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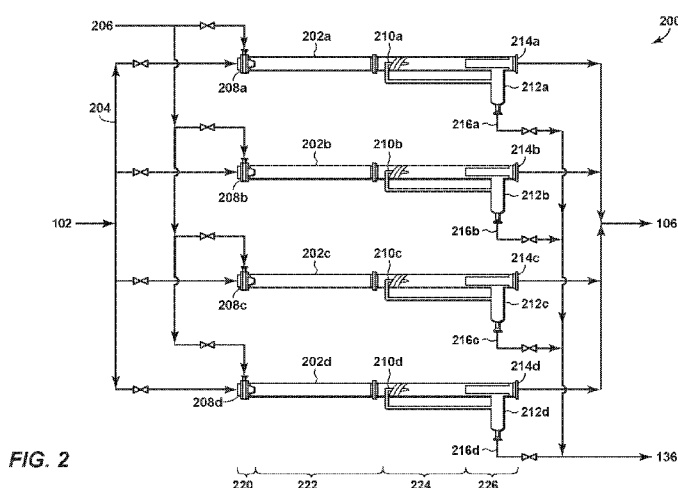
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[Continued on next page]

## (54) Title: INNER SURFACE FEATURES FOR CO-CURRENT CONTACTORS





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## INNER SURFACE FEATURES FOR CO-CURRENT CONTACTORS

### CROSS REFERENCE TO RELATED APPLICATIONS

[0001] This application claims the priority benefit of United States Provisional Patent  
5 Application 62/117,234 filed February 17, 2015 entitled INNER SURFACE FEATURES  
FOR CO-CURRENT CONTACTORS, the entirety of which is incorporated by reference  
herein.

### BACKGROUND

[0002] The production of hydrocarbons from a reservoir oftentimes carries with it the  
10 incidental production of non-hydrocarbon gases. Such gases include contaminants such as  
hydrogen sulfide (H<sub>2</sub>S) and carbon dioxide (CO<sub>2</sub>). When H<sub>2</sub>S or CO<sub>2</sub> are produced as part of  
a hydrocarbon stream (such as methane or ethane), the raw gas stream is sometimes referred  
to as “sour gas.” The H<sub>2</sub>S and CO<sub>2</sub> are often referred to together as “acid gases.”

[0003] In addition to hydrocarbon production streams, acid gases may be associated with  
15 synthesis gas streams, or with refinery gas streams. Acid gases may also be present within  
so-called flash-gas streams in gas processing facilities. Further, acid gases may be generated  
by the combustion of coal, natural gas, or other carbonaceous fuels.

[0004] Gas and/or hydrocarbon fluid streams may contain not only H<sub>2</sub>S or CO<sub>2</sub>, but may  
also contain other “acidic” impurities. These include mercaptans and other trace sulfur  
20 compounds (SO<sub>x</sub>). In addition, natural gas streams may contain water. Indeed, water is the  
most common contaminant in many natural gas streams. Such impurities should be removed  
prior to industrial or residential use.

[0005] Processes have been devised to remove contaminants from a raw natural gas  
stream. In the case of acid gases, cryogenic gas processing is sometimes used, particularly to  
25 remove CO<sub>2</sub> to prevent line freezing and plugged orifices. In other instances, particularly  
with H<sub>2</sub>S removal, the hydrocarbon fluid stream is treated with a solvent. Solvents may  
include chemical solvents such as amines. Examples of amines used in sour gas treatment  
include monoethanol amine (MEA), diethanol amine (DEA), and methyl diethanol amine  
(MDEA).

30 [0006] Physical solvents are sometimes used in lieu of amine solvents. Examples include  
physical solvents currently marketed under the brand names Selexol® (comprising dimethyl  
ethers of polyethylene glycol) and Rectisol™ (comprising methanol). In some instances

hybrid solvents, meaning mixtures of physical and chemical solvents, have been used. An example of one such hybrid solvent is currently marketed under the brand name Sulfinol® (comprising sulfolane, water, and one or more amines). However, the use of amine-based acid gas removal solvents is most common.

5 [0007] Amine-based solvents rely on a chemical reaction with the acid gases. The reaction process is sometimes referred to as “gas sweetening.” Such chemical reactions are generally more effective than the physical-based solvents, particularly at feed gas pressures below about 300 pounds per square inch absolute (psia) (about 20 bar). There are instances where special chemical solvents such as Flexsorb® (comprising hindered amine) are used,  
10 particularly for selectively removing H<sub>2</sub>S from CO<sub>2</sub>-containing gas and/or hydrocarbon fluid streams.

[0008] As a result of the gas sweetening process, a treated or “sweetened” gas stream is created. The sweetened gas stream is substantially depleted of H<sub>2</sub>S and/or CO<sub>2</sub> components. The sweetened gas can be further processed for liquids recovery, that is, by condensing out  
15 heavier hydrocarbon gases. The sweet gas may be sold into a pipeline or may be used for liquefied natural gas (LNG) feed. In addition, the sweetened gas stream may be used as feedstock for a gas-to-liquids process, and then ultimately used to make waxes, butanes, lubricants, glycols and other petroleum-based products. The extracted CO<sub>2</sub> may be sold, or it may be injected into a subterranean reservoir for enhanced oil recovery operations.

20 [0009] When a natural gas stream contains water, a dehydration process is usually undertaken before or after acid gas removal. This is done through the use of glycol or other desiccant in a water separator. The dehydration of natural gas is done to control the formation of gas hydrates and to prevent corrosion in distribution pipelines. The formation of gas hydrates and corrosion in pipelines can cause a decrease in flow volume as well as frozen  
25 control valves, plugged orifices and other operating problems.

[0010] Traditionally, the removal of acid gases or water using chemical solvents or desiccants involves counter-currently contacting the raw natural gas stream with the chemical. The raw gas stream is introduced into the bottom section of a contacting tower. At the same time, the solvent solution is directed into a top section of the tower. The tower has  
30 trays, packing, or other “internals.” As the liquid solvent cascades through the internals, it absorbs the undesirable components, carrying them away through the bottom of the contacting tower as part of a “rich” solvent solution. At the same time, gaseous fluid that is largely depleted of the undesirable components exits at the top of the tower.

[0011] The rich solvent or rich glycol, as the case may be, that exits the contactor is sometimes referred to as an absorbent liquid. Following absorption, a process of regeneration (also called “desorption”) may be employed to separate contaminants from the active solvent of the absorbent liquid. This produces a “lean” solvent or a “lean” glycol that is then typically recycled into the contacting tower for further absorption.

[0012] While perhaps capable of performing desired contacting for removal of contaminants from a gas and/or hydrocarbon-containing fluid stream, historic contactor solutions have had difficulty scaling-up from lab and/or pilot-sized units to units capable of efficiently processing up to a billion standard cubic feet per day (BSFD) of gas. Past scale-up solutions have high capital expenses (e.g., due to having larger and more pieces of equipment, etc.) and high operational expenses (e.g., due to less reliability and/or operability, larger size and weight equipment, etc.). Consequently, a need exists for a contacting solution that is smaller, has fewer pieces of equipment, has improved operability and reliability, and weighs less than traditional contacting equipment.

## 15 SUMMARY OF THE INVENTION

[0013] The disclosure includes a co-current contactor for separating components in a fluid stream, the co-current contactor comprising a first inlet configured to receive the fluid stream proximate to a first end of the co-current contactor, a second inlet configured to receive a solvent proximate the first end of the co-current contactor, and a mass transfer section configured to receive the fluid stream and the solvent and to provide a mixed, two-phase flow, wherein the mass transfer section comprises a surface feature along an inner surface of the mass transfer section configured to reduce film flow along an inner wall of the mass transfer section, and wherein the surface feature comprises at least one of a hydrophobic surface, a superhydrophobic surface, a porous wall surface, and a nonlinear surface irregularity extending radially inward or radially outward along the inner surface of the mass transfer section.

[0014] The disclosure further includes a method of separating components in a co-current contactor, comprising passing a fluid into the co-current contactor, passing a solvent into the co-current contactor, placing the fluid in contact with the solvent to create a combined stream, passing the combined stream through a mass transfer section of the co-current contactor, impeding an amount of liquid from propagating along a wall of the mass transfer section using a surface feature, and separating the fluid from the solvent.

- [0015] The disclosure additionally includes a co-current contacting system for separating a contaminant from an initial gas stream, comprising a gas stream supply, a solvent supply, a first co-current contactor and a second co-current contactor arranged in a counter current configuration, wherein each co-current contactor is configured (i) to receive a gas stream and  
5 a liquid solvent, and (ii) to release a treated gas stream and a separate gas-treating solution, and wherein each of the co-current contactors comprises a first inlet configured to receive the fluid stream proximate to a first end of the co-current contactor, a second inlet configured to receive a solvent proximate the first end of the co-current contactor, and a mass transfer section configured to receive the fluid stream and the solvent and to provide a mixed, two-  
10 phase flow, wherein the mass transfer section comprises a surface feature along an inner surface of the mass transfer section configured to reduce film flow along an inner wall of the mass transfer section, and wherein the surface feature is selected from a group consisting of a hydrophobic surface, a superhydrophobic surface, a raised surface, a recessed surface, and a porous wall surface.
- 15 [0016] It is understood that the methods above may be used to remove a contaminant, e.g., an acid gas component, a water component, etc., from other fluid streams. These separated fluid streams may include, for example, a sour water stream, a flash-gas stream, or a Claus tail gas stream.

#### DESCRIPTION OF THE DRAWINGS

- 20 [0017] So that the manner in which the present invention can be better understood, certain illustrations, charts and/or flow charts are appended hereto. It is to be noted, however, that the drawings illustrate only selected embodiments of the inventions and are therefore not to be considered limiting of scope, for the inventions may admit to other equally effective embodiments and applications.
- 25 [0018] FIG. 1A is a process flow diagram of a gas processing system that includes a co-current flow scheme.
- [0019] FIG. 1B is a process flow diagram of another gas processing system that includes a co-current flow scheme.
- [0020] FIG. 2 is a schematic diagram of a co-current contacting system comprising  
30 multiple co-current contactors.
- [0021] FIG. 3 is a side view of an embodiment of a single stage multiple co-current contactor bundle configuration.

[0022] FIG. 4A is a schematic view of a liquid droplet resting on a hydrophobic surface and a superhydrophobic surface.

[0023] FIG. 4B is a schematic view of a raised surface having an impingement angle relative to a direction of flow of a stream.

5 [0024] FIG. 5 is a schematic diagram of an embodiment of a co-current contactor having a plurality of surface features.

[0025] FIG. 6 is a schematic diagram of another embodiment of a co-current contactor having a plurality of surface features.

#### DETAILED DESCRIPTION

10 [0026] As used herein, the term “co-current contacting device” or “co-current contactor” means an apparatus, e.g., a pipe, a vessel, a housing, an assembly, etc., that receives (i) a stream of gas (or other fluid stream to be treated) and (ii) a separate stream of liquid solvent (or other fluid treating solution) in such a manner that the gas stream and the solvent stream contact one another while flowing in generally the same direction within the contacting  
15 device.

[0027] As used herein, the term “non-absorbing gas” means a gas that is not absorbed by a solvent during a gas treating or conditioning process, e.g., during co-current contacting.

[0028] As used herein, the term “natural gas” refers to a multi-component gas obtained from a crude oil well (associated gas) or from a subterranean gas-bearing formation (non-associated gas). The composition and pressure of natural gas can vary significantly. A  
20 typical natural gas stream contains methane (C<sub>1</sub>) as a significant component. The natural gas stream may also contain ethane (C<sub>2</sub>), higher molecular weight hydrocarbons, one or more acid gases, and water. The natural gas may also contain minor amounts of contaminants such as nitrogen, iron sulfide, and wax.

25 [0029] As used herein, an “acid gas” means any gas that dissolves in water producing an acidic solution. Non-limiting examples of acid gases include hydrogen sulfide (H<sub>2</sub>S), carbon dioxide (CO<sub>2</sub>), sulfur dioxide (SO<sub>2</sub>), carbon disulfide (CS<sub>2</sub>), carbonyl sulfide (COS), mercaptans, or mixtures thereof.

[0030] As used herein, the term “flue gas” means any gas stream generated as a by-product of hydrocarbon combustion.  
30

[0031] As used herein, the term “industrial plant” refers to any plant that generates a gas

stream containing at least one hydrocarbon or an acid gas. One non-limiting example is a coal-powered electrical generation plant. Another example is a cement plant that emits CO<sub>2</sub> at low pressures.

5 [0032] As used herein, the term “liquid solvent” means a fluid in substantially liquid phase that preferentially absorbs one component over another. For example, a liquid solvent may preferentially absorb an acid gas, thereby removing or “scrubbing” at least a portion of the acid gas component from a gas stream or a water stream.

[0033] As used herein, the term “sweetened gas stream” refers to a fluid stream in a substantially gaseous phase that has had at least a portion of acid gas components removed.  
10 Further, the term “sweetened” may also refer to a fluid stream that has been subjected to a dehydration or other conditioning process.

[0034] As used herein, the term “hydrocarbon” refers to an organic compound that includes primarily, if not exclusively, the elements hydrogen and carbon. Hydrocarbons generally fall into two classes: aliphatic, or straight chain hydrocarbons, and cyclic, or closed  
15 ring, hydrocarbons including cyclic terpenes. Examples of hydrocarbon-containing materials include any form of natural gas, oil, coal, and bitumen that can be used as a fuel or upgraded into a fuel.

[0035] As used herein, the term “hydrophobic” means a physical property wherein a surface exhibits a high contact angle (for example, between about 90° and about 150°) at the  
20 interface between the relevant liquid and the surface at standard ambient temperature and pressure and/or at operating temperature and pressure.

[0036] As used herein, the term “superhydrophobic” means a physical property wherein a surface seemingly exhibits a high contact angle (for example, between about 150° and about 179°) at the interface between the relevant liquid and the surface at standard ambient  
25 temperature and pressure and/or at operating temperature and pressure. Alternately or additionally, the term superhydrophobic may mean that only a relatively small portion of the surface area of a drop of liquid is in contact with a surface, e.g., between 0 and about 4%, between 0 and about 3%, between 0 and about 2%, between 0 and about 1%, etc.

[0037] As used herein, the terms “lean” and “rich,” with respect to the absorbent liquid  
30 removal of a selected gas component from a gas stream, are relative, merely implying, respectively, a lesser or greater degree of content of the selected gas component. The respective terms “lean” and “rich” do not necessarily indicate or require, respectively, either



that an absorbent liquid is totally devoid of the selected gaseous component, or that it is incapable of absorbing more of the selected gas component. In fact, it is preferred, as will be evident hereinafter, that the so called “rich” absorbent liquid produced in a first contactor in a series of two or more contactors retains significant or substantial residual absorptive capacity.

5     Conversely, a “lean” absorbent liquid will be understood to be capable of substantial absorption, but may retain a minor concentration of the gas component being removed.

[0038]     With respect to fluid processing equipment, the term “in series” means that two or more devices are placed along a flow line such that a fluid stream undergoing fluid separation moves from one item of equipment to the next while maintaining flow in a substantially constant downstream direction. Similarly, the term “in line” means that two or more  
10     components of a fluid mixing and separating device are connected sequentially or, more preferably, are integrated into a single tubular device.

[0039]     As used herein, the term “fluid” refers to gases, liquids, and combinations of gases and liquids, as well as to combinations of gases and solids, and combinations of liquids and  
15     solids.

#### DESCRIPTION OF SPECIFIC EMBODIMENTS

[0040]     FIG. 1A is a process flow diagram of a gas processing system **100** that includes a co-current flow scheme arranged in a counter current configuration. The gas processing system **100** may be used for the removal of H<sub>2</sub>S or other acid gas components from a gas stream **102**. In addition, in some embodiments, the gas processing system **100** may be used  
20     for the removal of water or other impurities from the gas stream **102**.

[0041]     The gas processing system **100** may employ a number of vertically oriented co-current contacting systems **104A-F**. In some embodiments, each vertically oriented co-current contacting system **104A-F** includes vertically oriented co-current contactor upstream  
25     of a separation system. In other embodiments, each vertically oriented co-current contacting system **104A-F** includes a number of vertically oriented co-current contactors upstream of a single separation system. As would be apparent to those of skill in the art, any or all of the co-current contacting systems **104A-F** may be either vertically oriented or horizontally oriented, depending on the details of the specific implementation, and such alternate  
30     embodiments are within the scope of this disclosure.

[0042]     The gas stream **102** may be a natural gas stream from a hydrocarbon production operation. For example, the gas stream **102** may be a flue gas stream from a power plant, or a

synthesis gas (syn-gas) stream. If the natural gas stream **102** is a syn-gas stream, the gas stream **102** may be cooled and filtered before being introduced into the gas processing system **100**. The gas stream **102** may also be a flash gas stream taken from a flash drum in a gas processing system itself. In addition, the gas stream **102** may be a tail gas stream from a Claus sulfur recovery process or an impurities stream from a regenerator. Furthermore, the gas stream **102** may be an exhaust emission from a cement plant or other industrial plant. In this instance, CO<sub>2</sub> may be absorbed from excess air or from a nitrogen-containing flue gas.

**[0043]** The gas stream **102** may include a non-absorbing gas, such as methane, and one or more impurities, such as an acid gas. For example, the gas stream **102** may include CO<sub>2</sub> or H<sub>2</sub>S. The gas processing system **100** may convert the gas stream **102** into a sweetened gas stream **106** by removing the acid gases.

**[0044]** In operation, the gas stream **102** may be flowed into a first co-current contacting system **104A**, where it is mixed with a solvent stream **108**. If the gas processing system **100** is to be used for the removal of H<sub>2</sub>S, or other sulfur compounds, the solvent stream **108** may include an amine solution, such as monoethanol amine (MEA), diethanol amine (DEA), or methyldiethanol amine (MDEA). Other solvents, such as physical solvents, alkaline salts solutions, or ionic liquids, may also be used for H<sub>2</sub>S removal. In embodiments used for other purposes, such as dehydration or reactions, other solvents or reactants, such as glycols, may be used. The solvent stream **108** may include a lean solvent that has undergone a desorption process for the removal of acid gas impurities. For example, in the gas processing system **100** shown in FIG. 1A, the solvent stream **108** introduced into the first co-current contacting system **104A** includes a semi-lean solvent that is taken from a central portion of a regenerator **110**. A lean solvent stream **112** taken from the regenerator **110** may also be directed into a final co-current contacting system **104F**.

**[0045]** In various embodiments, the gas processing system **100** employs a series of co-current contacting systems **104A-F**. In some embodiments, as shown in FIG. 1A, the co-current contacting systems **104A-F** may be arranged in a counter current configuration. Each co-current contacting system **104A-F** removes a portion of the acid gas content from the natural gas stream **102**, thereby releasing a progressively sweetened natural gas stream in a downstream direction. The final co-current contacting system **104F** provides the final sweetened natural gas stream **106**.

**[0046]** Before entering the first co-current contacting system **104A**, the natural gas stream **102** may pass through an inlet separator **114**. The inlet separator **114** may be used to clean

the natural gas stream **102** by filtering out impurities, such as brine and drilling fluids. Some particle filtration may also take place. The cleaning of the natural gas stream **102** can prevent foaming of solvent during the acid gas treatment process.

[0047] As shown in FIG. 1A, the solvent stream **108** is flowed into the first co-current contacting system **104A**. Movement of the semi-lean solvent stream **108** into the first co-current contacting system **104A** may be aided by a pump **116**. The pump **116** may cause the semi-lean solvent stream **108** to flow into the first co-current contacting system **104A** at a suitable pressure, for example, of about 15 psig to about 1,500 psig.

[0048] Once inside the first co-current contacting system **104A**, the natural gas stream **102** and the solvent stream **108** move along the longitudinal axis of the first co-current contacting system **104A**. As they travel, the solvent stream **108** interacts with the H<sub>2</sub>S, H<sub>2</sub>O, and/or other impurities in the natural gas stream **102**, causing the H<sub>2</sub>S, H<sub>2</sub>O, and/or other impurities to chemically attach to or be absorbed by the amine molecules. A first partially-loaded, or "rich," gas treating solution **118A** may be flowed out of the first co-current contacting system **104A**. In addition, a first partially-sweetened natural gas stream **120A** may be flowed out of the first co-current contacting system **104A** and into a second co-current contacting system **104B**. This general arrangement may be referred to as arranging co-current contactors in a counter current configuration.

[0049] As shown in the example illustrated in FIG. 1A, a third co-current contacting system **104C** may be provided after the second co-current contacting system **104B**, and a fourth co-current contacting system **104D** may be provided after the third co-current contacting system **104C**. In addition, a fifth co-current contacting system **104E** may be provided after the fourth co-current contacting system **104D**, and a final co-current contacting system **104F** may be provided after the fifth co-current contacting system **104E**. Each of the second, third, fourth, and fifth co-current contacting systems **104B**, **104C**, **104D**, and **104E** may generate a respective partially-sweetened natural gas stream **120B**, **120C**, **120D**, and **120E**. In addition, each of the second, third, fourth, fifth, and final co-current contacting systems **104B**, **104C**, **104D**, **104E**, and **104F** may generate respective partially-loaded gas treating solution **118B**, **118C**, **118D**, **118E**, and **118F**. If an amine is used as the solvent stream **108**, the partially-loaded gas treating solutions **118A-F** may include rich amine solutions. In the gas processing system **100**, the second loaded gas treating solution **118B** merges with the rich gas treating solution **118A** and goes through a regeneration process in the regenerator **110**.

[0050] As the progressively-sweetened natural gas streams **120A-E** are generated, the gas pressure in the gas processing system **100** will gradually decrease. As this occurs, the liquid pressure of the progressively-richer gas treating solutions **118A-F** may be correspondingly increased. This may be accomplished by placing one or more booster pumps (not shown) between each co-current contacting system **104A-F** to boost liquid pressure in the gas processing system **100**.

[0051] In the gas processing system **100**, solvent streams may be regenerated by flowing the partially-loaded gas treating solutions **118A** and **118B** through a flash drum **121**. Absorbed natural gas **122** may be flashed from the partially-loaded gas treating solutions **118A** and **118B** within the flash drum **121**, and may be flowed out of the flash drum **121** via an overhead line **124**.

[0052] The resulting rich solvent stream **126** may be flowed from the flash drum **121** to the regenerator **110**. The rich solvent stream **126** may be introduced into the regenerator **110** for desorption. The regenerator **110** may include a stripper portion **128** including trays or other internals (not shown). The stripper portion **128** may be located directly above a heating portion **130**. A heat source **132** may be provided with the heating portion **130** to generate heat. The regenerator **110** produces the regenerated, lean solvent stream **112** that is recycled for re-use in the final co-current contacting system **104F**. Stripped overhead gas from the regenerator **110**, which may include concentrated H<sub>2</sub>S (or CO<sub>2</sub>), may be flowed out of the regenerator **110** as an overhead impurities stream **134**.

[0053] The overhead impurities stream **134** may be flowed into a condenser **135**, which may cool the overhead impurities stream **134**. The resulting cooled impurities stream **138** may be flowed through a reflux accumulator **140**. The reflux accumulator **140** may separate any remaining liquid, such as condensed water, from the impurities stream **138**. This may result in the generation of a substantially pure acid gas stream **142**, which may be flowed out of the reflux accumulator **140** via an overhead line **144**.

[0054] In some embodiments, if the initial natural gas stream **102** includes CO<sub>2</sub>, and a CO<sub>2</sub>-selective solvent stream **108** is used, the acid gas stream **142** includes primarily CO<sub>2</sub>. The CO<sub>2</sub>-rich acid gas stream **142** may be used as part of a miscible EOR operation to recover oil. If the oil reservoir to be flooded does not contain a significant amount of H<sub>2</sub>S or other sulfur compounds, the CO<sub>2</sub> to be used for the EOR operation may not contain significant H<sub>2</sub>S or other sulfur compounds. However, concentrated CO<sub>2</sub> streams from oil and gas production operations may be contaminated with small amounts of H<sub>2</sub>S. Thus, it may be

desirable to remove the H<sub>2</sub>S from the CO<sub>2</sub>, unless the acid gas stream **142** is to be injected purely for geologic sequestration.

[0055] While a gas stream **102** is discussed herein, those of skill in the art will appreciate that generally the same principles may be applied to any fluid stream, including with respect to liquid-liquid contacting. Consequently, use of the phrases “gas stream,” “gas inlet,” “gas outlet,” etc. are to be understood as non-limiting and may optionally be replaced with “fluid stream,” “fluid inlet,” “fluid outlet,” and so forth in various embodiments within the scope of this disclosure. Use of the phrases “gas stream,” “gas inlet,” “gas outlet,” etc. are for the sake of convenience only.

10 [0056] In some embodiments, if the initial natural gas stream **102** includes H<sub>2</sub>S, an H<sub>2</sub>S-selective solvent stream **108** may be used to capture the H<sub>2</sub>S. The H<sub>2</sub>S may then be converted into elemental sulfur using a sulfur recovery unit (not shown). The sulfur recovery unit may be a so-called Claus unit. Those of ordinary skill in the art will understand that a “Claus process” is a process that is sometimes used by the natural gas and refinery industries to recover elemental sulfur from H<sub>2</sub>S-containing gas streams.

[0057] In practice, the “tail gas” from the Claus process, which may include H<sub>2</sub>S, SO<sub>2</sub>, CO<sub>2</sub>, N<sub>2</sub>, and water vapor, can be reacted to convert the SO<sub>2</sub> to H<sub>2</sub>S via hydrogenation. The hydrogenated tail gas stream has a high partial pressure, a large amount of CO<sub>2</sub>, e.g., more than 50%, and a small amount of H<sub>2</sub>S, e.g., a few percent or less. This type of gas stream, which is typically near atmospheric pressure, is amenable to selective H<sub>2</sub>S removal. The recovered H<sub>2</sub>S may be recycled to the front of the Claus unit, or may be sequestered downstream. Alternatively, a direct oxidation of the H<sub>2</sub>S to elemental sulfur may be performed using various processes known in the field of gas separation.

25 [0058] As shown in FIG. 1A, a residual liquid stream **146** may be flowed out of the bottom of the reflux accumulator **140**. The residual liquid stream **146** may be flowed through a reflux pump **148**, which may boost the pressure of the residual liquid stream **146** and pump the residual liquid stream **146** into the regenerator **110**. The residual liquid stream **146** may be flowed out of the regenerator **110**, for example, from the bottom of the heating portion **130** as part of the lean solvent stream **112**. Some water may be added to the lean solvent stream **112** to balance the loss of water vapor to the partially sweetened natural gas streams **120A-E**. This water may be added at an intake or suction of the reflux pump **148**.

30 [0059] The lean solvent stream **112** may be at a low pressure. Accordingly, the lean

solvent stream **112** may be passed through a pressure boosting pump **150**. From the pressure boosting pump **150**, the lean solvent stream **112** may be flowed through a cooler **154**. The cooler **154** may cool the lean solvent stream **112** to ensure that the lean solvent stream **112** will absorb acid gases effectively. The resulting chilled lean solvent stream **156** is then used  
5 as the solvent stream for the final co-current contacting system **104F**.

[0060] In some embodiments, a solvent tank **158** is provided proximate the final co-current contacting system **104F**. The chilled lean solvent stream **156** may be flowed from the solvent tank **158**. In other embodiments, the solvent tank **158** is off-line and provides a reservoir for the lean solvent stream **156**.

10 [0061] The process flow diagram of FIG. 1A is not intended to indicate that the gas processing system **100** is to include all of the components shown in FIG. 1A. Further, any number of additional components may be included within the gas processing system **100**, depending on the details of the specific implementation. For example, the gas processing system **100** may include any suitable types of heaters, chillers, condensers, liquid pumps, gas  
15 compressors, blowers, bypass lines, other types of separation and/or fractionation equipment, valves, switches, controllers, and pressure-measuring devices, temperature-measuring devices, level-measuring devices, or flow-measuring devices, among others.

[0062] FIG. 1B is a process flow diagram of another gas processing system **160** that includes a co-current flow scheme. Like numbered items are as described with respect to  
20 FIG. 1A. Operation of the gas processing system **160** of FIG. 1B is similar to that of the gas processing system **100** of FIG. 1A. However, in the gas processing system **160**, the first co-current contacting system **104A** receives the partially-loaded gas treating solution **118B** from the second co-current contacting system **104B**. Therefore, the gas processing system **160** does not include the semi-lean solvent stream **108**. In this example, the series of co-current  
25 contacting systems **104A-F** acts like a separation column, for example, wherein each stage corresponds to a packed stage.

[0063] Because the partially-loaded gas treating solution **118B** received by the first co-current contacting system **104A** in FIG. 1B has already been processed through the second co-current contacting system **104B**, the partially-loaded gas treating solution **118B** may be  
30 very rich. For this reason, it may be desirable to provide some level of intermediate processing of the partially-loaded gas treating solution **118B**.

[0064] Alternatively, a semi-lean liquid stream could be taken from other sweetening

operations in the gas processing system **160** and used, at least in part, as an amine solution for the first or second co-current contacting system **104A** or **104B**. In this respect, there are situations in which a single type of solvent is used for more than one service in the gas processing system **160**. This is referred to as integrated gas treatment. For example, MDEA  
5 may be used both for high-pressure, H<sub>2</sub>S-selective acid gas removal, as well as in a Claus tail gas treating (TGT) process. The rich amine stream from the TGT process is not heavily loaded with H<sub>2</sub>S and CO<sub>2</sub>, owing to the low pressure of the process. Thus, in some embodiments, the rich amine stream from the TGT process is used as a semi-lean stream for the first or second co-current contacting system **104A** or **104B**. The semi-lean stream (not  
10 shown) may be pumped to a suitable pressure and injected into the first or second co-current contacting system **104A** or **104B**, possibly along with the partially-loaded gas treating solution from the succeeding co-current contacting system.

[0065] Further, in the gas processing system **160** of FIG. 1B, the first partially-loaded treating solution **118A** is flowed through a heat exchanger **162** after being flowed through the  
15 flash drum **121**. Within the heat exchanger **162**, the temperature of the first partially-loaded solvent solution **118A** is increased via heat exchange with the lean solvent **112** taken from the regenerator **110**. This serves to heat the first partially-loaded treating solution **118A** before introduction into the regenerator **110**, while cooling the lean solvent stream **112**.

[0066] The process flow diagram of FIG. 1B is not intended to indicate that the gas processing system **160** is to include all of the components shown in FIG. 1B. Further, any  
20 number of additional components may be included within the gas processing system **160**, depending on the details of the specific implementation.

[0067] FIG. 2 is a schematic diagram of a co-current contacting system **200**, e.g., any one of the co-current contacting systems **104A-F** of FIG. 1. The components of FIG. 2 may be  
25 the substantially the same as the corresponding components of FIG. 1 except as otherwise noted. The co-current contacting system **200** has four contacting units **202a-202d** separately supplied by a header **204** for a natural gas stream **102**. The contacting units **202a-202d** are separately supplied by a header carrying a lean solvent stream **206**, e.g., a semi-lean solvent stream **108** or any of the partially-loaded gas treating solutions **118A-F**, and received  
30 proximate to a first end of each each contacting unit **202a-202d**. Each contacting unit **202a-202d** has an inlet nozzle **208a-208d** (respectively) for atomizing and/or dividing the liquid solvent into a large number of small droplets and introducing the lean solvent stream **206**. Atomizing the lean solvent stream **206** increases the surface area available for contact with

the natural gas stream **102** and decreases the distances required for diffusion of acid gas components in both the vapor and liquid phases. Each contacting unit **202a-202d** has a recycle gas inlet **210a-210d** supplied by gas collected and returned from a seal pot or liquid boot **212a-212d**. As depicted, each recycle gas inlet **210a-210d** may include a swirl vane or equivalent structure to assist in separation. The seal pot or liquid boot **212a-212d** may provide residence time for process control and may seal the contacting units **202a-202d** to prevent gas bypass. Each contacting unit **202a-202d** has a treated gas outlet **214a-214d** and a rich solvent outlet **216a-216d**. The treated gas outlets **214a-214d** are depicted as comprising vortex tube finders, but alternate embodiments are well known in the art. Treated gas exiting the contacting units **202a-202d** via the treated gas outlets **214a-214d** may be combined and passed as the sweetened gas stream **106**, while rich solvent exiting the contacting units **202a-202d** via the rich solvent outlets **216a-216d** may be combined and passed as the rich solvent stream **126**.

[0068] In operation, each contacting unit **202a-202d** receives a natural gas stream **102** at an inlet section **220**, where the inlet nozzles **208a-208d** atomize a lean solvent stream **206** and expose it to the natural gas stream **102**, creating a mixed, two-phase flow or combined stream (not depicted). The mixed, two-phase flow or combined stream passes through a mass transfer section **222** where absorption occurs. The mass transfer section **222** may comprise a tubular body having a substantially empty bore having one or more surface features, e.g., a hydrophobic surface **402** of FIG. 4A, a superhydrophobic surface **404** of FIG. 4A, a raised surface **450** of FIG. 4B, a recessed surface, or any combination thereof, along an inner surface of the mass transfer section **222**. A separation section **224** follows the mass transfer section. In the separation section **224**, entrained liquid droplets are removed from the gas stream, e.g., using a cyclone inducing element, resulting in an at least partially dehydrated and/or decontaminated treated gas stream. In some embodiments, the inlet section **220** and the mass transfer section **222** may collectively be referred to as a contacting section. The length of the contacting section may be determined based on the residence time required to obtain a predetermined decontamination and/or dehydration level for the natural gas stream **102**, e.g., in view of the intended flow rate, pressure drop, etc. The treated gas stream exits the contacting units **202a-202d** through the outlet section **226**. The contacting units **202a-202d** may operate at about 400 psig to about 1,200 psig, or higher. Because the contacting units **202a-202d** must be individually constructed so as to tolerate these pressures, weight and/or footprint increases linearly as the number of contacting units **202a-202d** is increased.



[0069] Co-current contactors are increasingly becoming more compact, both in length and diameter. As this trend increases, it is important to ensure as much solvent as possible reacts in the increasingly shortened mixing and/or mass transfer section. The H<sub>2</sub>S reaction is instantaneous relative to the CO<sub>2</sub> reactions, lowering the residence time, i.e., the contact time between the vapor and liquid phases, will result in less CO<sub>2</sub> being absorbed into the solvent. The design of the co-current contacting systems **104A-F** enhances selective H<sub>2</sub>S removal due to the short contact time inherent in the equipment design. Disclosed herein are techniques for inhibiting or impeding an amount of liquid from propagating along a wall of the mass transfer section using a surface feature. By inhibiting or impeding liquid propagation along a wall of the mass transfer section, a comparatively greater amount of solvent is retained in the interior volume of the mass transfer section and, consequently, remains available for reaction.

[0070] FIG. 3 is a side view of an embodiment of a single stage multiple co-current contactor bundle configuration **300**. The components of FIG. 3 are substantially the same as the corresponding components of FIG. 2 except as otherwise noted. The single stage multiple co-current contactor bundle configuration **300** is generally contained within a vessel **302** which may form a unitary (single and/or common) pressure boundary for the compact contacting occurring therein. The vessel **302** generally contains a single stage bundle of substantially parallel separation units or compact contactors comprising contacting units **202a-202n**, also referred to herein as separation units. Those of skill in the art will understand that the number of contacting units **202a-202n** in the bundle of compact contactors may be optionally selected based on the desired design characteristics, including desired flow rate, separation unit diameter, etc., and could number from anywhere between one to 300 or more units. The use of the letter nomenclature (i.e., 'a', 'b', 'n', etc.) in conjunction with the numerical reference characters is for ease of reference only and is not limiting. For example, those of skill in the art will understand that an illustrated set of contacting units **202a-202n** may, in various embodiments, comprise two, four, five, twenty, or several hundred contacting units. The vessel **302** comprises an inlet tubesheet **304** having inlet nozzles **208a-208n** in the inlet section **220**. The inlet section **220** is configured to receive the natural gas stream **102** in a common inlet plenum through which the natural gas stream **102** may be distributed substantially equally across the contacting units **202a-202n**. The contacting units **202a-202n** may be of a suitable size depending on the design requirements. For example, the contacting units **202a-202n** may have an individual diameter from about 2 inches (in) (about 5 centimeters (cm)) to about 24 in (about 61 cm), or any range there between. The inlet tubesheet **304** is configured to receive the lean solvent stream

**206** and pass the lean solvent stream **206** to the inlet nozzles **208a-208n**, where the lean solvent stream **206** may be atomized. In some embodiments, the lean solvent stream **206** originates from a glycol supply system (not depicted) and the lean solvent stream **206** comprises glycol. The inlet nozzles **208a-208n** may serve to entrain the atomized solvent stream in the natural gas stream **102**, and the mixed stream of atomized solvent and natural gas may be passed to the mass transfer section **222** where absorption occurs. Each contacting unit **202a-202n** has a recycle gas inlet **210a-210n** supplied by recycle gas collected and returned, e.g., from a common boot **316**. The boot **316** may be optionally included in low liquid rate applications to improve liquid rate flow control. As depicted, the boot **316** may have an internal vortex breaker **317** or other appropriate internals. For ease of viewing, the recycle gas supply lines for each of the recycle gas inlets **210a-210n** are not depicted. As will be understood by those of skill in the art, the recycle gas inlets **210a-210n** are optional, and recycle gas may additionally or alternatively be sent downstream in other embodiments. Rich solvent exiting the contacting units **202a-202n** via the rich solvent outlets **306a-306n** may drain into a common liquid degassing section or common contaminated liquid collection plenum **312**. The plenum **312** may provide sufficient residence time for desired degassing, may reduce liquid surges coming with the natural gas stream **102**, and may provide liquid seal to a cyclonic separation occurring in a contacting section of the separation device **202a-202n**. The residence time provided by the plenum **312** can vary from 5 seconds to 5 minutes, depending on the operation of the process, or from 30 seconds to 1 minute in various embodiments. The vessel **302** contains a mist eliminator **314**, e.g., a wire mesh, vane pack plates, baffles, or other internal devices to reduce liquid droplet carry over from degassing gas leaving the liquid phase of rich solvent in the plenum **312**. The mist eliminator **314** may also serve as a momentum breaker for the rich solvent liquid exiting the separation device **202a-202n** to minimize aeration of the liquid. In embodiments installed in offshore facilities or floating facilities or otherwise subject to motion, the mist eliminator **314** may mitigate wave motion effects in the bottom portion of the vessel **302**. Each contacting unit **202a-202n** has a treated gas outlet **214a-214n** and a rich solvent outlet **306a-306n**. The vessel **302** has a vent **318** for expelling degassing gas, e.g., gas degassed from rich solvent collected in the plenum **312** that may be fed upstream or downstream of the multiple co-current contacting unit, depending on the process configuration. The treated gas outlets **214a-214n** couple to an outlet tubesheet **310**. The treated gas exiting the contacting units **202a-202n** via the treated gas outlets **214a-214n** may be referred to as the dehydrated and/or decontaminated natural gas stream **106**. The vessel **302** also contains level control ports **320a** and **320b** for coupling

a level control system (not depicted) and controlling the amount of rich solvent **326**, e.g., a semi-lean solvent stream **108** or any of the partially-loaded gas treating solutions **118A-F**, exiting the boot **316**. Rich solvent **326** exiting the boot **316** may be sent to a regeneration system for treatment or combined with streams in other processes.

5    **[0071]**    FIG. 4A is a schematic view of a liquid droplet **400**, e.g., an atomized liquid droplet from a mixed, two-phase flow or combined stream of FIGS. 2-3, resting on a hydrophobic surface **402** and a superhydrophobic surface **404**. As depicted, the contact angle **406** between the liquid droplet **400** and the hydrophobic surface **402** is between about 90° and about 150° and the contact angle **408** between the liquid droplet **400** and the  
10    superhydrophobic surface **404** is between about 150° and about 179°. While not depicted, the hydrophobic surface **402**, the superhydrophobic surface **404**, or both may comprise a plurality of microstructures to create a heterogeneous texture for contacting the surface area of the liquid droplet **400**, e.g., via the Lotus effect. Those of skill in the art will appreciate that a variety of techniques, e.g., etching, silicon or other coatings, pitting, etc., may be  
15    utilized to obtain a Lotus effect characteristic (e.g., hydrophobicity and/or superhydrophobicity) along a surface, and this disclosure is not limited to any particular technique.

**[0072]**    FIG. 4B is a schematic view of a raised surface **450**, e.g., a surface feature on an inner wall of the mass transfer section **222** of FIGS. 2-3, having an impingement angle **452**,  
20    e.g., an orthogonal (about 90°) or non-orthogonal impingement angle (not about 90°), relative to a direction of flow **454** of a stream, e.g., the mixed, two-phase flow or combined stream of FIG. 2, having a liquid droplet **456**, e.g., a liquid droplet from a mixed, two-phase flow or combined stream of FIG. 2, traveling therewith. While depicted as a linear, raised surface extending into a diameter of a mass transfer section, e.g., the mass transfer section **222** of  
25    FIGS. 2-3, other raised surfaces are suitable for impingement by the liquid droplet **456**, e.g., non-linear, curved, scalloped, ridged, or irregular textures disposed on a parallel, raised, or recessed surface. Some embodiments may alternately or additionally include one or more slots, channels, grooves, fins, rifling, baffles, wall wipers, static mixers, etc. for disaggregating, dispersing, or directing a liquid droplet **456** along or away from a wall, e.g., a  
30    wall of the mass transfer section **222** of FIGS. 2-3, and such features may further include defining edges that function in the same manner as the raised non-orthogonal surface **450**. All such means of and/or structures for impeding an amount of liquid from propagating along a wall, e.g., a wall of the mass transfer section **222**, by disaggregating, dispersing, disposing,

or directing the amount of liquid away from the wall, e.g., a wall of the mass transfer section **222** of FIGS. 2-3, are to be considered within the scope of this embodiment except as otherwise noted. In some embodiments, the raised surface **450** includes structures that are non-orthogonal relative the direction of flow **454**. In some embodiments, extending a surface across the diameter of a mass transfer section may be impractical or may unacceptably reduce one or more performance characteristics of a contactor. Consequently, in some embodiments the raised surface **450** does not extend across the diameter of a mass transfer section, e.g., the mass transfer section **222** of FIGS. 2-3. Some embodiments may comprise a raised surface **450** (orthogonal or non-orthogonal) that extends into between 1% and 90% of the diameter of the mass transfer section, into between 1% and 80% of the diameter of the mass transfer section, into between 1% and 70% of the diameter of the mass transfer section, into between 1% and 60% of the diameter of the mass transfer section, into between 1% and 50% of the diameter of the mass transfer section, into between 1% and 40% of the diameter of the mass transfer section, into between 1% and 30% of the diameter of the mass transfer section, into between 1% and 20% of the diameter of the mass transfer section, into between 1% and 10% of the diameter of the mass transfer section, into between 1% and 5% of the diameter of the mass transfer section, or any ranges therebetween.

[0073] As described above, various embodiments of each of the contacting units **202a-202d** may include one or more surface features, e.g., a hydrophobic surface **402** of FIG. 4A, a superhydrophobic surface **404** of FIG. 4A, a raised surface **450** of FIG. 4B, a recessed surface, or any combination thereof, along an inner wall of the mass transfer section **222** or at least a portion thereof. The surface features on the inner surfaces of the mass transfer sections **222** may comprise a dimpled texture, a sawtooth texture, a sandpaper texture, or other nonlinear surface irregularity extending radially inward or radially outward along the inner surface of the mass transfer section **222**. The surface features may be disposed along the entire length of the inner surfaces of the mass transfer sections **222** or may only be disposed on a lesser portion thereof, e.g., along a bottom portion, at radial and/or axial intervals, etc. The surface features may impeded an amount of liquid from coalescing and propagating along a wall of the mass transfer section **222**, thereby reducing the likelihood of a laminar flow of solvent or “wall flow” along the wall of the mass transfer section **222**. Those of skill in the art will appreciate that this effect may be of particular concern along horizontally disposed surfaces where gravity may facilitate droplet coalescing and/or wall flow.

[0074] FIG. 5 is a schematic diagram of a co-current contactor **500**, e.g., any of the co-current contacting units **202a-202d** of FIGS. 2-3, having a plurality of surface features. The components of FIG. 5 are substantially the same as the corresponding components of FIGS. 2-3 except as otherwise noted. The co-current contactor **500** includes a porous wall surface section **502** in the mass transfer section **222** configured to pass and/or inject a fluid, e.g., the natural gas stream **102**, there through. The flow holes in the porous wall surface section **502** may be symmetrically or asymmetrically disposed and may extend along some or all of a circumference of at least a portion of the mass transfer section **222**. In some embodiments, the flow holes in the porous wall surface section **502** comprise nozzles, patterns, or other features configured to direct the fluid, e.g., the natural gas stream **102**, in a particular direction, e.g., to increase swirl, eddy current flow, etc. As the fluid passes through the flow holes in the porous wall surface section **502**, a turbulent flow may impede an amount of liquid from propagating along a wall of the mass transfer section **222**. The co-current contactor **500** includes a section **504** having a superhydrophobic surface **404** and a section **506** having a dimpled texture and/or surface feature, e.g., a plurality of raised surfaces **450**.

[0075] FIG. 6 is a schematic diagram of a co-current contactor **600**, e.g., any of the co-current contacting units **202a-202d** of FIGS. 2-3, having a plurality of surface features. The components of FIG. 6 are substantially the same as the corresponding components of FIGS. 2-3 except as otherwise noted. The co-current contactor **600** includes a plurality of baffle rings **602** along an inner wall of the mass transfer section **222**. The co-current contactor **600** further includes a plurality of static mixers **604** circumferentially disposed along an inner wall of the mass transfer section **222**. The co-current contactor **600** additionally includes a liquid collection line **606** for collecting liquid along a lower end of the inner wall of the mass transfer section **222** and passing the collected liquid to a seal pot or liquid boot **212**. Other liquid collection mechanisms will be apparent to those of skill in the art and are considered within the scope of this disclosure.

[0076] While it will be apparent that the invention herein described is well calculated to achieve the benefits and advantages set forth above, it will be appreciated that the invention is susceptible to modification, variation and change without departing from the spirit thereof.

## CLAIMS

What is claimed is:

1. A co-current contactor for separating components in a fluid stream, the co-current contactor comprising:
  - 5 a first inlet configured to receive the fluid stream proximate to a first end of the co-current contactor;
  - a second inlet configured to receive a solvent proximate the first end of the co-current contactor; and
  - a mass transfer section configured to receive the fluid stream and the solvent and to  
10 provide a mixed, two-phase flow;
- wherein the mass transfer section comprises a surface feature along an inner surface of the mass transfer section configured to reduce film flow along an inner wall of the mass transfer section, and wherein the surface feature comprises at least one of a hydrophobic surface, a superhydrophobic surface, a porous wall surface, and a nonlinear surface  
15 irregularity extending radially inward or radially outward along the inner surface of the mass transfer section.
2. The co-current contactor of claim 1, wherein the surface feature comprises a hydrophobic surface or a superhydrophobic surface.
3. The co-current contactor of claim 1 or claim 2, wherein the nonlinear surface  
20 irregularity comprises at least one of a curved texture, a scalloped texture, a ridged texture, a dimpled texture, a sawtooth texture, and a sandpaper texture.
4. The co-current contactor of claim 1 or claims 2-3, wherein the surface feature comprises a nonlinear surface irregularity, and wherein the nonlinear surface irregularity has an impingement angle for redirecting a film flow away from the wall.
- 25 5. The co-current contactor of claim 4, wherein the impingement angle is non-orthogonal relative to a direction of flow of the two-phase flow, and wherein the nonlinear surface irregularity does not extend across the diameter of the mass transfer section.
6. The co-current contactor of claim 4, wherein the surface feature comprises a nonlinear surface irregularity, wherein the nonlinear surface irregularity comprises a first raised surface  
30 and a second raised surface, and wherein the impingement angle of the first raised surface is greater than the impingement angle of the second raised surface.

7. The co-current contactor of claim 1 or any of claims 2-6, wherein:
- when the surface feature comprises a recessed surface, the recessed surface is a groove for directing flow along a path that is not parallel to a direction of flow of the two-phase flow;
- 5 when the surface feature comprises a raised non-orthogonal surface, the raised surface is a fin or a channel for directing flow along a path that is not parallel to a direction of flow of the two-phase flow; and
- when the surface feature comprises a porous wall surface, the porous wall surface comprises holes for injecting an injection fluid into a central chamber of the co-current
- 10 contactor.
8. The co-current contactor of claim 1 or any of claims 2-7, wherein the surface feature comprises a superhydrophobic surface, and wherein the surface feature further comprises a nonlinear surface irregularity having a non-orthogonal impingement angle, and wherein the impingement angle is not parallel to the inner surface.
- 15 9. A method of separating components in a co-current contactor, comprising:
- passing a fluid into the co-current contactor;
- passing a solvent into the co-current contactor;
- placing the fluid in contact with the solvent to create a combined stream;
- passing the combined stream through a mass transfer section of the co-current
- 20 contactor;
- impeding an amount of liquid from propagating along a wall of the mass transfer section using a surface feature; and
- separating the fluid from the solvent.
10. The method of claim 9, wherein impeding the amount of liquid from propagating
- 25 along the wall comprises impinging the amount of liquid on a surface such that the amount of liquid is directed radially inward.
11. The method of claim 9 or claim 10, wherein impeding the amount of liquid from propagating along the wall comprises directing the amount of liquid along a path that is not parallel to a direction of flow of the combined stream.
- 30 12. The method of claim 9 or any of claims 10-11, wherein impeding the amount of liquid

from propagating along the wall comprises reducing the surface area of the amount of liquid contacting the wall.

13. The method of claim 12, further comprising impinging the liquid on a raised wall surface extending radially inward.

5 14. The method of claim 9 or any of claims 10-13, wherein impeding the amount of liquid from propagating along the wall comprises injecting an injection fluid along at least a portion of the wall such that the amount of liquid is directed radially inward.

15. A co-current contacting system for separating a contaminant from an initial gas stream, comprising:

10 a gas stream supply;

a solvent supply;

a first co-current contactor and a second co-current contactor arranged in a counter current configuration, wherein each co-current contactor is configured (i) to receive a gas stream and a liquid solvent, and (ii) to release a treated gas stream and a separate gas-treating  
15 solution; and

wherein each of the co-current contactors comprises the elements of claim 1.

16. The co-current contacting system of claim 15, wherein:

when the surface feature comprises a recessed surface, the recessed surface is a groove for directing flow along a path that is not parallel to a direction of flow of the two-  
20 phase flow; and

when the surface feature comprises a raised non-orthogonal surface, the raised non-orthogonal surface extends radially towards a center of flow of the two-phase flow, wherein the raised non-orthogonal surface comprises a two-phase flow impingement surface having a non-orthogonal impingement angle relative to a direction of flow of the two-phase  
25 flow.

17. The co-current contacting system of claim 15 or claim 16, wherein at least a portion of the surface feature is hydrophobic.

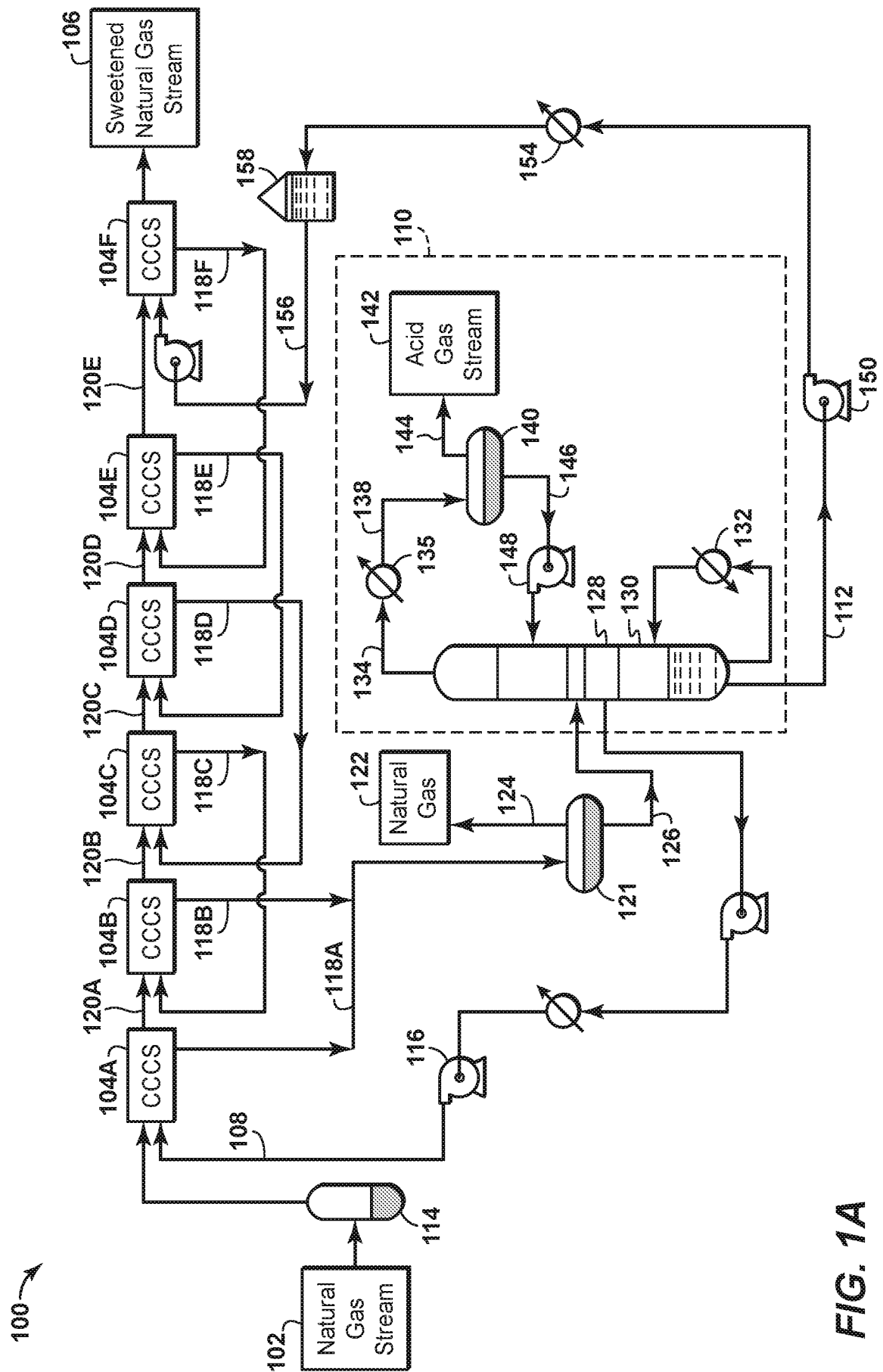
18. The co-current contacting system of claim 15 or any of claims 16-17, wherein at least a portion of the surface feature is superhydrophobic.

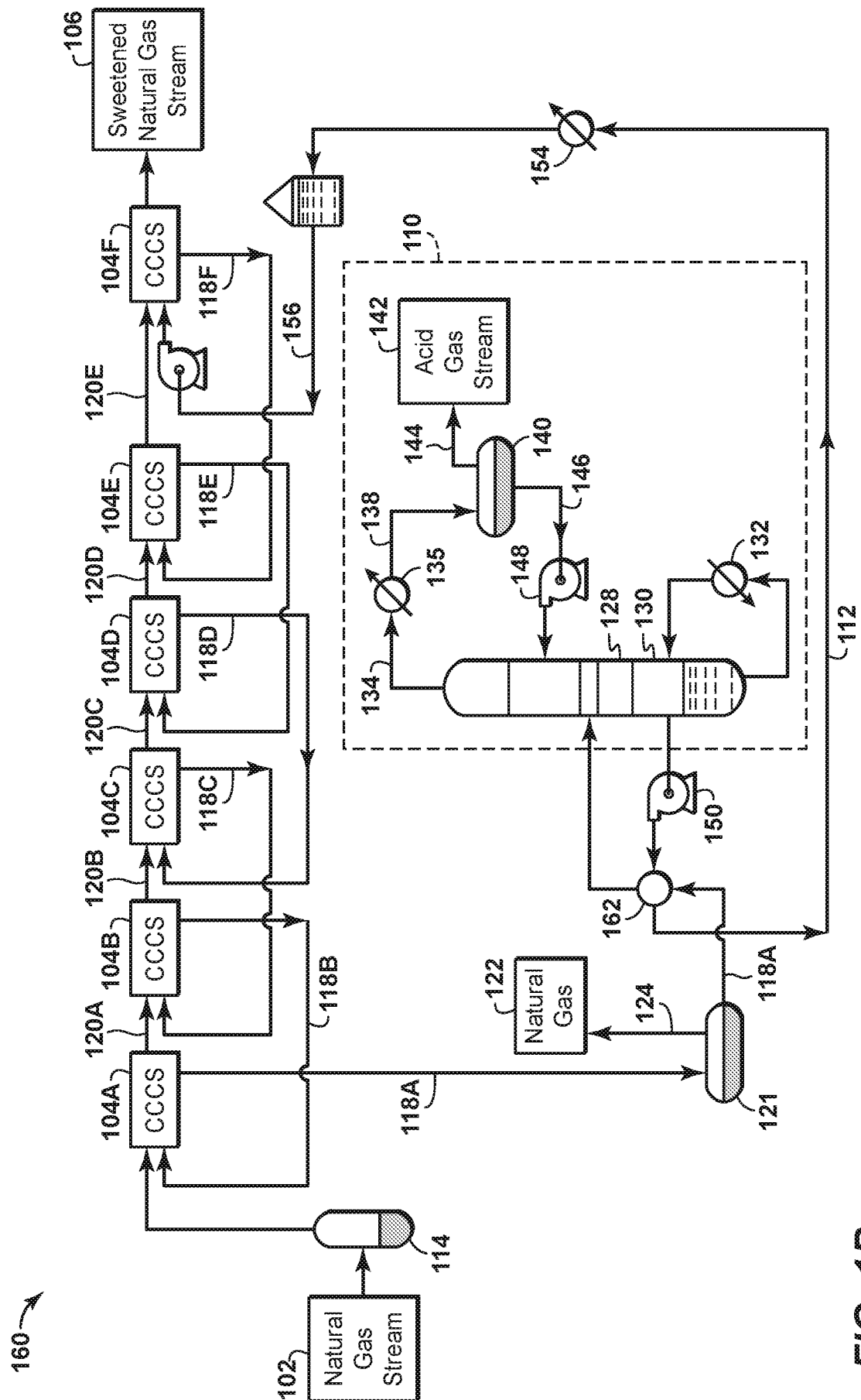
30 19. The co-current contacting system of claim 15 or any of claims 16-18, wherein at least



a portion of the wall of the mass transfer section is hydrophobic.

20. The co-current contacting system of claim 15 or any of claims 16-19, wherein at least a portion of the wall of the mass transfer section is superhydrophobic.





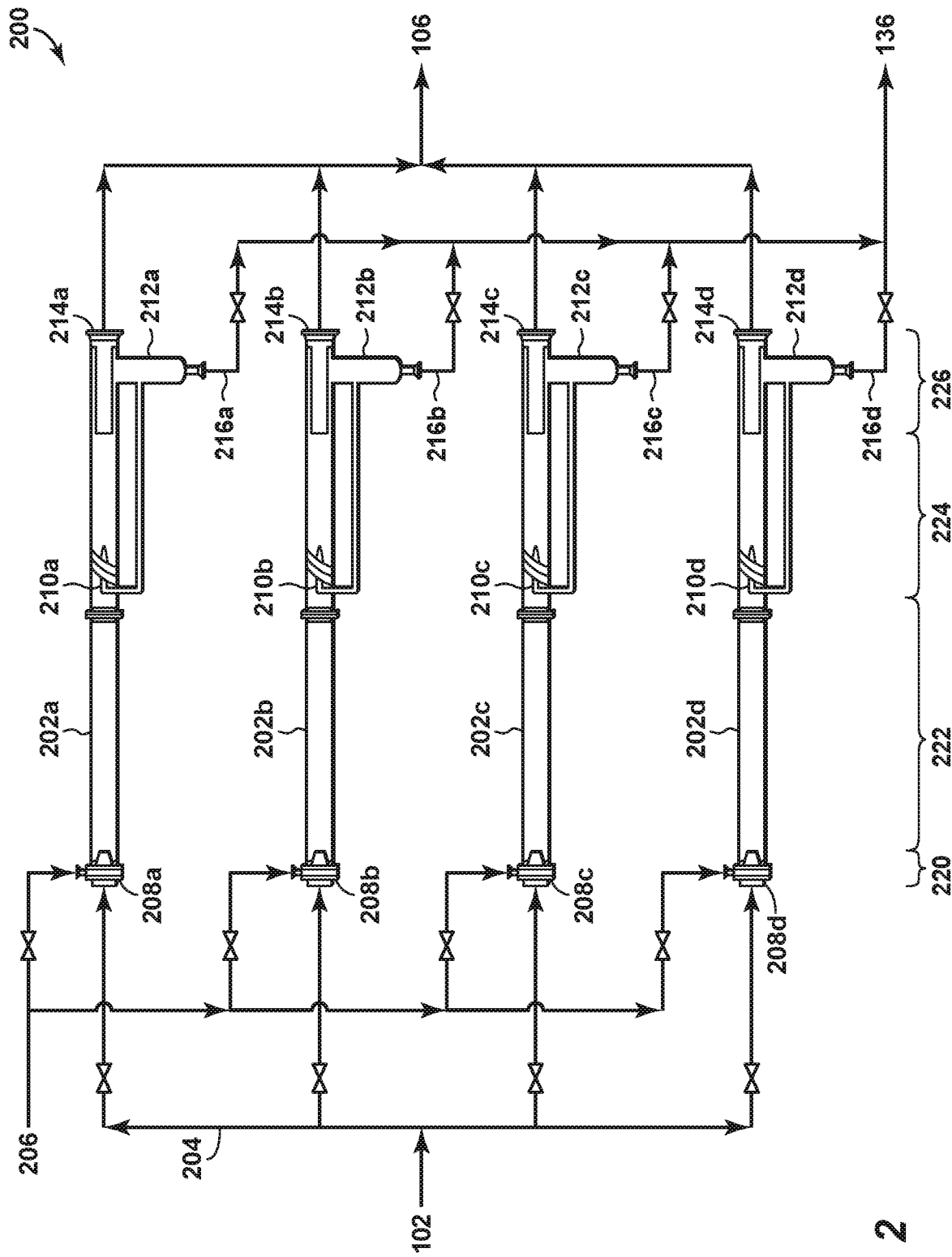


FIG. 2

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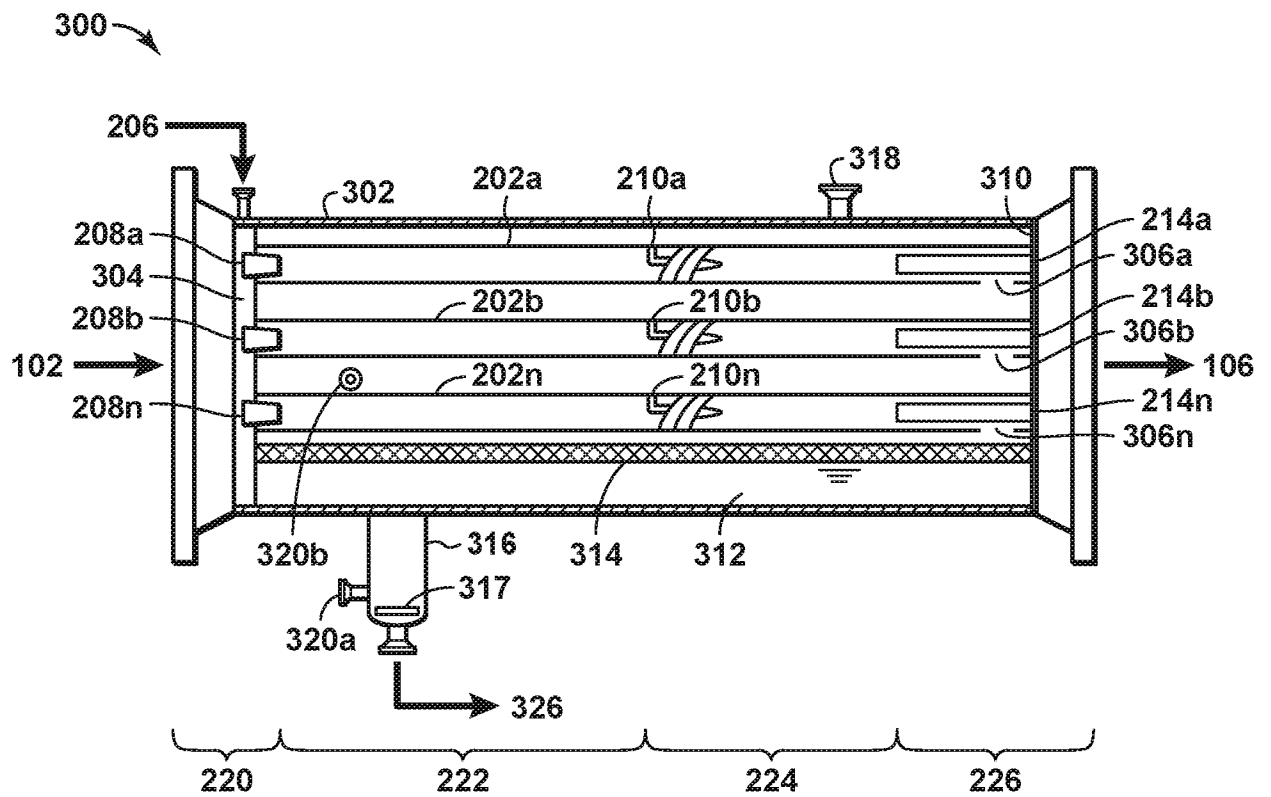


FIG. 3

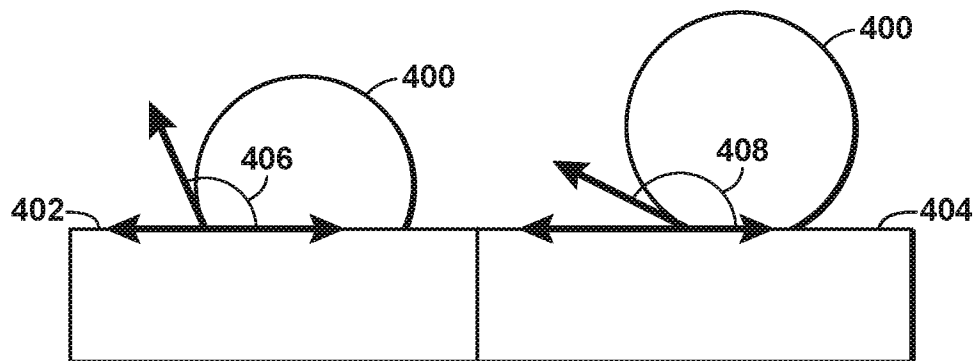


FIG. 4A

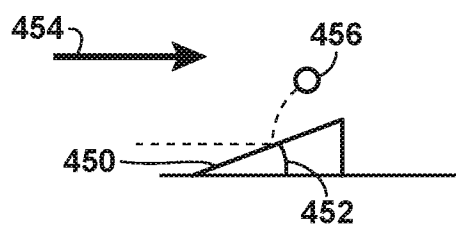


FIG. 4B

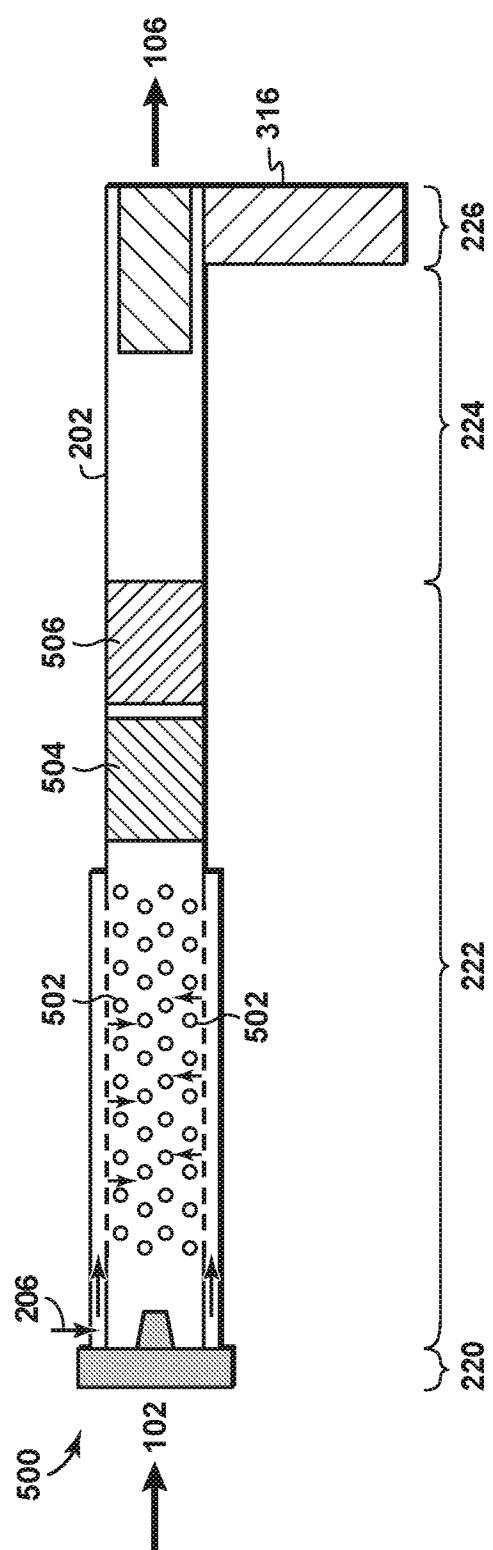


FIG. 5

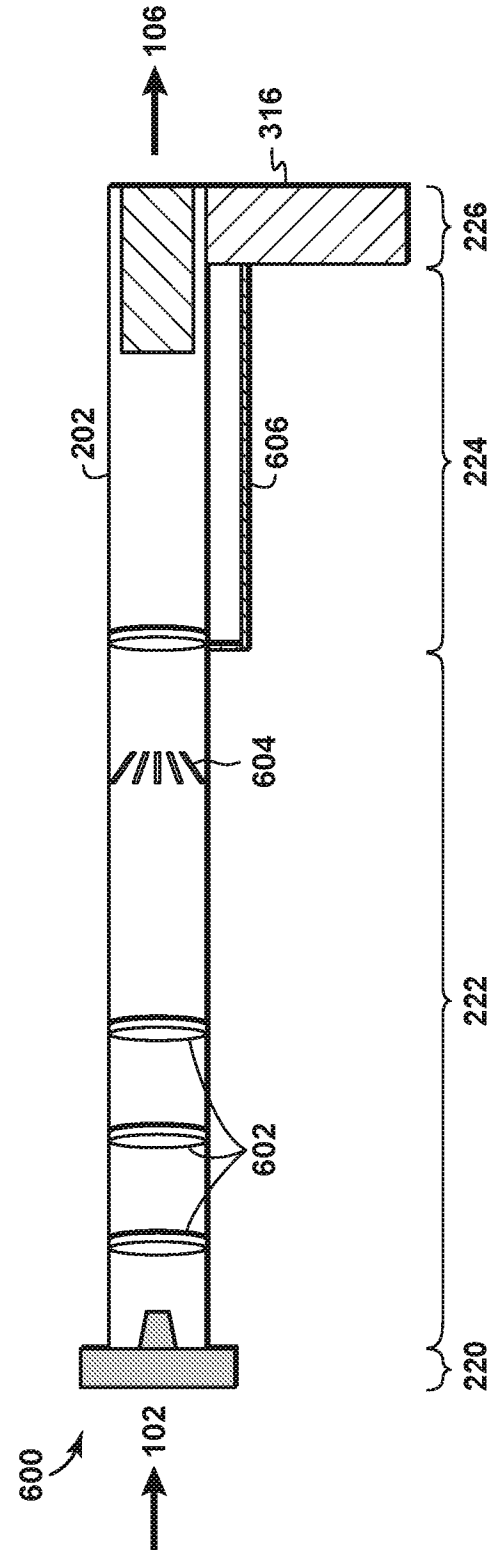


FIG. 6

## INTERNATIONAL SEARCH REPORT

International application No  
PCT/US2016/014513

A. CLASSIFICATION OF SUBJECT MATTER  
INV. B01D53/14 B01D53/18 C10L3/10  
ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
B01D B01F C10L

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal, WPI Data

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
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X	WO 02/32536 A1 (PROSCON SYSTEMS LTD [IE]; LE BLANC RON [IE]; LICHT STEVE [US]) 25 April 2002 (2002-04-25) figures 1-4,7,10	1-14
X	US 2011/296869 A1 (BUHRMAN FREDERIK ARNOLD [PH] ET AL) 8 December 2011 (2011-12-08) figures 1,2,4,5	1-20
X	US 4 603 035 A (CONNELL DAVID E [US] ET AL) 29 July 1986 (1986-07-29) figures 1-4	1-14
	-/-	



Further documents are listed in the continuation of Box C.



See patent family annex.

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"&" document member of the same patent family

Date of the actual completion of the international search

22 April 2016

Date of mailing of the international search report

04/05/2016

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## INTERNATIONAL SEARCH REPORT

International application No

PCT/US2016/014513

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

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Y	EP 1 340 536 A2 (RAUSCHERT VERFAHRENSTECHNIK GM [DE]) 3 September 2003 (2003-09-03) claims 1-3 -----	1-20
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