



(51) International Patent Classification:

F02G 1/055 (2006.01) *F02G 5/02* (2006.01)
F01K 23/10 (2006.01) *F28D 20/02* (2006.01)
F02C 6/18 (2006.01)

(21) International Application Number:

PCT/SG2016/050446

(22) International Filing Date:

15 September 2016 (15.09.2016)

(25) Filing Language:

English

(26) Publication Language:

English

(30) Priority Data:

10201507652V 15 September 2015 (15.09.2015) SG

(71) Applicant: NANYANG TECHNOLOGICAL UNIVERSITY [SG/SG]; 50 Nanyang Avenue, Singapore 639798 (SG).

(72) Inventors: **DUAN, Fei**; c/o Nanyang Technological University, 50 Nanyang Avenue, Singapore 639798 (SG). **DUBEY, Swapnil**; c/o Nanyang Technological University, 50 Nanyang Avenue, Singapore 639798 (SG). **CHOO, Fook Hoong**; c/o Nanyang Technological University, 50 Nanyang Avenue, Singapore 639798 (SG). **QIU, Lu**; c/o Nanyang Technological University, 50 Nanyang Avenue, Singapore 639798 (SG). **WANG, Kai**; c/o Nanyang Technological University, 50 Nanyang Avenue, Singapore 639798 (SG).

(74) Agent: **ONG, Lucille Frances, Kheng Lu**; Marks & Clerk Singapore LLP, Tanjong Pagar, P O Box 636, Singapore 910816 (SG).

(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BN, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IR, IS, JP, KE, KG, KN, KP, KR, KW, KZ, LA, LC, LK, LR, LS, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PA, PE, PG, PH, PL, PT, QA, RO, RS, RU, RW, SA, SC, SD, SE, SG, SK, SL, SM, ST, SV, SY, TH, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LR, LS, MW, MZ, NA, RW, SD, SL, ST, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, RU, TJ, TM), European (AL, AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MK, MT, NL, NO, PL, PT, RO, RS, SE, SI, SK, SM, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, KM, ML, MR, NE, SN, TD, TG).

Declarations under Rule 4.17:

— of inventorship (Rule 4.17(iv))

[Continued on next page]

(54) Title: POWER GENERATION SYSTEM AND METHOD

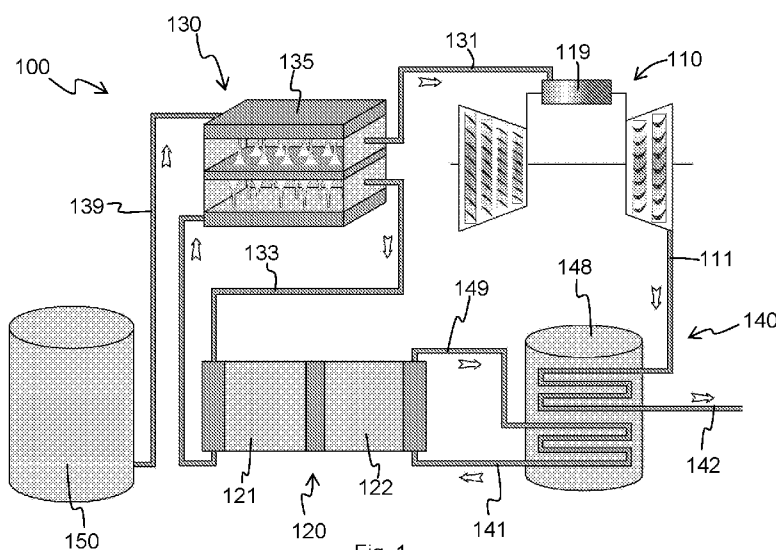


Fig. 1

(57) Abstract: A power generation system comprising: a liquefied natural gas (LNG) regasification unit configured to perform a re-gasification process to regasify LNG supplied from an LNG source to produce natural gas, the regasification process producing cold energy; a gas turbine configured to combust the natural gas to output power, the combusting producing an exhaust gas; a thermal storage unit configured to store heat obtained from the exhaust gas; and a Stirling engine configured to output power, the Stirling engine having a hot end heated by the heat stored in the thermal storage unit and a cold end cooled by the cold energy from the regasification process.



Published:

— *with international search report (Art. 21(3))*

POWER GENERATION SYSTEM AND METHOD

FIELD

This invention relates to a power generation system and method, and in particular to a power generation system and method fueled by liquefied natural gas.

5

BACKGROUND

Compared with traditional long-carbon-chain fossil fuels, natural gas has high reserves, a higher energy density, and does not contain sulphur. Natural gas fuel can produce remarkably lower emissions. It produces the lowest level of CO₂ in all hydrocarbon fuels.

10 Compared to traditional fossil fuels, natural gas reduces benzene emissions by 97%, NO_x emissions by 80%, carbon monoxide (CO) emissions by 76%, and CO₂ emissions by 22%. The use of nature gas does not produce lead, sulphur emissions, or particulate matters. When natural gas is cooled to a temperature of approximately -162 °C at atmospheric pressure, it condenses into liquefied natural gas (LNG). Since the density of LNG is 460
15 kg/m³, the volume of LNG takes up approximately 1/600 that of natural gas. LNG is an odourless, colourless, non-corrosive, and non-toxic liquid. The unit volume reduction dramatically eases its transport. The liquefaction process of natural gas removes O₂, CO₂, SO_x, and water vapor. In addition, the lower fuel cost per unit mass of LNG becomes less in comparison with the traditional fossil fuels; LNG, mainly made up of paraffinic
20 compounds, results in the combustion efficiency higher than that of traditional fossil fuels. Therefore, LNG is a promising fuel in the market of power generation.

Although LNG is convenient to transport and store with a specific volume compared with the gas phase, it is necessary to regasify LNG before combustion can take place in a gas
25 turbine for stationary power generation. A large amount of cold energy can be produced during the regasification process while exhaust gas from combustion of regasified LNG in the gas turbine contains abundant low-temperature thermal energy.

Various LNG regasification systems have been disclosed, as well as systems to generate
30 energy or power using the cold energy produced during LNG regasification. However, efficiency in regasification and power generation is still not optimized in any of the known systems, and can be further improved.

SUMMARY

The present application discloses a power generation system fuelled by LNG to recover exhaust thermal energy and cold energy from LNG regasification simultaneously with one single Stirling engine.

5

The power generation system uses LNG (or any liquid combustible gas) for gas turbine power generation after regasification of LNG, and applies cold energy from the LNG regasification and hot energy of exhaust gas from the gas turbine to drive a Stirling engine. A thermal storage system based on phase change materials (PCMs) is used to store the exhaust heat, stabilize the temperature of the exhaust gas and supply heat to a hot end of the Stirling engine.

10

The advantage of this is that a higher thermal efficiency is anticipated due to the large temperature differences between the hot end and cold end. The system provides a high efficient, highly integrated, and stable combined power generation system from LNG by comprehensive utilization of energies stored in LNG, including chemical energy, cold energy, and exhaust heat after combustion.

15

According to a first aspect, there is provided a power generation system comprising: a liquefied natural gas (LNG) regasification unit configured to perform a regasification process to regasify LNG supplied from an LNG source to produce natural gas, the regasification process producing cold energy; a gas turbine configured to combust the natural gas to output power, the combusting producing an exhaust gas; a thermal storage unit configured to store heat obtained from the exhaust gas; and a Stirling engine configured to output power, the Stirling engine having a hot end heated by the heat stored in the thermal storage unit and a cold end cooled by the cold energy from the regasification process.

20

25

The thermal storage unit may comprise at least one phase change material.

30

The thermal storage unit may be embedded with the hot end of the Stirling engine.

A heat exchanger of the regasification unit may be embedded with the cold end of the

Stirling engine.

According to a second aspect, there is provided a method of power generation, the method comprising the steps of:

- 5 (a) regasifying LNG in a regasification process to produce natural gas, the regasification process producing cold energy;
- (b) combusting the natural gas in a gas turbine to output power, the combusting producing an exhaust gas;
- (c) storing heat obtained from the exhaust gas in a thermal storage unit; and
- 10 (d) heating a hot end of a Stirling engine with the heat stored in the thermal storage unit and cooling a cold end of the Stirling engine with cold energy from the regasification process to output power with the Stirling engine.

15 Storing the heat may comprise storing the heat in at least one phase change material in the thermal storage unit.

The method may further comprise directly spraying the cold end of the Stirling engine with LNG.

20 BRIEF DESCRIPTION OF FIGURES

In order that the invention may be fully understood and readily put into practical effect there shall now be described by way of non-limitative example only exemplary embodiments of the present invention, the description being with reference to the accompanying illustrative drawings.

25 Fig. 1 is a schematic illustration of a power generation system.

Fig. 2 is a flow chart of a method of power generation.

DETAILED DESCRIPTION

30 Exemplary embodiments of the power generation system 100 will be described below with reference to Figs. 1 and 2. The same reference numerals are used throughout the figures to denote the same or similar parts among the various embodiments.

The power generation system 100 is a liquid natural gas (LNG) fuel based co-generation

system 100 which comprises two engines: gas turbine engine 110 and a Stirling engine 120. In one embodiment, the gas turbine may be a 30kW turbine while the Stirling engine 120 may be a 3kW engine. However, the outputs of the gas turbine and the Stirling engine could be up to 100MW and 10MW after scaling up.

5

The Stirling engine 120 utilizes a known Stirling cycle for outputting mechanical work as a net conversion of heat energy from cyclic compression and expansion of a fixed mass of gas under different temperatures. The Stirling engine 120 has a cold end 121 and a hot end 122, between which the fixed mass of gas in the Stirling engine is allowed to move. At the
10 hot end 122, the gas expands because its temperature rises due to external heat applied to the hot end 122. Expansion of the gas does work which is the output of the Stirling engine. This work is typically in the form of movement of an output piston that is moved by the gas expanding against it. Momentum obtained from the output is harnessed to compress the expanded gas. Compression of the gas increases its temperature, so cold energy is
15 externally applied to the cold end 121 to remove heat generated by the compression. The compressed gas is once again expanded by heating at the hot end 122 to repeat the work cycle.

The gas turbine 110 consumes natural gas 131 as the fuel which is regasified from LNG
20 139 in a LNG regasification unit 130, and discharges high temperature exhaust gas 111. The LNG regasification unit 130 may be a double impingement unit, and is supplied with LNG 139 from an LNG storage tank 150. The power generation system 100 also includes a thermal storage system 140 on the basis of PCMs. The Stirling engine 120 is used to recover cold energy 132 from the LNG regasification process 130 and the heat energy in
25 the exhaust gas 111 from the gas turbine 110, simultaneously. The cold energy 132 is applied to the cold end 121 of the Stirling engine 120 to remove heat generated by compression of the gas in the Stirling engine 120, while the heat energy in the exhaust gas 111 is applied to the hot end 122 of the Stirling engine to heat and thereby expand the gas in the Stirling engine 120.

30

A schematic illustration of the power generation system 100 is shown in Fig. 1. The first power generation subsystem 110 is the gas turbine 110. Natural gas 131, which is regasified from LNG 139 in the LNG regasification unit 130, is pumped into a combustor

119 of the gas turbine 110. The natural gas 131 may have a temperature of about 20 °C, or room temperature. Heat energy of hot exhaust gas 111 from the gas turbine 110 is stored in a PCM thermal storage tank 148 of the thermal storage system 140 into which the hot exhaust gas 111 is passed. The hot exhaust gas 111 may have a temperature of about 285 – 650 °C, while the PCM thermal storage tank 148 may have a temperature of about 220 – 600 °C, depending on the temperature of hot exhaust gas 111. Exhaust gas that leaves the PCM thermal storage tank 148 as emission 142 may have a temperature of about 200 °C.

The second power generator 120 is the Stirling engine 120 which operates between its high temperature or hot end (T_H) 122 and its cold end (T_C) 121. The hot end 122 is heated by a thermal fluid loop 141 of the thermal storage system 140 with heat from the PCM tank 148, and may have a temperature of about 200 – 580 °C. The cold end 121 is cooled by cold energy from a thermal fluid loop 133 of the LNG regasification unit 130, and may have a temperature of about -100 °C.

Boiling temperature (at 1 atm) of LNG is -162 °C, which significantly decreases the cold end 121 temperature of the Stirling engine 120, and increases its energy efficiency. In the power generation system 100, regasification of LNG 139 in the LNG regasification unit 130 heats the LNG 139 to produce natural gas 131 for the gas turbine 110 and also cools the cold end 121 of the Stirling engine 120. Thermal energy from the hot exhaust gas 111 of the gas turbine 110 is stored in the thermal storage unit 140 and applied to maintain the hot end 122 of the Stirling cycle 120. Aside from the Stirling engine 120, the LNG regasification unit 130 and the thermal storage unit 140 are thus two core components in the system 100.

The LNG regasification unit 130 comprises a heat exchanger 135 in which the LNG 139 absorbs heat energy and converts into gas phase 131 on one side of the heat exchanger 135. On the other side of the heat exchanger 135, the heat is taken away and the object is cooled down to a very low temperature.

In one embodiment of a compact design of the system 100, the heat exchanger 135 may be embedded in the Stirling engine 120, i.e. embedded with the cold end 121 of the Stirling engine 120, so that the heat transfer is conducted directly between the LNG 139

undergoing regasification in the regasification unit 130 and the Stirling engine 120.

In order to enhance heat transfer rate as well as the LNG phase change rate, LNG 139 from the LNG storage tank 150 may also simultaneously be sprayed (or otherwise impinged) onto the cold end 121 of the Stirling engine 120.

To enable the Stirling cycle power generation system 120 to achieve stable electric output, the thermal storage 140 can be integrated into the power generation system 120 to allow thermal energy to be stored and dispatched when power is required. PCMs are employed as the storage media in the thermal storage tank 148. Operating around a melting point of PCM stabilizes the temperature of the hot end 122 of the Stirling engine 120, thereby maintaining the hot end 122 of the Stirling cycle 120.

The exhaust gas 111 flows over the PCM tank 148 to charge the thermal storage system 140. The PCM tank 148 collects the heat from the exhaust gas 111 of the gas turbine 110 during operation. The heat transfer fluids 141 are circulated by a pump (not shown) to discharge the heat from the thermal storage tank 140. The heated heat transfer fluids 141 then send the heat to the Stirling engine 120 power generation system. The cooled heat transfer fluids 149 return to the PCM storage tank 148 for the next cycle. Pre-heating elements (not shown) are preferably installed in the tanks 148 to melt the PCMs at the beginning. Another function of the pre-heating elements is to make up the heat of the PCMs when it is in an emergent freeze situation. The tank 148 will be operated at atmospheric pressure, similar to commercial oil storage tanks. The proposed tanks 148 are preferably fabricated from stainless steel, and use self-supporting roofs. A heat exchanging tube for transferring thermal energy to superheat vapor is preferably be installed. To reduce heat loss, wall, bottom, and roof of the tanks 148 are insulated preferably with mineral wool batts and calcium silicate block insulation, respectively. The insulated foundation preferably comprises the following layers; (1) concrete slab, (2) foam glass insulation, (3) insulating fire bricks, (4) thin steel plate liner, and (5) sand. A perimeter ring wall of insulating firebricks is preferably provided to support the weight of the walls and roof of the tank 148.

Alternatively, the thermal storage unit 140 also can be embedded in the Stirling engine 120,

i.e., directly coupled with the hot end 122 of the Stirling engine 120, to make the system 100 more compact. In this case, the thermal fluid cycle is no longer needed as heat transfer is performed directly between the PCMs of the thermal storage unit 140 and the hot end 122 of the Stirling engine 120.

5

It can be predicted that LNG is promising in the market of power generation. Natural gas (NG) is an environmentally friendly fuel which is still in high reserve on earth. However, far field transportation of NG is necessary due to significant diversity of distribution of NG on the planet. The most common and economical way to transport NG is to ship the liquid phase as LNG. After delivery, LNG needs to be regasified into gas phase for utilization. The more popular NG is as a fuel in the global market, the more LNG transportation and regasification will be performed. This translates into a large amount of cold energy being produced in the LNG regasification process.

10

On the other hand, gas turbine power generator is still a very important method to supply electricity in many countries which produces a significant amount of waste heat. It is estimated that cold energy with an amount of 100 MJ will be output per hour for each MWe of power generation for a high efficiency power plant (such as TITAN250 with a capacity of 21.75 MWe). This accounts for just the latent heat of LNG-to-NG phase change alone. The value will be higher if sensible energy is accounted for. Power plants with low capacity (such as SATURN20 with a capacity of 1.21 MWe) consume 50% more fuels and waste around 150 MJ cold energy per hour for each MWe of power generation.

20

Therefore, the currently disclosed power generation system 100 presents an innovative method to recover this huge amount of cold energy from LNG regasification 130 as well as the heat energy in exhaust gas of the gas turbine 110 to be converted by the Stirling engine 120 into useful work. It has a potential for commercial application in energy industry.

25

Among the advantages of the power generation system 100, because a Stirling engine 120 is used to utilize the cold energy during regasification process of LNG 130 and the low temperature heat from exhaust gas from the gas turbine 110, the large temperature difference enhances the overall thermal efficiency of the Stirling engine 120. Simultaneous utilization of cold energy and low temperature heat solves the difficulties for recovering

30

them efficiently.

As the thermal storage system 140 on the basis of PCMs is applied to store the exhaust heat and stabilize the temperature of the exhaust gas 111 for the Stirling engine 120, operation of the power generation system 100 is more stable compared to other known systems.

With the power generation system 100, energy stored in LNG 139 including chemical energy and cold energy, and low temperature heat from exhaust gas 111 are all efficiently harnessed. All energy sources for the power generation system 100 come from LNG, and no extra energy sources or fuels are needed. By using LNG cold energy 133 and the gas turbine exhaust heat 111 simultaneously, high efficient recovery of both energies can be achieved with the Stirling engine 120 due to enhancement of thermal efficiency from the large temperature difference and the inherent high efficiency of the Stirling engine 120. Overall efficiency is expected to have an improvement of about 5% to 30% compared with conventional LNG fueled gas turbine power generation systems without recovery of cold energy and exhaust heat.

Using the power generation system 100 described above, referring to Fig. 2, a method 200 of generating power comprises regasifying LNG in a regasification process to produce natural gas (210), combusting the natural gas in a gas turbine to output power and produce an exhaust gas (220), storing heat obtained from the exhaust gas in a thermal storage unit (230), and heating a hot end of a Stirling engine with heat stored in the thermal storage unit and cooling a cold end of the Stirling engine in the regasification process to output power with the Stirling engine (240).

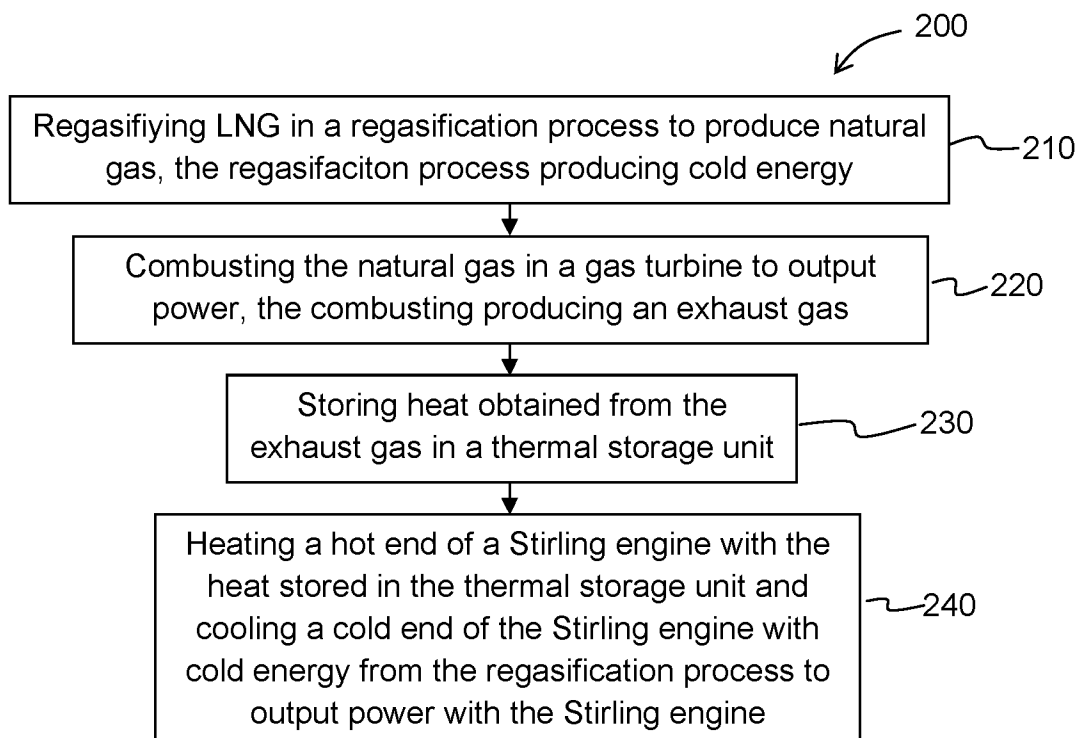
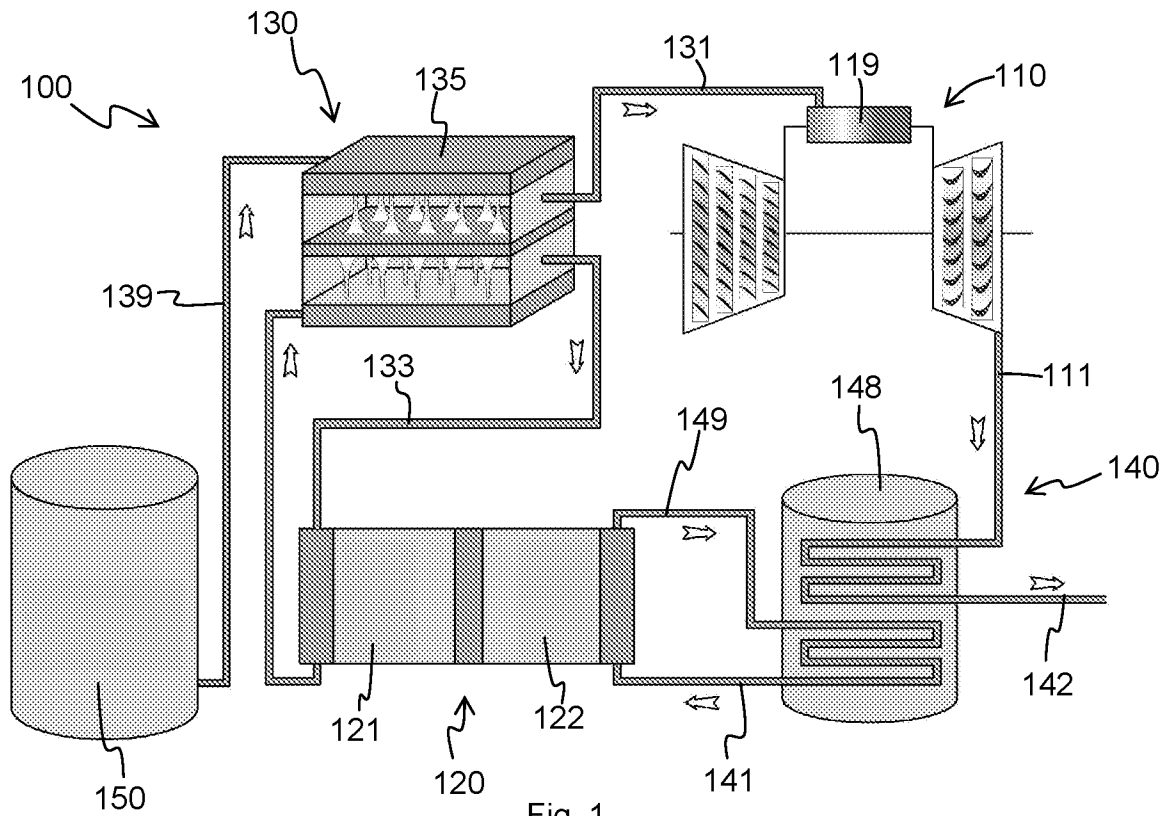
Whilst there has been described in the foregoing description exemplary embodiments of the present invention, it will be understood by those skilled in the technology concerned that many variations and combinations in details of design, construction and/or operation may be made without departing from the present invention.

CLAIMS

1. A power generation system comprising:
 - 5 a liquefied natural gas (LNG) regasification unit configured to perform a regasification process to regasify LNG supplied from an LNG source to produce natural gas, the regasification process producing cold energy;
 - a gas turbine configured to combust the natural gas to output power, the combusting producing an exhaust gas;
 - a thermal storage unit configured to store heat obtained from the exhaust gas; and
 - 10 a Stirling engine configured to output power, the Stirling engine having a hot end heated by the heat stored in the thermal storage unit and a cold end cooled by the cold energy from the regasification process.
2. The power generation system of claim 1, wherein the thermal storage unit comprises at
15 least one phase change material.
3. The power generation system of claim 1 or claim 2, wherein the thermal storage unit is embedded with the hot end of the Stirling engine.
- 20 4. The power generation system of any one of the preceding claims, wherein a heat exchanger of the regasification unit is embedded with the cold end of the Stirling engine.
5. A method of power generation, the method comprising the steps of:
 - 25 (a) regasifying LNG in a regasification process to produce natural gas, the regasification process producing cold energy;
 - (b) combusting the natural gas in a gas turbine to output power, the combusting producing an exhaust gas;
 - (c) storing heat obtained from the exhaust gas in a thermal storage unit; and
 - 30 (d) heating a hot end of a Stirling engine with the heat stored in the thermal storage unit and cooling a cold end of the Stirling engine with cold energy from the regasification process to output power with the Stirling engine.

6. The method of claim 5, wherein storing the heat comprises storing the heat in at least one phase change material in the thermal storage unit.
7. The method of claim 5 or claim 6, further comprising directly spraying the cold end of
5 the Stirling engine with LNG.

1 / 1



INTERNATIONAL SEARCH REPORT

International application No.

PCT/SG2016/050446

A. CLASSIFICATION OF SUBJECT MATTER

See Supplemental Box

According to International Patent Classification (IPC)

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

F02G; F01K; F02C; F28D

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

FAMPAT: liquefied natural gas, LNG, gas turbine, combustion, exhaust, Stirling, thermal storage, phase change, 斯特林发动机, 液化天然气 and similar terms

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	JP 2008-175151 A (CHUGOKU ELECTRIC POWER CO.) 31 July 2008 Figure 3; Paragraphs [0021]-[0031] of the machine translation	1-2, 5-7
X	JP 2006-200431 A (NISSAN DIESEL MOTOR CO. LTD.) 3 August 2006 Figure 1; Paragraphs [0008]-[0020] of the machine translation	1, 3-5, 7
X	JP 2014-207719 A (KAWASAKI HEAVY IND. LTD.) 30 October 2014 Figure 4; Paragraphs [0016]-[0020] and [0050]-[0053] of the machine translation	1, 3-5, 7
X	RU 2166705 C1 (VOENNYJ INZHENERNO-KOSMICHESKIY UNIVERSITET IM. A.F. MOZHAJSKOGO) 10 May 2001 Figure 1; Abstract; Page 2, 5 th paragraph – page 3, last paragraph of the machine translation	1, 5, 7

☒ Further documents are listed in the continuation of Box C.

☒ See patent family annex.

*Special categories of cited documents:

“A” document defining the general state of the art which is not considered to be of particular relevance

“E” earlier application or patent but published on or after the international filing date

“L” document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

“O” document referring to an oral disclosure, use, exhibition or other means

“P” document published prior to the international filing date but later than the priority date claimed

“T” later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

“X” document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

“Y” document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

“&” document member of the same patent family

Date of the actual completion of the international search

20/10/2016

(day/month/year)

Date of mailing of the international search report

02/11/2016

(day/month/year)

Name and mailing address of the ISA/SG



Intellectual Property Office of Singapore
51 Bras Basah Road
#01-01 Manulife Centre
Singapore 189554

Email: pct@ippos.gov.sg

Authorized officer

Meng Lei (Dr)

IPOS Customer Service Tel. No.: (+65) 6339 8616

INTERNATIONAL SEARCH REPORT

International application No.

PCT/SG2016/050446

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 2013/0091839 A1 (TAKAHASHI K. ET AL.) 18 April 2013 Figure 1; Paragraphs [0033]-[0035] and [0044]	
A	CN 102434257 A (XU M.) 2 May 2012 Whole document of the original non-English language document (a machine translation is enclosed only for your reference)	
A	US 3937017 A (BESCHORNER F. ET AL.) 10 February 1976 Whole document	
A	US 2015/0053367 A1 (PARKINSON N. ET AL.) 26 February 2015 Whole document	

INTERNATIONAL SEARCH REPORT

International application No.

PCT/SG2016/050446

Supplemental Box (Classification of Subject Matter)

Int. Cl.

F02G 1/055 (2006.01)

F01K 23/10 (2006.01)

F02C 6/18 (2006.01)

F02G 5/02 (2006.01)

F28D 20/02 (2006.01)

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No.

PCT/SG2016/050446

Note: This Annex lists known patent family members relating to the patent documents cited in this International Search Report. This Authority is in no way liable for these particulars which are merely given for the purpose of information.

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
JP 2008-175151 A	31/07/2008	NONE	
JP 2006-200431 A	03/08/2006	NONE	
JP 2014-207719 A	30/10/2014	WO 2013/008446 A1	17/01/2013
RU 2166705 C1	10/05/2001	NONE	
US 2013/0091839 A1	18/04/2013	WO 2011/155145 A1	15/12/2011
		EP 2573373 A1	27/03/2013
		JP 2011-256775 A1	22/12/2011
CN 102434257 A	02/05/2012	NONE	
US 3937017 A	10/02/1976	DE 2340269 A1	20/03/1975
		JP S50-49539 A	02/05/1975
		SE 7410170 A	10/02/1975
US 2015/0053367 A1	26/02/2015	WO 2013/020176 A1	14/02/2013
		EP 2764316 A1	13/08/2014
		AU 2012292959 A1	09/05/2013
		JP 2014-521918 A	28/08/2014
		CN 103998889 A	20/08/2014