



INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

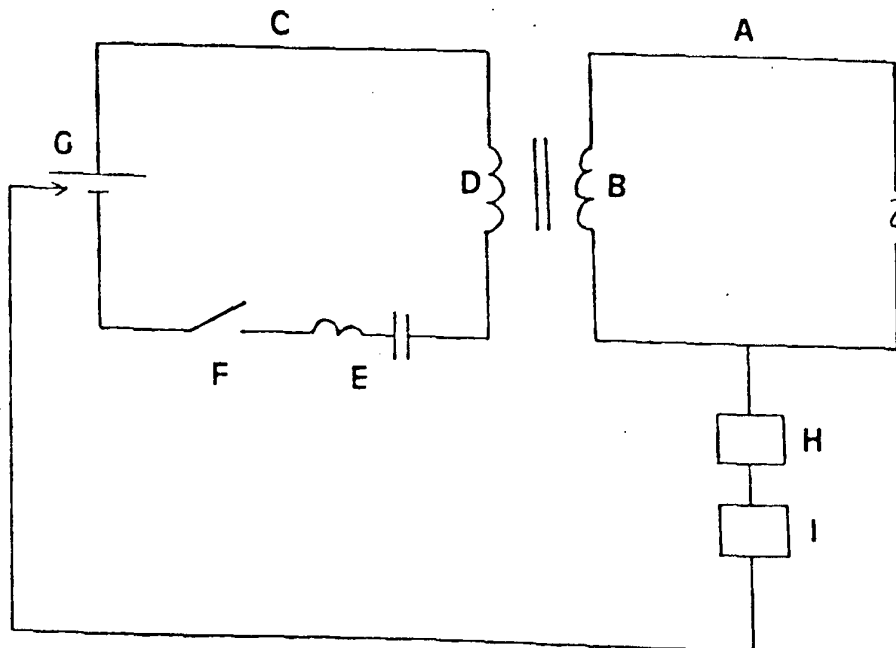
(51) International Patent Classification ⁶ : H02J 3/18, G05F 1/70	A1	(11) International Publication Number: WO 95/05697 (43) International Publication Date: 23 February 1995 (23.02.95)
(21) International Application Number: PCT/SE94/00341 (22) International Filing Date: 15 April 1994 (15.04.94) (30) Priority Data: 9302632-6 13 August 1993 (13.08.93) SE (71)(72) Applicant and Inventor: NYGREN, Peter [SE/ES]; Calle Andorra 3, 3C, E-28043 Madrid (ES). (74) Agent: NYGREN, Börje; Doktor Allards gata 51, S-413 24 Göteborg (SE).	(81) Designated States: AT, AU, BB, BG, BR, BY, CA, CH, CZ, DE, DK, ES, FI, GB, HU, JP, KP, KR, KZ, LK, LU, MG, MN, MW, NL, NO, NZ, PL, PT, RO, RU, SD, SE, SK, UA, US, VN. Published <i>With international search report.</i> <i>With amended claims.</i> <i>In English translation (filed in Swedish).</i>	

(54) Title: DEVICE FOR COMPENSATION OF REACTIVE POWER IN ELECTRICAL SYSTEMS

(57) Abstract

The invention relates to a device for compensation of reactive (inductive) power in a.c. circuits. The inductive power, which is caused by autoinduction = an inertia when the electrons are accelerated, is a problem which limits the useful power that can be transmitted in a.c. networks. Normally the problem is solved by compensation with capacitors or idling rotating machines. The invention solves the problem by connecting a transformer to the primary circuit. The secondary winding of the transformer is fed with a d.c. voltage during the first half of every half cycle of the primary current. A resonance circuit controls the rise of the d.c. current which induces a magnetic energy in the

primary circuit which compensates the autoinductance. The device is regulated automatically and infinitely variably by a regulator which is connected to a power factor (cos ϕ) meter. The interruption of the secondary circuit can be made by a mechanical breaker, by thyristors or by a static frequency converter. In an alternative design the secondary circuit consists of an extra winding in a normal power transformer.



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1. Denomination: Device for compensation of reactive power in electrical systems.

2. The invention relates to a device according to the precharacterizing part of claim 1 and consists of an apparatus which is connected to an electrical system and which permits a simple and infinitely variable compensation of reactive power.

3. It is well known that reactive power is a problem which limits the transmission capacity in electrical a.c. systems and also creates harmonics.

Normally the reactive power is inductive and caused by autoinduction and induction in conductors and coils in for example motors and transformers.

Today three methods are used to compensate the reactive power:

I. Statically connected capacitor banks.

Advantages: Low costs and low losses.

Disadvantages: No possibility of control, dangerous (risk for discharge)

II. Thyristor controlled capacitor banks.

Advantages: As above + possibility of control

Disadvantages: Expensive and complicated

III. Idling over/under magnetized d.c. magnetized synchronous machines.

Advantage: Possibility of simple control

Disadvantages: Expensive, only economically justified for very high voltages, maintenance needed, and cannot be placed anywhere.

Thus, there is a need for a simple, cheap and safe apparatus which can be regulated actively and placed anywhere.

THEORY

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Let us look at how reactive power arises.

Symbols: R resistance, U voltage, I current, L inductance, U_L inductive voltage, U_R resistive voltage, U_C capacitive voltage, C capacitance, U_e total applied voltage, Z impedance, φ phase angle, ω angular frequency, a acceleration, e^- electron

I. Resistive circuit with voltage stiff source.

See figure 1

$$U_e = U_{e0} \sin \omega t$$

$$Z = R \Rightarrow I_0 = U_{e0}/Z = U_{e0}/R$$

Current and voltage are in phase.

II. Inductive circuit.

See figure 2

Current and voltage are phase shifted with the angle ν .

$$Z = \sqrt{R^2 + \omega^2 L^2} \quad I_o = U_{eo} / \sqrt{R^2 + \omega^2 L^2}$$

III. Capacitive circuit.

See figure 3

Current and voltage are phase shifted with the angle ν .

Transmitted power $P = U_{eo} I_o$

In the cases II and III the current amplitude I_o decreases which gives a lower transmitted power P if the applied voltage U_{eo} is kept constant since the total countervoltage increases.

The objective is to compensate L and C so that the angle ν is as close to zero as possible so that the current reaches its maximum value.

A normal goal is to achieve a power factor ($\cos \nu$) of 0,9.

But what does ACTUALLY happen in the circuit? Why does the current decrease, i.e. the flow of the electrons?

To understand in depth what is happening in an electrical circuit, causes and effects in the movements of the electrons must be observed.

Inductance and capacitance are internal inertias in the system which affect the movements of the electrons.

Autoinductance:

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See figure 4

The generator pulls up and accelerates electrons from earth. The electron b is accelerated due to the repulsion from a but it is at the same time counteracted by the repulsion from c as well as by its own mass inertia. This chain of inertias is identical to the magnetism which is caused by the autoinductance.

All magnetism is caused by such relative movement and interaction between individual electrons.

In an electrical conductor: An a.c. current causes a variable magnetic field which is identical to the inertias above.

In a coil: The inertias, i.e. the magnetic field, is amplified since the electrons affect each other between the windings.

See figure 5

The inductive inertia (= the inductive voltage) has its maximum value 90 degrees phase shifted in relation to the current (which is parallel to the resistive voltage) since the acceleration reaches its maximum when the velocity reaches its minimum or: Acceleration = dI/dt and the acceleration reaches its maximum when the current curve reaches its maximum inclination which is in the point when the current curve passes zero.

Capacitance:
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When a capacitor is exposed to an a.c. voltage the following inertia arises:

Step 1:

See figure 6

Step 2: The polarity is reversed

See figure 7

Precisely when the polarity is reversed, the electrons rush in/out from the plates.

Step 3: When the lower of the plates is filled with electrones, the electrostatic repulsion counteracts the current (like a spring that is tightened)

See figure 8

Finally, this repulsion hinders completely the current.

See figure 9.

We can here make two interesting observations:

1. When U_c and I have opposite directions, the capacitor gives an "extra pull" to the current (electrons rush in/out when the polarity is reversed).

Observe that voltage = inertia against the movements of the electrons. Current is, as is well known, defined in opposite direction to the real direction of movement of the electrons.

2. When the current peak is passed, U_c counteracts the current.

We also see that the inertia of the capacitor is in 180 degrees counterphase to the inductance.

See figure 10

The following example shows that the two inertias have opposite directions:

Step 1: At polarity reversion

See figure 11

The remaining excess charge in the capacitor plates gives an "extra pull", U_c , which counteracts the inductive inertia.

Step 2: Then, when the right plate begins to be filled with electrons, the inertia of the capacitor manifests itself and counteracts the current.

The phenomenon can be compared with building up potential energy in a cause-effect chain which limits the current amplitude. Observe that no energy is consumed!

In an inductive or capacitive system, the total countervoltage increases compared to a purely resistive system. The extra pull and inertia cause the phase shift.

Compensated system i.e. $U_c = U_l$

See figure 12

- 1) Extra pull due to the discharge of the capacitor
- 2) Counteraction due to the inductive inertia
- 3) The inductive inertia gives an extra pull, counteracts the negative acceleration
- 4) The capacitor counteracts the current when it begins to be saturated.

We see that U_c and U_l compensate each other and the resulting voltage becomes purely resistive and in phase with the current.

Uncompensated systems: One of the inertias U_c or U_l prevails and the resulting voltage is phase shifted and the current amplitude decreases.

Conclusion: We see that the reactive power is equal to inertias which affect the electrons when they are accelerated and which limit the flow (= current) and that the inductance and capacitance counteract each other since they have opposite directions (they can therefore cause internal resonances in the system).

The actual location of coils and capacitors is of less importance since it is the resulting resonance mode of the system that is affected.

We can also state that the most common method to compensate an inductive circuit is to, in this way, introduce a capacitance.

Compare with idling overmagnetized synchronous machines which induce an EMF in counterphase to the inductive phase voltage.

4. The purpose of the invention is to compensate an inductive circuit, i.e. to eliminate the inductive inertia and thereby eliminate the reactive power and maximize the current amplitude but without using capacitors or idling rotating machines.

5. The invention constitutes a solution to this problem.

6. The solution is described in the characterizing part of claim 1.

7. One possible design of the invention is shown schematically in attached drawing.

Figure 13 shows the main components of the invention.

Legend of figure 13:

A = primary circuit which shall be compensated

B = coil connected in series with the primary circuit

C = secondary circuit which produces the compensation

D = coil connected in series with the secondary circuit, magnetically connected with coil B

E = resonance circuit

F = rotating breaker

G = d.c. voltage source

H = cos ϕ meter

I = regulator

The figure is repeated per phase!

8. According to figure 13, a coil is connected in series with the primary circuit. This coil is magnetically connected to another coil (through an iron core) which is connected in series with the secondary circuit (i.e. a transformer).

The secondary circuit is fed by a d.c. voltage source (this is important - otherwise the reactive power would just be transferred from the primary circuit to the secondary circuit) which is regulated by the cos ϕ meter and the regulator.

The voltage of the secondary circuit is switched on and off in the right moment by the rotating breaker and the rise of the secondary current is controlled by the resonance circuit.

The interruption can also be made by thyristors or by a static frequency converter with a d.c. link (the frequency converter then replaces both the d.c. voltage source and the rotating breaker).

In another design the secondary circuit consists of an extra winding in a normal power transformer.

9. The device functions in the following way:

We assume that the primary circuit which shall be compensated is inductive. The purpose of the invention is to apply a force on the electrons in opposite direction to the inductive inertia and thereby achieve an extra pull precisely like from a capacitor.

The rotating breaker is designed in such a way that the secondary current is switched on when the primary current passes zero. Thanks to the resonance circuit a suitable rise is obtained for the secondary current which induces a magnetic field in the secondary coil. This magnetic field is transferred to the primary coil and through the chosen current direction in the secondary circuit, an EMF and a current are induced in the primary circuit which give the necessary extra pull on the electrons. This induced current avoids the autoinductance.

Let us consider the following dimensioning example:

We assume that the primary circuit has the following characteristics:

See figure 14

Assume that the phase angle is 52 degrees i.e. the power factor, $\cos \phi_i = 0,6$

$$U_e = 5 \text{ kV} = U_{e0} \sin \omega t$$

$$I = I_0 \sin (\omega t - \phi_i)$$

See figure 15

$$\tan \phi_i = X/R \Rightarrow X = R \tan \phi_i = 50 * 1,3 = 65 \text{ ohm}$$

$$I = U_e/Z = U_e/\sqrt{X^2 + R^2} = 61 \text{ A}$$

$$L = X/\omega = 0,2 \text{ H}$$

$$P \text{ reactive} = XI^2 = 65 * 61^2 = 242 \text{ kVar}$$

Compare with a purely resistive load (without reactance X):

$$I = U_e/R = 5000/50 = 100 \text{ A}$$

Thus, we have "lost" an electron flow of $100 - 61 = 39 \text{ A}$ due to the autoinduction i.e. the inertia of the electrons.

The magnetic energy which is "stored" in the primary circuit due to the autoinduction is:

$$E = 0,5 * LI^2 = 0,5 * 0,2 * 61^2 = 372 \text{ J}$$

This means that we must add 372 Joule to the primary circuit from the secondary circuit during the first half of the first half cycle of the current through the induced current as extra pull to counteract the autoinduction.

On the other hand, we recover this energy during the second half of the first half cycle thanks to the extra pull of the inductance (see diagram above). The total energy change in the whole system is thus zero. The only extra energy that has to be added is to overcome resistive losses.

If we assume that the secondary circuit has the same autoinductance as the primary circuit, the same current of 61 A must be created in the secondary circuit which gives energy balance.

Losses in the secondary circuit: (Assume the resistance 1 ohm)

$$P = RI^2/2 = 1860 \text{ W} = 0,8 \% \text{ of the reactive power.}$$

Thus, we apply 61 A in the secondary circuit during the first half of every half cycle of the current, but this energy is recovered during the second half of every half cycle in the primary circuit.

The resonance circuit creates a suitable rise of the current with a duration of one quarter of a cycle.

Unfortunately, a current I' is also induced in the secondary circuit (in the same direction as I_2) due to the superposition principle, which has to be taken into consideration in the dimensioning (especially the losses).

See figure 16

10. Claims

1. Device for infinitely variable and self-regulating compensation of reactive (inductive) power in electrical a.c. circuits

c h a r a c t e r i z e d i n

that the apparatus consists of two circuits, the primary circuit which shall be compensated and a secondary circuit fed by a d.c. voltage source

that the two circuits are magnetically connected in a transformer

that the d.c. voltage is regulated by a regulator connected to a power factor ($\cos \phi$) meter

that the d.c. voltage is switched on during the first half of every half cycle of the primary current

that the rise of the secondary current during the first half of every half cycle is controlled by a resonance circuit

that the secondary circuit induces a current in the primary circuit in the same direction as the primary current.

2. Device according to claim 1 c h a r a c t e r i z e d i n

that the secondary circuit is interrupted by a rotating mechanical breaker which is synchronized with the frequency of the net

3. Device according to claim 1 c h a r a c t e r i z e d i n

that the secondary circuit is interrupted by a static breaker (power electronics, eg a thyristor) which is synchronized with the frequency of the net

4. Device according to claim 1 c h a r a c t e r i z e d i n

that the d.c. voltage source and breaker of the secondary circuit consist of a static frequency converter with a d.c voltage link

5. Device according to claim 1 c h a r a c t e r i z e d i n

that the secondary circuit consists of an extra winding in a normal power transformer

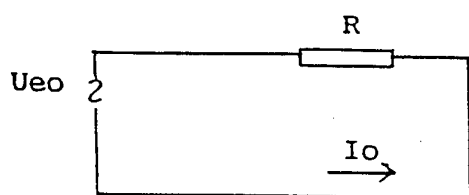
AMENDED CLAIMS

[received by the International Bureau on 29 December 1994 (29.12.94);
new claim 6 added; remaining claims unchanged (1 page)]

6. Device according to claim 1 c h a r a c t e r i z e d i n

that the compensation is regulated by controlling the length of the dc current pulse (i.e. controlling the moments of switching on and off the dc current) instead of regulating the applied dc voltage.

Figure 1



Phase diagram:

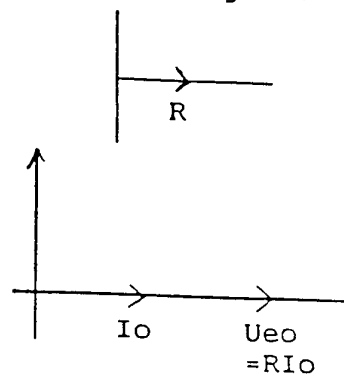


Figure 2

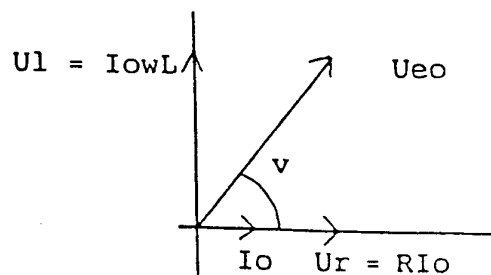
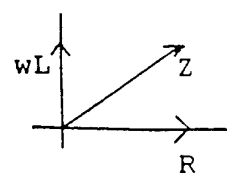
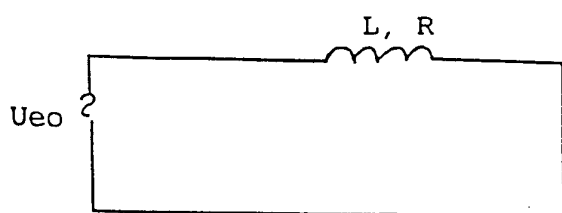


Figure 3

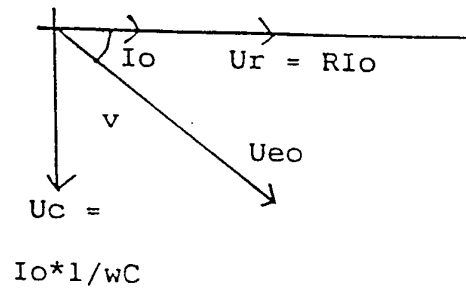
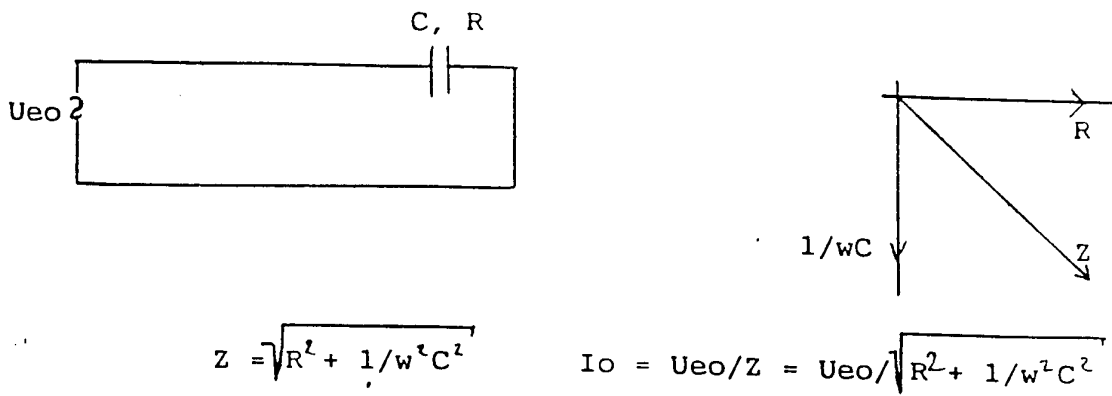


Figure 4

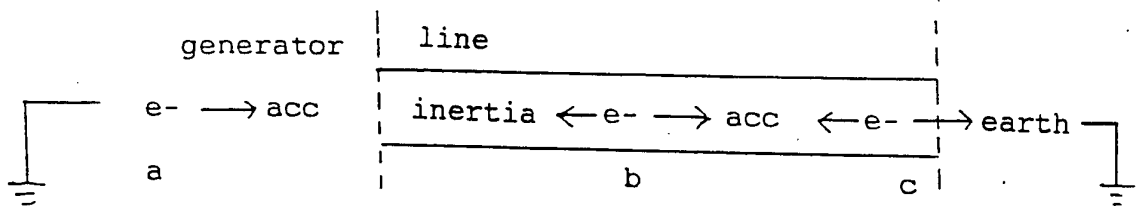


Figure 5

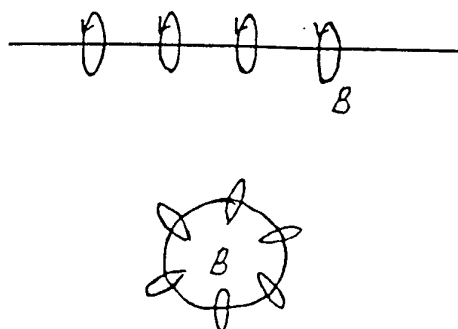


Figure 6

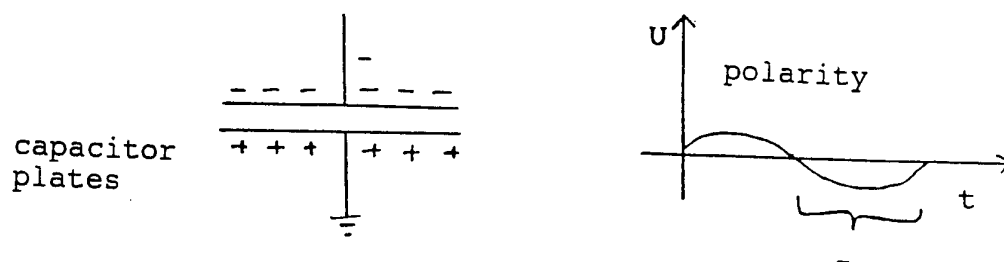


Figure 7

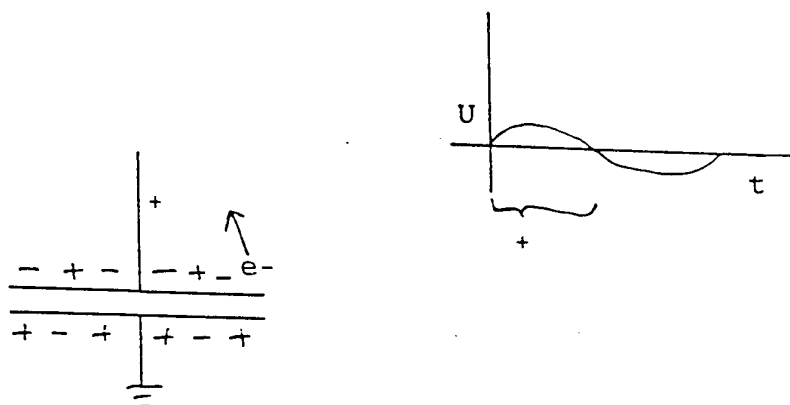


Figure 8

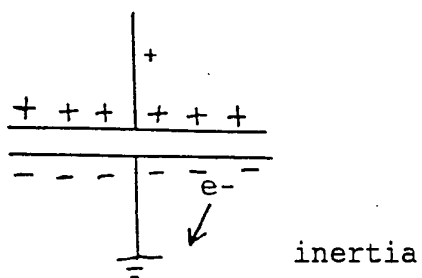


Figure 9

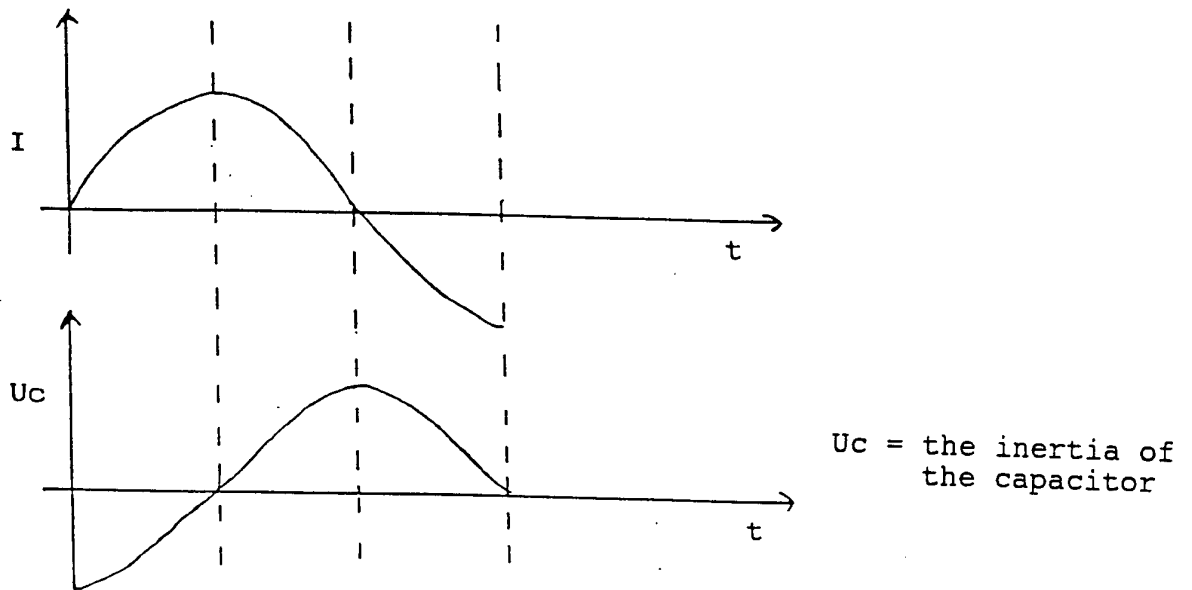
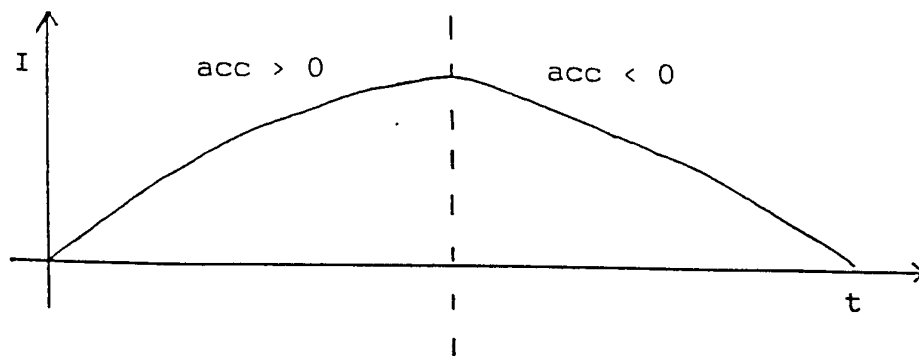


Figure 10



the inductance
counteracts
("takes energy
from the net")

the inductance
helps
("returns energy
to the net")

the capacitance
helps

the capacitance
counteracts

Figure 11

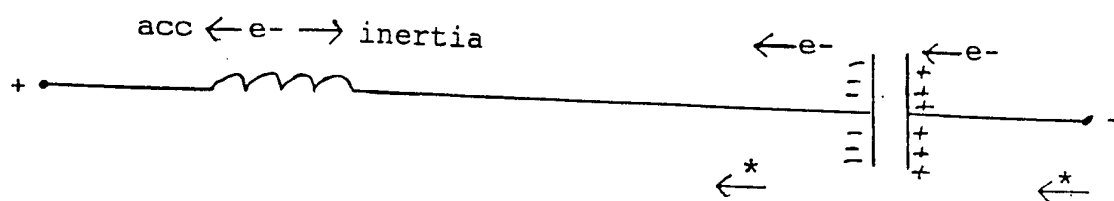


Figure 12

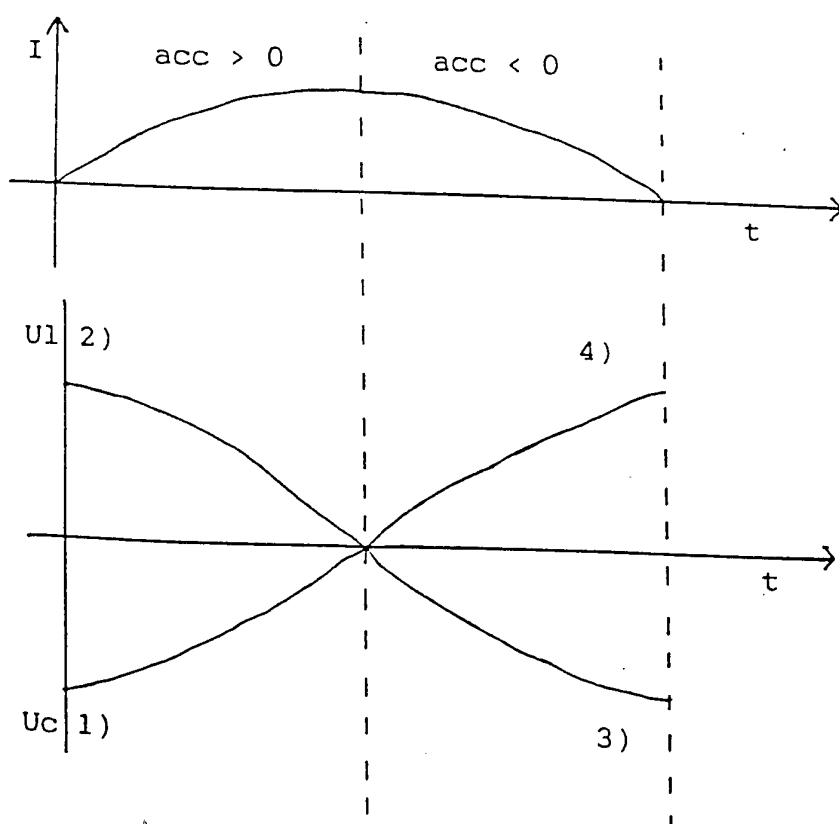


Figure 13

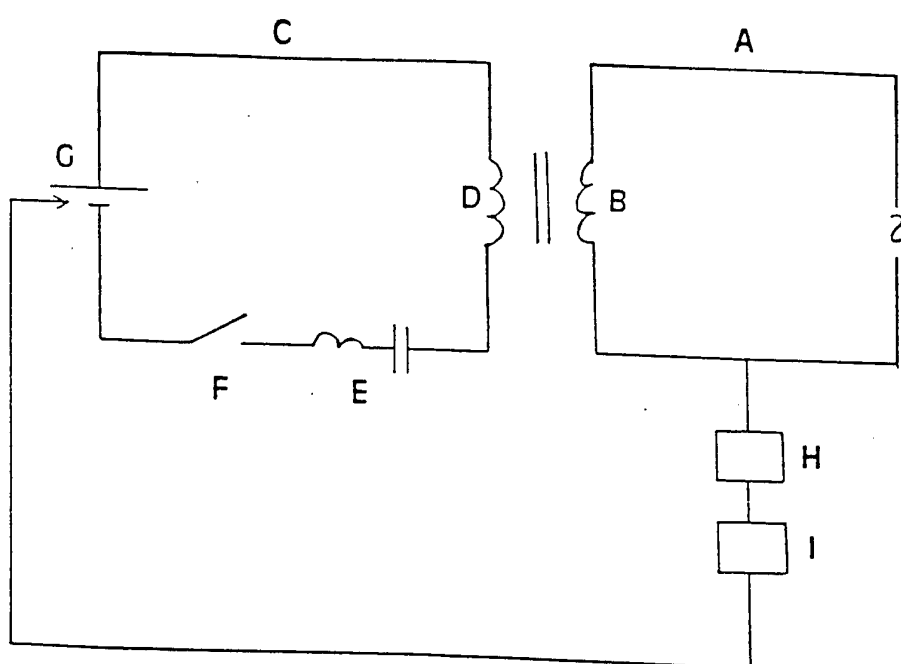


Figure 14

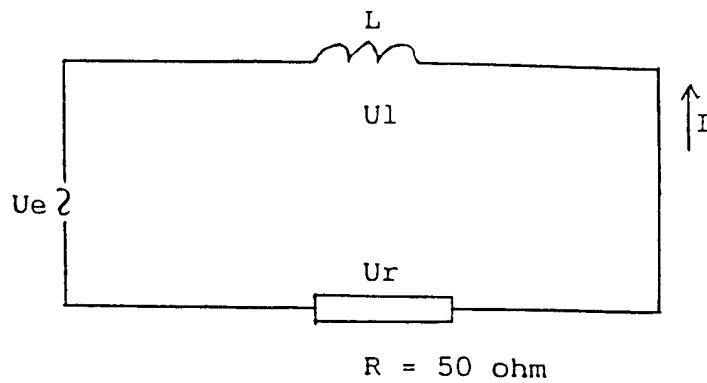


Figure 15

Phase diagram:

(X = reactance)

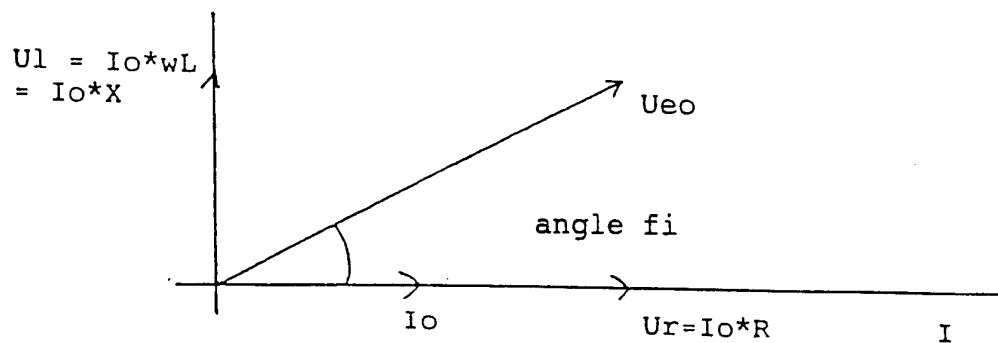
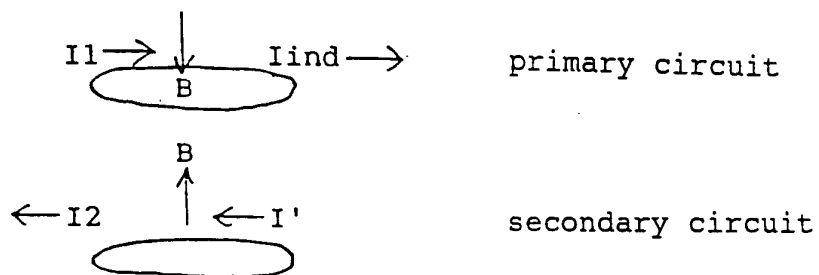


Figure 16



INTERNATIONAL SEARCH REPORT

International application No.

PCT/SE 94/00341

A. CLASSIFICATION OF SUBJECT MATTER		
IPC6: H02J 3/18, G05F 1/70 According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED		
Minimum documentation searched (classification system followed by classification symbols)		
IPC6: H02J, G05F		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
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Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US, A, 4914375 (T. HATANAKA), 3 April 1990 (03.04.90), column 1, line 60 - column 2, line 45 --	1
A	EP, A1, 0440988 (ASEA BROWN BOVERI AB), 14 August 1991 (14.08.91), column 1, line 4 - line 22; column 4, line 13 - column 5, line 56 --	1
A	US, A, 5032738 (JOHN J. VITHAYATHIL), 16 July 1991 (16.07.91), column 3, line 25 - column 4, line 36 --	1
☒ Further documents are listed in the continuation of Box C. ☒ See patent family annex.		
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Date of the actual completion of the international search		Date of mailing of the international search report
17 November 1994		23 - 11 - 1994
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C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	DE, A1, 4238892 (MOTTAGHIAN-MILANI, DARIUS-KARIM), 1 April 1993 (01.04.93), column 1, line 65 - column 3, line 30 --	1
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INTERNATIONAL SEARCH REPORT
Information on patent family members

01/10/94

International application No.

PCT/SE 94/00341

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US-A- 5032738	16/07/91	AU-A- 7026987 DE-D,T- 3787335 EP-A,B- 0258314 SE-T3- 0258314 WO-A- 8704538	14/08/87 05/01/94 09/03/88 30/07/87
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