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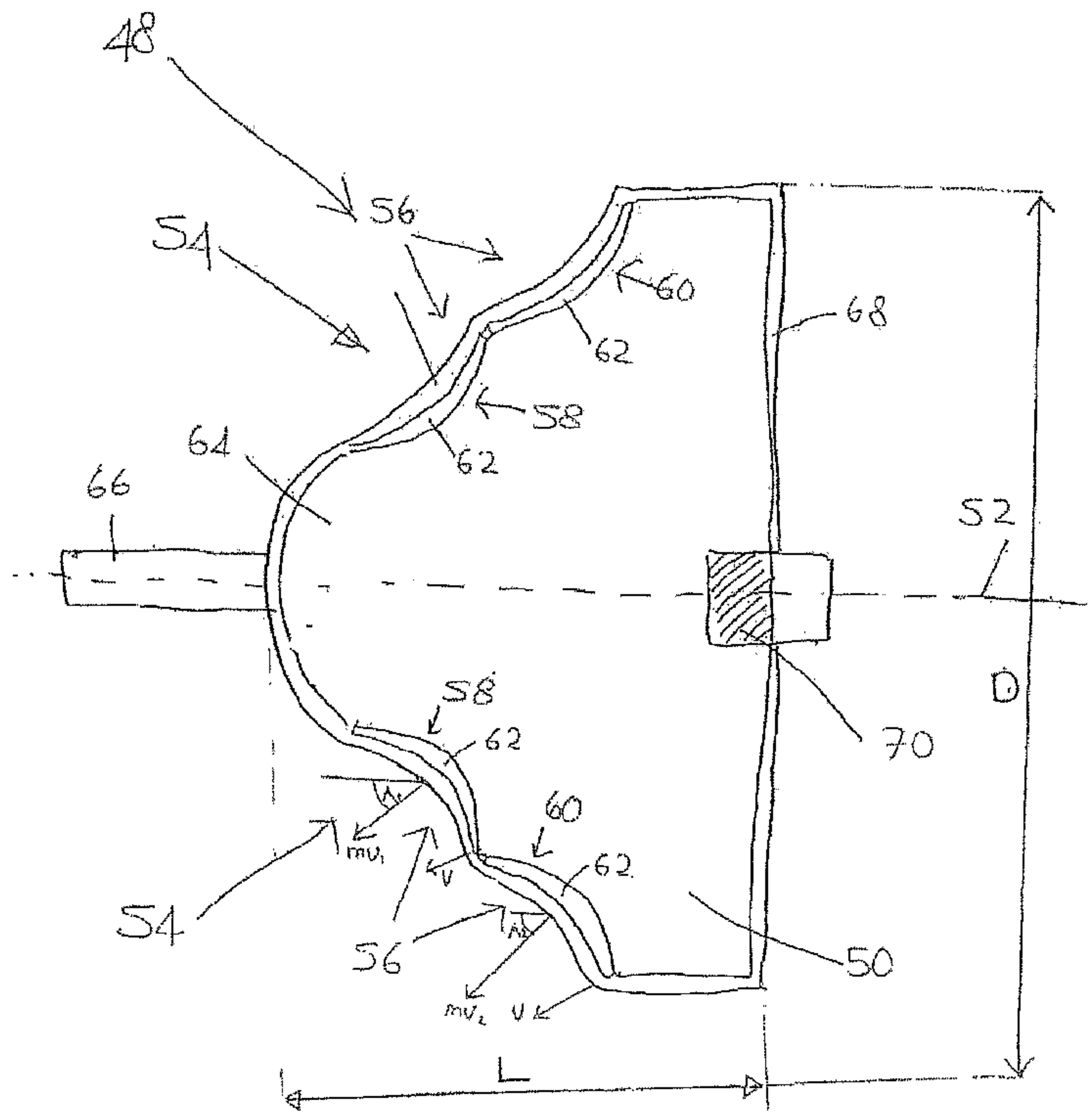


(57) Abrégé/Abstract:
A warhead configuration for forming a hole through a wall of a target, the warhead configuration comprising a charge of explosive material and a liner. The charge has an axis and a front surface. The front surface includes two annular front surface portions, an inner and an outer annular portion, circumscribing the axis. Each of the annular front surface portions is configured so as to exhibit a concave profile as viewed in a cross-section through the charge parallel to the axis. The liner includes a first liner disposed adjacent to the inner annular portion and a second liner disposed adjacent to the outer annular portion such that, when the charge is detonated, material from the first liner is formed into a first expanding explosively formed ring and material from the second liner is formed into a second explosively formed ring.

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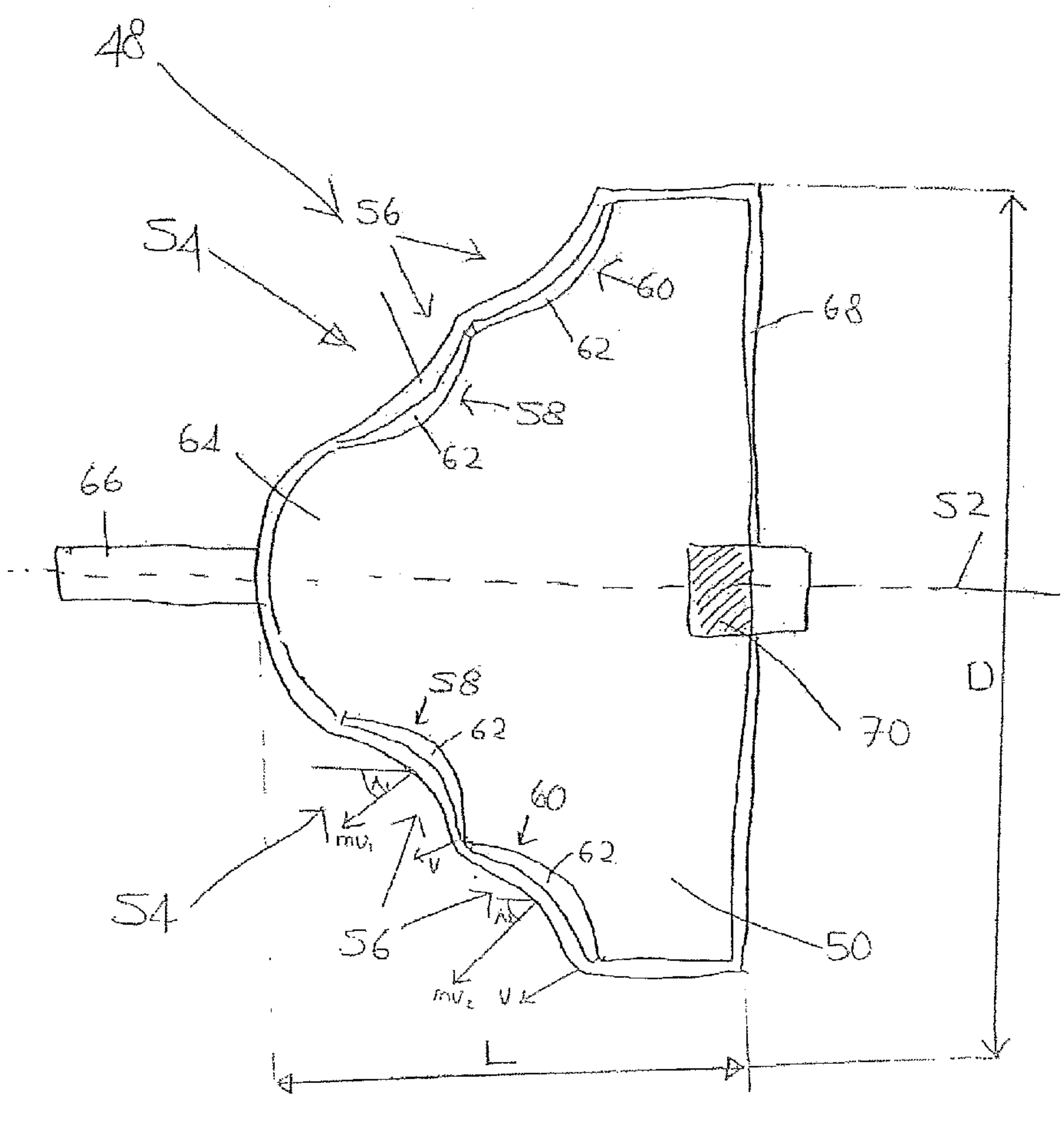
(54) **Title:** DOUBLE EXPLOSIVELY-FORMED RING (DEFR) WARHEAD




**(57) Abstract:** A warhead configuration for forming a hole through a wall of a target, the warhead configuration comprising a charge of explosive material and a liner. The charge has an axis and a front surface. The front surface includes two annular front surface portions, an inner and an outer annular portion, circumscribing the axis. Each of the annular front surface portions is configured so as to exhibit a concave profile as viewed in a cross-section through the charge parallel to the axis. The liner includes a first liner disposed adjacent to the inner annular portion and a second liner disposed adjacent to the outer annular portion such that, when the charge is detonated, material from the first liner is formed into a first expanding explosively formed ring and material from the second liner is formed into a second explosively formed ring.

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# DOUBLE EXPLOSIVELY-FORMED RING (DEFR) WARHEAD

## FIELD AND BACKGROUND OF THE INVENTION

The present invention relates to warheads and, in particular it concerns warheads having cutting and breaching effects.

Of relevance to the present invention is the Explosively Formed Penetrator (EFP) warhead, also known as Self-Forging Fragment (SFF) warhead. EFP's are taught by US Patents Nos. 4,590,861 to Bugiel, 5,792,980 to Weimann and 5,559,304 to Schweiger, et al. EFP's consist of an essentially axi-symmetric explosive charge with a concave cavity at its forward end being lined by a metallic liner. Upon detonation of the charge, the liner deforms under the effect of the detonation forming a projectile that is accelerated in the axial direction. When properly designed, such a projectile is stable and its effective range can be several hundreds of charge diameters. According to the same principle, reference is now made to Fig. 1, which is an axial-sectional view of a wall breaching warhead **10** which is constructed in accordance with the prior art. Wall breaching warhead **10** is described in U.S. Patent No. 6,477,959 to Ritman, et al., which is incorporated by reference for all purposes as if fully set forth herein. Generally speaking, wall-breaching warhead **10** includes a charge **14** of explosive material having a central axis **16**. The front surface of charge **14** includes a central portion **18**, adjacent to central axis **16**, having a generally convexly-curved shape, and an annular portion **20**, circumscribing central portion **18**, having a generally concavely-curved shape. A metallic liner **22** is disposed adjacent to at least annular portion **20** of the front surface of charge **14**. The effect of concavely-curved annular portion **20** is to substantially concentrate a major part of the material from metallic liner **22** into an expanding conical path. In preferred cases, metallic liner **22** deforms plastically into an expanding explosively formed ring ("EFR"). In other words, after detonation of charge **14**, metallic liner **22** expands along a generatrix **24** of cone **26**, which is defined by the centerline of annular portion **20**, diverging from the central axis **16** and stretches until it is fragmented. Subsequently the fragments continue their motion in the same direction. Reference numerals **28, 30, 32** and **34** depict the condition and displacement of metallic liner **22** at consecutive instants in time after detonation. The ring generally advances at a speed of roughly 2000 m/s, cutting a hole through the front layers of a wall. The EFR therefore serves as a cutting charge, nicknamed "cookie-cutter", in applications such as a wall-breaching charge opening a hole in a brick wall. In addition, convexly-curved central portion **18** produces a spherical blast wave that breaks the rear wall layers by a scabbing effect. The spherical blast wave together with the EFR also assists in knocking out the weakened front layer.

Reference is now made to Fig. 2a, which is an axial sectional view of wall breaching warhead **10** detonated at an adequate standoff $\mathbf{CC_1}$ from a target **36** where central axis **16** is perpendicular to target **36** in accordance with the prior art. The slant ranges $\mathbf{AA_1}$, $\mathbf{BB_1}$, traveled along any cone generatrix **24**, by the various elements of the ring circumference, are equal to each other.

Reference is now made to Fig. 2b, which is a front view of target **36** shortly after wall breaching warhead **10** was detonated at an adequate standoff $\mathbf{CC_1}$ (Fig. 2a) from target **36**, where central axis **16** is perpendicular to target **36** in accordance with the prior art. A footprint **38** of metallic liner **22** (Fig. 1) on target **36** is of circular shape. A circular hole is created by footprint **38** which is evenly cut into target **36** around the circumference of footprint **38**.

Unlike the EFP, the performance of the EFR is highly sensitive to the slant range traveled by its fragments, as the fragments are not aerodynamically stable and their density drops as the distance traveled increases. Therefore, the standoff distance of an EFR charge, which is defined by the distance between the charge and the target, is an important parameter since at excessive standoff distances the fragments will be unable to cut through the target. In addition, as further illustrated in Figs. 3a and 3b below, the performance of an EFR warhead is sensitive to the obliquity of the warhead axis relative to the target.

Reference is now made to Fig. 3a which is a side view of wall breaching warhead **10** detonated at a standoff distance $\mathbf{CC_2}$, which is equal to standoff distance $\mathbf{CC_1}$ of Fig. 2a, where central axis **16** is aligned with the surface of a target **40** with high obliquity in accordance with the prior art. Distances $AA_2$, $BB_2$, traveled along cone generatrices **42**, **44**, respectively, by the various elements of the ring circumference, are not equal to each other. Reference is also made to Fig. 3b, which is a front view of target **40** shortly after wall breaching warhead **10** was detonated at stand-off distance $CC_2$ where central axis **16** is aligned with the surface of target **40** with high obliquity in accordance with the prior art. A footprint **46** of metallic liner **22** on target **40** has an elliptical shape. Target **40** is unevenly cut around the circumference of footprint **46**. Specifically, at a point $A_2$, which corresponds to the ring elements of metallic liner **22** impacting at the shortest slant range $AA_2$ (Fig. 3a), as well as along a portion of footprint **46** corresponding to elliptical curves $A_2G_2$ and $A_2H_2$, target **40** is cut through. On the other hand, at the point $B_2$, which corresponds to the ring elements of metallic liner **22** impacting at the longest slant range $BB_2$, as well as along a portion of the ellipse corresponding to the elliptical curves $B_2G_2$ and $B_2H_2$, the energy of the ring elements is insufficient to cut through target **40**. At point $B_2$ and nearby, the ring elements of metallic liner **22** only cause superficial dents in target **40**. Moving from point $B_2$ toward points $G_2$ and $H_2$, the depth of the dents increases gradually until at points $G_2$ and $H_2$ the crater depth is sufficient to cut through target **40**. Therefore, detonating an EFR warhead at high obliquity to a target is generally not effective in making a hole in a target.

There is therefore a need for a warhead, which can make holes in a target even when the warhead is aligned obliquely to the target. This need is of special importance in the context of MOUT (Military Operation in Urban Terrain), which requires the breaching of walls by firing stand-off weapons with wall-breaching capability from various aspect angles as determined by operational conditions.

## SUMMARY OF THE INVENTION

The present invention is a warhead construction.

According to the teachings of the present invention there is provided, a warhead configuration for forming a hole through a wall of a target, the warhead configuration comprising: (a) a charge of explosive material, the charge having an axis and a front surface, the front surface including two annular front surface portions circumscribing the axis, one of the annular front surface portions being an inner annular portion, another of the annular front surface portions being an outer annular portion, the inner annular portion being disposed between the axis and the outer annular portion, each of the two annular front surface portions being configured so as to exhibit a concave profile as viewed in a cross-section through the charge parallel to the axis, at least part of the concave profile being configured such that a vector projecting outward from the part normal to the annular front surface portion diverges from the axis; and (b) a liner including a first liner disposed adjacent to at least part of the inner annular portion and a second liner disposed adjacent to at least part of the outer annular portion, such that, when the charge is detonated, material from the first liner is formed into a first expanding explosively formed ring and material from the second liner is formed into a second expanding explosively formed ring.

According to a further feature of the present invention the axis is disposed obliquely to a surface of the wall during detonation of the charge.

According to a further feature of the present invention: (a) a first average vector is defined as the vector average of two vectors projecting normally outward from opposite extremes of the concave profile of the inner annular portion; a second average vector is defined as the vector average of two vectors projecting normally outward from opposite extremes of the concave profile of the outer annular portion; (b) a first angle is defined as an angle between the first average vector and the axis; (c) a second angle is defined as an angle between the second average vector and the axis; and (d) the second angle exceeds the first angle by at least 5°.

According to a further feature of the present invention: (a) the first expanding explosively formed ring exhibits a first expanding conical path having a first angle relative to the axis; (b) the second expanding explosively formed ring exhibits a second expanding conical path having a second angle relative to the axis; and (c) the second angle exceeds the first angle by at least 5 degrees.

According to a further feature of the present invention the two annular front surface portions are substantially rotationally symmetric about the axis.

According to a further feature of the present invention the concave profile corresponds substantially to an arc of a circle.

According to a further feature of the present invention the arc subtends an angle of between 15° and 90° to a center of curvature of the arc.

According to a further feature of the present invention the arc subtends an angle of between 30° and 70° to a center of curvature of the arc.

According to a further feature of the present invention the concave profile turns through an angle of between 15° and 90°

According to a further feature of the present invention the concave profile turns through an angle of between 30° and 70°

According to a further feature of the present invention the two annular front surface portions correspond to at least about two-thirds of the total front surface of the charge as viewed parallel to the axis.

According to a further feature of the present invention the two annular front surface portions correspond to at least about 90% of the total front surface of the charge as viewed parallel to the axis.

According to a further feature of the present invention the charge and the liner are configured such that detonation of the explosive material imparts a velocity to the liner of between about 1000 and about 4000 meters per second.

According to a further feature of the present invention a central portion adjacent to the central axis having a generally convexly curved shape.

According to a further feature of the present invention, the charge includes between about ½ kg and about 3 kg of explosive material.

According to a further feature of the present invention, the charge includes less than about 2 kg of explosive material.

According to a further feature of the present invention, there is also provided a stand off detonation system including means for defining a stand off detonation distance of the charge from the wall.

According to a further feature of the present invention, the means for defining a stand off detonation distance includes a stand off rod projecting from the front surface substantially parallel to the axis.

According to a further feature of the present invention, the charge has a rear surface, the warhead further comprising a rear cover associated with at least the rear surface, the rear cover being formed from a non-fragmenting material.

According to the teachings of the present invention there is also provided a warhead configuration for forming a hole through a wall of a target, the warhead configuration comprising: (a) a charge of explosive material, the charge having an axis and presenting a front portion; and (b) a liner disposed adjacent to at least part of the front portion, wherein the charge and the liner are configured such that, when the charge is detonated, a majority of material from the liner forms two expanding explosively formed rings.

According to a further feature of the present invention: (a) one of the two expanding explosively formed rings exhibits a first expanding conical path having a first angle relative to the axis; (b) another of the two expanding explosively formed rings exhibits a second expanding conical path having a second angle relative to the axis; and (c) the second angle exceeds the first angle by at least 5 degrees.

## BRIEF DESCRIPTION OF THE DRAWINGS

The invention is herein described, by way of example only, with reference to the accompanying drawings, wherein:

Fig. 1 is an axial-sectional view of a wall breaching warhead which is constructed in accordance with the prior art;

Fig. 2a is an axial sectional view of the wall breaching warhead of Fig. 1 detonated at an adequate standoff distance from a target where the central axis of the warhead is perpendicular to the target;

Fig. 2b is a front view of a target shortly after the wall breaching warhead of Fig. 1 was detonated at an adequate standoff from the target, where the central axis of the warhead is perpendicular to the target;

Fig. 3a is a side view of the wall breaching warhead of Fig. 1 detonated at a standoff distance, where the central axis of the warhead is aligned with the surface of a target with high obliquity;

Fig. 3b is a front view of a target shortly after wall breaching warhead was detonated at a stand-off distance, where the central axis of the warhead is aligned with the surface of the target with high obliquity;

Fig. 4 is an axial-sectional view of a double explosively-formed ring (DEFR) warhead that is constructed and operable in accordance with a preferred embodiment of the invention;

Fig. 5 is a schematic axial-sectional view of the DEFR warhead of Fig. 4 shortly after detonation;

Fig. 6a is a schematic cross-sectional view of the DEFR warhead of Fig. 4 shortly after detonation, where the axis of the warhead is aligned perpendicular to the surface of a target;

Fig. 6b is a schematic front view of the footprints formed by the DEFR warhead on the target of Fig. 6a;

Fig. 6c is a schematic front view of the final damage caused to the target of Fig. 6a;

Fig. 7a is a schematic cross-sectional view of the DEFR warhead of Fig. 4 shortly after detonation, where the axis of the warhead is aligned obliquely to a target;

Fig. 7b is a schematic front view of the footprints formed by the DEFR warhead on the target of Fig. 7a; and

Fig 7c is a schematic front view of the final damage caused to the target of Fig. 7a.

## DESCRIPTION OF THE PREFERRED EMBODIMENTS

The present invention is a warhead construction.

The principles and operation of a warhead construction according to the present invention may be better understood with reference to the drawings and the accompanying description.

Reference is now made to Fig. 4, which is an axial-sectional view of a double explosively-formed ring (DEFR) warhead **48** that is constructed and operable in accordance with a preferred embodiment of the invention. Warhead **48** includes a charge **50** of explosive material. Charge **50** has an axis **52** and a front surface **54**. Front surface **54** includes two annular front surface portions **56** circumscribing axis **52**. One annular front surface portion **56** is an inner annular portion **58**. Another annular front surface portion **56** is an outer annular portion **60**. Inner annular portion **58** is disposed between axis **52** and outer annular portion **60**. Each annular front surface portion **56** is configured so as to exhibit a concave profile as viewed in a cross-section through charge **50** parallel to axis **52**. The concave profile of inner annular portion **58** and the concave profile of outer annular portion **60** are substantially rotationally symmetric about axis **52**. Charge **50** also includes a central portion **64** adjacent to axis **52**. Central portion **64** has a generally convexly-curved shape. A liner **62** is disposed adjacent to inner annular portion **58** and a liner **63** is disposed adjacent to outer annular portion **60**. Liners **62**, **63** are typically formed as separate elements, each of which being formed from the same or different materials. Alternatively, liners **62**, **63** are formed as part of a continuous metal cover lining the front side of the explosive charge. Preferably, liners **62**, **63** at least cover substantially the entirety of annular front surface portions **56**. When charge **50** is detonated, material from liner **62** and liner **63** is concentrated by inner annular portion **58** and outer annular portion **60**, respectively, to form two expanding explosively formed rings or double explosively formed rings (DEFR), which advance at a speed of roughly 2,000 meters per second, enabling wall breaching warhead **48** to cut into the front layers of a wall. The types of materials to be used for liners **62**, **63** may include, but are not limited to, metals such as copper, tantalum, aluminum, iron, tungsten, molybdenum and metallic alloys as well as ceramic materials, plastic materials, composites and pressed powder materials. In addition, on detonation, convexly-curved central portion **64** produces a spherical blast wave that breaks the rear wall layers by a scabbing effect. The combination of these two effects provides a very effective tool for breaching brick walls. The arrival of the blast wave together with the DEFR also assists in knocking out the weakened front layer, even when axis **52** is aligned obliquely to the surface of a wall, as will be explained later with reference to Fig. 7a, 7b and 7c.

Before turning to features of the present invention in more detail, it should be appreciated that the invention is useful for breaching a wide variety of types of walls in different circumstances. Although not limited thereto, the invention is believed to be of particular value for breaching brick walls. In this context, it should be noted that the term "brick wall" is used herein in the description and claims to refer generically to any wall constructed of one or more layer of relatively small units piled in overlapping formation. The term is used irrespective of the particular material used for the units, whether it is "brick", stone, or slabs or blocks of any other construction material. The term is also used to include composite walls in which one or more layer of a brick-like formation is used together with other structural or insulation elements.

Turning now to the features of wall breaching warhead **48** in more detail, inner annular portion **58** and outer annular portion **60** each exhibit a concave profile through charge **50** passing through axis **52**. Each concave profile is generally configured such that a vector, $v$, projecting outward from the concave profile, normal to the corresponding annular front surface portion **56** diverges from axis **52**. Additionally, an average vector $mv_1$ is defined as the vector average of two vectors $Va$, $Vb$ which project normally outward from opposite extremes **67**, **69** of the concave profile of inner annular portion **58.** Similarly, the concave profile of outer annular portion **60** has a similarly defined average vector $mv_2$. An angle $A_1$ is defined as an angle between vector $mv_1$ and axis **52**. An angle $A_2$ is defined as an angle between vector $mv_2$ and axis **52**. For most embodiments of the concave profiles, angle $A_2$ exceeds angle $A_1$. In order to effectively produce two distinct explosively formed rings, angle $A_2$ generally exceeds angle $A_1$ by at least 5°. As a reasonable approximation, inner annular portion **58** produces an explosively formed ring, which exhibits an expanding conical path with angle $A_1$ relative to axis **52**. Similarly, outer annular portion **60** produces an explosively formed ring, which exhibits an expanding conical path with angle $A_2$ relative to axis **52**. However, the exact angles of the expanding conical paths will depend on various factors such as the geometry of the point of initiation relative to the shaped surfaces, as will be discussed below. The converging vectors of the concave profiles of inner annular portion **58** and outer annular portion **60**, approximate closely to the direction of the explosive thrust experienced by the different parts of liner **62** and liner **63**, respectively, leading to liner **62** forming an inner concentric ring and liner **63** forming an outer concentric ring. These concentric rings form the expanding DEFR. The rings may break into fragments as they expand. However, the fragments of each ring are still generally sufficiently close together to perform a cutting action through the wall.

Additionally, the concave profile of each annular front surface portion **56** turns through no more than 90°. Typically, each concave profile corresponds substantially to an arc of a circle, which subtends an angle of between 15° and 90° to the center of curvature of the arc. In other words, each concave profile typically turns through an angle of between 15° and 90°. Preferably, the arc of the circle subtends an angle of between 30° and 70° to the center of curvature of the arc. In other words, each concave profile preferably turns through an angle of between 30° and 70°.

In order to allow spreading of the DEFR to cut a hole of the desired size, charge **50** should be detonated at a predefined distance from the surface of the wall to be breached. To this end, certain preferred implementations of warhead **48** include a stand off rod **66** projecting from the front surface substantially parallel to axis **52**. Stand off rod **66** is configured to define a stand off detonation distance of charge **50** from the wall, as is known in the art. Clearly, alternative implementations may achieve a similar effect using other techniques for detonating the charge at a predefined distance. Possible examples include, but are not limited to, systems employing optical or electromagnetic (radio frequency) proximity sensors.

It should be appreciated that the combination of the cutting effect of the EFR together with the blast effect of the central portion of the shaped charge provides a highly efficient breaching effect. Thus, in striking contrast to quantities of 10-20 kg which would be required if a conventional blast charge were used, the shaped charge of the present invention preferably includes between about ½ kg and about 3 kg of explosive material, and most preferably less than about 2 kg. This charge is light enough to be carried by a rocket or missile designed for carrying only a few kg of explosive, thereby avoiding the need to send the operating force to the wall.

As mentioned before, liners **62**, **63** are adjacent to inner annular portion **58** and outer annular portion **60**, respectively. This typically corresponds to at least about two-thirds, and preferably 90% of the total area of the front surface as viewed parallel to axis **52**. The rear surface of charge **50** may be substantially flat or of a conical shape. The rear surface of charge **50** is preferably covered by a rear cover **68** formed from non-fragmenting material. In this context, "non-fragmenting" is used to refer to materials, which do not generally form fragments that could pose a danger to the operating force. Rear cover **68** may extend to the front surface of charge **50** to form a continuous protective envelope, which covers liners **62**, **63** as well. Liners **62**, **63** are preferably mechanically connected, typically using adhesive, onto the protective envelope prior to loading the charge **50** therein. Alternatively, the forward part of the protective envelope is formed integrally with liners **62**, **63** and the rear part of the protective envelope is formed from non-fragmenting materials, such as plastic materials. An explosive booster **70** is installed at the rear side of charge **50**. Optionally, the rear side of charge **50** includes a more complex initiation system (not shown) including a wave-shaper (not shown) for peripheral initiation. The wave-shaper also includes an explosive duct along its centerline providing a central wave-source to liner **62** which is adjacent to inner annular portion **58** and a peripheral wave source to liner **63** which is adjacent to outer annular portion **60**. The rear side of charge **50** has mechanical and pyrotechnic interfaces (not shown). The design of rear cover **68**, the initiation system, the detonation chain and the interfaces are well-known to those skilled in the art of warhead systems.

It will be noted that the explosive thrust experienced by liners **62**, **63** is also influenced by the geometry of the point of initiation relative to the shaped surfaces. In the preferred example shown here, charge **50** is made relatively flat. In more quantitative terms, an outer diameter D of charge **50** measured perpendicular to axis **52** is preferably about twice the maximum length L of charge **50** measured parallel to axis **52**. The use of point initiation in the middle of the back surface of charge **50** tends to increase the conical angle (i.e., angles of divergence) of the DEFR. The various physical properties influencing the formation and properties of the DEFR, including the shape of charge **50**, the point of detonation, the material and thickness distribution of the liner, and the type and amount of explosive used, are preferable chosen to impart a velocity to parts of liners **62**, **63** of between about 1000 and about 4000 m/s, and most preferably, of about 2000 m/s.

Reference is now made to Fig. 5, which is a schematic axial-sectional view of warhead **48** of Fig. 4 shortly after detonation. Warhead **48** is described as a Double Explosively-Formed Ring (DEFR) warhead, as it generates two annular ring-shaped projectiles upon detonation. Each element in the rings, formed from liner **62** and liner **63** adjacent to inner annular portion **58** and outer annular portion **60**, respectively, moves in a direction essentially aligned to the centerline of the cavity of each ring. Therefore, liner **62** and liner **63** expand along generatrices **72** and **74** of the cones defined by the cavity centerlines, respectively. The cones stretch until they are fragmented. Generatrices **72**, **74** diverge from axis **52**. The angle of divergence of the outer cavity from axis **52** is larger than the angle of divergence of the inner cavity from axis **52** as discussed above with reference to Fig. 4. Subsequently, the fragments continue their motion in the same direction. Reference numerals **72a**, **72b**, **72c**, **72d** depict the condition and displacement of liner **62** at consecutive instants in time after detonation. Reference numerals **74a**, **74b**, **74c**, **74d** depict the condition and displacement of liner **63** at consecutive instants in time after detonation. The explosively formed rings do not have to be continuous in order to have a cutting capability. Indeed, for targets such as brick walls or aluminum plates, cutting can be achieved by the ring fragments provided that at a given slant range there is enough fragment density and energy to cut through the target. Therefore, as previously mentioned, the cutting capability of the ring elements depends on their slant range to the target, which is determined by the warhead detonation standoff distance and obliquity. As discussed above with reference to Fig. 4, charge **50** produces a blast wave that induces a strong shock in the target. For brittle targets, such as concrete or brick walls, such shock can have a scabbing effect breaking the rear layers of the target. The combination of the scabbing effect of the blast wave and the cutting effect of the explosively-formed rings impacting the target at close sequence provides a very effective breaching mechanism, also knocking out the weakened front layer.

The DEFR serves as a cutting charge in various applications, including defeating light armored vehicles and breaching concrete and brick walls. One of the preferred methods to bring the DEFR warhead onto the target is installing it onto an airframe, such as a rocket, a missile or a projectile (all of them to be hereinafter referred to as a "projectile"). Such a projectile will also include a standoff device, such as a standoff rod or proximity fuse, a Safety-and-Arming device and a projectile airframe or body including stabilization devices such as fins.

Reference is now made to Fig. 6a, which is a schematic cross-sectional view of warhead **48** of Fig. 4 shortly after detonation, at a standoff distance $CC_3$ from a target **76**, when axis **52** of warhead **48** is aligned perpendicular to the surface of target **76**. Target **76** is typically a brick wall. Warhead **48** produces an inner ring **86** and an outer ring **88**. The slant ranges $LL_1$ and $MM_1$ traveled along cone generatrices **78** and **80**, respectively, by the various elements of outer ring **88** are equal to each other. The slant ranges $NN_1$ and $OO_1$ traveled along cone generatrices **82** and **84**, respectively, by the various elements of inner ring **86**, are equal to each other. It should be noted that the slant ranges traveled by the elements of outer ring **88** are longer than those traveled by the elements of inner ring **86**.

Reference is now made to Fig. 6b, which is a schematic front view of target **76** and a footprint **90** and a footprint **91** formed by warhead **48** on target **76**, due to the detonation of warhead **48** as described with reference to Fig. 6a. Footprint **90** and footprint **91** of liner **62** and liner **63** (Fig. 4), respectively, on target **76** are circular. Target **76** is evenly cut around the circumferences of footprints **90**, **91**.

Reference is now made to Fig. 6c, which is a schematic front view of the final damage caused to target **76** due to the detonation of warhead **48** as described with reference to Fig. 6a. The blast wave generated by charge **50** impinges on the portion of target **76** inside footprint **91**, creating a hole in target **76**.

Reference is now made to Fig. 7a, which is a schematic cross-sectional view of warhead **48** of Fig. 4 shortly after detonation, at a standoff distance $CC_4$ from a target **92**, where axis **52** of warhead **48** is aligned obliquely to a surface of target **92** during detonation of charge **50**. Target **92** is typically a brick wall. Slant ranges $LL_2$, $MM_2$, and $NN_2$. $OO_2$ traveled along cone generatrices **94**, **96**, **98** and **100**, respectively, by the various elements of the rings, are not equal to each other.

Reference is now made to Fig. 7b, which is a schematic front view of target **92** and a plurality of footprints **102**, **104** formed by warhead **48** on target **92**, where warhead **48** was detonated as described with reference to Fig. 7a. Footprint **102** is formed by liner **62** (Fig. 4) and footprint **104** is formed by liner **63** (Fig. 4). Footprint **102** and footprint **104** are generally an elliptical shape. Target **92** is unevenly cut around the circumferences of footprints **102** and **104**. For any cross-section of warhead **48** coplanar with axis **52**, the slant ranges traveled by the elements associated with outer annular portion **60** are longer than those traveled by the elements associated with inner annular portion **58** for any given divergence angle from axis **52**. For this reason, better cutting performance is achieved along footprint **102** associated with inner annular portion **58** than along footprint **104** associated with outer annular portion **60**. Specifically, the entirety of footprint **102** and only part of footprint **104** are cut through target **92**. Target **92** is cut through at point $L_2$ on footprint **104**, which corresponds to liner **62** associated with outer annular portion **60** impacting at the shortest slant range $LL_2$ (Fig. 7a). Similarly, along elliptical curves $L_2R_2$ and $L_2S_2$ of footprint **104**, target **92** is cut through. On the other hand, at point $M_2$ on footprint **104**, which corresponds to liner **63** of outer annular portion **60** impacting at the longest slant range $MM_2$ (Fig. 7a). Similarly, along elliptical curves $M_2R_2$ and $M_2S_2$, the energy of fragments of liner **63** of outer annular portion **60** is insufficient to cut through target **92**. At point $M_2$ and nearby, the fragments of liner **63** causes only superficial dents. Moving from point $M_2$ towards points $R_2$ and $S_2$, respectively, the depth of the dents increases gradually until at points $R_2$ and $S_2$, respectively, the dent depth is sufficient to cut through target **92**.

Reference is now made to Fig 7c, which is a schematic front view of the final damage caused to target **92** due to the detonation of warhead **48** as described with reference to Fig. 7a. The blast wave generated by charge **50** impinges on the portion of the target inside the cut through part of footprint **104** creating a connection **106** between footprint **102** and footprint **104**, thereby creating a hole in target **92**. It should be noted that a hole created only by footprint **102** is not large enough for the required use, such as allowing entry of personal or warheads though the hole. However, the hole created by the combination of footprint **102** and footprint **104** is large enough for the required use.

If the blast wave generated by charge **50** impinging on the portion of target **92** within the cut through part of footprint **104** fails to knock out that part of target **92**, it will at least weaken it. In such cases, an additional DEFR warhead is directed towards target **92**, thereby generating additional footprints in target **92** and also creating connection **106** between footprint **102** and footprint **104** thereby breaching the target.

It will be appreciated by persons skilled in the art that the present invention is not limited to what has been particularly shown and described hereinabove. Rather, the scope of the present invention includes both combinations and sub-combinations of the various features described hereinabove, as well as variations and modifications thereof that are not in the prior art which would occur to persons skilled in the art upon reading the foregoing description.

WHAT IS CLAIMED IS.

1. A warhead configuration for forming a hole through a wall of a target, the warhead configuration comprising:

(a) a charge of explosive material, said charge having an axis and a front surface, said front surface including two annular front surface portions circumscribing said axis, one of said annular front surface portions being an inner annular portion, another of said annular front surface portions being an outer annular portion, said inner annular portion being disposed between said axis and said outer annular portion, each of said two annular front surface portions being configured so as to exhibit a concave profile as viewed in a cross-section through said charge parallel to said axis, at least part of said concave profile being configured such that a vector projecting outward from said part normal to said annular front surface portion diverges from said axis; and

(b) a liner including a first liner disposed adjacent to at least part of said inner annular portion and a second liner disposed adjacent to at least part of said outer annular portion, such that, when said charge is detonated, material from said first liner is formed into a first expanding explosively formed ring and material from said second liner is formed into a second expanding explosively formed ring.

2. The warhead configuration of claim 1, wherein said axis is disposed obliquely to a surface of the wall during detonation of said charge.

3. The warhead configuration of claim 1, wherein:

(a) a first average vector is defined as the vector average of two vectors projecting normally outward from opposite extremes of said concave profile of said inner annular portion;

(b) a second average vector is defined as the vector average of two vectors projecting normally outward from opposite extremes of said concave profile of said outer annular portion;

(c) a first angle is defined as an angle between said first average vector and said axis;

(d) a second angle is defined as an angle between said second average vector and said axis; and

(e) said second angle exceeds said first angle by at least 5°.

4. The warhead configuration of claim 1, wherein:

(a) said first expanding explosively formed ring exhibits a first expanding conical path having a first angle relative to said axis;

(b) said second expanding explosively formed ring exhibits a second expanding conical path having a second angle relative to said axis; and

(c) said second angle exceeds said first angle by at least 5 degrees.

5. The warhead configuration of claim 1, wherein said two annular front surface portions are substantially rotationally symmetric about said axis.

6. The warhead configuration of claim 1, wherein said concave profile corresponds substantially to an arc of a circle.

7. The warhead configuration of claim 6, wherein said arc subtends an angle of between 15° and 90° to a center of curvature of said arc.

8. The warhead configuration of claim 6, wherein said arc subtends an angle of between 30° and 70° to a center of curvature of said arc.

9. The warhead configuration of claim 1, wherein said concave profile turns through an angle of between 15° and 90°.

10. The warhead configuration of claim 1, wherein said concave profile turns through an angle of between 30° and 70°.

11. The warhead configuration of claim 1, wherein said two annular front surface portions correspond to at least about two-thirds of the total front surface of said charge as viewed parallel to said axis.

12. The warhead configuration of claim 1, wherein said two annular front surface portions correspond to at least about 90% of the total front surface of said charge as viewed parallel to said axis.

13. The warhead configuration of claim 1, wherein said charge and said liner are configured such that detonation of said explosive material imparts a velocity to said liner of between about 1000 and about 4000 meters per second.

14. The warhead configuration of claim 1, further comprising a central portion adjacent to said central axis having a generally convexly curved shape.

15. The warhead configuration of claim 1, wherein said charge includes between about ½ kg and about 3 kg of explosive material.

16. The warhead configuration of claim 1, wherein said charge includes less than about 2 kg of explosive material.

17. The warhead configuration of claim 1, further comprising a stand off detonation system including means for defining a stand off detonation distance of said charge from the wall.

18. The warhead configuration of claim 17, wherein said means for defining a stand off detonation distance includes a stand off rod projecting from said front surface substantially parallel to said axis.

19. The warhead configuration of claim 1, wherein said charge has a rear surface, the warhead further comprising a rear cover associated with at least said rear surface, said rear cover being formed from a non-fragmenting material.

20. A warhead configuration for forming a hole through a wall of a target, the warhead configuration comprising:

(a) a charge of explosive material, said charge having an axis and presenting a front portion; and

(b) a liner disposed adjacent to at least part of said front portion, wherein said charge and said liner are configured such that, when said charge is detonated, a majority of material from said liner forms two expanding explosively formed rings.

21. The warhead configuration of claim 20, wherein:

(a) one of said two expanding explosively formed rings exhibits a first expanding conical path having a first angle relative to said axis;

(b) another of said two expanding explosively formed rings exhibits a second expanding conical path having a second angle relative to said axis; and

(c) said second angle exceeds said first angle by at least 5 degrees.

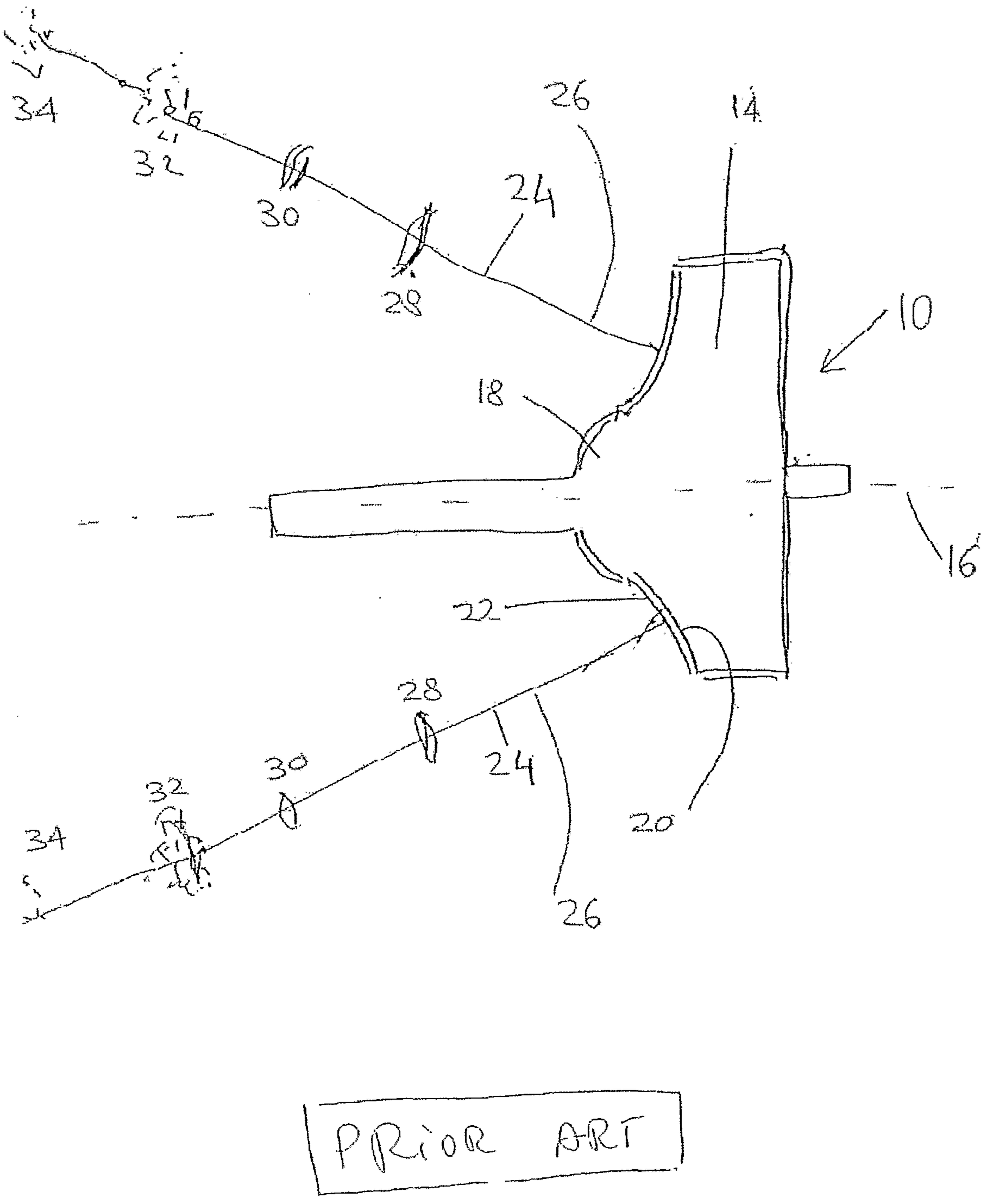
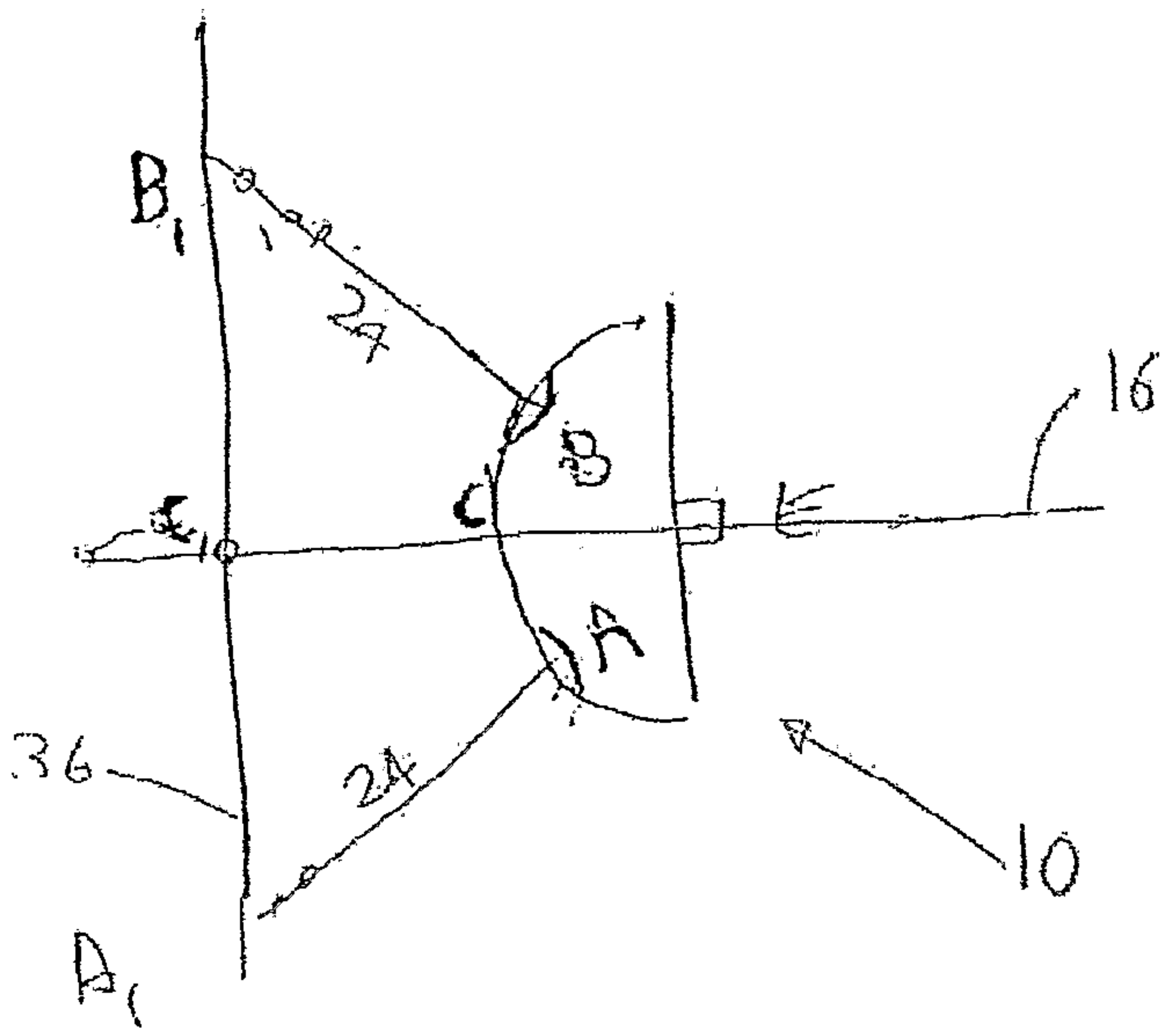
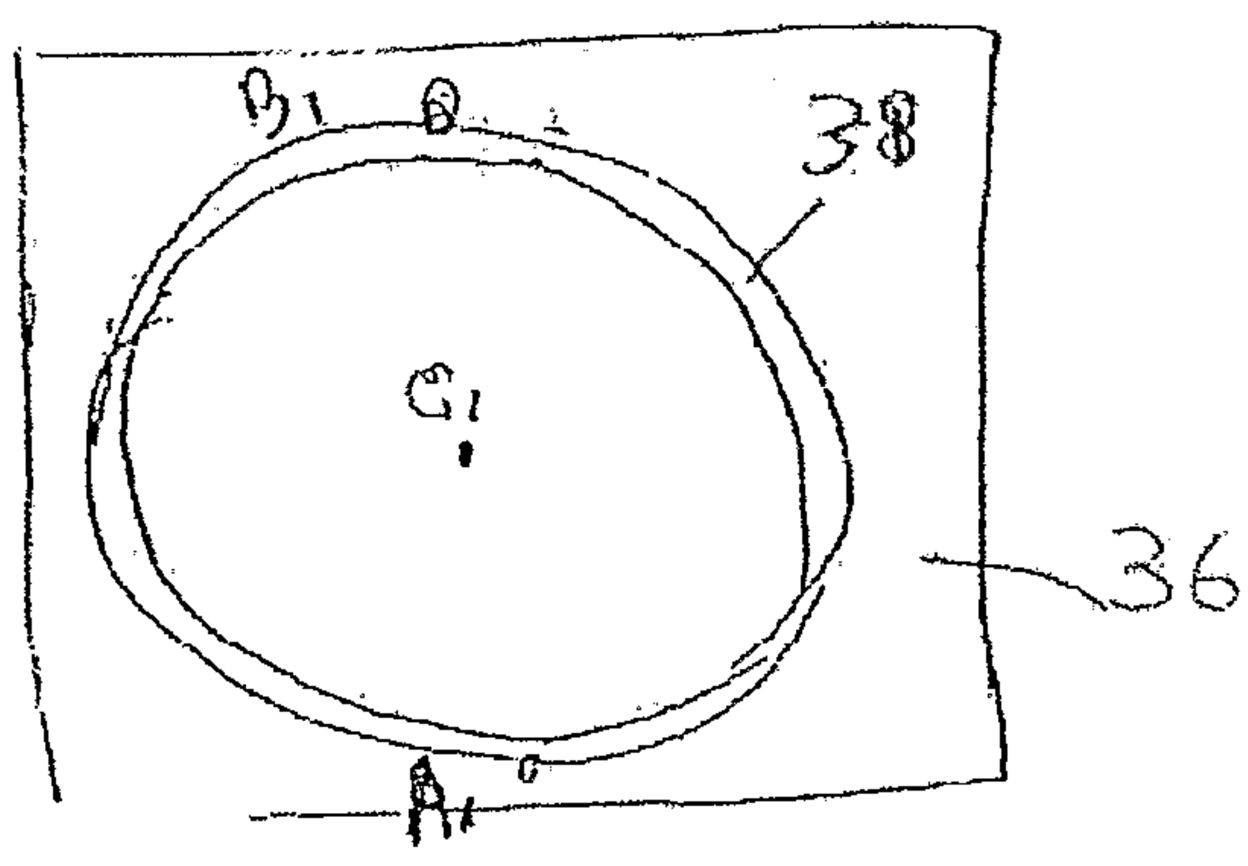



Fig 1



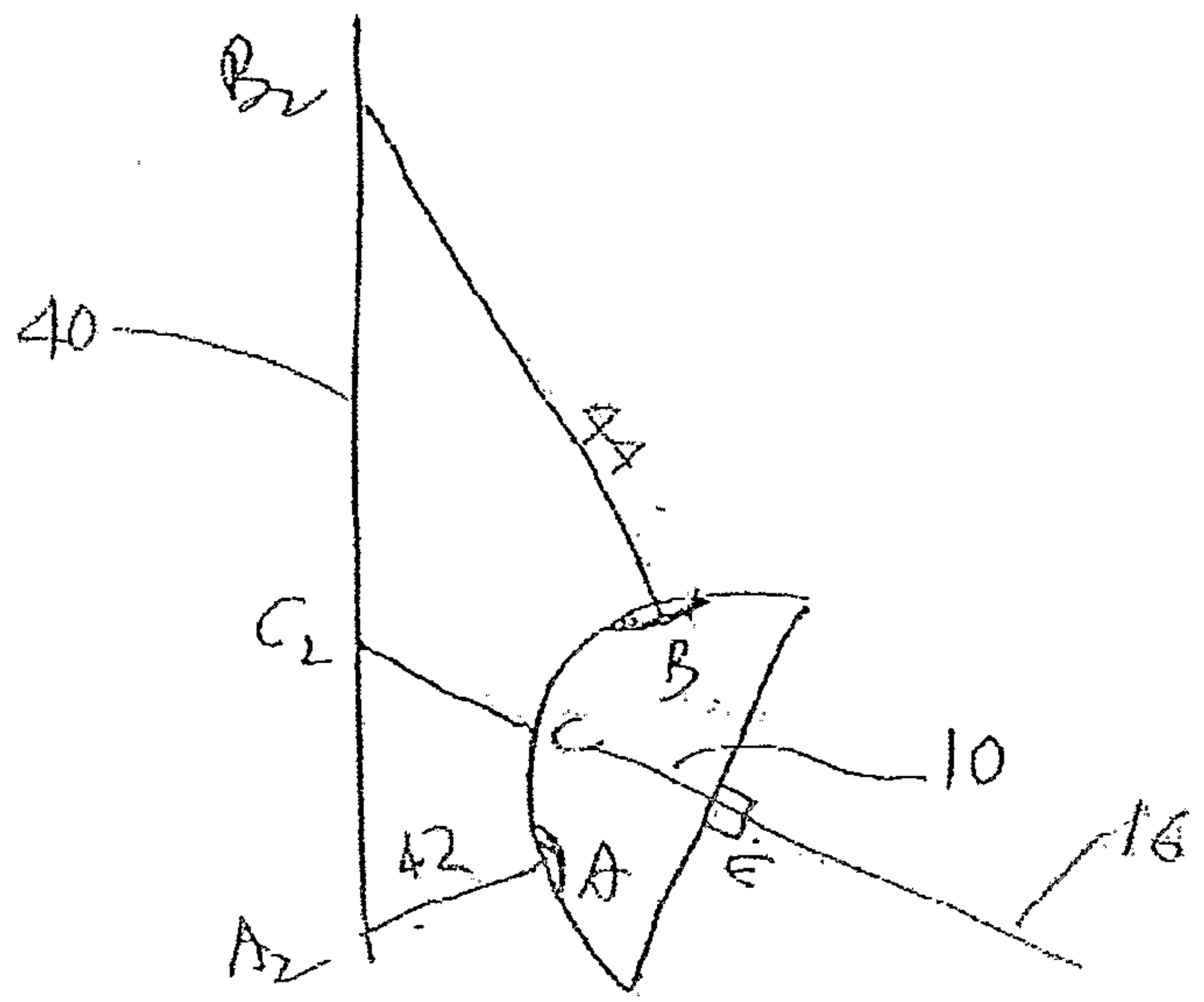

PRIOR ART

Fig 2a



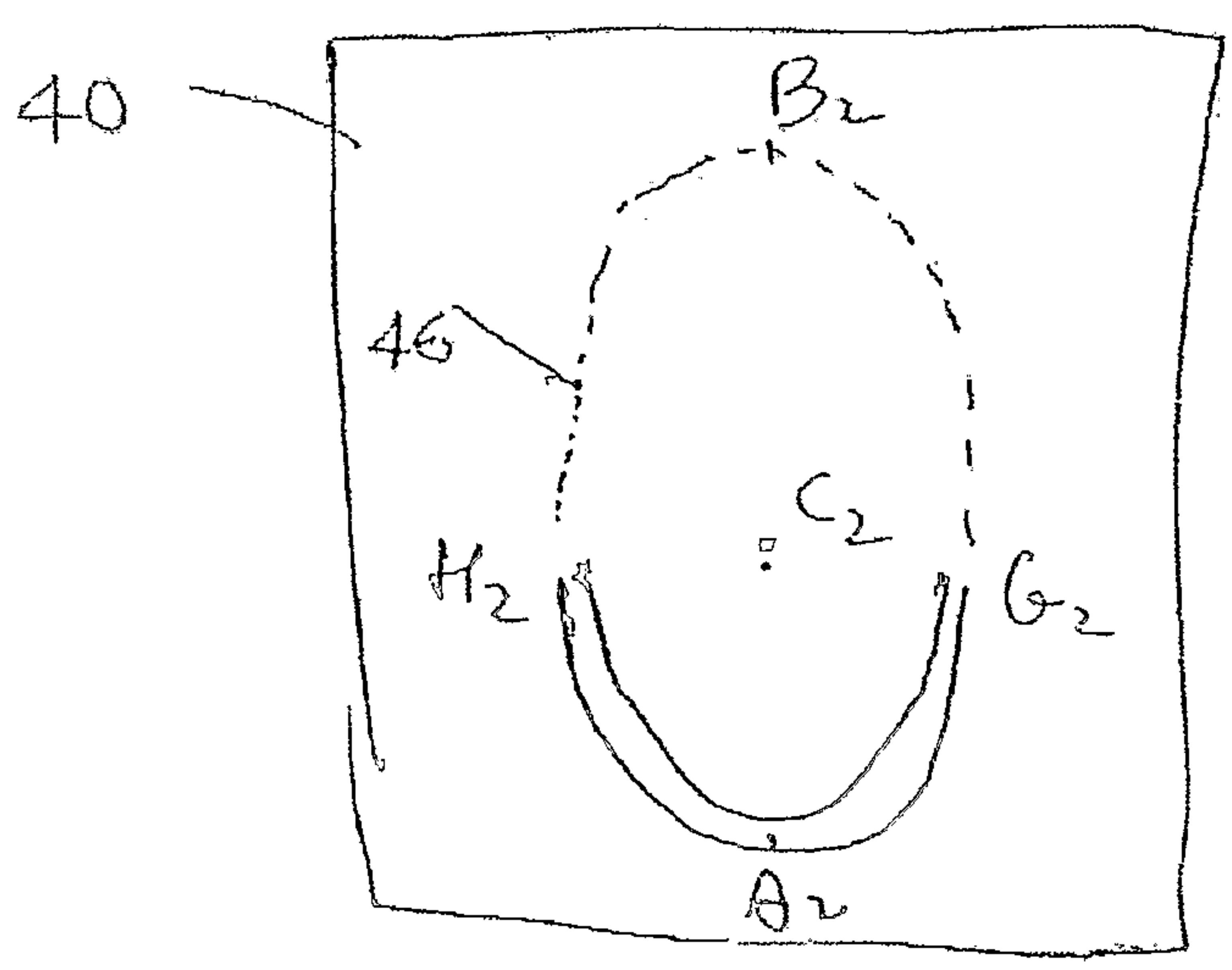

PRIOR ART

Fig 2b




PRIOR ART

Fig 3a




PRIOR ART

Fig 3b

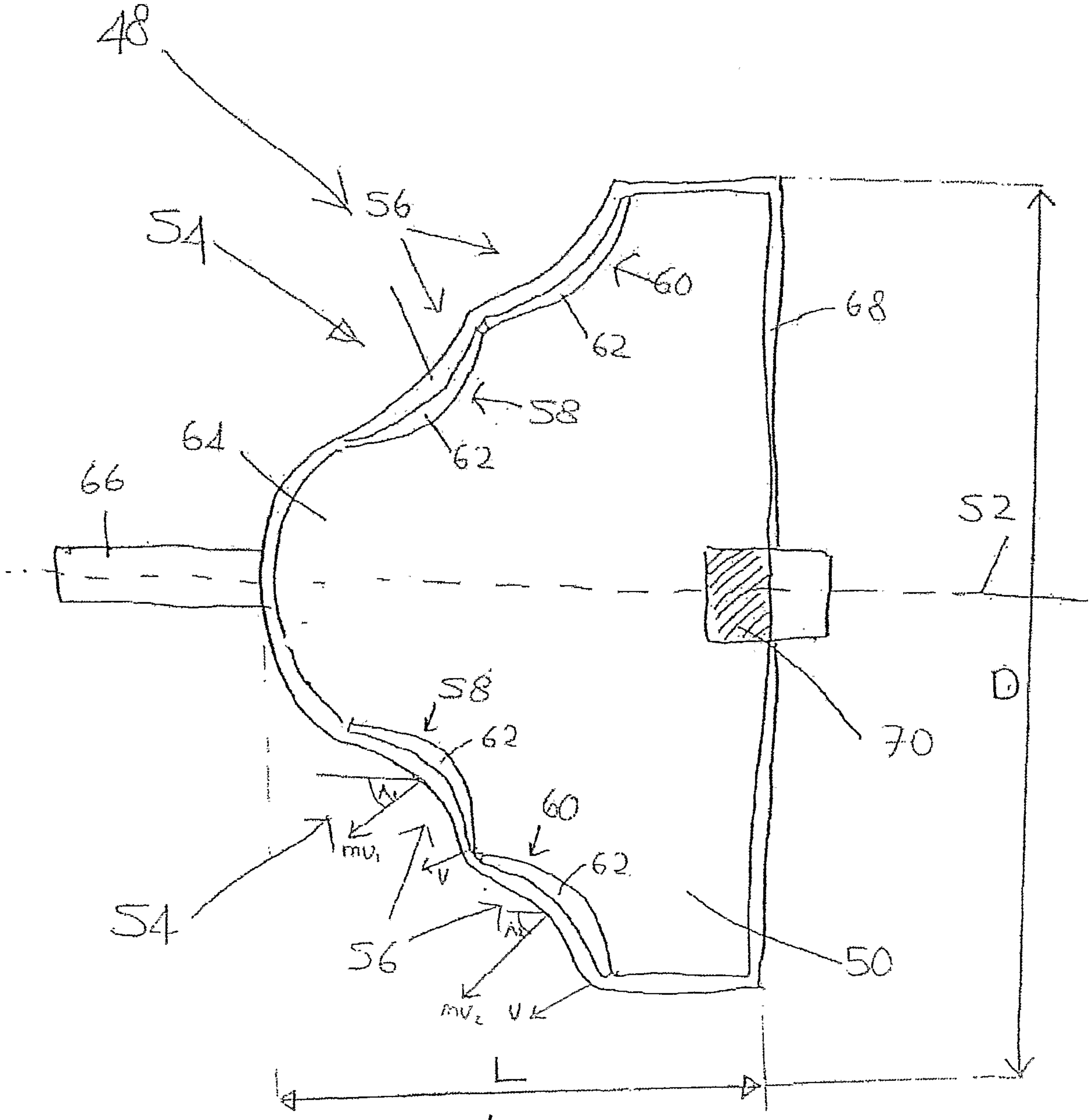



Fig 4

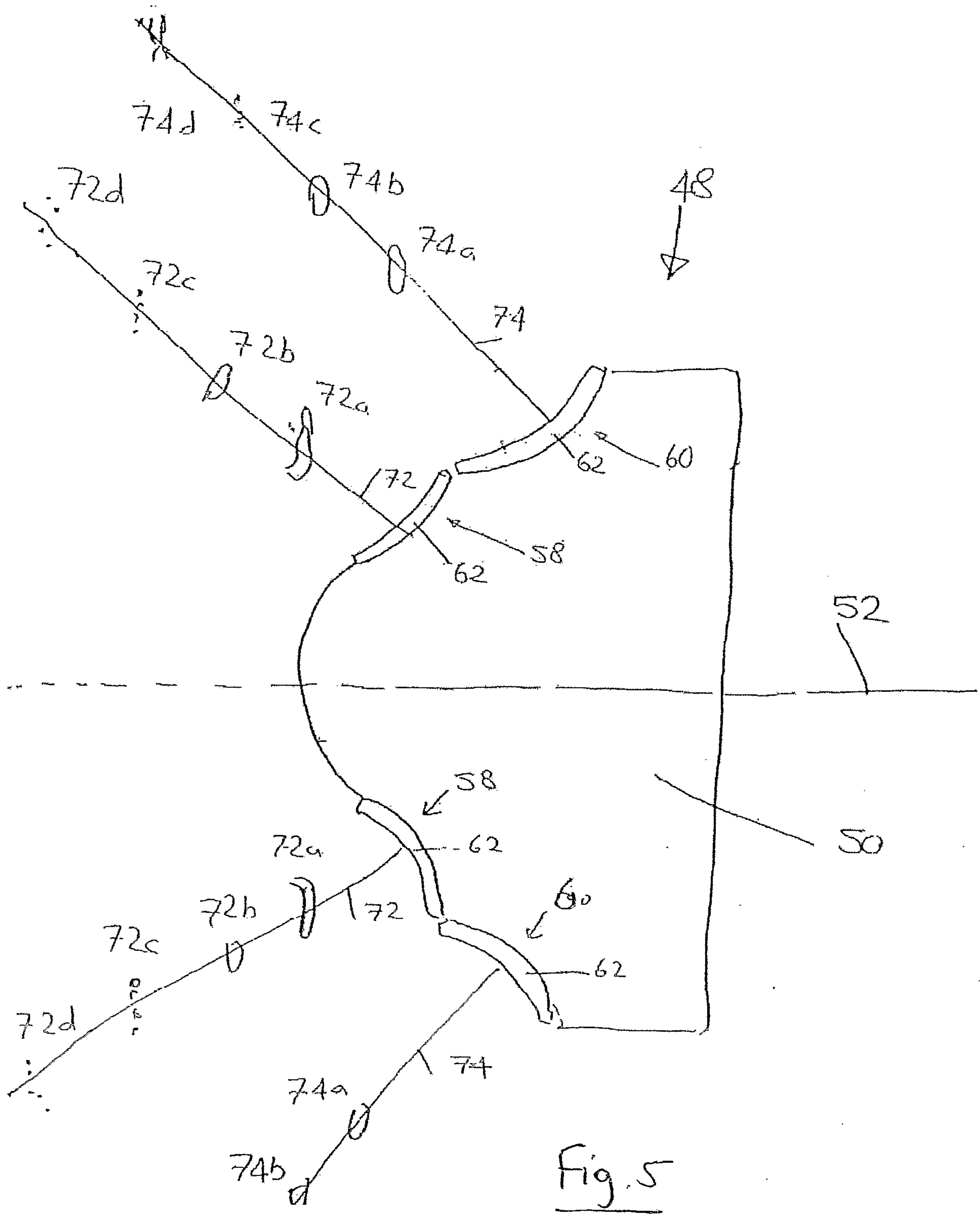



Fig.5

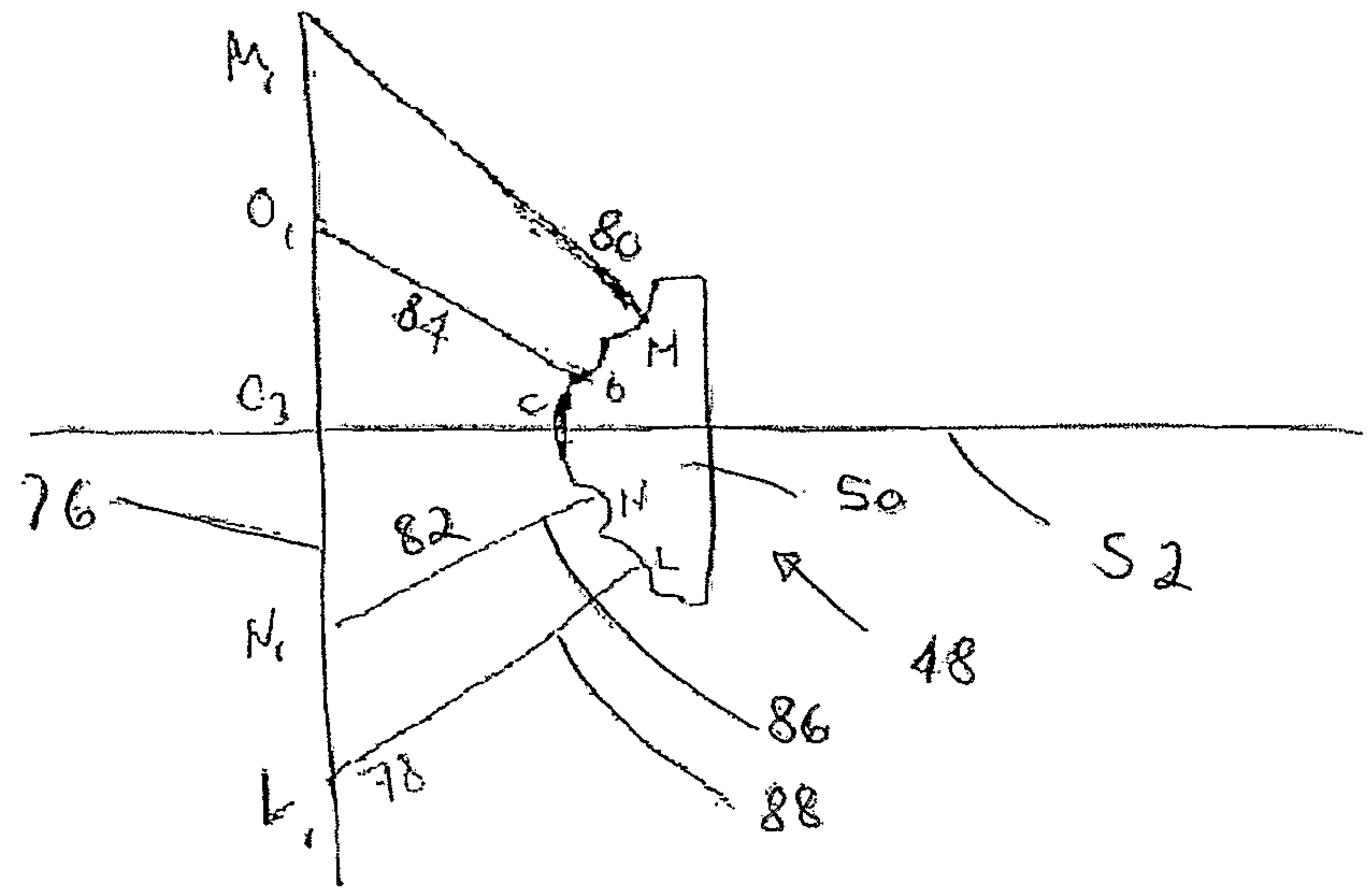



Fig 6a

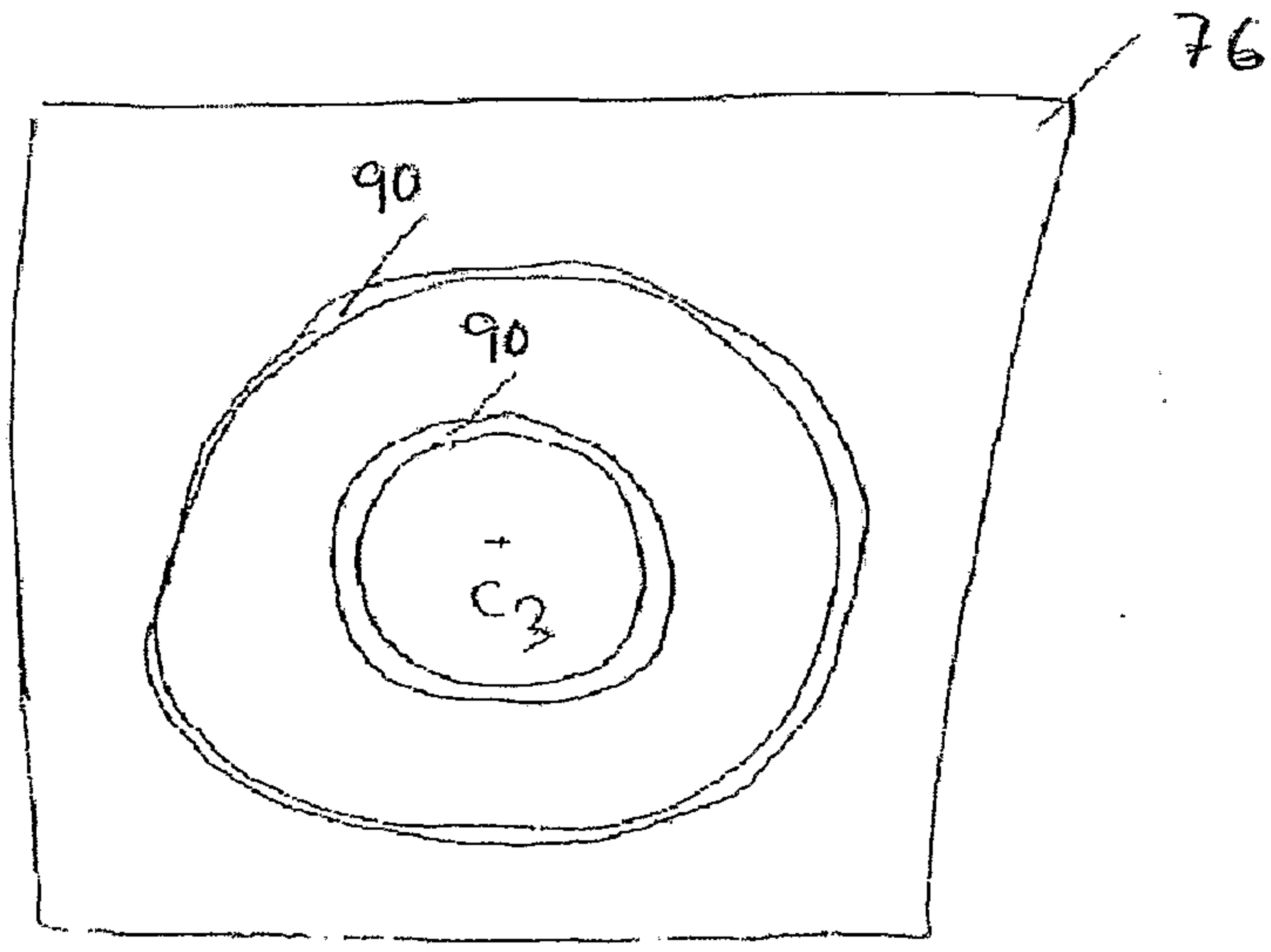



Fig 6b

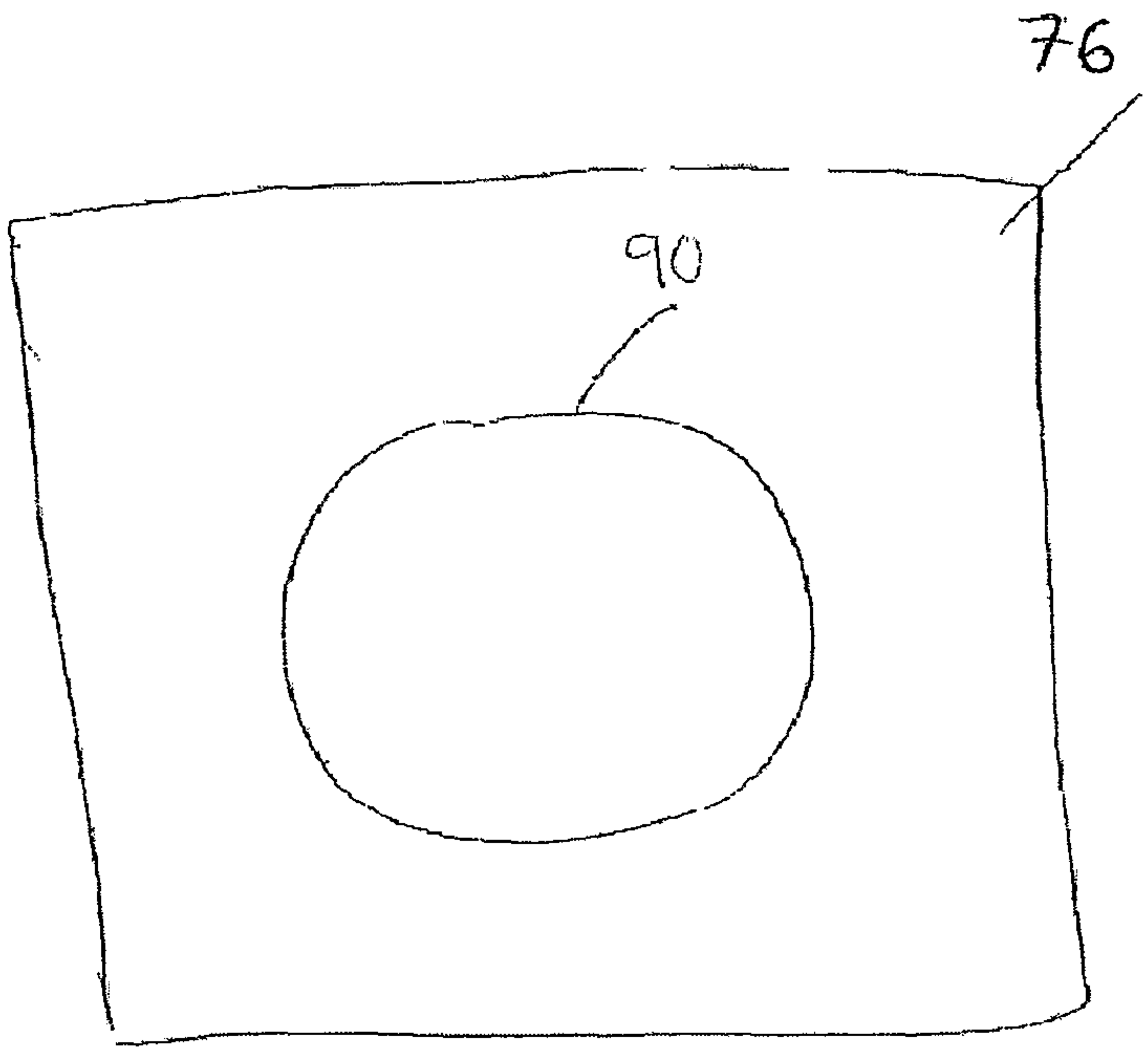



Fig 6c

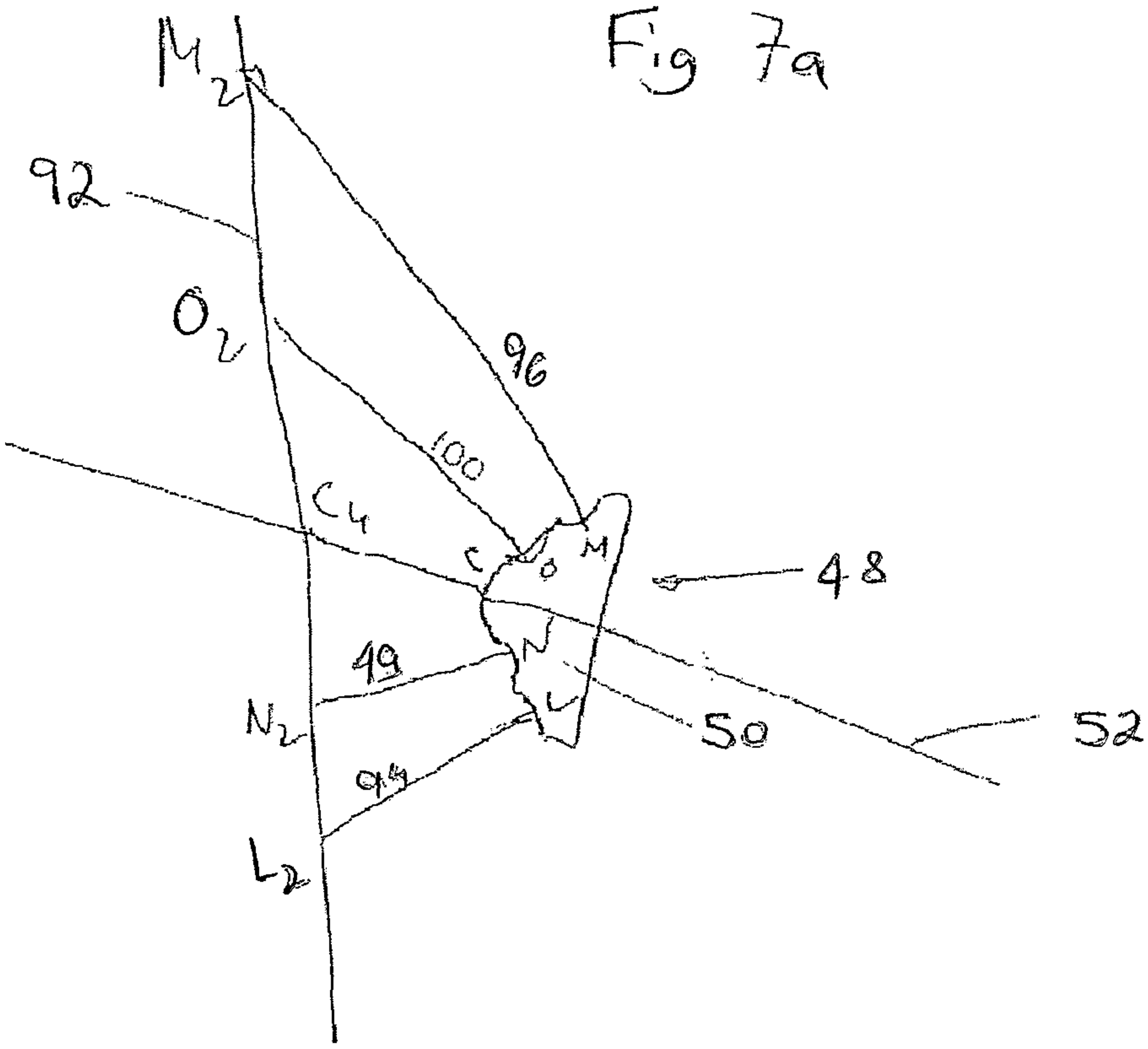

M2
92
O2
96
100
C4
C
O
M
48
N
49
N2
L
50
52
99
L2

Fig 7a

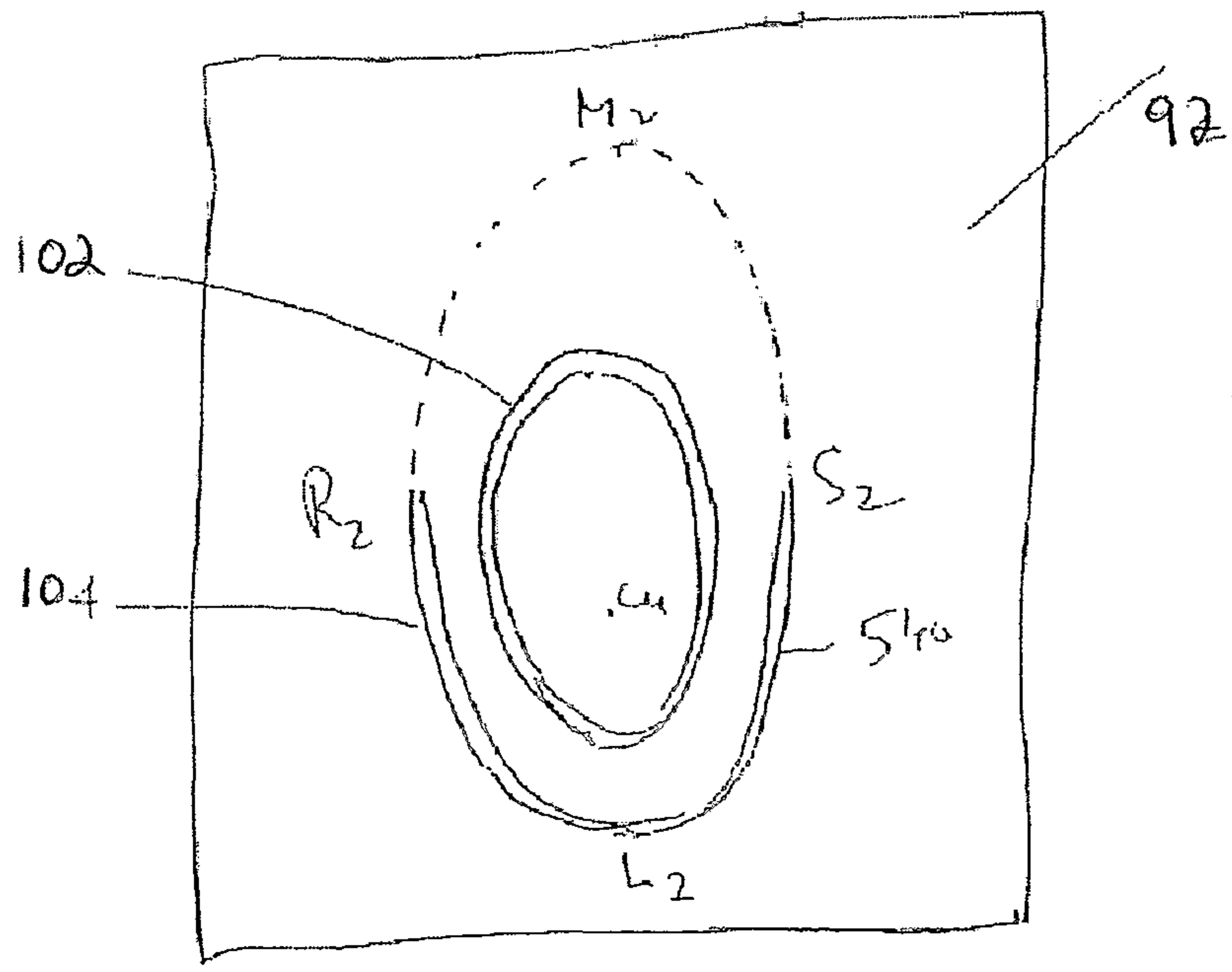

M2
92
102
S2
R2
104
.C4
S1
L2

Fig. 7b

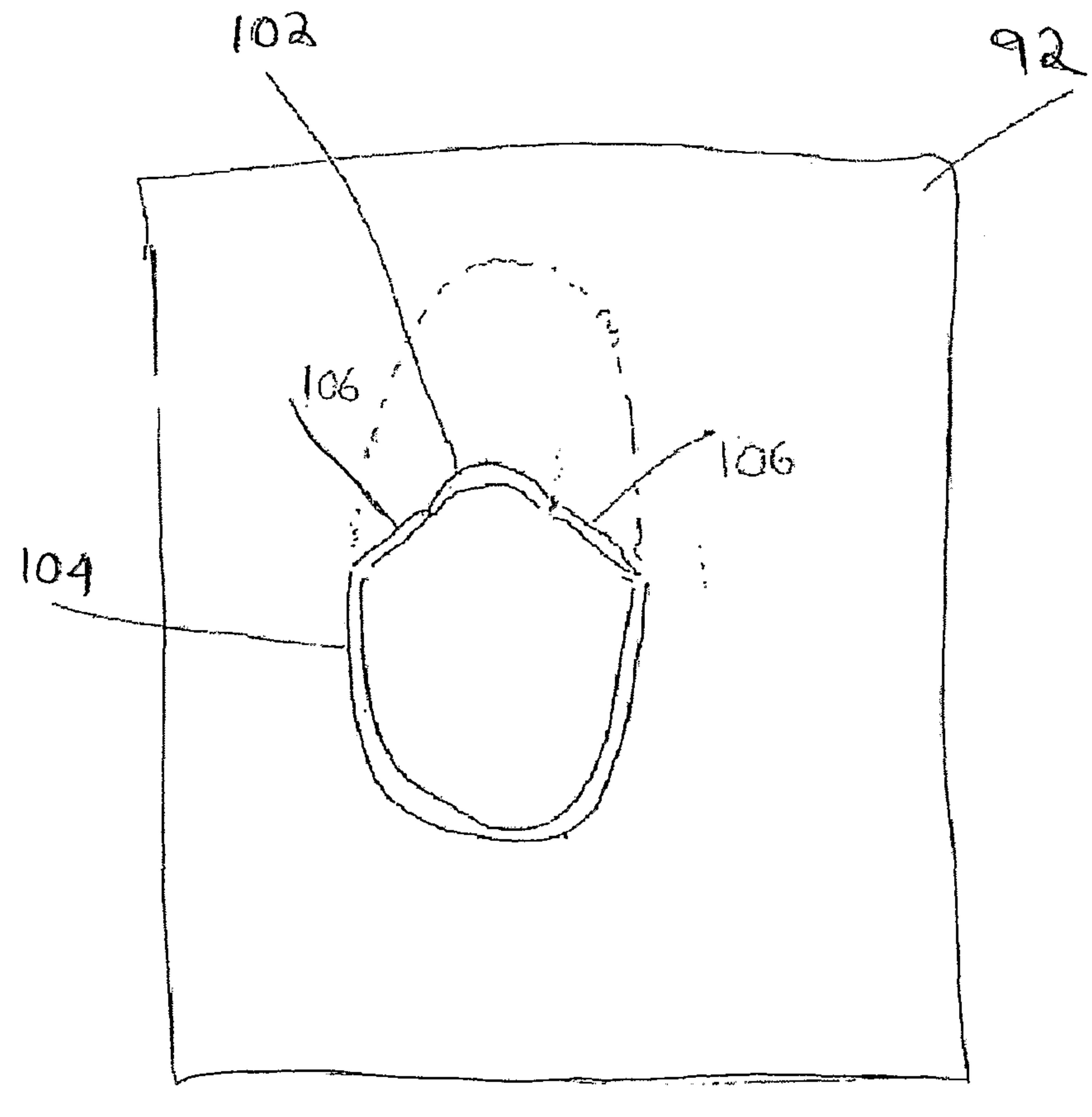
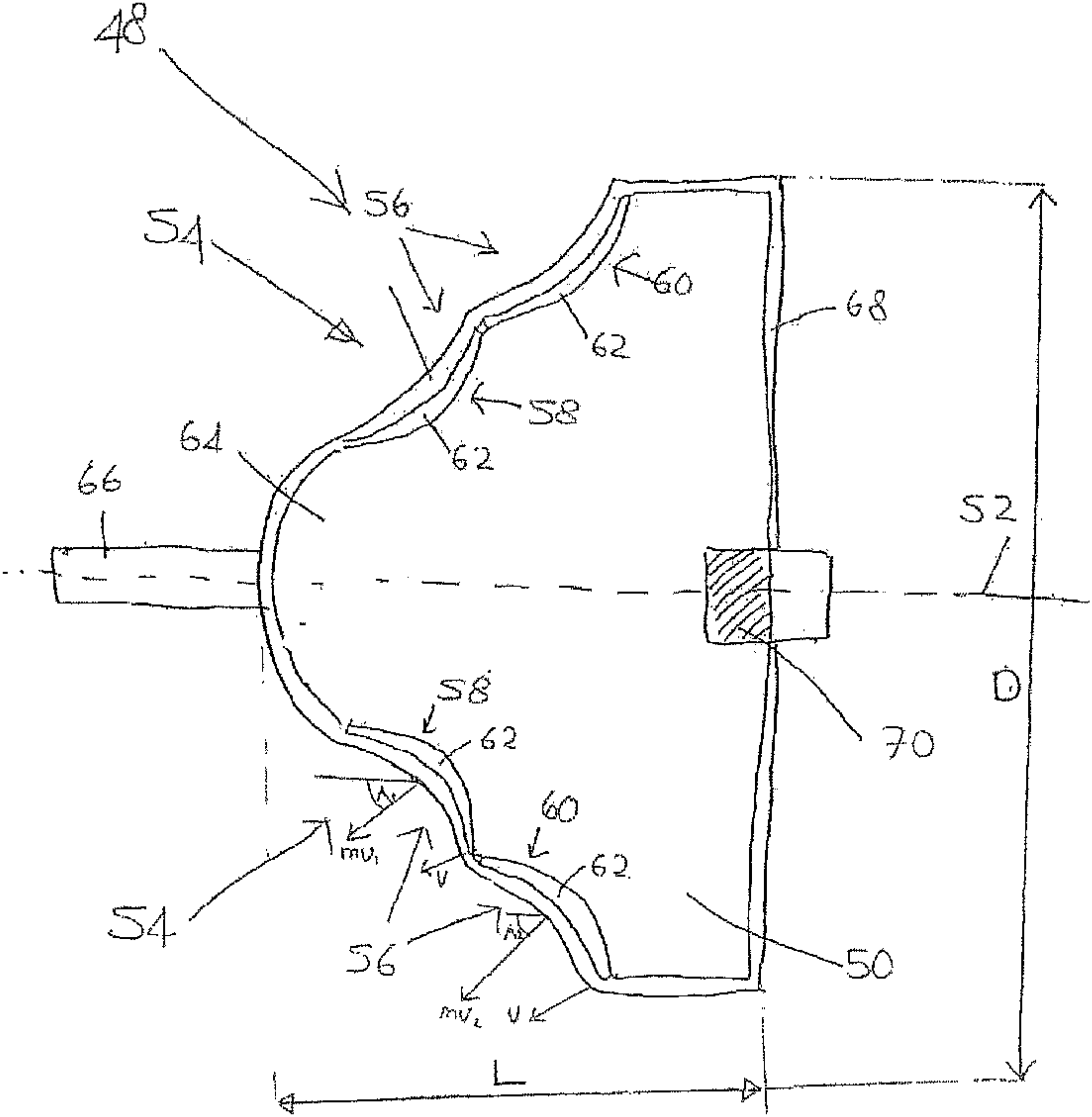



Fig. 7c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