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## (54) Title: CROSSTALK CALIBRATION FOR MULTI-CHANNEL SYSTEMS

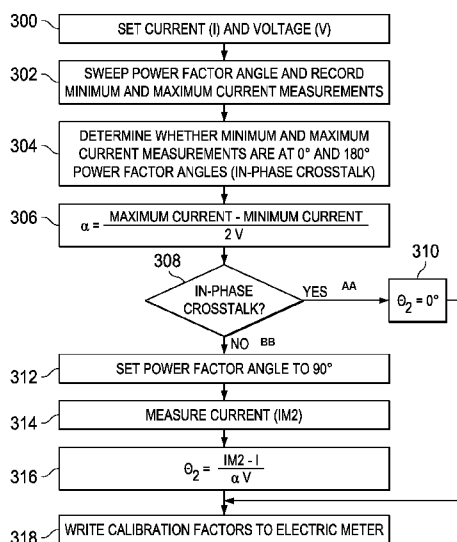


FIG. 6

(57) **Abstract:** In described examples, a system such as an electric meter includes a single-ended analog-to-digital converter, which is susceptible to crosstalk. To calibrate and cancel crosstalk effects, the system determines (308) whether voltage-induced cross-talk is in-phase or out-of-phase with respect to voltage. The system determines a first calibration factor (306) based on minimum and maximum measured current values and voltage. If the cross-talk is in-phase, the system sets (310) a second calibration factor to 0. If the cross-talk is out-of-phase, the system computes (316) the second calibration factor based on a measured current (314) when a power factor angle is set to 90 degrees (312). Calibration factors may be stored (318) in the multi-channel system. In use, the system measures current and voltage and computes the actual current, voltage and power based on the measured current and voltage by employing a crosstalk cancellation technique using the calibration factors.



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## CROSSTALK CALIBRATION FOR MULTI-CHANNEL SYSTEMS

### BACKGROUND

**[0001]** In analog or mixed signal systems when multiple channels of signals are present, crosstalk between the channels can significantly impact signal accuracy. One example of such a mixed signal system is a power metering circuit, which may use analog-to-digital converters (ADCs) to measure voltage and current to compute power. Crosstalk between the voltage and current signal paths greatly affects the accuracy of the power computation. The problem is even more apparent in systems which use single-ended ADCs because such systems include a return ground path that is shared by the multiple channels (e.g., voltage and current). A common return makes the system more susceptible to crosstalk.

### SUMMARY

**[0002]** In described examples, a system such as an electric meter includes a single-ended analog-to-digital converter, which is susceptible to crosstalk. To calibrate and cancel crosstalk effects, the system determines whether voltage-induced cross-talk is in-phase or out-of-phase with respect to voltage. The system determines a first calibration factor based on minimum and maximum measured current values and voltage. If the cross-talk is in-phase, the system sets a second calibration factor to 0. If the cross-talk is out-of-phase, the system computes the second calibration factor based on a measured current when a power factor angle is set to 90 degrees. Calibration factors may be stored in the multi-channel system. In use, the system measures current and voltage and computes the actual current, voltage and power based on the measured current and voltage by employing a crosstalk cancellation technique using the calibration factors.

### BRIEF DESCRIPTION OF THE DRAWINGS

**[0003]** FIG. 1 shows an electric meter circuit in accordance with various examples.

**[0004]** FIG. 2 illustrates an equivalent circuit diagram of the electric meter of FIG.1 in accordance with various examples.

**[0005]** FIG. 3 is a phasor diagram illustrating in-phase crosstalk in accordance with various examples.

[0006] FIG. 4 is a phasor diagram illustrating out-of-phase crosstalk in accordance with various examples.

[0007] FIG. 5 shows the electric meter coupled to a test system to perform a calibration process in accordance with various examples.

[0008] FIG. 6 is a method for calibrating the electric meter in accordance with various examples.

[0009] FIG. 7 is a method performed by the electric meter in the field to compensate measured current based on calibration factors determined during the calibration process in accordance with various examples.

[0010] FIG. 8 is an example of a voltage sensing circuit usable in the electric meter of FIG. 1.

[0011] FIG. 9 is an example of a current sensing circuit usable in the electric meter of FIG. 1.

#### DETAILED DESCRIPTION OF EXAMPLE EMBODIMENTS

[0012] In this description, the term “couple” or “couples” means either an indirect or direct wired or wireless connection. For example, if a first device couples to a second device, that connection may be through a direct connection or through an indirect connection via other devices and connections.

[0013] As described hereinabove, crosstalk between channels in a multichannel system may detrimentally impact signal measurement accuracy, especially in systems that use single-ended ADCs. The embodiments described herein provide a calibration technique that addresses this issue thereby permitting single-ended ADCs to be used in a low cost solution for data acquisition. An example of such an embodiment is provided hereinbelow in the context of an electric meter, but the principles may apply to other types of multichannel systems.

[0014] FIG. 1 shows a block diagram of an electric meter 100 in accordance with various embodiments. The illustrative meter 100 receives with two input signals, voltage and current. The circuit 100 comprises a voltage sensor 102, a current sensor 104, a voltage amplifier 106, a current amplifier 108, and an ADC 110. The electric meter 100 employs a multi-channel, single-ended ADC 110, which means that a return ground path 111 is shared between the voltage and current channels. As viewed from the voltage amplifier 106, the ADC 110 has an input impedance designated as  $Z_v$ . Similarly, as viewed from the current amplifier 108, the ADC 110 has an input impedance designated as  $Z_i$ .

[0015] The gain of each of the voltage and current paths may differ from its nominal value due to factors such as component variations. Such variations will cause gain error. One fixed gain

calibration generally may be sufficient to compensate for the gain error. Each path may also introduce certain amount of phase delay from the sensors 102, 104 to the respective ADC input and cause phase error. The phase error can be calibrated using reference signals. The calibrated gain and phase delay are static (constants) and are used in digital processing during normal operation to compensate for gain and phase errors. For traditional electric meters where high precision ADCs (such as differential ADCs) are used, the crosstalk between signals can generally be controlled to a minimum through careful board layout, and the static gain and phase calibrations are generally sufficient to ensure power measurement accuracy.

**[0016]** However, for electric meter applications where low cost single-ended ADCs are desired, significant crosstalk persists due to the common return path of multiple signals. The gain and phase calibration techniques described hereinabove are not sufficient when crosstalk is present in the circuit for the following reasons. First, crosstalk varies with the load. Second, the effect of crosstalk also depends on the phase angle between voltage and current (i.e., the power factor angle). Because crosstalk varies depending on load and power factor, the error crosstalk introduces cannot be corrected by traditional static gain and phase calibration.

**[0017]** FIG. 2 illustrates a circuit schematic model of the electric meter 100 of FIG. 1. As described hereinabove, the electric meter employs a common ground architecture. Albeit likely small, the common ground path has an impedance designated as  $Z_{GND}$  in FIG. 2. The voltage  $V$  and current  $I$  represent the voltage and current signal outputs, respectively, from the voltage and current amplifiers 106, 108. The schematic of FIG. 2 illustrates that the voltage signal will be coupled onto the current signal through  $Z_{GND}$ , and vice versa. Even with a carefully designed board layout, impedance will always be in the common return path. At low frequencies, the ground impedance,  $Z_{GND}$ , tends to behave like a pure resistive load.

**[0018]** FIG. 3 is a phasor diagram illustrating the effect of crosstalk of voltage on current. FIG. 3 shows the voltage and current vectors  $V$  and  $I$  (illustrated in solid line). The angle ( $\Theta_1$ ) between the vectors represents the phase difference between voltage and current and also may be referred to as the power factor angle. The vector designated as  $\alpha V$  represents the crosstalk from voltage on current. The crosstalk may be in-phase or out-of-phase with respect to voltage  $V$ . FIG. 3 illustrates in-phase cross-talk and FIG. 4 (described hereinbelow) illustrates out-of-phase crosstalk.

**[0019]** Referring still to FIG. 3, the crosstalk factor  $\alpha$  may be positive or negative, and thus the in-phase crosstalk  $\alpha V$  may have a phase angle with respect to voltage  $V$  of 0 degrees or 180

degrees. FIG. 3 shows an example in which  $\alpha$  is negative. Out-of-phase crosstalk (FIG. 4) means that  $\alpha V$  is at an angle other than 0 or 180 degrees with respect to voltage  $V$ . The amount of crosstalk will likely be much smaller than the amount of current  $I$ , that is  $\alpha V \ll I$ , because  $Z_{GND}$  is generally small.  $Z_{GND}$  is also fixed when the board containing the components of the electric meter 100 is made, which means that  $\alpha$  is a constant. In electric meter applications, the voltage  $V$  tends to stay the same because the power line voltage usually does not change. Due to the effect of  $\alpha V$ , the current detected at the ADC 110 is different than  $I$ . In FIG. 3, the ADC measured current is designated as  $I_m$ . Accordingly, the current sensor 104 generates a current  $I$ , but the ADC 110 digitizes a current  $I_m$  which results from the crosstalk  $\alpha V$  generated by the voltage signal path. Moreover, the embodiments described herein provide a technique to calibrate the electric meter so as to permit a calculation by the meter of  $I$  from a measurement of  $I_m$ .

**[0020]** The crosstalk can be easily cancelled or compensated by subtracting  $\alpha V$  from  $I_m$  to recover  $I$  if  $\alpha V$  is known. The purpose of the technique described hereinbelow is to compute the crosstalk factor  $\alpha$ . The power factor angle  $\Theta_1$  between  $V$  and  $I$  can be varied as desired. For example, in some embodiments (and as described hereinbelow with respect to FIG. 5), the electric meter 100 can be connected to a test system that can control: the amount of voltage and current provided to the electric meter; and the power factor angle. As the power factor angle varies, so does the angle of  $\alpha V$  with respect to current  $I$ .

**[0021]** As shown in FIG. 3, the  $I_m$  is a minimum at point P2 (at which the power factor angle would be 0 degrees) and a maximum at point P1 (at which the power factor angle would be 180 degrees). Thus, maximum and minimum RMS current  $I_m$  is found by sweeping (using the test system) the power factor angle. If the minimum and maximum values of  $I_m$  coincide with 0 and 180 degree power factor angles, then in-phase crosstalk is present. If the minimum and maximum values of  $I_m$  do not coincide with 0 and 180 degree power factor angles, then out-of-phase crosstalk is present. The value of  $\alpha$  can be computed as:

$$\alpha = \frac{I_m(P1) - I_m(P2)}{2V} \quad (1)$$

where  $I_m(P1)$  is the minimum RMS current measurement recorded by the ADC 110 and  $I_m(P2)$  is the maximum RMS current measurement recorded by the ADC as the power factor angle is swept, and  $V$  is the magnitude of the voltage set by the test system. Accordingly, the test system sets  $V$  and  $I$  and then sweeps the power factor (e.g., from 0 to 360 degrees) while receiving the measured values of current ( $I_m$ ) from the electric meter's ADC. The test system detects the minimum and

maximum  $I_m$  values, computes the difference and divides the difference by twice the voltage  $V$ . For both in-phase and out-of-phase crosstalks, the same approach is used to obtain crosstalk factor  $\alpha$ .

**[0022]** If the crosstalk of voltage on current were purely in-phase, then the computation of  $\alpha$  would be a sufficient calibration factor to fully calibrate the electric meter 100 and cancel the effects of the crosstalk. In the case of in-phase crosstalk, the electric meter 100 measures voltage ( $V$ ) and current ( $I_m$ ), and computes the current without the effect of crosstalk as:

$$I = I_m + \alpha V \quad (2)$$

**[0023]** However, in cases in which crosstalk of voltage on current is out-of-phase with respect to voltage  $V$ , then additional calibration factor is calculated in accordance with some embodiments. FIG. 4 illustrates a scenario in which the coupled impedance  $Z_{GND}$  is not purely resistive. As shown, the  $\alpha V$  vector (solid line) is not aligned with  $V$  (solid line) and has a phase difference of  $\Theta_2$  with respect to  $V$ . The phase difference  $\Theta_2$  is a second calibration factor (in addition to calibration factor  $\alpha$ ) that can be used to calibrate the electric meter in the face of out-of-phase crosstalk of voltage on current. The calibration factor  $\Theta_2$  can be computed by setting the power factor angle (between  $V$  and  $I$ ) to 90 degrees and measuring the resulting current magnitude. The current magnitude is shown in FIG. 4 as  $I_{m2}$  and coincides with point P4 as shown. The value of  $\Theta_2$  is computed as:

$$\Theta_2 = \frac{I_{m2} - I}{\alpha V} \quad (3)$$

**[0024]** With both calibration factors  $\alpha$  and  $\Theta_2$ , the electric meter can compensate the measured current  $I_m$  as follows:

$$I = I_m + \alpha V e^{\Theta_2} \quad (4)$$

**[0025]** In some embodiments, equation (4) is used to compensate the measured current regardless of whether the crosstalk is in-phase or out-of-phase with respect to voltage  $V$ . If the crosstalk is in-phase,  $\Theta_2$  will be 0. As a result, current compensation equation (4) reduces to equation (2). If the crosstalk is out-of-phase, the test system computes  $\Theta_2$  as described hereinabove and still uses equation (4).

**[0026]** FIG. 5 illustrates the electric meter 100 coupled to a test system 200 during a calibration factor determination process. The process may be performed upon manufacturing of the electric meter or subsequently, but preferably before the meter is used to take voltage and current measurements. The process described hereinbelow may be performed only once or multiple times

during the life of the meter.

**[0027]** The test system 200 includes a voltage and current control 208 which comprises voltage and current generators capable of generating a voltage and a current at magnitudes dictated by the processor 202 and at a power factor angle also dictated by the processor 202. The power factor can be set to a specific value (e.g., 90 degrees) by the test system 200 or swept through a range of values (e.g., 0 to 360 degrees). The test system 200 may be implemented as a computer, custom standalone test device, or as any other type of electronic system. Generally, the test system 200 generates high precision voltage and current source signals which are used to calibrate the electric meter 100.

**[0028]** The electric meter includes the voltage and current sensors 102 and 104, amplifiers 106 and 108, ADC 110, a processor 120, calibration factor storage 122, and a transmitter 124. The ADC 110 may be a component of the processor 120, or may be separate from the processor 120. The processor 120 includes CAL code 125 and meter code 127. The CAL code 125 comprises machine instructions that are executable by the processor 120 to perform the calibration described herein, and the meter code comprises machine instructions that are executable by the processor 120 to operate the meter during run-time to measure power consumption by the user of the meter. The power computation results of the electric meter 200 can be transmitted to the test system 200 via the transmitter 124. The test system 200 can verify and report the accuracy of the electric meter's power computations. The computed calibration factors (e.g.,  $\Theta_2$  and  $\alpha$ ) are computed by the processor 120 during execution of CAL code 125 and stored in CAL factor storage 122 for subsequent use during runtime by execution of the meter code 127.

**[0029]** The digital output of the ADC 110 can be provide to the processor 120, and the processor 120 can access the calibration factor storage 122 to store the computed  $\alpha$  and  $\Theta_2$  calibration factors. The processor 120 performs multiple operations. For example, the processor 120 during calibration time, executes calibration code (125) to obtain calibration factors (122); (2) during normal meter operation, compute V, I, power.

**[0030]** In the embodiment of FIG. 5, the calibration code 125 executes in the electric meter to calibration the meter. In other embodiments, the calibration code executes in the test system 200 on a processor contained therein. In this latter embodiment, the test system receives digitized current and voltage measurements from the electric meter, computes the calibration factors, and programs the calibration back into the CAL factor storage 122 in the meter.



**[0031]** FIG. 6 illustrates a flow chart of the calibration process performed by test system 200 and processor 120 in accordance with various embodiments. The operations may be performed in the order shown, or in a different order. Further, two or more of the operations may be performed concurrently, instead of sequentially.

**[0032]** At 300, the test system 200 sets a current (I) and a voltage (V), such as through the voltage and current control 208. The magnitude of I and V may be indicative of typical values seen by electric meters in the field, but generally can be any desired values.

**[0033]** At 302, the method includes sweeping the factor angle and recording the minimum and maximum current measurements. The test system 200 can assert a signal to the voltage and current control 208 to sweep the power factor angle from a first angle (e.g., 0 degrees) to a second angle (e.g., 360 degrees), while the processor 120 computes current based on the digitized current readings from the meter's ADC 110. The processor 120 determines the minimum and maximum current measurements received from the ADC 110 during the power factor angle sweep.

**[0034]** At 304, the calibration process further includes determining whether the minimum and maximum current measurements coincided with power factor angles of 0 and 180 degrees. If minimum and maximum current measurements coincide with power factor angles of 0 and 180 degrees, then the crosstalk is determined to be in-phase. The processor 202 may set a flag or a variable to indicate whether the crosstalk is in-phase or out-of-phase.

**[0035]** The value of the  $\alpha$  calibration factor is computed at 306. The value of  $\alpha$  may be computed as per equation (1) hereinabove as the difference between the maximum and minimum current measurements divided by  $2 \cdot V$ . If at 308 the crosstalk is determined to be in-phase, then at 310, the value of the  $\Theta_2$  calibration factor is set to 0. Otherwise, if the crosstalk is determined to be out-of-phase, then at 312, the test system 200 sets the power factor angle between voltage and current to 90 degrees. At 314, the method then includes measuring the current, which may be performed by retrieving an output digital current value from ADC 110. At 316, the method then computes the  $\Theta_2$  calibration factor per equation (3) hereinabove.

**[0036]** At 318, the processor 120 writes the calibration factors  $\alpha$  and  $\Theta_2$  to the electric meter 100, such as to the meter's calibration factor storage 122. The electric meter then can be installed in the field (e.g., at a residence or business).

**[0037]** FIG. 7 illustrates an example of a method of operation of the electric meter 100 following being programmed with the calibration factors. The operations may be performed by the processor

120 in the meter and may be performed in the order shown, or in a different order. Two or more of the operations may be performed concurrently instead of sequentially.

**[0038]** At 350 and 354, the meter takes respective voltage (V) and current ( $I_m$ ) measurements. The meter may be preprogrammed to do so or may receive a command to take the measurements.

**[0039]** At 354, the meter compensates the measured value of current ( $I_m$ ) based on the calibration factors  $\alpha$  and  $\Theta_2$  per equation (4) hereinabove. The meter also may compute power based on the compensated value of current (I) and the measured value of voltage (V) at 356 and transmit data of energy usage (e.g., the calculated power) through the transmitter 124.

**[0040]** The voltage and current sensors 102, 104 can be implemented using any suitable sensor circuit. For example, FIG. 8 illustrates one embodiment of a voltage sensor 102. The sensor includes resistors R1, R2, R3, R4, and R5, capacitors C1, C2, and C3, and an operational amplifier OP1. The voltage sensor in the example of FIG. 8 is configured as a differential amplifier circuit with negative feedback via resistor R4. FIG. 9 illustrates an embodiment of a current sensor 104. The current sensor in the example of FIG. 9 has two gain stages 370, 375 connected in series.

**[0041]** All references to numerical values such as power factor angles (e.g., 0 degrees, 180 degrees, 360 degrees) refer to approximate numerical values. Thus, a reference to 90 degrees means approximately 90 degrees. In some embodiments, “approximate” may mean  $\pm 5\%$ .

**[0042]** Modifications are possible in the described embodiments, and other embodiments are possible, within the scope of the claims.

## CLAIMS

What is claimed is:

1. A method of calibrating an electric meter, comprising:
  - setting current (I) and voltage (V) to the electric meter;
  - sweeping a power factor angle between the voltage and current while measuring minimum and maximum current values; and
  - computing a first calibration factor as a difference between the minimum and maximum current values divided by  $2 \cdot V$ ;
  - when a voltage-induced cross-talk is in-phase with the voltage, setting a second calibration factor to 0; and
  - when the voltage-induced cross-talk is out-of-phase with the voltage, computing the second calibration factor based on a current value measured when the power factor angle is set to 90 degrees.
2. The method of claim 1, further comprising determining whether the voltage-induced cross-talk is in-phase or out-of-phase with the voltage.
3. The method of claim 2, wherein determining whether the voltage-induced cross-talk is in-phase or out-of-phase with the voltage comprises determining whether the minimum and maximum current measurements occurred at power factor angles of 0 degrees and 180 degrees.
4. The method of claim 1, wherein when the voltage-induced cross-talk is out-of-phase with the voltage:
  - setting the power factor angle to 90 degrees;
  - measuring the current value ( $I_m$ ); and
  - computing the second calibration factor based on  $I_m$  and the first calibration factor.
5. The method of claim 1, wherein when the voltage-induced cross-talk is out-of-phase with the voltage:
  - setting the power factor angle to 90 degrees;
  - measuring the current value ( $I_m$ ); and
  - computing the second calibration factor as  $\frac{I_m - I}{\text{first calibration factor} \cdot V}$ .
6. The method of claim 1, further comprising loading the first and second calibration factors into storage in the electric meter.

7. An apparatus, comprising:
  - a voltage and current control configurable to output controllable voltages and currents at a controllable power factor angle;
  - a voltage and current control to: set current (I) and voltage (V) to an electric meter; and cause the voltage and current control to sweep a power factor angle while recording minimum and maximum current values measured by the electric meter; and
  - a processor configured to compute a first calibration factor as a difference between the minimum and maximum current values divided by  $2*V$  and, when a voltage-induced cross-talk is out-of-phase with the voltage, compute a second calibration factor based on the first calibration factor and a current value measured when the power factor angle is set to 90 degrees.
8. The apparatus of claim 7, wherein the processor is configured to determine that the voltage-induced cross-talk is in-phase with the voltage and set the second calibration factor to 0.
9. The apparatus of claim 7, wherein the processor is further configured to determine whether the voltage-induced cross-talk is in-phase or out-of-phase with the voltage.
10. The apparatus of claim 7, wherein the processor is further configured to determine whether the voltage-induced cross-talk is in-phase or out-of-phase with the voltage through determination of whether the minimum and maximum current measurements occurred at power factor angles of 0 degrees and 180 degrees.
11. The apparatus of claim 7, wherein when the voltage-induced cross-talk is out-of-phase with the voltage, the processor is configured to:
  - set the power factor angle to 90 degrees;
  - measure the current value ( $I_m$ ); and
  - compute the second calibration factor based on  $I_m$  and the first calibration factor.
12. The apparatus of claim 7, wherein when the voltage-induced cross-talk is out-of-phase with the voltage, the processor is configured to:
  - set the power factor angle to 90 degrees;
  - measure the current value ( $I_m$ ); and
  - compute the second calibration factor as  $\frac{I_m - I}{\text{first calibration factor} * V}$ .
13. The apparatus of claim 7, wherein the processor computes the first and second calibration factors and stores the first and second calibration factors into storage in the electric meter.
14. The apparatus of claim 7, wherein the processor is included in the electric meter.

15. An apparatus, comprising:  
a voltage sensor;  
a current sensor;  
a single-ended analog-to-digital converter (ADC) coupled to the voltage and current sensors to convert analog voltage and current signals from the voltage and current sensors to digital values;  
a processor or microcontroller coupled to the ADC; and  
a storage device coupled to the processor or microcontroller;  
wherein the storage device is configured to include first and second calibration factors computed by a calibration system; and  
wherein the processor or microcontroller is configured to: receive a voltage (V) from the voltage sensor; receive a current (Im) from the current sensor; compute a current value (I) based on Im; and compute a power value based on I and V.
16. The apparatus of claim 15, wherein the processor or microcontroller is configured to compute I based on Im and the first and second calibration factors.
17. The apparatus of claim 15, wherein the processor or microcontroller is configured to compute I as:  $I = I_m + \alpha V e^{\theta_2}$ , where  $\alpha$  is the first calibration factor and  $\theta_2$  is the second calibration factor.
18. The apparatus of claim 17, wherein  $\theta_2$  is a function of the first calibration factor, a voltage sensed by the voltage sensor, and a measured current when a power factor angle between current voltage is set to 90 degrees.
19. The apparatus of claim 17, wherein  $\theta_2$  is 0.
20. The apparatus of claim 17, further comprising a transmitter, and wherein the controller is configured to transmit energy data through the transmitter.

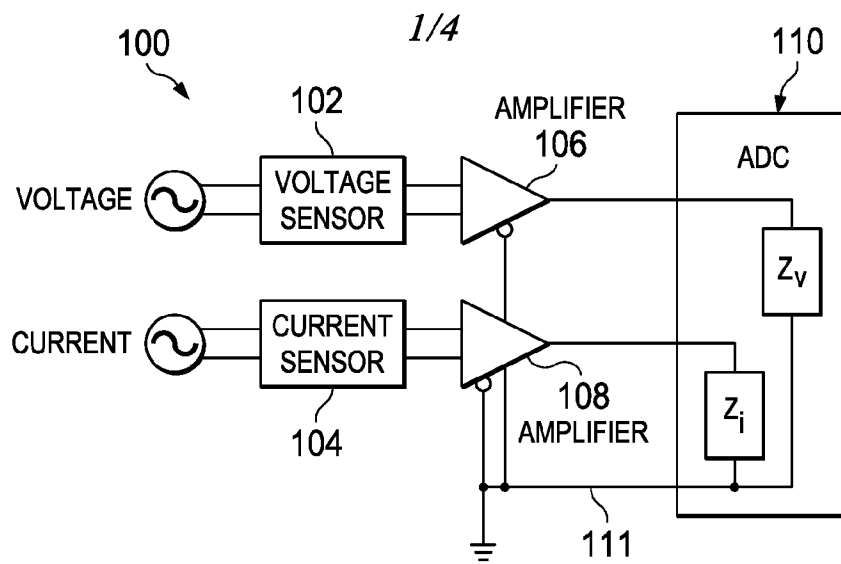


FIG. 1

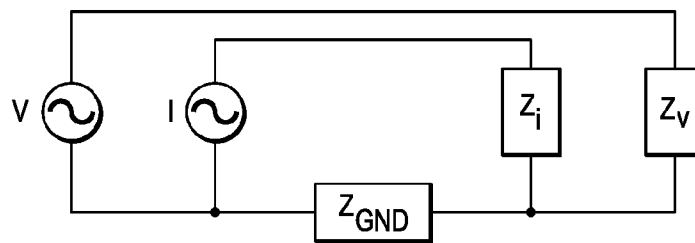


FIG. 2

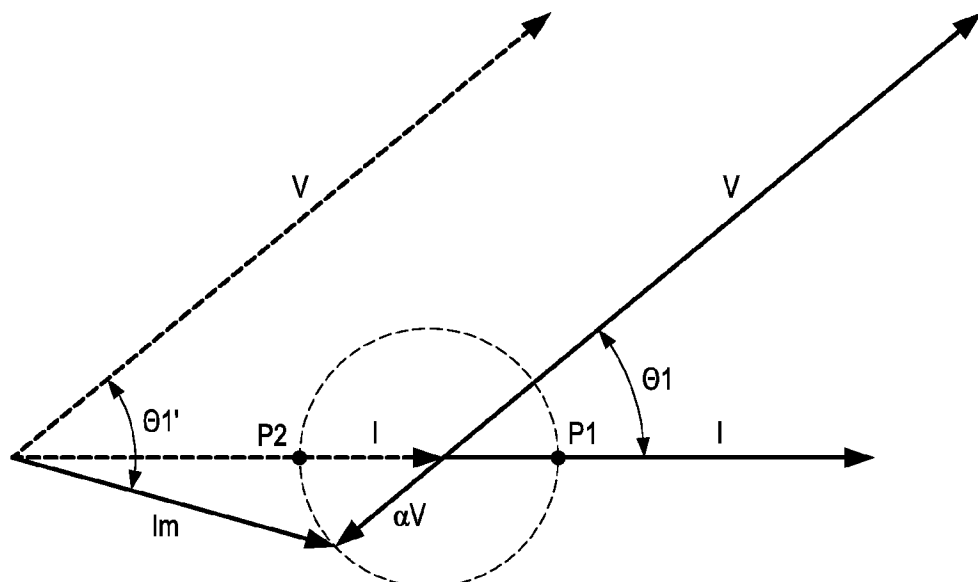


FIG. 3

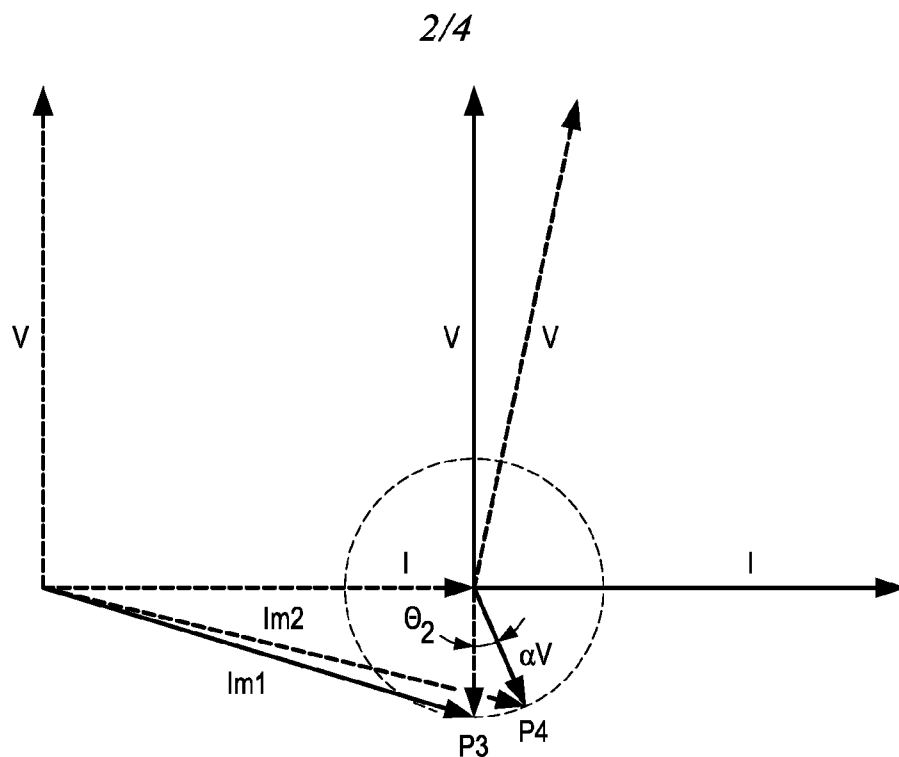


FIG. 4

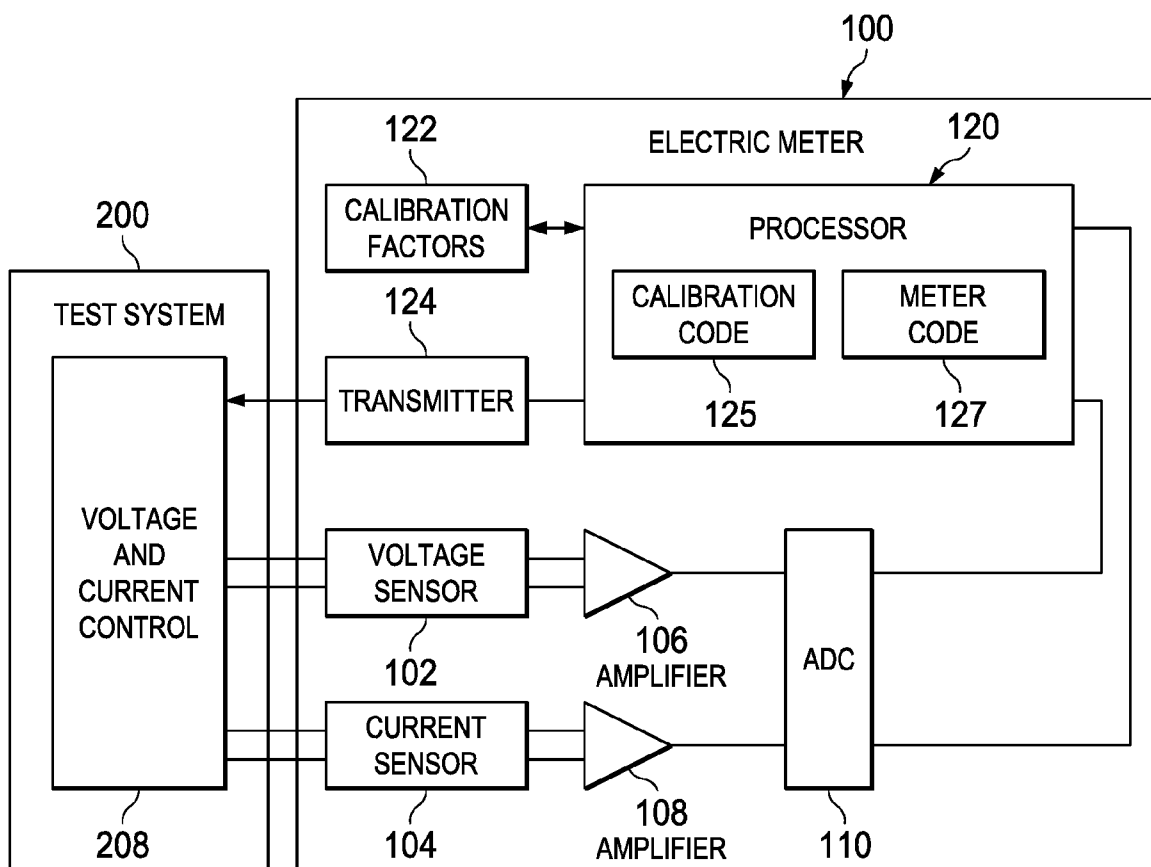


FIG. 5

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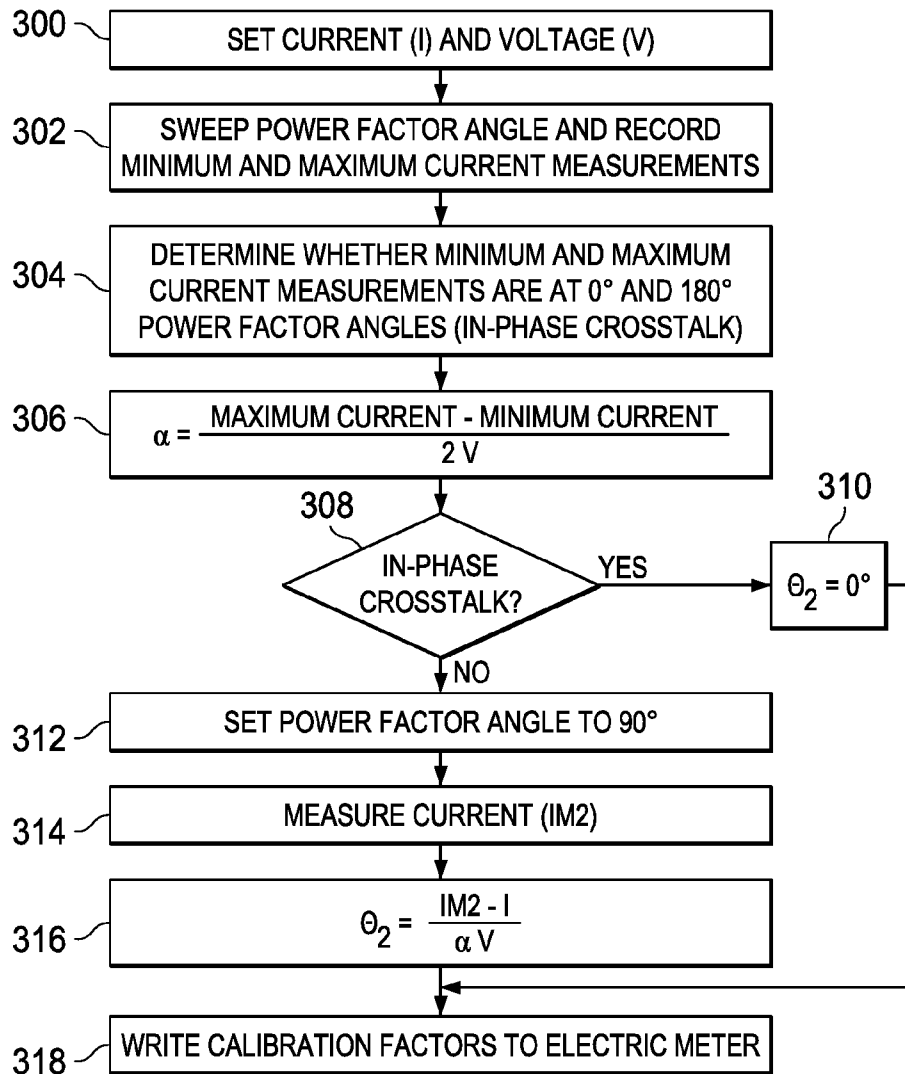


FIG. 6

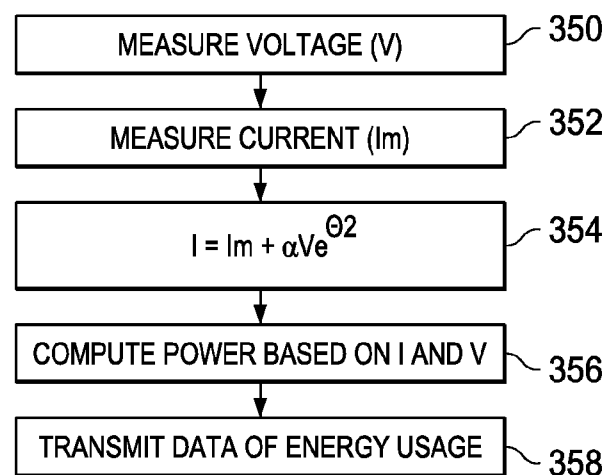


FIG. 7



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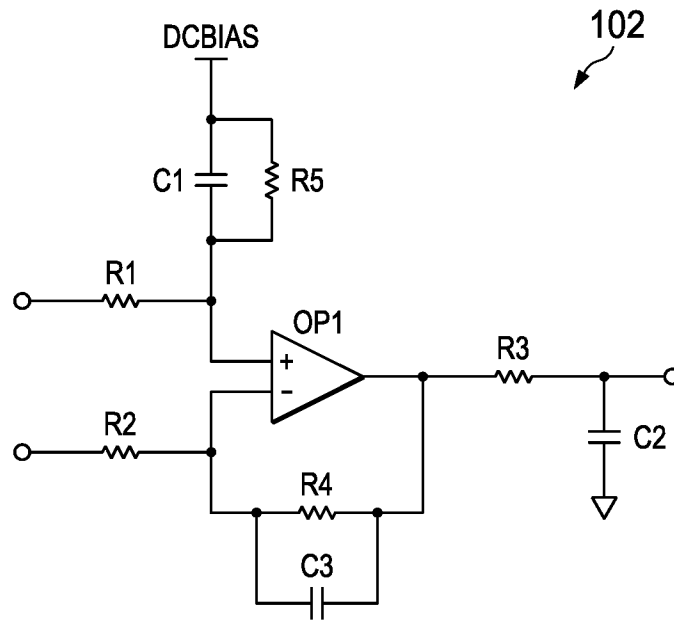


FIG. 8

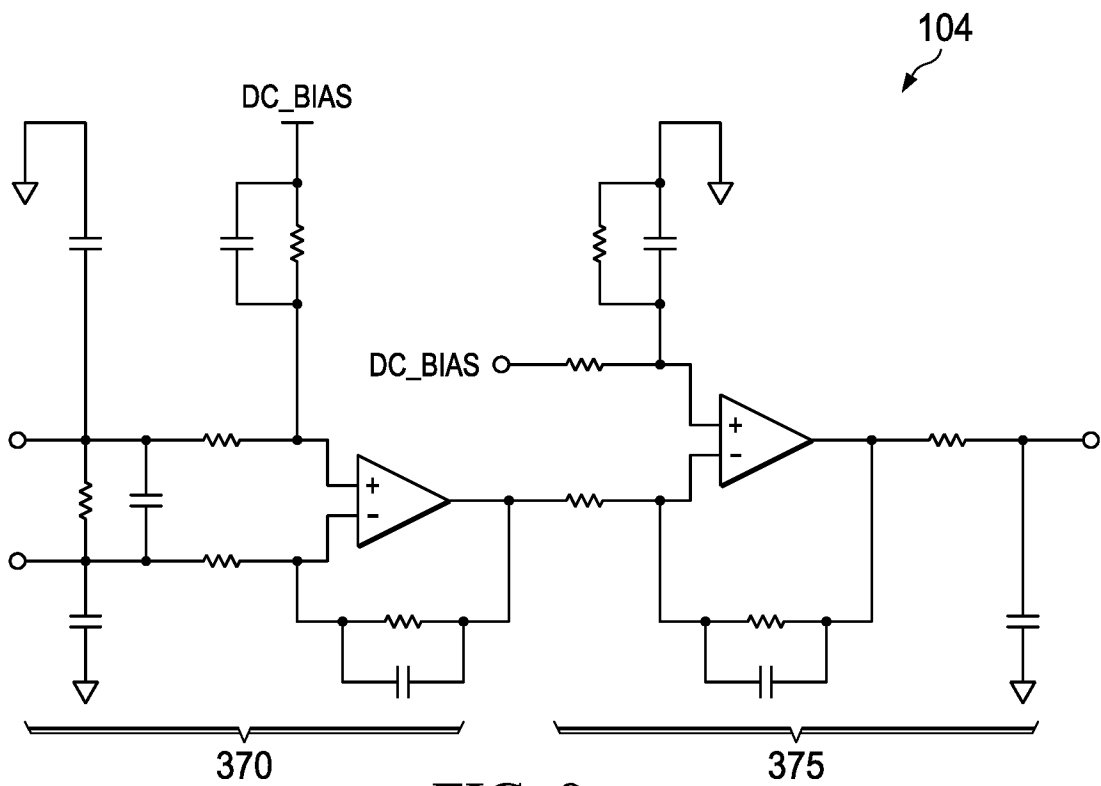


FIG. 9

## INTERNATIONAL SEARCH REPORT

International application No.

PCT/US 2017/022684

A. CLASSIFICATION OF SUBJECT MATTER		
<p style="text-align: center;"><b>G01R 21/133 (2006.01)</b>  <b>G01R 35/04 (2006.01)</b></p> <p>According to International Patent Classification (IPC) or to both national classification and IPC</p>		
B. FIELDS SEARCHED		
Minimum documentation searched (classification system followed by classification symbols)		
G01R 1/04, 21/00, 21/133, 35/00, 35/04, G06F 17/00		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)		
PatSearch (RUPTO internal), USPTO, PAJ, Esp@cenet, DWPI, EAPATIS, PATENTSCOPE		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 5548527 A (ABB POWER T&D COMPANY INC.) 20.08.1996	1-20
A	WO 1995/029409 A1 (DIGITAL KWH, INC.) 02.11.1995	1-20
A	WO 2001/051937 A1 (ABB AB et al.) 19.07.2001	1-20
A	CN 1201909 A (SCHLUMBERGER INDUSTRIES LTD) 16.12.1998	1-20
<input type="checkbox"/> Further documents are listed in the continuation of Box C. <input type="checkbox"/> See patent family annex.		
* Special categories of cited documents:	“T” later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention	
“A” document defining the general state of the art which is not considered to be of particular relevance	“X” document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone	
“E” earlier document but published on or after the international filing date	“Y” document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art	
“L” document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	“&” document member of the same patent family	
“O” document referring to an oral disclosure, use, exhibition or other means		
“P” document published prior to the international filing date but later than the priority date claimed		
Date of the actual completion of the international search	Date of mailing of the international search report	
29 June 2017 (29.06.2017)	14 August 2017 (14.08.2017)	
Name and mailing address of the ISA/RU: Federal Institute of Industrial Property, Berezhkovskaya nab., 30-1, Moscow, G-59, GSP-3, Russia, 125993 Facsimile No: (8-495) 531-63-18, (8-499) 243-33-37	Authorized officer  A. Semenova  Telephone No. 8-499-240-25-91	