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- (73) Patenthaver: **DAIKIN INDUSTRIES, LTD., Osaka Umeda Twin Towers South, 1-13-1 , Umeda, Kita-ku, Osaka-Shi, Osaka 530-0001, Japan**
- (72) Opfinder: **SATOU Kiichirou, c/o DAIKIN INDUSTRIES, LTD., Umeda Center , Building, 4-12, Nakazaki-Nishi 2-chome, Kita-ku, Osaka-shi, Osaka 530-8323, Japan**
NAKANO Masataka, c/o DAIKIN INDUSTRIES, LTD., Umeda Center , Building, 4-12, Nakazaki-Nishi 2-chome, Kita-ku, Osaka-shi, Osaka 530-8323, Japan
- (74) Fuldmægtig i Danmark: **Dennemeyer & Associates S.A, P.O. Box 700425, DE-81304 Munich, Tyskland**
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US-A1- 2017 268 811

DESCRIPTION

TECHNICAL FIELD

[0001] The present disclosure relates to a refrigerant leakage determination device, a refrigeration apparatus including the refrigerant leakage determination device, and a method for determining refrigerant leakage.

BACKGROUND ART

[0002] A typical air conditioner includes a refrigeration cycle in which an outdoor unit including a compressor is connected to an indoor unit by a refrigerant pipe. The air conditioner has a configuration that determines whether a refrigerant has leaked (refer to, for example, Patent Document 1). In such an air conditioner, whether the refrigerant has leaked is determined by comparing an outside temperature when the compressor is activated at an initial stage after installation of the air conditioner, a discharge side temperature of the compressor when the air conditioner is operated under a predetermined condition, an outside temperature when the compressor is activated later, and a discharge side temperature of the compressor when the air conditioner is operated in the same predetermined condition.

[0003] Patent Document 2 describes an abnormality diagnosis system performing diagnosis of abnormality in an air conditioning device. A first deriving portion derives a derived value on the basis of a state value relating to a state of the air conditioning device in diagnosis. A second deriving portion derives a normal value on the basis of the state value in a normal operation of the air conditioning device. An abnormality diagnosing portion performs examination by statistical processing to the derived value and the normal value, and diagnoses that the air conditioning device is in an abnormal state when significant difference is found between the derived value and the normal value.

Patent Document 3 describes a refrigeration cycle apparatus including a control unit that detects abnormality of a refrigeration cycle based on the pressure or temperature of the refrigeration cycle in an off time of the refrigeration cycle. The abnormality can be refrigerant leakage

Patent Document 4 describes a refrigerating and air-conditioning apparatus capable of calculating the internal volume of a refrigerant extension pipe using operation data obtained during normal operation, and calculating the total amount of refrigerant in a refrigerant circuit and detecting leakage of refrigerant with high accuracy.

[0004] Patent Document 5 describes detecting a leakage of a refrigerant by analysing the discharged refrigerant temperature of a compressor (see paragraphs [0048]-[0052] of Patent Document 5).

[0005] Patent Document 6 describes detecting abnormality in a blower including a propeller fan, and to prevent breakage of the blower (see paragraphs [0046]-[0049] of Patent Document 6).

[0006] Patent Document 7 describes detecting degradation of an air conditioner by detecting abnormality before fails and stops.

[0007] Patent Document 8 describes recognizing abnormality/normality of an appliance capable of not being recognized when setting an absolute threshold value.

[0008] Patent Document 9 describes regulation of a detected voltage of a supply voltage detecting circuit in an inverter air conditioner.

PRIOR ART DOCUMENT

PATENT DOCUMENT

[0009]

Patent Document 1: JP 2013-204871 A

Patent Document 2: JP 2009-002650 A

Patent Document 3: US 2017/268811 A1

Patent Document 4: EP 2 546 588 A1

Patent Document 5: JP 2016-090177 A

Patent Document 6: JP 2015-222151 A

Patent Document 7: JP 2003-161495 A

Patent Document 8: JP 2006-064307 A

Patent Document 9: JP H07-217973 A

SUMMARY OF THE INVENTION

Problems that the Invention is to Solve

[0010] In the typical air conditioner, to determine whether the refrigerant has leaked, the operation condition of the air conditioner at the initial stage after installation of the air conditioner needs to conform to a later operation condition of the air conditioner. Therefore, a special operation for determining whether the refrigerant has leaked needs to be performed. In this configuration, the air conditioner cannot perform a normal operation while determining whether the refrigerant has leaked. This drawback is not limited to an air conditioner and also occurs in any refrigeration apparatus including a refrigerant circuit.

[0011] It is an object of the present invention to provide a refrigerant leakage determination device, a refrigeration apparatus including the refrigerant leakage determination device, and a method for determining refrigerant leakage that dispense with a special operation for determining whether the refrigerant has leaked.

Means for Solving the Problems

[0012] This object is accomplished by the refrigerant leakage determination device and the refrigerant leakage determination method defined in the independent claims. The dependent claims concern particular embodiments.

[0013] With this configuration, the deviation degree of the refrigerant circuit from the normal state is calculated based on the deviation degree between the first index value and the second index value that are calculated using data related to operation of the refrigeration apparatus including operation of the refrigeration apparatus in the pre-trip inspection and normal operations of the refrigeration apparatus. This allows for the determination of whether the refrigerant has leaked or the estimation of a refrigerant leakage occurrence time. The data related to operation of the refrigeration apparatus is obtained from, for example, operations including normal operations of the refrigeration apparatus and a pre-trip inspection operation of the refrigeration apparatus. Thus, the determination of whether the refrigerant has leaked or the estimation of a refrigerant leakage occurrence time is performed without performing a special operation for determining whether the refrigerant has leaked.

BRIEF DESCRIPTION OF THE DRAWINGS

[0014]

Fig. 1 is a conceptual diagram showing the present embodiment of a refrigeration apparatus.

Fig. 2 is a block diagram showing electrical configurations of the refrigeration apparatus.

Fig. 3 is a block diagram showing electrical configurations of a refrigerant leakage determination device for the refrigeration apparatus.

Fig. 4A is a graph showing an example of changes in a discharge side refrigerant temperature ratio of the refrigeration apparatus, and Fig. 4B is a graph showing an example of changes in a deviation degree of a first index value from a second index value.

Fig. 5 is a flowchart showing an example of procedures of a refrigerant leakage determination process executed by the refrigerant leakage determination device.

Fig. 6 is a conceptual diagram showing a modified example of a refrigeration apparatus.

MODES FOR CARRYING OUT THE INVENTION

[0015] A transporting refrigeration apparatus, which is an example of a refrigeration apparatus (hereafter, simply referred to as "refrigeration apparatus 1"), will be described below with reference to the drawings. The refrigeration apparatus 1 is configured to refrigerate the inside of storage, for example, a shipping container or a road transportation trailer container. The inside of a casing of the refrigeration apparatus 1 is divided into an interior accommodation space that circulates the air in the storage and an exterior accommodation space that circulates the air outside the storage.

[0016] As shown in Fig. 1, the refrigeration apparatus 1 includes a refrigerant circuit 20 in which, for example, a compressor 11, a condenser 12, and an evaporator 13 are connected by a refrigerant pipe. The refrigerant circuit 20 includes a main circuit 21, a hot gas bypass circuit 22, and a liquid refrigerant bypass circuit 31.

[0017] In the main circuit 21, the compressor 11 that is motor-driven, the condenser 12, a first expansion valve 14A that is an example of a decompression device, and the evaporator 13 are sequentially connected in series by the refrigerant pipe.

[0018] As shown in Fig. 1, the exterior accommodation space accommodates the compressor 11, the condenser 12, the first expansion valve 14A, and an exterior fan 15 that circulates the air outside the storage to the condenser 12. The interior accommodation space accommodates the evaporator 13 and an interior fan 16 that circulates the air in the storage to the evaporator 13.

[0019] The compressor 11 may be, for example, a rotary compressor or a scroll compressor. The compressor 11 is configured so that the operating capacity is variable when an inverter controls the operating frequency to control the rotational speed.

[0020] The condenser 12 and the evaporator 13 may be a fin-and-tube heat exchanger. The condenser 12 exchanges heat between the air outside the storage supplied by the exterior fan 15 and the refrigerant circulating in the condenser 12. The evaporator 13 exchanges heat between the air in the storage supplied by the interior fan 16 and the refrigerant circulating in

the evaporator 13. An example of the exterior fan 15 and the interior fan 16 is a propeller fan. A drain pan 28 is disposed below the evaporator 13. The drain pan 28 collects, for example, frost and ice blocks falling from the evaporator 13 and water condensed from the air.

[0021] The first expansion valve 14A may be, for example, an electric expansion valve having an opening degree that is variable using a pulse motor.

[0022] The compressor 11 and the condenser 12 are connected by a high pressure gas pipe 23 that includes a first opening-closing valve 17A and a check valve 18 sequentially arranged in a direction in which the refrigerant flows. The first opening-closing valve 17A may be, for example, an electric expansion valve having an opening degree that is variable using a pulse motor. The check valve 18 allows the refrigerant to flow in the directions of the arrows shown in Fig. 1.

[0023] The condenser 12 and the first expansion valve 14A are connected by a high pressure liquid pipe 24 that includes a receiver 29, a second opening-closing valve 17B, a dryer 30, and a supercooling heat exchanger 27 sequentially arranged in the direction in which the refrigerant flows. The second opening-closing valve 17B may be, for example, an electromagnetic valve capable of opening and closing.

[0024] The supercooling heat exchanger 27 includes a primary passage 27a and a secondary passage 27b configured to exchange heat with each other. The primary passage 27a is disposed in the main circuit 21 between the dryer 30 and the first expansion valve 14A. The secondary passage 27b is disposed in the liquid refrigerant bypass circuit 31. The liquid refrigerant bypass circuit 31 is a bypass circuit that connects the high pressure liquid pipe 24 and an intermediate-pressure portion (not shown) of a compression mechanism of the compressor 11. A third opening-closing valve 17C and a second expansion valve 14B, which is an example of a metering device, are sequentially connected in the direction in which the high pressure liquid refrigerant flows to the liquid refrigerant bypass circuit 31 between the high pressure liquid pipe 24 and the secondary passage 27b. In this configuration, when the liquid refrigerant flows into the liquid refrigerant bypass circuit 31 from the high pressure liquid pipe 24, the second expansion valve 14B expands the liquid refrigerant to an intermediate pressure, so that the liquid refrigerant has a lower temperature than the liquid refrigerant flowing through the high pressure liquid pipe 24 and flows to the secondary passage 27b. Thus, the high pressure liquid refrigerant flowing through the primary passage 27a is supercooled by the refrigerant flowing through the secondary passage 27b. The third opening-closing valve 17C may be, for example, an electromagnetic valve capable of opening and closing. The second expansion valve 14B may be, for example, an electric expansion valve having an opening degree that can be varied using a pulse motor.

[0025] The hot gas bypass circuit 22 connects the high pressure gas pipe 23 and the inlet side of the evaporator 13 and sends the high-pressure high-temperature gas refrigerant discharged from the compressor 11 to the inlet side of the evaporator 13. The hot gas bypass circuit 22 includes a main passage 32, and a first branch passage 33 and a second branch passage 34

divided from the main passage 32. The first branch passage 33 and the second branch passage 34 are configured to be a parallel circuit in which one end of each of the first branch passage 33 and the second branch passage 34 is connected to the main passage 32 and the other end is connected to the inlet side of the evaporator 13, that is, a low pressure connection pipe 25 that extends between the first expansion valve 14A and the evaporator 13. The main passage 32 includes a fourth opening-closing valve 17D. The fourth opening-closing valve 17D may be, for example, an electromagnetic valve capable of opening and closing. The first branch passage 33 includes only a pipe. The second branch passage 34 includes a drain pan heater 35. The drain pan heater 35 is disposed at the bottom of the drain pan 28 to heat the drain pan 28 with the refrigerant having a high temperature.

[0026] The refrigeration apparatus 1 includes various sensors. In an example, as shown in Figs. 1 and 2, the refrigeration apparatus 1 includes a discharge temperature sensor 41, a discharge pressure sensor 42, an intake temperature sensor 43, an intake pressure sensor 44, a current sensor 45, a rotation sensor 46, a condensation temperature sensor 47, and an evaporation temperature sensor 48. The sensors 41 to 48 may be, for example, known sensors.

[0027] The discharge temperature sensor 41 and the discharge pressure sensor 42 are arranged, for example, on the high pressure gas pipe 23 in the vicinity of a discharge port of the compressor 11. The discharge temperature sensor 41 outputs a signal corresponding to the temperature of a discharge gas refrigerant discharged from the compressor 11. The discharge pressure sensor 42 outputs a signal corresponding to the pressure of the discharge gas refrigerant discharged from the compressor 11. The intake temperature sensor 43 and the intake pressure sensor 44 are arranged, for example, on an intake pipe of the compressor 11, namely, a low pressure gas pipe 26 in the vicinity of the intake port of the compressor 11. The intake temperature sensor 43 outputs a signal corresponding to the temperature of an intake gas refrigerant drawn into the compressor 11. The intake pressure sensor 44 outputs a signal corresponding to the pressure of the intake gas refrigerant drawn into the compressor 11. The current sensor 45 is arranged, for example, on an inverter circuit that drives the motor of the compressor 11. The current sensor 45 outputs a signal corresponding to the amount of current flowing to the inverter circuit. The rotation sensor 46 is arranged, for example, on the motor of the compressor 11. The rotation sensor 46 outputs a signal corresponding to the rotational speed of the motor.

[0028] The condensation temperature sensor 47 is arranged, for example, on the condenser 12 and outputs a signal corresponding to the condensation temperature of the refrigerant flowing through the condenser 12. In the present embodiment, the condensation temperature sensor 47 is attached to, for example, an intermediate portion of the condenser 12. In this case, the condensation temperature sensor 47 obtains the temperature of the refrigerant in the intermediate portion of the condenser 12 as the condensation temperature and outputs a signal corresponding to the condensation temperature. The attachment position of the condensation temperature sensor 47 to the condenser 12 may be changed in any manner.

[0029] The evaporation temperature sensor 48 is arranged, for example, on the evaporator 13 and outputs a signal corresponding to the evaporation temperature of the refrigerant flowing through the evaporator 13. In the present embodiment, the evaporation temperature sensor 48 is attached to, for example, an intermediate portion of the evaporator 13. In this case, the evaporation temperature sensor 48 obtains the temperature of the refrigerant in the intermediate portion of the evaporator 13 as the evaporation temperature and outputs a signal corresponding to the evaporation temperature. The attachment position of the evaporation temperature sensor 48 to the evaporator 13 may be changed in any manner.

[0030] As shown in Fig. 2, the refrigeration apparatus 1 includes a notification unit 52 and a control device 50 that controls operation of the refrigeration apparatus 1. The control device 50 is electrically connected to each of the discharge temperature sensor 41, the discharge pressure sensor 42, the intake temperature sensor 43, the intake pressure sensor 44, the current sensor 45, the rotation sensor 46, the condensation temperature sensor 47, and the evaporation temperature sensor 48. The control device 50 is also electrically connected to the compressor 11, the first expansion valve 14A, the second expansion valve 14B, the exterior fan 15, the interior fan 16, the first opening-closing valve 17A, the second opening-closing valve 17B, the third opening-closing valve 17C, the fourth opening-closing valve 17D, and the notification unit 52. The notification unit 52 notifies information related to the refrigeration apparatus 1 to the outside of the refrigeration apparatus 1. The notification unit 52 includes, for example, a display 53 that shows information related to the refrigeration apparatus 1. The notification unit 52 may include a speaker instead of or in addition to the display 53. In this case, the notification unit 52 may issue notification of information related to the refrigeration apparatus 1 with sound.

[0031] The control device 50 includes a controller 51. The controller 51 includes, for example, an arithmetic unit that executes a predetermined control program and a storage unit. The arithmetic unit includes, for example, a central processing unit (CPU) or a micro processing unit (MPU). The storage unit stores various control programs and information used for various control processes. The storage unit includes, for example, nonvolatile memory and volatile memory. The controller 51 controls the compressor 11, the expansion valves 14A and 14B, the exterior fan 15, the interior fan 16, and the opening-closing valves 17A to 17D based on detection results of the sensors 41 to 48. The refrigeration apparatus 1 performs a refrigerating-cooling operation and a defrosting operation using the controller 51.

Refrigerating-Cooling Operation

[0032] In the refrigerating-cooling operation, the first opening-closing valve 17A, the second opening-closing valve 17B, and the third opening-closing valve 17C are open, and the fourth opening-closing valve 17D is closed. The opening degree of each of the first expansion valve 14A and the second expansion valve 14B is appropriately adjusted. Also, the compressor 11, the exterior fan 15, and the interior fan 16 are operated.

[0033] During the refrigerating-cooling operation, the refrigerant circulates as indicated by the solid arrows shown in Fig. 1. More specifically, a high-pressure gas refrigerant compressed in the compressor 11 is condensed to become a liquid refrigerant in the condenser 12 and then is stored in the receiver 29. The liquid refrigerant stored in the receiver 29 flows through the second opening-closing valve 17B and the dryer 30. The liquid refrigerant is supercooled to become a supercooled liquid refrigerant in the primary passage 27a of the supercooling heat exchanger 27 and flows to the first expansion valve 14A. As indicated by the wave arrows shown in Fig. 1, some of the liquid refrigerant discharged from the receiver 29 flows as a supercooling source through the third opening-closing valve 17C and the second expansion valve 14B to become an intermediate-pressure refrigerant. The intermediate-pressure refrigerant flows to the secondary passage 27b of the supercooling heat exchanger 27 to cool the liquid refrigerant in the primary passage 27a. The liquid refrigerant supercooled in the supercooling heat exchanger 27 is decompressed in the first expansion valve 14A and then flows to the evaporator 13. In the evaporator 13, a low-pressure liquid refrigerant absorbs heat from the air in the storage and evaporates. As a result, the air in the storage is cooled. The low-pressure gas refrigerant evaporated in the evaporator 13 is drawn into the compressor 11 and compressed again.

Defrosting Operation

[0034] When the refrigerating-cooling operation is continuously performed, frost collects on a surface of, for example, a heat transfer tube of the evaporator 13. The frost gradually develops and enlarges. The controller 51 performs the defrosting operation, that is, an operation for defrosting the evaporator 13.

[0035] As indicated by the broken arrows shown in Fig. 1, the defrosting operation allows a high-temperature high-pressure gas refrigerant that is compressed in the compressor 11 to flow to the inlet side of the evaporator 13 through a bypass to defrost the evaporator 13. In the defrosting operation, the fourth opening-closing valve 17D is open, and the first opening-closing valve 17A, the second opening-closing valve 17B, the third opening-closing valve 17C, and the second expansion valve 14B are fully closed. While the compressor 11 is operated, the exterior fan 15 and the interior fan 16 are stopped.

[0036] The high-pressure high-temperature gas refrigerant compressed in the compressor 11 flows through the main passage 32 and then the fourth opening-closing valve 17D and is divided into the first branch passage 33 and the second branch passage 34. The refrigerant divided into the second branch passage 34 flows through the drain pan heater 35. The refrigerant discharged from the drain pan heater 35 joins the refrigerant that has passed through the first branch passage 33 and flows to the evaporator 13. In the evaporator 13, a high-pressure gas refrigerant (so-called hot gas) flows in the heat transfer tube. Thus, in the evaporator 13, the frost collected on the heat transfer tube and the fin is gradually heated by the high-temperature gas refrigerant. As a result, the drain pan 28 gradually receives the frost from the evaporator 13. The refrigerant used to defrost the evaporator 13 is drawn into the

compressor 11 and compressed again. The drain pan 28 receives, for example, an ice block that falls from the surface of the evaporator 13 in addition to water, that is, melted frost. The ice block is heated and melted by the refrigerant flowing in the drain pan heater 35. The melted water is discharged out of the storage through a predetermined flow passage.

[0037] As shown in Fig. 2, the control device 50 further includes a refrigerant leakage determination device 60 that determines whether the refrigerant has leaked or estimates a refrigerant leakage occurrence time. When the refrigerant has leaked, an abnormality occurs in the refrigeration apparatus 1. An example of such an abnormality is a decrease in the compression efficiency of the compressor 11 due to a shortage of the refrigerant. The refrigerant leakage determination device 60 monitors the temperature of the discharge gas refrigerant discharged from the compressor 11 (hereafter, referred to as "discharge side refrigerant temperature") to determine whether the refrigerant has leaked or estimate a refrigerant leakage occurrence time.

[0038] As shown in Fig. 3, the refrigerant leakage determination device 60 includes a data obtainment unit 61, data storage 62, a pre-processing unit 63, a refrigerant leakage determination unit 64, and an output unit 65.

[0039] The data obtainment unit 61 is connected to the sensors 41 to 48 to communicate with the sensors 41 to 48. The data obtainment unit 61 receives time series data from the sensors 41 to 48. In an example, each of the sensors 41 to 48 outputs a detection result to the refrigerant leakage determination device 60 in each predetermined time TX. An example of the predetermined time TX is one hour. In an example, each of the sensors 41 to 48 stores detection results detected in a predetermined sampling cycle for the predetermined time TX and outputs an average of the detection results in the predetermined time TX to the refrigerant leakage determination device 60. Each of the sensors 41 to 48 may output a detection result detected at a point in time specified in each predetermined time TX to the refrigerant leakage determination device 60.

[0040] The data storage 62 is electrically connected to the data obtainment unit 61. The data storage 62 receives data from the data obtainment unit 61. The data storage 62 stores data from the data obtainment unit 61. In an example, the data storage 62 sequentially stores data from the data obtainment unit 61 in time order. In the present embodiment, the data storage 62 is configured to be a memory medium incorporated in the refrigerant leakage determination device 60. In this case, the data storage 62 may include, for example, nonvolatile memory and volatile memory. The data storage 62 may be a memory medium provided outside the refrigerant leakage determination device 60 or outside the refrigeration apparatus 1. In this case, the data storage 62 may include at least one of universe serial bus (USB) memory, a secure digital (SD) memory card, and a hard disk drive (HDD) memory medium.

[0041] The pre-processing unit 63 removes, from the time series data, data that act as noise when determining whether the refrigerant has leaked or estimating a refrigerant leakage occurrence time and replaces the section corresponding to the removed data with alternative

data. The pre-processing unit 63 includes a first processor 63a and a second processor 63b. The noise data include data having momentary variations that occur, for example, immediately after activation of the compressor 11 and data in temporally noncontinuous sections.

[0042] The first processor 63a is electrically connected to the data storage 62. The second processor 63b is electrically connected to the first processor 63a. The first processor 63a extracts a section that is replaced with alternative data. Such a section includes, for example, at least one of a section in which the refrigeration apparatus 1 is stopped, a section immediately after activation of the compressor 11, a section immediately after deactivation of the compressor 11, or a section immediately after operation of the compressor 11 is switched. In the present embodiment, the first processor 63a extracts all of the section in which the refrigeration apparatus 1 is stopped, a section immediately after activation of the compressor 11, the section immediately after deactivation of the compressor 11, and the section immediately after the operation of the compressor 11 is switched.

[0043] The second processor 63b inputs alternative data into the section extracted by the first processor 63a. The alternative data is a value before or after the section extracted by the first processor 63a or a predetermined representative value. For example, when the first processor 63a extracts the section in which the refrigeration apparatus 1 is stopped, the second processor 63b uses a value in the section before or after the section in which the refrigeration apparatus 1 is stopped as the alternative data. Data in sections being stopped, that is, temporally noncontinuous sections, are assumed to be, for example, zero. When the first processor 63a extracts the section immediately after activation of the compressor 11, the second processor 63b uses the value after the section immediately after activation of the compressor 11 as the alternative data. The value after the section immediately after activation of the compressor 11 may be an average value of data obtained during a predetermined period after the section immediately after activation of the compressor 11 or data obtained at a time immediately after the section immediately after activation of the compressor 11. When the first processor 63a extracts the section immediately after deactivation of the compressor 11, the second processor 63b uses a value in a section before the section immediately after deactivation of the compressor 11 as the alternative data. The section before the section immediately after deactivation of the compressor 11 may be the section immediately before deactivation of the compressor 11. The value in the section before the section immediately after deactivation of the compressor 11 may be an average value of data in the section immediately before deactivation of the compressor 11 or may be data related to time immediately before deactivation of the compressor 11. When the first processor 63a extracts the section immediately after operation of the compressor 11 is switched, the second processor 63b uses a value in the section before or after the section immediately after operation of the compressor 11 is switched as the alternative data. The value in the section before or after the section immediately after operation of the compressor 11 is switched may be an average value of data in the section before or after the section immediately after operation of the compressor 11 is switched or may be data related to a predetermined time in the section before or after the section immediately after operation of the compressor 11 is switched. As the process for calculating alternative data, data obtained before and after the

section that is replaced with the alternative data may be interpolated (e.g., linearly interpolated), and the calculated value may be used as the alternative data.

[0044] The refrigerant leakage determination unit 64 is electrically connected to the pre-processing unit 63. The refrigerant leakage determination unit 64 uses the data that has been processed by the pre-processing unit 63 to determine whether the refrigerant has leaked or estimate a refrigerant leakage occurrence time. The refrigerant leakage determination unit 64 includes a calculator 66 and a determination unit 67.

[0045] The calculator 66 calculates a first index value and a second index value to calculate a deviation degree of the refrigerant circuit 20 from a normal state. The normal state of the refrigerant circuit 20 is, for example, that the amount of refrigerant enclosed in the refrigerant circuit 20 (refrigerant contained amount) is in an appropriate range. The calculator 66 calculates the first index value from data related to operation of the refrigeration apparatus 1 in a first period. The calculator 66 calculates the second index value from data related to operation of the refrigeration apparatus 1 in a second period that differs in length from the first period. The calculator 66 calculates the deviation degree of the refrigerant circuit 20 from the normal state based on the first index value and the second index value. In the present embodiment, the calculator 66 calculates the deviation degree of the refrigerant circuit 20 from the normal state based on a deviation degree between the first index value and the second index value. The calculator 66 outputs the calculation result to the determination unit 67.

[0046] The determination unit 67 determines whether the refrigerant has leaked or estimates a refrigerant leakage occurrence time based on the deviation degree of the refrigerant circuit 20 from the normal state calculated by the calculator 66. The determination unit 67 outputs the determination result or the estimation result to the output unit 65.

[0047] Determination of whether the refrigerant has leaked is made based on the refrigerant leak amount per unit time being greater than or equal to a first threshold value and not based on a small amount of refrigerant leak. In an example, the first threshold value is an amount of refrigerant leak that causes the refrigeration apparatus 1 to have an abnormality and is determined in advance by experiments or the like. An example of the abnormality of the refrigeration apparatus 1 is an excessive increase in the temperature of the compressor 11 that occurs when the refrigerant contained amount is less than a lower limit value of the appropriate range and results in a failure to cool the compressor 11. The refrigerant leakage occurrence time may be, for example, a time at which the refrigerant contained amount becomes less than the lower limit value of the appropriate range or a time at which the temperature of the compressor 11 becomes greater than or equal to a second threshold value due to the refrigerant contained amount becoming less than the lower limit value of the appropriate range and resulting in a failure to cool the compressor 11. An example of the second threshold value is a temperature that increases the possibility of producing an abnormality such as galling of the compression mechanism of the compressor 11 and is determined in advance by experiments or the like.

[0048] The output unit 65 is electrically connected to the data storage 62 and the notification unit 52. The output unit 65 outputs the determination result of whether the refrigerant has leaked or the estimation result of a refrigerant leakage occurrence time to the data storage 62 and the notification unit 52. The notification unit 52 uses, for example, the display 53 to show the determination result of whether the refrigerant has leaked or the estimation result of a refrigerant leakage occurrence time. The output unit 65 further includes a wireless communicator including an antenna. The output unit 65 is configured to communicate with a terminal of a manager (manager terminal 70) through the wireless communicator. The output unit 65 outputs the determination result of whether the refrigerant has leaked or the estimation result of a refrigerant leakage occurrence time to the manager terminal 70. The manager terminal 70 may be a mobile communication device such as a smartphone or a tablet computer or may be a desktop personal computer.

[0049] The determination of whether the refrigerant has leaked and the estimation of a refrigerant leakage occurrence time, which are performed by the refrigerant leakage determination unit 64, will now be described in detail.

[0050] The calculator 66 uses data stored in the data storage 62 and related to operation of the refrigeration apparatus 1 to calculate the first index value from a moving average of data related to operation of the refrigeration apparatus 1 in the first period and calculate the second index value from a moving average of data related to operation of the refrigeration apparatus 1 in the second period. The calculator 66 calculates the first index value and the second index value using data in the first period and the second period that are before execution of the process. Then, the calculator 66 calculates the deviation degree between the first index value and the second index value. In the present embodiment, data in the first period include data for one day, and data in the second period include data for ten days. In the present embodiment, a sampling cycle is one hour, and data related to operation of the refrigeration apparatus 1 is obtained per hour. Hence, data in the first period and data in the second period may be expressed by the number of data sets as well as the length of a period. Data for one day include twenty-four data sets, and data for ten days include two hundred and forty data sets.

[0051] Each of the first index value and the second index value is a discharge side refrigerant temperature ratio. The discharge side refrigerant temperature ratio is an example of a discharge side refrigerant temperature index and is expressed by a ratio of an actual value of the discharge side refrigerant temperature of the compressor 11 to an estimated value of the discharge side refrigerant temperature of the compressor 11. In the present embodiment, the ratio of the actual value of the discharge side refrigerant temperature of the compressor 11 to the estimated value of the discharge side refrigerant temperature of the compressor 11 is defined as the discharge side refrigerant temperature ratio.

[0052] The calculator 66 calculates the discharge side refrigerant temperature ratio as data related to operation of the refrigeration apparatus 1. More specifically, the calculator 66 calculates the estimated value of the discharge side refrigerant temperature of the compressor 11 and the actual value of the discharge side refrigerant temperature of the compressor 11 and

calculates the discharge side refrigerant temperature ratio as a ratio of the calculated actual value of the discharge side refrigerant temperature of the compressor 11 to the calculated estimated value of the discharge side refrigerant temperature of the compressor 11.

[0053] The calculator 66 calculates an estimated value of the discharge side refrigerant temperature of the compressor 11 for each power source frequency and power source voltage of a power source, which is a source of power supplied to the refrigeration apparatus 1, using a regression analysis. A variable for the regression analysis is, for example, at least one of the condensation temperature, the evaporation temperature, the opening degree of the first expansion valve 14A, the opening degree of the second expansion valve 14B, the operating frequency of the compressor 11, or the rotational speed of the compressor 11 when the refrigerant contained amount of the refrigerant circuit 20 is in the appropriate range.

[0054] More specifically, in a transporting refrigeration apparatus such as a shipping container, the power source frequency and the power source voltage of a power source arranged at a terminal such as a harbor may differ from the power source frequency and the power source voltage of a power source arranged in a ship. In an example, the power source arranged at a terminal has a power source frequency of 50 Hz and a power source rated voltage of 380 V \pm 10%. The power source arranged in a ship has a power source frequency of 60 Hz and a power source rated voltage of 440 V \pm 10%. Examples of combination of a power source frequency and a power source voltage include first to sixth combinations. In the first combination, the power source frequency is 50 Hz, and the power source voltage is 342 V (lower limit value of the power source voltage when the power source frequency is 50 Hz). In the second combination, the power source frequency is 50 Hz, and the power source voltage is 380 V (median of the power source voltage when the power source frequency is 50 Hz). In the third combination, the power source frequency is 50 Hz, and the power source voltage is 418 V (upper limit value of the power source voltage when the power source frequency is 50 Hz). In the fourth combination, the power source frequency is 60 Hz, and the power source voltage is 396 V (lower limit value of the power source voltage when the power source frequency is 60 Hz). In the fifth combination, the power source frequency is 60 Hz, and the power source voltage is 440 V (median of the power source voltage when the power source frequency is 60 Hz). In the sixth combination, the power source frequency is 60 Hz, and the power source voltage is 484 V (upper limit value of the power source voltage when the power source frequency is 60 Hz). The calculator 66 calculates an estimated value of the discharge side refrigerant temperature of the compressor 11 for each of the first to sixth combinations. The combinations of the power source frequency and the power source voltage may be changed in any manner.

[0055] The calculator 66 calculates an actual value of the discharge side refrigerant temperature of the compressor 11 from a signal from the discharge temperature sensor 41. The actual value of the discharge side refrigerant temperature of the compressor 11 increases relative to the estimated value of the discharge side refrigerant temperature of the compressor 11, for example, as the refrigerant leak amount of the refrigerant circuit 20 per unit time increases per unit time. The refrigerant leak amount per unit time is correlated with the

deviation degree of the actual value of the discharge side refrigerant temperature of the compressor 11 from the estimated value of the discharge side refrigerant temperature of the compressor 11.

[0056] The calculator 66 calculates the discharge side refrigerant temperature ratio obtained in the first period (hereafter, referred to as "first refrigerant temperature ratio") as the first index value and calculates the discharge side refrigerant temperature ratio obtained in the second period (hereafter, referred to as "second refrigerant temperature ratio") as the second index value. Fig. 4A is a graph showing an example of changes in the first refrigerant temperature ratio and the second refrigerant temperature ratio. As shown in Fig. 4A, on and before July 9th, the deviation degree between the first refrigerant temperature ratio and the second refrigerant temperature ratio is small. From July 9th, the deviation degree gradually increases.

[0057] The calculator 66 calculates, for example, the degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio. In the present embodiment, the degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio is expressed by a ratio of the first refrigerant temperature ratio to the second refrigerant temperature ratio. As the ratio increases, the degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio increases. Alternatively, the degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio may be expressed by a difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio. As the difference increases, the degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio increases. Fig. 4B is a graph showing an example of changes in the degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio. As shown in Fig. 4B, on and before July 9th, the degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio is substantially 1.00. From July 9th, the degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio gradually increases.

[0058] When the degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio is greater than or equal to a threshold value XT , the determination unit 67 determines that the refrigerant has leaked. The threshold value XT is set in advance by experiments or the like and is used to determine an occurrence of the refrigerant leakage that may provoke an abnormality of the refrigeration apparatus 1.

[0059] The determination unit 67 estimates a refrigerant leakage occurrence time based on a change tendency of the degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio. More specifically, the calculator 66 calculates, for example, a degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio for each day and outputs the degree of difference to the determination unit 67. The determination unit 67 obtains a change tendency of the degree of difference, for example, based on the degree of difference between the first refrigerant

temperature ratio and the second refrigerant temperature ratio of each day. The determination unit 67 estimates a refrigerant leakage occurrence time based on information indicating that the degree of difference has an increasing tendency and the slope of the degree of difference. More specifically, the determination unit 67 estimates a time in which the degree of difference reaches the threshold value XT based on the slope of the degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio. The determination unit 67 may calculate the slope of the degree of difference using, for example, regression analysis or a straight line that connects degrees of difference in two predetermined periods. In an example, as shown in Fig. 4B, the determination unit 67 estimates the degree of difference from July 16th based on changes in the degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio until July 16th (broken line in Fig. 4B). The determination unit 67 estimates a refrigerant leakage occurrence time based on a comparison of the threshold value XT with changes in the degree of difference from July 16th.

[0060] Procedures of determining whether the refrigerant has leaked or estimating a refrigerant leakage occurrence time performed by the refrigerant leakage determination device 60 will be described in detail with reference to Fig. 5. This process is executed, for example, at least one of when there is a user request, when the transporting refrigeration apparatus 1 or the refrigerant leakage determination device 60 is powered on, when transportation of the refrigeration apparatus 1 is completed, or when the pre-trip inspection of the refrigeration apparatus 1 is conducted. In the present embodiment, at each of when there is a user request, when the refrigeration apparatus 1 or the refrigerant leakage determination device 60 is powered on, when transportation of the refrigeration apparatus 1 is completed, and when the pre-trip inspection of the refrigeration apparatus 1 is conducted, the refrigerant leakage determination device 60 determines whether the refrigerant has leaked or estimates a refrigerant leakage occurrence time.

[0061] In step S11, the refrigerant leakage determination device 60 calculates a first refrigerant temperature ratio and a second refrigerant temperature ratio from data related to operation of the refrigeration apparatus 1 and then proceeds to step S12. In step S12, the refrigerant leakage determination device 60 calculates a degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio and then proceeds to step S13.

[0062] In step S13, the refrigerant leakage determination device 60 determines whether the degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio is greater than or equal to the threshold value XT. When an affirmative determination is made in step S13, the refrigerant leakage determination device 60 proceeds to step S14 to determine that the refrigerant has leaked and then proceeds to step S15. In step S15, the refrigerant leakage determination device 60 transmits the determination result to at least one of the display 53 or the manager terminal 70 and then temporarily ends the process. In step S15, the display 53 and the manager terminal 70 issue notification of the determination result of whether the refrigerant has leaked or notification of the estimation result of a refrigerant leakage occurrence time at least one of when there is a user request, when the

refrigeration apparatus 1 or the refrigerant leakage determination device 60 is powered on, when transportation of the refrigeration apparatus 1 is completed, or when the pre-trip inspection of the refrigeration apparatus 1 is conducted. In the present embodiment, the display 53 and the manager terminal 70 issue notification of the determination result of whether the refrigerant has leaked or notification of the estimation result of a refrigerant leakage occurrence time each of when there is a user request, when the refrigeration apparatus 1 or the refrigerant leakage determination device 60 is powered on, when transportation of the refrigeration apparatus 1 is completed, and when the pre-trip inspection of the refrigeration apparatus 1 is conducted. In step S15, the result may be transmitted to the notification unit 52 instead of the display 53. When the notification unit 52 includes a speaker, the notification unit 52 may issue, using the speaker, notification of the determination result of whether the refrigerant has leaked or notification of the estimation result of a refrigerant leakage occurrence time.

[0063] When a negative determination is made in step S13, the refrigerant leakage determination device 60 proceeds to step S16 to calculate a change tendency of the degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio and then proceeds to step S17.

[0064] In step S17, the refrigerant leakage determination device 60 estimates a refrigerant leakage occurrence time based on a slope of changes in the degree of difference between the first refrigerant temperature ratio and the second refrigerant temperature ratio and then proceeds to step S18. In step S18, the refrigerant leakage determination device 60 transmits the estimation result to at least one of the display 53 or the manager terminal 70 and then temporarily ends the process. As shown in the flowchart of Fig. 5, the refrigerant leakage determination device 60 estimates a refrigerant leakage occurrence time after determining whether the refrigerant has leaked.

[0065] The method for determining the refrigerant leakage executed by the refrigerant leakage determination device 60 and described above includes a data storing step, a first calculating step, a second calculating step, and a determining step. The steps will be described below.

[0066] The data storing step is a step of storing data related to operation of the refrigeration apparatus 1. In an example, the data storing step stores data related to operation of the refrigeration apparatus 1 and obtained from the data obtainment unit 61 in the data storage 62 as time series data.

[0067] The first calculating step is a step of calculating the first index value from data related to operation of the refrigeration apparatus 1 in the first period and calculating the second index value from data related to operation of the refrigeration apparatus 1 in the second period. In an example, the first calculating step is executed by the calculator 66. The first calculating step is a step of calculating the first index value from a moving average of data related to operation of the refrigeration apparatus 1 in the first period and calculating the second index value from a moving average of data related to operation of the refrigeration apparatus 1 in the second

period. In an example, the first calculating step includes a pre-processing step that removes data that act as noise when determining whether the refrigerant has leaked or estimating a refrigerant leakage occurrence time and replaces it with alternative data with the pre-processing unit 63. The relationship of the first calculating step with Fig. 5 is that step S11 in Fig. 5 corresponds to the first calculating step.

[0068] The second calculating step is a step of calculating a deviation degree of the refrigerant circuit 20 from the normal state based on the first index value and the second index value. In an example, the second calculating step is executed by the calculator 66. The relationship of the second calculating step with Fig. 5 is that step S12 in Fig. 5 corresponds to the second calculating step.

[0069] The determining step is a step of determining whether the refrigerant has leaked or estimating a refrigerant leakage occurrence time based on the deviation degree of the refrigerant circuit 20 from the normal state. In an example, in the determining step, when the second index value refers to the normal state of the refrigerant circuit 20 and the deviation degree of the first index value from the second index value becomes greater than or equal to a threshold value, it is determined that the refrigerant has leaked. In the determining step, a time at which the deviation degree reaches the threshold value is estimated based on a change tendency of the deviation degree of the first index value from the second index value, so that a refrigerant leakage occurrence time is estimated. The relationship of the determining step with Fig. 5 is that steps S13 to S18 in Fig. 5 correspond to the determining step.

[0070] The operation of the present embodiment will now be described. The refrigerant leakage determination device 60 calculates the second index value from a moving average of data related to operation of the refrigeration apparatus 1 in the second period and uses the calculated second index value as reference. In the present embodiment, data in the second period is related to operation of the refrigeration apparatus 1 obtained during a long period of ten days to thirty days and thus is subtly affected by variations related to operation of the refrigeration apparatus 1 obtained in a short period such as one day.

[0071] The refrigerant leakage determination device 60 also calculates the first index value from a moving average of data related to operation of the refrigeration apparatus 1 in the first period. In the present embodiment, data in the first period is related to operation of the refrigeration apparatus 1 in a short period, that is, one day, and thus is greatly affected by recent variations related to operation of the refrigeration apparatus 1.

[0072] As described above, the second index value, which is subtly affected by recent variations related to operation of the refrigeration apparatus 1, is used as reference to monitor how much the first index value, which is greatly affected by variations related to operation of the refrigeration apparatus 1, is deviated from the second index value. This facilitates extraction of variations related to operation of the refrigeration apparatus 1. With this configuration, when the refrigerant has leaked, the first index value is prominently deviated from the second index value so that the refrigerant leakage determination device 60

determines that the refrigerant has leaked. In addition, the refrigerant leakage determination device 60 obtains a change tendency of the deviation degree of the first index value from the second index value and estimates changes in the deviation degree to estimate a refrigerant leakage occurrence time.

[0073] The present embodiment has the following advantages.

1. (1) In data related to operation of the refrigeration apparatus 1, the calculator 66 calculates a first index value from data related to operation of the refrigeration apparatus 1 in the first period and calculates a second index value from data related to operation of the refrigeration apparatus 1 in the second period that differs length from the first period. Then, the calculator 66 calculates a deviation state of the refrigerant circuit 20 from the normal state based on the first index value and the second index value. The determination unit 67 determines whether the refrigerant has leaked or estimates a refrigerant leakage occurrence time based on the deviation degree of the refrigerant circuit 20 from the normal state. With this configuration, the deviation state of the refrigerant circuit 20 from the normal state is calculated based on the state of difference between the first index value and the second index value calculated using data related to operation of the refrigeration apparatus 1 including the pre-trip inspection operation of the refrigeration apparatus 1 and normal operations of the refrigeration apparatus 1 such as the cooling operation and the defrosting operation. The determination of whether the refrigerant has leaked or the estimation of a refrigerant leakage occurrence time is performed based on the deviation state of the refrigerant circuit 20 from the normal state. Thus, the determination of whether the refrigerant has leaked or the estimation of a refrigerant leakage occurrence time is performed without performing a special operation for determining whether the refrigerant has leaked.
2. (2) The second index value, which is calculated from the long second period, is subtly affected by variations related to operation of the refrigeration apparatus 1. The first index value, which is calculated from the short first period, is greatly affected by variations related to operation of the refrigeration apparatus 1. In the present embodiment, the calculator 66 calculates a first index value and a second index value and calculates a deviation degree of the refrigerant circuit 20 from the normal state based on the degree of difference between the first index value and the second index value. This facilitates extraction of variations in operation of the refrigeration apparatus 1. The determination of whether the refrigerant has leaked or the estimation of a refrigerant leakage occurrence time is performed based on the variations in operation of the refrigeration apparatus 1.
3. (3) The first index value is calculated from a moving average of data related to operation of the refrigeration apparatus 1 in the first period. The second index value is calculated from a moving average of data related to operation of the refrigeration apparatus 1 in the second period. With this configuration, the determination of whether the refrigerant has leaked or the estimation of a refrigerant leakage occurrence time is performed based on a degree of difference between variations in operation of the refrigeration apparatus 1 during a long period and variations in operation of the refrigeration

apparatus 1 in a short period.

4. (4) When the amount of refrigerant enclosed in the refrigerant circuit 20 (refrigerant contained amount) is less than the appropriate range, suction pressure of the compressor 11 decreases and the cooling the inside of the compressor 11 with the refrigerant may become insufficient. As a result, the temperature of the compressor 11 may be excessively increased. More specifically, when the amount of refrigerant enclosed in the refrigerant circuit 20 is less than the lower limit value of the appropriate range, the discharge side refrigerant temperature of the compressor 11 is higher than when the amount of refrigerant enclosed in the refrigerant circuit 20 is in the appropriate range. In the present embodiment, the discharge side refrigerant temperature ratio, which is a ratio of the actual value of the discharge side refrigerant temperature of the compressor 11 to the estimated value of the discharge side refrigerant temperature, is used as each of the first index value and the second index value. Thus, the determination of whether the refrigerant has leaked or the estimation of a refrigerant leakage occurrence time is performed with high accuracy.
5. (5) The calculator 66 calculates an estimated refrigerant temperature for each power source frequency and power source voltage and calculates the first refrigerant temperature ratio and the second refrigerant temperature ratio for each power source frequency and power source voltage. Since the first refrigerant temperature ratio and the second refrigerant temperature ratio are calculated with higher accuracy, the determination of whether the refrigerant has leaked or the estimation of a refrigerant leakage occurrence time is performed with high accuracy.
6. (6) The pre-processing unit 63 eliminates data related to operation of the refrigeration apparatus 1 and acting as noise when determining whether the refrigerant has leaked or estimating a refrigerant leakage occurrence time, and replaces it with alternative data. This allows for an accurate determination of whether the refrigerant has leaked or an accurate estimation of a refrigerant leakage occurrence time.
7. (7) When the first processor 63a extracts a section immediately after activation of the compressor 11, the second processor 63b uses a value after the section immediately after activation of the compressor 11 as the alternative data. When the first processor 63a extracts the section immediately after deactivation of the compressor 11, the second processor 63b uses a value in a section before the section immediately after deactivation of the compressor 11 as the alternative data. When the first processor 63a extracts the section immediately after operation of the compressor 11 is switched, the second processor 63b uses a value in the section before or after the section immediately after operation of the compressor 11 is switched as the alternative data. This configuration uses data temporally close to the section extracted by the first processor 63a as alternative data, so that the deviation degree of the alternative data from the actual data related to operation of the refrigeration apparatus 1 is decreased. Thus, the determination of whether the refrigerant has leaked or the estimation of a refrigerant leakage occurrence time is performed with high accuracy.
8. (8) The notification unit 52 indicates occurrence of refrigerant leakage or a refrigerant leakage occurrence time in the display 53 of the refrigeration apparatus 1 or the manager terminal 70. This allows the manager or the operator of the refrigeration

apparatus 1 to recognize the occurrence of refrigerant leakage or the refrigerant leakage occurrence time.

Modified Examples

[0074] The description related to the above embodiment exemplifies, without any intention to limit, applicable forms of a refrigerant leakage determination device, a refrigeration apparatus including the refrigerant leakage determination device, and a method for determining a refrigerant leakage according to the present disclosure. The refrigerant leakage determination device, the refrigeration apparatus including the refrigerant leakage determination device, and the method for determining a refrigerant leakage according to the present disclosure can be applicable to, for example, modified examples of the embodiment that are described below and combinations of at least two of the modified examples that do not contradict each other. In the following modified examples, the same reference characters are given to those elements that are the same as the corresponding elements of the above embodiment. Such elements will not be described in detail.

[0075] In the embodiment, the degree of difference between the first index value and the second index value is expressed by the ratio of the first index value to the second index value. However, there is no limit to such a configuration. The process of calculating the degree of difference between the first index value and the second index value may be changed in any manner. In an example, the calculator 66 may calculate the degree of difference between the first index value and the second index value based on at least one of a standard deviation, skewness, likelihood, kurtosis, or an average that is obtained using the first index value and the second index value.

[0076] In the embodiment, the refrigerant leakage determination device 60 performs both the determination of whether the refrigerant has leaked and the estimation of a refrigerant leakage occurrence time. Instead, the refrigerant leakage determination device 60 may perform only the determination of whether the refrigerant has leaked. When the degree of difference between the first index value and the second index value is less than the threshold value XT, the refrigerant leakage determination device 60 may estimate a refrigerant leakage occurrence time. In this case, the refrigerant leakage determination device 60 may omit the determination of whether the refrigerant has leaked.

[0077] In the embodiment, the pre-processing unit 63 removes, from time series data, data that act as noise when determining whether the refrigerant has leaked or estimating a refrigerant leakage occurrence time, and replaces the section corresponding to the removed data with alternative data. However, there is no limitation to such a configuration. For example, the pre-processing unit 63 may only remove, from time series data, data that act as noise when determining whether the refrigerant has leaked or estimating a refrigerant leakage

occurrence time. This configuration accurately determines whether the refrigerant has leaked or accurately estimates a refrigerant leakage occurrence time.

[0078] In the embodiment, the first index value and the second index value may be calculated from the estimated value of the discharge side refrigerant temperature or the actual value of the discharge side refrigerant temperature instead of the discharge side refrigerant temperature ratio. In an example, the calculator 66 calculates the first index value from a moving average of estimated values of the discharge side refrigerant temperature in the first period and calculates the second index value from a moving average of estimated values of the discharge side refrigerant temperature in the second period. In an example, the calculator 66 calculates the first index value from a moving average of actual values of the discharge side refrigerant temperature in the first period and calculates the second index value from a moving average of actual values of the discharge side refrigerant temperature in the second period.

[0079] In the embodiment, the first index value and the second index value may be a discharge side refrigerant pressure ratio, which is a ratio of an actual value of a discharge side refrigerant pressure of the compressor 11 to an estimated value of the discharge side refrigerant pressure of the compressor 11, instead of the discharge side refrigerant temperature ratio. The calculator 66 calculates a discharge side refrigerant pressure ratio in the first period (hereafter, referred to as "first refrigerant pressure ratio") as the first index value and a discharge side refrigerant pressure ratio in the second period (hereafter, referred to as "second refrigerant pressure ratio") as the second index value. The calculator 66 calculates a degree of difference between the first refrigerant pressure ratio and the second refrigerant pressure ratio. When the degree of difference between the first refrigerant pressure ratio and the second refrigerant pressure ratio is greater than or equal to a predetermined threshold value, the determination unit 67 determines that the refrigerant has leaked. The determination unit 67 also estimates a refrigerant leakage occurrence time based on a change tendency of the degree of difference between the first refrigerant pressure ratio and the second refrigerant pressure ratio. The discharge side cooling temperature ratio may be replaced with a ratio of an actual value of a degree of superheating the intake gas refrigerant drawn into the compressor 11 to an estimated value of the degree of superheating the intake gas refrigerant or a ratio of an actual value of a degree of subcooling the liquid refrigerant at an outlet of the condenser 12 to an estimated value of the degree of subcooling the liquid refrigerant at the outlet of the condenser 12.

[0080] In the modified example, the first index value and the second index value may be calculated from an estimated value of the discharge side refrigerant pressure of the compressor 11 or an actual value of the discharge side refrigerant pressure of the compressor 11 instead of the discharge side refrigerant pressure ratio. In an example, the calculator 66 calculates the first index value from a moving average of estimated values of the discharge side refrigerant pressure of the compressor 11 in the first period and calculates the second index value from a moving average of estimated values of the discharge side refrigerant pressure of the compressor 11 in the second period. In an example, the calculator 66 calculates the first index value from a moving average of actual values of the discharge side

refrigerant pressure of the compressor 11 in the first period and calculates the second index value from a moving average of actual values of the discharge side refrigerant pressure of the compressor 11 in the second period.

[0081] In the embodiment, the data storage 62 may be an external server of the refrigeration apparatus 1 connected to the refrigeration apparatus 1 to communicate with the refrigeration apparatus 1. An example of the server includes a cloud server. More specifically, the refrigerant leakage determination device 60 transmits data obtained in the data obtainment unit 61 to the server so that the server stores the data.

[0082] In the embodiment, the refrigerant leakage determination device 60 and the notification unit 52 are separately arranged. Instead, the refrigerant leakage determination device 60 may include the notification unit 52.

[0083] In the embodiment, the configuration of a transporting refrigeration apparatus is described as the refrigeration apparatus 1. However, the refrigeration apparatus is not limited to this configuration. For example, a refrigeration apparatus may be used for a stationary storage. When the refrigeration apparatus 1 is used as a refrigeration apparatus other than a transporting refrigeration apparatus, the refrigerant leakage determination device 60 determines whether the refrigerant has leaked or estimates a refrigerant leakage occurrence time at least one of when there is a user request, when the refrigeration apparatus 1 or the refrigerant leakage determination device 60 is powered on, or when the pre-trip inspection of the refrigeration apparatus 1 is conducted. In addition, the notification unit 52 issues notification of a determination result of whether the refrigerant has leaked or notification of an estimation result of a refrigerant leakage occurrence time at least one of when there is a user request, when the refrigeration apparatus 1 or the refrigerant leakage determination device 60 is powered on, or when the pre-trip inspection of the refrigeration apparatus 1 is conducted.

[0084] In the embodiment, the refrigeration apparatus 1 is configured to be installed on a container. However, the refrigeration apparatus is not limited to this the configuration. For example, as shown in Fig. 6, a refrigeration apparatus may be used as an air conditioner 80. The air conditioner 80 includes a refrigerant circuit 90 in which an outdoor unit 80A and a wall-mounted indoor unit 80B are connected by a refrigerant pipe 91. The outdoor unit 80A is arranged outdoors. The indoor unit 80B is installed on an indoor wall surface.

[0085] The outdoor unit 80A includes a compressor 81 having a variable displacement varied by a change in an operating frequency, a four-way switching valve 82, an outdoor heat exchanger 83, an expansion valve 84, an outdoor fan 85, and an outdoor control device 86. The compressor 81 is, for example, a rocking piston compressor and includes, for example, a compression mechanism, a motor, and a crankshaft that transmits driving power of the motor to the compression mechanism. The outdoor heat exchanger 83 exchanges heats between the outside air and the refrigerant and may be, for example, a fin-and-tube heat exchanger. The expansion valve 84 is, for example, an electronic expansion valve. The outdoor fan 85 includes a motor, which is a drive source having a changeable number of revolutions, and an impeller

connected to an output shaft of the motor. An example of the impeller is a propeller fan. When the impeller is rotated by the motor, the outdoor fan 85 generates an airflow of outdoor air flowing through the outdoor heat exchanger 83. The outdoor control device 86 is electrically connected to the motor of the compressor 81, the four-way switching valve 82, the expansion valve 84, and the motor of the outdoor fan 85 to control their operations.

[0086] The indoor unit 80B includes an indoor heat exchanger 87, an indoor fan 88, and an indoor control device 89. The indoor heat exchanger 87 exchanges heat between the inside air and the refrigerant and may be, for example, a fin-and-tube heat exchanger. The indoor fan 88 includes a motor, which is a drive source having a changeable number of revolutions, and an impeller connected to an output shaft of the motor. An example of the impeller is a cross-flow fan. The indoor control device 89 is electrically connected to the indoor fan 88 to control operation of the indoor fan 88.

[0087] The refrigerant circuit 90 is formed by connecting the compressor 81, the four-way switching valve 82, the outdoor heat exchanger 83, and the expansion valve 84 to the indoor heat exchanger 87 and an accumulator 81a with the refrigerant pipe 91 as a loop. The refrigerant circuit 90 is configured to execute a vapor compression refrigeration cycle that reversibly circulates the refrigerant by switching the four-way switching valve 82.

[0088] More specifically, when the four-way switching valve 82 is switched to a cooling mode connection state (illustrated with solid line), the refrigerant circuit 90 forms a cooling cycle in which the refrigerant circulates in the order of the compressor 81, the four-way switching valve 82, the outdoor heat exchanger 83, the expansion valve 84, the indoor heat exchanger 87, the four-way switching valve 82, the accumulator 81a, and the compressor 81. As a result, the air conditioner 80 performs a cooling operation in which the outdoor heat exchanger 83 acts as a condenser, and the indoor heat exchanger 87 acts as an evaporator. When the four-way switching valve 82 is switched to a heating mode connection state (illustrated with broken lines), the refrigerant circuit 90 forms a heating cycle in which the refrigerant circulates in the order of the accumulator 81a, the compressor 81, the four-way switching valve 82, the indoor heat exchanger 87, the expansion valve 84, the outdoor heat exchanger 83, the four-way switching valve 82, and the compressor 81. As a result, the air conditioner 80 performs a heating operation in which the indoor heat exchanger 87 acts as a condenser and the outdoor heat exchanger 83 acts as an evaporator.

[0089] In the air conditioner 80, for example, the refrigerant leakage determination device 60 (not shown in Fig. 6) is arranged on one of the outdoor control device 86 and the indoor control device 89. The notification unit 52 (not shown in Fig. 6) is arranged on, for example, a remote controller of the air conditioner 80.

[0090] In the embodiment, the refrigeration apparatus 1 includes the refrigerant leakage determination device 60. However, the refrigeration apparatus 1 is not limited to this configuration. For example, the refrigerant leakage determination device 60 may be omitted from the refrigeration apparatus 1. The refrigerant leakage determination device 60 and the

refrigeration apparatus 1 may be separately arranged. In an example, the refrigerant leakage determination device 60 may be arranged on a server configured to communicate with the refrigeration apparatus 1. In this case, the refrigeration apparatus 1 communicates with the refrigerant leakage determination device 60 to obtain a determination result of whether the refrigerant has leaked or an estimation result of a refrigerant leakage occurrence time.

[0091] While the embodiments of the device have been described herein above, it is to be appreciated that various changes in form and detail may be made without departing from the scope of the device presently or hereafter claimed.

REFERENCES CITED IN THE DESCRIPTION

Cited references

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Patent documents cited in the description

- [JP2013204871A \[0009\]](#)
- [JP2009002650A \[0009\]](#)
- [US2017268811A1 \[0009\]](#)
- [EP2546588A1 \[0009\]](#)
- [JP2016090177A \[0009\]](#)
- [JP2015222151A \[0009\]](#)
- [JP2003161495A \[0009\]](#)
- [JP2006064307A \[0009\]](#)
- [JPH07217973A \[0009\]](#)

**ANORDNING TIL BESTEMMELSE AF KØLEMIDDELLÆKAGE,
FRYSEANORDNING, DER INDBEFATTER DENNE ANORDNING TIL
BESTEMMELSE AF KØLEMIDDELLÆKAGE, OG FREMGANGSMÅDE TIL
BESTEMMELSE AF KØLEMIDDELLÆKAGE**

PATENTKRAV

1. Anordning til bestemmelse af kølemiddellækage (60), der er konfigureret til at bestemme en kølemiddellækage i et køleapparat (1), hvilket køleapparatet (1) indbefatter et kølemiddelkredsløb (20), hvilket kølemiddelkredsløb (20) indbefatter en kompressor (11), en kondensator (12), en dekompressionsanordning (14A, 14B) og en fordamper (13) og er konfigureret, således at et kølemiddel cirkulerer gennem kompressoren (11), kondensatoren (12), dekompressionsanordningen (14A, 14B) og fordamperen (13), idet anordningen til bestemmelse af kølemiddellækage (60) omfatter:

en kalkulator (66), der er konfigureret til at beregne en afvigelsesgrad for kølemiddelkredsløbet (20) fra en normal tilstand baseret på data relateret til drift af køleapparatet (1); og

en bestemmelsesenhed (67), der er konfigureret til at bestemme, om kølemidlet er lækket, eller estimere en forekomsttid for kølemiddellækage baseret på et beregningsresultat fra kalkulatoren (66), hvor

dataene relateret til drift af køleapparatet (1) indbefatter data relateret til drift af køleapparatet (1) i en første periode og data relateret til drift af køleapparatet (1) i en anden periode, der afviger i længde fra første periode,

kalkulatoren (66) er konfigureret til at beregne en første indekxsværdi ud fra dataene relateret til drift af køleapparatet (1) i den første periode og beregne en anden indekxsværdi ud fra dataene relateret til drift af køleapparatet (1) i den anden periode,

kalkulatoren (66) er konfigureret til at beregne afvigelsesgraden for kølemiddelkredsløbet (20) fra den normale tilstand baseret på den første indekxsværdi og den anden indekxsværdi,

bestemmelsesenheden (67) er konfigureret til at bestemme, om kølemidlet er lækket, eller estimere forekomsttiden for kølemiddellækage baseret på kølemiddelkredsløbets (20) afvigelsesgrad fra den normale tilstand,

hver af den første indekxsværdi og den anden indekxsværdi indbefatter én af en estimeret værdi for en kølemiddeltemperatur på udledningssiden af kompressoren (11) eller et kølemiddeltemperaturindeks på udledningssiden, der beregnes baseret på den

estimerede værdi for kølemiddeltemperaturen på udledningssiden af kompressoren (11) og den faktiske værdi for kølemiddeltemperaturen på udledningssiden af kompressoren (11),

kalkulatoren (66) er konfigureret til at beregne den første indekxsværdi ud fra et glidende gennemsnit af dataene relateret til drift af køleapparatet (1) i den første periode,

kalkulatoren (66) er konfigureret til at beregne den anden indekxsværdi ud fra et glidende gennemsnit af dataene relateret til drift af køleapparatet (1) i den anden periode, og

kalkulatoren (66) er konfigureret til at beregne den estimerede værdi for kølemiddeltemperaturen på udledningssiden af kompressoren (11) for hver strømkildefrekvens og strømkildespænding for en strømkilde, der er en strømkilde, der leveres til køleapparatet (1), ved anvendelse af en regressionsanalyse, hvor en variabel for regressionsanalysen er mindst én af en kondensationstemperatur, en fordampningstemperatur, en åbningsgrad af en ekspansionsventil (14A, 14B), der er dekompressionsanordningen, en driftsfrekvens for kompressoren (11) eller en rotationshastighed for kompressoren (11), når en mængde kølemiddel indeholdt i kølemiddelkredsløbet (20) er inden for en passende værdimængde.

2. Anordning til bestemmelse af kølemiddellækage (60) ifølge krav 1, hvor kalkulatoren (66) er konfigureret til at påvise afvigelsesgraden for kølemiddelkredsløbet (20) fra den normale tilstand baseret på en afvigelsesgrad mellem den første indekxsværdi og den anden indekxsværdi.

3. Anordning til bestemmelse af kølemiddellækage (60) ifølge krav 1 eller 2, hvor dataene relateret til drift af køleapparatet (1) i den første periode indbefatter data for én dag, og

dataene relateret til drift af køleapparatet (1) i den anden periode indbefatter data for ti dage eller mere og tredive dage eller mindre.

4. Anordning til bestemmelse af kølemiddellækage ifølge krav 3, hvor dataene relateret til drift af køleapparatet (1) i den første periode indbefatter fireogtyve datasæt, og

dataene relateret til drift af køleapparatet (1) i den anden periode indbefatter to hundrede og fyrre datasæt eller mere og syv hundrede og tyve datasæt eller mindre.

5. Anordning til bestemmelse af kølemiddellækage ifølge et hvilket som helst af kravene 1 til 4, hvor kalkulatoren (66) er konfigureret til at beregne den første indekssværdi og den anden indekssværdi ud fra data, der ekskluderer mindst ét af data i en sektion, i hvilken køleapparatet (1) stoppes, data i en sektion umiddelbart efter aktivering af kompressoren (11), data i en sektion umiddelbart efter deaktivering af kompressoren (11) eller data i en sektion, umiddelbart efter drift af kompressoren (11) skiftes.

6. Anordning til bestemmelse af kølemiddellækage ifølge et hvilket som helst af kravene 1 til 4, hvor kalkulatoren (66) er konfigureret til at beregne den første indekssværdi og den anden indekssværdi ved anvendelse af alternative data til mindst ét af data i en sektion, i hvilken køleapparatet (1) stoppes, data i en sektion umiddelbart efter aktivering af kompressoren (11), data i en sektion umiddelbart efter deaktivering af kompressoren (11) eller data i en sektion, umiddelbart efter drift af kompressoren (11) skiftes.

7. Anordning til bestemmelse af kølemiddellækage ifølge krav 6, hvor de alternative data er en forudbestemt repræsentativ værdi eller en værdi før eller efter sektionen, der anvender de alternative data i sektionen, i hvilken køleapparatet (1) stoppes, sektionen umiddelbart efter aktivering af kompressoren (11), sektionen umiddelbart efter deaktivering af kompressoren (11) eller sektionen, umiddelbart efter drift af kompressoren (11) skiftes.

8. Anordning til bestemmelse af kølemiddellækage ifølge et hvilket som helst af kravene 1 til 7, hvor kalkulatoren (66) er konfigureret til at beregne en afvigelsesgrad mellem den første indekssværdi og den anden indekssværdi baseret på mindst én/ét af en standardafvigelse, skævhed, sandsynlighed, topstejlhed eller et gennemsnit, der opnås ved anvendelse af den første indekssværdi og den anden indekssværdi.

9. Anordning til bestemmelse af kølemiddellækage ifølge et hvilket som helst af kravene 1 til 8, hvor

køleapparatet (1) yderligere indbefatter en meddelelsesenhed (52), der udsender en meddelelse om et bestemmelsesresultat af, om kølemidlet er lækket, eller en meddelelse om et estimeret resultat af forekomsttiden for kølemiddellækage, og

meddelelsesenheden (52) er konfigureret til at udsende en meddelelse om et bestemmelsesresultat af, om kølemidlet er lækket, eller en meddelelse om et estimeret resultat af forekomsttiden for kølemiddellækage ved mindst ét af, når der er en

brugeranmodning, når køleapparatet (1) eller anordningen til bestemmelse af kølemiddellækage (60) tændes, eller når en inspektion før tur af køleapparatet (1) udføres.

10. Køleapparat, der omfatter:

anordningen til bestemmelse af kølemiddellækage (60) ifølge et hvilket som helst af kravene 1 til 9.

11. Køleapparat ifølge krav 10, hvor

køleapparatet er et transportkøleapparat (1),

transportkøleapparatet (1) yderligere indbefatter en meddelelsesenhed (52), der er konfigureret til at udsende en meddelelse om et bestemmelsesresultat af, om kølemidlet er lækket, eller en meddelelse om et estimeret resultat af forekomsttiden for kølemiddellækage, og

meddelelsesenheden (52) er konfigureret til at udsende en meddelelse om et bestemmelsesresultat af, om kølemidlet er lækket, eller en meddelelse om et estimeret resultat af forekomsttiden for kølemiddellækage ved mindst ét af, når der er en brugeranmodning, når transportkøleapparatet (1) eller anordningen til bestemmelse af kølemiddellækage (60) tændes, når transport af transportkøleapparatet (1) afsluttes, eller når en inspektion før tur af transportkøleapparatet (1) udføres.

12. Fremgangsmåde til bestemmelse af en kølemiddellækage i et køleapparat (1), idet køleapparatet (1) indbefatter et kølemiddelkredsløb (20), og kølemiddelkredsløbet (20) indbefatter en kompressor (11), en kondensator (12), en dekompressionsanordning (14A, 14B) og en fordamper (13) og er konfigureret, således at et kølemiddel cirkulerer gennem kompressoren (11), kondensatoren (12), dekompressionsanordningen (14A, 14B) og fordamperen (13), hvilken fremgangsmåde omfatter:

at lagre data relateret til drift af køleapparatet (1);

at beregne en første indekssværdi ud fra data relateret til drift af køleapparatet (1) i en første periode og beregne en anden indekssværdi ud fra data relateret til drift af køleapparatet (1) i en anden periode, der afviger i længde fra den første periode;

at beregne en afvigelsesgrad for kølemiddelkredsløbet (20) fra en normal tilstand baseret på den første indekssværdi og den anden indekssværdi; og

at bestemme, om kølemidlet er lækket, eller estimere en forekomsttid for kølemiddellækage baseret på afvigelsesgraden for kølemiddelkredsløbet (20) fra den

normale tilstand, hvor

hver af den første indekssværdi og den anden indekssværdi indbefatter én af en estimeret værdi for en kølemiddeltemperatur på udledningssiden af kompressoren (11) eller et kølemiddeltemperaturindeks på udledningssiden, der beregnes baseret på den estimerede værdi for kølemiddeltemperaturen på udledningssiden af kompressoren (11) og den faktiske værdi for kølemiddeltemperaturen på udledningssiden af kompressoren (11),

den første indekssværdi beregnes ud fra et glidende gennemsnit af dataene relateret til drift af køleapparatet (1) i den første periode,

den anden indekssværdi beregnes ud fra et glidende gennemsnit af dataene relateret til drift af køleapparatet (1) i den anden periode, og

den estimerede værdi for kølemiddeltemperaturen på udledningssiden af kompressoren (11) beregnes for hver strømkildefrekvens og strømkildespænding for en strømkilde, der er en strømkilde, der leveres til køleapparatet (1), ved anvendelse af en regressionsanalyse, hvor en variabel for regressionsanalysen er mindst én af en kondensationstemperatur, en fordampningstemperatur, en åbningsgrad af en ekspansionsventil (14A, 14B), der er dekompressionsanordningen, en driftsfrekvens for kompressoren (11) eller en rotationshastighed for kompressoren (11), når en mængde kølemiddel indeholdt i kølemiddelkredsløbet (20) er inden for en passende værdimængde.

DRAWINGS

Fig.1

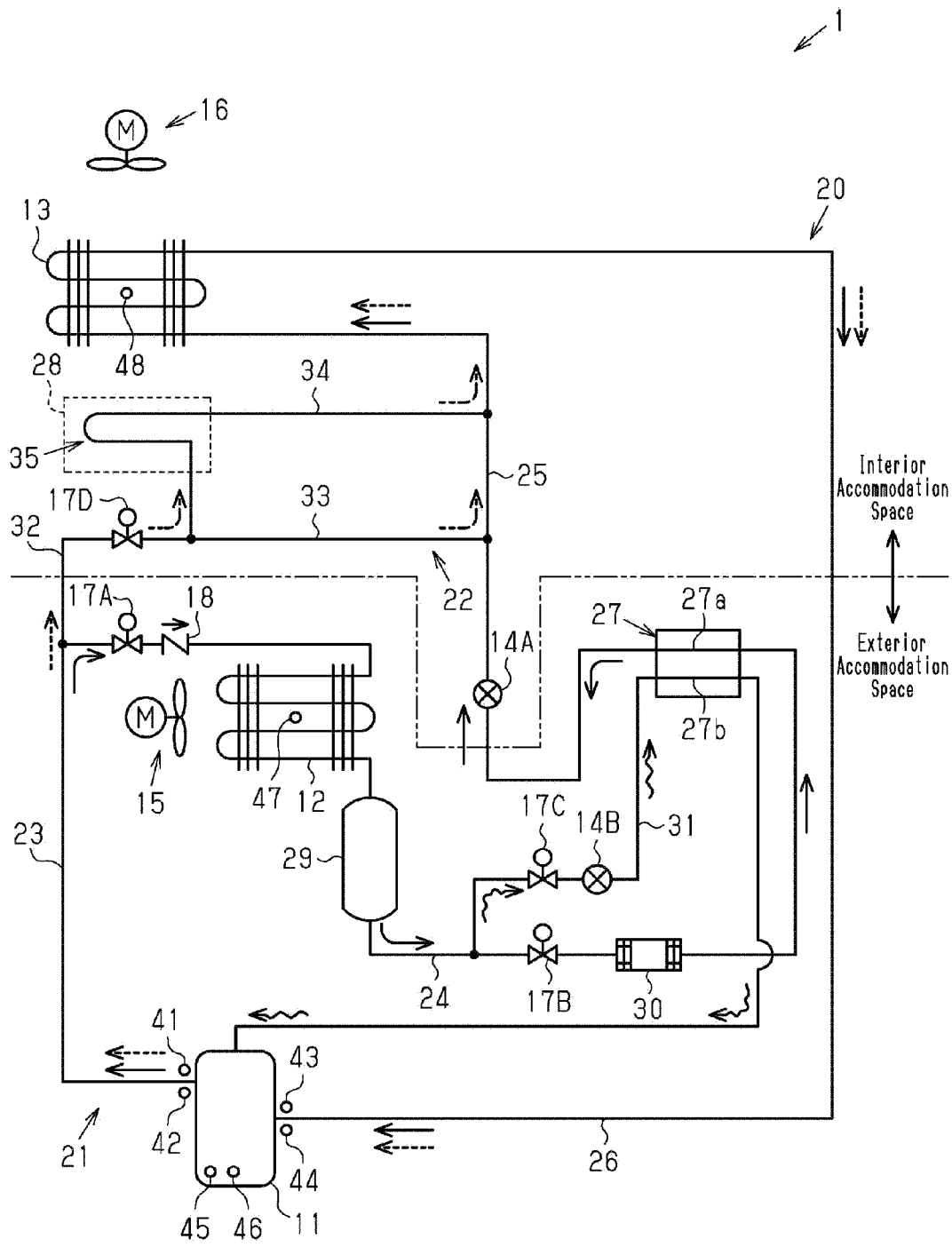


Fig.2

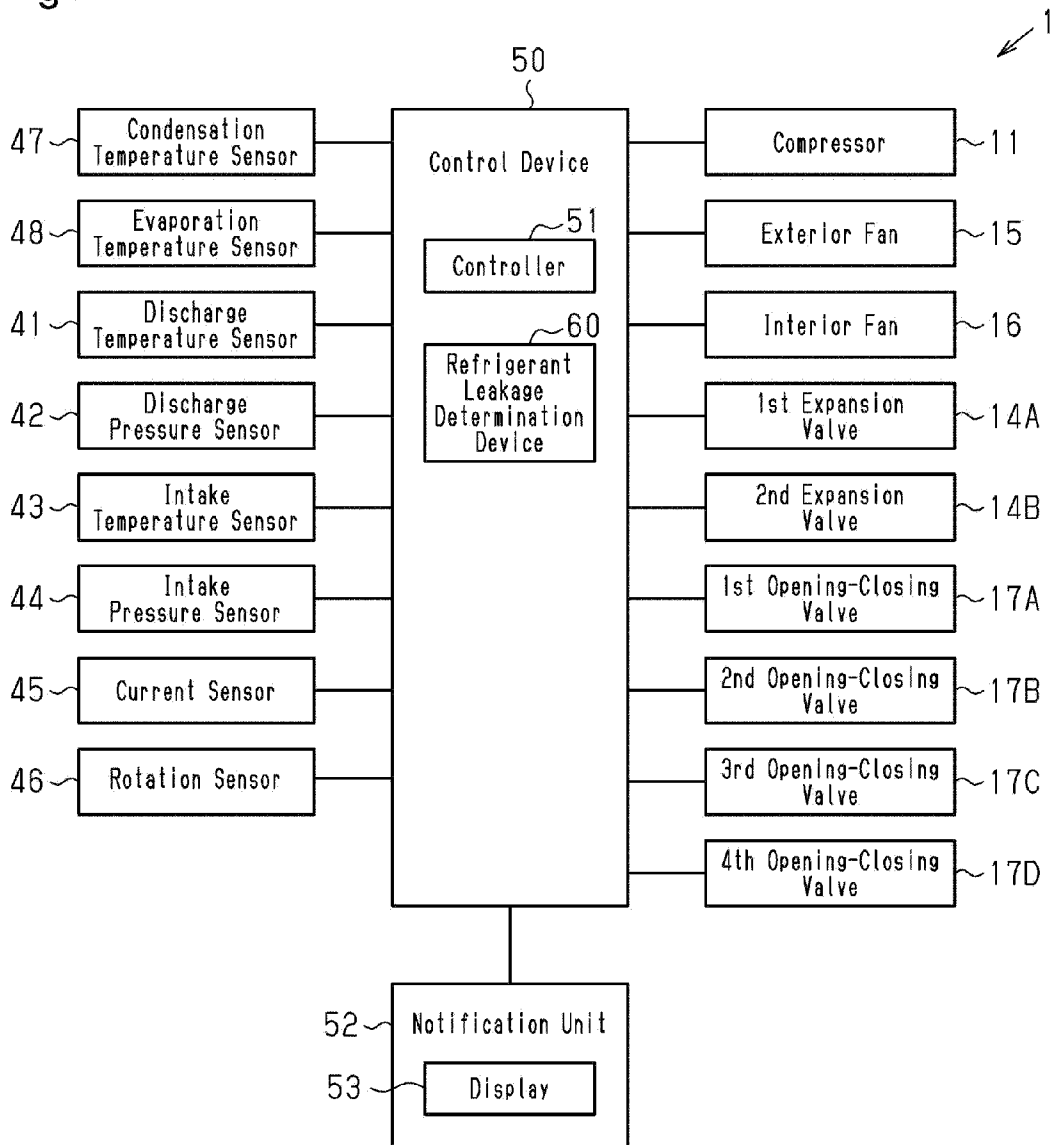


Fig.3

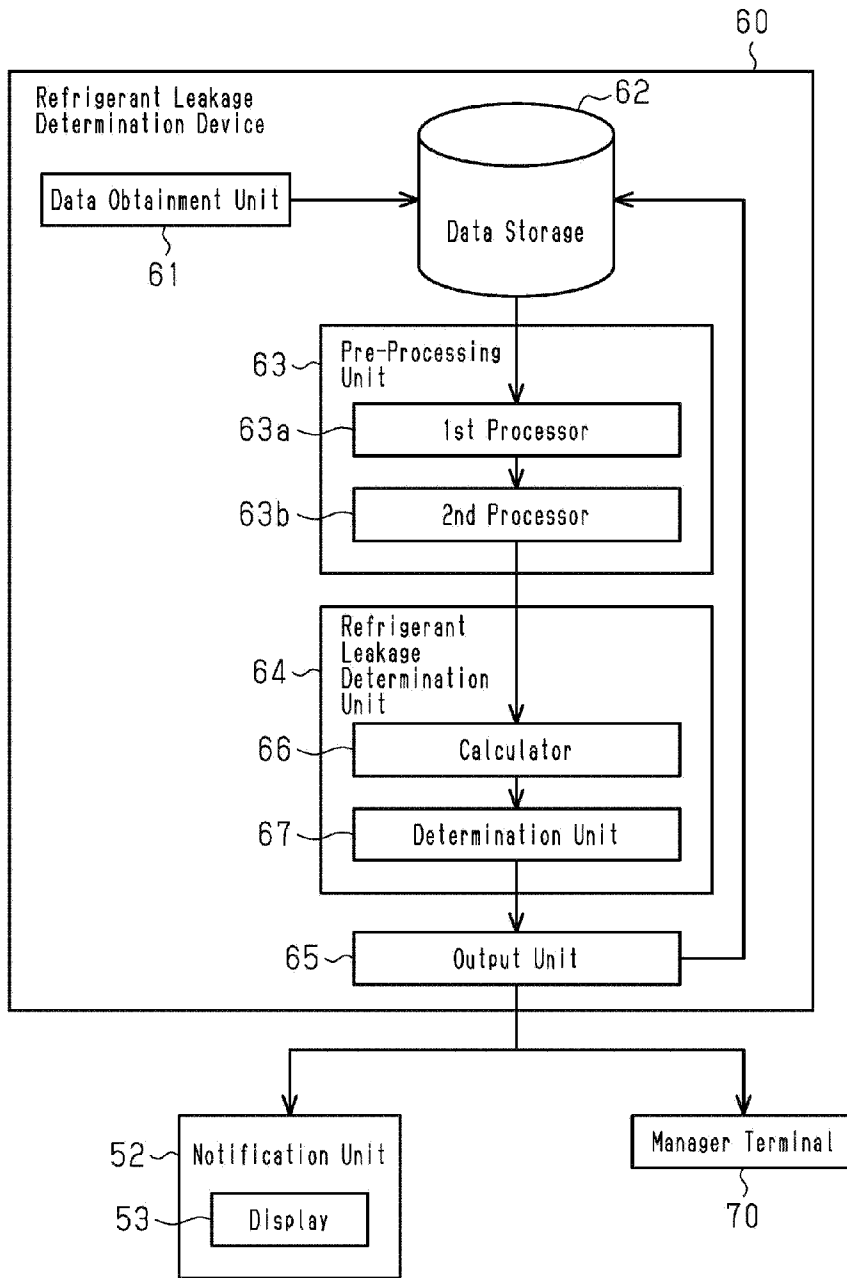


Fig.4A

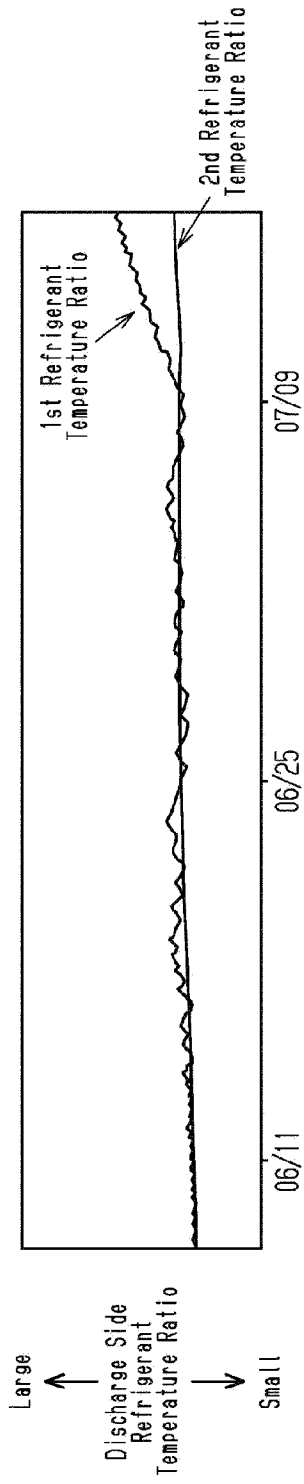


Fig.4B

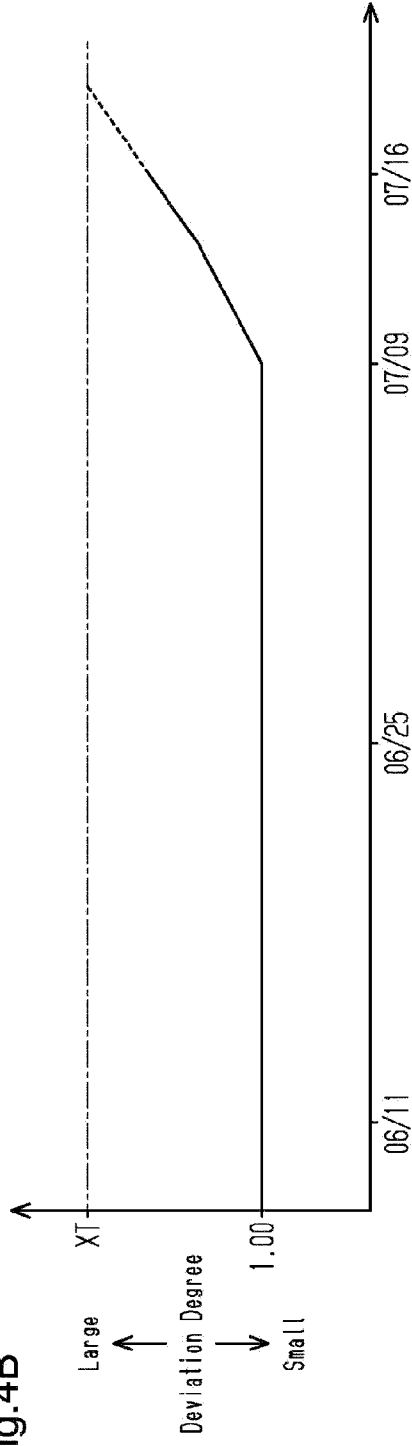


Fig.5

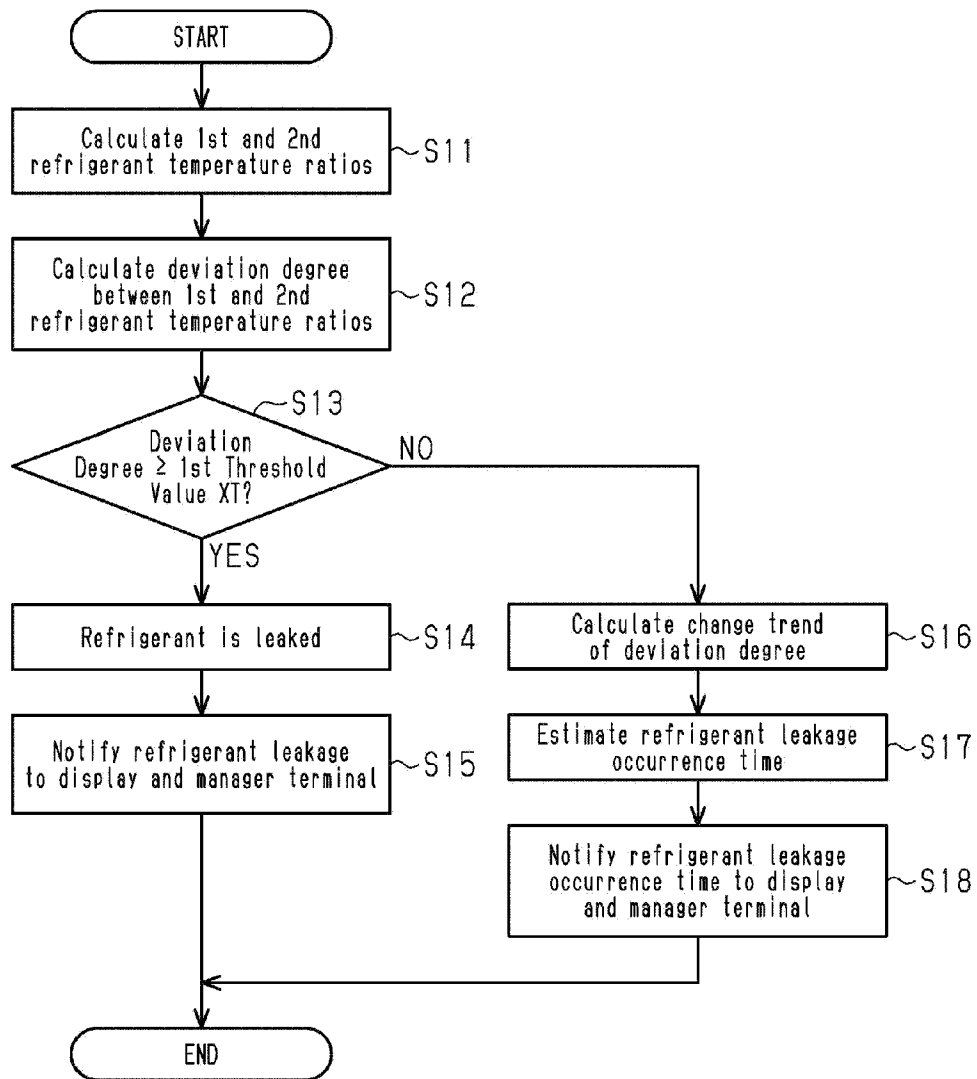


Fig.6

