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DESCRIPTION

CROSS-REFERENCE TO RELATED APPLICATIONS

BACKGROUND OF THE INVENTION

[0001] It is well understood that vessels or structures that in part reside below the surface of sea water or fresh water are subjected to various levels of fouling by marine (salt water) or aquatic (fresh water from lakes and rivers) organisms, respectively. Vessels such as boats, ships, or submarines require routine removal (cleaning) of fouling such as algae, weed, barnacles, mollusks, etc., in order to maintain the performance or even the function of the vessel. At the base of the fouling mechanism for vessels and structures residing in sea or fresh water are the biofilms formed on such structures that constitute the glue between marine or aquatic organisms and the actual structure. The biofilms form and the fouling-organisms attach to all subsurface structures and as a result the more diverse or intricate the structure (such as propellers, rudders, inlet and outlet ports, sonar housings, protective grills, etc.) the more difficult and costly to remove the biofilms and these organisms. Fouling is a major problem, leading to higher fuel consumption and consequently increased air pollution. It can also cause the spread of alien species that do not belong in the local marine environment. The type of paint or coatings applied to the vessel or structures also change the types of fouling. The economic impact of fouling is very high too. For example, in the US Navy the propeller cleaning is recommended up to six times a year and hull cleaning or grooming is recommended up to three times a year.

[0002] The fouling of platform structures below the water's surface such as pilings and beams creates an uneven water flow around the supporting features, which causes an uneven pressure distribution throughout the structure leading to material stresses and the potential for collapse of the platform. In conclusion a system that can perform a thorough grooming, meaning the removal of the biofilm(s) from structures and vessels, prevents the organisms from growing to a size that affects the vessel or structure's function or performance, which will require cleaning (removal of microorganisms and biofilms).

[0003] The cleaning or grooming of a marine (salt water) or aquatic (fresh water) vessel or structure (such as oil platforms) generally involves methods that use brushes, scrapers, other abrasive means to clean and very high pressure water sprays. Abrasive methods can be damaging to the welds and rivets of the water vessels or underwater structures compromising their mechanical integrity. Some of these methods require that the water vessel be dry-docked, which is a not only a large expense but a risk to the structure of the vessel each time it is removed from the water. Present cleaning or grooming methods are labor intensive and fall short of being thorough, leaving behind the biofilms, which represent the substrate and hold the nutrients that different salt water or fresh water organisms use for growth and anchor. Due

to this drawback, the actual marine (salt water) or aquatic (fresh water) vessels or structures will need cleaning more often. These other methods also tend to remove one or more surface layers of coatings or paint protecting the vessel or platform structure, which can requires that it be recoated or repainted. When the cleaning or grooming is performed below water surface another drawback may occur due to the fact that removed coatings or paint from the ship can be toxic for the surrounding marine or aquatic life.

[0004] Patents US 2005/0199171, US 2012/0006244, US 2013/0298817 and US 2014/0230711 present different systems and methods that use brushes to clean ship hulls. These systems can be used without the necessity of dry docking the ship. These patent publications present support frames with articulated arms or movable chassis/frames that help the brushes to reach the actual area that needs to be cleaned. These systems are complicated, expensive, labor intensive and can be dangerous to divers. Furthermore, it is well known that the brushes also remove a significant amount of the anti-fouling paint (a third of the paint coating can be gone during cleaning or grooming process), which can significantly increase the cost of cleaning or grooming, due to the necessity of re-painting of the hull.

[0005] A robotically operated device that uses an ultrasonic transducer for cleaning of ships' hulls is presented in US 4,890,567. This device was designed to be used during dry-dock cleaning of a ship and also can be used to spray paint on the hull after cleaning. The cavitation generated by the negative pressure of the ultrasound is thought to be the main mechanism that produces the hull cleaning. However, the ultrasound by its nature has a weak negative pressure (this pressure generates cavitation bubbles) and is immediately followed by the tensile (positive pressure), which collapse the cavitation bubbles before reaching their maximum size and thus full cleaning power. This is why this method is less effective, labor intensive and requires the dry-docking of the ship, which dramatically increases the cost.

[0006] High pressure water sprays systems for cleaning ship hulls (US 6,595,152) or pile cleaning of submerged structures (US 8,465,228) represent popular systems that are used for cleaning of marine (salt water) or aquatic (fresh water) vessels or structures. The disadvantage of these systems is the high operating pressures that can be dangerous for the divers and damaging to the actual structures that need to be cleaned. Not to mention that these systems require bulky installations and a lot of safety features to make them as safe as possible.

[0007] A "cavitation (negative pressure) jet" technology has been developed, such as described in US pat. No. 7,494,073, for use in cleaning surfaces underwater, with the added benefit of removing little to none of the coatings or paint layers, and therefore making the cleaning process of little to no contamination risk to the surrounding marine environment. However, this is a hand-held system by a diver that was designed for action on small surfaces (due to the nature of jet technology) and still requires a labor intensive operation to accomplish the desired results. Larger systems were created by Russians that are called "cavitators". These systems rely only on hydrodynamic cavitation bubbles that collapse and send so-called localized "shock waves" towards the surface in need of cleaning. Due to high pressures used for the jets providing flowing liquid and gas that generate the cavitation, the cavitation bubbles

do not have an optimum environment to develop to their full potential (high pressures from outside the bubbles prevent them to grow to their largest dimension, which translates in less energy put in the so-called "shock waves" produced during their collapse), which reduces significantly their efficiency. In other words, the smaller the pressure outside the cavitation bubbles (unpressurized liquid) the larger the bubbles will grow until the pressure inside the bubbles is higher than the pressure outside the bubbles, which will initiate their collapse capable of generating much more efficient high pressure jets. CN 103895835 discloses a plasma shock wave cleaning system utilizing a magnetic walking robot in which plasma shock waves are produced underwater in an open reflector toward marine organisms on a ship's hull for loosening and removal. CN 103895835 does not disclose a membrane-covered reflector environment for producing acoustic pressure shock waves or the ability to rotate an inspection and cleaning or grooming module about X and Y axes. U.S. Pat. App. Pub. No. 2014/305877 discloses acoustic pressure shock waves produced in a reflector covered with a membrane for fracking, oil recovery and cleaning process waters in the energy industry, but does not disclose the cleaning of submerged structures or a shock wave cleaning system with an inspection and cleaning or grooming module capable of rotating about the X and Y axes.

[0008] All of the above alternatives for cleaning or grooming underwater structures or ship hulls rely on the support of a remotely operated "underwater" vehicle (ROV). The ROV is commercially fabricated for various purposes including underwater applications. These ROVs allow underwater navigation while being remotely controlled above water surface. Remote navigation is possible since ROVs contain onboard cameras and underwater lighting systems to transmit live images of the environment surrounding the ROV to the above surface station/control station. The ROVs are equipped with thrusters to propel the ROV through the water and contain wheels, traction grip tracks, or other traction means such as controlled suctioning or controlled magnetic attraction to move along a surface. There are particular commercial ROVs that can maintain direct contact with an underwater structure while traversing alongside it, even beyond vertical. These highly developed and capable ROVs require extensive technical expertise [refer to patents US 8,386,112, US 2011/0083599, US 2013/0263770, US 2014/0076224 A1, US 2014/0076225 A1, and US 2014/0081504 A1] to support their unique capabilities, which is not in the scope of this invention.

SUMMARY OF THE INVENTION

[0009] The present invention is proposing a ship's hull and underwater structures cleaning or grooming apparatus employing acoustic pressure shock waves that can provide high compressive pressures (pressures in excess of 100 MPa/1000 bar) followed by large and long lasting tensile/negative pressures (in excess of 10 MPa/100 bar), which can generate large cavitation bubbles producing during their collapse very powerful water jets with speeds in excess of 100 m/s. These two synergetic phase effects of the acoustic pressure shock waves are capable of working in tandem for cleaning or grooming ships' hull or any underwater structures subject to marine or aquatic biofilms formation and subsequently to marine or aquatic fouling.

[0010] Compared to "cavitation jet" technology based on flowing liquid and hydrodynamic cavitation, the acoustic pressure shock waves of the present invention produce much stronger and larger scale shock waves that move with the speed of sound. As mentioned above, these acoustic pressure shock waves have a compressive phase (pressures in excess of thousands of bar) followed by a long tensile phase that creates significantly larger cavitation bubbles capable of producing during their implosions (collapses) water jets with speeds in excess of 100 m/s combined with localized ultrahigh pressures and high temperatures. Thus, the acoustic pressure shock wave technology produces a "double punch" effect, and it is capable of much higher efficiency during cleaning or grooming process when compared to "cavitation jet" technology.

[0011] The present invention describes non-contact and non-abrasive acoustic pressure shock waves cleaning or grooming apparatuses, which are also compatible and potentially non-destructive to paints or coatings, including antifouling or environmental coatings applied to the water vessel or underwater structure, which is an important financial and environmental benefit. These acoustic pressure shock wave systems are capable of removing the layers of marine or aquatic fouling down to the biofilms that have become bonded to the subsurface structures. Furthermore, the application of acoustic pressure shock waves is most significant on removing the aquatic or marine biofilms, which are the source of fouling, without destroying the integrity of the underlying structure/substrate (grooming of marine (salt water) or aquatic (fresh water) vessels or structures). This would reduce the need to use antifouling coatings that only slow down the biofilm growth without eliminate it. Furthermore, the antifouling toxic coatings/paints incorporate copper, heavy metals and other biocides, which when released into surrounding marine or aquatic environment can pose a danger to the local marine or aquatic life. Thus, the acoustic pressure shock waves cleaning or grooming apparatuses described in the embodiments of this invention can eliminate or reduce the negative environmental impact produced by existing technologies used for the cleaning or grooming of fouling on ships' hull or any underwater structures.

[0012] There are different degrees of fouling, depending on the material (metal, fiber glass, plastics, wood, cement, etc.) and/or external paint or coating of the surface being cleaned. The fouling organisms can be extremely bonded to the structure such that to remove these organisms and the biofilm layer will sometimes result in removing some of the surface coating, and if the coatings are toxic would require proper containment. This is why the present invention also provides a means to contain the cleaning or grooming waste and therefore reducing the likelihood of posing a danger to the surrounding marine (salt water) or aquatic (fresh water) life. The inflatable bladder of the present invention provides a sufficient seal between the cleaning or grooming apparatus and the working surfaces so that the debris can be collected, pumped away and render them harmless through filtering by topside managing systems.

[0013] Acoustic pressure shock wave technology being a non-contact technology can easily protect the structural integrity of rivets, welds, indents, which if affected by the cleaning or

grooming process can compromise the integrity of the hulls or underwater structures. Furthermore, by adjusting the focusing (deep or shallow) of the acoustic pressure shock waves apparatuses, the cleaning or grooming can be done in difficult to reach areas, due to small radiuses of the hull/structures, crevices or intricate constructions present underwater. The focused acoustic pressure shock wave technology due to its ability to get to very difficult to reach areas of intricate structure, can also eliminate biofilms and fouling build-up from propellers, rudders, inlet ports for cooling of nuclear submarines, outlet ports, sonar housings, protective grills, etc., without affecting their structural integrity.

[0014] The cleaning or grooming methods of the present invention that mainly use acoustic pressure shock waves that are non-abrasive, non-contacting, and have the capability to adjust the applied acoustic pressure shock wave energy to the specific cleaning or grooming surface, which allows different materials (e.g. metals, fiberglass, plastics, wood or cement) with different mechanical properties to be cleaned without causing damage or structural stresses. Furthermore, the targeted area for cleaning or grooming can be hit by the acoustic pressure shock waves at different angles (5 to 90 degrees), which create multidirectional forces (perpendicular and tangential to the surface that requires cleaning or grooming) that allow a better detachment of the fouling microorganisms and biofilms. The non-specificity of acoustic pressure shock waves to the material of the hull or underwater structures and to the environment that produces different types of biofilms/fouling represents a great advantage when compared with existing methods that are in general specific to the respective material that is cleaned or type of fouling microorganisms.

[0015] The present invention allows the water vessel or potentially any subsurface structure to be cleaned dockside or out to sea or lake or river and relies on the support of a remotely operated "underwater" vehicle (ROV). These ROVs are commercially fabricated for various purposes including underwater applications and require extensive technical expertise to support their unique capabilities, which is not in the scope of this invention. This invention requires that such a remotely operated "underwater" vehicle (ROV) be the carrier for the inspection and cleaning or grooming apparatuses that use acoustic pressure shock waves described herein, so as to enable remotely navigating underwater alongside a vessel or structure, and holding position underwater for inspection and cleaning or grooming. The present invention by utilizing a remotely operated "underwater" vehicle (ROV) is alleviating the need to use divers and thus the danger to human life, it is more effective and in general not damaging to antifouling paints or coatings, since the cleaning or grooming methods utilized are non-abrasive and non-contacting.

[0016] To perform a thorough inspection and effective cleaning or grooming of fouling from ships' hull and underwater structures, the present invention utilizes remotely operated cameras and fluorimeters installed on ROVs. The cameras and fluorimeters can be directed via remote control to a specific field of view towards the working surface. The existing technology of fluorimeters enables the cleaning or grooming operator or an expert system to detect biofilms that have adhered to the structure of the ship/underwater structures, which are promoting the growth of algae, barnacles, mollusks, etc., and therefore can distinguishing a clean surface

from an unclean/marine or aquatic fouled surface. The use of cameras and fluorimeters is also very important to determine where the cleaning or grooming was already done and where it needs to continue, especially for cleaning or grooming processes that must be done with interruptions on multiple days. The field of view can be optimized by the operators ability to set the direction of each camera, and in the event of murky water, which can hamper visibility and fluorimeter sensing, this invention provides a method to seal off the working area, so that clean/clear water can replace the murky water that exists in the working environment. To accomplish this, the present invention identifies the use of an inflatable bladder that will seal the space between the cleaning or grooming apparatus and the working surface. Once the bladder is inflated, the majority of the water that is trapped is pumped out of the working environment and replaced with clean/clear water. Replacing the water in the working environment also enhances the cleaning or grooming inspection process as it progresses, since debris generated during cleaning or grooming process need to be removed to improve the visibility of the working area.

[0017] The above water remote operators station for the present invention is capable of controlling the ROV to navigate alongside a structure or vessel's waterline and below for inspection and cleaning or grooming. The remote operators station provides CCTV (closed circuit television) displays of the environment surrounding the ROV and the viewing of the working area to be cleaned, including the output of fluorometric sensors for detecting biofilms. The remote operators via their remote workstations have the ability to control all aspects of the inspection and cleaning or grooming processes.

[0018] In addition to cameras, the present invention in embodiments incorporates sonar transceivers on the ROV and the cleaning or grooming apparatuses to prevent collision and therefore to prevent damage to the ship, ROV, or cleaning or grooming apparatuses. To prevent collision, the present invention will override the controls of the operator if a collision is eminent.

[0019] Another embodiment of this invention uses high pressure water jet(s) that augment the cleaning or grooming provided by the acoustic pressure shock waves. The pressurized water would be applied before or after application of the acoustic pressure shock waves to facilitate the best effect on the surfaces being cleaned. The amount of pressure applied by the water jets is adjustable so that it will not remove the protective paint or coatings on the structure's surface. The combination of the two cleaning or grooming methods (water jet technology and shock wave technology) provides a thorough cleaning or grooming system that removes not only the visible fouling debris such as barnacles, mussels, algae, etc., but also removes the microorganisms that have formed biofilms on the surface of water vessels and structures occurring in an underwater environment.

[0020] The present invention enables remote control of all the cleaning or grooming apparatuses such that the individual acoustic pressure shock wave generating devices and water jet sources can be made independently active or inactive, and can be directed/oriented to provide a focused area of cleaning or grooming on a fouled subsurface structure, in order to

facilitate the removal of organism growth and marine or aquatic biofilms.

BRIEF DESCRIPTION OF THE DRAWINGS

[0021]

FIG. 1 is a schematic representation of a remotely operated underwater vehicle (ROV) equipped with a cleaning or grooming apparatus that is generating acoustic pressure shock waves toward the water vessel's hull and having thrusters and wheels to transition across the subsurface features of a water vessel according to one embodiment of the present invention;

FIG. 2 is a schematic representation of an ROV equipped with a cleaning or grooming apparatus that is generating acoustic pressure shock waves toward the water vessel's hull and using thrusters and controlled magnetic coupling to transition across the subsurface features of a water vessel according to one embodiment of the present invention;

FIG. 3 is a schematic representation of an inspection and cleaning or grooming system including the operators station and of an ROV according to one embodiment of the present invention;

FIG. 4A is a front view schematic representation of an inspection and cleaning or grooming module containing multiple cleaning or grooming apparatuses and sensors according to one embodiment of the present invention;

FIG. 4B is a cross-sectional side view schematic representation of the module of FIG. 4A according to one embodiment of the present invention;

FIG. 5 is a schematic representation of the interaction of focused acoustic pressure shock waves with an underwater surface when an ellipsoid reflector is used as one embodiment of the acoustic pressure shock wave generator of the invention;

FIG. 6 is a schematic representation of the planar acoustic pressure shock waves that emanate from a parabolic reflector as one embodiment of the acoustic pressure shock wave generator of the invention;

FIG. 7A is a cross-sectional top view schematic representation of a ROV that is generating both acoustic pressure shock waves and pressurized water jets at the subsurface features of a water vessel or other underwater structure according to one embodiment of the present invention;

FIG. 7B is a schematic representation of the ROV of FIG. 7A, illustrating the functional features of the different cleaning or grooming and inspection modules according to one embodiment of the present invention;

FIG. 7C is a schematic representation showing an inflated bladder positioned between the cleaning or grooming modules of the ROV of FIG. 7A and the ship's hull according to one

embodiment of the present invention;

FIG. 7D is a schematic representation of the ROV of **FIG. 7A** with the cleaning or grooming and inspection modules folded down for transport in according to one embodiment of the present invention;

FIG. 8 is a perspective schematic view along the section plane A-A of the cleaning or grooming and inspection module of **FIG. 7B** that uses high voltage tip discharge to create an acoustic pressure shock wave according to one embodiment of the present invention;

FIG. 9 is a perspective schematic view along the section plane A-A of the cleaning or grooming and inspection module from **FIG. 7B** that uses high energy laser(s) to create an acoustic pressure shock wave according to one embodiment of the present invention;

FIG. 10 is a perspective schematic view along the section plane A-A of the cleaning or grooming and inspection module from **FIG. 7B** that uses a piezoelectric fiber composite structure to create an acoustic pressure shock wave according to one embodiment of the present invention;

FIG. 11 is a perspective schematic view along the section plane A-A of the cleaning or grooming and inspection module from **FIG. 7B** that uses an electromagnetic force to create an acoustic pressure shock wave according to one embodiment of the present invention;

FIG. 12 is a schematic representation of the electronic subsystems contained in the inspection and cleaning or grooming module of **FIG. 4A** or contained in the outer left and right inspection and cleaning or grooming modules depicted in **FIG. 7B** according to one embodiment of the present invention;

FIG. 13 is a schematic representation of the electronic subsystems contained in the center inspection and cleaning or grooming module depicted in **FIG. 7B** according to one embodiment of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

[0022] Embodiments of the invention will be described with reference to the accompanying figures, wherein like numbers represent like elements throughout. Further, it is to be understood that the phraseology and terminology used herein is for the purpose of description and should not be regarded as limiting. The use of "including", "comprising", or "having" and variations thereof herein is meant to encompass the items listed thereafter and equivalents thereof as well as additional items. The terms "connected", and "coupled" are used broadly and encompass both direct and indirect mounting, connecting and coupling. Further, "connected" and "coupled" are not restricted to physical or mechanical connections or couplings.

[0023] The inventions summarized below and defined by the enumerated claims are better understood by referring to the following detailed description, which should be read in conjunction with the accompanying figure. The detailed description of the particular embodiment, is set out to enable one to practice the invention, it is not intended to limit the enumerated claims, but to serve as a particular example thereof.

[0024] Also, the list of embodiments presented in this patent is not an exhaustive one and for those skilled in the art, new embodiments can be realized,

[0025] It is an objective of the present inventions to disclose different embodiments of inspection and cleaning or grooming modules **15** for the inspection and removal of (salt water or fresh water) fouling organism layers **19** from underwater structures such as in FIG. 1 depicting the cleaning or grooming of a water vessel hull, which includes the inspection and removal of the biofilm layer (grooming) that supports the organism growth (cleaning module will remove both organisms and biofilm). The inspection and cleaning or grooming module **15** is supported by an underwater carrier such as a remotely operated (underwater) vehicle **10** (ROV). The ROV **10** is self-propelled, having thrusters **11** and wheels **12** (magnetic or non-magnetic) to navigate along a water vessel surface **18** as in FIG. 1, and controlled from an on-board expert software system or remote controlled using wireless communication with an above water surface control station via floating surface radio antenna **14**. The present invention does not limit the means by which the ROV can navigate in order to perform inspection and cleaning or grooming. In the example in FIG. 2, the ROV is equipped with thrusters **11** and controlled magnetic attraction **22** to move along a water vessel surface **18**.

[0026] The inspection and cleaning or grooming module **15** will utilize one or more cleaning or grooming apparatuses to facilitate removal of the subsurface fouling from water vessels and underwater structures. The primary apparatus being an acoustic pressure shock wave generating device **16** (identified in FIG. 1 and FIG. 2) to not only remove the exterior fouling organism layers **19** but also the removal of the internal biofilm (substrate) layer. The secondary apparatus is the use of pressurized water jets **27** identified in FIG. 2. A general construction of the acoustic pressure shock wave generating device **16** shown in FIG. 2 comprises a reflector **24** to focus the acoustic pressure shock waves **17**, a coupling membrane **26** to protect the acoustic pressure shock wave generating device **16** from the external environment, and an energy transfer mechanism that will convert electrical energy into mechanical energy, which in the later case is pressure. The pressurized water jets **27** can use direct positive pressure or a "cavitation (negative pressure) jet" technology, such as described in US patent no. 7,494,073, to assist with removal of fouling organism layers **19**.

[0027] It is an objective of the present invention to provide an acoustic pressure shock wave generating device **16** (as in FIG. 1 and FIG. 2) (for generating focused acoustic pressure shock waves **17**) that is modular, does not need high maintenance, and can be applied/used in conjunction or separately with the high pressure water jets **27** (see FIG. 2).

[0028] It is a further objective of the present invention to provide different energy transfer

mechanisms for generating focused acoustic pressure shock waves **17** (as in FIG. 1 and FIG. 2) for the removal of marine (salt water) or aquatic (fresh water) fouling organism layers **19** (including the biofilm) that are attached to the underwater surfaces of water vessels or structures (cleaning). The energy transfer mechanisms/principle of operation for generating acoustic pressure shock waves **17** can comprise any of the following means:

electrohydraulic generators using high voltage discharges

electrohydraulic generators using one or multiple laser sources

piezoelectric generators using piezoelectric crystals

piezoelectric generators using piezoelectric fibers

electromagnetic generators using a flat coil

electromagnetic generators using a cylindrical coil

[0029] It is a further objective of the present invention to provide a means of controlling the accumulative energy at the cleaning or grooming surface of the water vessel or other underwater structures. Controlling the accumulative energy translates to the benefit of the acoustic pressure shock waves to remove the thick fouling organism layers **19** (FIG. 1 and FIG. 2) occurring on water vessels and other underwater structures without the risk of imparting material stress to the water vessel or structure, or the risk of damage to the layers of paint or coatings that exist on the water vessel or structure. If paint or coating layers are detached as part of the cleaning or grooming process they can introduce potential toxins into the water environment. The accumulative energy is the combination of energy (or energy flux density) delivered by one shock wave pulse generated acoustic pressure shock wave generating devices **16**, the total number of the acoustic pressure shock waves/pulses delivered to the targeted area, repetition frequency of the acoustic pressure shock waves and special construction of the reflector **24** (refer to FIG. 2) used in the acoustic pressure shock wave generating device **16**.

[0030] It is a further objective of the present invention to provide a variety of novel acoustic pressure shock wave generating device **16** (as in FIG. 1 and FIG. 2) constructions and assemblies for the wide area or small area removal of fouling organisms **19** including the biofilm from water vessels and other subsurface structures (cleaning process) or only for the removal of the biofilm (grooming process). The potential size of the cleaning or grooming target area is determined by 'the number of acoustic pressure shock wave reflectors **24** (refer to FIG. 2) contained in the inspection and cleaning or grooming module **15**, the shape/geometry of specific reflector **24**, the energy created within the reflector **24**, and the capability of the reflector **24** to direct or focus the acoustic pressure shock waves **17** on a specific target.

[0031] The present invention pictorialized in FIG. 3 performs the inspection and cleaning or grooming of water vessels and underwater structures with the use of a remotely operated inspection and cleaning or grooming vehicle 30 (the integration of the ROV with the inspection and cleaning or grooming module 15) to perform the underwater navigation, inspection, and the control of cleaning or grooming process. The level of operating autonomously in navigating and for inspection or cleaning or grooming can vary depending on the level of software intelligence developed for the ROV and for the inspection and cleaning or grooming module 15. In the embodiment of FIG. 3, the inspection and cleaning or grooming vehicle 30 is expected to perform some level of remote communications with the operator's station 32 using either wireless communication via floating surface radio antenna 14, or wired communication through a system hybrid cable 13 connected between the operator's station 32 and the inspection and cleaning or grooming vehicle 30. The remote operator's station 32 in FIG. 3 is on a trailer 35 so that it is portable and can be located dockside or on-board of the ship so inspection and cleaning or grooming can be performed dockside or out to sea, respectively. The remote operator's station 32 provides the power sources for the entire inspection and cleaning or grooming system using various on-board generators 36 to create the electrical power, filtered pressurized water, and an underwater vacuum source. The generator for the pressurized water extracts and filters the local sea water from a siphoning hose 37. Remotely operating the inspection and cleaning or grooming vehicles 30 simplifies the coordination of having multiple such vehicles performing the inspection and cleaning or grooming of a large water vessel or large underwater structure and reduces the chances of tangling cables between vehicles.

[0032] In FIG. 3 there is a system hybrid cable 13 that the operator's station 32 supplies to the remote cleaning or grooming vehicle 30, which can comprise, but not limited to, supplying power, an optical fiber, a high pressure water hose, and a vacuum hose. The optical fiber can be used as an optional wideband communication link, or used strictly to send the video images from underwater cameras located on the inspection and cleaning or grooming vehicle 30. The high pressure water hose will supply pressurized water jet 27 (see FIG. 2) to the inspection and cleaning or grooming vehicle 30 for various purposes to be described later. The vacuum hose will enable the inspection and cleaning or grooming vehicle 30 to transfer the removed fouling material to the operator's station 32 for processing.

[0033] The embodiment of FIG. 1 and FIG. 2 shows the use of acoustic pressure shock waves 17 to remove the fouling organism layers 19, which includes the biofilm (not specifically shown in the figure as a distinct feature), from a water vessel surface or underwater structure surface 18. The acoustic pressure shock waves 17 are generated from the inspection and cleaning or grooming module 15 that is attached to a remotely operated "underwater" vehicle (ROV) 10. An embodiment of an inspection and cleaning or grooming module 15 is shown in FIG. 4A that would be carried by the ROV 10, as shown in FIG. 1 or FIG. 2, to a position along the water vessel surface or underwater structure surface 18 for inspection and cleaning or grooming. The navigation and inspection features of the inspection and cleaning or grooming module 15 embodiment of FIG. 4A provides an array of light emitting diodes 44 for underwater illumination, four closed circuit cameras 42 for underwater inspection, a fluorometric sensor 46

for detecting biofilm, and two ultrasonic sonar sensors **43** to measure distance to the underwater structure. The cleaning or grooming apparatuses of FIG. **4A** comprises seven acoustic pressure shock wave generating devices **16** and three high pressure water jet nozzles **41**. The acoustic pressure shock wave generating device **16** receives its power from the power and control system **40** (see FIG. **4B**), whereas the pressurized water is supplied externally from a remote operator's station **32** (as in FIG. **3**). The particular number of functional features just described is an example for the embodiment in FIG. **4A** and the number of features can be scaled appropriately for the type or size of structure features being cleaned. For example vacuum intakes can be added to the inspection and cleaning or grooming module **15** (not shown in FIG. **4A**) for the case when the removal of fouling material is necessary via a vacuum hose that will enable the inspection and cleaning or grooming vehicle **30** to transfer to the operator's station **32** the mixture of water and fouling material for processing/cleaning/filtration.

[0034] As presented in FIG. **4B**, the acoustic pressure shock wave generating devices **16** from FIG. **4A** can have their acoustic pressure shock wave reflectors **24** able to tilt their angle (see arrows from FIG. **4B**) in both X and Y planes with respect to the inspection and cleaning or grooming module **15** position so that it can optimally direct its focal energy towards the cleaning or grooming target. The ability to tilt to a specific angle can be controlled locally by the power and control system **40** contained within the inspection and cleaning or grooming module **15**, or controlled remotely by a remote operator's station **32** (as in FIG. **3**) communicating with the inspection and cleaning or grooming module **15**.

[0035] The high pressure water jet nozzles **41** from FIG. **4A** can be directed toward the same cleaning or grooming target as the acoustic pressure shock wave reflector **24** by controlling the pitch of the water jet nozzle **41** shown in FIG. **4B**. The ability to control the pitch of the water jet nozzle **41** can be done locally by the power and control system **40** contained within the inspection and cleaning or grooming module **15**, or controlled remotely by a remote operators station **32** (as in FIG. **3**) communicating with the inspection and cleaning or grooming module **15**. The combination of the directed water jet nozzles **41** and the directed acoustic pressure shock wave reflectors **24** toward the same cleaning or grooming target would reduce the overall cleaning or grooming time and would also increase the efficacy of the cleaning or grooming process.

[0036] Each acoustic pressure shock wave generating device **16** in FIG. **4A** has an acoustic pressure shock wave reflector **24** and a coupling membrane **26** both shown in FIG. **4B**. The energy source for the acoustic pressure shock wave generating device **16** from FIG. **4B** is provided in the form of high voltage generated by the power and control system **40** and applied across an anode tip **49** and cathode tip **48** that are immersed in the reflector liquid **47**. The reflector liquid **47** is contained by the reflector cavity **25** and the coupling membrane **26**. A high voltage applied between the tips results in an electrical current flowing between the anode tip **49** and cathode tip **48**. The electrical current increases at an extremely fast rate, in the tens of nanoseconds, while at the same time superheating the reflector liquid **47** in between the tips to create a plasma bubble in the reflector liquid **47**. The formation of a plasma bubble in between the anode tip **49** and cathode tip **48** occurs at a rate in the tens of nanoseconds, similar to the

increasing rate of change of the electrical current. The rise in electrical current that creates the fast growing plasma bubble generates the primary shock wave front, which together with reflected shock waves on the acoustic pressure shock wave reflector **24** produces the positive pressure component of the acoustic pressure shock waves **17** (see FIG. 1). Once the potential voltage between the tips is no longer supplied or sufficient to support the flow of electrical current, the pressure of the reflector liquid **47** surrounding the plasma bubble will be higher than the plasma bubbles internal pressure. It is this transition that will cause the plasma bubble to rapidly collapse creating the negative (cavitation) pressure component of the acoustic pressure shock wave **17**, known also as the tensile component of the acoustic pressure shock wave **17**. The magnitude of voltage applied in between the anode tip **49** and cathode tip **48** can be controlled locally by the power and control system **40** contained within the inspection and cleaning or grooming module **15**, or controlled remotely by a remote operators station **32** (as in FIG. 3) communicating with the inspection and cleaning or grooming module **15**.

[0037] One embodiment of the acoustic pressure shock wave reflector **24** described by FIG. **4B** is a partial ellipsoidal reflector **50** diagramed in FIG. **5**. The acoustic pressure shock waves **17** produced at the first focal point F_1 , as diagramed in FIG. **5**, are reflected and focused by the partial ellipsoidal reflector **50** towards the second focal point F_2 **52** of the partial ellipsoid reflector **50**. It is the combination of partial ellipsoidal reflector **50** design, together with the applied energy in first focal point F_1 **51** that will dictate the distance where the second focal point F_2 **52** is found. The placement of the acoustic pressure shock wave generating device **16** relatively to the cleaning or grooming target will also dictate where the second focal point F_2 **52** is found in the targeted area. Due to the fact that different pressures fronts (direct or reflected) reach the second focal point F_2 **52** with certain small time differences, the acoustic pressure shock waves **17** are in reality concentrated or focused on a three-dimensional space around second focal point F_2 **52** which is called focal volume **58**. Inside the focal volume **58** are found the highest pressure values for each acoustic pressure shock wave **17**, which means that is preferable to position the targeted area **57** for cleaning or grooming so that it intersects the focal volume **58** and if possible it is centered on the second focal point F_2 **52**. This positioning will allow the highest efficiency in cleaning or grooming the targeted area **57** using the acoustic pressure shock wave generating devices **16**. An ultrasonic sonar sensor **43** (as described in FIG. **4A**) would provide the position information to set the cleaning or grooming target distance at the focal point F_2 **52** and maintaining the targeted area **57** intersecting the focal volume **58** at all times.

[0038] The ability of acoustic pressure shock waves **17** (shown in FIG. **5**) to destroy biofilms (grooming process) is a significant benefit for it eliminates the possibility of growth of marine (salt water) or aquatic (fresh water) organisms that would result in fouling that requires a cleaning process (more laborious and intensive compared to grooming process). In order to be effective, the acoustic pressure shock wave generating device **16** and its components are designed in such way to ensure that the focal volume **58** (where acoustic pressure shock waves **17** are focused) is positioned deep enough to allow its overlap with the fouling organism layers **19** and the water vessel's or underwater structure's surface **18**, where the biofilm layer

59 is present as shown in FIG. 5. The acoustic pressure shock wave **17** penetration through to the biofilm layer **59** and the geometry of the focal volume **58** are dictated by the energy generated at focal point F_1 **51**, and the dimensional characteristics of the ellipsoidal reflector **50** (the ratio of the large semi-axis **53** and small semi-axis **54** of the ellipsoid and its aperture **55** defined as the dimension of the opening of the ellipsoidal reflector **50**). Thus the ellipsoidal reflector **50** needs to be deep enough to allow the second focal point F_2 **52** to be positioned within the deepest fouling organism layers **19** of the structure down to the water vessel surface or underwater structure surface **18** of the structure without any physical contact of the acoustic pressure shock wave generating device **16** with the surface **18** of the structure (avoids any scrapping or other mechanical damage to the water vessel surface or underwater structure surface **18** or to the inspection and cleaning or grooming vehicle **30** (see FIG. 3). The deep ellipsoidal reflector **50** is also advantageous due to the fact that the larger the focusing area of the ellipsoidal reflector **50**, the larger the focal volume will be and the energy associated with it, which is deposited into the targeted area. In general to accomplish that, the ratio of the large semi-axis **53** and small semi-axis **54** of the ellipsoidal reflector **50** should have values larger than 1.6 (the dimension of the small axis of the ellipsoid **54** and the large axis of the ellipsoid **53** identified in FIG. 5 is given by their intersection with the ellipsoid and with semi-axis value being defined as half of their respective full dimensions).

[0039] In the embodiment from FIG. 6 the acoustic pressure shock wave generating device uses a parabolic reflector **60** that sends pseudo-planar acoustic pressure shock waves **17** outside the coupling membrane **26** and inside the targeted fouling organism layers **19** attached to the water vessel's or underwater structure's surface **18**. The parabolic reflector **60** has only a central point F where radial acoustic pressure shock waves **17** are generated (from an energy source). The radial acoustic pressure shock waves **17** propagate and reflect on the parabolic reflector **60** at different time points, which creates secondary wave fronts (not shown on FIG. 6 to keep clarity), especially at the edge/aperture **65** of the parabolic reflector **60**. The combination of direct radial acoustic pressure shock waves **17** with the secondary wave fronts creates pseudo-planar acoustic pressure shock waves **64** outside the coupling membrane **26**. By their nature, the pseudo-planar acoustic pressure shock waves **64** (exiting through the aperture **65** of the parabolic reflector **60**) are unfocused and thus they move inside the fouling organism layers **19** away from their point of origin F without being able to be concentrated/focused in a certain focal region, as seen before in FIG. 5 for the acoustic pressure shock waves **17** that are focused. The pseudo-planar acoustic pressure shock waves **64** deposit their energy into the fouling organism layers **19** including the biofilm **59**, until all of their energy is consumed. In other words, the pseudo-planar acoustic pressure shock waves **64** have their maximum energy superficially at the interface of the underwater structure **66** and the biofilm layer **59** that forms on the underwater structure surface **18**, and become weaker as they travel further inside the underwater structure **66** away from the underwater structure surface **18**. This means that it may preferable to use this embodiment presented in FIG. 6 to clean surfaces that are structurally weak and do not have deep fouling organism layers **19**. The advantage of this embodiment presented in FIG. 6 is that in one position of the inspection and cleaning or grooming vehicle **30** a larger area is groomed or cleaned by pseudo-planar acoustic pressure shock waves **64** when compared to the focused acoustic pressure shock

waves **17** where the groomed or cleaned area in one position is given mainly by the dimensions of the focal volume **58** (see FIG. 5). The pseudo-planar acoustic pressure shock wave **64** penetration depths are controlled by the input energy applied to the origin F.

[0040] The quantity of acoustic pressure shock wave energy deposited into the fouling organism layers **19** in one cleaning or grooming session is dependent on the dosage, which comprises the following characteristics.

[0041] *Input energy* delivered to the focal point F_1 **51** shown in FIG. 5, and the central point F **61** shown in FIG. 6, which is:

1. a. for electrohydraulic shock wave generating devices it is the voltage applied to the electrodes as described for FIG. 4B and FIG. 8
2. b. for piezoelectric shock wave generating devices it is the voltage applied to the piezoelectric fibers or piezoelectric crystal structures, as described in detail for FIG. 10
3. c. for electromagnetic generators it is the voltage applied to the electromagnetic coil, as described in detail for FIG. 11
4. d. for laser generated energy it is the optical energy delivered to the focal point F_1 and central point F, as described in detail for FIG. 9

[0042] *Output energy* of each acoustic pressure shock wave in the targeted zone; known as energy flux density [mJ/mm^2] or instantaneous intensity [mJ] at a particular impact point in space.

[0043] *Frequency* of repetition for acoustic pressure shock waves, defined as number of acoustic pressure shock waves per each second.

[0044] *Total number of acoustic pressure shock waves* delivered in one cleaning or grooming session.

[0045] Cavitation plays a primary role in the destruction of the biofilm layer **59** (see FIG. 5). In order to have maximum potential for the cavitation phase of the acoustic pressure shock waves **17**, the repetition rate or frequency of acoustic pressure shock waves **17** is recommended to be in the range of 4 to 8 Hz so as to not be negatively influenced by the subsequent inbound acoustic pressure wave **17**. The maximum frequency is to be limited so that the cavitation bubbles have sufficient time to grow to their maximum dimension and then collapse with velocities of more than 100 m/s, which will allow the maximum effects to be seen on the biofilm layer **59** (grooming process) or on the fouling organism layers **19** plus the biofilm layer **59** (cleaning process).

[0046] FIG. 7A is the embodiment of a remote inspection and cleaning or grooming vehicle **30** that is fitted with three inspection and cleaning or grooming modules mounted to a rotating

vertical frame **71**, which itself is mounted to a supporting base/rotating base **70**. The rotating vertical frame **71** can rotate the outer two inspection and cleaning or grooming modules **73** from 0 to a 45 degree angle relative to the center inspection and cleaning or grooming module **72**, and all three modules can rotate through an angle of 120 degrees relative to the a supporting base/rotating base **70**. The ability to rotate the angle of the inspection and cleaning or grooming modules (**72** and **73**) in two directions allows this embodiment to inspect and clean different surface angles of the water vessel or underwater structure, and while covering a wider area or a smaller focused area. This rotation ability also can place the inspection and cleaning or grooming modules (**72** and **73**) into a transport position so they lay flat with the bed of the remote inspection and cleaning or grooming vehicle **30** (shown in FIG. **7D**).

[0047] FIG. **7B** is a front view of the embodiment in FIG. **7A** illustrating that each inspection and cleaning or grooming module **72** and **73** contains four flood lights **76** to illuminate underwater, two ultrasonic sonar sensors **43** to detect distance to the cleaning or grooming target, four closed-circuit cameras **42** provide a panoramic view of the water vessel or underwater structure, and three fluorometric sensors **46** for detecting biofilms, all to support inspection. The actual cleaning or grooming process is performed by the inspection and cleaning or grooming module **72** and **73** consists of comprising two acoustic pressure shock wave generating devices **16** and six high pressure water jet nozzles **41**. The remote inspection and cleaning or grooming vehicle **30** provides a retractable cable **74** connection to a floating surface radio antenna **14** (shown also in FIG. **1**, FIG. **2** and FIG. **3**) for wireless communication with a remote operators station **32** (shown in FIG. **3**). The remote inspection and cleaning or grooming vehicle **30** provides a system hybrid cable **13** connection that will supply high pressure water for the water jet nozzles **41** used in cleaning or grooming and in filling an inflatable bladder **75**, and a vacuum hose connection to transfer murky water or the removed fouling material from the cleaning or grooming environment to a topside processing station. Additionally, the system hybrid cable **13** connections provide electrical power for all of the inspection and cleaning or grooming modules **72** and **73**, and an optical fiber connection for transmission of optical images and/or wired communication from each of the inspection and cleaning or grooming modules **72** and **73** to the remote operators station **32** (shown in FIG. **3**).

[0048] The inspection and cleaning or grooming modules **72** and **73** of FIG. **7B** refer to an inflatable bladder **75** that is shown inflated in FIG. **7C**. When inflated the inflatable bladder **75** extends from the inspection and cleaning or grooming modules **72** and **73** towards the water vessel or underwater structure surface **18** to provide a partial seal (partial because of the uneven topology of the organism fouling layers **19**). This way murky water or fouling debris contained in within the (salt or fresh) water environment can be pumped out and replaced with clear water. Providing clear water in the inspection environment improves the ability to observe with the underwater closed-circuit cameras **42** (shown in FIG. **7B**) or fluorometric sensors **46** (shown in FIG. **7B**) to detect biofilm **59**. The inflatable bladder **75** also provides a means to collect the fouling debris as it is being removed and transferred topside for proper disposal. The inflatable bladder **75** is partitioned within and between the inspection and cleaning or grooming modules **72** and **73** so that each bladder section can be separately pressurized to account for the potentially different spatial volumes the bladder will need to enclose. Each

bladder section can be inflated using pressurized air or pressurized (salt or fresh) water under the control of a local power and control system **40** contained within the inspection and cleaning or grooming modules **72** and **73**, or controlled remotely by a remote operator's station **32** (shown in FIG. 3) communicating with the inspection and cleaning or grooming modules **72** and **73**. The inflatable bladder **75** is made of flexible plastic materials with smooth surface to accomplish a good sealing with the vessel hull or underwater structure surface **18** and also to protect the integrity/no scratching of the vessel hull or underwater structure surface **18**.

[0049] The drawing of FIG. 8 is a cross sectional A-A view of a special embodiment of the outer inspection and cleaning or grooming modules **73** of FIG. 7B. The emphasis for the following description is of the acoustic pressure shock wave generating device **16** that operates identically for all the inspection and cleaning or grooming modules **72** and **73** of FIG. 7B. The outer inspection and cleaning or grooming module **73** is being described for it has the unique ability to rotate about the Y-axis as shown in FIG. 7A, whereas the center inspection and cleaning or grooming module **72** (in FIG. 7B) remains fixed about the Y-axis. The two acoustic pressure shock wave generating devices **16** utilize an ellipsoidal reflector **50** and a coupling membrane **26** to contain the reflector liquid **47** that is partially/localized superheated with an energy source to create a plasma bubble that during its oscillation produce the focused acoustic pressure shock waves **17** (shown in FIG. 5). The energy source for the acoustic pressure shock waves **17** occurs by applying a high voltage across two electrodes (similar to what was described for FIG. 4B). In FIG. 8 there is an anode tip **49** and a cathode tip **48** (the electrodes) that connect to a switched high voltage supply **80** with the most positive potential connected to the anode tip **49**. The power and control system **40** controls the voltage level, the repetition rate, and the duration that the voltage is applied to the electrodes (anode tip **49** and cathode tip **48**). Applying the high differential voltage between the electrodes produces an electrical current in the reflector liquid **47** environment flowing from the anode tip **49** to the cathode tip **48**. The electrical current is occurring in the geometric focal point F_1 **51** (see FIG. 5) of the ellipsoidal reflector **50**, and the magnitude of the electrical current increases while the high voltage is applied. As the magnitude of the electrical current increases the reflector liquid **47** in the region of the focal point F_1 **51** is superheated to produce a plasma bubble that grows rapidly in size as the electrical current increases in magnitude. The rapid expansion and then collapse (when the high voltage between the electrodes will stop the flow of electrical current between the electrodes) of the plasma bubble produce the acoustic pressure shock waves **17**, which are then focused toward the focal volume **58** (see FIG. 5). The embodiments of FIG. 7A and FIG. 7B use six high pressure water jet nozzles **41** to augment the acoustic pressure shock wave generators **16** action on the fouling organism layer **19** and biofilm layer **59** (see FIG. 5). There is an electronic valve **83** associated with each high pressure water jet nozzle **41** to enable individual on/off control. A module hybrid cable **85** integrates a power cable, fiber optic cable, pressurized water tube, and a vacuum tube in one with an external protective jacket to connect to the inspection and cleaning or grooming module **73**. The power cable can provide one or more voltages to power the systems in the inspection and cleaning or grooming module **73**, however the switched high voltage supply **80** would be best located within the inspection and cleaning or grooming module **73** to reduce power loss due to cable length. The pressurized water tube (from module hybrid cable **85**) would be the source of pressurized

water to the high pressure water jet nozzles **41** and potentially the source for filling the inflatable bladder **75**. Alternatively the inflatable bladder **75** could be filled by pressurized air but that would require another tube be added to the module hybrid cable **85**. The vacuum tube is the source for extracting fouling debris contained within the cleaning or grooming environment trapped by the inflatable bladder **75**. A similar module hybrid cable **85** would connect to the inspection and cleaning or grooming module **72** (the central module presented in FIG. **7A**). This drawing also illustrates the means of rotating the inspection and cleaning or grooming modules **72** and **73** in both X and Y rotation. The X-motor with gear head **82** rotates all of the inspection and cleaning or grooming modules **72** and **73** through a 120 degree angle about the X-axis (refer to bottom of FIG. **8**) by its connection to the rotating base **70**, which in turn rotates about the X-axis the vertical frame **71** that each of the inspection and cleaning or grooming modules **72** and **73** are mounted to (refer to FIG. **7A**). The Y-motor with gear head **81** rotates the inspection and cleaning or grooming module **73** about the Y-axis from 0 to 45 degrees relative to the center of the inspection and cleaning or grooming module **72** (in FIG. **7B**). The combination of the two angular movements allow the system to adapt to the pitch and curvature of a water vessel's hull or other underwater structures for inspection and cleaning or grooming and to also position all of the inspection and cleaning or grooming modules **72** and **73** in a home position for transport as shown in FIG. **7D**. On the same FIG. **8** other elements that comprise the cleaning or grooming modules **72** and **73** can be seen as the fluorometric sensors **46**, flood lights **76**, closed circuit cameras **42** and ultrasonic sonar sensors **43**.

[0050] The drawing of FIG. **9** is another embodiment of a cross sectional A-A view of an outer inspection and cleaning or grooming module **73** of FIG. **7B**. The difference being that the two acoustic pressure shock wave generating devices **16** utilize a different source of energy than FIG. **8** to create acoustic pressure shock waves **17** (see FIG. **5**). In the embodiment of FIG. **9** the energy source for the acoustic pressure shock wave **17** occurs from two lasers **90** for each acoustic pressure shock wave generator **16**. In other embodiments three or four lasers may be used to generate the acoustic pressure shock waves **17**, but for simplicity of the drawing in FIG. **9** an embodiment with two lasers **90** will be presented. The laser **90** output is coupled by the fiber optic cable **93** to the optical feed-through assembly **92**. The optical feed-through assembly **92** is used to convey and direct the optical energy from the laser **90** into the reflector liquid **47** at the focal point F_1 **51** (see FIG. **5**) of the ellipsoidal reflector **50**, while protecting the internal elements of the optical feed-through assembly that in part ends with an optical lens or beam collimator **94** to direct the optical energy to the focal point F_1 **51**. The amplitude, modulation, and duration of the laser output is precisely controlled by the power and control system **40** so that the reflector liquid **47** environment at the focal point F_1 **51** is superheated to create a plasma bubble that rapidly expands and collapses transforming the heat into acoustic pressure shock waves that possess both a compressive and tensile force behavior in each wave. Though the embodiment of FIG. **9** shows two laser sources for each acoustic pressure shock wave generator **16**, one or more laser sources can be used based on cost versus benefit. Each of the shock wave generating devices **16** in FIG. **9**, as in FIG. **8** and FIG. **7B**, are augmented by six of the pressurized water jet nozzles **41** to assist in the removal of the marine or aquatic fouling organism layer **19** and biofilm layer **59** (see FIG. **5**). All other features and

functions of the embodiment in FIG. 9 are identical to those from FIG. 8.

[0051] The drawing of FIG. 10 is another embodiment of a cross sectional A-A view of an outer inspection and cleaning or grooming module 73 of FIG. 7B. The difference from the previous embodiments is that the two acoustic pressure shock wave generating devices 16 utilize a different source of energy than FIG. 8 and FIG. 9 to create acoustic pressure shock waves 17 (see FIG. 5). In the embodiment of FIG. 10 the energy source for the acoustic pressure shock wave occurs from a piezoelectric crystals or piezoelectric fiber composite structure 102 embodied in each acoustic pressure shock wave generator 16. The piezoelectric crystals or piezoelectric fiber composite structure 102 is a flexible substrate for the individual piezoelectric crystals or piezoelectric fiber groups 104 and provides the power distribution to the individual piezoelectric crystals or piezoelectric fiber groups 104. Power is applied 180 degrees out of phase with adjacent piezoelectric crystals or piezoelectric fiber groups 104 to generate an alternating pressure wave by the flexing of the piezoelectric crystals or piezoelectric fiber composite structure's 102 substrate. Piezoelectric crystals or piezoelectric fiber groups 104 are distributed along the ellipsoidal reflector 50 to align with the focal point (F_1) 51 (see also FIG. 5) of the ellipsoidal reflector 50. Each piezoelectric crystals or piezoelectric fiber group 104 is energized by a high voltage pulse generator 100 that when energized produce an acoustic pressure shock wave directed toward the focal point (F_2) 52 of the ellipsoidal reflector 50 (see FIG. 5). When all piezoelectric crystals or piezoelectric fiber group 104 are energized concurrently the multiple acoustic pressure shock waves combine through superposition and interference in the reflector liquid 47 to produce a larger amplitude acoustic pressure shock wave 17 (see FIG. 5). Each of the acoustic pressure shock wave generating devices 16, similar to FIG. 8, FIG. 9 and FIG. 7B, are augmented by six of the pressurized water jets nozzles 41 to assist in the removal of the marine or aquatic fouling organism layer 19 and biofilm layer 59 (see FIG. 5). All other features and functions of the embodiment in FIG. 10 are identical to FIG. 8.

[0052] The drawing of FIG. 11 is another embodiment of a cross sectional A-A view of an outer inspection and cleaning or grooming module 73 of FIG. 7B. The differences from the previous embodiments is that the two acoustic pressure shock wave generating devices 16 utilize a different source of energy than FIG. 8, FIG. 9, and FIG. 10 to create acoustic pressure shock waves 17 (see FIG. 5). In the embodiment of FIG. 11 a piston cylinder 112 encloses an electromagnetic driven piston 114 and a cylinder fluid 116, with the later being sealed by a diaphragm 118. The piston power source 110 generates a high frequency pulse into the piston coil 116 that in turn drives the magnetic piston rod 115 connected to piston 114 rapidly toward the diaphragm 118 through electromagnetic force creating an acoustic planar wave (not shown in FIG. 11 to maintain the clarity of the figure). The resulting acoustic planar wave is moving in the fluid-filled cavity 117 towards the acoustic lens 119 that is focusing the planar wave and thus creating acoustic pressure shock waves 17 (as described in FIG. 5) that are focused towards the targeted area. Each of the shock wave generating devices 16, as in FIG. 8, and FIG. 9, FIG. 10 and FIG. 7B, are augmented by six of the pressurized water jets nozzles 41 to assist in the removal of the marine or aquatic fouling organism layer 19 and biofilm layer 59 (see FIG. 5). All other features and functions of the embodiment in FIG. 11 are identical to FIG. 8.

8.

[0053] The drawing of FIG. 12 is a diagram of a control and power system 40 that is contained in the inspection and cleaning or grooming module 15 of FIG. 4B or the outer inspection and cleaning or grooming modules 73 of FIG. 7B. The module processor 120 can contain expert system software to perform the inspection and cleaning or grooming autonomously, or be partially controlled by the remote operator's station 32, as described in FIG. 3. In a partially controlled system, the remote operator's station 32 would communicate the high level command to invoke a task and the module processor 120 would perform all of the low level actions in support of the task. The low level actions would be part of the module processor's 120 inherent knowledge base.

[0054] In order to provide a directional capability for inspection and cleaning or grooming each acoustic pressure shock wave generator 16 in FIG. 4A requires an X-axis motor controller 128 and Y-axis motor controller 129 (both shown in FIG. 12) to tilt the direction of the reflector 24 in FIG. 4B either vertically or laterally, respectively, toward the specific cleaning or grooming target. There would be seven X-axis motor controllers 128 and seven Y-axis motor controllers 129 to support the seven acoustic pressure shock wave generator 16 in the embodiment of FIG. 4A. In the embodiment of FIG. 7B, FIG. 8, FIG. 9, FIG. 10 and FIG. 11, there is one X-axis motor controller 128 needed to rotate both of the outer inspection and cleaning or grooming modules 73 and the center inspection and cleaning or grooming module 72 together about the X axis, and two Y-axis motor controller 129 to rotate independently each of outer inspection and cleaning or grooming modules 73 about their Y axis.

[0055] The diagrams of FIG. 12 and FIG. 13 contain the power distribution subsystem 121 to create the specific power sources needed by the inspection and cleaning or grooming modules 15 of FIG. 4B or modules 72 and 73 of FIG. 7B and a hybrid cable interface 122 to connect to the electrical cables and hoses supplied by the remote cleaning or grooming vehicle 10 in FIG. 1 or FIG. 2, or the inspection and cleaning or grooming vehicle 30 in FIG. 7A. A remote communication processor 123 is present in the diagram of FIG. 12 and FIG. 13 to facilitate fast communication with the remote operators station 32 and offload that task from the module processor 120. To support the inspection activities the diagram contains a lighting control function (dotted box) integrated in the power distribution subsystem 121 to adjust the intensity of the underwater lighting, a sonar range finder interface 124 to measure distance to an object and also to prevent collision with an underwater structure, and an imaging interface 125 to process the output from the closed-circuit camera(s) and fluorometric sensor(s). The imaging interface 125 may process the inspection images itself to make autonomous decisions regarding cleaning or grooming or can forward the images to remote operator's station 32 using an optical fiber connection or a wireless connection. To support the cleaning or grooming functions of the module, a water jet interface 126 is provided to enable turning the water jets on and off, or if the jet nozzle can be rotated as in FIG. 3A the water jet control interface 126 would perform that function as well. A cleaning or grooming head power interface 127 provides the specialized power to each shock wave generator 16 (in FIG. 3A and FIG. 7B). This specialized power would be in the form that is compatible with the mode of generating the

shock wave, i.e. electrode discharge in FIG. 8, laser heating in FIG. 9, piezoelectric fiber excitation described for FIG. 10, or the electromagnetic excitation utilized in FIG. 11.

[0056] The module processor **120** of FIG. **12** controls the voltage output level, the repetition rate and the enabling of the cleaning or grooming head power interface **127**. In the embodiment of FIG. **4A** there would be seven cleaning or grooming head power interfaces **127** to support each acoustic pressure shock wave generator **16**. To support the embodiment of FIG. **7B** there would be two cleaning or grooming head power interfaces **127** for each of the outer inspection and cleaning modules **73**.

[0057] The drawing of FIG. **13** is a diagram of a control and power system **40** contained in the center inspection and cleaning or grooming module **72** of FIG. **7B**. There is an inter-module communication link **131** between the center inspection and cleaning or grooming module **72** and the outer inspection and cleaning or grooming modules **73** (of FIG. **7B**) to provide a master and slave control system hierarchy. The center inspection and cleaning or grooming module **72** in this embodiment is the master and the outer inspection and cleaning or grooming modules **73** would be the slaves. The purpose being that the central module processor **130** of the center inspection and cleaning or grooming module **72** would be the initiator in managing the coordination of tasks through the use of the expert system software it contains, or the receipt of commands from the remote operator's station **32**. This type of communication interface could then eliminate the remote communication processor **123** described in FIG. **12**. The remainder of the diagram and functions of FIG. **13** is the same as FIG. **12** with the exception there are no x/y motor controllers needed.

[0058] While the invention has been described with reference to exemplary structures and methods in embodiments, the invention is not intended to be limited thereto, but to extend to modifications and improvements within the scope of equivalence of such claims to the invention.

REFERENCES CITED IN THE DESCRIPTION

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Patentkrav

1. Apparat til rengøring eller pleje af en overflade neddykket i vand omfattende:

en indretning til at generere akustisk trykchokbølge (16), som inkluderer en reflektor (24); et styresystem (40) til indretningen til at generere trykchokbølge (16) konfigureret til at styre akkumulativ chokenergi til et energiniveau, som fjerner udvalgt uønsket materiale, som dækker en overflade neddykket i vand (18) uden at tilføre materialepåvirkning, malingsskade eller coatingskade til den underliggende neddykkede overflade (18);

10 kendetegnet ved, at,

reflektoren (24) er dækket af en membran (26), og et fjernstyret undervandsfartøj (10), som inkluderer trykmotorer (11), er koblet til indretningen til at generere akustisk trykchokbølge (16); og

fartøjet (10) inkluderer et inspektions- og rengørings- eller plejemodul (15) omfattende indretningen til at generere akustisk trykchokbølge (16), hvor inspektions- og rengørings- eller plejemodulet (15) er drejeligt omkring både en X-akse med en X-motor med gearhoved (82) og Y-akse med en Y-motor og gearhoved (81) og inkluderer en eller flere undervandssensorer (43) konfigureret til at detektere afstanden mellem indretningen til at generere akustisk trykchokbølge og den neddykkede overflade, hvor inspektions- og rengørings- eller plejemodulet (15) er operativt koblet til styresystemet (40), som aktiverer indretningen til at generere akustisk trykchokbølge (16), roterer rengørings- eller plejemodulet (15) omkring X-aksen og Y-aksen, og dirigerer det fjernstyrede undervandsfartøj (10).

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2. Apparatet ifølge krav 1, yderligere omfattende en flerhed af indretninger til at generere akustisk trykchokbølge hver konfigureret til at producere en fokuseret chokbølge, som har en kompressionsfase med en højere trykamplitude end en anden strækningsfase, som følger og er længerevarende end kompressionsfasen.

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3. Apparatet ifølge kravene 1 eller 2, hvor inspektions-, rengørings- eller plejemodulet inkluderer et eller flere lys og et eller flere kameraer.

4. Apparatet ifølge et hvilket som helst af kravene 1 til 3, hvor inspektions-, rengørings- eller plejemodulet (15) inkluderer en eller flere fluidstråledyser (41).
5. Apparatet ifølge et hvilket som helst af kravene 1 til 4, hvor indretningen til at generere akustisk trykchokbølge (16) inkluderer en af en anode og katode af en elektrohydraulisk chokbølgegenerator, en laser, piezoelektriske fibre, piezoelektrisk krystalkompositstruktur og elektromagneter.
- 10 6. Apparatet ifølge et hvilket som helst af kravene 1 til 5, hvor indretningen til at generere akustisk trykchokbølge (16) inkluderer en af en elliptisk reflektor (50) og parabolisk reflektor (60).
- 15 7. Apparatet ifølge et hvilket som helst af kravene 1 til 6, hvor reflektoren (24) er en kipbar reflektor konfigureret til at justere lokationen af en målchokbølgevolumen (58) af styresystemet (40).
- 20 8. Fremgangsmåde omfattende påføring af akustiske trykchokbølger undervands til en neddykket overflade i en målchokbølgevolumen (58) fra et fjernstyret undervandsfartøj (10)), hvorved den neddykkede overflade (18) rengøres eller plejes ved påføring af de akustiske trykchokbølger, hvor de akustiske trykchokbølger har en kompressionsfase efterfulgt af en anden strækningsfase, og hvor akkumulativ chokenergibølger i en målchokbølgevolumen (58) styres til at fjerne uønsket materiale, som dækker den neddykkede overflade (18) i målchokbølgevolumenen (58) uden at tilføre materialepåvirkning, malingsskade eller coatingskade til den underliggende neddykkede overflade (18) i målchokbølgevolumenen (58); **kendetegnet ved**, fjerndetektering af en lokation på den neddykkede overflade (18) til at dirigere de akustiske trykchokbølger og koordinere en eller flere indretninger til at generere akustisk trykchokbølge (16) ved rotation af et rengørings- eller plejemodul (15) af et fjernstyret undervandsfartøj (10) omkring en X-akse og Y-akse til at påføre de akustiske trykchokbølger til nævnte lokation.
- 30

9. Fremgangsmåden ifølge krav 8, yderligere omfattende fjernstyring af trykmotorer (11) og magnetisk tiltrækning (22) af det fjernstyrede undervandsfartøj (10) til påføring af de akustiske trykchokbølger til nævnte lokation.

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10. Fremgangsmåden ifølge kravene 8 eller 9, yderligere omfattende fjernstyring af akkumulativ energi leveret af en eller flere indretninger til at generere akustisk trykchokbølge (16), som påfører de akustiske trykchokbølger til den neddykkede struktur (18).

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11. Fremgangsmåden ifølge et hvilket som helst af kravene 8 til 10, yderligere omfattende anvendelse af en eller flere fluidstråledyser (41) til at forbedre rengøring eller pleje med akustiske trykchokbølger.

15 **12.** Fremgangsmåden ifølge et hvilket som helst af kravene 8 til 11, yderligere omfattende støvsugning af rester løsrevet fra den neddykkede overflade (18).

13. Fremgangsmåden ifølge et hvilket som helst af kravene 8 til 12, hvor de akustiske trykchokbølger påføres af en af en elektrohydraulisk indretning til at
20 generere akustisk trykchokbølge, en elektromagnetisk indretning til at generere akustisk trykchokbølge, en laserindretning til at generere akustisk trykchokbølge, en indretning til at generere chokbølge af piezoelektriske fibre, og en piezoelektrisk krystalindretning til at generere akustisk trykchokbølge.

25 **14.** Fremgangsmåden ifølge et hvilket som helst af kravene 8 til 13, yderligere omfattende påføring af de akustiske trykchokbølger igennem en koblingsmembran (26) mellem en indretning til at generere akustisk trykchokbølge (16) og den neddykkede overflade (18).

30 **15.** Fremgangsmåden ifølge et hvilket som helst af kravene 8 til 14, hvor den neddykkede overflade (18) er en del af et skib, en båd, fartøj eller platformsstruktur.

DRAWINGS

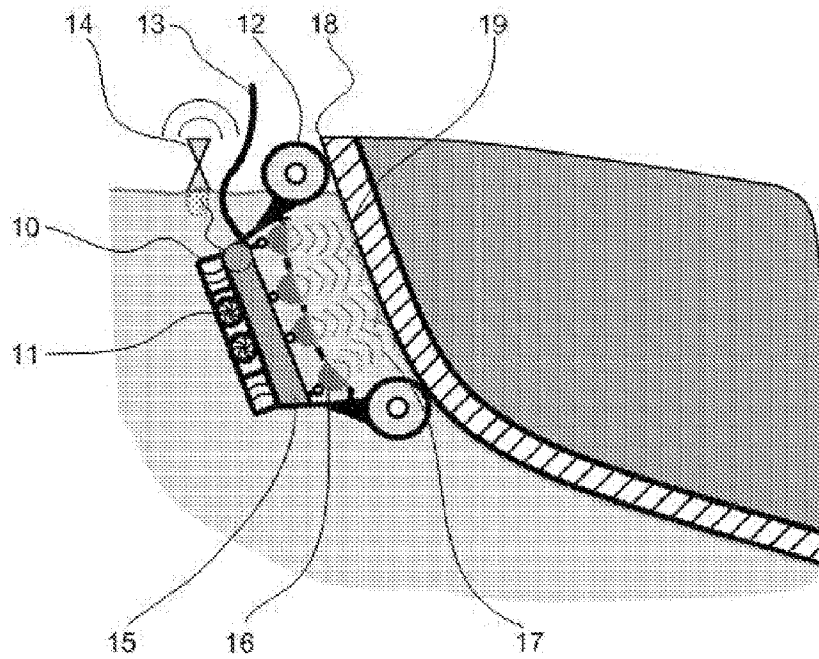


FIG. 1

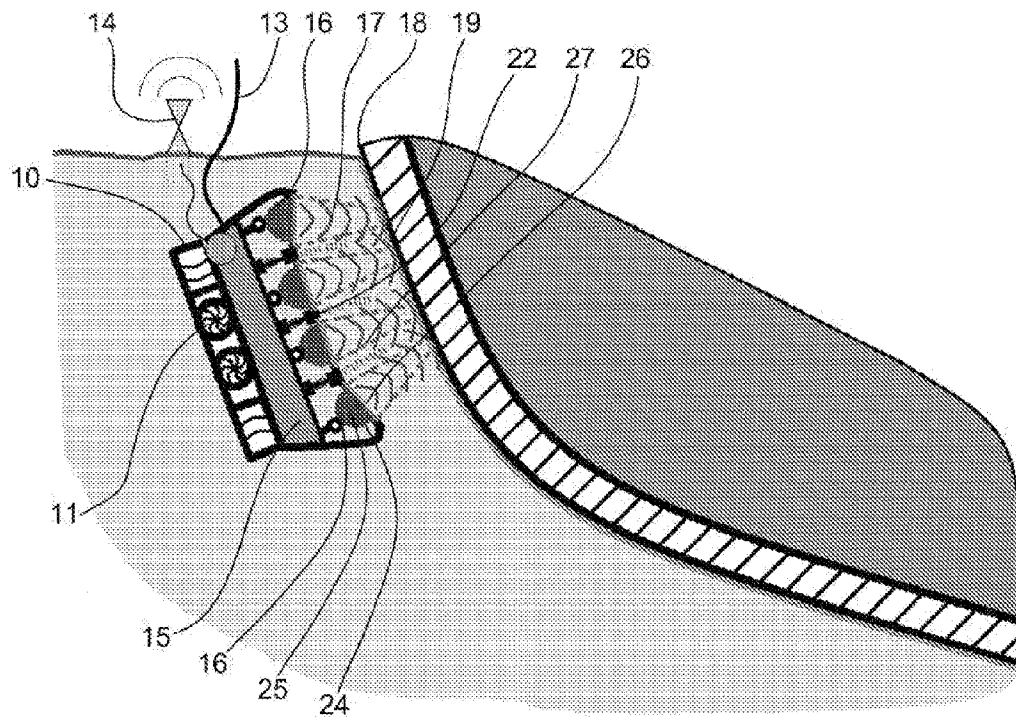


FIG. 2

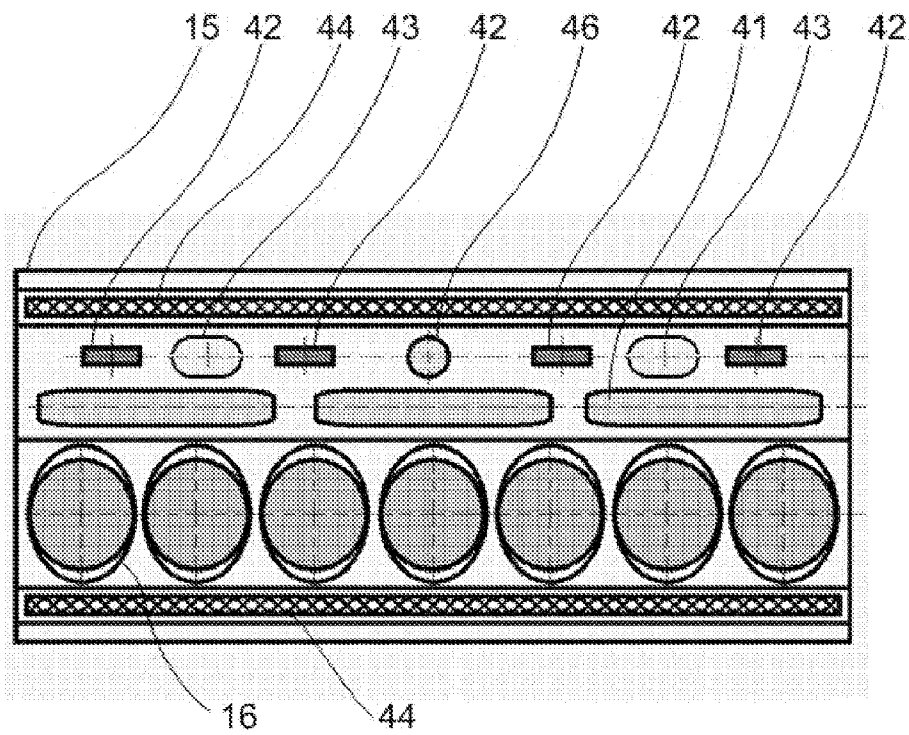


FIG. 4A

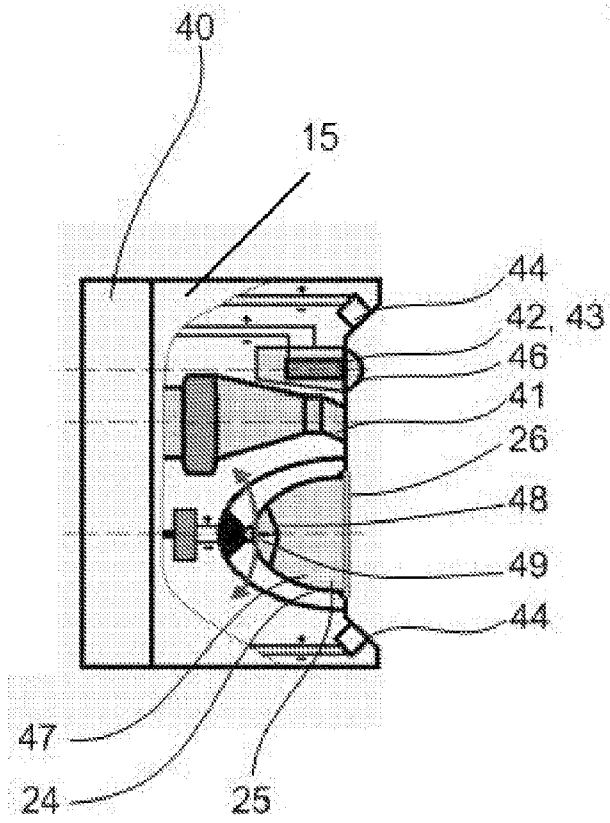


FIG. 4B

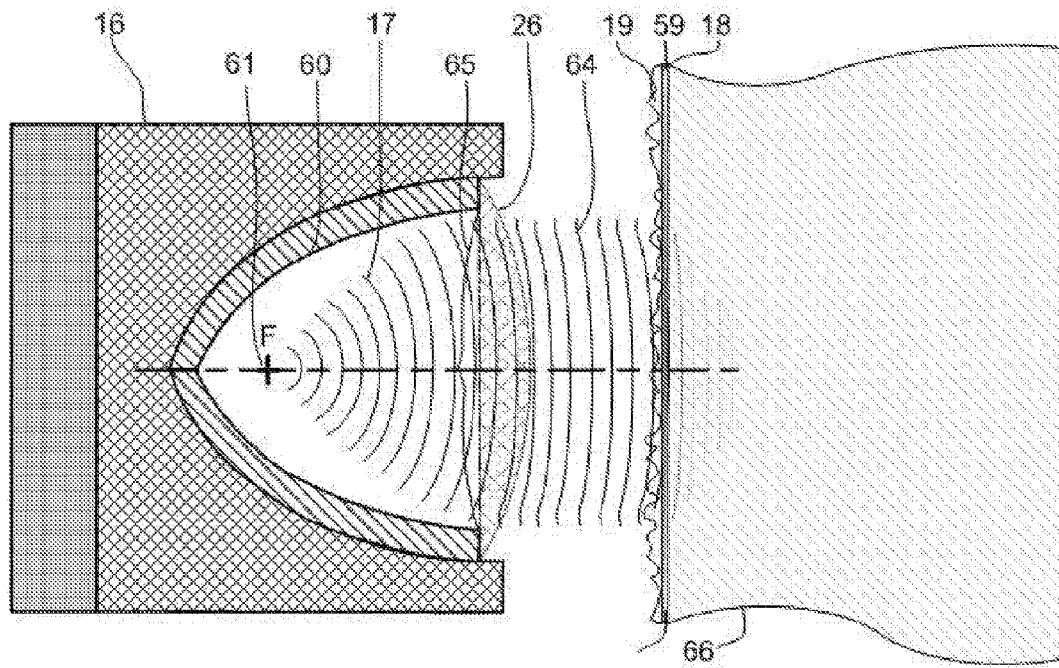


FIG. 6

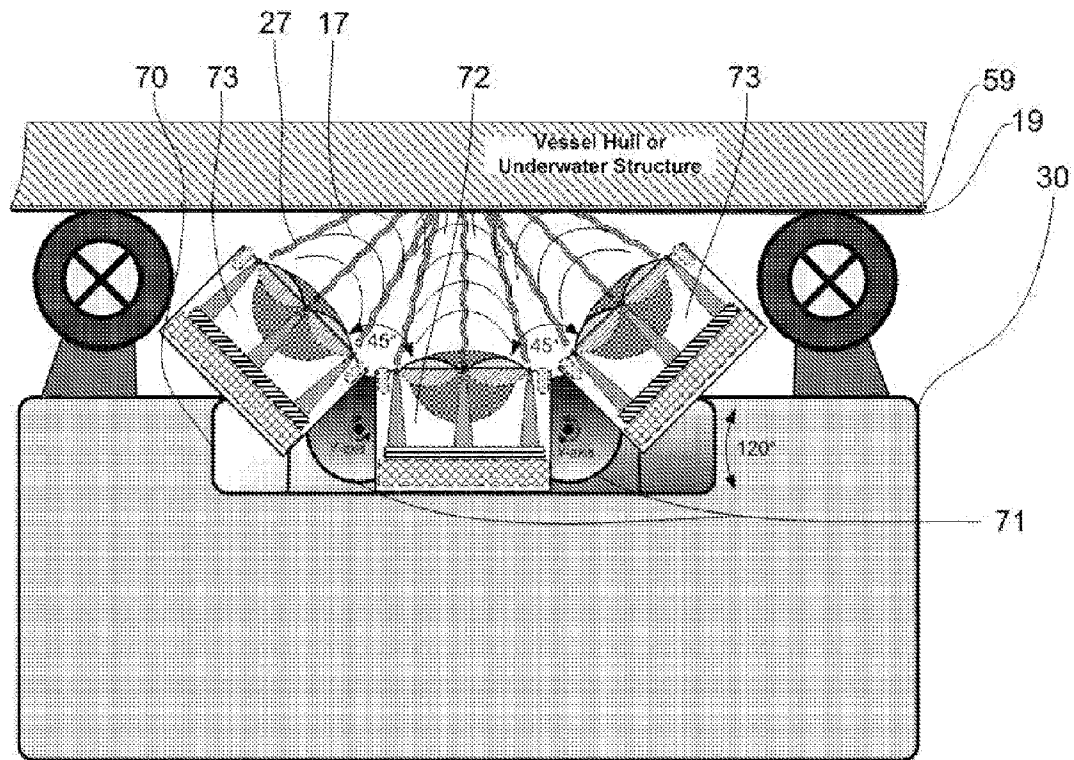


FIG. 7A

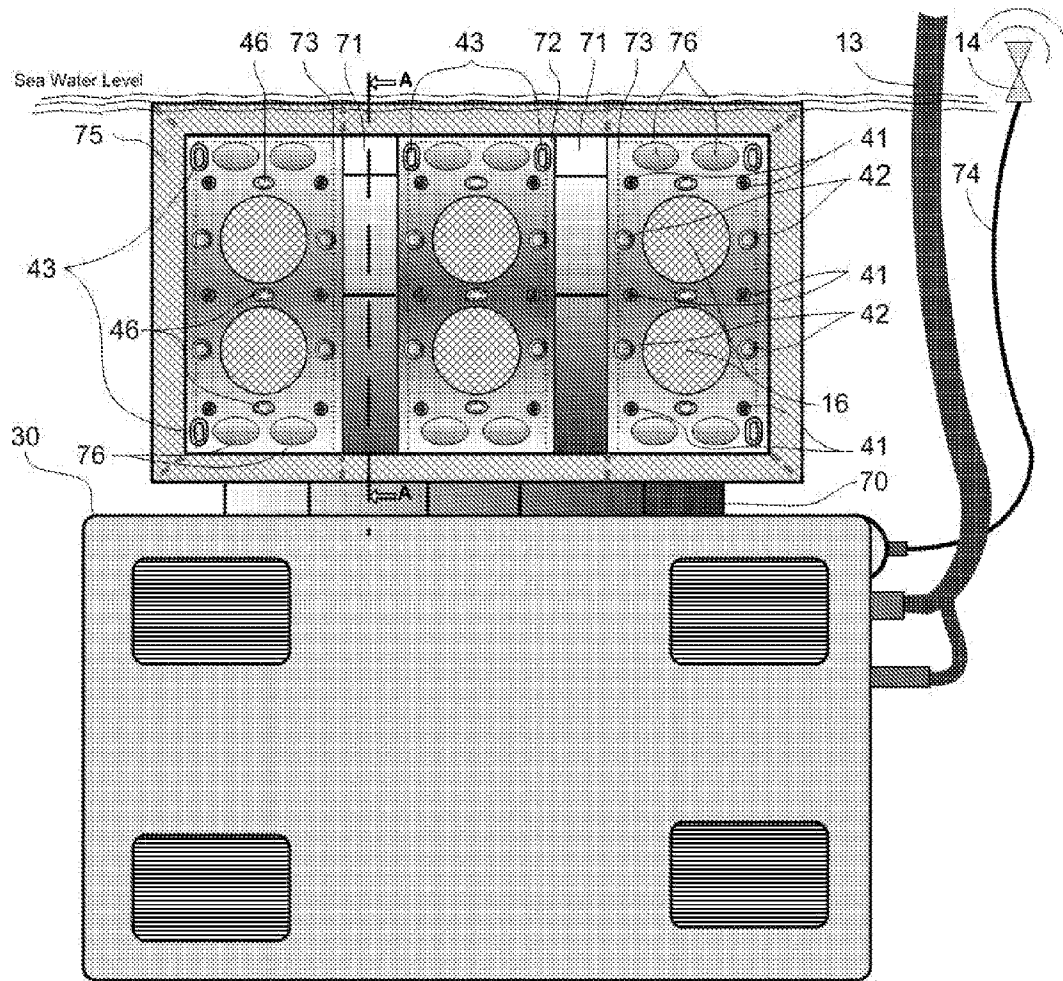


FIG 7B

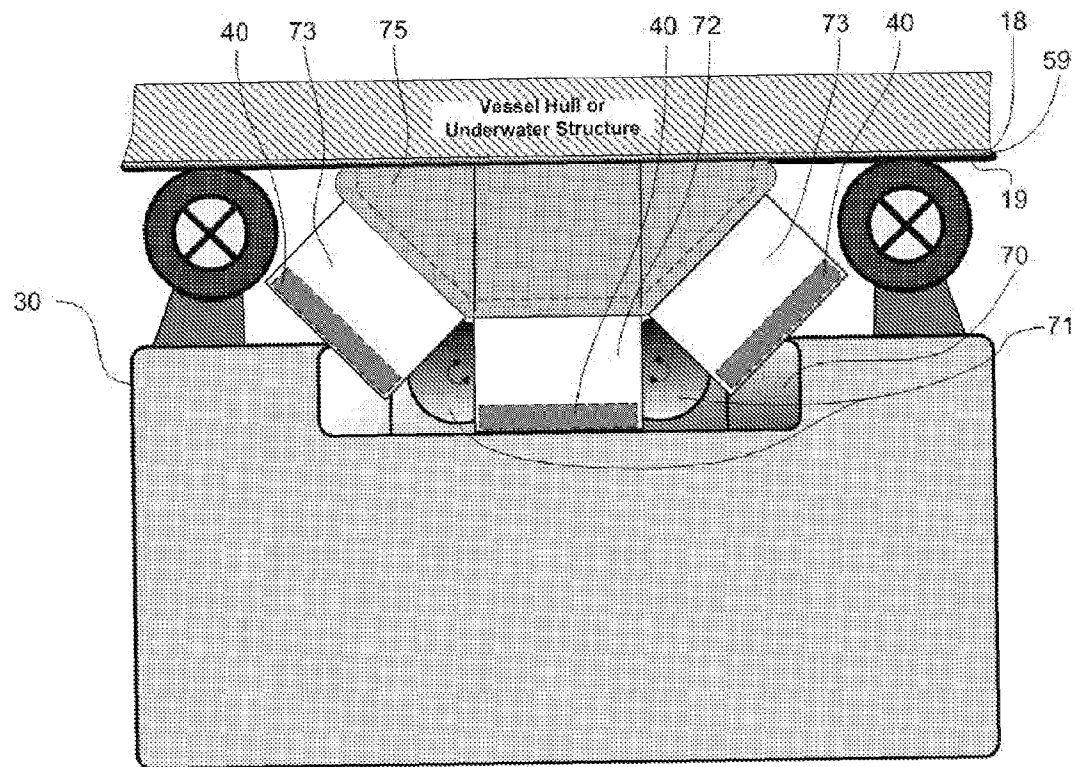


FIG. 7C

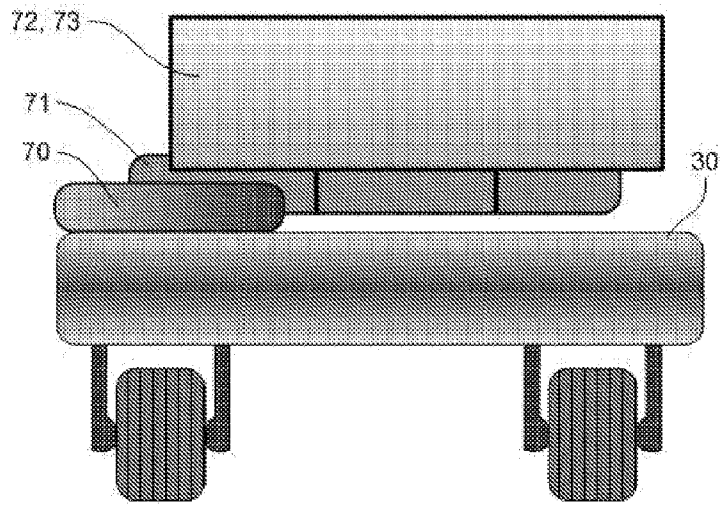


FIG. 7D

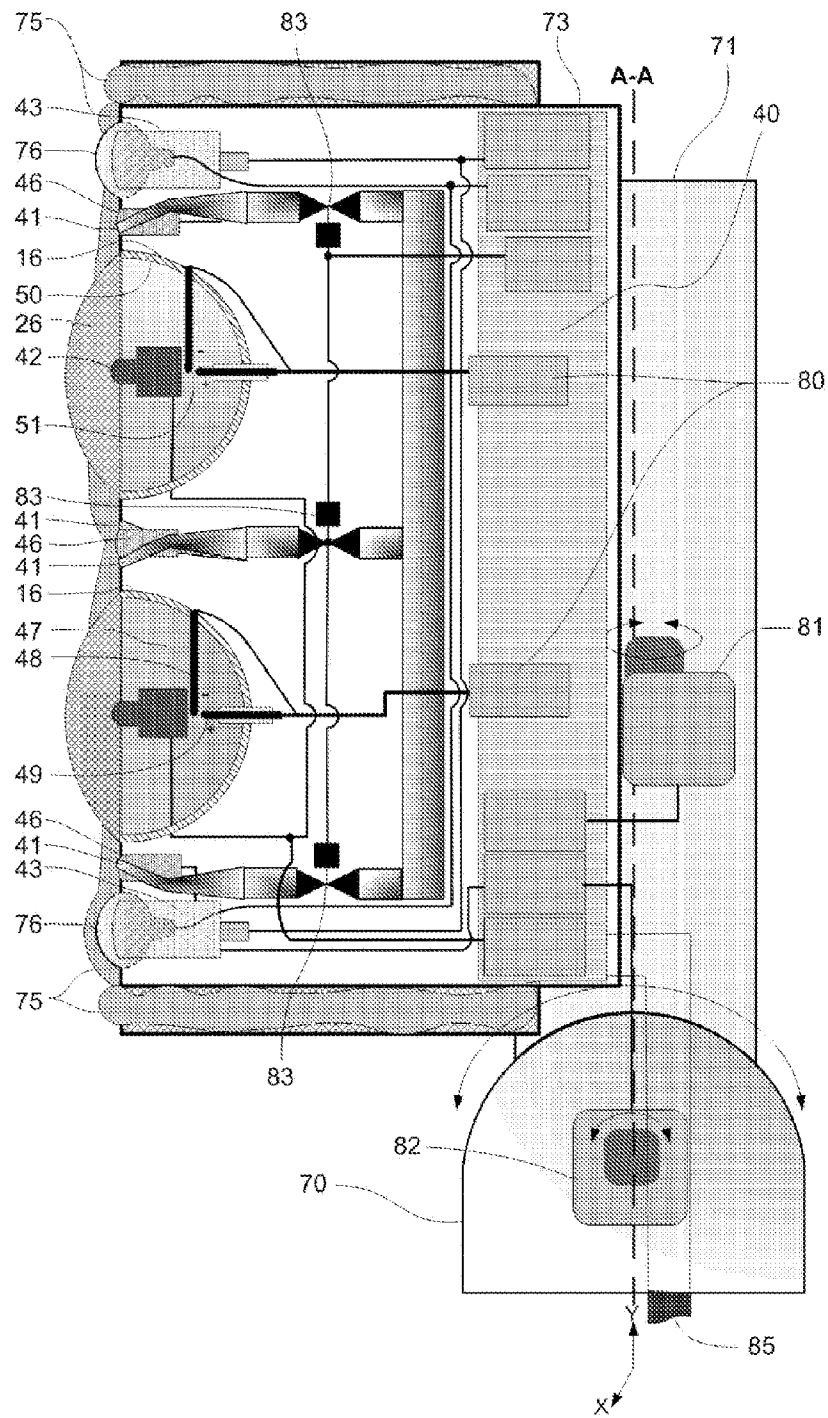


FIG. 8

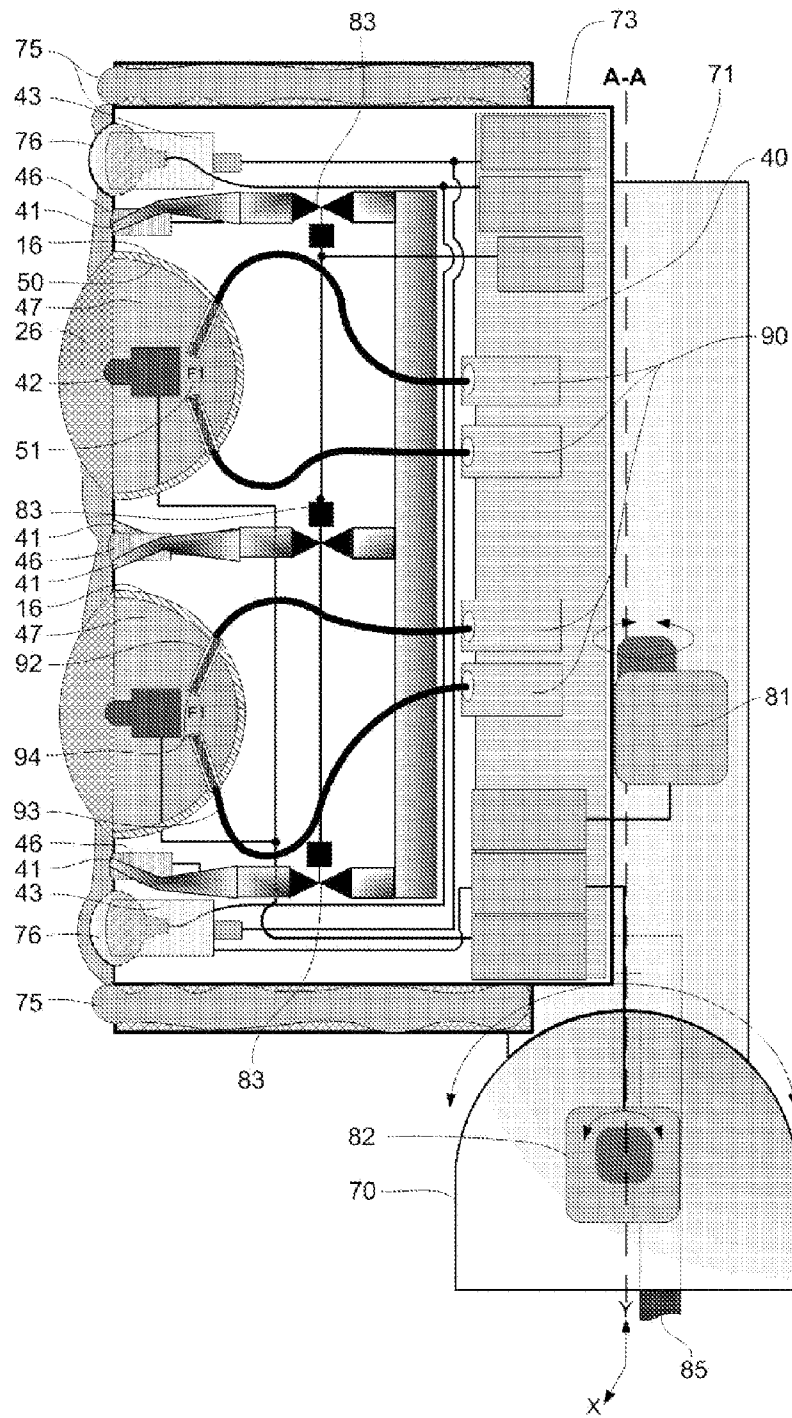


FIG. 9

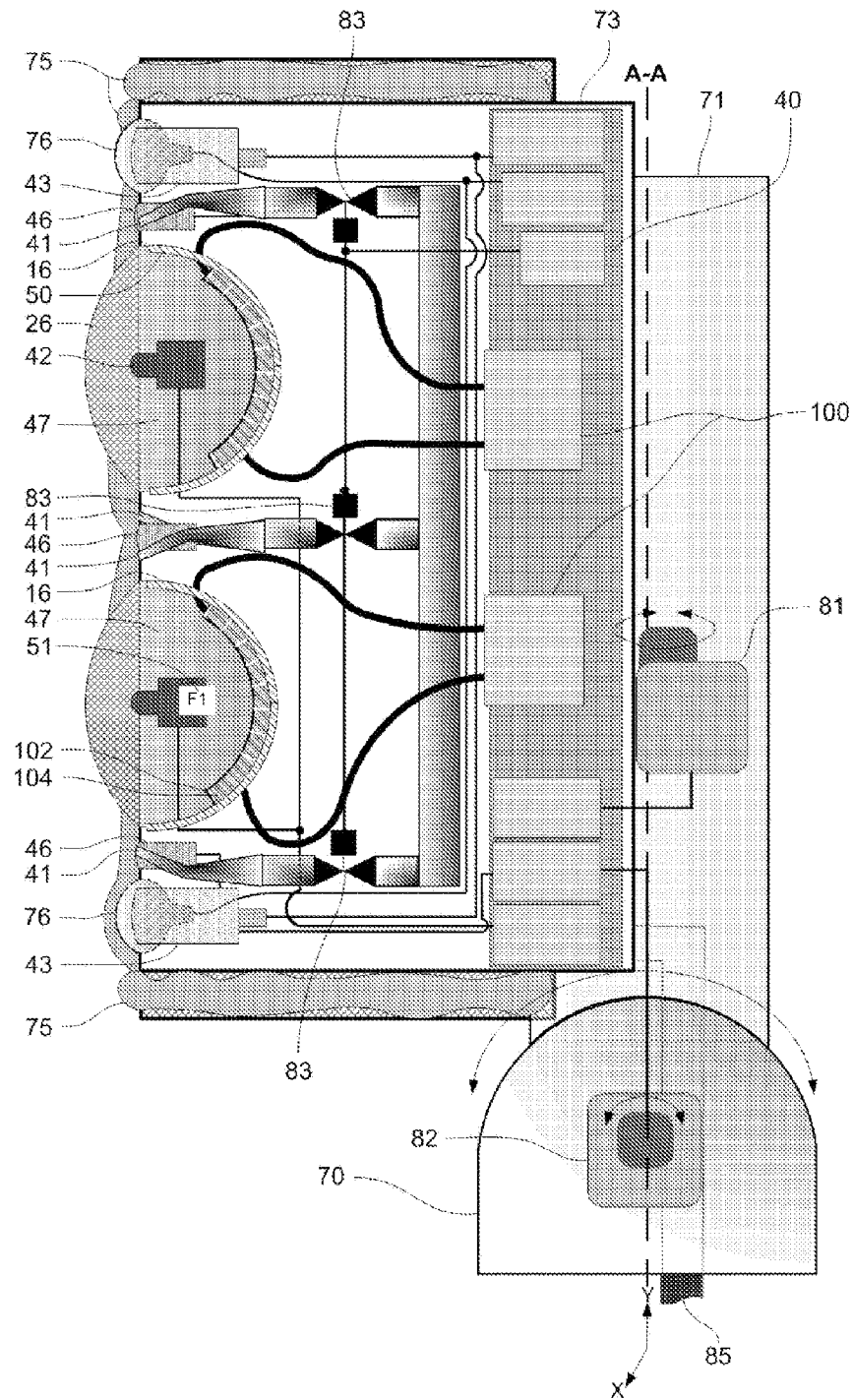


FIG. 10

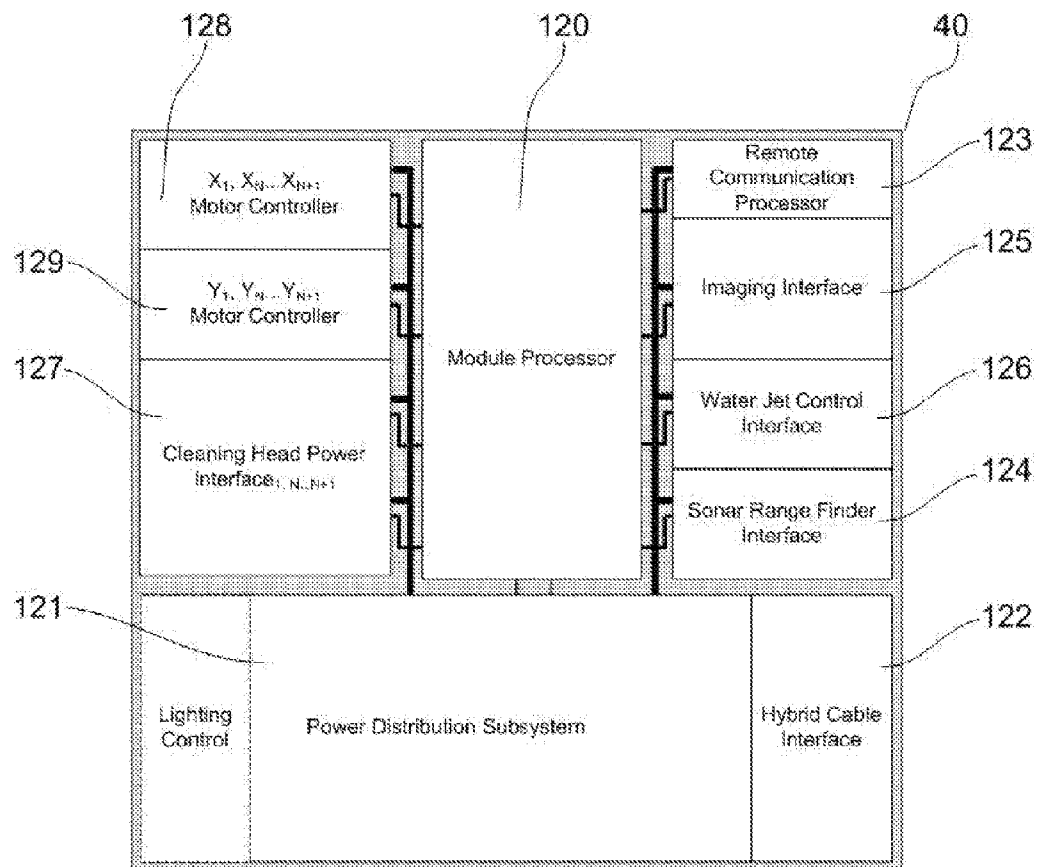


FIG. 12

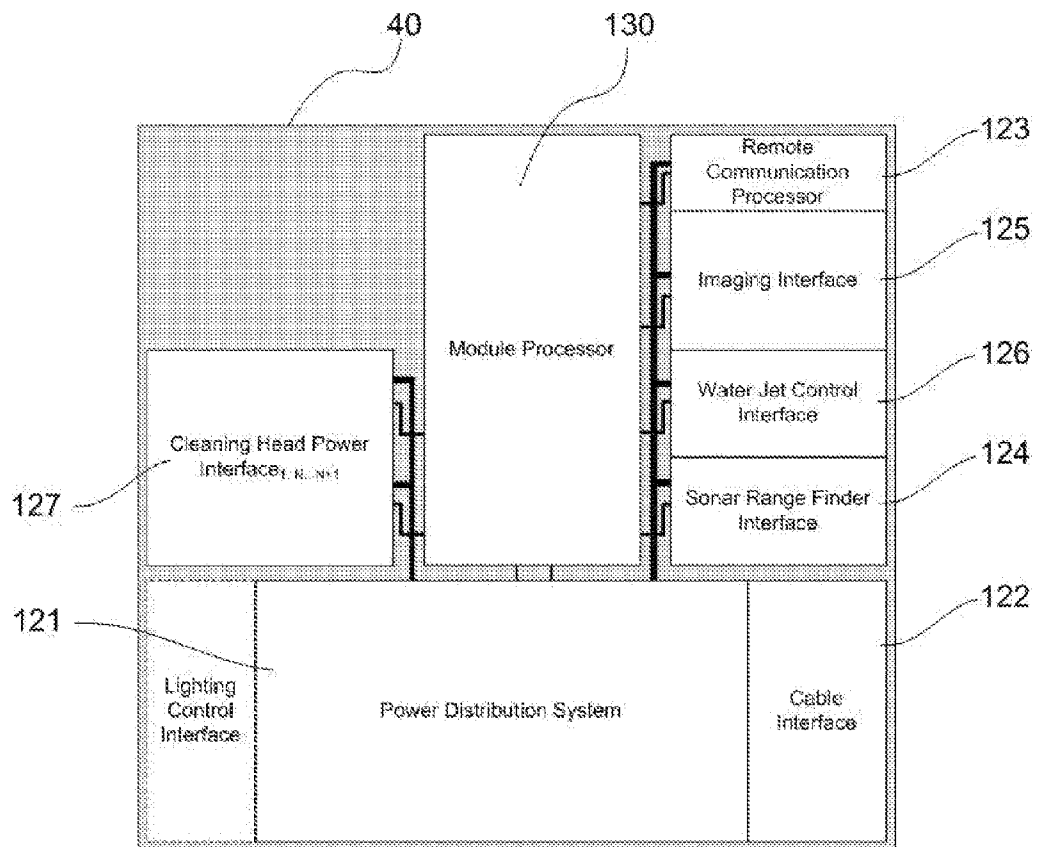


FIG. 13