\Delta F_{REF}$ , then a signal FL is generated at unit 125, indicating presence of a fine leak FL in the container 1 under test. This according to the situation as shown in fig. 11b. If the  $\Delta F$ -signal does not reach  $\Delta F_{REF}$  then the container is considered unleaky, as none of the

signals VGL, GL and FL has been generated. This accords with fig. 11c.

If the VGL signal is generated according to fig. 12 irrespective of the embodiment according to one of the  
5 figs. 1, 2 and 3, further biasing is immediately stopped.  
In the embodiment of fig. 3 making use of an evacuation pump 15 as a biasing drive, the evacuation pump 15 is immediately disconnected from the respective testing chamber 13. This because by a very large leak the vacuum  
10 pump 15 could become contaminated by leaking content of the container 1.

In a multiple chamber inline testing system making use of the embodiment of fig. 3 with a multitude of testing chambers occurrence of the signal GL - indicating a large  
15 leak - and possibly even the occurrence of the signal FL - indicating for a fine leak - leads preferably to disabling or "bypassing" that chamber from further being supplied with containers to be tested, whereas the other chambers are still operating and performing tests on newly supplied  
20 containers.

This bypass of a testing chamber 13, whereat a container has been identified as heavily or even slightly leaking, is performed so as not to influence further testing results at that chamber and especially not to spoil the vacuum pump 15  
25 connected thereto due to content of the leaky container being suctioned towards and into such pump. This bypass chamber is reconditioned during further testing cycles at the other chambers after the leaky container having been removed.



Reconditioning may be done by heating that chamber 13, flushing it by a liquid and/or a gas, preferably nitrogen, especially by a heated gas.

When looking to the figs. 11a and 11b it may be recognised  
5 that setting the reference value  $RFGL$  and especially setting of the reference force difference value  $\Delta FREF$  may be very critical and may largely influence accuracy of the system. Thereby, influences as surrounding temperature, tolerances of container manufacturing etc. may influence  
10 the prevailing force course and lead to false results if these critical reference levels and especially  $\Delta FREF$  are set for utmost accuracy.

In fig. 13 there is qualitatively shown the biasing force course according to the courses of fig. 11a to 11b, but  
15 measured at containers of the same type which have been proven as unleaky. This may have been done by long-term experiments and/or leak detecting systems, which are standard and of utmost accuracy, but slow and/or very expensive.

20 At  $t_{13}$  the force values measured at the tight containers are slightly different and define a statistic distribution as shown in fig. 13. There results an average value  $(RFGL)_m$ . The value of  $RFGL$  as used at the comparator 111 of fig. 12 or as used according to the figs. 11a to 11c is  
25 found in that an offset value  $\Delta RFGL$  is subtracted from  $(RFGL)_m$ . During ongoing operation on large series of equal containers, temperatures and manufacturing tolerances of such containers may vary. Such parameters may slowly change and may vary  $(RFGL)_m$ .

Every time during multiple successive testing at the respective times  $t_{13}$  up to which the respective container has been identified as not heavily leaky, the actual output signal of the force detector is entered into an averaging unit 130 as shown in fig. 14, wherein the last  $m$  values of actual force of not heavily leaky containers are averaged. The output average result signal accords with  $(RFGL)_m$  of fig. 13, now varies in time e.g. due to varying manufacturing parameters of one and the same type of containers. To the output average result  $\overline{S(F)}$  and according to fig. 13 the offset  $\Delta RFGL$  is subtracted, the result of this operation is a dynamically varying reference value  $RFGL$ , which is applied to comparator unit 111 of fig. 12. This dynamically varying reference value  $RFGL$  is shown in fig. 15 qualitatively, starting from an initial setting as e.g. found as was explained with the help of measurements at unleaky test containers.

As may clearly be seen from fig. 15 the average force value  $\overline{S(F)}(t_{13})$  is now the basis for also referring  $\Delta FREF$  to. Therefore, and as is shown in fig. 12, the force difference reference value  $\Delta FREF$  is not referred to an absolute static value as  $\phi_R$ , but is referred to  $\overline{S(F)}$ .

An even further improvement of accuracy is reached, which may be realised separately or additionally to realising a dynamic  $RFGL$  and based thereon a dynamic upper limit of  $\Delta FREF$ . Thereby and according to fig. 16 at the end of the time span  $T_T$  the actual force difference  $\Delta F$ -signal is led to an averaging unit 135 whenever the output signal  $FL$  indicates that the container under test is unleaky. The

output signal of unit 135, which accords to an average force difference signal  $\overline{\Delta F}$  averaged over the last m test cycles is, offset by an amount  $\Delta\Delta F$ , the result thereof being used as time varying  $\Delta F_{REF}$ -signal applied at unit 127  
5 of fig. 12.

Looking back on fig. 15 whereat a constant  $\Delta F_{REF}$  signal was applied, the technique of averaging  $\Delta F$  results as schematically shown with the course  $(\Delta F_{REF})_t$  in a dynamically varying value  $\Delta F_{REF}$ , varying according to  
10 variations of disturbing parameters influencing such force difference. It is clear that provision of a dynamically varying  $(\Delta F_{REF})_t$  signal according to that representation in fig. 15 could be realised without providing a dynamically varying base value  $\overline{S(F)}$  in referring  $(\Delta F_{REF})_t$   
15 to a stable constant value  $\phi_R$  as shown in fig. 12 in dashed representation instead of referring to a dynamically varying  $\overline{S(F)}$  value.

It is evident that preferably the evaluation of the output signal  $S(F)$  of the one or more than one force detectors is  
20 performed digitally.

In fig. 17 there is shown an inline plant, wherein generically assembling and testing of containers is done inline. As an example pouches are first welded at a welding station 60 in a base plate 30 as shown in fig. 7 used as  
25 carrier and support for assembling. With the same carrier, namely base plate 30, after a pouch has been assembled therein by welding, the carrier formed by plate 30 is moved to an applicator station, where the top plate 37 as of fig.

8 is assembled upon the bottom plate 30. Thereafter, the thus sealingly closed test cavity is moved and applied to a test station 64, where the inventive test is performed. The system of welder 60 and/or applicator 62 and/or tester 64 may thereby be stationary with respect to a conveyor 66 for base plate 30. Nevertheless, and depending on time requested for a certain operation, especially tester 64 may be moved together with conveyor 66 for a predetermined time, so as to become independent of speed of conveyor 66.

10 With the inventive method and apparatus there is provided a leak testing technique which is much less critical in achieving the same accuracy as with leak testing techniques evaluating pressure measurements. Biasing containers according to the present invention is much simpler than

15 establishing a perfect vacuum around such container and measuring a biasing force considerably easier than accurately measuring the time development of a vacuum pressure surrounding the container. In vacuum measurement much more unknown and uncontrollable parameters may affect

20 the measured entities, namely vacuum pressure, than in the here inventively exploited force measurement. Whereas setting of the measuring level in vacuum measurement technique greatly influences the expenditure for vacuum pumps, varying and setting a biasing force is of much less

25 effort.

The inventive method and apparatus are especially suited for testing pouches, but clearly may be used for testing all kinds of containers up to big tanks as long as a wall portion thereof is flexibly bendable. The present invention

30 may be realised at inline plants with a multitude of

testing stations, e.g. arranged on a carousel with a very high throughput.

**The claims defining the invention are as follows:**

1. A method for leak testing closed containers with at least one flexible  
5 wall area, comprising the steps of:
- moving a biasing member relatively to, towards and onto said wall area;
  - stopping said moving;
  - monitoring a biasing force on said container;
  - sampling said biasing force monitored at a first point in time, resulting in a first  
10 force measuring signal;
  - storing a signal dependent on said first force measuring signal, thereby  
generating a stored signal;
  - forming a first difference signal of said signal dependent on said first force  
measuring signal and said stored signal substantially when said storing is performed;
  - 15 - sampling said biasing force monitored at at least one second subsequent point  
in time, resulting in a second force measuring signal;
  - generating a second difference signal in dependency of said stored signal, said  
second force measuring signal and said first difference signal as a leak indicative signal.
- 20 2. The method of claim 1, further comprising the step of biasing said wall  
area up to a predetermined biasing.
3. The method of claim 2, thereby installing between reaching said  
predetermined force a time span before performing said sampling.
- 25 4. The method of claim 1, further comprising the step of controlling said  
biasing as a function of said difference signal so as to hold said difference signal on a  
predetermined value and exploiting relative action of said biasing member as a leak  
indication.
- 30 5. The method of one of claims 1 to 4, further comprising the step of  
performing said moving by establishing a pressure difference between the inside of said  
container and its surrounding.

6. The method of claim 5, further comprising the step of establishing said pressure difference by evacuating said surrounding.

7. The method of one of claims 1 to 6, further comprising the step of  
5 providing surface areas contacted by the wall of said container as it is biased with a structure.

8. The method of one of claims 1 to 7, further comprising the step of  
comparing said biasing force monitored with at least one predetermined threshold value at  
10 the latest when sampling at said first point in time.

9. The method of one of claims 1 to 8, further comprising the step of  
comparing said second difference signal with at least one predetermined threshold value.

10. The method of one of claims 1 to 9, further comprising the step of  
15 storing said first force measuring signal by means of an analogue to digital converter enabled for conversion at said first point in time.

11. The method of claim 10, further comprising the step of reconvert the  
20 digital output signal of said analogue to digital converter into an analogue signal and generating said difference signals with said reconverted analogue signal.

12. The method of one of claims 1 to 11, further comprising the step of  
performing an impedance measurement at or at least adjacent to the wall of said  
25 container, preferably a resistance measurement with DC and enabling or disabling further moving of said biasing member towards and onto said wall area by the result of said impedance measurement.

13. The method of one of claims 1 to 12, further comprising the step of  
30 monitoring said biasing force by means of a resistance gauge.

14. The method of one of claims 1 to 13, further comprising the steps of  
sampling said biasing force monitored at a third point in time, not later than said first  
point in time, resulting in a third force measuring signal, comparing said third force

measuring signal with a presettable threshold signal value and generating a "large leak" indication, if said third force measuring signal does not reach said threshold signal value.

15        15.        The method of one of claims 1 to 14, further comprising the step of  
providing a test cavity for said container and cleaning said test cavity after a container  
therein has been detected as leaky, said cleaning being performed by flushing with a gas,  
preferably with nitrogen and/or by flushing with a liquid and/or by heating.

10        16.        The method of one of claims 1 to 15, further comprising the step of  
inline testing a series of said containers in a set of test cavities and further comprising the  
step of disabling testing in a test cavity for at least one testing cycle if the container  
previously tested therein has turned out to be leaky to a predetermined amount.

15        17.        The method of one of claims 1 to 16, further comprising the steps of :  
- moving said biasing member towards and onto said wall area with a  
predetermined rate;  
- identifying for a large leak by monitoring said biasing force after a  
predetermined time of said moving and by monitoring whether said biasing force  
monitored has or has not reached a first predetermined threshold value.

20        18.        The method of one of claims 1 to 17, further comprising the step of  
moving said biasing member at a constant rate towards and onto said wall area.

25        19.        The method of one of claims 1 to 18, further comprising the steps of  
averaging said first force measuring signal with first force measuring signals sampled  
during previous testing of containers and generating said difference in dependency of said  
averaged first measuring signal.

30        20.        The method of claim 19, further comprising the steps of shifting said  
averaged signal by a predetermined signal amount and generating said difference in  
dependency of said shifted averaged signal.

35        21.        The method of one of claims 1 to 20, further comprising the step of  
comparing said second difference signal with at least one threshold signal.



22. The method of claim 21, further comprising the step of averaging said second difference signal with such difference signals generated during previous testing of containers and controlling said threshold value in dependency of said averaging.

5 23. A leak testing apparatus for leak testing a closed container with at least one flexible wall area comprising:

- a biasing arrangement for compressing or expanding a container under test;
- a force detector applicable to the wall of a container under test and generating an electric output signal, the output of said force detector being operationally connected

10 to a storing unit, the output of said storing unit being operationally connected to a comparator unit, the second input thereof being operationally connected to the output of said force detector.

24. The apparatus of claim 23, wherein said biasing arrangement comprises

15 a pair of spaced apart members, said members being drivingly movable relatively to each others and towards and from each others.

25. The apparatus of claim 24, wherein said at least one force detector is mounted to one of said members.

20

26. The apparatus of claim 23, further comprising a sealingly closable test chamber connected to an evacuation pump, said force detector being rigidly mounted to said test chamber with a force sensing surface exposed to the interior of said test chamber.

25 27. The apparatus of one of claims 23 to 26, wherein said force detector comprises a resistance gauge.

28. The apparatus of one of claims 23 to 27, further comprising a timing unit controlling storing at said storage unit at a first point in time and comparison at said

30 comparing unit at a second point in time after said first point in time.

29. The apparatus of one of claims 23 to 28, wherein said storing unit comprises an analogue to digital converter.

30. The apparatus of one of claims 23 to 29, wherein said comparator unit comprises a difference input stage, the inputs thereof being operationally connected to the output of said force detector and to the output of said storage unit, the output of said input stage being operationally connected to a further storage unit, the output of said further storage unit being fed back towards the input of said comparator unit.

31. The apparatus of one of claims 23 to 30, comprising an evacuable test chamber and at least a pair of electrodes arranged within said test chamber and operationally connected to an impedance measuring unit.

32. The apparatus of one of claims 23 to 31, wherein external surfaces contacting a container to be tested as it is biased by said biasing arrangement are provided with a surface structure.

33. The apparatus of claim 32, wherein said surface structure is formed by mesh or grid inlay or by a surface roughening machining of said surfaces.

34. The apparatus of one of claims 23 to 33, further comprising a first threshold-sensitive unit, one input thereof being operationally connected to the output of said force detector, the output thereof being operationally connected to a control input of the biasing arrangement.

35. The apparatus of claim 34, further comprising a second threshold-sensitive unit, the input thereof being operationally connected to the output of said force detector and comprising a timing unit enabling said first and second threshold-sensitive units at different points in time.

36. The apparatus of one of claims 23 to 35, further comprising an averaging unit, the input thereof being operationally connected to the output of said force detector, the output thereof being operationally connected to a threshold unit, a second input thereof being operationally connected to the output of said force detector.

37. A method for leak testing closed containers with at least one flexible wall area, said method being substantially as described herein with reference to the accompanying drawings.

38. A leak testing apparatus for leak testing a closed container with at least one flexible wall area, said leak testing apparatus being substantially as described herein with reference to the accompanying drawings.

5

DATED this twelfth Day of July, 2005

**Martin Lehmann**

10

Patent Attorneys for the Applicant

SPRUSON & FERGUSON

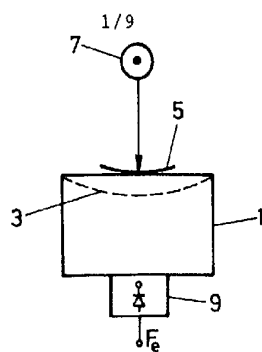


FIG. 1

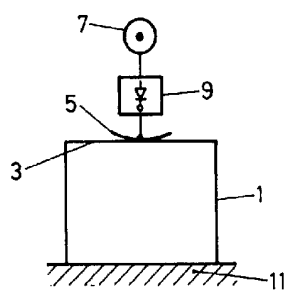


FIG. 2

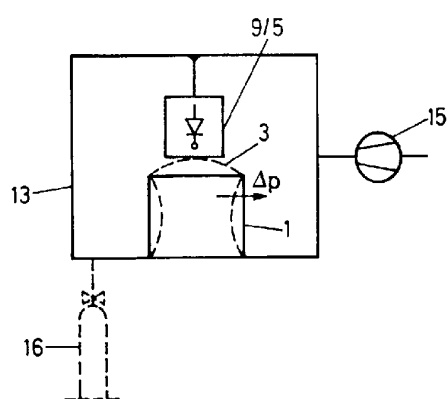


FIG. 3

SUBSTITUTE SHEET (RULE 26)

2/9

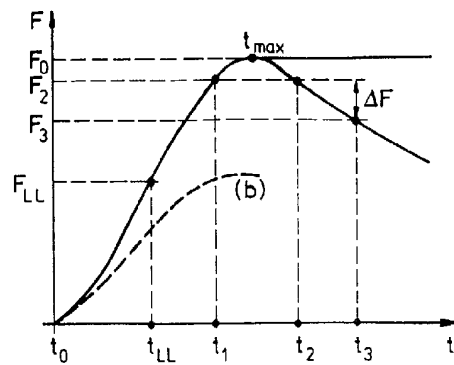


FIG. 4

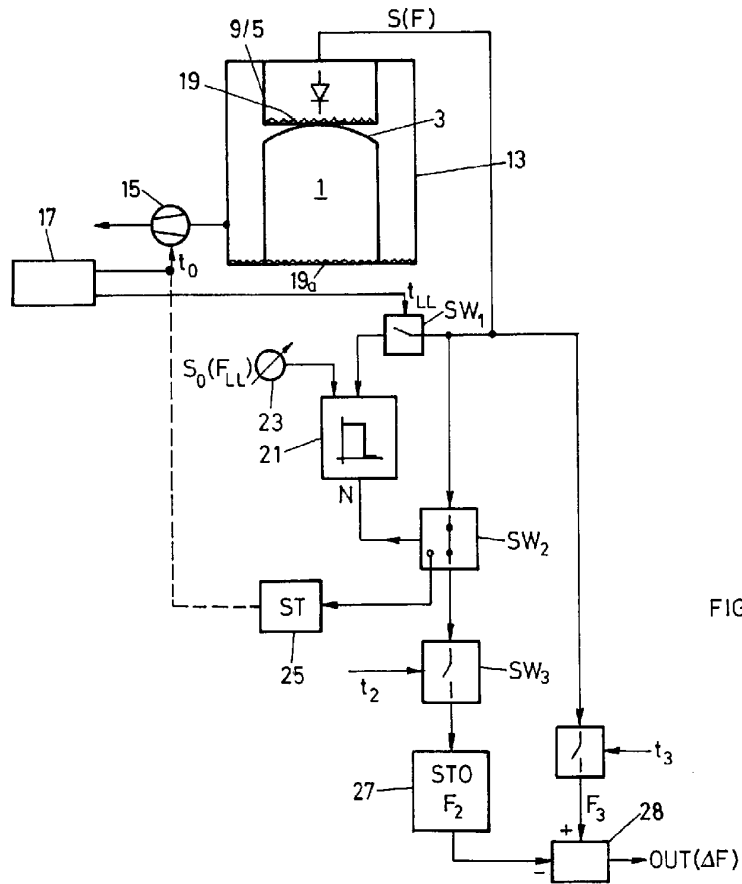
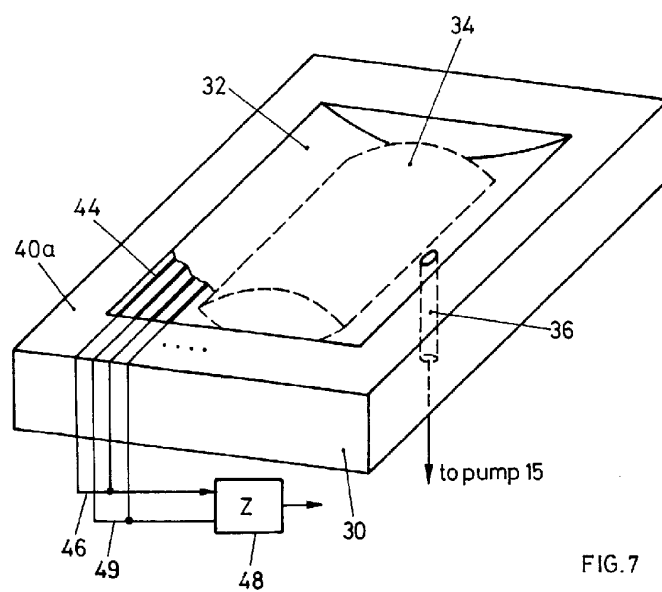
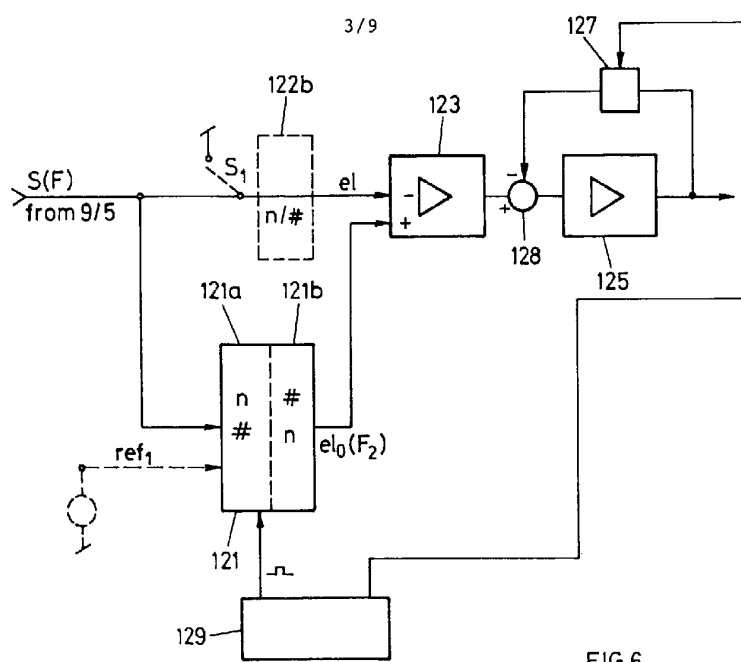


FIG. 5

SUBSTITUTE SHEET (RULE 26)



SUBSTITUTE SHEET (RULE 26)

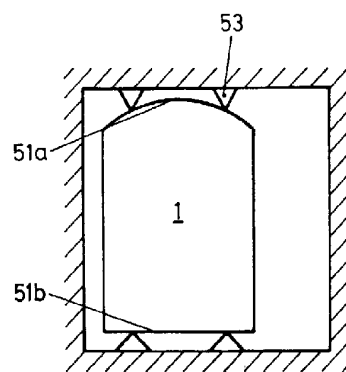
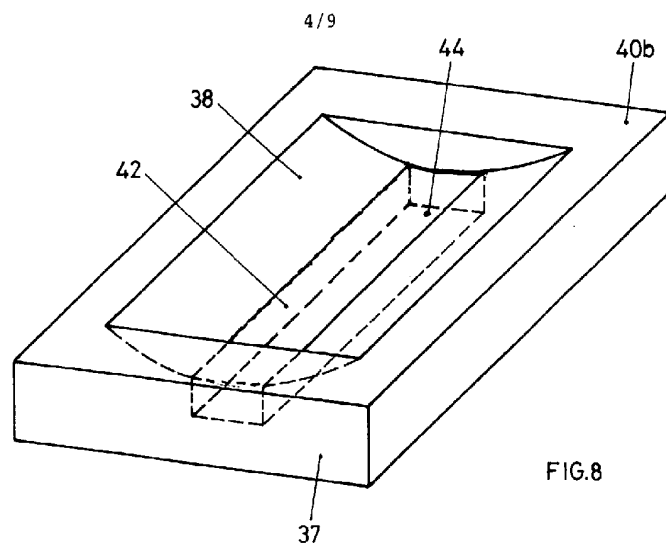


FIG. 9

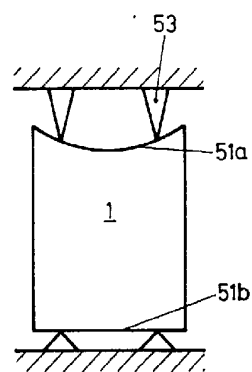
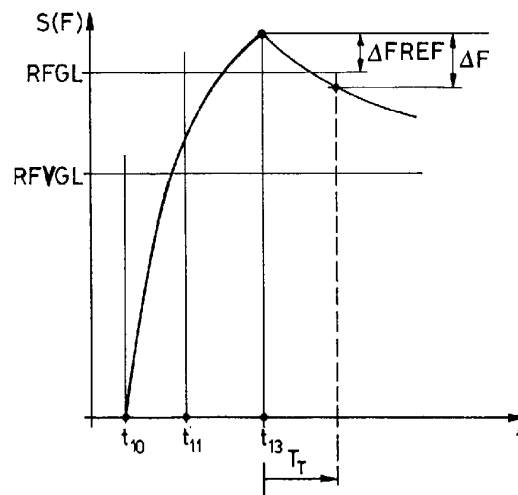
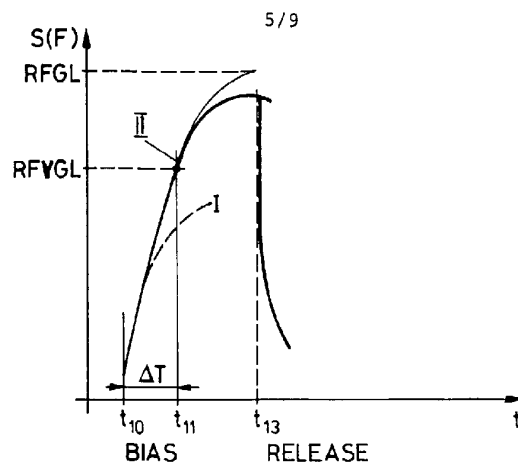


FIG. 10

SUBSTITUTE SHEET (RULE 26)



SUBSTITUTE SHEET (RULE 26)



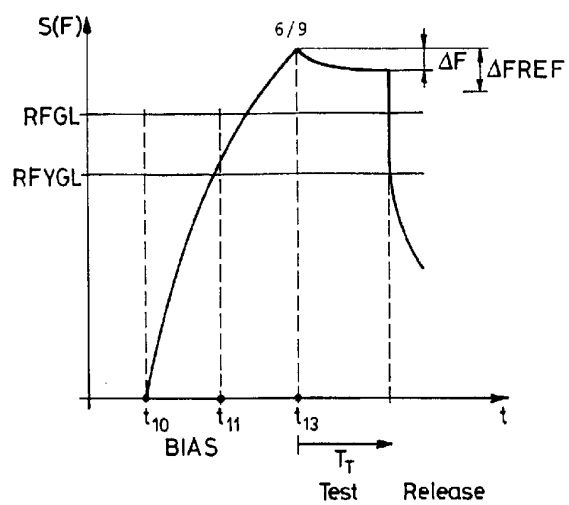


FIG.11c

SUBSTITUTE SHEET (RULE 26)

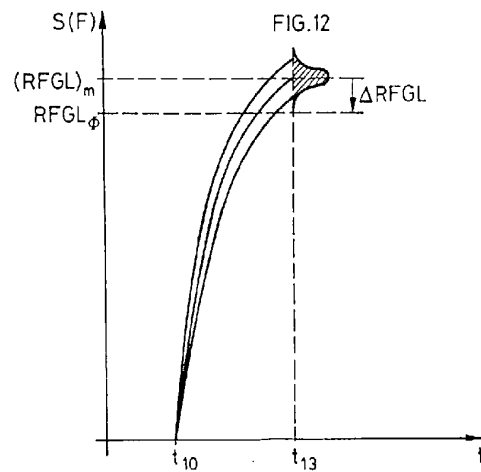
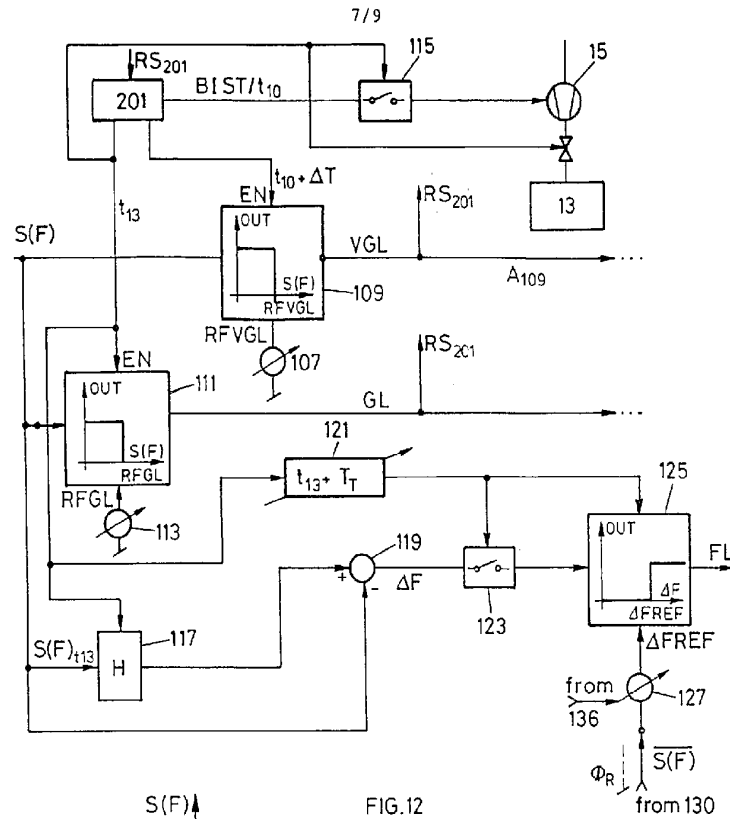


FIG. 13

SUBSTITUTE SHEET (RULE 26)

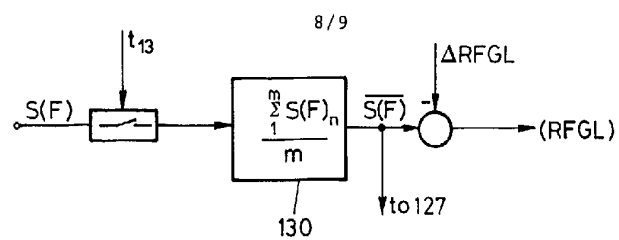


FIG.14

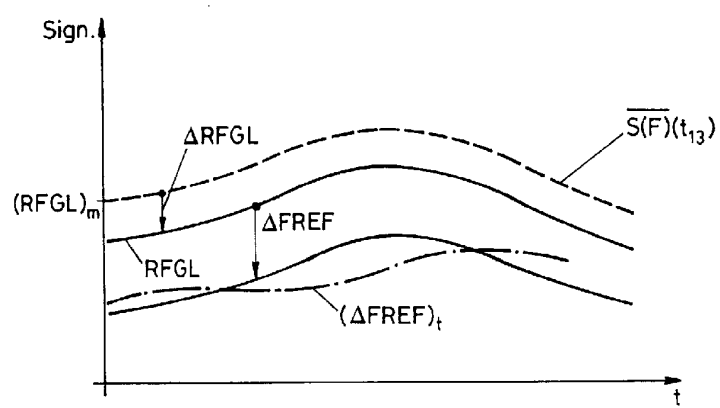


FIG.15

SUBSTITUTE SHEET (RULE 26)

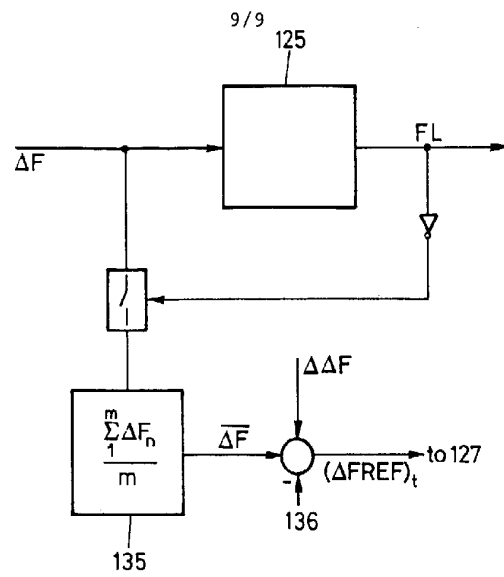


FIG.16

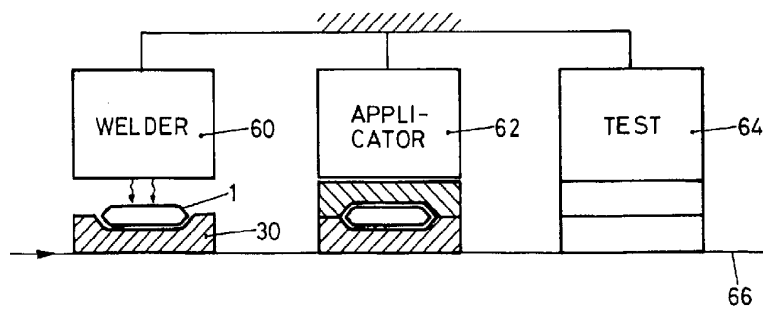


FIG.17

SUBSTITUTE SHEET (RULE 26)