METHOD AND DEVICE FOR EXTRACTION OF LIQUIDS FROM A SOLID PARTICLE MATERIAL

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Abstract
A method, system, and device for separating oil from oil sands or oil shale is disclosed. The method includes heating the oil sands, spinning the heated oil sands, confining the sand particles mechanically, and recovering the oil substantially free of the sand. The method can be used without the addition of chemical extraction agents. The system includes a source of centrifugal force, a heat source, a separation device, and a recovery device. The separation device includes a method of confining the sands while allowing the oil to escape, such as through an aperture.
FIG. 4

Extraction % (based on 12% oil fraction) for 2 Samples Heated to 94°C vs. Spin Time at Maximum Speed (3300 rpm)
Fig. 5

- Extraction % (based on 12% oil fraction) for Samples Heated to 52C, 72C, and 94C vs. Spin Time at Maximum Speed (3300rpm)
Extraction % (based on 12% oil fraction) vs. Time for 1 Sample at 3300 rpm and 1 Sample at 2000 rpm, both heated to 94°C.

FIG. 6
FIG. 23
FIG. 35
FIG. 36
METHOD AND DEVICE FOR EXTRACTION OF LIQUIDS FROM A SOLID PARTICLE MATERIAL

RELATED APPLICATIONS


BACKGROUND

[0002] Given high oil prices and the finite amount of crude oil available, unconventional petroleum reserves in the form of, for example, oil sands and oil shale are becoming more attractive as an alternative source of hydrocarbons. Oil sands are found in over 60 countries in the world, including the United States. The main deposits occur in Alberta, Canada, and represent the second largest reserves of petroleum in the world, after those in Saudi Arabia.

BRIEF SUMMARY

[0003] This invention relates to a process for extracting liquids, such as bitumen or crude oil, from discrete solid particles, such as sand or shale. The invention is particularly applicable to oil sands and oil shale in which oil is present as a highly viscous liquid.

BRIEF DESCRIPTION OF THE DRAWINGS

[0004] The physical process for extracting liquid such as oil from the solid-liquid mixture such as oil sands or oil shale involves submitting the heated mixture to centrifugal forces to allow the liquid to mechanically separate from the solid particles and exit the device through small apertures.

[0005] FIG. 1 is a cross-sectional view of a first system.

[0006] FIG. 2 is a cross-sectional view of the first system unassembled.

[0007] FIG. 3 is an exploded detail of the first system.

[0008] FIG. 4 is a diagram illustrating the effect of spinning time.

[0009] FIG. 5 is a diagram illustrating the effect of temperature.

[0010] FIG. 6 is a diagram illustrating the effect of the spin rate.

[0011] FIG. 7 is a cross-sectional view of a second system.

[0012] FIG. 8 is a top view of the bottom portion of the second system.

[0013] FIG. 9 is a perspective view of the top and bottom portions of the second system.

[0014] FIG. 10 is a cross-sectional view of the second system in an open conformation.

[0015] FIG. 11 is a cross-sectional view of the second system in a closed conformation and surrounded by a liquid collector.

[0016] FIG. 12 is a cross-sectional view of the second system in an open conformation and surrounded by a cylindrical particle collector.

[0017] FIG. 13 is a cross-sectional view of the second system in open conformation with a solids-liquids mixture inside.

[0018] FIG. 14 is a cross-sectional view of a third system.

[0019] FIG. 15 is a perspective view of the third system.

[0020] FIG. 16 is a perspective view of the fourth system.

[0021] FIG. 17 is a perspective view of the fourth system with a top and a bottom.

[0022] FIG. 18 is a top view of the fourth system.

[0023] FIG. 19 is an exploded detail of the fourth system.

[0024] FIG. 20 is an exemplary top view of the spinning and cleaning process of the fourth system.

[0025] FIG. 21 is a perspective view of a fifth system.

[0026] FIG. 22 is a cross section view of the fifth system.

[0027] FIG. 23 is a cross-sectional view of an exemplary separation process in the fifth system.

[0028] FIG. 24 is a cross section view of the sixth system.

[0029] FIG. 25 is a cross-sectional view of the sixth system surrounded by a liquid collector.

[0030] FIG. 26 is a cross-sectional view of the sixth system in an open conformation.

[0031] FIG. 27 is a perspective view of the seventh system in an open conformation.

[0032] FIG. 28 is a cross-sectional view of the seventh system in a closed conformation.

[0033] FIG. 29 is a perspective view of a component of the seventh system.

[0034] FIG. 30 is a cross-sectional view of the seventh system in an open conformation.

[0035] FIG. 31 is a second cross-sectional view of the seventh system in an open conformation.

[0036] FIG. 32 is a partial cross-sectional view of the eighth system.

[0037] FIG. 33 is a first cross-sectional view of the ninth system.

[0038] FIG. 34 is a second cross-sectional perspective view of the ninth system.

[0039] FIG. 35 is a third cross-sectional view of the ninth system.

[0040] FIG. 36 is a fourth cross-sectional view of the ninth system.

[0041] FIG. 37 is a perspective view of the tenth system.

[0042] FIG. 38 is a cross-sectional view of the tenth system.

[0043] FIG. 39 is a perspective view of the eleventh system.

[0044] FIG. 40 is a first cross-sectional view of the eleventh system.

[0045] FIG. 41 is a second cross-sectional view of the twelfth system.

[0046] FIG. 42 is a cross-sectional view of the thirteenth system.

DETAILED DESCRIPTION

[0047] Oil sands (also referred to as tar sands) are found in over sixty countries in the world, including the United States. Oil sands consist mainly of bitumen, water, mineral particles, sand, and clay. Bitumen is a natural, tar-like mixture of hydrocarbons that exists as a solid at room temperature. In nature, bitumen has a density range of 8° to 12° API, and at room temperature its viscosity is greater than 50,000 centipoises.

[0048] The physical process disclosed for separating liquids from solids uses fewer natural resources to produce bitumen from oil sand than the conventional method of separation. The conventional method of separating bitumen from oil sand requires more than 1,000 cubic feet of natural gas to separate one barrel of bitumen from two tons of oil sand, according to the National Energy Board of Canada. However, the physical process disclosed for separating liquids from solids requires less than 190 cubic feet of natural gas and no fresh water or other solvents to produce one barrel of bitumen.
The physical process disclosed produces a clean effluent. The only ingredient in the produced effluent is sand, which almost all of the oil is removed. On a laboratory scale, approximately over 85% of the available oil is removed. The physical process disclosed is also effective on a laboratory scale. Approximately 90% of the available oil is removed in less than 15 minutes.

The physical process disclosed is a simple mechanized method. Using less than 25% of the energy required of the conventional hot-water process method to separate oil from oil sands, the disclosed physical process is environmentally conscious.

As an illustration, the energy needed to heat oil sand is calculated by multiplying the oil sand specific heat at constant pressure by the mass of the oil sand and the change in temperature. For example, the energy needed to heat two tons (2,000 kg) of oil sand with a specific heat at constant pressure of 1 kJ/kg-K from 0°C up to 100°C equals 200,000 KJ. The specific heat at constant pressure of Utah oil sand ranges from 0.67 kJ/kg-K to 1.57 kJ/kg-K in the temperature range of 100-350°C. Converted to the energy units of BTU based on 1.055 KJ per BTU, 200,000 KJ equals 189,574 BTU. Each cubic foot of natural gas contains 1,028 BTU of energy, as a result, 189,574 BTU equals 184 cubic feet of natural gas. Therefore, the physical process disclosed for separating liquids from solids may require less than 190 cubic feet of natural gas to separate one barrel of bitumen from two tons of oil sand, which is 80% less than the 1,000 cubic feet used in the conventional separation method.

Additionally, the negative impact on the environment from the physical process disclosed for separating liquids from solids may be less than the conventional separation method because the physical process disclosed does not require any water to separate bitumen from oil sand. Conversely, the conventional separation process requires up to 4 barrels of fresh water to produce one barrel of bitumen from two tons of oil sand. The spent water used in the conventional oil separation process is suspected to cause environmental, wildlife, and health problems. The spent water may contain chemicals used in the conventional separation process and may enter rivers and fresh ground water supplies after leaking from spent water retention ponds. Therefore, the physical process disclosed for separating liquids from solids may be less harmful to the environment than the conventional separation method.

A physical process for separating liquids from solids is disclosed. As a non-limiting example, this physical process may be used to separate liquids, such as oil, from solid particles, such as sand or shale. The process may involve at least the following steps in any order (a) applying heat to a mixture of solids and liquids; (b) rapidly spinning the mixture; and (c) confining the solid particles mechanically.

A first system includes a separation device 90 as shown in FIG. 1. The separation device 90 may be made up of one or more tubes such as test tubes. The separation device 90 may, for example, include a first tube 106 and a second tube 100. The tubes 106, 100 of this example are dimensioned such that the second tube 100 fits inside of the first tube 106, for example, in a nested configuration. The second tube 100 has an aperture 102 at one end. In this example, the aperture may have a diameter of approximately 0.40-1.50 mm, 0.45-1.35 mm, 0.80-1.50 mm, or more preferably 0.90-1.20 mm. However, the optimal aperture size may vary with other variables, such as the type of solid or liquid being separated or other considerations.

The separation device 90 may be dimensioned as described below and illustrated by FIG. 2. The dimensions are representative of this system but may be varied depending upon, for example the system, production needs, and type of solids and liquids being separated.

The first tube 106 of this example may be, for example but not limited to, a 15 ml centrifuge tube. The second tube 100 of this example may be, for example but not limited to, a 5 ml centrifuge tube. Again, recognized by those of ordinary skill in the art that dimensions, supply source, and specifications for the first tube 106 and the second tube 100 may be varied to suit the needs of a particular application.

The second tube 100 may have an aperture 102 at one end. The aperture may facilitate separation by retaining solids, such as sand or shale, within the second tube 100 while allowing liquids, such as oil, to escape. The aperture 102 may be added to a tube, for example, the second tube 100 using a tungsten probe. By way of example, to create an aperture, an area on the second tube 100 may be warmed and bored through with a super-heated tungsten probe. The tungsten probe may be a 1/16 inch tungsten probe which may be filed to a point. Other known methods may also be used to create an aperture 102.

The process for removing, for example, oil from sand, may proceed as follows. A solids-liquids mixture 104, for example oil shale or oil sands, may be heated to approximately 25°C-200°C, 50°C-175°C, 75°C-150°C, 95°C-125°C, and preferably approximately 92°C-110°C, and more preferably approximately 94°C. (e.g., in a water bath). The solids-liquids mixture 104 may be heated prior to loading into the separation device 90. Alternatively, the solids-liquids mixture may be heated in the separation device, or during spinning. Before or after heating, the solids-liquids mixture may be loaded into the second tube 100. In this example, the tube may be filled to approximately 3/5 of capacity; however, any amount of solids-liquids mixture 104 may be used. The second tube 100 may be placed inside the first tube 106, before or after filling, to create a separation device 90. The separation device 90 including the solids-liquids mixture 104 may then be placed into a centrifuge, such as an I.W. Scientific Ultra 8 Centrifuge. The separation process may be performed without the addition of chemicals.

An example of the physical principles of operation is shown in FIG. 3. The separation device 90 may be spun in a centrifuge or similar machine. The optimum range for the spin rate may be 500 rpm to 10,000 rpm. As a result of centrifugal force 204, the liquid 202 may exit the aperture 102 and may collect in the bottom of the first tube FIG. 1, 106, which may be the outer tube. The solid particles 206 may remain in the second tube FIG. 1, 100, which may be the inner tube. The particles 206 may be retained in the second tube 100 rather than escaping through the aperture 102 because, for example, the centrifugal force 204 causes them to jam up, leaving gaps 208 through which the liquid 202 may move toward the aperture 102 and escape. The optimum time range for spinning may be 15 seconds to 20 minutes.

The optimum aperture 102 size for extracting oil from Athabasca oil sands may be, for example, approximately 0.40-1.50 mm, 0.45-1.35 mm, 0.80-1.30 mm, or preferably approximately 0.85-1.10 mm. In the case of, for example, Athabasca oil sands, an aperture 102 larger than
approximately 1.5 mm would let the solid particles escape (e.g., absent the presence of supplementary retaining devices such as a screen). However, as recognized by those of skill in the art, the size of the aperture may be optimized to find an appropriate range for different combinations of solids and liquids, including oil sands from other regions, oil shale and including Athabasca oil sands that have different particle sizes.

The following example illustrates performance of the process in one system and also includes exemplary results. This example is merely illustrative of the effect on oil recovery from oil sands of different centrifuge speeds and temperatures. The example also illustrates oil extraction from oil sands without the addition of chemicals.

Athabasca oil sand was purchased from the Alberta Research Council. Materials accompanying the oil sand samples provided an estimated composition of 6-12 weight % bitumen, 5-20 weight % water and the balance sand. The bitumen content was not expressed with certainty, therefore a conservative estimate of 12% bitumen was used to calculate percent oil extracted, unless otherwise noted.

The oil sands were loaded into a separation device. The separation device was placed into a boiling water bath at approximately 94°C for approximately 5 minutes or such time as it takes for the temperature of the sand to reach approximately 94°C.

At a spin rate of 3300 rpm and at an initial temperature of 94°C, about 90% of the extractable liquid 202 in FIG. 3 was recovered in 10 minutes (under the conservative assumption the oil sands contained 12 weight % bitumen). The configuration of the centrifuge used in this experiment caused the oil sands sample to experience a g-force of about 900 gs. At lower temperatures, down to 52°C, longer times were needed to remove smaller portions of oil 202 (~64% at ~72°C and ~35% at 52°C, respectively) even at maximum rotation speeds (~3300 rpm). (All calculations assume that the oil sands contained 12 weight % bitumen.) See FIG. 5. The separation process was performed without the addition of chemicals.

The following examples illustrate the effect on recovery of various process variables.

### Example 1

**Effect of Spinning Time**

The following example is included to illustrate the effect of spinning time on recovery in one system. This example is merely illustrative.

In this example, the effect of spinning time was investigated. The example was performed in duplicate. For this exemplary experiment two devices 90 were weighed.

<table>
<thead>
<tr>
<th>Sample</th>
<th>Initial, empty w/oil sand</th>
<th>Spin 1 min</th>
<th>Spin 2 min</th>
<th>Spin 3 min</th>
</tr>
</thead>
<tbody>
<tr>
<td>sample 1</td>
<td>10.493</td>
<td>12.958</td>
<td>12.911</td>
<td>12.901</td>
</tr>
<tr>
<td>sample 2</td>
<td>15.649</td>
<td>15.791</td>
<td>15.835</td>
<td>15.850</td>
</tr>
<tr>
<td>inner tube</td>
<td>10.632</td>
<td>13.350</td>
<td>13.311</td>
<td>13.320</td>
</tr>
</tbody>
</table>

Each device 90 consisted of a first tube and a second tube. The second tube 100 was nested inside of the first tube 106 to form a separation device 90. The second tube 100 included an aperture 102.

Prior to spinning, the first tube 106 and the second tube 100 of each separation device 90 were weighed. Each device 90 was loaded with an approximately equal amount of solids-liquids mixture 104, which in this example was oil sand. The devices 90 were loaded by inserting the solids-liquids mixture 104, in this case oil sand, into the second tube 100 to a level of approximately 3/4 full. The second tube 100 was then inserted into the first tube 106 and the resulting separation device 90 was reweighed to determine sample size (i.e., the difference between the weight of the unloaded assembled separation device versus the weight of the loaded and assembled separation device 90). The weight of the bitumen present in each sample of oil sand was approximated by assuming that the samples contained 12 weight % bitumen.

Each loaded separation device 90 was then placed in a constant temperature bath at 94°C until the temperature in each stabilized at 94°C. After heating, each loaded separation device 90 was then placed in the centrifuge and spun for approximately 1 minute at about 3300 rpm.

After spinning, each loaded separation device 90 was disassembled and weighed. Each separation device 90 was disassembled by removing the second tube 100 from the first tube 106. The first tube 106 of each device was weighed to determine the amount of liquid 202, in this case oil, was deposited into the first tube 106 (as demonstrated by increased weight) by the spinning. The second tube 100 of each device was weighed to determine the amount of liquid 202 removed from the solids-liquids mixture 104 (as demonstrated by decreased weight) by the spinning.

After weighting, each separation device 90 was reassembled by inserting the second tube 100 into the first tube 106. Each loaded separation device 90 was then placed in a constant temperature bath at 94°C until the temperature in each stabilized at 94°C. After heating, each loaded separation device 90 was then placed in the centrifuge and spun for approximately 1 minute at about 3300 rpm. After spinning for 1 minute, each separation device 90 was again separated by removing the second tube 100 from the first tube 106. The first tube 106 and second tube 100 were weighed to determine the degree of separation after 2 minutes. This process was repeated for 3 more cycles. The degree of separation at 1, 2, 3, and 4 minutes is illustrated in the following tables and plotted into FIG. 4. Where the X-axis displays the total spin time and the Y-axis shows percent of the oil.

| Raw Data Summary |

<table>
<thead>
<tr>
<th>sample</th>
<th>sample 1 mass gain (g)</th>
<th>sample 2 mass gain (g)</th>
<th>tube 1 % mass gain*</th>
<th>tube 2 % mass gain*</th>
</tr>
</thead>
<tbody>
<tr>
<td>sample 1</td>
<td>0.142</td>
<td>0.186</td>
<td>45.3</td>
<td>53.5</td>
</tr>
<tr>
<td>sample 2</td>
<td>0.169</td>
<td>0.186</td>
<td>45.3</td>
<td>53.5</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>sample</th>
<th>sample 1 mass gain (g)</th>
<th>sample 2 mass gain (g)</th>
<th>tube 1 % mass gain*</th>
<th>tube 2 % mass gain*</th>
</tr>
</thead>
<tbody>
<tr>
<td>sample 1</td>
<td>0.201</td>
<td>0.198</td>
<td>64.1</td>
<td>56.4</td>
</tr>
</tbody>
</table>
### Sample 1 Summary, aperture size 0.79 mm

<table>
<thead>
<tr>
<th>Time (min)</th>
<th>Oil Sand (g)</th>
<th>Oil (g)</th>
<th>% Extracted</th>
</tr>
</thead>
<tbody>
<tr>
<td>Start</td>
<td>2.614</td>
<td>0.314</td>
<td></td>
</tr>
<tr>
<td>1 min</td>
<td>(0.149)</td>
<td>0.146</td>
<td>46%</td>
</tr>
<tr>
<td>2 min</td>
<td>(0.196)</td>
<td>0.191</td>
<td>61%</td>
</tr>
<tr>
<td>3 min</td>
<td>(0.206)</td>
<td>0.204</td>
<td>65%</td>
</tr>
<tr>
<td>4 min</td>
<td>(0.218)</td>
<td>0.211</td>
<td>67%</td>
</tr>
</tbody>
</table>

### Sample 2 Summary, aperture size 0.93 mm

<table>
<thead>
<tr>
<th>Time (min)</th>
<th>Oil Sand (g)</th>
<th>Oil (g)</th>
<th>% Extracted</th>
</tr>
</thead>
<tbody>
<tr>
<td>Start</td>
<td>2.896</td>
<td>0.348</td>
<td></td>
</tr>
<tr>
<td>1 min</td>
<td>(0.176)</td>
<td>0.173</td>
<td>50%</td>
</tr>
<tr>
<td>2 min</td>
<td>(0.195)</td>
<td>0.191</td>
<td>55%</td>
</tr>
<tr>
<td>3 min</td>
<td>(0.206)</td>
<td>0.201</td>
<td>58%</td>
</tr>
<tr>
<td>4 min</td>
<td>(0.213)</td>
<td>0.207</td>
<td>59%</td>
</tr>
</tbody>
</table>

All data is calculated based on an assumed, conservative value of 12 weight % oil per oil sand sample. Actual percent extraction is likely higher.

The combination of heating, spinning and an appropriate aperture size is highly effective at separating oil from oil sands, even in the absence of chemical extraction agents.

As illustrated in FIG. 4, when the liquid is oil and the solid-liquid mixture is oil sands, the oil is removed rather quickly and in a large proportion to the amount available at 94°C and 3300 rpm. These results are expected to vary, depending upon the nature of the device used and the starting materials.

### Example 2

**Effect of Temperature**

The following example is included to illustrate the effect of temperature on recovery. This example is merely illustrative.

In this example, the effect of temperature on recovery was investigated. The example was performed at three exemplary temperatures, 94°C, 72°C, and 52°C. For this exemplary experiment three separation devices were prepared, each of which consisted of a first tube 106 and a second tube 100. The second tube 100 was nested inside of the first tube 106 to form a separation device 90. The second tube 106 included an aperture 102 as described above. Each separation device 90 was weighed prior to loading. The weight amount of the bitumen present in each sample of oil sand was approximated by assuming that the samples contained 12 weight % bitumen.

After weighing, each separation device 90 was loaded with an approximately equal amount of solids-liquids mixture 104, which in this example was oil sand. The devices 90 were loaded by inserting the solids-liquids mixture 104 in this case oil sand, into the second tube 100 to a level of approximately 1/3 full. The second tube 100 was then nested into the first tube 106 and the resulting separation device 90 was reweighed to determine sample size.

Each loaded separation device 90 was then placed in a constant temperature bath. In this example, each of the three separation devices 90 was warmed to a different temperature. One separation device 90, represented in FIG. 5 as a triangle, was warmed in a constant temperature bath at approximately 94°C. Until the temperature in the separation device 90 stabilized at approximately 94°C. A second separation device 90, represented in FIG. 5 as a circle, was warmed in a constant temperature bath at approximately 72°C. Until the temperature in the separation device 90 stabilized at approximately 72°C. A third separation device 90, represented in FIG. 5 as a square, was warmed in a constant temperature bath at approximately 52°C. Until the temperature in the separation device 90 stabilized at approximately 52°C.

After heating, each loaded separation device 90 was then placed in the centrifuge and spun for approximately 1 minute at about 3300 rpm. After spinning for one minute, each loaded separation device 90 was removed from the centrifuge. The separation device 90 was disassembled by removing the second tube 100 from the first tube 106. The first tube 106 of each separation device 90 was weighed to determine the amount of liquid 202 in this case oil, deposited into the first tube 106 (as demonstrated by increased weight) by the spinning. The second tube 100 of each separation device 90 was weighed to determine the amount of liquid 202 removed from the solids-liquids mixture 104 (as demonstrated by decreased weight) by the spinning.

After weighing, each separation device 90 was reassembled by inserting the second tube 100 into the first tube 106. Each loaded separation device 90, represented by a triangle, circle, and square, was then placed back into a constant temperature bath at approximately 94°C, 72°C, or 52°C, respectively until the temperature in each stabilized at approximately 94°C, 72°C, or 52°C, respectively. After heating, each loaded separation device 90 was then placed in the centrifuge and spun for approximately 5 minutes at about 3300 rpm. After spinning for approximately 5 minutes, each separation device 90 was again separated by removing the
second tube 100 from the first tube 106. The first tube 106 and second tube 100 were weighed to determine the degree of separation after 5 minutes.

[0083] After weighing, each separation device 90 was reassembled by inserting the second tube 100 into the first tube 106. Each loaded separation device 90, represented by a triangle, circle, and square, was then placed back into a constant temperature bath at approximately 94°C, 72°C, or 52°C, respectively until the temperature in each stabilized at approximately 94°C, 72°C, or 52°C, respectively. After heating, each loaded separation device 90 was then placed in the centrifuge and spun for approximately 10 minutes at about 3300 rpm. After spinning for 10 minutes, each separation device 90 was again separated by removing the second tube 100 from the first tube 106. The first tube 106 and second tube 100 were weighed to determine the degree of separation after 10 minutes.

[0084] The degree of separation for each separation device 90 at three temperatures 94°C, 72°C, or 52°C was plotted in FIG. 5. The degree of separation at each temperature and at each of 1, 5, and 16 minutes is plotted.

[0085] As illustrated in FIG. 5, even in the absence of chemical agents, the extraction percentage of oil from oil sands on laboratory scale at approximately 94°C, and approximately 3300 rpm levels off at about 10 minutes spinning time. These results are expected to vary depending upon the nature of the device and the starting materials.

Example 3
Effect of Spin Rate on Recovery

[0086] The following example is included to illustrate the effect of spin rate on recovery in a laboratory scale system. This example is merely illustrative and not meant to be limiting.

[0087] In this example, the effect of spin rate on recovery was investigated. The example was performed at two exemplary spin rates, 3300 rpm and 2000 rpm. All other variables were identical between the two samples. For this exemplary experiment two separation devices 90 were prepared, each of which consisted of a first tube 106 and a second tube 100. The second tube 100 was nested inside of the first tube 106 to form a separation device 90. The second tube 100 included an aperture 102. Each separation device 90 was weighed prior to loading.

[0088] After weighing, each device 90 was loaded with an approximately equal amount of solids-liquids mixture 104, which in this example was oil sand. The separation devices 90 were loaded by inserting the solids-liquids mixture 104, in this case oil sand, into the second tube 100 to a level of approximately ⅔ full. The second tube 100 was then nested into the first tube 106 and the resulting separation device 90 was reweighed to determine sample size.

[0089] Each loaded separation device 90 was then placed in a constant temperature bath. In this example, each separation device 90, was warmed in a constant temperature bath at 94°C until the temperature in the separation device 90 stabilized at 94°C.

[0090] After heating, each loaded separation device 90 was then placed in the centrifuge and spun for approximately 1 minute. One separation device 90 represented in FIG. 6 by the letter B, was spun at about 3300 rpm. A second separation device 90 represented in FIG. 6 by the letter E, was spun at about 2000 rpm. After spinning each separation device 90 at its respective speeds for one minute, each loaded separation device 90 was removed from the centrifuge. Each separation device 90 was disassembled by removing the second tube 100 from the first tube 106. The first tube 106 of each device was weighed to determine the amount of liquid 202, in this case oil, deposited into the first tube 106 (as demonstrated by increased weight) by the spinning. The second tube 100 of each device was weighed to determine the amount of liquid 202 removed from the solids-liquids mixture 104 (as demonstrated by decreased weight) by the spinning. The weight amount of bitumen present in each sample of oil sand was approximated by assuming that the samples contained 12 weight % bitumen.

[0091] After weighing, each separation device 90 was reassembled by inserting the second tube 100 into the first tube 106. Each loaded separation device 90, represented by a B or an E, was then placed back into a constant temperature bath at approximately 94°C until the temperature in each stabilized at approximately 94°C. After heating, each loaded separation device 90, represented by a B or an E, was then placed in the centrifuge and spun for approximately 1 minute at about 3300 rpm and 2000 rpm, respectively. After spinning for 1 minute, each separation device 90 was again separated by removing the second tube 100 from the first tube 106. The first tube 106 and second tube 100 were weighed to determine the degree of separation after 1 minute at about 3300 rpm and 2000 rpm, respectively.

[0092] After weighing, each separation device 90 was reassembled by inserting the second tube 100 into the first tube 106. The cycle of heating, spinning, and weighing was repeated and results were plotted on FIG. 6 for each device 90 at 1, 2, 3, 4, and 5 minutes. FIG. 6 illustrates that percent extraction begins to converge at longer spin times.

[0093] The underlying data is included in the charts below:

<table>
<thead>
<tr>
<th>Samples B &amp; E</th>
<th>inner tube Sample B (g)</th>
<th>outer tube Sample B (g)</th>
<th>inner tube Sample E (g)</th>
<th>outer tube Sample E (g)</th>
<th>Sample B mass gain (g)</th>
<th>Sample E mass gain (g)</th>
<th>Sample B % gain*</th>
<th>Sample E % gain*</th>
</tr>
</thead>
<tbody>
<tr>
<td>initial, empty w/oil sand</td>
<td>10.542</td>
<td>15.384</td>
<td>10.389</td>
<td>15.253</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>oild sand spin 1 min</td>
<td>13.512</td>
<td>3.034</td>
<td>13.405</td>
<td>3.046</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>oild sand spin 2 min</td>
<td>13.429</td>
<td>15.333</td>
<td>13.335</td>
<td>15.35</td>
<td>0.149</td>
<td>0.097</td>
<td>47.5</td>
<td>27.9</td>
</tr>
<tr>
<td>Samples</td>
<td>inner tube Sample B (g)</td>
<td>outer tube Sample B (g)</td>
<td>inner tube Sample E (g)</td>
<td>outer tube Sample E (g)</td>
<td>Sample B mass gain (g)</td>
<td>Sample E mass gain (g)</td>
<td>Sample B % gain*</td>
<td>Sample E % gain*</td>
</tr>
<tr>
<td>---------</td>
<td>-------------------------</td>
<td>-------------------------</td>
<td>-------------------------</td>
<td>-------------------------</td>
<td>-----------------------</td>
<td>-----------------------</td>
<td>------------------</td>
<td>------------------</td>
</tr>
<tr>
<td>spin 3 min</td>
<td>13.382</td>
<td>15.577</td>
<td>13.282</td>
<td>15.398</td>
<td>0.193</td>
<td>0.145</td>
<td>61.5</td>
<td>41.7</td>
</tr>
<tr>
<td>spin 4 min</td>
<td>13.348</td>
<td>15.609</td>
<td>13.271</td>
<td>15.408</td>
<td>0.225</td>
<td>0.155</td>
<td>71.7</td>
<td>44.6</td>
</tr>
<tr>
<td>spin 5 min</td>
<td>13.338</td>
<td>15.621</td>
<td>13.255</td>
<td>15.421</td>
<td>0.237</td>
<td>0.168</td>
<td>75.6</td>
<td>48.3</td>
</tr>
<tr>
<td>hole size (mm)</td>
<td>tube 5</td>
<td>0.9906</td>
<td>tube 6</td>
<td>0.889</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

*percent gains based on oil fraction of 12%

### Summary Sample B

**Hole size 0.99 mm**

<table>
<thead>
<tr>
<th>Start</th>
<th>Oil Sand (g)</th>
<th>Oil (g)</th>
<th>% Extracted</th>
</tr>
</thead>
<tbody>
<tr>
<td>3.034</td>
<td>0.36</td>
<td>18%</td>
<td></td>
</tr>
<tr>
<td>1 min (0.064)</td>
<td>0.066</td>
<td>18%</td>
<td></td>
</tr>
<tr>
<td>2 min (0.147)</td>
<td>0.148</td>
<td>41%</td>
<td></td>
</tr>
<tr>
<td>3 min (0.194)</td>
<td>0.194</td>
<td>54%</td>
<td></td>
</tr>
<tr>
<td>4 min (0.228)</td>
<td>0.227</td>
<td>63%</td>
<td></td>
</tr>
<tr>
<td>5 min (0.237)</td>
<td>0.238</td>
<td>66%</td>
<td></td>
</tr>
</tbody>
</table>

### Summary Sample E

**Hole size 0.89 mm**

<table>
<thead>
<tr>
<th>Start</th>
<th>Oil Sand (g)</th>
<th>Oil (g)</th>
<th>% Extracted</th>
</tr>
</thead>
<tbody>
<tr>
<td>3.046</td>
<td>0.37</td>
<td>7%</td>
<td></td>
</tr>
<tr>
<td>1 min (0.030)</td>
<td>0.027</td>
<td>7%</td>
<td></td>
</tr>
<tr>
<td>2 min (0.097)</td>
<td>0.099</td>
<td>27%</td>
<td></td>
</tr>
<tr>
<td>3 min (0.151)</td>
<td>0.149</td>
<td>40%</td>
<td></td>
</tr>
<tr>
<td>4 min (0.164)</td>
<td>0.160</td>
<td>43%</td>
<td></td>
</tr>
<tr>
<td>5 min (0.180)</td>
<td>0.174</td>
<td>47%</td>
<td></td>
</tr>
</tbody>
</table>

For another example, the following calculations may be helpful in the evaluation and description of the spin rate.

\[
a_c = r w^2 \\
g_c = \frac{g_r}{g_o} \\
g_c = \frac{r^2}{g_o}
\]

\[
a_c = \text{centripetal acceleration} \ (\text{m/s}^2) \\
r = \text{radius} \ (\text{m}) \\
w = \text{angular velocity} \ (\text{rpm})
\]

\[g_r = \text{gravitational acceleration at Earth's surface} \ (9.8 \text{ m/s}^2)\]

\[g_o = \text{G force} \ (g)\]

FIGS. 7-13 illustrate a second system 300 of a separation device. The second system may have a clam shell-like formation which may further have a first portion 302 and a second portion 304. The first portion 302 and the second portion 304, depending on the orientation of the device, may be the top and the bottom of the separation device 300. In FIG. 4, the first portion 302 and the second portion 304 of the second system fit together with the aid of, for example, an aligning pivot 305. The first portion 304 may have cavities 306, wherein each cavity 306 may form an aperture 308 where the first portion 302 and second portion 304 of the second system come together.

FIG. 8 illustrates how the cavities 306 may align radially. For example, the cavities 306 may be roughly semi conical with an opening that is wider toward the center 402 of the second portion 304 of the second system 300 and narrows as it reaches the perimeter 404. While the cavities 306 are illustrated as semi conical in FIG. 9, other shapes may be used.

The second system 300 may also include a liquid collector 706, as shown in FIG. 11, which may be cylindrical, or any other shape. For example, the liquid collector may or may not approximate the shape of the second system separation device 300. The liquid collector 706 may include a gutter 707 which may collect and funnel the liquid to a collection reservoir. The gutter 707 may be located on the lower edge of the liquid collector, or may be located in any other location. The liquid collector 706 may be arranged with the second system separation device 300 such that the second system separation device 300 may be raised and lowered into position with the liquid collector 706 as the separation process proceeds.

FIGS. 10-13 illustrate how the process for extracting liquids from solid particles might be adapted for the second system 300 separation device described above. The solids-liquids mixture 602 may be placed inside the cavities 306 in the second system 300. In FIG. 10 the solids-liquids mixture 602 may be heated before loading, during loading, or after loading into the device 300. The second system 300 may be lowered into a liquid collector 706 and may be spun as shown in FIG. 11. Spinning may cause the liquid 702 to separate from the solid particles 704. The liquid 702 may exit apertures 308, and may accumulate, for example, on the liquid collector 706, and/or in a gutter 707. The solid particles 704 may remain inside the closed second system 300.
After separation has been accomplished, the liquid collector 706 may be raised, and the second system 300 may be opened as shown in FIG. 12. The first portion 302 and second portion 304 may be spun such that the solid particles are spun out of the cavities 306. A solid particles collector 802 may be used to catch the solid particles 704.

The second system 300 may then be reused. A new load of heated or unheated solids-liquids mixture 602 may be inserted into the second system 300 and the liquid collector 706 may replaced into a position that will allow it to capture extracted liquids. The second system 300 may be closed and spun, as shown in FIG. 13, continuing the cycle. Alternatively, the cycle may terminate after one use. The optimal aperture 308 size for removing oil from Athabasca oil sands is approximately 0.40-1.50 mm, 0.45-1.35 mm, 0.80-1.30 mm, but more preferably 0.90-1.20 mm. However, other sizes may be used.

FIG. 14 is a cross-sectional view of a third system, which may have a cyclone formation 1010. The third system 1010 may be approximately conical in shape and may have baffles 1020 located along the interior. The baffles 1020 may be engaged in a screw-thread-like fashion along the interior of the third system 1010. The walls 1018 of the third system 1010 may include small apertures or capillaries 1022. An exploded view example of a wall 1018 including capillaries 1022 is illustrated in FIG. 14a. The third system 1010 may further include a central shaft 1011 which may be supported by a bearing 1012 and a feed tube 1016. The third system 1010 may also include a liquid collector 1026 which may be cylindrical or any other shape.

FIGS. 13-15 illustrate how the process for extracting liquids from solid particles might be adapted for the third system 1010 described above. The solids-liquids mixture 602, for example, oil sands, may be heated prior to loading or may be heated during loading or, alternatively, in the third system 1010. For example, the solids-liquids mixture 602 may be heated in the feed tube, in the cyclone, or in a retaining tank attached to the feed tube, and etc.; alternatively, it may be heated prior to being loaded into the feed tube.

The heated or unheated solids-liquids mixture 602 may be loaded into the third system 1010 by a feed tube 1016. The feed tube 1016 may be centrally located. A coaxial piston 1014 may push an amount of a heated solids-liquids mixture 602 down a central feed tube 1016 and out the bottom of the central feed tube 1016 into the centrifuge wall 1018, rotating co-axially as shown in FIG. 15. The heated solids-liquids mixture 602 may be centrifugally forced outward and upward along the baffles 1020. The liquid 702 may escape through the small apertures 1022, which may have a diameter of approximately 0.40-1.50 mm, 0.45-1.35 mm, 0.80-1.30 mm or more preferably 0.90-1.20 mm. Solid particles 704 may be centrifugally pushed upward and eventually go over the top 1024 of the third system 1010 where it may be collected and recycled, disposed of or otherwise. The liquid 702 that is extracted may be collected by the oil collector 1026, for example, by accumulating at the bottom 1028. This may be a continuous process by which the feed tube 1016 continually feeds solids-liquids mixture 602 into the third system 1010 to replace the liquid and solids that are removed.

FIG. 16 shows a fourth system which may be formed of rotating planes. The fourth system may have a chamber 1202. This device may be self-cleaning. As shown in FIG. 17, the rotating planes system may have a top plate 1205 and a bottom plate 1207, which may be coaxially mounted with a main shaft 1204 so that the top plate 1205 can be raised and the bottom plate 1207 can be lowered. The chamber may be formed of multiple chamber walls 1206. The chamber walls may have apertures or capillaries 1402 through which liquid may be extracted from the liquids-solid mixture. The chamber 1202 can take many shapes depending on the number of walls 1206, such as a hexagonal shape as shown in FIGS. 16-20. Each of the walls 1206 may be centrally pivoted 1208. The rotating planes separator 1202 may have at least two configurations, for example, a closed configuration (see, e.g., FIGS. 16, 17, 20, 20c, 20e) and an open configuration (see, e.g., FIGS. 20b, 20d). In the closed configuration, the walls 1206 may be sealed by outer 1304 and inner 1306 splines as shown in FIG. 19. The apertures 1402 in the chamber walls 1206 may have a diameter of approximately 0.40-1.50 mm, 0.45-1.35 mm, 0.80-1.30 mm, or more preferably 0.90-1.20 mm. In the open configuration, the walls 1206 may be rotated on their pivot point such that they are no longer in contact. (See, e.g., FIGS. 20b, 20d).

In operation, heated solids-liquids mixture 602 may be placed in the chamber and the chamber may be spun, as shown in the top view in FIG. 20. The liquid 702 separates from the solid particles 704 and may be collected by a liquid collector 1504 surrounding the chamber. The liquid collector 1504 may be, for example, cylindrical or may otherwise approximate the shape of the fourth system 1202. Alternatively, the liquid collector 1504 may be of any other shape or format. When separation has been completed and rotation has stopped, the bottom plate may be lowered. The top plate may be raised and the fourth system 1504 may be raised even more, so that its bottom is above the top of the chamber walls 1206, which are rotated as shown in the second step in FIG. 20b.

Next, the chamber walls 1206 may be locked by the splines at for example 180° so that the apertures face toward the center of the chamber. The separation device 1202 may be spun to cleanse the remaining solid particles 704. The solid particles 704 removed from the chamber may be caught by a solid-particle collector 1506 as shown in the third step in FIG. 20c.

After cleaning, the separator 1202 may be stopped; the solid-particle collector 1506 may be lowered away from the separator 1202. The separator may be returned to a closed position by rotating the walls 1206 180° as shown in the fourth step in FIG. 20d. The bottom plate may rise to complete the closed configuration. At that point, more solids-liquids mixture 602 may be placed inside the chamber, and the top may be lowered and the liquid collector 1504 raised into configuration for the next round of processing.

FIG. 21 shows a fifth system 1600 which may be a double piston type of a separator. The fifth system 1600 may have a rotating main shaft 1602. The rotating main shaft 1602 may further have an attached top piston 1604 and a bottom piston 1606. The fifth system 1600 may also include a filtering portion 1607 which may have a top band 1608, a bottom band 1610 and a screen 1612.

The screen 1612 may be made of any material and may be of sufficient strength to withstand centrifugal force and retain the solid particles. The screen may be supported by bands 1608, 1609 and 1610 as illustrated in FIG. 21. The screen 1612 may have openings or apertures, which may be dimensioned to retain the solid particles 704 and let the liquid 702 through, as shown in FIG. 21. For separation of oil from Athabasca oil sands, the aperture may have a diameter of...
approximately 0.40-1.50 mm, 0.45-1.35 mm, 0.80-1.30 mm, or more preferably 0.90-1.20 mm. As stated above, the aperture size may vary depending on the properties of the liquid-solid material and the efficiency of the separation may vary as a function of aperture size.

[0117] The attached top piston 1604 and bottom piston 1606 may be separated by a distance such that, in the closed position, the top piston 1604 is even with the top band 1608 of the filtering portion 1607, and the bottom piston 1606 is even with the bottom band 1610 of the filtering portion 1607.

[0118] In operation, the top 1604 and bottom 1606 pistons may be raised enough to introduce the solids-liquids mixture 602 as shown in the first step in FIG. 23. The pistons may be lowered and aligned with the filtering portion 1607. The apparatus may be spun, as shown in the second step 1802 in FIG. 23. Heat may be applied to the mixture prior to loading or the apparatus may be heated before or during spinning.

[0119] During spinning the solid particles 704 may be restrained by the screen 1612; the liquid 702 may pass through the screen 1612 and may be captured by the liquid collector 1804.

[0120] After the spinning is completed and extraction has concluded, the apparatus may be cleaned as follows. The pistons may be lowered until the bottom edge of the top of the filter 1604 is even with the bottom edge of top band 1610, as shown in the third step in FIG. 23. The solids particles may be removed from the piston by spinning such that the solid particles 704 leave the filter system 1600 and are collected by a solid-particle collector 1806.

[0121] After cleaning, the process may be repeated. For example, a new batch of heated or unheated solids-liquids mixture 602 may be inserted into the double piston system, as shown in the fourth step in FIG. 23.

[0122] While various systems of the invention have been described, it will be apparent to those of ordinary skill in the art that many more systems and implementations are possible that are within the scope of the invention.

[0123] FIG. 23 shows a cross sectional view of a sixth system 2100 which may be a centrifugal type of separator. The sixth system 2100 may have a rotor 2104. The rotor 2104 may spin a tube 2102. The sixth system 2100 may include multiple tubes 2102 depending on the size of the tube 2102 and the rotor 2104. The tube 2102 may include multiple parts. For example, the tube 2102 may have a first part 2118 and a second part 2118. The multiple parts may be connected, such as by a hinge 2114 or otherwise. When the first part 2116 and the second part 2118 are in contact, they may form a tube 2102. The tube 2102 may include an aperture 2106 at one end. The aperture 2106 may facilitate separation of liquids, such as oil or water, from solids, such as sand or shale, by retaining solids within the tube 2102. The sixth system 2100 may also include an extractor 2108. As shown in FIG. 26, the extractor 2108 may remove the tube 2102 from the rotor 2104, may split the tube 2102 into its first part 2116 and second part 2118, and may spin the tube 2102 to remove the solid particles.

[0124] The sixth system 2100 may include a liquid collector 2202, as shown in FIG. 25, which may be any shape capable of containing the liquid, such as a cylinder, rectangle, or hexagon.

[0125] The process for extracting liquids from solid particles may be adapted for the sixth system 2100, described above, by placing a solids-liquids mixture in the tube 2102, which may be placed in the rotor 2104. The solids-liquids mixture may be heated before, during, or after placement in the tube 2102. The solids-liquids mixture, for example oil shale or oil sands, may be heated to approximately 25° C.-200° C., 50° C.-175° C., 75° C.-150° C., 95° C.-125° C., and preferably approximately 92° C.-110° C. and more preferably approximately 94° C. (e.g., in a water bath). The tube 2102 may be inserted into the rotor 2104 and spin perpendicular to the long axis of the tube 2102. The tube 2102 may be spun to approximately 500 rpm to 10,000 rpm. Spinning may cause the liquid to separate from the solid particles. The tube 2102 may be spun for approximately 15 seconds to 20 minutes. The liquid may exit the aperture 2106 and may accumulate, for example, on the liquid collector 2202. The optimum aperture 2106 size for extracting oil from Athabasca oil sands may be, for example, approximately 0.40-1.50 mm, 0.45-1.35 mm, 0.80-1.30 mm, or preferably approximately 0.85-1.10 mm. Once the liquid has left the tube 2102, the second part of the rotor 2504 may
be moved to allow the tube 2402 to pivot along the pivot point 2410. If the tube 2410 is spun, the remaining solid particles may exit the open end 2502 of the tube 2402, as shown in FIG. 31. The collector 2702 may be changed to collect the solid particles. The seventh system 2400 may then be reused with a new solids-liquids mixture.

[0129] FIG. 32 shows an eighth system 2900, which may be a centrifugal type of separator. The eight system 2900 may include a rotor 2904. The rotor 2904 may spin a tube 2902. The eighth system 2900 may include multiple tubes 2902 depending on the size of the tube 2902 and the rotor 2904. The tube 2902 may be open on one end 2910 and may include a smaller aperture 2906 at the other end. The aperture 2906 may facilitate separation of liquids, such as oil or water, from solids, such as sand or shale, by retaining solids within the tube 2902. The tube 2902 may include a lockable pivot point 2908, such as a geared axle, along the length of the tube that may be perpendicular to the tube length.

[0130] The eight system 2900 may include a liquid collector 2912, as shown in FIG. 32, which may be any shape capable of containing the liquid, such as a cylinder, rectangle, or hexagon.

[0131] The process for extracting liquids from solid particles may be adapted for the eighth system 2900, described above, by placing a solids-liquids mixture in the tube 2902, which may be positioned within the rotor 2904 and secured in place by the lockable pivot point 2908. The solids-liquids mixture may be heated before, during, or after placement in the tube 2902. The solids-liquids mixture, for example oil shale or oil sands, may be heated to approximately 25° C.-200° C., 50° C.-175° C., 75° C.-150° C., 95° C.-125° C., and preferably approximately 92° C.-110° C. and more preferably approximately 94° C. (e.g., in a water bath). The rotor 2904 may spin the tube 2902 perpendicular to the long axis of the tube 2902. The tube 2902 may be spun to approximately 500 rpm to 10,000 rpm. The tube 2902 may be spun for approximately 15 seconds to 20 minutes. Spinning may cause the liquid to separate from the solid particles. The liquid may exit the aperture 2906 and accumulate, for example, on the liquid collector 2912. The optimum aperture 2906 size for extracting oil from Athabasca oil sands may be, for example, approximately 0.40-1.50 mm, 0.45-1.35 mm, 0.80-1.30 mm, or preferably approximately 0.85-1.10 mm. Once the liquid 3304 has left the tube 3002, the disk 3004 may be repositioned perpendicular to the length of the tube 3002 and removed from the tube 3002, as shown in FIG. 36c, extracting the remaining solid particles 3306 as it is removed. The ninth system 3000 may then be reused with a new solids-liquids mixture 3306, as shown in FIG. 36d.

[0133] FIGS. 37-38 show a tenth system 3400, which may have a cylindrical formation. The tenth system 3400 may include a shaft 3406. The shaft 3406 may be placed within a first cylinder 3402. The shaft 3406 may be angled to allow the movement of a solids-liquids mixture 3504 down the inside of the first cylinder 3402 by gravity. The first cylinder 3402 may include apertures 3416. An exploded exemplary view of the first cylinder 3402 including apertures 3416 is illustrated in FIG. 38a. The apertures 3416 may facilitate the separation of liquids 3502, such as oil or water, from solids, such as sand or shale, by retaining solids 3506 within the first cylinder 3402. The first cylinder 3402 may be placed within a second cylinder 3404. As shown in FIG. 37, the second cylinder 3404 may include a protrusion 3412. The protrusion 3412 may collect and direct the liquid 3502 to a collection point 3414.

[0135] The process for extracting liquids 3502 from solid particles 3506 may be adapted for the tenth system 3400, described above, by placing a solids-liquids mixture 3504 on the inside of the spinning first cylinder 3402 and allowing it to travel along the surface of the first cylinder 3402 by gravity. The solids-liquids mixture 3504 mixture may be heated before, during, or after placement in the first cylinder 3402. The solids-liquids mixture 3504, for example oil shale or oil sands, may be heated to approximately 25° C.-200° C., 50° C.-175° C., 75° C.-150° C., 95° C.-125° C., and preferably approximately 92° C.-110° C. and preferably approximately 94° C. (e.g., in a water bath). Spinning the first cylinder 3402 may cause the liquid 3502 to separate from the solid particles 3506. The first cylinder 3402 may be spun to approximately 500 rpm to 10,000 rpm. The first cylinder 3402 may be spun for approximately 15 seconds to 20 minutes. The liquid 3502 may exit the first cylinder 3402 through the apertures 3416. The optimum aperture 3416 size for extracting oil from Athabasca oil sands may be, for example, approximately 0.40-1.50 mm, 0.45-1.35 mm, 0.80-1.30 mm, or preferably approximately...
approximately 0.85-1.10 mm. The liquid 3502 may accumulate on the second cylinder 3404 and may be contained by the protrusion 3412 and drained at the collection point 3414. A person skilled in the art may be able to adjust the angle of the first cylinder 3402, the rotational rate of the first cylinder 3402, and the feed rate of the solids-liquids mixture 3504 such that a majority of the liquid 3502 may be removed by the time the solids-liquids mixture 3504 reaches the lower end of the first cylinder 3402. The tenth system 3400 may be used in a continuous process.

[0136] The process for extracting liquids 3702 from solid particles 3704 may be adapted for the eleventh system 3600, described above, by placing a solids-liquids mixture 3608 on the inside of the spinning first cylinder 3602 and using the rotating screw 3606 to move the solids-liquids mixture 3608 along the inner surface of the first cylinder 3602. The solids-liquids mixture 3608 may be heated before, during, or after placement in the first cylinder 3602. The solids-liquids mixture 3608, for example oil shale or oil sands, may be heated to approximately 25° C.-200° C., 50° C.-175° C., 75° C.-150° C., 95° C.-125° C., and preferably approximately 92° C.-110° C. and more preferably approximately 94° C. (e.g., in a water bath). Spinning the first cylinder 3602 may cause the liquid 3702 to separate from the solid particles 3704. The first cylinder 3602 may be spun to approximately 500 rpm to 10,000 rpm. The first cylinder 3602 may be spun for approximately 15 seconds to 20 minutes. The liquid 3702 may exit the first cylinder 3602 through the apertures 3614. The optimum aperture size for extracting oil from Athabasca oil sands may be, for example, approximately 0.40-1.50 mm, 0.45-1.35 mm, 0.80-1.30 mm, or preferably approximately 0.85-1.10 mm. The liquid 3702 may accumulate on the second cylinder 3604 and may be contained by the protrusion 3610 and drained at the collection point 3612. A person skilled in the art may be able to adjust the rotational rate of the screw 3606, the feed rate of the solids-liquids mixture 3608, and the rotational rate of the first cylinder 3602 such that a majority of the liquid 3702 may be removed by the time the solids-liquids mixture 3608 reaches the end of the first cylinder 3602. The eleventh system 3600 may be used in a continuous process.

[0138] FIG. 41 shows a cross sectional view of a twelfth system 3800, which may include a cylindrical formation. The thirteenth system may include a vertical first cylinder 3902 and a vertical second cylinder 3904, placed concentrically around a shaft 3906. The first cylinder 3902 and the second cylinder 3904 may include baffles 3910. The baffles 3910 may be arranged in a screw-thread-like fashion on the first wall of the second cone 3904, in the space between the first cone 3902 and the second cone 3904. The second cone 3904 may include apertures 3918. An exploded exemplary view of the second cone 3904 including apertures 3918 is illustrated in FIG. 41 a. The apertures 3918 may facilitate the separation of liquids 3912, such as oil or water, from solids 3914, such as sand or shale, by retaining solids 3914, within the second cone 3904. The twelfth system 3800 may also include a liquid collector 3908. The liquid collector 3908 may surround the second cone 3904.
The process for extracting liquids from solid particles may be adapted for the thirteenth system, described above, by placing a solids-liquid mixture in the space between the rotating first cylinder and a second cylinder. The solids-liquid mixture may be heated before, during, or after placement in the space between the first cylinder and second cylinder. The solids-liquid mixture may be heated to approximately 25°C to 200°C. The separation device comprises: a structure for confining sand particles; a structure for recovering the oil; and wherein the separation device is subjected to centrifugal force.

The method of claim wherein the aperture is about 0.80 to about 1.20 mm in diameter.

The method of claim wherein the oil sands are subjected to centrifugal force.

The method of claim wherein the oil is extracted from the oil sands without the use of chemicals.

A separation device for separating liquids from a solid particulate material, the separation device comprising: a structure for confining sand particles; a structure for recovering the oil; and wherein the separation device is subjected to centrifugal force.

The separation device of claim wherein: the structure for confining sand particles comprises a first tube and a second tube; the first tube and the second tube being dimensioned such that the first tube fits inside the second tube; the first tube including at least one aperture sized smaller than the oil sand; the first tube for confining the sand particles mechanically; and the second tube for recovering the oil.

The separation device of claim wherein: the structure for confining the particles has a clam shell formation comprising:

1. A method for separating oil from oil sands comprising:
   - heating the oil sands;
   - spinning the heated oil sands;
   - confining mechanically sand particles present in the oil sands away from the oil, and recovering the oil substantially free of sand.
2. The method of claim wherein the oil sands are heated to approximately 25-200°C.
3. The method of claim wherein the oil sands are heated to approximately 92°C to 110°C.
4. The method of claim wherein the particles are confined away from the oil by an aperture.
5. The method of claim wherein the aperture is about 0.40 to about 1.5 mm in diameter.
6. The method of claim wherein the aperture is about 0.80 to about 1.20 mm in diameter.
7. The method of claim wherein the oil sands are subjected to centrifugal force.
8. The method of claim wherein the oil is extracted from the oil sands without the use of chemicals.
9. A separation device for separating liquids from a solid particulate material, the separation device comprising:
   - a structure for confining sand particles; a structure for recovering the oil; and wherein the separation device is subjected to centrifugal force.
10. The separation device of claim wherein: the structure for confining sand particles comprises a first tube and a second tube; the first tube and the second tube being dimensioned such that the first tube fits inside the second tube; the first tube including at least one aperture sized smaller than the oil sand; the first tube for confining the sand particles mechanically; and the second tube for recovering the oil.
11. The separation device of claim wherein: the structure for confining the particles has a clam shell formation comprising:
   - a first portion and a second portion; the first portion and the second portion being dimensioned to fit together with an aligning pivot; the first portion including at least one cavity; the second portion including at least one cavity that mirrors the cavity of the first portion; and wherein, when the first portion and the second portion are fit together, the cavity in the first portion and the cavity in the second portion align to form one cavity; and the cavities terminate to form an aperture through which oil escapes; and the aperture is dimensioned to confine the sand particles within the cavity.
12. The device of claim wherein the aperture is about 0.40 to about 1.5 mm in diameter.
13. The device of claim wherein the aperture is about 0.80 to about 1.20 mm in diameter.
14. The separation device of claim wherein: the structure for confining the particles comprises:
   - one or more walls; the walls including apertures; the walls also including baffles located along the interior of the conical separator; the baffles being continuous and arranged radially; and wherein the separation device further comprises a structure for recovering the oil.
15. The device of claim wherein the aperture is about 0.40 to about 1.5 mm in diameter.
16. The device of claim wherein the aperture is about 0.80 to about 1.20 mm in diameter.
17. The separation device of claim wherein: the structure for confining the particles comprises:
   - three or more planes; the planes being freely rotatable about a central axis; the central axis having a pivot; the planes being orientated so that they form walls of a closed chamber when rotated to a closed formation; the planes further including apertures through which oil escapes; and a structure for recovering the oil.
18. The device of claim 17 wherein the aperture is about 0.80 to about 1.20 mm in diameter.

19. The separation device of claim 9, the separation device wherein the structure for confining the particles comprises:
   a rotating main shaft;
   a top piston and a bottom piston removably attached to the main shaft;
   a filtering portion;
   the filtering portion having a top band, a bottom band, and a screen;
   the screen having apertures through which oil escapes;
   the screen, the top piston, and the bottom piston being arranged such that the pistons may be raised or lowered out of the plane of the screen.

20. A system for separating oil from oil sands comprising:
   a source of centrifugal force;
   a heat source;
   a separation device; and
   a recovery device.

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