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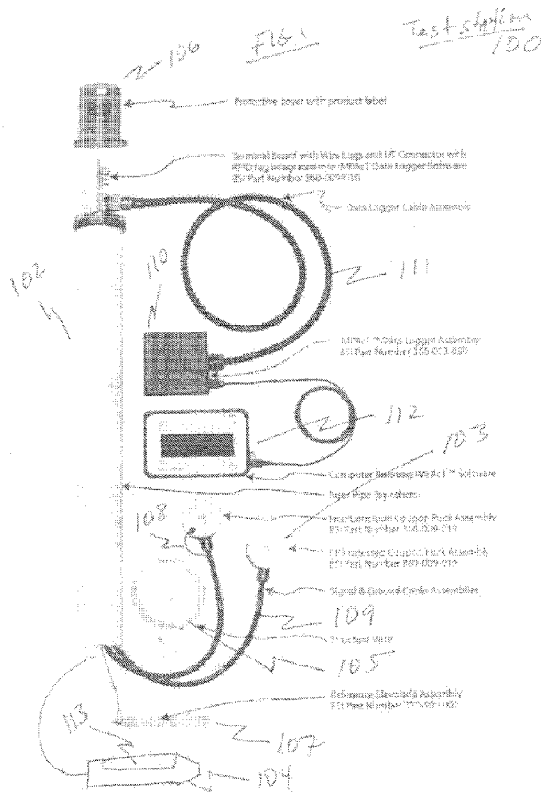
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(54) Title: **ULTRASONIC CATHODIC PROTECTION TEST STATION**

(57) Abstract: Ultrasonic transducers are imbedded into sacrificial metal coupons which are located in the vicinity of underground or aboveground structures, such as a pipe or tank, which allow for the measurement of the effectiveness of impressed current cathodic protection systems and can be used to determine the corrosion rate of the structure that is being protected. When excited by a pulser-receiver excitation pulse, the ultrasonic transducers can be used to determine the thickness of the coupon and its rate of change over time. The sacrificial metal coupon ultrasonic transducer assembly can be located in the vicinity of underground piping, under or inside of a tank, underground or underwater, or inserted into structures where absolute material loss values or material loss rate of change is being monitored.



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ULTRASONIC CATHODIC PROTECTION TEST STATION

CROSS REFERENCE TO RELATED APPLICATIONS

This application claims the benefit of US provisional application no. 62/213,813, filed
5 September 3, 2015, the contents of which are incorporated herein by reference.

FIELD OF INVENTION

This application relates to the use of ultrasound transducers imbedded into a
sacrificial anode that is located in the vicinity of an underground structure, such as a pipe or
10 tank, for measuring the effectiveness of impressed current cathodic protection systems and
determining the corrosion rate of the structure that is being protected.

BACKGROUND

Buried or immersed metal structures, such as pipes and tanks, are exposed to an
15 electrochemical corrosion process in the underground environment. The metal structure
becomes an electrode and the soil an electrolyte so that an electrolytic cell is formed causing
the corrosion of the buried structure. Some corrosion arises from naturally occurring
processes at specific locations on the underground structure involving electrical current flow
into the ambient soil electrolyte from sites acting as anodes via the corrosion reaction.
20 Current will flow to specific locations on underground structures acting as cathodes where
reduction reactions occur. Corrosion can also be caused or accelerated by voltages applied to
a local region of the pipe by manmade structures, including local transit systems, overhead
high voltage power (AC) lines, overhead sub-surface power distribution systems, and
industrial plants.

25 There are generally two methods to protect the underground structure from corroding.
These methods are referred to as "cathodic protection." The first method is to attach
sacrificial anodes onto or near the underground structure being protected, and the second is to
install an impressed current system that generates a DC voltage and a low constant current in
the specific vicinity of the structure being protected.

30 Sacrificial anodes are pieces of metal more electrically active than the underground
structures that can be attached to the underground structure for corrosion protection. Because
these anodes are more active than the underground structure, the corrosive current will exit

from the sacrificial anodes rather than from the underground structure. Thus, the underground structure is protected while the attached anode is sacrificed. Depleted anodes must be replaced for continued corrosion protection of the underground structure.

5 An impressed current system uses a rectifier that converts alternating current to direct current. This current is sent through an insulated wire to the anodes, which are metal bars buried in the soil near the underground structure being protected. The current flows through the soil to the underground structure and returns to the rectifier through an insulated wire attached to the underground structure. The underground structure is protected because the current going to the underground structure overcomes the corrosion-causing current normally
10 flowing away from it.

With a cathodic protection system, industry accepted criteria involve the measurement of the electrochemical potential of the structure to establish the level of cathodic protection sufficient to mitigate corrosion of the buried metal structure. The ordinary practice to determine the necessary level of cathodic protection is to measure the potential difference
15 between the buried structure, which is an electrode, and a reference electrode placed, at grade, in contact with the soil, which is an electrolyte. However, when this measurement is taken while the cathodic protection system is operating, a voltage drop through the soil due to the cathodic protection current, referred to as the IR (voltage) drop, causes an error in the potential measurement.

20 In order to measure a potential that is free of IR drop, it is common to measure the potential immediately following interruption of the cathodic protection current. The instantaneous voltage drop which occurs immediately after the cathodic protection is turned off is equal to the IR drop caused by the interrupted cathodic protection current. Because the electrochemical interface of the protected structure has a capacitive component, the potential
25 of that interface does not change immediately following interruption as does the IR drop. Therefore, the potential measured immediately following interruption of the cathodic protection current, when current, I , is zero, is the potential of the protected structure free of IR drop. This potential is referred to as off-potential.

30 Problems arise in interrupting the cathodic protection. Extremely long buried pipelines have multiple cathodic protection stations, all of which must be interrupted simultaneously, or interrupted using a non-synchronous method in which all of the IR drops are summed. Galvanic cathodic protection systems are not designed to be interrupted because

the anodes are typically directly connected to the protected structure. Additionally, second-party cathodic protection systems that are either unknown or cannot be interrupted may be present in the area. Other problems exist, also, such as stray current effects, e.g., from power distribution systems, dc transit systems, etc., that are not interruptable, and rapid IR
5 transients, which immediately follow interruption. For instance, AC current magnetic fields created in the vicinity of high voltage power lines can propagate into the earth and induce corrosion. This is known as AC-induced corrosion. Such corrosion on cathodically protected underground pipelines is commonly the result of a combined action of the induced AC voltage, the cathodic protection conditions, a piping coating defect and the chemical and
10 physical conditions of the soil. As a result, both DC and AC current fields can influence corrosion of underground structures.

In order to avoid the problems associated with interruption of the entire cathodic protection system, “coupons” are used to monitor the level of cathodic protection on buried metal structures such as pipes. The coupon is a bare metal sample having substantially the
15 same metallurgical attributes as the pipe or other structure being monitored. The coupon is placed in the soil near the pipe and connected to the pipe. Therefore, the coupon is exposed to the same cathodic protection current source as the pipe. The connection between the pipe and the coupon is interrupted for a time period, during which time the potential difference between the coupon and a reference electrode is measured. The pipe's cathodic protection is
20 never interrupted, since only the pipe-to-coupon connection is interrupted. The coupon's potential simulates the potential of a pipe coating defect of a similar surface area as the coupon. The coupon's potential can be measured without interrupting the cathodic protection to the pipe, and therefore without some of the problems inherent in interrupting the entire cathodic protection system. In addition, once the coupon is interrupted, it is an isolated, small
25 piece of metal in the soil and stray currents are eliminated from its surface. In contrast, stray currents are generally not eliminated from a pipeline upon interruption of the entire cathodic protection system.

Despite the existence of a significant number of devices for determining the effectiveness of cathodic protection, the need exists for a simple, inexpensive and accurate
30 measuring device. In the description provided above, the coupon serves as a simulation of the behavior of the underground structure that is being protected. The coupon is used for measuring changes in electrical potential near and in the vicinity of the underground structure

that is being protected. The changes in electrical potential are characteristically “noisy.” That is, the changes in the electrical potentials or the resistance of a coupon are not always consistent and are affected by temperature variations, the presence of stray currents themselves, instrumentation calibration challenges and operator error. There is a need for
5 coupons that are not impacted by environmental or operator data-acquisition variables; coupons that can be measured with more precision and accuracy.

SUMMARY

The present invention solves the foregoing problems by providing a coupon imbedded
10 with one or more ultrasonic transducers that can determine the thickness of the coupon and can be energized and read from the surface by an operator with a suitable ultrasound pulse/receiver instrument. The piezoelectric ultrasound transducer converts the pulse of electrical energy into an acoustic pressure wave (sound). The pressure wave is coupled to the surface of a plate via fluid in a reservoir, or by an equivalent acoustic coupler. Most of the
15 energy (sound) is reflected from the front surface of the plate due to the acoustic impedance discontinuity. Some energy enters the plate and travels through the plate and is reflected from the back surface of the plate back towards the front surface. Some of the reflected energy leaves the front of the plate and some is reflected towards the back surface of the plate. This reflection process continues. Energy is lost from the plate boundary surfaces for each
20 reflection. Energy lost at the front of the plate travels back towards the ultrasound transducer where it is received and converted back to electrical energy. The electrical pulses received represent the two way acoustic front-to-back acoustic travel times. The thickness of the plate can be estimated by measuring the pulse to pulse travel time and knowing the velocity of sound in the plate under test. By searching for a reduction in the plate thickness, plate
25 corrosion or pitting can be located.

The transducers can be positioned directly underneath the coupon’s surface and can, on operator demand, measure the thickness of the coupon. The coupon’s thickness will change as the metallurgy of the underground structure changes in a way that alters the thickness of the coupon material as well. This information provides a direct rather than an
30 inferred measure of rate of material loss due to any corrosion activity that may be occurring with the underground structure under protection.

In one of many possible embodiments of the invention, the system includes two “smart ultrasonic coupons” or for simplicity “probes.” Each ultrasonic transducer has 2 wires. Each probe has 2 to 3 transducers; therefore, there are 4 to 6 transducer wires that allow each transducer to be activated from the surface by an operator. There is an additional ground wire available to the operator for each probe. Additionally, one probe has a reference electrode with a wire connected to it and available at the surface for operator access. A wire also is connected to the underground structure and is also available to the operator at the surface. This arrangement provides the operator with all the functionality associated with traditional cathodic protection test stations. However, the addition of the ultrasonic coupons located within each probe provides the operator with the added ability to directly monitor metal loss, a more accurate assessment of underground structural integrity.

Coupons with imbedded ultrasonic transducers optionally but preferably can include one or more of the following features:

1. Frequencies of the probe can be selected based on the required thickness of the coupon.
2. The metallic, sacrificial material within each probe can be changed to match that of the structure being monitored.
3. The area of the exposed surface of the coupon can be modified to accommodate increased sensitivity to DC current (10 cm^2) or AC current (1 cm^2).
4. The distance of the transducer from the coupon can be changed to improve the quality of the ultrasonic return and better decipher the echo-to-echo pulses needed to determine coupon thickness and change of thickness sensitivity.
5. Each transducer within the probe can generate a bulk wave that can be received by any adjacent transducer. Such a bulk wave can be used to evaluate local changes in the coupon surface that might not be detected if not present directly above an individual transducer.
6. Signal processing techniques can be applied to the activation and signal reception of each ultrasonic transducer such that “chirp” signals can be generated, received and analyzed in addition to traditional pulse-echo signals.

Non-limiting examples of applications for which a cathodic protection test station of the present invention can be used include:

1. Aboveground or belowground tanks

2. Aboveground or belowground pipes and piping
3. Submerged structures such as those for bridges and buildings
4. Underground pilings, tunnels, and related infrastructure

The ultrasonic cathodic protection test station of the present invention solves many of the monitoring accuracy and handling problems through the use of one or more piezoelectric ultrasonic testing (UT) transducers integrated into a sacrificial coupon. UT transducers are known to the non-destructive testing industry as one of the most accurate, repeatable and precise methods of determining material degradation and material loss. UT transducers have not been used in connection with sacrificial coupons, at least in part, because of the inability to effectively secure an ultrasonic transducer to a coupon for long periods of time. The connection interface between the UT transducer and the coupon changes over time, e.g., by evaporation or other chemical or physical changes, and as a result the ability of the transducer to transfer acoustic energy to the coupon is affected. The present invention solves this problem, and as a result UT transducers can be used to measure and monitor changes over time in a sacrificial coupon.

The present invention further solves the foregoing problems by providing a coupon-ultrasonic measurement system combined with one or more transducers for determining material loss. The system includes a sacrificial coupon; one or more transducers supported under the sacrificial coupon and responsive to electrical energy from a pulser/receiver; remotely-located drive circuitry for energizing and receiving energy from the transducers; an attachment mechanism for use in above ground storage tanks for positioning the sacrificial coupon and transducer assembly under the tank; an a cabling mechanism for use adjacent to an underground pipe or underground tank; and processing and memory means for producing the excitation pulse, receiving the transmitted pulse, processing the signal to determine material thickness, and storing the resultant material thickness values for display and tracking.

A sacrificial metal coupon is provided with one or more ultrasonic transducers which, when excited by a pulser-receiver excitation pulse, determines the thickness of the coupon and its rate of change over time. The sacrificial metal coupon ultrasonic transducer assembly can be placed adjacent to a pipe, under or inside of a tank, underground or underwater, or inserted adjacent to structures where absolute material loss values or material loss rate of change is being monitored. In order to characterize the type of metal loss due to corrosion or

erosion, the excitation pulse can be a pulse-echo or chirp pulse and one transducer can insonify the coupon and the second transducer can receive the transmission a fixed distance away for further analysis. The use of ultrasound to measure metal loss in a sacrificial coupon minimizes the inaccuracy of traditional sacrificial coupon metal loss measurements and provides for a more convenient and safe method for determining coupon integrity.

The test station's coupon-ultrasonic material measurement system can also be used to evaluate the effectiveness of chemical inhibitors which are used to mitigate the impact of localized electrical interference by changing the resistance characteristics of the surrounding earth electrolyte conditions. The UT test station, in its standard configuration, consists of a reference electrode, e.g., CuCuSo₄ material, used to simultaneously measure the effectiveness of neighboring electromagnetic fields generated by cathodic protection impressed current systems.

One aspect of the invention is a corrosion coupon probe including: two or more coupon bodiess adapted for receiving sensors, receivers, transmitters, electrical components, and cabling for altering the distance of the corrosion coupons from the primary aboveground test station; cabling connected to the coupon body and adapted for receiving an ultrasonic testing (UT) transducer; one or more UT transducers secured to the coupon holder member; an acoustic couplant positioned adjacent the one or more UT transducers; a sacrificial coupon connected to the coupon holder member such that the sacrificial coupon is adjacent the acoustic couplant; an attachment body for inserting the sacrificial coupon into a liquid or underground, dry environment; and a reference electrode either attached to or positioned adjacent to the coupon body for simultaneously measuring corrosion rate of the sacrificial coupon and an electromagnetic field created by an impressed current cathodic protection system.

A second aspect of the invention is a corrosion coupon probe including: a sacrificial coupon; one or more UT transducers; and an acoustic couplant, wherein the one or more transducers are connected to the sacrificial coupon and the acoustic couplant is positioned between the sacrificial coupon and the one or more UT transducers.

A third aspect of the invention is a corrosion monitoring system including: a corrosion coupon probe having (i) a sacrificial coupon, (ii) one or more UT transducers, and (iii) an acoustic couplant, wherein the one or more transducers are connected to the sacrificial coupon and the acoustic couplant is positioned between the sacrificial coupon and the one or

more UT transducers; processing means for producing an excitation pulse, for receiving a transmitted pulse from the sacrificial coupon, and for processing signals to determine sacrificial coupon material thickness; and memory means for storing material thickness values determined by the processing means.

5 A fourth aspect of the invention is a separate wire that is welded to an aboveground or underground structure that is being protected and terminated at the at-grade, remote, test station for acquiring data for tracking and reporting.

A fifth aspect of the invention is the presence of a ground reference wire fastened to each of the underground, or under tank, coupons and terminated at the at-grade test station.

10 A sixth aspect of the invention is the presence of an above ground test station where all of the above-cited wires are terminated on separate test points along with the multi-pin connector containing the corrosion coupon probe UT transducer wires for receiving a transmitted pulse from the sacrificial coupon, and for processing signals to determine sacrificial coupon material thickness.

15

BRIEF DESCRIPTION OF THE DRAWINGS

The present invention is described with reference to the accompanying drawings. In the drawings, like reference numbers indicate identical or functionally similar elements. Additionally, the left-most digit(s) of a reference number identifies the drawing in which the reference number first appears.

20

FIG. 1 is an exploded view of one of many possible embodiments of an ultrasonic cathodic protection test station;

FIG. 2 is an exploded view of one of many possible embodiments of an ultrasonic corrosion coupon;

25

FIG. 3 illustrates two potential operating locations of the test station;

FIG. 4 illustrates five modes of electrical to mechanical energy conversion used to characterize the amount of and type of material loss;

FIG. 5 is a block diagram of the total coupon probe inspection system showing the relationship between the data logger and the test station probe assembly; and

30

FIG. 6 illustrates the electrical terminals and connector for pulsing the UT transducers and receiving the UT data from the UT sacrificial coupons.

DETAILED DESCRIPTION

Referring generally to FIG. 1, there is shown an embodiment of an ultrasonic cathodic protection test station (“test station”) 100 of the present invention. The test station 100 includes a mounting tube (:tube”) 102 that is adapted for receiving sensor wires and/or transmitters, electrical components, and various connectors for configuring the tube 102 depending on the intended use of the test station 100. The tube 102 optionally but preferably includes a data I/O terminal 106, which optionally but preferably is detachably fastened to the tube 102.

Two or more ultrasonic coupons can be located via a cabling assembly at any distance from the test station tube 102. The shape of the coupon can be altered to fit the requirements of the environment that it is monitoring. In Figure 1, two types of coupon bodies are shown. A round body 103 coupon preferably is used adjacent to, for instance, an underground pipeline. An elongated body 104 coupon can be used for use in aboveground storage tanks. A wire 105 is provided for attachment to an underground structure, in the case of a pipe, for instance, or for attachment to an above or below ground tank. The wire 105 is terminated at the I/O terminal 106. A reference electrode assembly 107 is connected to a cable assembly of any length that is terminated at the I/O terminal 106. Ground wires 108 and 109 are connected to each of the UT sacrificial coupons, e.g., 103, and terminated at the I/O terminal 106.

The test station 100 can include a data logger 110, which optionally but preferably contains software to pulse and acquire the UT information, prepare the data for subsequent analysis within the data logger, or transmit the data wirelessly to a remotely located receiver. The data logger 110 further can be used to organize the data within a database for future analysis. The data logger 110 can interface to any computer 112 via an input/output cable such as a USB cable.

The test station 100 can include an umbilical 111 in communication with the data logger 110, which optionally but preferably is interfaced with a general purpose computer or has independent processing means, and further includes a pulser/receiver unit. The umbilical 111 can transmit electrical energy, or pulses, created by the pulser/receiver in the data logger 110 to the test station coupons 103 or 104. The umbilical 111 also can transmit an electrical representation of the return signal from one more transducers in the test station 100 coupon 103 or 104 back to the data logger 110.

Referring generally to Figure 2, there is shown one of many possible embodiments of an ultrasonic corrosion coupon transducer assembly (“transducer assembly”) 200. The transducer assembly optionally but preferably has a body with one or more openings. A piezoelectric chip 201 can be positioned in each of the openings in the transducer assembly
5 200. For purposes of this invention, “piezoelectric chip” and “transducer” can be used interchangeably. In one of many possible alternative embodiments of the invention, the transducers 201 can be connected to a bottom surface of a coupon 203 by machine screws or other fastening means. An acoustic couplant 202 can be positioned within the transducer assembly 200 adjacent to the sacrificial coupon 203 and couplant 202. The acoustic couplants
10 202 are placed between the face of the piezoelectric chips 201 in the transducer assemblies 200 and the bottom surface of the coupon 203. As the machine screws or other fastening means are tightened, the couplants 202 are compressed to a fixed point that will not alter the quality of the UT transducer A-scan. The transducer assemblies 200 optionally but preferably are sealed and are waterproof so the assembly 200 can be positioned anywhere to monitor
15 metal loss remotely using ultrasound as long as the wiring is properly sealed.

The coupon 202 material can be of one or more types of metal or non-metal that are subject to loss of integrity due to corrosion or erosion and where the loss and rate of loss can be precisely measured with the use of ultrasound transducers attached to the coupon material. In an alternative embodiment, the coupon material can be of one or more types of metal or
20 non-metal that are subject to loss of integrity due to chemical attack and where the chemical attack can be associated with change in the exposed liquid product quality or a change in process conditions. In yet another alternative embodiment, the coupon material can be of one or more types of metal or non-metal that are subject to loss of integrity due to corrosion, erosion or chemical attack and where the electrical pulses of one or more transducers can be
25 used to induce one or more different mechanical wave patterns which can be used to characterize the amount and type of material loss on the surface of the coupon material.

The ultrasonic corrosion coupon assembly 200 can be placed near or offset from a surface it is designed to monitor. The ultrasonic corrosion coupon 203 is used as a surrogate to extrapolate the corrosion, pitting, metal loss, etc. of the pipe or other structure being
30 monitored. The changes to the coupon 203 are representative of the changes to the pipe or other structure being monitored, and the condition of the structure being monitored can be determined indirectly by monitoring the status of the coupon 203 from the I/O terminal 106.

FIG 3 shows two of the many possible locations for the placement of an ultrasonic cathodic protection test station 100. The test station 100 can be placed adjacent to a mechanical structure, such as an aboveground storage tank. The coupon 113 located on the elongated embodiment of a ultrasonic test station probe 114 can be used as a surrogate to
5 extrapolate the corrosion, pitting, metal loss, etc. of the storage tank or other structure being monitored. The changes to the coupon 113 are representative of the changes to the underside of the tank, e.g., the condition of the tank floor or other structure being monitored can be determined indirectly by monitoring the status of the coupon 113. The probe 114 also can include a reference electrode 115, which can be used to measure potential difference of the
10 impressed current impinging on the pipe or tank bottom, for instance, and ground. The data logger 116 contains software to pulse and acquire the UT information, prepare the data for subsequent analysis within the data logger, or transmit the data wirelessly to a remotely located receiver, and organize the data within a database for future analysis.

As shown in FIG. 4, there are at least five modes of mechanical energy signal
15 processing that may be applicable to the present invention. The first mode, shown in FIG. 4(a), is created by the compression of the material directly under the UT transducer that reverberates from the front surface of the coupon to the back surface. The thickness of the coupon material can be determined by dividing the signal travel time from surface-to-surface in the coupon material by the speed of sound of the material.

20 The second mode, shown in FIG. 4(b), of mechanical energy created by the UT transducer is referred to as a bulk wave. The bulk wave is created by one UT transducer, Transducer(i), that is received by the adjacent UT transducer, Transducer(ii), located a fixed distance from the transmitting UT transducer. The energy transmitted into the coupon material will change as a function of any change in the mechanical integrity of the coupon.
25 Changes in mechanical integrity can be in the form of overall reduction in thickness, the appearance of localized pitting or the appearance of cracks. The total energy created by the bulk wave can be referred to as the root mean squared (RMS). The RMS value of a set of continuous-time waveforms is the square root of the arithmetic mean of the squares of the values, or the square of the function that defines the continuous waveform. The formula for a
30 continuous function (or waveform) $f(t)$ defined over the interval $T_1 \leq t \leq T_2$ is:

$$f_{rms} = \sqrt{\frac{1}{T_2 - T_1} \int_{T_1}^{T_2} [f(t)]^2 dt},$$

and the RMS for a function over all time is

$$f_{rms} = \lim_{T \rightarrow \infty} \sqrt{\frac{1}{T} \int_0^T [f(t)]^2 dt}.$$

The effective RMS voltage (or power) of one or more sinusoids can be obtained without the use of calculus and can be calculated by squaring a waveform, taking the mean of the squared waveform and then computing the square root, as given by:

$$V_{rms} = \sqrt{\text{mean}\{v(t) * v(t)\}} = \sqrt{\frac{\text{area under the curve of } \{v(t) * v(t)\}}{\text{observation length}}}$$

10

where the observation length is the period, or integer multiple of the period, for as long as possible for the aperiodic signals generated by the piezoelectric-induced mechanical waves in the coupon. The total RMS value for any bulk wave can be measured and the resultant RMS return can be displayed as depicted in FIG. 4(c).

15

An additional way to provide greater information about the current condition of the coupon and any change due to external factors is through the frequency response of the coupon. The total frequency response associated with the mechanical vibrations produced by the coupon as a result of the piezoelectric transducer, shown in FIG. 4(d), can provide information about changes in the coupon's integrity. A fast Fourier transform (FFT) algorithm can be used to convert components of a signal, in this case mechanical vibrations, from its time domain to a representation in the frequency domain. There are a number of different types of FFT formulas but the most common one used for discrete Fourier analysis is noted below and is used in the current embodiment of the coupon-ultrasonic material measurement system:

25

$$X_k = \sum_{n=0}^{N-1} x_n e^{-i2\pi k \frac{n}{N}} \quad k = 0, \dots, N - 1.$$

Finally, another method of detecting change in the integrity of the coupon is through the use of a spectrographic analysis as shown in FIG. 4(e). In this case, the mechanical energy resulting from the vibrations produced by the coupon as a result of the piezoelectric transducer can be displayed in terms of the coupon's frequency response distributed over time.

5

FIG 5 depicts the relationship of the components of a UT testing station 100. One or more coupons, e.g., a round coupon 103 or an elongated coupon 104, depending on the structure to be monitored and its location, is communicably connected with an I/O terminal. The I/O terminal can be connected to a data logger, which optionally but preferably contains software to pulse and acquire the UT information, prepare the data for subsequent analysis within the data logger, or transmits the data wirelessly to a remotely located receiver. The data logger further can be used to organize the data within a database for future analysis. The data logger can interface to any computer via an input/output cable such as a USB cable.

10

FIG 6 shows one of many possible embodiments of an I/O terminal 600 with terminal connections: a reference electrode 601; a connection 602 to a wire connected to an underground structure; a connection 603 to an UT coupon located adjacent to the underground structure; a connection 604 to an UT coupon located further away from the underground structure; and one or more external electronic connectors 605 can be included and adapted for receiving an electronic connector extension cable 606 or an umbilical. An umbilical can be used as a conduit that houses wires necessary for providing electrical pulses to and from a pulser/receiver, which can be either attached to or located remotely from, a coupon-ultrasonic material measurement system of the present invention. A Radio Frequency Identification Device (RFID) 607 can be located onto the terminal I/O block 600.

15

20

25 CONCLUSION

While various embodiments of the present invention have been described above, it should be understood that they have been presented by way of example only, and not limitation. It will be understood by those skilled in the art that various changes in form and details may be made therein without departing from the spirit and scope of the invention.

30

Thus, the breadth and scope of the invention should not be limited by any of the above-described exemplary embodiments.

What is claimed is:

1. A cathodic protection test station, comprising:
 - a mounting tube havng a top and a bottom;
 - an input/output terminal secured to the top of the mounting tube;
 - 5 a transducer assembly having a body with one or more openings;
 - one or more ultrasonic testing (UT) transducers positioned in the one or more openinga in the transducer assembly;
 - an acoustic couplant positioned adjacent the one or more UT transducers;
 - a sacrificial coupon connected to the transducer assembly such that the sacrificial
 - 10 coupon is adjacent to the acoustic couplant; and
 - a reference electrode connected to an input/output terminal with a wire for simultaneously measuring corrosion rate of the sacrificial coupon and an electromagnetic field created by an impressed current cathodic protection system.
- 15 2. The corrosion coupon probe of claim 1, wherein the reference electrode is a Cu-CuSO₄ grounding electrode.
3. A transducer assembly, comprising:
 - a sacrificial coupon;
 - 20 one or more UT transducers; and
 - an acoustic couplant, wherein the one or more transducers are connected to the sacrificial coupon and the acoustic couplant is positioned between the sacrificial coupon and the one or more UT transducers.
- 25 4. The transducer assembly of claim 3, further comprising a coupon body adapted for receiving sensors, receivers, transmitters, electrical components, or connectors for altering the configuration of the transducer assembly.
- 30 5. The transducer assembly of claim 3, further comprising a coupon holder member connected to the transducer assembly and adapted for receiving the one or more UT transducers, and wherein the UT transducers are secured to the coupon holder member.

6. The transducer assembly of claim 3, further comprising a mounting tube for inserting the sacrificial coupon into an underground or aboveground environment.

7. The transducer assembly of claim 4, further comprising a reference electrode attached to the coupon body for simultaneously measuring corrosion rate of the sacrificial coupon and an electromagnetic field created by an impressed current cathodic protection system.

8. The corrosion coupon member of claim 7, wherein the reference electrode is a Cu-CuSO₄ grounding electrode.

10

9. A corrosion monitoring system, comprising:

a corrosion coupon probe, comprising:

a sacrificial coupon;

one or more UT transducers; and

15

an acoustic couplant, wherein the one or more transducers are

connected to the sacrificial coupon and the acoustic couplant is positioned

between the sacrificial coupon and the one or more UT transducers;

processing means for producing an excitation pulse, for receiving a transmitted pulse from the sacrificial coupon, and for processing signals to determine sacrificial coupon material thickness; and

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memory means for storing material thickness values determined by the processing means.

10. The corrosion monitoring system of claim 9, further comprising:

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a drive circuit that energizes the one or more transducers with either a narrow band or broadband electrical pulse of substantially identical duration but offset in time from one another;

a pulser/receiver that has a separate channel for each UT transducer integrated into the sacrificial coupon; and

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an umbilical attached to the pulser/receiver for producing and receiving the ultrasonic electrical pulse and connecting the reference electrode to a separate or integrated electromagnetic field measurement device.

11. The corrosion monitoring system of claim 9, wherein the corrosion coupon probe further comprises a body adapted for receiving sensors, receivers, transmitters, electrical components, or connectors for altering the configuration of the elongated body.

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12. The corrosion monitoring system of claim 9, wherein the corrosion coupon probe further comprises a coupon holder member connected to the body and adapted for receiving the one or more UT transducers, and wherein the UT transducers are secured to the coupon holder member.

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13. The corrosion monitoring system of claim 9, wherein the corrosion coupon probe further comprises a mounting tube for inserting the sacrificial coupon into an underground or aboveground environment.

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14. The corrosion monitoring system of claim 9, wherein the corrosion coupon probe further comprises a reference electrode attached to the coupon body for simultaneously measuring corrosion rate of the sacrificial coupon and an electromagnetic field created by an impressed current cathodic protection system.

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15. The corrosion monitoring system of claim 9, wherein the reference electrode is a Cu-CuSO₄ grounding electrode.

16. The corrosion coupon probe of claim 9, wherein the broadband or narrow band electrical pulse comprises energy from about 1.0 MHz to about 10.0 MHz.

25

*Test start/Com
100*

FIG 1

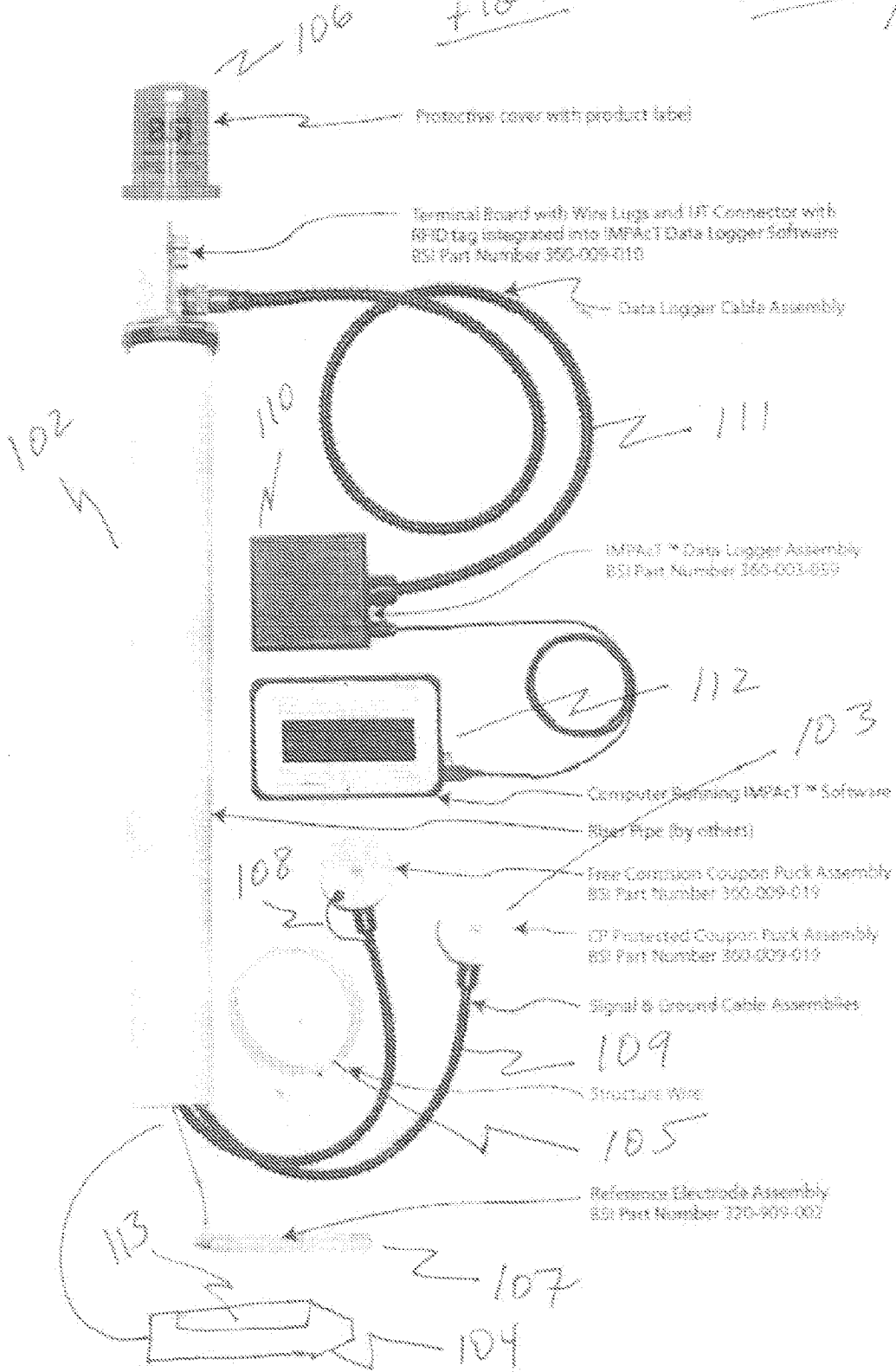
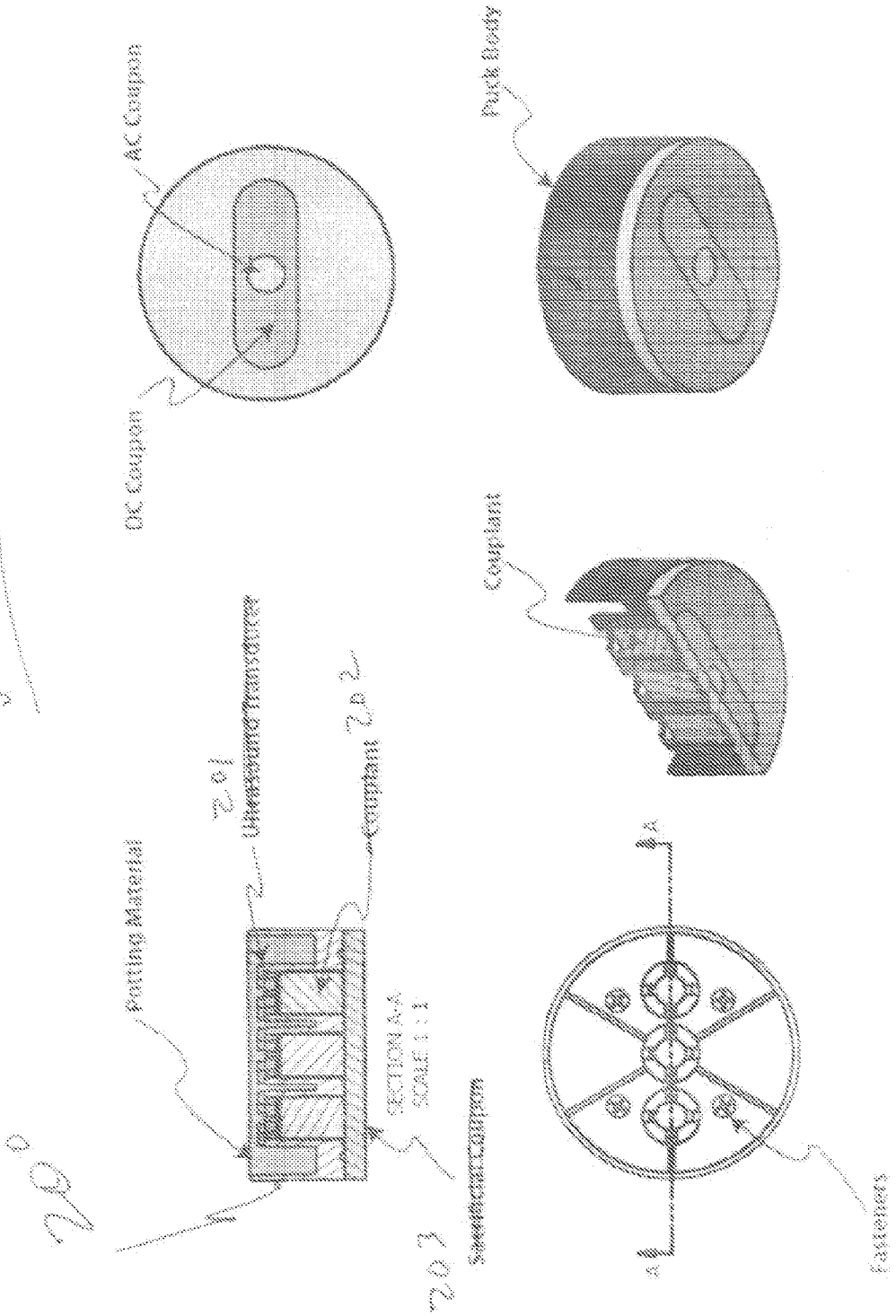
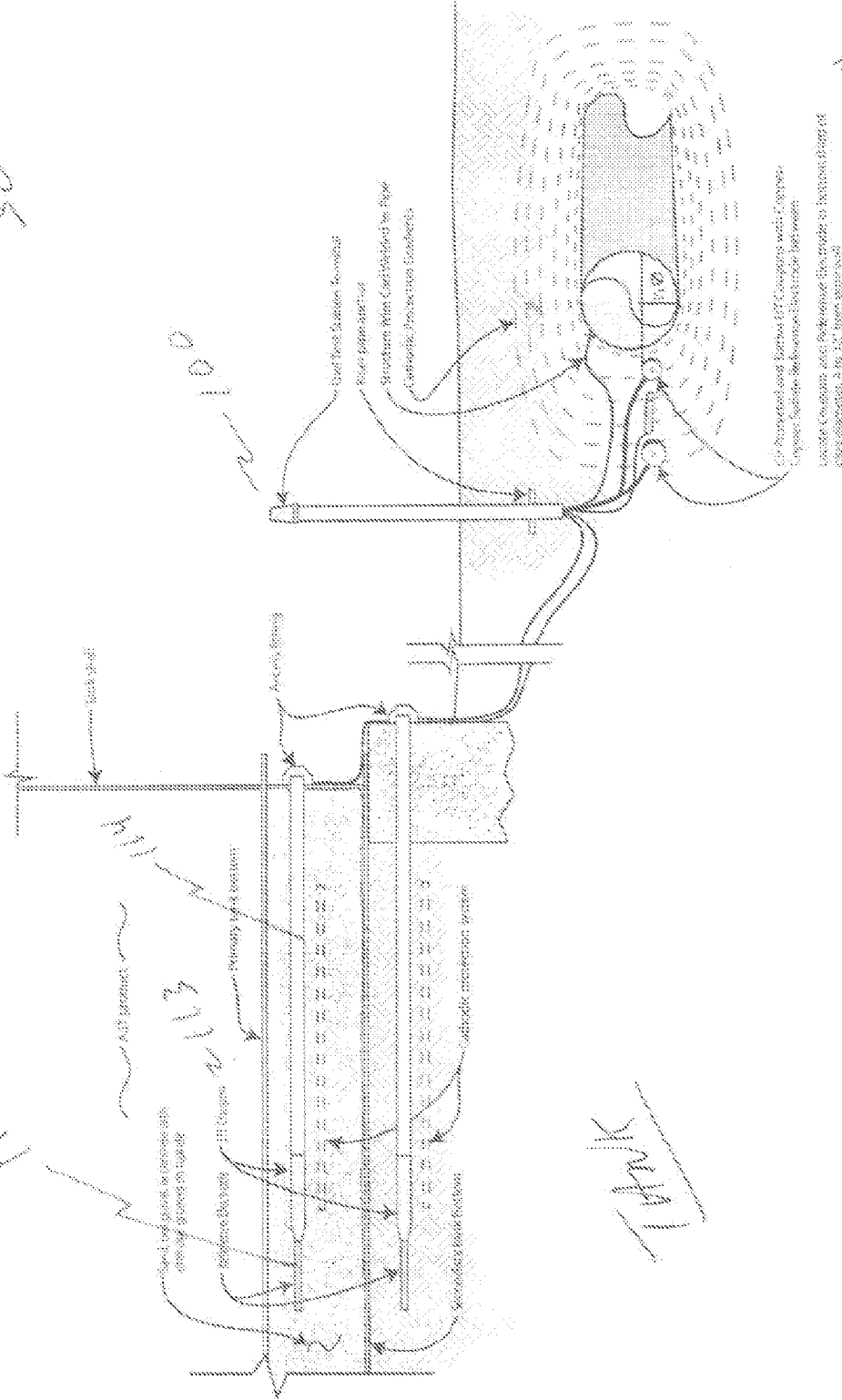


Fig 2



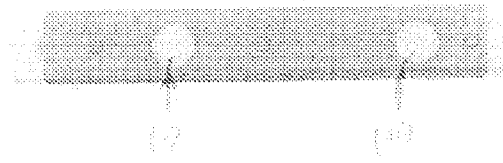
Flr 3
300



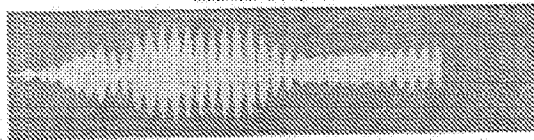
Added 6/1/16
2/1/16

Thank

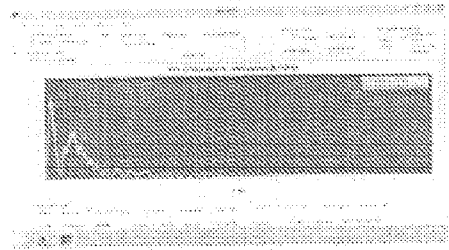
FIG. 4



(11)



(12)



(13)



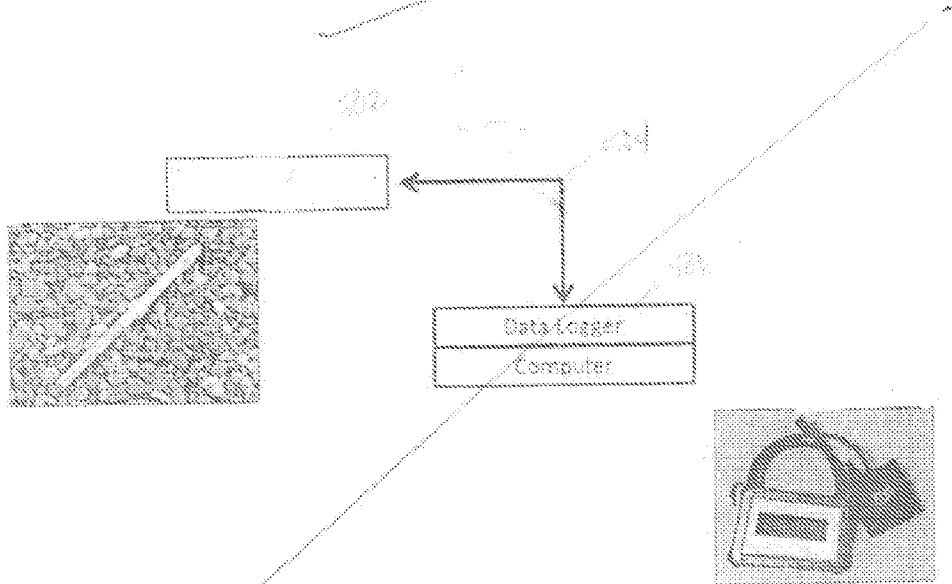
(14)



(15)

[Handwritten signature]

FIG 5



UT COMPONE FOR Terminal

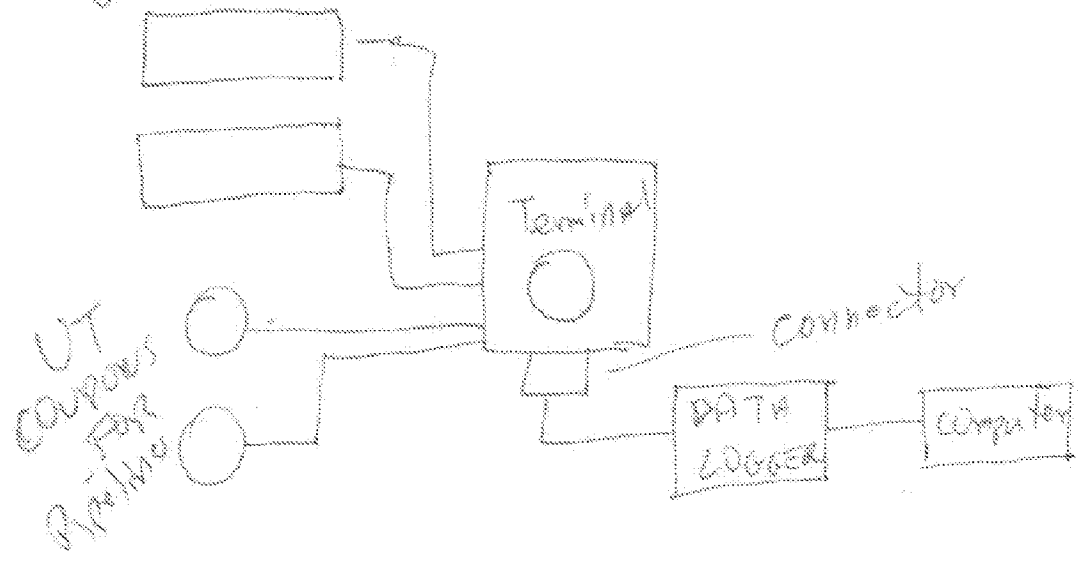
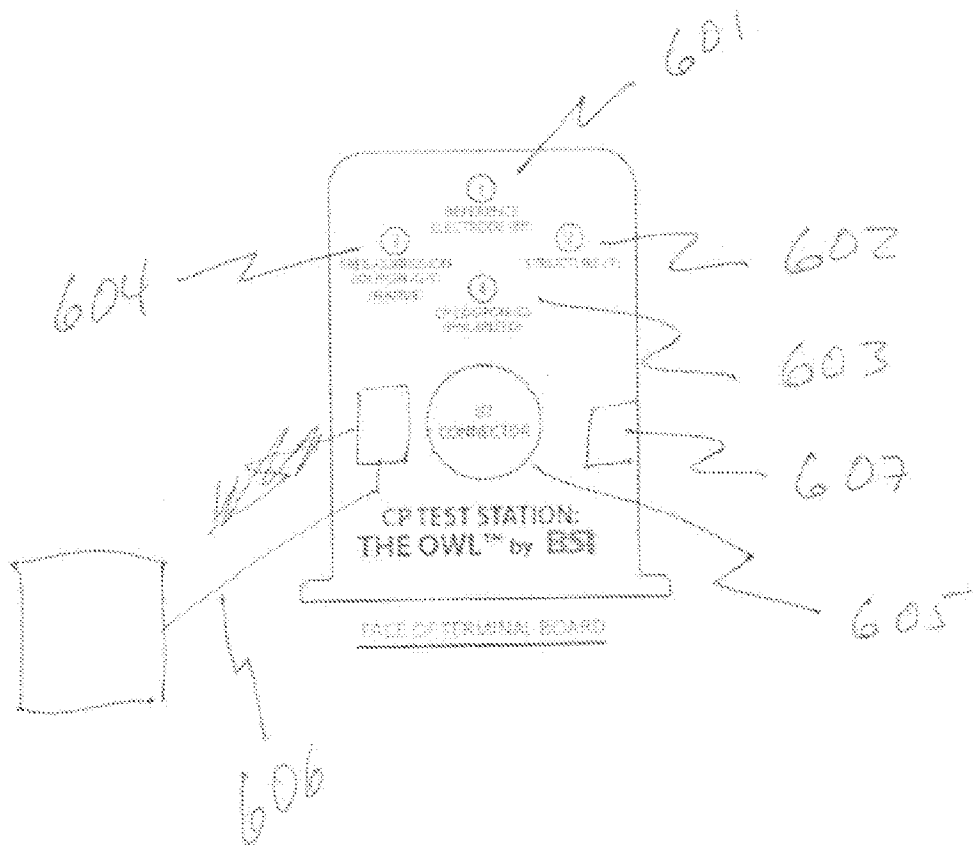


FIG. 6
600



INTERNATIONAL SEARCH REPORT

International application No.

PCT/US16/50117

Box No. II Observations where certain claims were found unsearchable (Continuation of item 2 of first sheet)

This international search report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. Claims Nos.:
because they relate to subject matter not required to be searched by this Authority, namely:

2. Claims Nos.:
because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically:

3. Claims Nos.:
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

Box No. III Observations where unity of invention is lacking (Continuation of item 3 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:
See extra sheet.

1. As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims.
2. As all searchable claims could be searched without effort justifying additional fees, this Authority did not invite payment of additional fees.
3. As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims for which fees were paid, specifically claims Nos.:
4. No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:
1-8

Remark on Protest

- The additional search fees were accompanied by the applicant's protest and, where applicable, the payment of a protest fee.
- The additional search fees were accompanied by the applicant's protest but the applicable protest fee was not paid within the time limit specified in the invitation.
- No protest accompanied the payment of additional search fees.

INTERNATIONAL SEARCH REPORT

International application No.

PCT/US16/50117

A. CLASSIFICATION OF SUBJECT MATTER
 IPC(8) - G01F 17/00; G01N 29/14, 29/30, 29/34, 29/44 (2016.01)
 CPC - G01F 17/00; G01N 29/14, 29/30, 29/343, 29/44
 According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
 IPC(8): G01F 17/00; G01N 29/04, 29/14, 29/30, 29/34, 29/44 (2016.01)
 CPC: G01F 17/00; G01N 29/043, 29/14, 29/30, 29/343, 29/44, 2291/044

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)
 PatSeer (US, EP, WO, JP, DE, GB, CN, FR, KR, ES, AU, IN, CA, INPADOC Data); Google; Google Scholar; EBSCO; KEYWORDS:
 cathodic protection test station mounting tube input/output terminal transducer assembly ultrasonic testing acoustic couplant sacrificial coupon reference electrode corrosion rate electromagnetic field impressed current

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y --- A	US 8,521,453 B1 (SILVERMAN, E. et al.) August 27, 2013; figures 18-19; column 6, lines 26-471; column 7, lines 7-12	3-6 ----- 1-2, 7-8
Y --- A	US 2004/0055391 A1 (DOUGLAS, D. et al.) March 25, 2004; figure 1; paragraphs [0054-0056]	3-6 ----- 1-2, 7-8
A	US 5,728,943 A (COLTER, L. et al.) March 17, 1998; column 7, line 66 to column 8, line 12	7-8

Further documents are listed in the continuation of Box C. See patent family annex.

* Special categories of cited documents:
 "A" document defining the general state of the art which is not considered to be of particular relevance
 "E" earlier application or patent but published on or after the international filing date
 "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
 "O" document referring to an oral disclosure, use, exhibition or other means
 "P" document published prior to the international filing date but later than the priority date claimed
 "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
 "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
 "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
 "&" document member of the same patent family

Date of the actual completion of the international search 23 November 2016 (23.11.2016)	Date of mailing of the international search report 26 JAN 2017
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Name and mailing address of the ISA/US Mail Stop PCT, Attn: ISA/US, Commissioner for Patents P.O. Box 1450, Alexandria, Virginia 22313-1450 Facsimile No. 571-273-8300	Authorized officer Shane Thomas PCT Helpdesk: 571-272-4300 PCT OSP: 571-272-7774
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INTERNATIONAL SEARCH REPORT

International application No.

PCT/US16/50117

-***-Continued from Box III-***-

The application contains the following inventions or groups of inventions which are not so linked as to form a single general inventive concept under PCT Rule 13.1. In order for all inventions to be examined, the appropriate additional examination fee must be paid.

Group I: Claims 1-8 are directed towards a cathodic protection test station, comprising: a mounting tube; an input/output terminal; a transducer assembly; a corrosion rate; a reference electrode; a wire; and an impressed current cathodic protection system.

Group II: Claims 9-16 are directed towards a corrosion monitoring system, comprising: a corrosion coupon probe; processing means for producing an excitation pulse; a transmitted pulse; sacrificial coupon material thickness; and memory means.

The inventions listed as Groups I and II do not relate to a single general inventive concept under PCT Rule 13.1 because, under PCT Rule 13.2, they lack the same or corresponding special technical features. Group I has at least a mounting tube; an input/output terminal; a transducer assembly; a corrosion rate; a reference electrode; a wire; and an impressed current cathodic protection system that Group II does not have. Group II has at least a corrosion coupon probe; processing means for producing an excitation pulse; a transmitted pulse; sacrificial coupon material thickness; and memory means that Group I does not have.

The common technical features of Groups I and II are one or more ultrasonic testing (UT) transducers; an acoustic couplant; a sacrificial coupon; and an electromagnetic field.

These common features are disclosed by US 2009/0039864 A1 to GORDON, G. (hereinafter "Gordon") which discloses one or more ultrasonic testing (UT) transducers (SAW-based sensor tag 12 comprising an input and output interdigital transducers 18, 26; figure 1; paragraph [0017]); an acoustic couplant (elastic wave travels down SAW filter 24 to couple wave to ER sensor 34 as shown; figure 1; paragraph [0017]); a sacrificial coupon (layers of material 52, 54 subject to corrosion for purposes of sensing via ER sensor 34; figure 3; paragraphs [0021-0022]; claim 2 of Gordon); and an electromagnetic field (RF electrical signal is received at input transducer 18 and transmitted at output transducer 26 as shown; figure 1; paragraph [0017]).

Since the common technical features are previously disclosed by the Gordon reference, these common features are not special and so Groups I and II lack unity.