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MOTOR VEHICLE ON THE BASIS OF A
SINGLE-PHASE POWER SUPPLY
NETWORK, AND METHOD OF
CONTROLLING THE DEVICE****Publication Classification**(51) **Int. Cl.****B60L 11/18**

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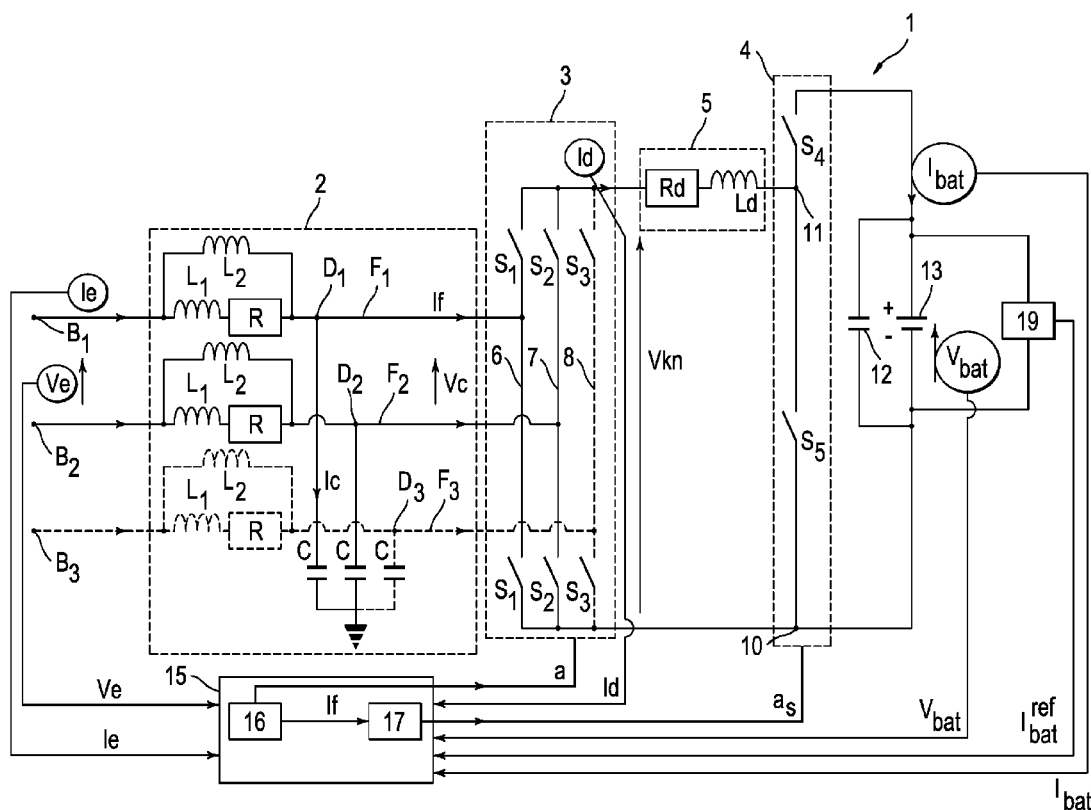
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Mar. 25, 2014, now Pat. No. 9,469,204, filed as
application No. PCT/FR12/50806 on Apr. 12, 2012.**Foreign Application Priority Data**

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(57)

ABSTRACT

A device for charging a battery, in particular a battery of an electric traction motor vehicle, on the basis of a single-phase power supply network, including a filtering stage intended to be connected to the single-phase network, a voltage step-down stage connected to the filtering stage, a voltage step-up stage intended to be connected to the battery and coupled to the voltage step-down stage via an inductive component such as an induction coil, a regulating unit able to impose chopping duty ratios on the voltage step-down stage and on the voltage step-up stage. The regulating unit includes means for compensating for the phase shift between the input current of the voltage step-down stage and the input voltage of the voltage step-down stage.



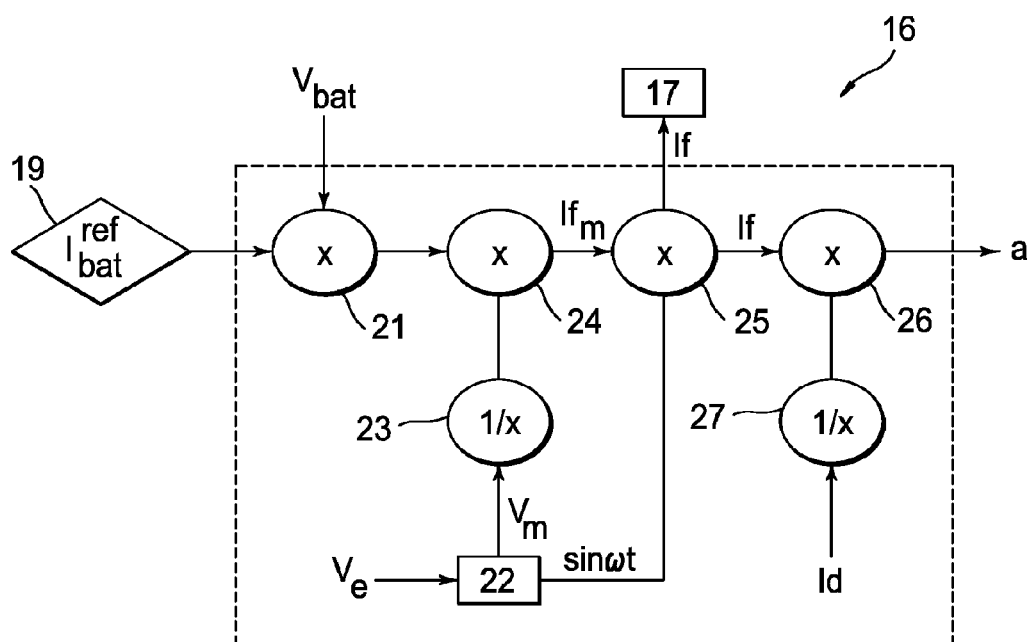


FIG. 2A

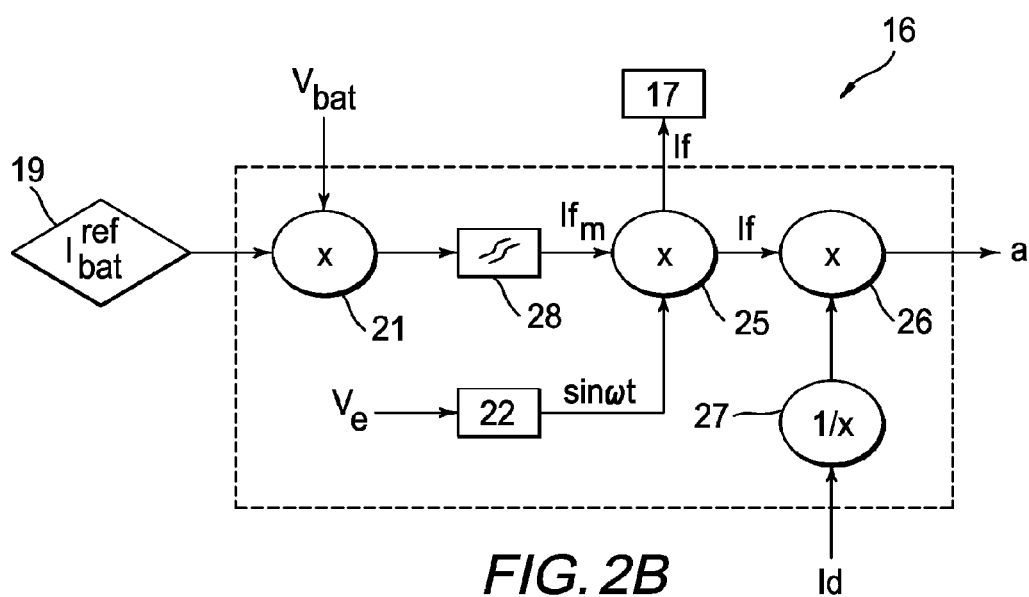


FIG. 2B

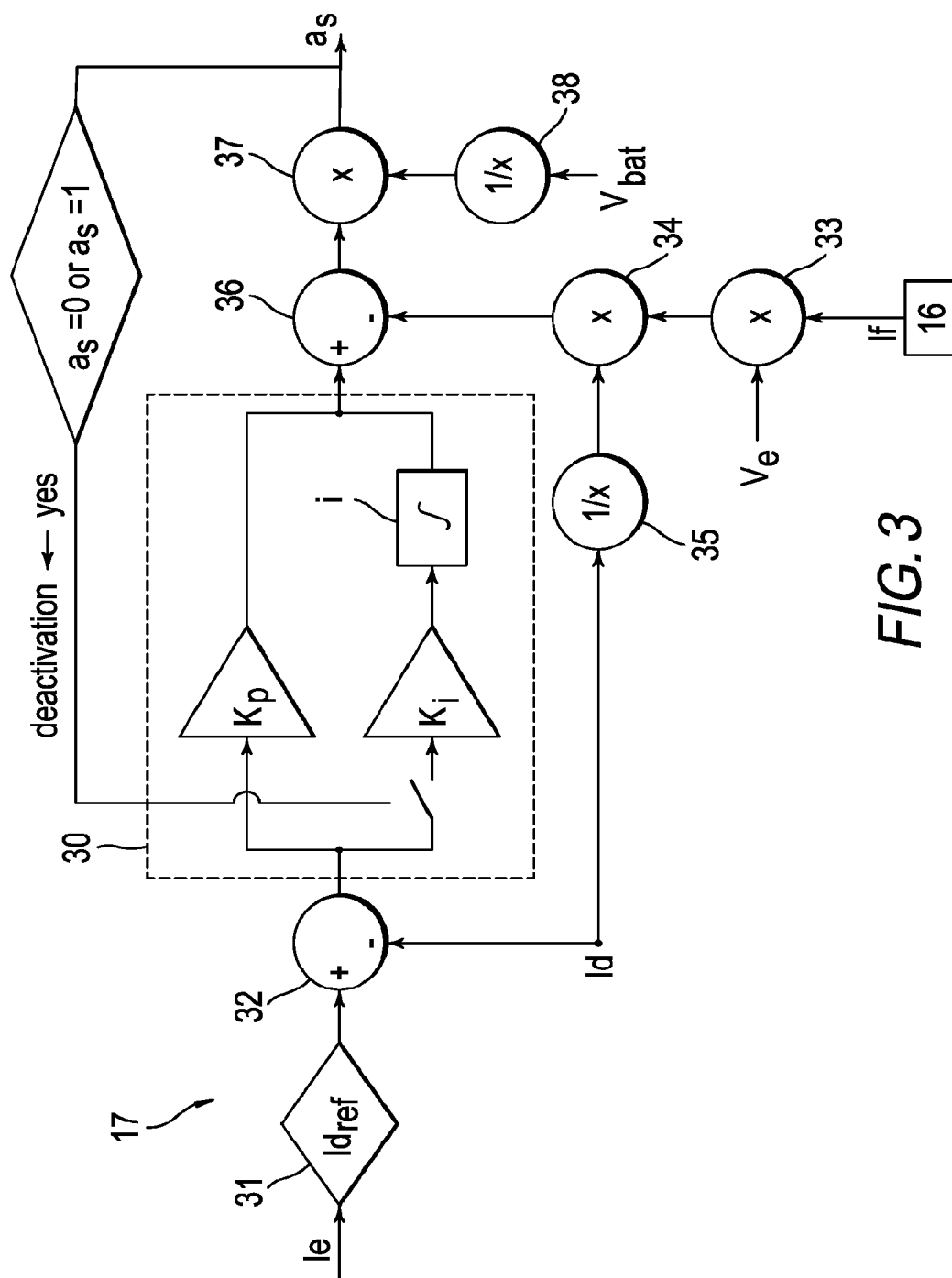


FIG. 3

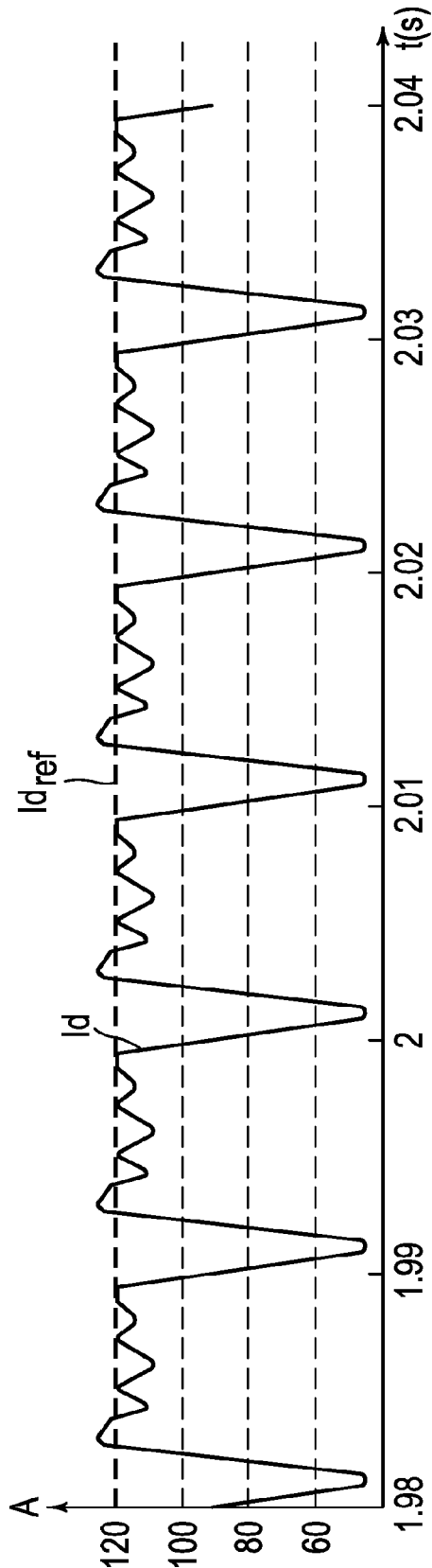


FIG. 4

**DEVICE FOR CHARGING A BATTERY OF A
MOTOR VEHICLE ON THE BASIS OF A
SINGLE-PHASE POWER SUPPLY
NETWORK, AND METHOD OF
CONTROLLING THE DEVICE**

**CROSS-REFERENCE TO RELATED
APPLICATIONS**

[0001] This application is a continuation of U.S. Ser. No. 14/111,925 filed Mar. 25, 2014, which is incorporated herein by reference and which is a National Phase of PCT/FR2012/50806, filed Apr. 12, 2012, which claims priority under 35 U.S.C. 119 from French Application No. 11 01177 filed Apr. 14, 2011.

BACKGROUND OF THE INVENTION

[0002] Field of the Invention

[0003] The invention relates to a high-voltage battery charging device, in particular for an electric-traction motor vehicle, on the basis of a single-phase power supply network.

[0004] In high-voltage battery recharging systems, the electrical power from the network is delivered to the battery successively via two converters: a voltage step-down or “buck” converter and a voltage step-up or “boost” converter. These two converters enable the voltage ratio between the output and input terminals thereof to be decreased or increased by successively opening and closing a series of switches, at a frequency controlled as a function of the output current and/or the desired output voltage.

[0005] Description of the Related Art

[0006] Such recharging systems are for example described in patent application FR 2 943 188, which relates to an on-board recharging system for motor vehicles enabling a battery of the vehicle to be recharged from a three-phase or single-phase circuit, the recharging circuit incorporating the coils of an electric machine that also provides other functions such as current generation or vehicle propulsion.

[0007] The chopping of the current drawn from the power supply network induces high-frequency components in the current drawn, i.e. harmonics of an order higher than the fundamental frequency of the distribution network, which is conventionally 50 Hz.

[0008] As the electricity distributor imposes a standard concerning the harmonics of the current drawn, such a recharge system also includes a resistive/inductive/capacitive (RLC) filter at the input of the voltage step-down converter. This filter induces a phase shift between the current and the voltage drawn from the network. This phase shift results in a reactive power flowing through the network that is not drawn by the user and that should ideally be minimized.

[0009] Furthermore, most domestic power supply networks are single-phase power supply networks. A vehicle including a device for recharging a battery from a single-phase power supply can therefore be recharged from a domestic power supply network, for example in a private parking spot or garage.

[0010] Recharging from a single-phase power supply network has some specific features. Depending on the topology thereof, it is not always possible to bring the input current into phase with the network voltage. Moreover, when the input sinusoidal voltage is close to zero, the system becomes

momentarily uncontrollable, which is not very inconvenient if the storage inductance of the electric machine between the voltage step-down converter and the voltage step-up converter is high, because the current in the inductor does not have time to drop, but has the drawback of this inductor being voluminous.

[0011] Furthermore, for the power flow to be continuous, a non-zero current needs to be flowing through the storage inductor of the electric machine between the voltage step-down converter and the voltage step-up converter.

BRIEF SUMMARY OF THE INVENTION

[0012] The aim of the invention is to propose a device for controlling the voltage step-down converter and the voltage step-up converter of such a recharging device that enables a reduced phase angle to be maintained between the current and the voltage drawn from the single-phase power supply network, despite the presence of an RLC filter at the device input.

[0013] Another aim of the invention is to propose an on-board recharging device for a motor vehicle that can be connected to an external single-phase power supply network and that incorporates the winding of an electric machine of the vehicle in the circuit thereof.

[0014] According to one aspect, one embodiment proposes a device for charging a battery, in particular a battery of an electric-traction motor vehicle, from a single-phase power supply network, comprising a filtering stage intended to be connected to the single-phase network, a voltage step-down stage connected to the filtering stage, a voltage step-up stage intended to be connected to the battery and coupled to the voltage step-down stage via an inductive component such as an inductance coil, a control unit able to impose chopping duty cycles on the voltage step-down stage and the voltage step-up stage.

[0015] According to a general feature, the control unit includes means for compensating for the phase shift between the input current of the voltage step-down stage and the input voltage of the voltage step-down stage.

[0016] Advantageously, the control unit includes a first open-loop control module able to determine a chopping duty cycle of the voltage step-down stage as a function of the voltage of the single-phase power supply network, a setpoint power, and the intensity of the current flowing through the inductance coil, to compensate for the phase shift between the input current of the voltage step-down stage and the input voltage of the voltage step-down stage, and to control the power received by the battery as a function of the setpoint power.

[0017] The first control module may advantageously include a map providing the amplitude of the input current of the voltage step-down stage as a function of the amplitude of the input voltage and of the setpoint power.

[0018] Preferably, the control unit includes a second control module able to determine a chopping duty cycle of the voltage step-up stage as a function of the voltage at the output of the voltage step-down stage, the voltage of the battery, and the difference between the setpoint induction intensity and the intensity of the current flowing through the inductance coil, providing closed-loop control of the intensity of the current flowing through the battery.

[0019] The setpoint induction intensity is preferably always greater than the intensity flowing through the battery, and the intensity flowing through the inductance coil.

[0020] Advantageously, the second control module includes a proportional-integral controller to which is sent the difference between the intensity of the current flowing through the inductance coil and the setpoint inductance intensity, and overspeed protection means designed to deactivate the integral part of the controller if the chopping duty cycle determined by the second module is approximately equal to "0" or "1".

[0021] According to another aspect, the invention proposes a motor vehicle with at least partial electrical traction including an electric machine coupled to the drive wheels and an inverter stage able to power the electric machine.

[0022] According to a general feature, said vehicle includes a device for charging a battery from a single-phase network as described above, the electrical connections and a switch of the voltage step-up stage of said device being included in the inverter stage, and the inductance coil of said device corresponding to the windings of said electric machine.

[0023] According to another aspect, one embodiment proposes a method for controlling the charging of a battery, in particular a battery of a motor vehicle, from a single-phase network, in which the input voltage is filtered, the electrical power is taken from the network to the battery via a voltage step-down stage and a voltage step-up stage coupled via an inductive component such as an inductance coil.

[0024] According to a general feature, the phase shift between the input current of the voltage step-down stage and the input voltage of the voltage step-down stage is compensated.

[0025] Preferably, the input current of the voltage step-down stage is controlled by means of the open-loop control of a chopping duty cycle of the voltage step-down stage as a function of the voltage of the single-phase power supply network, a setpoint power, and the intensity of the current flowing through the inductance coil, to compensate for the phase shift between the input current of the voltage step-down stage and the input voltage of the voltage step-down stage, and to control the power received by the battery as a function of the setpoint power.

[0026] The intensity of the current flowing through the battery can also be set to a reference battery intensity by setting, in a closed loop, a chopping duty cycle of the voltage step-up stage as a function of the voltage at the output of the voltage step-down stage, the voltage of the battery, and the difference between the setpoint induction intensity and the intensity of the current flowing through the inductance coil.

[0027] The integral part of a proportional-integral controller can advantageously be deactivated if the chopping duty cycle is approximately equal to "0" or "1".

BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWINGS

[0028] Other advantages and features of the invention are set out in the detailed description of an embodiment of the invention, which is in no way limiting, and the attached drawings, in which:

[0029] FIG. 1 shows a recharging device according to an embodiment of the invention;

[0030] FIGS. 2a and 2b show respectively first and second embodiments of a first control module;

[0031] FIG. 3 is a schematic view of an embodiment of a second control module;

[0032] FIG. 4 is a graphical representation of the current flowing through the inductance coil.

DETAILED DESCRIPTION OF THE INVENTION

[0033] FIG. 1 shows a schematic view of a device for charging a battery of an electric-traction motor vehicle from a single-phase power supply network, according to one embodiment.

[0034] The recharging device 1 includes a filtering stage 2, a voltage step-down stage 3 coupled to the filtering stage 2, and a voltage step-up stage 4 coupled to the voltage step-down stage 3 via an electric machine 5.

[0035] Since the device 1 can be coupled to a three-phase or single-phase power supply, it has three terminals B₁, B₂, B₃ coupled to the input of the filtering stage 2, and that can be coupled to a power supply network. In single-phase recharging, only the inputs B₁ and B₂ are coupled to a single-phase power supply network delivering an input voltage V_e and an input current I_e.

[0036] Each input terminal B₁, B₂ and B₃ is coupled to a filtering branch of the filtering stage 2. Each filtering branch includes two branches in parallel, one having an inductor of value L₂ and the other having an inductor of value L₁ and a resistor of value R in series.

[0037] The outputs of these two filtering branches are each coupled to a capacitor of capacitance C also coupled to ground, at a point respectively named D₁, D₂, D₃ for each of the filtering branches. The set of resistors of value R, inductors of value L₁ or L₂, and capacitors of capacitance C form an RLC filter at the input of the voltage step-down converter 3.

[0038] In single phase recharging, terminal B₃ is not coupled to the power supply network. Since the filtering branch coupled to terminal B₃ is not used, it is not taken into account in the remainder of the description and is shown using dotted lines. The other elements of the electrical circuit shown using dotted lines are elements that are only used when coupling to a three-phase power supply network.

[0039] The voltage step-down stage 3 is coupled to the filtering stage 2 at points D₁ and D₂. When operating with a single-phase power supply, the voltage step-down converter 3 includes two parallel branches 6 and 7, each having two switches S₁ or S₂ controlled by a control unit 15.

[0040] Each input D₁ or D₂ of the voltage step-down converter is connected, respectively by a branch F₁ and F₂ to a connection point located between two switches S₁ or S₂ of a single branch 6 and 7, respectively.

[0041] The common extremities of the branches 6 and 7 form two output terminals of the voltage step-down converter 3. One of the terminals is linked to the "−" terminal of the battery 13 and to a first input 10 of a voltage step-up converter 4. The other of these terminals is connected to a first terminal of an electric machine 5, the other terminal of which is connected to a second input 11 of the voltage step-up converter 4.

[0042] The voltage step-up converter 4 has two switches S₄ and S₅ that can be controlled by the control unit 15 independently. These two switches S₄ and S₅ are located on a branch connecting the first input 10 of the voltage step-up converter 4 and the "+" terminal of the battery 13. The second input 11 of the voltage step-up converter 4, to which the electric machine 5 is connected, is connected between the two switches S₄ and S₅, the switch S₄ being connected

between the second input 11 and the “+” terminal of the battery 143, and the switch S_5 being coupled between the first input 10 and the second input 11.

[0043] An electric machine 5, similar to a resistor of value R_d placed in series with an inductance coil L_d , is connected between the output terminal of the voltage step-down converter 3 and the second input 11 of the voltage step-up converter 4. The electric machine 5 may be replaced by a non-resistive inductance coil or a supplementary inductance coil may be connected in series with the electric machine 5 without moving outside the scope of the invention.

[0044] The terminals of the battery 13 are connected to a capacitor 12 intended to keep the voltage at the terminals of the battery 13 relatively stable, and a module 19 for monitoring the charge of the battery that is able to deliver a setpoint value I_{bat}^{ref} determining, as a function of the battery charge level, the optimal current intensity to inject via the “+” terminal of the battery 13. The charge monitoring module 19 sends the setpoint value I_{bat}^{ref} to the control unit 15 over a dedicated connection.

[0045] Measurement means, built into the module 19 or otherwise, also send the control unit 15 a value I_{bat} determining a measured current actually entering the battery, and a value V_{bat} determining the voltage between the “-” terminal and the “+” terminal of the battery 13.

[0046] Other current intensity measurement modules make it possible to measure and send to the control unit 15 the value I_d of the current flowing through the electric machine 5, the intensity I_e of the current of the power supply network entering the filtering stage 2, and the input voltage value V_e of the power supply from the network.

[0047] The control unit 15 includes a first control module 16 determining the chopping duty cycle a of the voltage step-down stage 3, and a second control module 17 determining a chopping duty cycle setpoint a_s of the voltage step-up stage 4.

[0048] For this, the control unit 15 includes two pilot modules (not shown), the first to impose a temporal opening and closing pattern for each of the switches of the voltage step-down converter 3 such as to obtain the chopping duty cycle a of the voltage step-down stage 3, and the second to impose a temporal opening and closing pattern for each of the switches S_4 and S_5 of the voltage step-up converter 4 such as to obtain the duty cycle a_s .

[0049] The switches are preferably transistors enabling rapid switching, for example insulated gate bipolar transistors (IGBT).

[0050] When used exclusively in single-phase mode, the switch S_4 between the second input 11 of the voltage step-up converter 4 and the “+” terminal of the battery 13 is always closed and may as a result be replaced by a diode enabling a flow from said second input 11 to the “+” terminal of the battery 13. If the device 1 can be coupled to a single-phase power supply network as well as a three-phase power supply network, a diode can be connected in parallel with the switch S_4 coupled between said second input 11 and the “+” terminal of the battery 13, the diode enabling a flow from said second input 11 to the “+” terminal of the battery 13.

[0051] To assess the duty cycles a and a_s , the control unit 15 receives as input the values of the power supply voltage V_e from the network, the intensity I_d of the current flowing through the electric machine 5, the voltage V_{bat} across the battery 13, the intensity I_{bat} of the current flowing through

the battery 13, and the reference battery intensity I_{bat}^{ref} delivered by the charge monitoring module 19.

[0052] By way of example, the characteristic values of the electrical elements of the charging device 1 are within the following ranges:

[0053] the capacitance values of the filter 2 represent several hundred pF, for example between 100 and 500 μ F each,

[0054] the capacitance 12 between the terminals of the battery 13 used to stabilize the voltage of the terminals is around mF, for example between 1 and 10 mF,

[0055] the resistance values R of the filtering circuit 2 are around one ohm, for example between 1 and 10 Ω ,

[0056] the resistance R_d of the rotor of the electric machine M_e is around several tens of m Ω , for example between 0.01 Ω and 0.1 Ω ,

[0057] the inductance values L_1 , L_2 , L_d corresponding respectively to the inductors of the filtering stage 2 and the winding of the electric machine 5, have values of around several tens of μ H, for example between 10 μ H and 100 μ H.

[0058] Using the first control module 16 and the second module 17, the control unit prepares chopping duty cycle setpoint values a and a_s for the voltage step-down converter 3 and for the voltage step-up converter 4, satisfying the following three objectives:

[0059] controlling the amplitude of the input current I_f of the voltage step-down stage 3 and ensuring that this current I_f is in phase with the input voltage V_e (this control minimizes the phase shift between the input current I_f of the voltage step-down stage 3 and the input voltage V_e of the voltage step-down stage 3), thereby controlling the power drawn as a function of the power supply network,

[0060] obtaining a measured input current I_{bat} at the “+” terminal of the battery 13, corresponding to the power supply needs of the battery 13, these needs being determined by the charge monitoring module 19 and delivered as the I_{bat}^{ref} function to the control unit 15,

[0061] preventing elimination of the current I_d flowing through the inductance coil L_d of the electric machine 5 so as not to generate unwanted harmonics in the current drawn from the network.

[0062] Since the voltage drop in the filtering stage 2 is negligible for the power range used, the equations of the input filter need not be described.

[0063] The voltage V_c at the input of the voltage step-down stage 3 is deemed to be equal to the input voltage V_e of the power supply network.

[0064] The output voltage V_{kn} of the voltage step-down stage 3 is $a \cdot V_e$. As it is equal to $a \cdot V_e$, the equation of the branch bearing the electric machine 5 can be written in the following form:

$$R_d \cdot Id + L_d \cdot s \cdot Id = a \cdot V_e - a_s \cdot V_{bat} \quad (\text{equation 1})$$

where s is the derivative operator in relation to time “ t ”, or

$$\frac{d}{dt} = s,$$

a is the chopping duty cycle of the voltage step-down stage 3, a_s the duty cycle of the voltage step-up stage 4.

[0065] The chopping duty cycle a of the voltage step-down stage 3 can also be written $a=I_f/I_d$, where I_f is the input current in the voltage step-up stage 3, and the chopping duty cycle a_s of the voltage step-up stage 4 is given by $a_s=I_{bat}/I_d$.

[0066] The equation (1) can therefore also be written in the following form:

$$Rd \cdot Id + Ld \cdot s \cdot Id = (If \cdot Ve - I_{bat} \cdot V_{bat}) / Id \quad (\text{equation 2})$$

or:

$$Rd \cdot Id^2 + \frac{Ld}{2} \cdot s \cdot Id^2 = If \cdot Ve - I_{bat} \cdot V_{bat} \quad (\text{equation 3})$$

[0067] According to equation 3, the intensity I_f of the input current of the voltage step-down stage 3 can therefore be used as a control variable to lock the current I_d flowing through the electric machine 5 to a setpoint value I_d^{ref} prepared such as to prevent the elimination of the current in the inductance coil Ld .

[0068] If the input voltage Ve approaches zero, the system becomes uncontrollable, even if it is locked. According to the equations, during these uncontrollable phases, the current I_d in the coil Ld of the electric machine 5 can only drop, as shown in FIG. 4.

[0069] Dividing the value of the intensity I_f of the input current of the voltage step-down stage 3 by the value of the intensity I_d of the current measured through the electric machine 5 by definition gives the value of the chopping duty cycle a of the voltage step-down stage 3. Controlling the voltage step-down stage 3 using the chopping duty cycle setpoint a makes it possible to lock the power supply current I_e of the network to a zero reference, in order to eliminate the phase shift between the current and the voltage at the input of the voltage step-down stage 3, and to lock the current I_d flowing through the electric machine 5 to the desired setpoint value, i.e. the setpoint induction intensity I_d^{ref} .

[0070] The input voltage V_c of the voltage step-down stage 3, equal to the input voltage Ve of the power supply network, takes the form $V_c=Ve=V_m \sin(\omega t)$.

[0071] The command guarantees that I_f is in phase with the input voltage. The input current I_e is given by $I_e=I_f+I_c$, i.e. $I_e=I_{fm} \sin(\omega t)+C/2 V_m \cos(\omega t)$.

[0072] The current I_f is therefore an image of the active power taken from the network. This latter is given by the relationship $P_{active}=I_{fm} V_m/2$, where $I_{fm}=2 P_{active}/V_m$.

[0073] If the input current I_e is controlled by the input current I_f of the voltage step-down stage 3 to eliminate the phase shift, and the current I_d flowing through the electric machine 5 is controlled by the input current I_f of the voltage step-down stage 3 to prevent elimination of current in the coil Ld of the electric machine 5, then the third objective of the control provided by the control unit 15 relating to locking the input current in the battery I_{bat} to the setpoint value I_{bat}^{ref} delivered by the charge monitoring module 19 remains to be fulfilled.

[0074] To do so, a chopping duty cycle a_s can for example be applied to the voltage step-up converter such as to satisfy the relationship $a_s=I_{bat}^{ref}/I_d$.

[0075] The relationship determining the dynamic of the current through the electric machine 5, given by the equation

(1), directly links the duty cycle a_s of the voltage step-up stage 4 and the current I_d flowing through the electric machine 5.

[0076] It is therefore possible to control a_s directly from the error between the reference value I_d^{ref} and the measured value I_d flowing through the electric machine 5.

[0077] FIG. 2a is a schematic view of a first embodiment of the first control module 16. The first control module includes open-loop control of the input current I_f of the voltage step-down stage 3. The input current I_f of the voltage step-down stage 3 is controlled by calculating the chopping duty cycle a of the voltage step-down converter 3.

[0078] The chopping duty cycle a of the voltage step-down stage 3 is determined as a function of the setpoint power P_{bat}^{ref} , determined from the voltage of the battery V_{bat} and the setpoint battery intensity I_{bat}^{ref} , the input voltage Ve of the single-phase power supply network and the intensity I_d of the current flowing through the inductance coil Ld .

[0079] The first control module 16 receives the battery intensity setpoint I_{bat}^{ref} at a first input and the voltage measured at the terminals of the battery V_{bat} at a second input. The setpoint intensity of the battery I_{bat}^{ref} and the voltage V_{bat} of the battery are inputted to a first multiplier 21 which then outputs the setpoint power P_{bat}^{ref} .

[0080] At a third input, the control module 16 receives the input voltage Ve from the power supply network. The module 16 includes a signal analyzer 22 enabling the standardized amplitude signal V_m proportional to the input voltage Ve of the single-phase power supply network to be extracted. The amplitude signal V_m is delivered to a first reversing switch 23 that outputs the reverse of the amplitude V_m . The reverse V_m of this amplitude is delivered to a second multiplier 24 that also receives as an input the setpoint power P_{bat}^{ref} .

[0081] The second multiplier 24 then outputs the amplitude I_{fm} of the input current of the voltage step-down stage 3 to a third multiplier 25, which also receives as an input the phase signal $\sin(\Omega t)$ of the input voltage Ve of the single-phase power supply network.

[0082] The third multiplier 25 then outputs the input current I_f of the output voltage step-down stage 3, firstly to the second control module 17 and secondly to a fourth multiplier 26. The module 16 receives, via a fourth input, the value I_d of the intensity of the current flowing through the coil Ld of the electric machine 5. The value I_d of the current flowing through the coil Ld is delivered to a second reversing switch 27 that outputs the reverse of the intensity I_d of the current flowing through the coil Ld to the fourth multiplier 26.

[0083] The fourth multiplier 26 then performs the calculation I_f/I_d and outputs the value of the chopping duty cycle a of the voltage step-down stage 3, enabling the input current I_f of the voltage step-down stage 3 to be controlled.

[0084] FIG. 2b shows a second embodiment of the first control module 16.

[0085] In this module 16, the second multiplier 24 has been replaced by a map 28 delivering the amplitude I_{fm} of the input current I_f of the voltage step-down stage 3 as a function of the amplitude V_m of the input voltage Ve and of the setpoint power P_{bat}^{ref} .

[0086] FIG. 3 shows an embodiment of the second control module 17.

[0087] In the charging device 1, the current I_{bat} flowing through the battery 13 is controlled by the voltage step-up stage 4. Indeed the current I_{bat} of the battery is given by the relationship $I_{bat}=a_s I_d$.

[0088] Thus, the current I_{bat} in the battery 13 can simply be locked to the related reference value with $a_s=I_{bat}^{ref}/I_d$.

[0089] It is also possible to add a correction loop if the current measurement of the battery is available. In this case, the following is obtained:

$$a_s = \frac{1}{I_d} \cdot \{I_{bat}^{ref} + \alpha \cdot (I_{bat}^{ref} - I_{bat})\} \quad (\text{equation 4})$$

where α is a setting parameter.

[0090] The second control module 17 includes closed-loop control of the intensity I_d of the current flowing through the inductance coil L_d of the electric machine 5.

[0091] The second control module 17 receives, at a first input, a value I_e of the input intensity of the power supply network. This intensity value I_e is delivered to a module 31 determining the value of the setpoint induction intensity I_d^{ref} . The second control module 17 receives, at a second input, the value I_d of the intensity of the current flowing through the coil L_d of the electric machine 5. The value I_d of the intensity is delivered to a negative input of a first subtracter 32 that receives at a positive input the value I_d^{ref} of the setpoint induction intensity.

[0092] The first subtracter 32 then outputs the difference between the intensity I_d of the current flowing through the inductance coil L_d and the setpoint induction intensity I_d^{ref} to a proportional/integral controller 30.

[0093] The proportional/integral controller 30 includes two branches in parallel, the first of which includes a proportional control module K_p and the second includes an integral control module K_i and an integration module i .

[0094] The second control module 17 receives, at a third input, the value I_f of the intensity of the input current of the voltage step-down stage 3 delivered by the first control module 16. The intensity I_f is delivered to a first multiplier 33, which also receives as input the input voltage V_e of the single-phase network received at a fourth input of the second control module 17.

[0095] The first multiplier 33 thus outputs a value P_{active} of the active power. This value P_{active} is inputted to a second multiplier 34 that also receives as input the reverse of the current I_d , the current I_d having previously been delivered to a first reversing switch 35.

[0096] The second multiplier 34 performs the calculation P_{active}/I_d and outputs a value V_{kn} of the output voltage of the voltage step-down stage 3. The voltage V_{kn} of the voltage step-down stage 3 is delivered to a positive input of a second subtracter 36 that receives on a negative input the output from the proportional/integral controller 30.

[0097] The second subtracter 36 then outputs the sum of the difference between the intensity I_d of the current flowing through the inductance coil L_d and the setpoint induction intensity I_d^{ref} corrected by the proportional/integral controller 30, with the output voltage V_{kn} of the voltage step-down stage 3 at the input of a third multiplier 37. The third multiplier 37 also receives as input the reverse of the battery voltage V_{bat} , the battery voltage V_{bat} having been received at a fifth input of the second control module and delivered in advance to a second reversing switch 38.

[0098] The third multiplier 37 then outputs the setpoint value of the chopping duty cycle a_s of the voltage step-up stage 4.

[0099] The second control module 17 also includes a feedback loop between the output of the third multiplier 37 and the input of the branch of the proportional/integral controller 30 containing the integral control module K_i .

[0100] If the value of the chopping duty cycle a_s of the voltage step-up stage 4 is approximately 0 or 1, the integral control branch is deactivated.

[0101] This feedback loop is an overspeed protection technique used to overcome the loss of control of the device when the input voltage V_e approaches zero. Indeed during uncontrollable phases, control is saturated, i.e. the duty cycles of the switches, or IGBT transistors, are at 1, as it is not able to reduce the difference. To prevent this error from continuing to be integrated, the feedback loop is used. Accordingly, once the device can be controlled, the current I_d flowing through the coil L_d of the electric machine 5 is brought to the reference value I_d^{ref} .

[0102] The use of this feedback loop also makes it possible to control a system that has a very-low-inductance coil L_d . The use of a low-inductance coil makes it possible to reduce the volume of the charger.

[0103] The invention provides an on-board charging device for a motor vehicle designed to be connected to an external single-phase power supply network, incorporating within its circuit the winding of an electric machine of the vehicle, and making it possible to control the voltage step-down converter and the voltage step-up converter such as to maintain a reduced phase shift between the current and the voltage drawn from the single-phase power supply network.

1. A device for charging a battery (13), in particular a battery of an electric-traction motor vehicle, from a single-phase power supply network, comprising a filtering stage (2) intended to be connected to the single-phase network, a voltage step-down stage (3) connected to the filtering stage (2), a voltage step-up stage (4) intended to be connected to the battery (13) and coupled to the voltage step-down stage (3) via an inductive component (L_d) such as an inductance coil, a control unit (15) able to impose chopping duty cycles (a_s) on the voltage step-down stage (3) and the voltage step-up stage (4),

characterized in that the control unit (15) includes means for compensating for the phase shift between the input current (I_f) of the voltage step-down stage (3) and the input voltage (V_e) of the voltage step-down stage (3),

the control unit (15) including a first open-loop control module (16) able to determine a chopping duty cycle (a_s) of the voltage step-down stage (3) as a function of the voltage (V_e) of the single-phase power supply network, a setpoint power (P_{bat}^{ref}), and the intensity (I_d) of the current flowing through the inductive component (L_d), to compensate for the phase shift between the input current (I_f) of the voltage step-down stage (3) and the input voltage (V_e) of the voltage step-down stage (3), and to control the power (P_{bat}) received by the battery as a function of the setpoint power P_{bat}^{ref} ,

the control unit (15) including a second control module (17) able to determine a chopping duty cycle (a_s) of the voltage step-up stage (4) as a function of the voltage (V_{kn}) at the output of the voltage step-down stage (3), the voltage (V_{bat}) of the battery (13), and the difference between the setpoint induction intensity (I_d^{ref}) and the

intensity (I_d) of the current flowing through the inductive component (L_d), providing closed-loop control of the intensity (I_{bat}) of the current flowing through the battery (13).

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