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DESCRIPTION

Description

Technical Field

[0001] The present invention belongs to the technical field of glass ceramics and particularly relates to glass ceramics with excellent mechanical properties, and a preparation method and a product thereof as defined by the appended claim set.

Background Art

[0002] In the context of today's information interconnection, 5G communication has become the mainstream in the industry. By employing the 5G communication technology, a frequency of a transmission signal is raised to a higher frequency. If a traditional metal back cover is employed, transmission of a signal is influenced due to occurrence of severe dielectric loss. Moreover, the development of a wireless charging technology also sets higher requirements for a cover plate of a mobile terminal. At present, a high-alumina glass material is employed as a back cover material for a main cover plate of a mobile phone.

[0003] Glass material is generally employed as a screen and back cover material for mobile terminal electronic equipment to exert the protection effect to corresponding electronic equipment. However, with the increase of the size of a display screen of the mobile terminal, glass on the surface becomes more and more likely to be broken and scratched. The mechanical properties of the existing high-alumina glass cannot meet the demand of development of the mobile terminals, so the mechanical properties of a glass protective layer of an electronic product must be further improved. Furthermore, as the high-alumina glass is high in aluminum content and melting temperature, energy consumption is large, and the cost of a product is high.

[0004] Starting from implementation of controllable preparation in glass ceramics by Corning Incorporated of America in the 1950s, the glass ceramics have started to attract attention from related researchers. The glass ceramics combine the characteristics of glasses and ceramics. In presence of crystalline phases, microcracks on the surface or insides can be prevented from further propagating, or defect without easily propagating, so that the strength and the mechanical properties of the glass ceramics are greatly improved. Compared with original glasses, the glass ceramics have the advantages that the mechanical strength, thermal shock resistance and chemical stability are remarkably improved, the thermal expansion coefficient is adjustable at the same time and the like. The glass ceramics, as an important structural and functional material, play an important role in industrial production and daily life. Due to a structure of coexistence of a glass phase and a crystalline phase, the glass ceramics have more excellent performance than the high-alumina glasses.

[0005] Patent CN106242299A has disclosed glass ceramics and a substrate with the glass ceramics as a base material. Although a sufficient compressive stress value may be obtained through an ion exchange process, a relatively deep stress layer cannot be formed, so that the glass ceramics are easily damaged in the dropping process and cannot be used as a front cover or a back cover of the mobile phone.

[0006] Patent CN107845078A has provided lithium disilicate-containing glass ceramics and a substrate. However, in the composition of the lithium disilicate-containing glass ceramics, contents of Al_2O_3 and Na_2O are too high, uniformly precipitating glass ceramics cannot be obtained in the microcrystallization process although high strength of the surface may be achieved through ion strengthening, so that the transmittance and the strength of the glasses are lowered.

[0007] Patent CN107001120A has provided transparent glass ceramics with petalite and lithium disilicate as main crystalline phases. However, due to too high lithium content in the composition, a glass process window prepared from the transparent glass ceramics is relatively narrow and is easily opacified and devitrified in the operation process.

[0008] Existing glass materials applied to the mobile terminals are single in type and are difficult to meet the demands on individuality development of users. In an industrial preparation coloring method, the surface of glasses is sprayed with an organic material color layer, but a coating may age and even fall off over time, and thus the coloring effect naturally becomes poor. With social and economic development, interest is growing in individualization products. However, colored glasses colored based on a glass substrate have the advantages of uniform and stable coloring and simple preparation flow.

[0009] To sum up, the glass materials applied to the mobile terminals at present have the following problems:

1. Performance aspect: the high-alumina glasses are relatively low in mechanical properties, low in hardness, intolerant in scratching, large in melting difficulty and high in cost and cannot meet the demands of a large screen and a light weight of the mobile terminals; the existing glass ceramic material also has the problems of large brittleness, difficulty in obtaining relatively large depth of the stress layer, uneven crystallization, easiness in opacification and the like.
2. Appearance aspect: a traditional high-strength cover plate is single in color and is inadequate to meet the demands of modern individuation.

[0010] The publication US 9 757 311 B2 discloses a process of using lithium silicate glass ceramic or a lithium silicate glass which comprise the following components

Component wt.-%

SiO₂ 54.0 to 78.0

Li₂O 11.0 to 19.0

Cs₂O 4.0 to 13.0

Al₂O₃ 1.0 to 9.0

P₂O₅ 0.5 to 9.0,

for coating a substrate selected from oxide ceramics, metals and alloys. In example 11 in table 1 a glass-ceramic composition is described that comprises lithium disilicate as the main crystal phase and aluminium phosphate as one of the minor crystal phases.

[0011] The publication US 5 698 482 A discloses a ZrO₂-containing glass-ceramic composition, comprising a ZrO₂ crystalline phase, a lithium phosphate crystalline phase, and at least one additional crystalline phase, and comprising the following components:

Component % by wt.

SiO₂ 42.5 to 58.5; Al₂O₃ 0 to 7.0; La₂O₃ 0 to 9.5; Li₂O 7.0 to 14.5; Na₂O 0 to 7.5; K₂O 0 to 13.5; P₂O₅ 4.0 to 13.5; ZrO₂ 15.0 to 28.0; TiO₂ 0 to 6.0; F 0 to 2.0; BaO 0 to 6.5; CaO 0 to 6.0; B₂O₃ 0 to 3.3. In particular, a glass-ceramic composition is disclosed that comprises lithium silicate and aluminium phosphate crystal phases.

Summary of the Invention

[0012] In order to overcome the deficiencies in the prior art, the technical problem to be solved by the present invention is to provide a preparation method for a glass material and a glass cover plate prepared with the glass material as defined by the appended claim set. The technical solution employed to solve the technical problem by the present invention is as follows:

The glass material prepared in the preparation method of the present invention contains a lithium salt crystalline phase and a phosphate crystalline phase. For the entire material, the crystallinity is up to 90%, the lithium salt crystalline phase accounts for 40-90 wt% of the entire material, and the phosphate crystalline phase accounts for 2-15 wt% of the entire material, wherein the lithium salt crystalline phase is one or more of lithium silicate, lithium disilicate and petalite, and the phosphate crystalline phase is aluminum phosphate or/and aluminum metaphosphate.

[0013] Further, crystalline phase combination types contained in the glass material includes the following types in percentage by mass: 5-15% of the lithium silicate, 20-50% of the lithium disilicate, 20-45% of the petalite and 3-10% of the aluminum phosphate; 5-15% of the aluminum phosphate and 10-40% of the lithium disilicate; or 5-15% of the lithium silicate, 10-15% of the aluminum phosphate and 20-50% of the lithium disilicate; or 30-45% of the petalite, 25-45% of the lithium disilicate and 2-5% of the aluminum metaphosphate; or 20-45% of the petalite, 20-40% of the lithium disilicate and 3-15% of the aluminum metaphosphate; or 25-45% of the petalite and 20-45% of the lithium disilicate; or 25-45% of the petalite and 2-5% of the aluminum metaphosphate. The glass material further contains 1-5 wt% of zirconia.

[0014] A coloring agent is further added to the glass material.

[0015] The coloring agent is a mixture of CoO, CuO, MnO₂, Cr₂O₃, NiO, CeO₂ and TiO₂ and a mixture of CdS and ZnO.

[0016] By using the CoO as the coloring agent for preparing blue glass ceramics, the selected content of the CoO does not exceed 3%. If the content exceeds 3%, a great influence may be caused on the performance of glasses. If the content is lower than 0.5%, the color of a glass flake is not obvious. Thus, preferably, the content of the CoO is 0.5-3 wt%.

[0017] By using the CuO as the coloring agent for preparing green glass ceramics, the selected content of the CuO does not exceed 4%. If the content exceeds 4%, the performance of glasses may be lowered, and the color distribution of the glasses is uneven. If the content is lower than 0.5%, the color of a glass flake is not obvious. Thus, preferably, the content of the CuO is 0.5-4 wt%.

[0018] By using the MnO₂ as the coloring agent for preparing brownish yellow glass ceramics, the selected content of the MnO₂ does not exceed 6%. If the content exceeds 6%, the performance of glasses may be lowered. If the content is lower than 1%, the color of a glass flake is not obvious. Thus, preferably, the content of the MnO₂ is 1-6 wt%.

[0019] By using the Cr₂O₃ as the coloring agent for preparing green glass ceramics, the selected content of the Cr₂O₃ does not exceed 3%. If the content exceeds 3%, the color distribution of glasses is uneven while the performance of the glasses may be lowered. If the content is lower

than 0.1%, the color of a glass flake is not obvious. Thus, preferably, the content of the Cr_2O_3 is 0.1-3 wt%. By using the NiO as the coloring agent for preparing brown or green glass ceramics, the selected content of the NiO does not exceed 4%. If the content exceeds 4%, the color distribution of glasses is uneven while the performance of the glasses may be lowered. If the content is lower than 0.3%, the color of a glass flake is not obvious. Thus, preferably, the content of the NiO is 0.1-3 wt%. By using a mixed coloring agent of CeO_2 and TiO_2 for preparing a yellow glass composition, the usage amount of the CeO_2 is within 6%, and the lowest use amount is larger than 0.8%. A combined amount of the mixed coloring agent is 2-8 wt%.

[0020] By using a mixed coloring agent of CdS and ZnO, the glasses are opacified with thermal treatment, the content of the CdS does not exceed 4%, and the lowest use amount is larger than 0.6%. A combined amount of the mixed coloring agent is 2.5-9 wt%.

[0021] By using Nd_2O_3 as the coloring agent for preparing a magenta glass composition, as Nd_2O_3 as a rare earth element is relatively light in coloring, the color of the glasses cannot be further darkened much even when the used content exceeds 6%, instead, the cost of the glasses is increased. A lower limit of the content of the Nd_2O_3 is 2%. If the content is lower than 2%, a color of a glass flake is light. Thus, preferably, the content of the Nd_2O_3 is 2-6 wt%.

[0022] The method of the present invention preparing the above glass material comprises the steps of:

step 1, uniformly mixing the following raw materials in percentage by mass: 68-74% of SiO_2 , 4-10% of Al_2O_3 , 8-12% of Li_2O , 0.1-3% of Na_2O , 0.1-1% of K_2O , 3-9% of P_2O_5 and 1-6% of ZrO_2 , and putting a mixture in a platinum or alumina crucible;

step 2, heating the mixture for 10-30h in an electric furnace at a temperature ranging from 1250°C to 1450°C for uniformly melting the mixture, and forming a basic glass plate with a thickness of 0.2-2mm with a cast ingot cutting method and a rolling process; and

step 3, implementing thermal treatment on the obtained basic glass plate in order to conduct nucleation and crystal growth, and preparing the glass material.

[0023] In the step 1, the following components are further added to the raw materials in percentage by mass: 0-2% of CaO, 0-1% of BaO, 0-2% of Sb_2O_3 , 0-3% of MgO, 0-6% of ZnO, 0-5% of Y_2O_3 , 0-5% of La_2O_3 , 0-2% of Eu_2O_3 , 0-2% of Gd_2O_3 , 0-4% of TiO_2 , 0.5-3 wt% of CoO, 0.5-4 wt% of CuO, 1-6 wt% of MnO_2 , 0.1-3 wt% of Cr_2O_3 , 0.1-3 wt% of NiO, 2-8 wt% of CeO_2 and TiO_2 and 2.5-9 wt% of CdS and ZnO.

[0024] In the step 3, the thermal treatment process comprises the steps of: keeping the basic glass plate for 2-6h at a temperature of 600-650°C and then for 2-10h at a temperature of 690-770°C.

[0025] Further, the method further comprises step 4 of: conducting ion strengthening on the prepared glass material. The specific operation comprises the steps of: step 1, soaking the glass material in a NaNO_3 molten salt bath for about 5-16h at a temperature of about 420-460°C for ion exchange; and step 2, soaking the glass material in a KNO_3 molten salt bath for about 2-16h at a temperature of about 400-460°C for ion exchange.

[0026] Further, a melting temperature in the step 2 is 1450°C, preferably, 1400°C, and more preferably, 1340°C.

[0027] Furthermore, the whole size of crystals produced in a glass body after being subjected to thermal treatment is smaller than 60nm, preferably, smaller than 50nm, and more preferably, smaller than 40nm.

[0028] A glass cover plate product is prepared by the steps of: conducting cutting and polishing processes on the glass material prepared by the above method and preparing a cover plate with a target thickness and size.

[0029] Further, the Vickers hardness Hv of the glass cover plate product is 900 kgf/mm² or above, and more preferably, is 1000 kgf/mm².

[0030] Further, the glass cover plate product cannot be broken when a 102g steel ball falls onto the glass from 300mm, preferably, a height is 400mm, and more preferably, the height is 450mm or above. Further, the transmittance of the glass cover plate product is 85% or above in the visible light range, and preferably, is 90% or above.

[0031] Further, a compressive stress value CS of a compressive stress layer on the surface of the glass cover plate product is 200Mpa or above, preferably, is 300Mpa or above, and more preferably, is 400Mpa or above.

[0032] Further, a depth DOL of a potassium ion exchange layer of the compressive stress layer of the glass cover plate product is 2μm or above, preferably, is 5μm or above, and more preferably, is 7μm or above.

[0033] Further, a depth DOC of a sodium ion exchange layer of the compressive stress layer of the glass cover plate product is 70μm or above, preferably, is 80μm or above, and more preferably, is 90μm or above.

[0034] SiO_2 is an essential component for a glass reticular structure and becomes an essential component for composing a crystalline phase after being subjected to thermal treatment on original glasses. If an amount of the SiO_2 is smaller than 68%, the obtained glasses cannot obtain a corresponding crystalline phase and crystallinity. Thus, a lower limit of the content of the SiO_2 is preferably 68%. On the other hand, by enabling

the content of the SiO_2 to be 74% or below, over viscosity increase and meltability weakening may be inhibited. Thus, an upper limit of the content of the SiO_2 is preferably 74% or below.

[0035] Al_2O_3 may form a component for forming the glass reticular structure. As a glass network intermediate and an important component for facilitating stabilization of the structure of the glasses and improvement in chemical durability, the Al_2O_3 may further improve the thermal conductivity of the glasses; and the Al_2O_3 can also become an essential component for composing the crystalline phase after being subjected to thermal treatment on original glasses. However, if the content of the Al_2O_3 is smaller than 4%, the best effect cannot be achieved. Thus, a lower limit of the content of the Al_2O_3 is 4%. On the other hand, as the melting point of the Al_2O_3 is high, if the content exceeds 10%, the meltability and the devitrification resistance are poor correspondingly. Thus, an upper limit of the content of the Al_2O_3 is 10%.

[0036] Na_2O is obvious in fluxing action. When chemical strengthening is conducted through ion exchange, the Na_2O in the glass ceramics may be subjected to ion exchange to form a compressive stress layer and is an essential component for forming high-strength glass ceramics, and thus the content of the Na_2O is at least 0.1% or above. However, over introduction may easily cause an increase in expansion coefficient of the glasses as well as a weakening in thermostability, chemical stability and mechanical strength of the glasses. In the composition of the glass ceramics prepared according to the present invention, an increase of the content of sodium oxide may be against precipitation of required crystalline phases in a glass substrate, and thus the content of the sodium oxide is preferably 3%. Thus, when chemical toughening is conducted through ion exchange, a lower limit of the content of the Na_2O is 0.1%, and an upper limit is 3%.

[0037] K_2O is an alternative component for facilitating improvement in meltability and formability of the glasses, and the effect of the K_2O is similar to Na_2O , capable of improving the whiteness and the smoothness of the glasses. In the composition of the glass ceramics prepared according to the present invention, an increase of the content of potassium oxide may be against precipitation of required crystalline phases in a glass substrate, and thus the content of the potassium oxide is preferably 1% or below. When chemical toughening is conducted through ion exchange, potassium contained in the glasses has the effects of improving the compressive stress of the surface and increasing the depth of a stress layer. Thus, a lower limit of the content of the K_2O is 0.1%, and an upper limit is preferably 1%.

[0038] ZrO_2 has the effect of a nucleating agent in the glass ceramics, and can also become an essential component for composing the crystalline phase through thermal treatment on the original glasses and is beneficial to improving the refractive index and the chemical stability of the glasses and lowering the ultraviolet transmitting ability of the glasses. However, if the glasses contain excessive ZrO_2 , melting of the glasses may be difficult, and the glasses may be easily devitrified. A lower limit of the content of the ZrO_2 is preferably 1%, and an upper limit is preferably 6%. TiO_2 is an alternative component for facilitating a decrease in melting temperature of the glass ceramics, improvement in refractive index and chemical stability of the glass ceramics and improvement in absorption ability to ultraviolet light. In addition, TiO_2 has the effect of a nucleation agent and is beneficial to crystallization in the thermal treatment process. A lower limit of the content of the TiO_2 is larger than 0. On the other hand, by enabling the content of the TiO_2 to be 4% or below, the melting temperature of the glasses may be decreased, and the crystallization degree may be controlled. Thus, an upper limit of the content of the TiO_2 is preferably 4%.

[0039] BaO is an alternative component for facilitating improvement in low-temperature melting property of the glasses. When used in a small amount, the BaO assists melting and has the effects of improvement in refractive index, density and chemical stability of the glasses, strong radiation absorption ability and the like. When the amount of the BaO is excessive, clarification may be difficult, secondary bubbles are produced, and the glasses are easily devitrified. Thus, an upper limit of the content of the BaO is preferably 1%.

[0040] MgO is beneficial to lowering the viscosity of the glasses and inhibiting crystallization of the original glasses, also has the effect of improving the low-temperature melting property and is an alternative component. A lower limit of the content of the MgO is larger than 0. However, if the content of the MgO is over high, the devitrification resistance may be weakened, non-ideal crystals may be obtained after crystallization, and the performance of the glass ceramics is lowered, so that an upper limit of the content of the MgO is preferably 3%.

[0041] ZnO can improve the melting property of the glasses and improve the chemical stability of the glasses and is an alternative component. A lower limit of the content of the ZnO is preferably larger than 0. On the other hand, an upper limit of the content of the ZnO is controlled to be 6%, so that the required opacification effect may be obtained, and the influence on mechanical properties of the glasses is little.

[0042] Y_2O_3 and La_2O_3 are alternative components for facilitating the meltability and the formability of the glasses and both are capable of improving the hardness, chemical stability and thermal conductivity of the glass ceramics. With the addition of the Y_2O_3 and the La_2O_3 in a small amount, the melting temperature of the glasses may be lowered, and the temperature of a liquid phase is decreased to a certain degree. However, if the content of the Y_2O_3 is excessive, the devitrification of the glasses may be caused. Thus, the content of the Y_2O_3 or the La_2O_3 is 5%.

[0043] Eu_2O_3 and Gd_2O_3 are alternative components for facilitating the meltability and the formability of the glasses. Through the introduction, the Eu_2O_3 and the Gd_2O_3 may both obviously improve the melting effect of the glasses and are beneficial to the formation of the glasses. More importantly, in presence of the Li_2O , the Na_2O , the MgO and the ZnO , by introducing Eu_2O_3 or Gd_2O_3 for exerting synergistic effect with the above three components, the components mutually support functionally, further have the effects of improving the paramagnetism of the glass ceramics, lowering the magnetic loss and improving the mechanical properties of the glass ceramics and are beneficial to being used as a protective material of a mobile terminal. An upper limit of an introduction amount of the Eu_2O_3 or the Gd_2O_3 is preferably 2%.

[0044] Introduction of Sb_2O_3 , as a clarifying agent of the glasses, is beneficial to lowering an amount of bubbles in a melt and improving the

clarifying effect of the glass body and is crucial to prepare the glass ceramics satisfying the use of the mobile terminal. An upper limit of an introduction amount of the Sb_2O_3 is preferably 2%.

[0045] Li_2O is a component for improving the low-temperature meltability and the formability of the glasses and may become an essential component required for crystalline phase composition through thermal treatment on the original glasses. However, if the content of the Li_2O is smaller than 8%, the crystallization effect is poor, while the melting difficulty is increased. On the other hand, if the content of the Li_2O is excessive, the obtained crystals are easily unstable and largened, the chemical durability of the glasses is lowered, or the average coefficient of linear expansion of the glasses is raised. Thus, an upper limit of the content of the Li_2O is preferably 12%. When chemical toughening is conducted through ion exchange, if a system contains the Li_2O component, a large content of lithium is also very effective to the aspect of forming a relatively deep compressive stress layer.

[0046] P_2O_5 can exert the effects of a network former and the nucleating agent in the glasses and is also beneficial to lowering a melting temperature of the glasses. Under a low concentration, P_2O_5 is the nucleating agent in the crystallization process mainly and exerts the effect of controlling the size of crystals. After the concentration of the P_2O_5 is increased, the P_2O_5 participates to formation of a glass network. Due to a strong electric field produced by lone pair electrons in a P-O structure, the structure of a silica tetrahedron in the glass network changes. In this glass system, the P_2O_5 is also an essential component for precipitating the phosphate crystalline phase and is also capable of increasing abbe number and improving the ultraviolet transparency and the transparency. When basic glasses do not contain P_2O_5 or the content of the P_2O_5 is too low, the basic glasses cannot entirely crystallized in the microcrystallization process, so that atomization is caused on the surface of the basic glasses, and the glass ceramics with uniform crystallization is difficult to obtain.

[0047] In this system, on one hand, by increasing the content of the P_2O_5 , a part of $[\text{SiO}_4]$ silica tetrahedron is converted to $[\text{SiOe}]$ octahedral structure. In the crystallization process, in the glasses, Li^+ is combined with a silica structure to form LiSiO_3 crystals, and a $\text{Li}_2\text{Si}_2\text{O}_5$ crystalline phase is formed finally. As crystallization proceeds, Li_2SiO_3 or $\text{Li}_2\text{Si}_2\text{O}_5$ is further combined with an Al-O structure to form a $\text{Li}[\text{AlSi}_4\text{O}_{10}]$ petalite crystalline phase. On the other hand, by lowering the content of lithium in the glass composition system at the same time, more Al-O structures which more easily form the petalite originally and more P-O structures which are weak in a glass network form a part of the aluminum metaphosphate and aluminum phosphate crystalline phases, so that the purpose of improving the mechanical properties and the machining properties of the glass ceramics with multiple crystalline phases is achieved. However, if the content of the P_2O_5 in the system is too large, phase separation is easily caused to enable the devitrification resistance of the glasses to be weakened and batch production of the glasses to be poor. Thus, the content of the P_2O_5 is preferably 3-9 wt%.

[0048] For the present invention, by lowering the content of the lithium and increasing the content of the phosphorus in the raw materials for preparing the glass material at the same time and combining with a preparation process, the contents of the lithium salt crystalline phase and the phosphor salt crystalline phase in the glass material are controlled, the problems of large brittleness, poor toughness and the like of the glass ceramics with the lithium disilicate as a main crystalline phase are solved, and the mechanical properties of a product are improved compared with inventions and products on the existing market. For the glass material subjected to thermal treatment, combinations with various crystal types may be formed, and thus a corresponding crystalline phase may be selected according to the actual needs. The glass material may have different personalized colors by selectively adding various coloring agents. In the present invention, through repeated tests and researches, for specific components for composing a glass ceramic product, the contents of the specific components and a content ratio are stipulated as specific values, and several specific crystalline phases precipitate from the specific components, so that the glass ceramics or a glass product of the present invention is obtained with a relatively low cost. After the glass material produced according to the present invention is toughened, the Vickers hardness (Hv) is 900 kgf/mm² or above. The glass material or substrate produced according to the present invention is suitable for protective members such as mobile terminal equipment and optical equipment and has high hardness and strength. Furthermore, the glass material produced according to the present invention may also be used for other decorations such as outer frame members of portable electronic equipment.

Brief Description of the Drawings

[0049]

Fig. 1 is a curve of differential scanning calorimetry (DSC) for measuring Embodiment 1.

Fig. 2 is a curve of the transmittance for measuring Embodiment 2.

Fig. 3 is an XRD pattern for measuring Embodiment 1.

Fig. 4 is an XRD pattern for measuring Embodiment 2.

Fig. 5 is an XRD pattern for measuring Embodiment 3.

Fig. 6 is an XRD pattern for measuring Embodiment 4.

Fig. 7 measures an SEM morphology of crystals after Embodiment 3 is corroded by HF.

Fig. 8 measures line scanning of energy spectrum of potassium and sodium elements on a section of Embodiment 3.

Fig. 9 is a display picture of FSM-6000 for measuring Embodiment 3.

Fig. 10 is impressions for measuring a hardness test for measuring Embodiment 3.

Fig. 11 is a glass size schematic view for a ball falling test.

Detailed Description of the Invention

[0050] A composition range of various components of the glass ceramics produced according to the present invention is described below. In this description, the contents of various components are expressed by employing a weight percentage relative to a glass material total weight of the composition converted into oxides, unless otherwise noted. Here, the "composition converted into oxides" refers to that under the condition that oxides, mixed salts and the like which are used as the raw materials of the composition of the glass ceramics of the present invention are totally decomposed and converted into oxides when molten, the material total weight of the oxides is taken as 100%.

Embodiment

Embodiment 1

Step 1, weighing and mixing of components

[0051] According to various components and mass percentages thereof listed in example 1 in Table 1, corresponding raw materials were selected and uniformly mixed, and a uniformly mixed mixture was put in a platinum or alumina crucible.

Step 2, preparation of a basic glass plate

[0052] According to the degree of difficulty of melting of the glass composition, heat preservation was conducted on the mixture for 20h in an electric furnace at a temperature of 1450°C, the mixture was uniformly molten, and a basic glass plate with a thickness of 0.1mm was formed with a cast ingot cutting method.

Step 3, thermal treatment for crystallization

[0053] Thermal treatment for crystallization was conducted on the obtained basic glass plate, the specific method of which comprises the steps that thermal insulation was performed on the basic glass plate for 2h at 650°C for nucleation and then for 8h at 760°C for crystal growth, and then furnace cooling was conducted to prepare glass ceramics. Process systems of thermal treatment for crystallization of the glasses of other examples are as shown in the table.

Step 4, machining of the glass ceramics

[0054] A prepared glass ceramic sheet was subjected to treatment with processes of cutting, edging, polishing and the like by using a machine, and a glass sheet in a specified size and with a thickness of 160×70×0.6mm was prepared.

Step 5, chemical strengthening of the glass ceramics

[0055] A compressive stress layer was formed on the surface of the glasses with a high-temperature ion exchange method to achieve strengthening of a glass cover plate. A two-step high-temperature ion exchange method was uniformly selected for strengthening and comprises the following specific steps that step 1, the glass material was soaked in a NaNO_3 molten salt bath for about 8h at a temperature of 450°C; and step 2, the glass material was soaked in a KNO_3 molten salt bath for 2h at a temperature of 400°C.

[0056] Performance tests were conducted on the obtained glass material cover plate product, and each performance data is shown as corresponding data in Table 1.

Embodiment 2

Step 1, weighing and mixing of components

[0057] According to various components and mass percentages thereof listed in example 2 in Table 2, corresponding raw materials were selected and uniformly mixed, and a uniformly mixed mixture was put in a platinum crucible.

Step 2, preparation of a basic glass plate

[0058] According to the degree of difficulty of melting of the glass composition, heat preservation was conducted on the mixture for 20h in an electric furnace at a temperature of 1420°C, the mixture was uniformly molten, and a basic glass plate with a thickness of 2.0mm was formed with a cast ingot cutting method.

Step 3, thermal treatment for crystallization

[0059] Thermal treatment for crystallization was conducted on the obtained basic glass plate, the specific method of which comprises the steps that thermal insulation was performed on the basic glass plate for 4h at 630°C for nucleation and then for 3h at 730°C for crystal growth, and then furnace cooling was conducted to prepare glass ceramics.

Step 4, machining of the glass ceramics

[0060] A prepared glass ceramic sheet was subjected to treatment with processes of cutting, edging, polishing and the like by using a machine, and a glass sheet in a specified size and with a thickness of 160×70×0.6mm was prepared.

[0061] Performance tests were conducted on the obtained glass material cover plate product, and each performance data is shown as corresponding data in Table 1.

[0062] For crystalline phases of the glass ceramics before high-temperature ion strengthening in Embodiments 1-14, by using an X-ray diffractometer and comparing with a standard PDF card, corresponding crystalline phases in the glass ceramics were analyzed, and corresponding crystallinity was calculated.

[0063] Average grain size: determination was conducted by using a scanning electron microscope, surface treatment was conducted on the glass ceramics in HF acid, coating with gold spraying was conducted on the surfaces of the glass ceramics, surface scanning was conducted under the scanning electron microscope to observe diameters of grains, average diameter sizes of all the grains are added together, and a sum was divided by an amount of crystalline grains in an image. Transmittance: test was conducted by using an ultraviolet and visible spectrophotometer.

[0064] Vickers hardness: measurement was conducted by using Vickers, wherein a loading force was 200g, and a loading time was 15s.

[0065] CS: that is the surface compressive stress layer formed by potassium ions, and determination was conducted by using a glass surface stress gauge FSM-6000.

[0066] DOC: that is a depth of a sodium ion strengthened layer, and determination was conducted by using a glass surface stress gauge SLP-1000 from Japan ORIHARA.

[0067] DOL: that is a depth of a potassium ion strengthened layer, and determination was conducted by using a glass surface stress gauge FSM-6000 from Japan ORIHARA.

[0068] Ball falling height: that is a maximal ball falling height obtained in such a way that a strengthened glass ceramic plate in a size of 160×70×0.8mm was put on a rubber frame for fixing after two surfaces of the strengthened glass ceramic plate were polished, 102g steel ball fallen down from a specified height, and the glass sheet was not broken and could bear the impact. Particularly, test data recorded as 380-420mm in the embodiments expresses the impact borne by the glass plate without being broken although the steel ball falls onto the glass sheet from a height of 400mm. Colors in the embodiments are those of corresponding glass plates, obtained through visual inspection.

Table 1

| Component (wt%) | Embodiment | | | | | | |
|--------------------------------|------------|-----|-----|-----|-----|-----|-----|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| SiO ₂ | 68 | 69 | 70 | 71 | 72 | 73 | 74 |
| Al ₂ O ₃ | 10 | 7 | 9 | 5 | 6.5 | 7.2 | 5.5 |
| TiO ₂ | 0 | 1.2 | 1.6 | 1.2 | 2 | 0.1 | 0.5 |
| CaO | 0.5 | 0.8 | 1 | 0.5 | 0.2 | 0.1 | 0.2 |
| Li ₂ O | 10 | 9 | 8 | 8 | 9 | 10 | 12 |
| Na ₂ O | 1 | 3 | 1.5 | 1.8 | 1 | 0.2 | 0.5 |
| K ₂ O | 0.1 | 0.3 | 0.4 | 0.5 | 0.7 | 0.1 | 0.4 |
| P ₂ O ₅ | 3 | 4.5 | 5 | 9 | 6 | 3 | 4 |

| Component (wt%) | Embodiment | | | | | | |
|---|--|--|--|---------------------------------|---------------------------------|--|--|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| ZrO ₂ | 5 | 2 | 1 | 1 | 1 | 5 | 1.8 |
| BaO | 0 | 1 | 0.5 | 0 | 0 | | 0 |
| Sb ₂ O ₃ | 2 | 1.8 | 2 | 2 | 1.5 | 1.3 | 1.1 |
| MgO | 0.2 | 0.2 | | | | | |
| ZnO | 0.2 | | | | | | |
| Y ₂ O ₃ | | 0.2 | | | | | |
| La ₂ O ₃ | | | | 0.2 | | | |
| Eu ₂ O ₃ | | | | 0.2 | | | |
| Gd ₂ O ₃ | | | | | 0.1 | | |
| SiO ₂ /Li ₂ O | 6.8 | 7.7 | 8.8 | 8.9 | 8.0 | 7.3 | 6.2 |
| ZrO ₂ +P ₂ O ₅ +TiO ₂ | 8 | 7.7 | 7.6 | 7.8 | 9 | 8.1 | 6.3 |
| Melting process | 1450°C 20h | 1420°C 20h | 1400°C 20h | 1430°C 30h | 1360°C 20h | 1340°C 30h | 1400°C 25h |
| Nucleation process | 650°C 2h | 630°C 4h | 620°C 4h | 620°C 4h | 620°C 4h | 630°C 4h | 620°C 4h |
| Crystallization process | 760°C 8h | 730°C 3h | 720°C 3h | 700°C 6h | 700°C 6h | 720°C 3h | 720°C 3h |
| Crystalline phase | Zirconia Aluminum phosphate Lithium disilicate | Aluminum silicate phosphate Lithium disilicate | Petalite Lithium disilicate Aluminum metaphosphate | Petalite Aluminum metaphosphate | Petalite Aluminum metaphosphate | Petalite Lithium disilicate Aluminum metaphosphate | Petalite Lithium disilicate Aluminum metaphosphate |
| CS (MPa) | 400 | 300 | 380 | 400 | 360 | 395 | 432 |
| DOC (μm) | 100 | 95 | 110 | 105 | 90 | 110 | 93 |
| DOL (μm) | 7 | 8 | 8 | 7 | 6 | 8 | 7 |
| Vickers hardness | 1055 | 950 | 970 | 925 | 930 | 950 | 1000 |
| Ball falling | 400 | 400 | 400 | 400 | 400 | 450 | 450 |
| Color | Opacifi | Transpa | Transpa | Transpa | Transp | Transpa | Transpa |

Table 2

| Component | Embodiment | | | | | | |
|---|------------|------------|------------|------------|------------|------------|------------|
| | 1' | 2' | 3' | 4' | 5' | 6' | 7' |
| SiO ₂ | 68 | 69 | 70 | 71 | 70 | 71 | 73 |
| Al ₂ O ₃ | 9 | 6 | 8 | 5 | 6 | 5 | 5 |
| TiO ₂ | 0.3 | 0.1 | 0.5 | 0.8 | 1 | 0 | 0.6 |
| CaO | 0.4 | 0.8 | 1 | 0.5 | 0.8 | 0.2 | 0.6 |
| Li ₂ O | 9 | 11.5 | 12 | 12 | 9 | 12 | 11 |
| Na ₂ O | 0.3 | 0.5 | 0.7 | 1.5 | 1 | 1.5 | 0.5 |
| K ₂ O | 0.1 | 0.3 | 0.4 | 0.7 | 0.5 | 0.4 | 0.2 |
| P ₂ O ₅ | 9 | 3.5 | 4 | 6 | 6 | 5 | 3 |
| ZrO ₂ | 1.5 | 5 | 1 | 1 | 3 | 3.5 | 4.6 |
| BaO | 0 | 1 | 0.4 | 0 | 0.2 | 0 | |
| Sb ₂ O ₃ | 2 | 1.8 | 2 | 1.5 | 1.5 | 1.4 | 1.5 |
| MgO | 0.2 | 0.5 | | | 1 | | |
| ZnO | 0.2 | | | | 0 | | |
| SiO ₂ /Li ₂ O | 7.6 | 6.0 | 5.8 | 5.9 | 7.8 | 5.9 | 6.6 |
| ZrO ₂ +P ₂ O ₅ +TiO ₂ | 10.8 | 8.6 | 5.5 | 7.8 | 10 | 8.5 | 8.2 |
| Melting process | 1450°C 20h | 1420°C 20h | 1380°C 20h | 1400°C 30h | 1360°C 20h | 1400°C 30h | 1400°C 25h |
| Melting temperature/°C | 1450°C | 1450°C | 1340°C | 1360°C | 1380°C | 1400°C | 1450°C |
| Nucleation process/°C | 640°C 2h | 630°C 4h | 620°C 5h | 630°C 4h | 630°C 4h | 620°C 4h | 630°C 6h |
| Crystallization | 730°C 4h | 740°C 3h | 720°C 3h | 700°C 6h | 720°C 3h | 720°C 3.5h | 760°C 4h |

| Component | Embodiment | | | | | | |
|--|--|--|--|--|--|--|---|
| | 1' | 2' | 3' | 4' | 5' | 6' | 7' |
| process/°C | | | | | | | |
| Crystalline phase | Petalite Lithium disilicate Aluminu m metapho sphate | Lithium silicate Lithium disilicate Aluminu m phosphat e | Petalite Lithium disilicate Aluminu m metapho sphate | Petalite Lithium disilicate Aluminu m metapho sphate | Petalite Lithium disilicate Aluminu m metapho sphate | Lithium silicate Lithium disilicate Aluminu m phosphat e | Lithiu m silicate Lithiu m disilica te Alumi num phosph ate |
| CS (MPa) | 380 | 390 | 410 | 420 | 400 | 420 | 430 |
| DOC (µm) | 100 | 105 | 105 | 100 | 98 | 93 | 95 |
| DOL (µm) | 9 | 10 | 9 | 9 | 8 | 7 | 8 |
| Vickers hardness (Kgf/mm ²) | 1000 | 950 | 970 | 930 | 950 | 1000 | 1010 |
| Ball falling height (mm) | 400 | 380 | 400 | 390 | 400 | 420 | 405 |
| Color | Transpa rent | Transpar ent | Transpare nt | Transpar ent | Transpar ent | Transpar ent | Transp arent |

Table 3

| Component | Embodiment | | | | | | |
|---|--|--|--|--|--|---|--|
| | 8 | 9 | 10 | 11 | 12 | 13 | 14 |
| SiO ₂ | 70.5 | 69 | 70 | 71 | 70 | 68 | 70 |
| Al ₂ O ₃ | 8 | 7 | 6 | 9 | 6.5 | 6 | 4.5 |
| TiO ₂ | 0 | 1.2 | 1.6 | 1.5 | 4 | 2 | 0 |
| CaO | 0.5 | 0.8 | 1 | 1.4 | 0.5 | 1.8 | 0.5 |
| Li ₂ O | 12 | 9 | 9 | 8 | 9 | 8 | 12 |
| Na ₂ O | 1 | 2.5 | 1.5 | 1.8 | 1 | 1.5 | 0.5 |
| K ₂ O | 0.1 | 0.3 | 0.4 | 0.5 | 0.6 | 1 | 0.4 |
| P ₂ O ₅ | 3.5 | 4.5 | 3 | 3 | 4 | 3 | 5 |
| ZrO ₂ | 1 | 2 | 1 | 1.3 | 1 | 1 | 2 |
| BaO | 0 | 1 | 0.5 | 0 | 0 | 0.2 | 0 |
| Sb ₂ O ₃ | 2 | 1.8 | 2 | 2 | 1.5 | 1.3 | 1.1 |
| MgO | 0.2 | 0.2 | | | | | |
| ZnO | 0.2 | | | | | 5 | |
| CoO | 1 | | | | 0.2 | | |
| CuO | | 0.7 | | | | | |
| MnO ₂ | | | 4 | | | | |
| Cr ₂ O ₃ | | | | 0.5 | | 1 | |
| NiO | | | | | 0.7 | | |
| CeO ₂ | | | | | | | |
| CdS | | | | | | 1.2 | |
| Nd ₂ O ₃ | | | | | | | 4 |
| SiO ₂ /Li ₂ O | 79.5 | 78 | 77 | 80.3 | 77.5 | 75 | 76.5 |
| ZrO ₂ +P ₂ O ₅ +TiO ₂ | 5.9 | 7.7 | 7.8 | 8.9 | 7.8 | 8.5 | 5.4 |
| Melting temperature | 1430°C 20h | 1420°C 20h | 1350°C 25h | 1420°C 25h | 1350°C 20h | 1340°C 15h | 1340°C 20h |
| Nucleation process | 620°C 4h | 620°C 4h | 620°C 4h | 620°C 4h | 620°C 4h | 620°C 4h | 620°C 4h |
| Crystallization process | 720°C 3h | 720°C 3h | 720°C 3h | 720°C 3h | 720°C 3h | 720°C 3h | 720°C 3h |
| Crystalline phase | Petalite Lithium disilicat e Aluminu m metapho sphate | Petalite Lithium disilicat e Aluminu m metapho sphate | Petalite Lithium disilicat e Aluminu m metapho sphate | Petalite Lithium disilicat e Aluminu m metapho sphate | Petalite Lithium disilicat e Aluminu m metapho sphate | Petalite Cadmium sulfide Aluminu m metapho sphate | Petalite Lithium disilicat e Aluminu m metapho sphate |
| CS (MPa) | 400 | 300 | 380 | 410 | 380 | 385 | 420 |
| DOC (µm) | 100 | 95 | 110 | 105 | 88 | 91 | 120 |

| | | | | | | | |
|--|--|--|--|--|--|---|--|
| Crystalline phase | Petalite Lithium disilicat e Alumin um metaphosphate | Petalite Lithium disilicat e Alumin um metaphosphate | Petalite Lithium disilicat e Alumin um metaphosphate | Petalite Lithium disilicat e Alumin um metaphosphate | Petalite Lithium disilicat e Alumin um metaphosphate | Petalite Cadmiu m sulfide Alumin um metaphosphate | Petalite Lithium disilicat e Alumin um metaphosphate |
| DOL (μm) | 7 | 8 | 8 | 7 | 9 | 7 | 8 |
| Vickers hardness (Kgf/mm^2) | 950 | 950 | 950 | 950 | 950 | 1000 | 950 |
| Ball falling height (mm) | 400 | 400 | 350 | 400 | 400 | 400 | 400 |
| Color | Blue | Green | Browni sh yellow | Green | Opacify ing green | White | Lavend er |

[0069] The above are only embodiments of the present invention and do not limit the patent scope of the present invention.

REFERENCES CITED IN THE DESCRIPTION

Cited references

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Patent documents cited in the description

- [CN106242299A \[0008\]](#)
- [CN107845078A \[0009\]](#)
- [CN107001120A \[0007\]](#)
- [US9757311B2 \[0010\]](#)
- [US5696462A \[0011\]](#)

Patentkrav

1. En fremgangsmåde til fremstilling af et glasmateriale, der indeholder en litiumsaltkrystallinsk fase og en fosfatkrystallinsk fase, kendetegnet ved, at krystalliniteten for hele materialet er op til 90 %, den litiumsaltkrystallinske fase udgør 40-90 vægt% af hele materialet, og den fosfatkrystallinske fase udgør 2-15 vægt% af hele materialet, kendetegnet ved, at den litiumsaltkrystallinske fase er en eller flere af litiumsilikat, litiumdisilikat og petalit, og kendetegnet ved, at den fosfatkrystallinske fase er aluminiumfosfat og/eller aluminiummetafosfat, **kendetegnet ved, at** den omfatter følgende trin:

trin 1, ensartet blanding af følgende råmaterialer i masseprocent: 68-74 % SiO_2 , 4-10 % Al_2O_3 , 8-12 % Li_2O , 0,1-3 % Na_2O , 0,1-1 % K_2O og 3-9 % P_2O_5 , og anbringelse af en blanding i en platin- eller aluminadigel;

trin 2, opvarmning af blandingen i 10-30 timer i en elektrisk ovn ved en temperatur på mellem 1250 °C og 1450 °C for at smelte blandingen ensartet og danne en grundglasplade med en tykkelse på 0,2-2 mm ved hjælp af en støbeblokskæringsmetode og en valseproces; og

trin 3, udførelse af varmebehandling på den fremstillede grundglasplade for at foretage kerneudvikling og krystalvækst og fremstille glasmaterialet.

2. Fremgangsmåden til fremstilling af glasmaterialet ifølge krav 1, **kendetegnet ved, at** den yderligere omfatter trin 4: udførelse af ionforstærkning på det fremstillede glasmateriale; den specifikke operation omfatter trin 1, iblødsætning af glasmaterialet i et NaNO_3 -smeltsaltbad i 5-16 timer ved en temperatur på 420-460 °C for ionudveksling; og trin 2, iblødsætning af glasmaterialet i et KNO_3 -smeltsaltbad i cirka 2-16 timer ved en temperatur på 400-460 °C for ionudveksling.

3. Fremgangsmåden til fremstilling af glasmaterialet ifølge krav 1, **kendetegnet ved, at** der i trin 1 yderligere tilsættes følgende komponenter i råmaterialerne i masseprocent: 1-6 % ZrO_2 , 0-2 % CaO , 0-1 % BaO , 0-2 % Sb_2O_3 , 0-3 % MgO , 0-6 % ZnO , 0-5 % Y_2O_3 , 0-5 % La_2O_3 , 0-2 % Eu_2O_3 , 0-2 % Gd_2O_3 og 0-4 % TiO_2 .

4. Fremgangsmåden til fremstilling af glasmaterialet ifølge krav 1, **kendetegnet ved, at** varmebehandlingsprocessen i trin 3 omfatter følgende trin: opbevaring af grundglaspladen i 2-6 timer ved en temperatur på 600-650 °C og derefter i 2-10 timer ved en temperatur på 690-770 °C.

5. Et glasdækselpladeprodukt, **kendetegnet ved, at** det er fremstillet ved at udføre skære- og poleringsprocesser på det glasmateriale, der er fremstillet ved fremgangsmåden i et hvilket som helst af kravene 1-4, og fremstille en dækselplade med en målt tykkelse og -størrelse.

DRAWINGS

Drawing

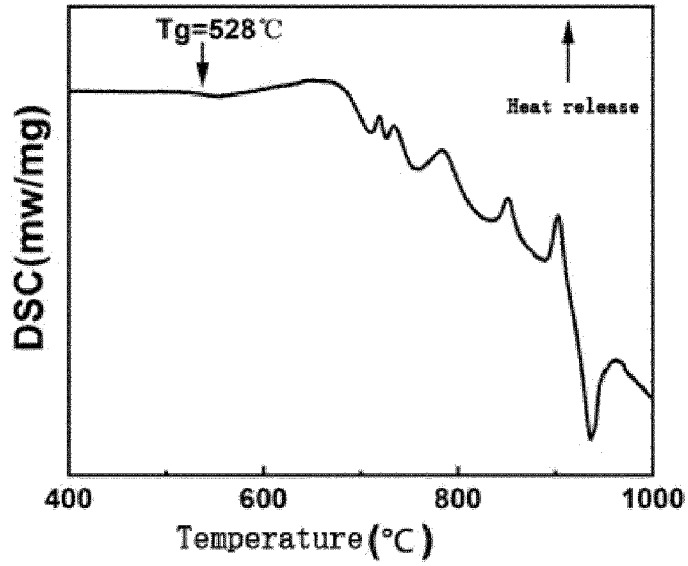


FIG 1

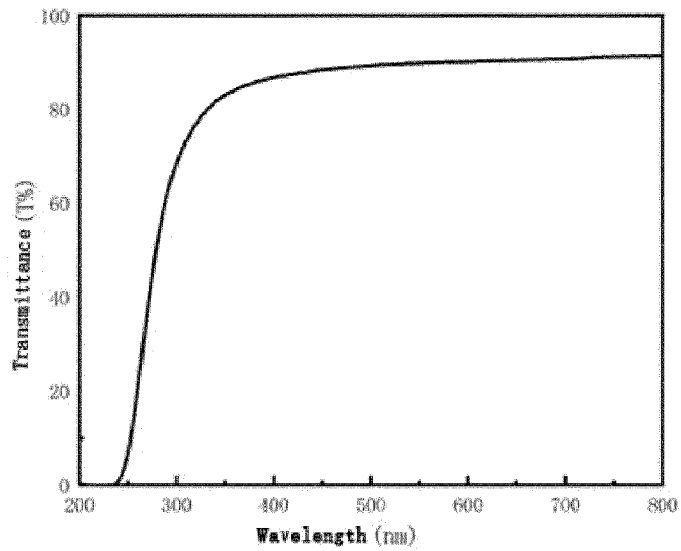


FIG 2

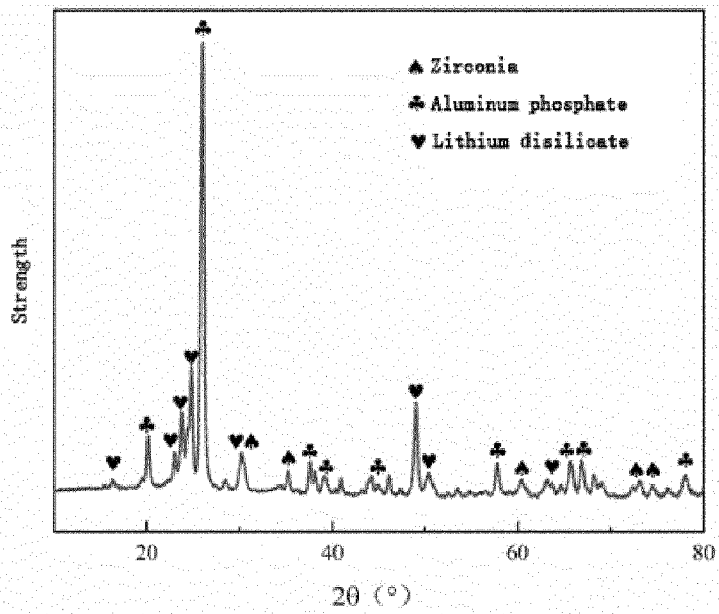


FIG 3

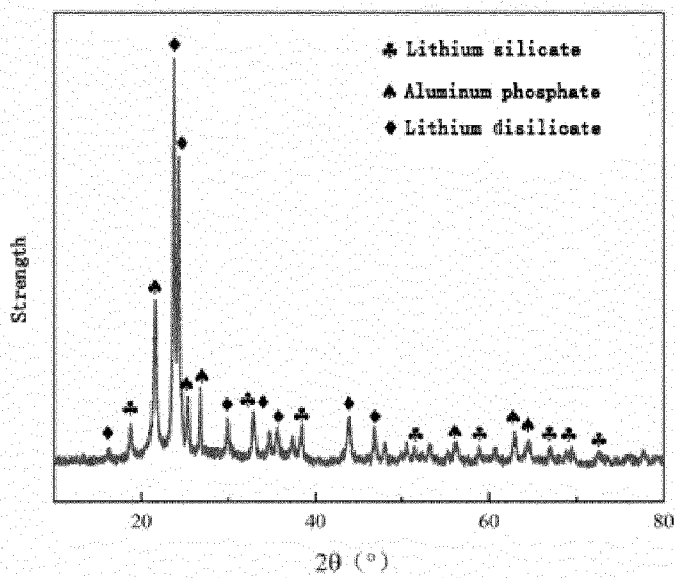


FIG 4

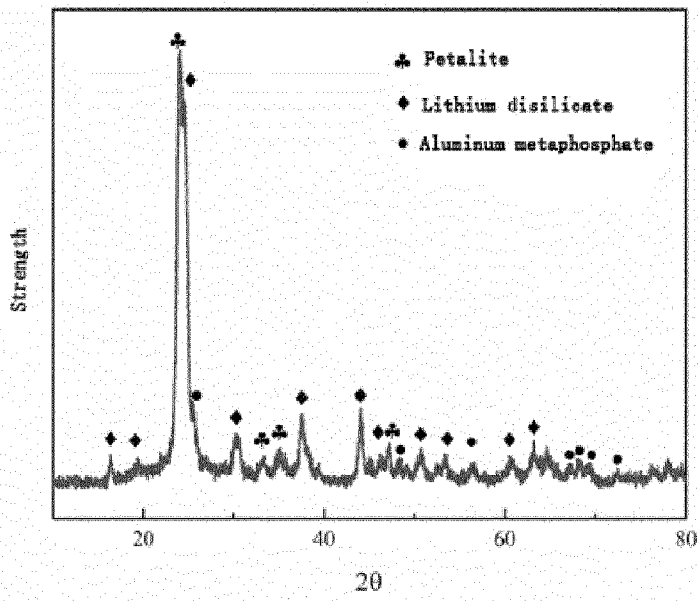


FIG 5

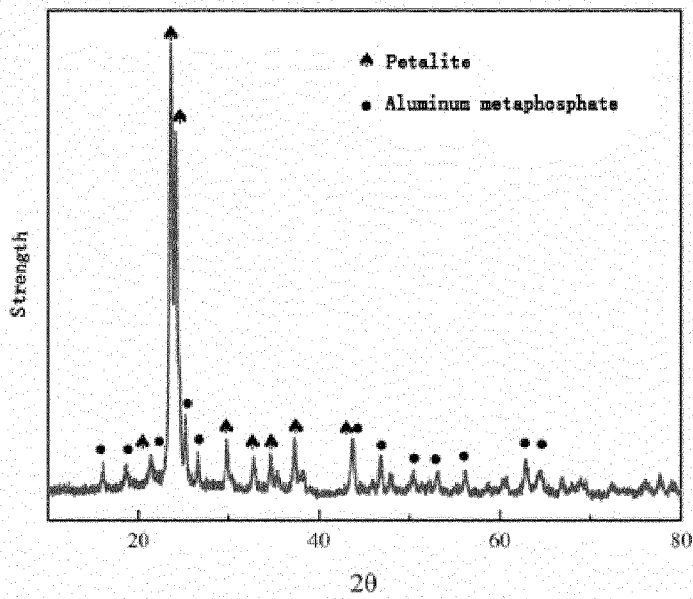


FIG 6

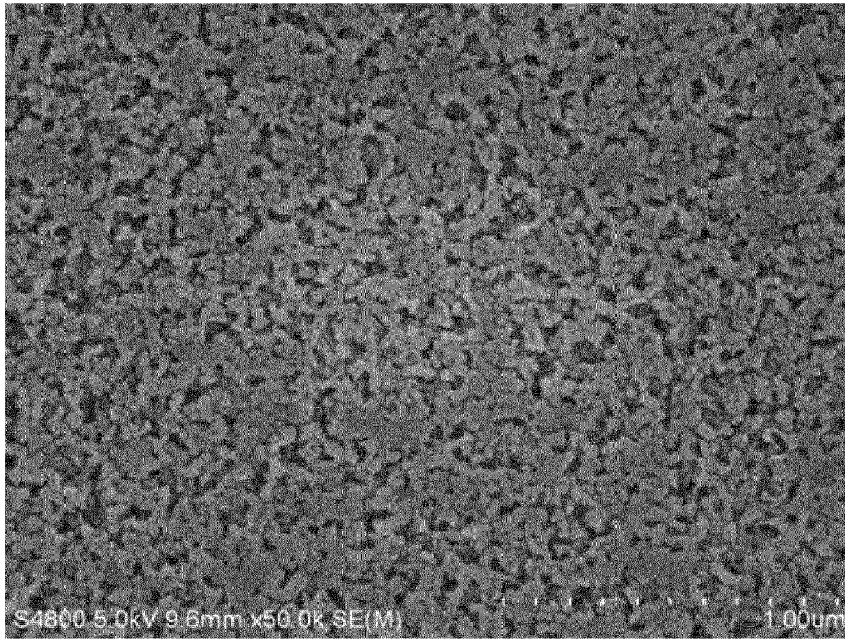


FIG 7

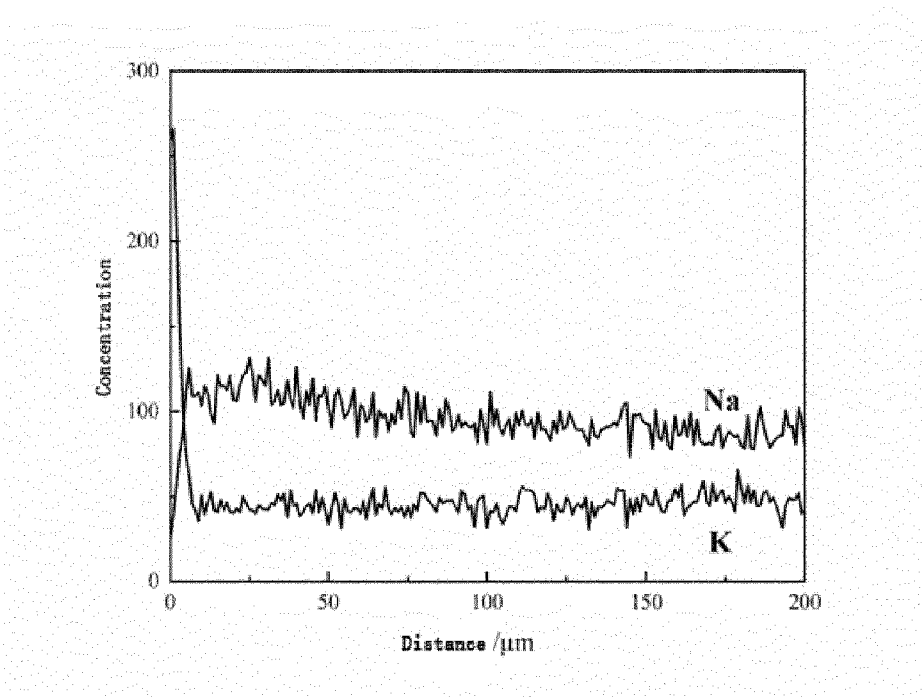


FIG 8

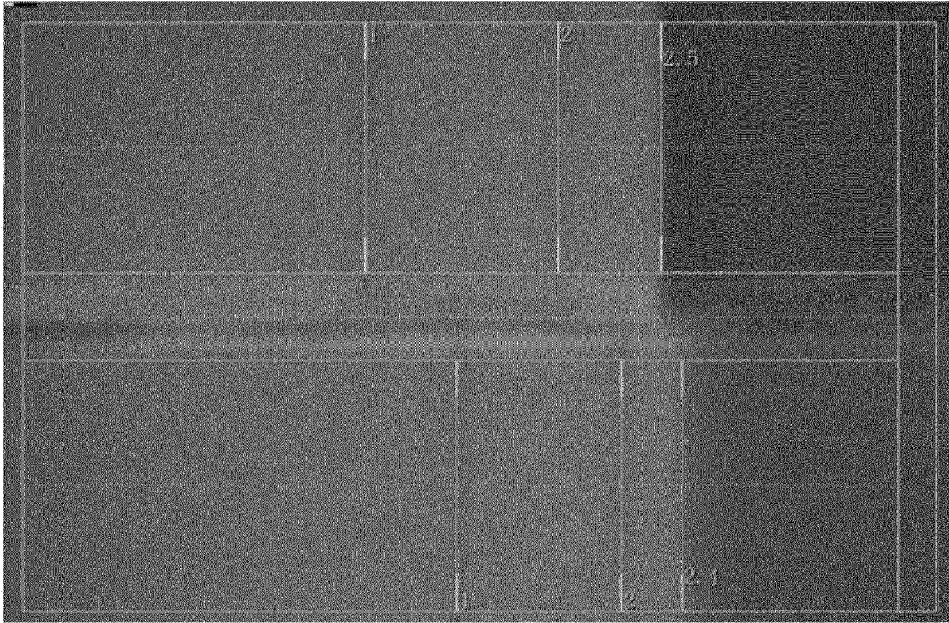


FIG 9

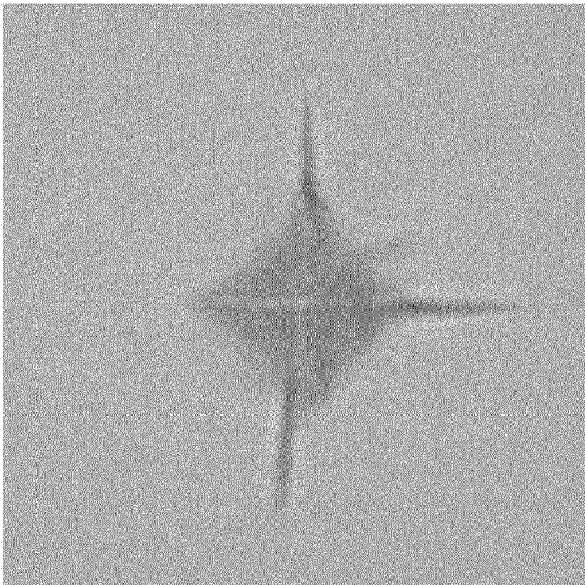


FIG 10

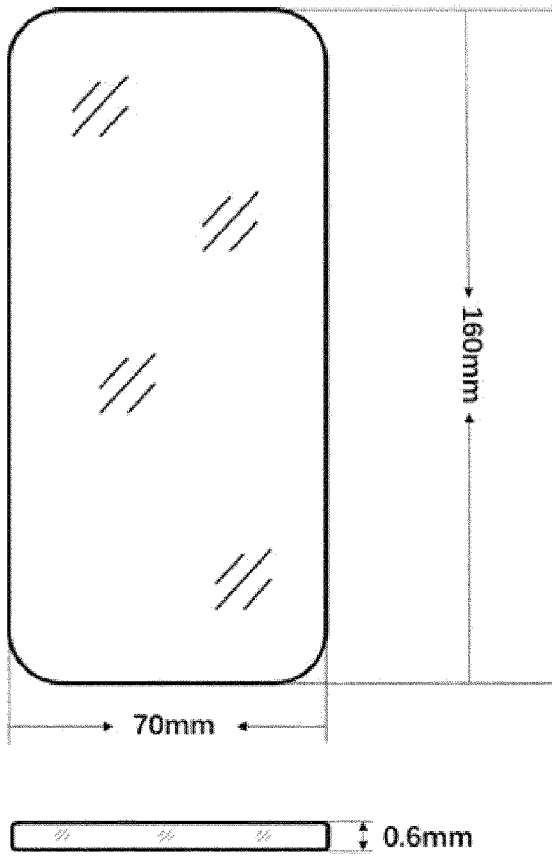


FIG 11