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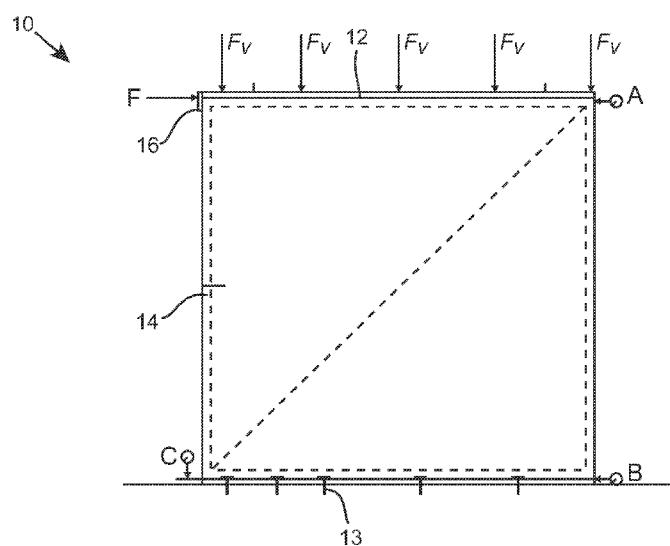


Fig. 1

(57) Abstract: A partition for a building structure comprises a support frame and a plasterboard affixed to the support frame. The support frame comprises a plurality of elongate timber members. The plasterboard comprises a gypsum matrix having fibres embedded therein in an amount of at least 1 wt% relative to the gypsum, as well as a polymeric additive that is present in an amount of at least 1 wt% relative to the gypsum.

IMPROVEMENTS IN THE DEFORMATION RESISTANCE OF TIMBER FRAME PARTITIONS

Field of the invention

The present invention relates to timber frame-based partitions having improved resistance to

5 deformation, in particular to partitions having improved resistance to wind loading.

Background to the invention

Gypsum sheathing boards are often less preferred for use in timber frame construction,

because they do not provide the structure with sufficient resistance to wind loading to meet

10 regulatory requirements. Therefore, other boards such as oriented strand board and

plywood have previously been used.

Resistance to wind loading is generally characterised through the racking strength of the

board, that is, the ability of the board to resist shear loading in the plane of the board.

15 Racking strength is difficult to predict, as it does not correlate closely with other mechanical parameters.

It is desirable to provide gypsum-based boards having improved racking strength, such that they may be used in timber frame construction.

20

Summary of the invention

It has been found that gypsum-based plasterboard containing high levels of fibre and at least one polymeric additive have increased levels of racking resistance.

25 Therefore, in a first aspect, the present invention may provide a partition for a building structure, the partition comprising a support frame and at least one plasterboard affixed to the support frame, wherein:

the support frame comprises a plurality of elongate timber members; and
the plasterboard comprises a gypsum matrix having fibres embedded therein in an
amount of at least 1 wt% relative to the gypsum, the gypsum matrix further comprising a
polymeric additive that is present in an amount of at least 1 wt% relative to the gypsum.

5

Preferably, the fibres are present in an amount of at least 3 wt% relative to the gypsum,
more preferably in an amount of at least 5 wt% relative to the gypsum.

Preferably, the polymeric additive is present in an amount of at least 3 wt% relative to the
10 gypsum, more preferably in an amount of at least 5 wt% relative to the gypsum.

It has been found that the use of relatively short fibres helps to promote an even distribution
of fibres throughout the board, which has a beneficial effect on racking resistance. Thus, it is
preferred that the fibre length is less than 20mm, preferably less than 15mm, more
15 preferably less than 10mm. The fibre length is preferably greater than 1mm. Preferably, the
fibres are glass fibres.

Preferably, the plasterboard is provided with a backing lamina such as a fibreglass sheet.

20 The lamina represents a layer that provides a discrete component of the panel, that is, it is
not integrally formed with the substrate. Effectively, there is a well-defined interface or
boundary between the substrate and the lamina.

Typically, the lamina has a thickness of at least 0.25 mm, preferably at least 0.5 mm, more
25 preferably at least 1 mm. Typically, the thickness of the lamina is less than 4 mm, preferably
less than 3 mm, more preferably less than 2.5 mm.

In certain cases, the polymeric additive is a starch. In other cases, the polymeric additive is a synthetic polymer such as polyvinyl acetate.

Typically, the racking stiffness of the partition, measured in accordance with British standard

5 BS EN 594:1996 is greater than 1500 N/m, preferably greater than 2000N/m.

The plasterboard is prepared through a process comprising mixing stucco and water to form a stucco slurry, and allowing the slurry to set. Thus, the plasterboard is distinguished from boards such as fibreboard, which are prepared through a process of mixing water, fibres and

10 calcium dihydrate to form a slurry, heating the slurry to calcine the gypsum, removing water from the slurry to form a filter cake, and forming the filter cake into the desired shape prior to the complete setting of the calcined gypsum.

Detailed description

15 The invention will now be described by way of example with reference to the following

Figures in which:

Figure 1 shows a schematic elevation view of a test apparatus for measuring racking resistance.

20

Testing racking resistance of boards

Racking resistance was measured in accordance with British standard BS EN 594:1996.

Referring to Figure 1, a 2400mm high x 2400 mm long test specimen 10 was constructed

25 and placed within the test rig. The test specimen comprised a frame consisting of 90mm x 38mm cross-section timber top and bottom rails, and 90mm x 38mm cross-section timber studs extending therebetween at 600mm intervals. A head binder 12 was rigidly attached to

the top and bottom rails. The test specimen was bolted into the test rig by means of bolts 13 inserted through the bottom rail of the frame.

Plasterboard sheathing 14 was fixed to the frame in a single layer below the head binder.

5 The boards were screw fixed with 41mm British Gypsum drywall timber screws at 300mm intervals around the perimeter of the boards.

In a first loading step, a downward vertical pre-load F_v was applied to the test specimen at the positions of the studs. This load was subsequently removed. In a second loading step,

10 a racking load F was applied horizontally to the top of the test specimen onto a metal plate 16 attached to the top rail of the panel and the head binder. The deformation d of the board was measured as the displacement at transducer A minus the displacement at transducer B.

The racking stiffness is calculated as the ratio of racking load F to the deformation d of the

15 board.

Examples

Example 1

A plasterboard having a gypsum core containing the following additional components:

20

- 3 wt% 6mm glass fibre
- 6 wt% starch (a mixture of Amidon MB065X from Roquette and Coatmaster K57 ethylated starch from Grain Processing Corporation)
- a water-resistant additives: silicone oil and cement
- biocide: sodium omadine

25 The board has a thickness of 12.5 mm and a weight of 12.3 kg/m².

The board has a liner provided by a pre-coated glass mat having a weight of 360 g/m² and a mineral coating.

5 **Example 2**

A plasterboard having a gypsum core containing the following additional components:

- 3wt% of 12mm glass fibre
- 3wt% starch (a mixture of Amidon MB065X from Roquette and Coatmaster K57

10 ethylated starch from Grain Processing Corporation)

The plasterboard has a paper liner on both sides of the board, the liner having a weight of 240 g/m², and additionally a backing lamina provided by a 1.5 mm fibre glass sheet. The total thickness of the composite board (including the gypsum board and the backing lamina) is 15 mm. The total weight of the composite board is 15.6 kg/m².

15

Example 3

A plasterboard having a gypsum core containing the following additional components:

- 3 wt% of 6mm glass fibre; and
- 5 wt% starch (Merifilm starch from Tate & Lyle).

The plasterboard has a paper liner on each side of the board. The weight of the paper liner is 190 g/m² on the side of the board facing away from the support frame and 180 g/m² on the side of the board facing towards the support frame. It is 12.5mm thick product with a weight of approx. 12 kg/m².

25

Comparative example 1

A plasterboard having a gypsum core containing the following additional components:

- 0.5 wt% of 12 mm glass fibres

The board has a liner provided by a pre-coated glass mat. The weight of the board is 11 kg/m².

5 Results

Example	Mean racking stiffness	Mean racking strength	Failure mode
1	2426 N/mm	8726 N	2 studs detached from rail
2	3108 N/mm	14044 N	3 studs detached from rail
3	3652 N/mm	9989 N	2 studs detached from rail
Comparative example 1	1122 N/mm	4666 N	Screws pulled through board

CLAIMS

1. A partition for a building structure, the partition comprising a support frame and at least one plasterboard affixed to the support frame, wherein:
 - the support frame comprises a plurality of elongate timber members; and
- 5 the plasterboard comprises a gypsum matrix having fibres embedded therein in an amount of at least 1 wt% relative to the gypsum, the gypsum matrix further comprising a polymeric additive that is present in an amount of at least 1 wt% relative to the gypsum.
- 10 2. A partition according to claim 1, wherein the fibres are present in an amount of at least 3 wt% relative to the gypsum.
- 15 3. A partition according to claim 1 or claim 2, wherein the polymeric additive is present in an amount of at least 3 wt% relative to the gypsum.
- 5 4. A partition according to claim 3, wherein the polymeric additive is present in an amount of at least 5 wt% relative to the gypsum.
- 20 5. A partition according to any one of the preceding claims, wherein the fibres are present in an amount of about 3 wt% relative to the gypsum and the polymeric additive is present in an amount of about 5 wt% relative to the gypsum.
6. A partition according to any one of the preceding claims, wherein the plasterboard has a backing lamina attached to one of the faces thereof.
- 25 7. A partition according to claim 6, wherein the backing lamina has a thickness greater than 0.5 mm, preferably greater than 1 mm.

8. A partition according to claim 6 or claim 7, wherein the backing lamina is a fibreglass lamina.

9. A partition according to any one of the preceding claims, wherein the fibres are glass fibres.

10. A partition according to claim 9, wherein the fibres have an average length less than 12 mm.

10 11. A partition according to claim 10, wherein the fibres have an average length less than 10 mm.

12. A partition according to any one of the preceding claims, wherein the polymeric additive is a starch.

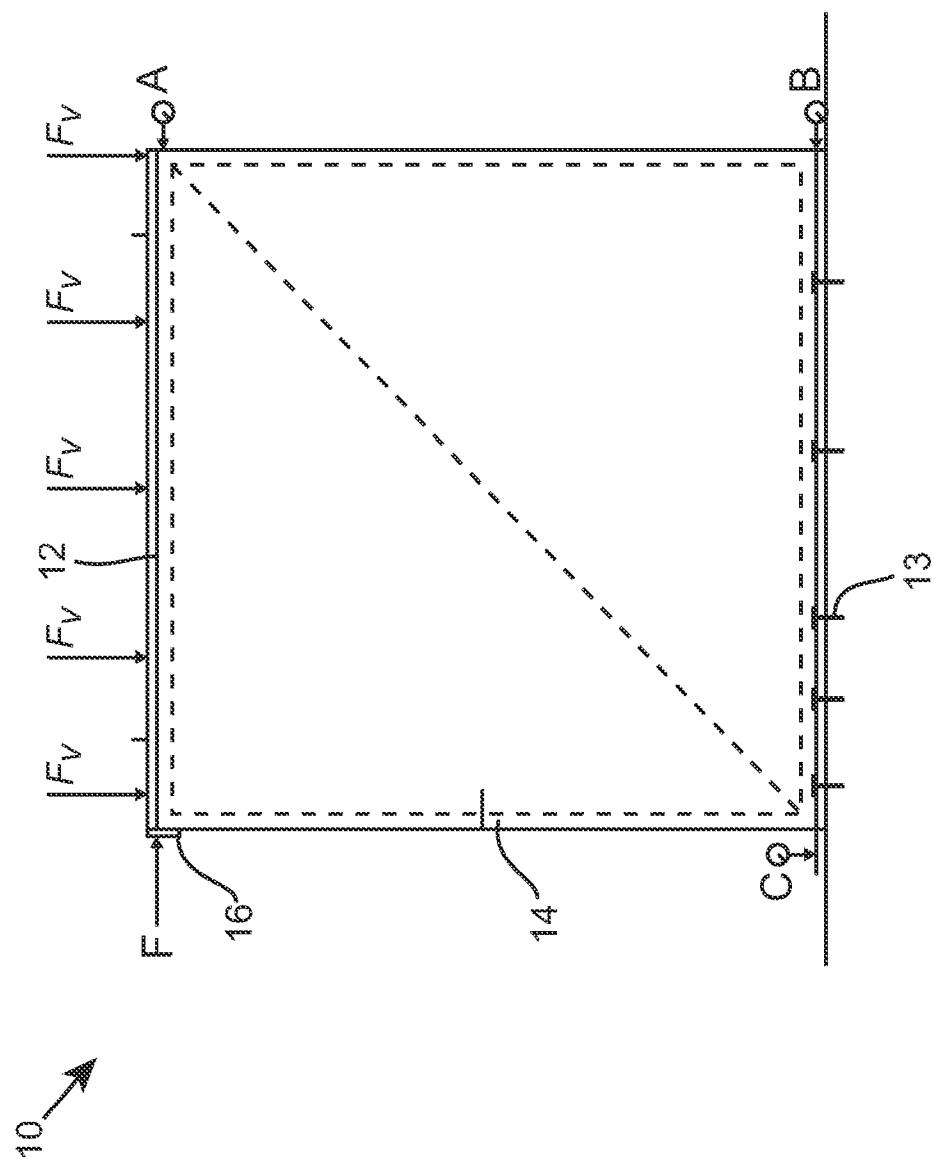
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13. A partition according to any one of claims 1-11, wherein the polymeric additive is polyvinyl acetate.

14. A partition according to any one of the preceding claims having a racking stiffness, 20 measured in accordance with British standard BS EN 594:1996, that is greater than 1500 N/m.

15. A partition according to claim 14, wherein the racking stiffness is greater than 2000 N/m.

Fig. 1



INTERNATIONAL SEARCH REPORT

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A. CLASSIFICATION OF SUBJECT MATTER
INV. C04B28/14 E04C2/04
ADD. C04B111/00

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
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Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	JP 2009 299460 A (YOSHINO GYPSUM CO) 24 December 2009 (2009-12-24) the whole document -----	1-4,9-15
X	WO 2014/138283 A1 (INTELLECTUAL GORILLA B V [NL]) 12 September 2014 (2014-09-12) page 1, line 2 - line 21 page 2, line 28 - page 5, line 6 -----	1-7,9, 12,14,15
X	US 2007/048490 A1 (YU QIANG [US] ET AL) 1 March 2007 (2007-03-01) paragraphs [0008], [0042], [0047]; claims 1,4,21 -----	1,3,4, 6-9,12, 14,15



Further documents are listed in the continuation of Box C.



See patent family annex.

* Special categories of cited documents :

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"&" document member of the same patent family

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INTERNATIONAL SEARCH REPORT

Information on patent family members

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