

(12) INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
14 July 2011 (14.07.2011)

(10) International Publication Number
WO 2011/084813 A1

PCT

(51) International Patent Classification:
C09K 5/04 (2006.01)

(21) International Application Number:
PCT/US2010/061611

(22) International Filing Date:
21 December 2010 (21.12.2010)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:
61/288,504 21 December 2009 (21.12.2009) US

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(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KN, KP, KR, KZ, LA, LC, LK, LR, LS, LT, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PE, PG, PH, PL, PT, RO, RS, RU, SC, SD, SE, SG, SK, SL, SM, ST, SV, SY, TH, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LR, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European (AL, AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MK, MT, NL, NO, PL, PT, RO, RS, SE, SI, SK, SM, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

Published:

— with international search report (Art. 21(3))

(54) Title: COMPOSITIONS COMPRISING TETRAFLUOROPROPENE AND DIFLUOROMETHANE AND USES THERE-OF

(57) Abstract: The present invention relates to compositions for use in refrigeration, air-conditioning and heat pump systems wherein the composition comprises tetrafluoropropene and difluoromethane. The compositions of the present invention are useful in processes for producing cooling or heat, as heat transfer fluids, foam blowing agents, aerosol propellants, fire suppression, fire extinguishing agents, as power cycle working fluids and in methods for replacing HFC-134a, R410A, R404A, or R507.



WO 2011/084813 A1

TITLE**COMPOSITIONS COMPRISING TETRAFLUOROPROPENE AND
DIFLUOROMETHANE AND USES THEREOF**

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BACKGROUND

1. Field of the Disclosure.

The present disclosure relates to compositions for use in refrigeration, air-conditioning and heat pump systems wherein the composition comprises tetrafluoropropene and difluoromethane. The compositions of the present invention are useful in processes for producing cooling or heat, as heat transfer fluids, foam blowing agents, aerosol propellants and power cycle working fluids.

2. Description of Related Art.

The refrigeration industry has been working for the past few decades to find replacement refrigerants for the ozone depleting chlorofluorocarbons (CFCs) and hydrochlorofluorocarbons (HCFCs) being phased out as a result of the Montreal Protocol. The solution for most refrigerant producers has been the commercialization of hydrofluorocarbon (HFC) refrigerants. The new HFC refrigerants, HFC-134a being the most widely used at this time, have zero ozone depletion potential and thus are not affected by the current regulatory phase out as a result of the Montreal Protocol.

Further environmental regulations may ultimately cause global phase out of certain HFC refrigerants. Currently, industry is facing regulations relating to global warming potential (GWP) for refrigerants used in mobile air-conditioning. Should the regulations be more broadly applied in the future, for instance for stationary air conditioning and refrigeration systems, an even greater need will be felt for refrigerants that can be used in all areas of the refrigeration and air-conditioning industry. Uncertainty as to the ultimate regulatory requirements relative to GWP, have forced the industry to consider multiple candidate compounds and mixtures.

Currently proposed replacement refrigerants for HFC refrigerants and refrigerant blends include HFC-152a, pure hydrocarbons, such as

butane or propane, or "natural" refrigerants such as CO₂. Each of these suggested replacements has problems including toxicity, flammability, low energy efficiency, or requires major equipment design modifications. New replacements are also being proposed for HCFC-22, R-134a, R-404A, R-507, R-407C and R-410A, among others. Uncertainty as to what regulatory requirements relative to GWP will ultimately be adopted have forced the industry to consider multiple candidate compounds and mixtures that balance the need for low GWP, non-flammability or low flammability, and existing system performance parameters.

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BRIEF SUMMARY

Compositions comprising 2,3,3,3-tetrafluoropropene and difluoromethane have been found to possess certain properties to allow replacement of higher GWP refrigerants currently in use, including R-134a, R404A and R410A.

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Thus, herein is provide a composition comprising about 1 weight percent to about 80 weight percent 2,3,3,3-tetrafluoropropene and about 99 weight percent to about 20 weight percent difluoromethane.

Also disclosed herein are methods of producing cooling and heating, methods for replacing refrigerants such as R-134a, R410A and R404A, and air conditioning and refrigeration apparatus containing compositions comprising 2,3,3,3-tetrafluoropropene and difluoromethane.

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DETAILED DESCRIPTION

Before addressing details of embodiments described below, some terms are defined or clarified.

25

Definitions

As used herein, the term heat transfer composition means a composition used to carry heat from a heat source to a heat sink.

A heat source is defined as any space, location, object or body from which it is desirable to add, transfer, move or remove heat. Examples of heat sources are spaces (open or enclosed) requiring refrigeration or cooling, such as refrigerator or freezer cases in a supermarket, building spaces requiring air conditioning, industrial water chillers or the passenger

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compartments of an automobile requiring air conditioning. In some embodiments, the heat transfer composition may remain in a constant state throughout the transfer process (i.e., not evaporate or condense). In other embodiments, evaporative cooling processes may utilize heat transfer compositions as well.

A heat sink is defined as any space, location, object or body capable of absorbing heat. A vapor compression refrigeration system is one example of such a heat sink.

A heat transfer system is the system (or apparatus) used to produce a heating or cooling effect in a particular space. A heat transfer system may be a mobile system or a stationary system.

Examples of heat transfer systems include but are not limited to air conditioners, freezers, refrigerators, heat pumps, water chillers, flooded evaporator chillers, direct expansion chillers, walk-in coolers, mobile refrigerators, mobile air conditioning units, dehumidifiers, and combinations thereof.

As used herein, mobile heat transfer system refers to any refrigeration, air conditioner or heating apparatus incorporated into a transportation unit for the road, rail, sea or air. In addition, mobile refrigeration or air conditioner units, include those apparatus that are independent of any moving carrier and are known as "intermodal" systems. Such intermodal systems include "container" (combined sea/land transport) as well as "swap bodies" (combined road/rail transport).

As used herein, stationary heat transfer systems are systems that are fixed in place during operation. A stationary heat transfer system may be associated within or attached to buildings of any variety or may be stand alone devices located out of doors, such as a soft drink vending machine. These stationary applications may be stationary air conditioning and heat pumps, including but not limited to chillers, high temperature heat pumps, residential, commercial or industrial air conditioning systems (including residential heat pumps), and including window, ductless, ducted, packaged terminal, and those exterior but connected to the building such as rooftop systems. In stationary refrigeration applications,

the disclosed compositions may be useful in equipment including commercial, industrial or residential refrigerators and freezers, ice machines, self-contained coolers and freezers, flooded evaporator chillers, direct expansion chillers, walk-in and reach-in coolers and freezers, and combination systems. In some embodiments, the disclosed compositions may be used in supermarket refrigeration systems. Additionally, stationary applications may utilize a secondary loop system that uses a primary refrigerant to produce cooling in one location that is transferred to a remote location via a secondary heat transfer fluid.

Refrigeration capacity (also referred to as cooling capacity) is a term which defines the change in enthalpy of a refrigerant in an evaporator per pound of refrigerant circulated, or the heat removed by the refrigerant in the evaporator per unit volume of refrigerant vapor exiting the evaporator (volumetric capacity). The refrigeration capacity is a measure of the ability of a refrigerant or heat transfer composition to produce cooling. Therefore, the higher the capacity, the greater the cooling that is produced. Cooling rate refers to the heat removed by the refrigerant in the evaporator per unit time.

Coefficient of performance (COP) is the amount of heat removed divided by the required energy input to operate the cycle. The higher the COP, the higher is the energy efficiency. COP is directly related to the energy efficiency ratio (EER) that is the efficiency rating for refrigeration or air conditioning equipment at a specific set of internal and external temperatures.

The term "subcooling" refers to the reduction of the temperature of a liquid below that liquid's saturation point for a given pressure. The saturation point is the temperature at which the vapor is completely condensed to a liquid, but subcooling continues to cool the liquid to a lower temperature liquid at the given pressure. By cooling a liquid below the saturation temperature (or bubble point temperature), the net refrigeration capacity can be increased. Subcooling thereby improves refrigeration capacity and energy efficiency of a system. Subcool amount is the amount of cooling below the saturation temperature (in degrees).

Superheat is a term that defines how far above its saturation vapor temperature (the temperature at which, if the composition is cooled, the first drop of liquid is formed, also referred to as the “dew point”) a vapor composition is heated.

5 Temperature glide (sometimes referred to simply as “glide”) is the absolute value of the difference between the starting and ending temperatures of a phase-change process by a refrigerant within a component of a refrigerant system, exclusive of any subcooling or superheating. This term may be used to describe condensation or
10 evaporation of a near azeotrope or non-azeotropic composition. When referring to the temperature glide of a refrigeration, air conditioning or heat pump system, it is common to provide the average temperature glide being the average of the temperature glide in the evaporator and the temperature glide in the condenser.

15 By azeotropic composition is meant a constant-boiling mixture of two or more substances that behave as a single substance. One way to characterize an azeotropic composition is that the vapor produced by partial evaporation or distillation of the liquid has the same composition as the liquid from which it is evaporated or distilled, i.e., the mixture
20 distills/refluxes without compositional change. Constant-boiling compositions are characterized as azeotropic because they exhibit either a maximum or minimum boiling point, as compared with that of the non-azeotropic mixture of the same compounds. An azeotropic composition will not fractionate within a refrigeration or air conditioning system during
25 operation. Additionally, an azeotropic composition will not fractionate upon leakage from a refrigeration or air conditioning system.

 A near-azeotropic composition (also commonly referred to as an “azeotrope-like composition”) is a substantially constant boiling liquid admixture of two or more substances that behaves essentially as a single
30 substance. One way to characterize a near-azeotropic composition is that the vapor produced by partial evaporation or distillation of the liquid has substantially the same composition as the liquid from which it was evaporated or distilled, that is, the admixture distills/refluxes without substantial composition change. Another way to characterize a near-

azeotropic composition is that the bubble point vapor pressure and the dew point vapor pressure of the composition at a particular temperature are substantially the same. Herein, a composition is near-azeotropic if, after 50 weight percent of the composition is removed, such as by evaporation or boiling off, the difference in vapor pressure between the original composition and the composition remaining after 50 weight percent of the original composition has been removed is less than about 10 percent.

A non-azeotropic composition is a mixture of two or more substances that behaves as a simple mixture rather than a single substance. One way to characterize a non-azeotropic composition is that the vapor produced by partial evaporation or distillation of the liquid has a substantially different composition as the liquid from which it was evaporated or distilled, that is, the admixture distills/refluxes with substantial composition change. Another way to characterize a non-azeotropic composition is that the bubble point vapor pressure and the dew point vapor pressure of the composition at a particular temperature are substantially different. Herein, a composition is non-azeotropic if, after 50 weight percent of the composition is removed, such as by evaporation or boiling off, the difference in vapor pressure between the original composition and the composition remaining after 50 weight percent of the original composition has been removed is greater than about 10 percent.

As used herein, the term "lubricant" means any material added to a composition or a compressor (and in contact with any heat transfer composition in use within any heat transfer system) that provides lubrication to the compressor to aid in preventing parts from seizing.

As used herein, compatibilizers are compounds which improve solubility of the hydrofluorocarbon of the disclosed compositions in heat transfer system lubricants. In some embodiments, the compatibilizers improve oil return to the compressor. In some embodiments, the composition is used with a system lubricant to reduce oil-rich phase viscosity.

As used herein, oil-return refers to the ability of a heat transfer composition to carry lubricant through a heat transfer system and return it

to the compressor. That is, in use, it is not uncommon for some portion of the compressor lubricant to be carried away by the heat transfer composition from the compressor into the other portions of the system. In such systems, if the lubricant is not efficiently returned to the compressor, the compressor will eventually fail due to lack of lubrication.

As used herein, "ultra-violet" dye is defined as a UV fluorescent or phosphorescent composition that absorbs light in the ultra-violet or "near" ultra-violet region of the electromagnetic spectrum. The fluorescence produced by the UV fluorescent dye under illumination by a UV light that emits at least some radiation with a wavelength in the range of from 10 nanometers to about 775 nanometers may be detected.

Flammability is a term used to mean the ability of a composition to ignite and/or propagate a flame. For refrigerants and other heat transfer compositions, the lower flammability limit ("LFL") is the minimum concentration of the heat transfer composition in air that is capable of propagating a flame through a homogeneous mixture of the composition and air under test conditions specified in ASTM (American Society of Testing and Materials) E681. The upper flammability limit ("UFL") is the maximum concentration of the heat transfer composition in air that is capable of propagating a flame through a homogeneous mixture of the composition and air under the same test conditions. In order to be classified by ASHRAE (American Society of Heating, Refrigerating and Air-Conditioning Engineers) as non-flammable, a refrigerant must be non-flammable under the conditions of ASTM E681 as formulated in both the liquid and vapor phase as well as non-flammable in both the liquid and vapor phases that result during leakage scenarios.

Global warming potential (GWP) is an index for estimating relative global warming contribution due to atmospheric emission of a kilogram of a particular greenhouse gas compared to emission of a kilogram of carbon dioxide. GWP can be calculated for different time horizons showing the effect of atmospheric lifetime for a given gas. The GWP for the 100 year time horizon is commonly the value referenced. For mixtures, a weighted average can be calculated based on the individual GWPs for each component.

Ozone depletion potential (ODP) is a number that refers to the amount of ozone depletion caused by a substance. The ODP is the ratio of the impact on ozone of a chemical compared to the impact of a similar mass of CFC-11 (fluorotrichloromethane). Thus, the ODP of CFC-11 is defined to be 1.0. Other CFCs and HCFCs have ODPs that range from 0.01 to 1.0. HFCs have zero ODP because they do not contain chlorine.

As used herein, the terms "comprises," "comprising," "includes," "including," "has," "having" or any other variation thereof, are intended to cover a non-exclusive inclusion. For example, a composition, process, method, article, or apparatus that comprises a list of elements is not necessarily limited to only those elements but may include other elements not expressly listed or inherent to such composition, process, method, article, or apparatus. Further, unless expressly stated to the contrary, "or" refers to an inclusive or and not to an exclusive or. For example, a condition A or B is satisfied by any one of the following: A is true (or present) and B is false (or not present), A is false (or not present) and B is true (or present), and both A and B are true (or present).

The transitional phrase "consisting of" excludes any element, step, or ingredient not specified. If in the claim such would close the claim to the inclusion of materials other than those recited except for impurities ordinarily associated therewith. When the phrase "consists of" appears in a clause of the body of a claim, rather than immediately following the preamble, it limits only the element set forth in that clause; other elements are not excluded from the claim as a whole.

The transitional phrase "consisting essentially of" is used to define a composition, method or apparatus that includes materials, steps, features, components, or elements, in addition to those literally disclosed provided that these additional included materials, steps, features, components, or elements do materially affect the basic and novel characteristic(s) of the claimed invention. The term 'consisting essentially of' occupies a middle ground between "comprising" and 'consisting of'.

Where applicants have defined an invention or a portion thereof with an open-ended term such as "comprising," it should be readily understood that (unless otherwise stated) the description should be

interpreted to also describe such an invention using the terms “consisting essentially of” or “consisting of.”

Also, use of “a” or “an” are employed to describe elements and components described herein. This is done merely for convenience and to give a general sense of the scope of the invention. This description should be read to include one or at least one and the singular also includes the plural unless it is obvious that it is meant otherwise.

Unless otherwise defined, all technical and scientific terms used herein have the same meaning as commonly understood by one of ordinary skill in the art to which this invention belongs. Although methods and materials similar or equivalent to those described herein can be used in the practice or testing of embodiments of the disclosed compositions, suitable methods and materials are described below. All publications, patent applications, patents, and other references mentioned herein are incorporated by reference in their entirety, unless a particular passage is cited. In case of conflict, the present specification, including definitions, will control. In addition, the materials, methods, and examples are illustrative only and not intended to be limiting.

Compositions

Disclosed are compositions comprising from about 1 weight percent to about 80 weight percent 2,3,3,3-tetrafluoropropene and about 99 weight percent to about 20 weight percent difluoromethane. 2,3,3,3-tetrafluoropropene may also be referred to as HFO-1234yf, HFC-1234yf, or R1234yf. HFO-1234yf may be made by methods known in the art, such as by dehydrofluorination 1,1,1,2,3-pentafluoropropane (HFC-245eb) or 1,1,1,2,2-pentafluoropropane (HFC-245cb). Difluoromethane (HFC-32 or R32) is commercially available or may be made by methods known in the art, such as by dechlorofluorination of methylene chloride.

Both HFO-1234yf and HFC-32 are being considered as low GWP replacements for certain refrigerants and refrigerant mixtures that have relatively high GWP. In particular, R410A (ASHRAE designation for a mixture containing 50 wt% HFC-32 and 50 wt% pentafluoroethane, or HFC-125) has a global warming potential of 2088 and will be in need of

replacement when regulations related to global warming of refrigerants are enacted. Additionally, R404A (ASHRAE designation for a mixture containing 44 wt% HFC-125, 52 wt% HFC-143a (1,1,1-trifluoroethane), and 4 wt% HFC-134a) has a GWP of 3922 and will be in need of replacement. Further, R-507 (ASHRAE designation for a mixture containing 50 wt% HFC-125 and 50 wt% HFC-143a), which has virtually identical properties to R404A and can therefore be used in many R404A systems, has a GWP equal to 3985, and therefore does not provide a lower GWP replacement for R404A, but will be in need of replacement as well.

Tetrafluoroethane, in particular 1,1,1,2-tetrafluoroethane (HFC-134a), currently used as a refrigerant in many applications, has a GWP of 1430 and is in need of replacement. Of note is the use of HFC-134a in automotive heat pumps. In one embodiment, a composition having about 21.5 weight percent HFC-32 and about 78.5 weight percent HFO-1234yf demonstrates significantly improved heating capacity versus HFC-134a, but has a GWP below 150, which meets the European F-Gas directive.

Compositions falling within the range of the present invention have been found to provide reduced GWP as compared to R410A, a refrigerant commonly used in air conditioning systems. A composition that contains 80 weight percent HFO-1234yf and 20 weight percent HFC-32 has a GWP of only 138 as compared to R410A with GWP = 2088. Such a composition has considerably lower cooling capacity than R410A. However, should GWP regulations require a GWP lower than 150, it would be possible to compensate for the deficiency in cooling capacity. And the composition has improved energy efficiency relative to R410A.

In a particular embodiment, the compositions of the present invention comprise from about 30 weight percent to about 80 weight percent 2,3,3,3-tetrafluoropropene and about 70 weight percent to about 20 weight percent difluoromethane. A composition containing 30 weight percent HFO-1234yf and 70 weight percent HFC-32 still provides GWP < 500, with cooling capacity and energy efficiency essentially matching that of R410A

In another embodiment, the compositions of the present invention comprise from about 25 weight percent to about 60 weight percent HFO-1234yf and from about 75 weight percent to about 40 weight percent difluoromethane. These compositions have been found to provide heating capacity within $\pm 20\%$ of that for R410A, comparable energy efficiency and average temperature glide of less than about 5 °C. Of particular note are compositions having about 72.5 weight percent HFC-32 and about 27.5 weight percent HFO-1234yf that have been found to be a match for R410A for both capacity and energy efficiency.

10 In another particular embodiment, the compositions of the present invention comprise about 45 weight percent to about 80 weight percent 2,3,3,3-tetrafluoropropene and about 55 weight percent to about 20 weight percent difluoromethane. Compositions falling within this embodiment provide cooling capacity within $\pm 20\%$ of that for R404A while also matching the energy efficiency. Additionally, the GWP for a composition in this range falls between about 500 to about 335, which is significantly lower than the GWP of R404A or R410A.

In another embodiment, the compositions of the present invention comprise from about 55 weight percent to about 80 weight percent 2,3,3,3-tetrafluoropropene and about 45 weight percent to about 20 weight percent difluoromethane. Compositions in this range provide cooling capacity and energy efficiency in the desired range as a replacement for R404A, while maintaining GWP values less than 400.

25 In a particular embodiment, compositions according to the present invention comprise about 35 weight percent to about 60 weight percent HFO-1234yf and about 65 weight percent to about 40 weight percent HFC-32. Such compositions have a temperature glide similar or less than that of R407C.

30 A refrigerant mixture with some temperature glide may be acceptable in the industry or even have advantages as mentioned previously herein. R407C (ASHRAE designation for a mixture of 23 wt% HFC-32, 25 wt% HFC-125, and 52 wt% HFC-134a) is an example of a commercial refrigerant product with glide. It has been demonstrated that certain compositions as disclosed herein provide a refrigerant composition

with temperature glide that approaches the temperature glide of R407C or is lower than the temperature glide of R407C. And therefore, such compositions will be commercially acceptable to the refrigerant, air conditioning and heat pump industry.

5 In one embodiment, the compositions of the present invention comprise from about 20 weight percent to about 55 weight percent HFO-1234yf and from about 80 weight percent to about 45 weight percent HFC-32. Compositions in this range have been found to have cooling capacity within 20% of R410A and slightly better energy efficiency than R410A,
10 making them acceptable replacements for R410A.

 Of particular note are compositions comprising a working fluid wherein the working fluid consists essentially of from about 20 to about 42.5 weight percent 2,3,3,3-tetrafluoropropene and from about 80 to about 57.5 weight percent difluoromethane. These compositions have been
15 found to exhibit low temperature glide thus allowing use in a wide variety of equipment with a GWP of less than 600.

 In another embodiment, the compositions of the present invention may comprise from about 45 weight percent to about 55 weight percent 2,3,3,3-tetrafluoropropene and about 55 weight percent to about 45 weight
20 percent difluoromethane. Compositions in this range, along with cooling capacity within 20% of R410A and slightly better energy efficiency than R410A also have GWP values less than 400. Further, compositions in this range show cooling capacity greater than that of R404A, while the energy efficiency is within a few percent of R404A. Additionally, the temperature
25 glide for these compositions is in the range of R407C and therefore, should be commercially acceptable refrigerants. Compositions in the range from about 45 weight percent to about 55 weight percent 2,3,3,3-tetrafluoropropene and about 55 weight percent to about 45 weight
30 percent difluoromethane should be acceptable as replacements for R410A or R404A.

 Of note are compositions comprising a working fluid wherein the working fluid consists essentially of from about 25 weight percent to about 30 weight percent 2,3,3,3-tetrafluoropropene and from about 75 weight percent to about 70 weight percent difluoromethane. These compositions

provide low temperature glide and matching energy efficiency and cooling capacity relative to R410A of the compositions as disclosed herein.

Additionally of note are compositions comprising a working fluid wherein the working fluid consists essentially of from about 40 weight percent to about 45 weight percent 2,3,3,3-tetrafluoropropene and from about 60 weight percent to about 55 weight percent difluoromethane. These compositions provide good match in energy efficiency and improved cooling and heating capacity relative to R404A as well as low temperature glide and GWP of less than 400.

10 The disclosed compositions are generally expected to maintain the desired properties and functionality when the components are present in the concentrations as listed above +/- 2 weight percent.

Certain of the compositions of the present invention are non-azeotropic compositions. In particular, a composition comprising 43 to 99 weight percent 2,3,3,3-tetrafluoropropene and 57 to 1 weight percent difluoromethane are non-azeotropic. A non-azeotropic composition may have certain advantages over azeotropic or near azeotropic mixtures. For instance, the temperature glide of a non-azeotropic composition provides an advantage in counter current flow heat exchanger arrangements.

20 Compositions with higher capacity than the refrigerant being replaced provide reduced carbon footprint by allowing a lower charge size (less refrigerant will be necessary to achieve the same cooling effect). Therefore, even with a higher GWP such compositions may provide a net reduced environmental impact. Additionally, new equipment may be designed to provide even greater energy efficiency improvements, thus also minimizing the environmental impact of using a new refrigerant.

In some embodiments, in addition to the tetrafluoropropene and difluoromethane, the disclosed compositions may comprise optional other components.

30 In some embodiments, the optional other components (also referred to herein as additives) in the compositions disclosed herein may comprise one or more components selected from the group consisting of lubricants, dyes (including UV dyes), solubilizing agents, compatibilizers, stabilizers, tracers, perfluoropolyethers, anti wear agents, extreme

pressure agents, corrosion and oxidation inhibitors, metal surface energy reducers, metal surface deactivators, free radical scavengers, foam control agents, viscosity index improvers, pour point depressants, detergents, viscosity adjusters, and mixtures thereof. Indeed, many of
5 these optional other components fit into one or more of these categories and may have qualities that lend themselves to achieve one or more performance characteristic.

In some embodiments, one or more additive present in small amounts relative to the overall composition. In some embodiments, the
10 amount of additive(s) concentration in the disclosed compositions is from less than about 0.1 weight percent to as much as about 5 weight percent of the total composition. In some embodiments of the present invention, the additives are present in the disclosed compositions in an amount between about 0.1 weight percent to about 3.5 weight percent of the total
15 composition. The additive component(s) selected for the disclosed composition is selected on the basis of the utility and/or individual equipment components or the system requirements.

In some embodiments, the lubricant is a mineral oil lubricant. In some embodiments, the mineral oil lubricant is selected from the group
20 consisting of paraffins (including straight carbon chain saturated hydrocarbons, branched carbon chain saturated hydrocarbons, and mixtures thereof), naphthenes (including saturated cyclic and ring structures), aromatics (those with unsaturated hydrocarbons containing one or more ring, wherein one or more ring is characterized by alternating
25 carbon-carbon double bonds) and non-hydrocarbons (those molecules containing atoms such as sulfur, nitrogen, oxygen and mixtures thereof), and mixtures and combinations of thereof.

Some embodiments may contain one or more synthetic lubricant. In some embodiments, the synthetic lubricant is selected from the group
30 consisting of alkyl substituted aromatics (such as benzene or naphthalene substituted with linear, branched, or mixtures of linear and branched alkyl groups, often generically referred to as alkylbenzenes), synthetic paraffins and naphthenes, poly (alpha olefins), polyglycols (including polyalkylene

glycols), dibasic acid esters, polyesters, neopentyl esters, polyvinyl ethers (PVEs), silicones, silicate esters, fluorinated compounds, phosphate esters, polycarbonates and mixtures thereof, meaning mixtures of the any of the lubricants disclosed in this paragraph.

- 5 The lubricants as disclosed herein may be commercially available lubricants. For instance, the lubricant may be paraffinic mineral oil, sold by BVA Oils as BVM 100 N, naphthenic mineral oils sold by Crompton Co. under the trademarks Suniso[®] 1GS, Suniso[®] 3GS and Suniso[®] 5GS, naphthenic mineral oil sold by Pennzoil under the trademark Sontex[®]
- 10 372LT,,naphthenic mineral oil sold by Calumet Lubricants under the trademark Calumet[®] RO-30,, linear alkylbenzenes sold by Shrieve Chemicals under the trademarks Zerol[®] 75, Zerol[®] 150 and Zerol[®] 500 and branched alkylbenzene sold by Nippon Oil as HAB 22, polyol esters (POEs) sold under the trademark Castrol[®] 100 by Castrol, United
- 15 Kingdom, polyalkylene glycols (PAGs) such as RL-488A from Dow (Dow Chemical, Midland, Michigan), and mixtures thereof, meaning mixtures of any of the lubricants disclosed in this paragraph.

- The lubricants used with the present invention may be designed for use with hydrofluorocarbon refrigerants and may be miscible with
- 20 compositions as disclosed herein under compression refrigeration and air-conditioning apparatus' operating conditions. In some embodiments, the lubricants are selected by considering a given compressor's requirements and the environment to which the lubricant will be exposed.

- In the compositions of the present invention including a lubricant,
- 25 the lubricant is present in an amount of less than 5.0 weight % to the total composition. In other embodiments, the amount of lubricant is between about 0.1 and 3.5 weight % of the total composition.

- Notwithstanding the above weight ratios for compositions disclosed herein, it is understood that in some heat transfer systems, while the
- 30 composition is being used, it may acquire additional lubricant from one or more equipment components of such heat transfer system. For example, in some refrigeration, air conditioning and heat pump systems, lubricants may be charged in the compressor and/or the compressor lubricant sump. Such lubricant would be in addition to any lubricant additive present in the

refrigerant in such a system. In use, the refrigerant composition when in the compressor may pick up an amount of the equipment lubricant to change the refrigerant-lubricant composition from the starting ratio.

In such heat transfer systems, even when the majority of the lubricant resides within the compressor portion of the system, the entire system may contain a total composition with as much as about 75 weight percent to as little as about 1.0 weight percent of the composition being lubricant. In some systems, for example supermarket refrigerated display cases, the system may contain about 3 weight percent lubricant (over and above any lubricant present in the refrigerant composition prior to charging the system) and 97 weight percent refrigerant. In another embodiment, in some systems, for example mobile air conditioning systems, the system may contain about 20 weight percent lubricant (over and above any lubricant present in the refrigerant composition prior to charging the system) and about 80 weight percent refrigerant.

The additive used with the compositions of the present invention may include at least one dye. The dye may be at least one ultra-violet (UV) dye. The UV dye may be a fluorescent dye. The fluorescent dye may be selected from the group consisting of naphthalimides, perylenes, coumarins, anthracenes, phenanthracenes, xanthenes, thioxanthenes, naphthoxanthenes, fluoresceins, and derivatives of said dye, and combinations thereof, meaning mixtures of any of the foregoing dyes or their derivatives disclosed in this paragraph.

In some embodiments, the disclosed compositions contain from about 0.001 weight percent to about 1.0 weight percent UV dye. In other embodiments, the UV dye is present in an amount of from about 0.005 weight percent to about 0.5 weight percent; and in other embodiments, the UV dye is present in an amount of from 0.01 weight percent to about 0.25 weight percent of the total composition.

UV dye is a useful component for detecting leaks of the composition by permitting one to observe the fluorescence of the dye at or in the vicinity of a leak point in an apparatus (e.g., refrigeration unit, air-conditioner or heat pump). The UV emission, e.g., fluorescence from the dye may be observed under an ultra-violet light. Therefore, if a

composition containing such a UV dye is leaking from a given point in an apparatus, the fluorescence can be detected at the leak point, or in the vicinity of the leak point.

The additive which may be used with the compositions of the present invention may include at least one solubilizing agent selected to improve the solubility of one or more dye in the disclosed compositions. In some embodiments, the weight ratio of dye to solubilizing agent ranges from about 99:1 to about 1:1. The solubilizing agents include at least one compound selected from the group consisting of hydrocarbons, hydrocarbon ethers, polyoxyalkylene glycol ethers (such as dipropylene glycol dimethyl ether), amides, nitriles, ketones, chlorocarbons (such as methylene chloride, trichloroethylene, chloroform, or mixtures thereof), esters, lactones, aromatic ethers, fluoroethers and 1,1,1-trifluoroalkanes and mixtures thereof, meaning mixtures of any of the solubilizing agents disclosed in this paragraph.

In some embodiments, at least one compatibilizer is selected to improve the compatibility of one or more lubricant with the disclosed compositions. The compatibilizer may be selected from the group consisting of hydrocarbons, hydrocarbon ethers, polyoxyalkylene glycol ethers (such as dipropylene glycol dimethyl ether), amides, nitriles, ketones, chlorocarbons (such as methylene chloride, trichloroethylene, chloroform, or mixtures thereof), esters, lactones, aromatic ethers, fluoroethers, 1,1,1-trifluoroalkanes, and mixtures thereof, meaning mixtures of any of the compatibilizers disclosed in this paragraph.

The solubilizing agent and/or compatibilizer may be selected from the group consisting of hydrocarbon ethers consisting of the ethers containing only carbon, hydrogen and oxygen, such as dimethyl ether (DME) and mixtures thereof, meaning mixtures of any of the hydrocarbon ethers disclosed in this paragraph.

The compatibilizer may be linear or cyclic aliphatic or aromatic hydrocarbon compatibilizer containing from 3 to 15 carbon atoms. The compatibilizer may be at least one hydrocarbon, which may be selected from the group consisting of at least propane, n-butane, isobutane, pentanes, hexanes, octanes, nonane, and decanes, among others.

Commercially available hydrocarbon compatibilizers include but are not limited to those from Exxon Chemical (USA) sold under the trademarks Isopar[®] H, a mixture of undecan (C₁₁) and dodecane (C₁₂) (a high purity C₁₁ to C₁₂ iso-paraffinic), Aromatic 150 (a C₉ to C₁₁ aromatic) (, Aromatic 200 (a C₉ to C₁₅ aromatic) and Naptha 140 (a mixture of C₅ to C₁₁ paraffins, naphthenes and aromatic hydrocarbons) and mixtures thereof, meaning mixtures of any of the hydrocarbons disclosed in this paragraph.

The additive may alternatively be at least one polymeric compatibilizer. The polymeric compatibilizer may be a random copolymer of fluorinated and non-fluorinated acrylates, wherein the polymer comprises repeating units of at least one monomer represented by the formulae $\text{CH}_2=\text{C}(\text{R}^1)\text{CO}_2\text{R}^2$, $\text{CH}_2=\text{C}(\text{R}^3)\text{C}_6\text{H}_4\text{R}^4$, and $\text{CH}_2=\text{C}(\text{R}^5)\text{C}_6\text{H}_4\text{XR}^6$, wherein X is oxygen or sulfur; R¹, R³, and R⁵ are independently selected from the group consisting of H and C₁-C₄ alkyl radicals; and R², R⁴, and R⁶ are independently selected from the group consisting of carbon-chain-based radicals containing C, and F, and may further contain H, Cl, ether oxygen, or sulfur in the form of thioether, sulfoxide, or sulfone groups and mixtures thereof. Examples of such polymeric compatibilizers include those commercially available from E. I. du Pont de Nemours and Company. (Wilmington, DE, 19898, USA) under the trademark Zonyl[®] PHS. Zonyl[®] PHS is a random copolymer made by polymerizing 40 weight percent $\text{CH}_2=\text{C}(\text{CH}_3)\text{CO}_2\text{CH}_2\text{CH}_2(\text{CF}_2\text{CF}_2)_m\text{F}$ (also referred to as Zonyl[®] fluoromethacrylate or ZFM) wherein m is from 1 to 12, primarily 2 to 8, and 60 weight percent lauryl methacrylate $(\text{CH}_2=\text{C}(\text{CH}_3)\text{CO}_2(\text{CH}_2)_{11}\text{CH}_3$, also referred to as LMA).

In some embodiments, the compatibilizer component contains from about 0.01 to 30 weight percent (based on total amount of compatibilizer) of an additive which reduces the surface energy of metallic copper, aluminum, steel, or other metals and metal alloys thereof found in heat exchangers in a way that reduces the adhesion of lubricants to the metal. Examples of metal surface energy reducing additives include those commercially available from DuPont under the trademarks Zonyl[®] FSA, Zonyl[®] FSP, and Zonyl[®] FSJ.

The additive which may be used with the compositions of the present invention may be a metal surface deactivator. The metal surface deactivator is selected from the group consisting of areoxalyl bis (benzylidene) hydrazide (CAS reg no. 6629-10-3), N,N'-bis(3,5-di-tert-butyl-4-hydroxyhydrocinnamoylhydrazine (CAS reg no. 32687-78-8) , 2,2', - oxamidobis-ethyl-(3,5-di-tert-butyl-4-hydroxyhydrocinnamate (CAS reg no. 70331-94-1), N,N'-(disalicyclidene)-1,2-diaminopropane (CAS reg no. 94-91-7) and ethylenediaminetetra-acetic acid (CAS reg no. 60-00-4) and its salts, and mixtures thereof, meaning mixtures of any of the metal surface deactivators disclosed in this paragraph.

The additive used with the compositions of the present invention may alternatively be a stabilizer selected from the group consisting of hindered phenols, thiophosphates, butylated triphenylphosphorothionates, organo phosphates, or phosphites, aryl alkyl ethers, terpenes, terpenoids, epoxides, fluorinated epoxides, oxetanes, ascorbic acid, thiols, lactones, thioethers, amines, nitromethane, alkylsilanes, benzophenone derivatives, aryl sulfides, divinyl terephthalic acid, diphenyl terephthalic acid, ionic liquids, and mixtures thereof, meaning mixtures of any of the stabilizers disclosed in this paragraph.

The stabilizer may be selected from the group consisting of tocopherol; hydroquinone; t-butyl hydroquinone; monothiophosphates; and dithiophosphates, commercially available from Ciba Specialty Chemicals, Basel, Switzerland, hereinafter "Ciba", under the trademark Irgalube[®] 63; dialkylthiophosphate esters, commercially available from Ciba under the trademarks Irgalube[®] 353 and Irgalube[®] 350, respectively; butylated triphenylphosphorothionates, commercially available from Ciba under the trademark Irgalube[®] 232; amine phosphates, commercially available from Ciba under the trademark Irgalube[®] 349 (Ciba); hindered phosphites, commercially available from Ciba as Irgafos[®] 168 and Tris-(di-tert-butylphenyl)phosphite, commercially available from Ciba under the trademark Irgafos[®] OPH; (Di-n-octyl phosphite); and iso-decyl diphenyl phosphite, commercially available from Ciba under the trademark Irgafos[®] DDPP; trialkyl phosphates, such as trimethyl phosphate, triethylphosphate, tributyl phosphate, trioctyl phosphate, and tri(2-

ethylhexyl)phosphate; triaryl phosphates including triphenyl phosphate, tricresyl phosphate, and trixylenyl phosphate; and mixed alkyl-aryl phosphates including isopropylphenyl phosphate (IPPP), and bis(t-butylphenyl)phenyl phosphate (TBPP); butylated triphenyl phosphates, such as those commercially available under the trademark Syn-O-Ad[®] including Syn-O-Ad[®] 8784; tert-butylated triphenyl phosphates such as those commercially available under the trademark Durad[®] 620; isopropylated triphenyl phosphates such as those commercially available under the trademarks Durad[®] 220 and Durad[®] 110; anisole; 1,4-dimethoxybenzene; 1,4-diethoxybenzene; 1,3,5-trimethoxybenzene; myrcene, alloocimene, limonene (in particular, d-limonene); retinal; pinene; menthol; geraniol; farnesol; phytol; Vitamin A; terpinene; delta-3-carene; terpinolene; phellandrene; fenchene; dipentene; caratenoids, such as lycopene, beta carotene, and xanthophylls, such as zeaxanthin; retinoids, such as hepaxanthin and isotretinoin; bornane; 1,2-propylene oxide; 1,2-butylene oxide; n-butyl glycidyl ether; trifluoromethyloxirane; 1,1-bis(trifluoromethyl)oxirane; 3-ethyl-3-hydroxymethyl-oxetane, such as OXT-101 (Toagosei Co., Ltd); 3-ethyl-3-((phenoxy)methyl)-oxetane, such as OXT-211 (Toagosei Co., Ltd); 3-ethyl-3-((2-ethyl-hexyloxy)methyl)-oxetane, such as OXT-212 (Toagosei Co., Ltd); ascorbic acid; methanethiol (methyl mercaptan); ethanethiol (ethyl mercaptan); Coenzyme A; dimercaptosuccinic acid (DMSA); grapefruit mercaptan ((R)-2-(4-methylcyclohex-3-enyl)propane-2-thiol)); cysteine ((R)-2-amino-3-sulfanyl-propanoic acid); lipoamide (1,2-dithiolane-3-pentanamide); 5,7-bis(1,1-dimethylethyl)-3-[2,3(or 3,4)-dimethylphenyl]-2(3H)-benzofuranone, commercially available from Ciba under the trademark Irganox[®] HP-136; benzyl phenyl sulfide; diphenyl sulfide; diisopropylamine; dioctadecyl 3,3'-thiodipropionate, commercially available from Ciba under the trademark Irganox[®] PS 802 (Ciba); didodecyl 3,3'-thiopropionate, commercially available from Ciba under the trademark Irganox[®] PS 800; di-(2,2,6,6-tetramethyl-4-piperidyl)sebacate, commercially available from Ciba under the trademark Tinuvin[®] 770; poly-(N-hydroxyethyl-2,2,6,6-tetramethyl-4-hydroxy-piperidyl succinate, commercially available from Ciba under the trademark Tinuvin[®] 622LD (Ciba); methyl bis tallow amine; bis tallow

amine; phenol-alpha-naphthylamine; bis(dimethylamino)methylsilane (DMAMS); tris(trimethylsilyl)silane (TTMSS); vinyltriethoxysilane; vinyltrimethoxysilane; 2,5-difluorobenzophenone; 2',5'-dihydroxyacetophenone; 2-aminobenzophenone; 2-chlorobenzophenone; benzyl phenyl sulfide; diphenyl sulfide; dibenzyl sulfide; ionic liquids; and mixtures and combinations thereof.

The additive used with the compositions of the present invention may alternatively be an ionic liquid stabilizer. The ionic liquid stabilizer may be selected from the group consisting of organic salts that are liquid at room temperature (approximately 25 °C), those salts containing cations selected from the group consisting of pyridinium, pyridazinium, pyrimidinium, pyrazinium, imidazolium, pyrazolium, thiazolium, oxazolium and triazolium and mixtures thereof ; and anions selected from the group consisting of [BF₄]⁻, [PF₆]⁻, [SbF₆]⁻, [CF₃SO₃]⁻, [HCF₂CF₂SO₃]⁻, [CF₃HFCCF₂SO₃]⁻, [HCClFCF₂SO₃]⁻, [(CF₃SO₂)₂N]⁻, [(CF₃CF₂SO₂)₂N]⁻, [(CF₃SO₂)₃C]⁻, [CF₃CO₂]⁻, and F⁻ and mixtures thereof. In some embodiments, ionic liquid stabilizers are selected from the group consisting of emim BF₄ (1-ethyl-3-methylimidazolium tetrafluoroborate); bmim BF₄ (1-butyl-3-methylimidazolium tetraborate); emim PF₆ (1-ethyl-3-methylimidazolium hexafluorophosphate); and bmim PF₆ (1-butyl-3-methylimidazolium hexafluorophosphate), all of which are available from Fluka (Sigma-Aldrich).

In some embodiments, the stabilizer may be a hindered phenol, which is any substituted phenol compound, including phenols comprising one or more substituted or cyclic, straight chain, or branched aliphatic substituent group, such as, alkylated monophenols including 2,6-di-tert-butyl-4-methylphenol; 2,6-di-tert-butyl-4-ethylphenol; 2,4-dimethyl-6-tertbutylphenol; tocopherol; and the like, hydroquinone and alkylated hydroquinones including t-butyl hydroquinone, other derivatives of hydroquinone; and the like, hydroxylated thiodiphenyl ethers, including 4,4'-thio-bis(2-methyl-6-tert-butylphenol); 4,4'-thiobis(3-methyl-6-tertbutylphenol); 2,2'-thiobis(4methyl-6-tert-butylphenol); and the like, alkylidene-bisphenols including, : 4,4'-methylenebis(2,6-di-tert-butylphenol); 4,4'-bis(2,6-di-tert-butylphenol); derivatives of 2,2'- or 4,4-

biphenoldiols; 2,2'-methylenebis(4-ethyl-6-tertbutylphenol); 2,2'-methylenebis(4-methyl-6-tertbutylphenol); 4,4'-butylidenebis(3-methyl-6-tert-butylphenol); 4,4'-isopropylidenebis(2,6-di-tert-butylphenol); 2,2'-methylenebis(4-methyl-6-nonylphenol); 2,2'-isobutylidenebis(4,6-dimethylphenol); 2,2'-methylenebis(4-methyl-6-cyclohexylphenol, 2,2- or 4,4'- biphenyldiols including 2,2'-methylenebis(4-ethyl-6-tert-butylphenol); butylated hydroxytoluene (BHT, or 2,6-di-tert-butyl-4-methylphenol), bisphenols comprising heteroatoms including 2,6-di-tert-alpha-dimethylamino-p-cresol, 4,4'-thiobis(6-tert-butyl-m-cresol); and the like; acylaminophenols; 2,6-di-tert-butyl-4-(N,N'-dimethylaminomethylphenol); sulfides including; bis(3-methyl-4-hydroxy-5-tert-butylbenzyl)sulfide; bis(3,5-di-tert-butyl-4-hydroxybenzyl)sulfide and mixtures thereof, meaning mixtures of any of the phenols disclosed in this paragraph.

The additive which is used with compositions of the present invention may alternatively be a tracer. The tracer may be two or more tracer compounds from the same class of compounds or from different classes of compounds. In some embodiments, the tracer is present in the compositions at a total concentration of about 50 parts per million by weight (ppm) to about 1000 ppm, based on the weight of the total composition. In other embodiments, the tracer is present at a total concentration of about 50 ppm to about 500 ppm. Alternatively, the tracer is present at a total concentration of about 100 ppm to about 300 ppm.

The tracer may be selected from the group consisting of hydrofluorocarbons (HFCs), deuterated hydrofluorocarbons, perfluorocarbons, fluoroethers, brominated compounds, iodated compounds, alcohols, aldehydes and ketones, nitrous oxide and combinations thereof. Alternatively, the tracer may be selected from the group consisting of fluoroethane, 1,1,-difluoroethane, 1,1,1-trifluoroethane, 1,1,1,3,3,3-hexafluoropropane, 1,1,1,2,3,3,3-heptafluoropropane, 1,1,1,3,3-pentafluoropropane, 1,1,1,3,3-pentafluorobutane, 1,1,1,2,3,4,4,5,5,5-decafluoropentane, 1,1,1,2,2,3,4,5,5,6,6,7,7,7-tridecafluoroheptane, iodotrifluoromethane, deuterated hydrocarbons, deuterated hydrofluorocarbons, perfluorocarbons, fluoroethers, brominated compounds, iodated

compounds, alcohols, aldehydes, ketones, nitrous oxide (N₂O) and mixtures thereof. In some embodiments, the tracer is a blend containing two or more hydrofluorocarbons, or one hydrofluorocarbon in combination with one or more perfluorocarbons.

- 5 The tracer may be added to the compositions of the present invention in predetermined quantities to allow detection of any dilution, contamination or other alteration of the composition.

 The additive which may be used with the compositions of the present invention may alternatively be a perfluoropolyether. A common
 10 characteristic of perfluoropolyethers is the presence of perfluoroalkyl ether moieties. Perfluoropolyether is synonymous to perfluoropolyalkylether. Other synonymous terms frequently used include "PFPE", "PFAE", "PFPE oil", "PFPE fluid", and "PFP AE". In some embodiments, the perfluoropolyether has the formula of CF₃-(CF₂)₂-O-[CF(CF₃)-CF₂-O]^{j'}-R'^f,
 15 and is commercially available from DuPont under the trademark Krytox[®]. In the immediately preceding formula, j' is 2 - 100, inclusive and R'^f is CF₂CF₃, a C3 to C6 perfluoroalkyl group, or combinations thereof.

 Other PFPEs, commercially available from Ausimont of Milan, Italy, and Montedison S.p.A., of Milan, Italy, under the trademarks Fomblin[®] and
 20 Galden[®], respectively, and produced by perfluoroolefin photooxidation, can also be used.

 PFPE commercially available under the trademark Fomblin[®]-Y can have the formula of CF₃O(CF₂CF(CF₃)-O-)_{m'}(CF₂-O-)_{n'}-R_{1f}. Also suitable is CF₃O[CF₂CF(CF₃)O]_{m'}(CF₂CF₂O)_{o'}(CF₂O)_{n'}-R_{1f}. In the formulae R_{1f} is
 25 CF₃, C₂F₅, C₃F₇, or combinations of two or more thereof; (m' + n') is 8 - 45, inclusive; and m/n is 20 - 1000, inclusive; o' is 1; (m'+n'+o') is 8 - 45, inclusive; m'/n' is 20 - 1000, inclusive.

 PFPE commercially available under the trademark Fomblin[®]-Z can have the formula of CF₃O(CF₂CF₂-O-)_{p'}(CF₂-O)_{q'}CF₃ where (p' + q') is
 30 40 - 180 and p'/q' is 0.5 - 2, inclusive.

 Another family of PFPE, commercially available under the trademark Demnum[™] from Daikin Industries, Japan, can also be used. It can be produced by sequential oligomerization and fluorination of 2,2,3,3-

tetrafluorooxetane, yielding the formula of $F-[(CF_2)_3-O]_{t'}-R_{2f}$ where R_{2f} is CF_3 , C_2F_5 , or combinations thereof and t' is 2 - 200, inclusive.

- In some embodiments, the PFPE is unfunctionalized. In an unfunctionalized perfluoropolyether, the end group can be branched or
- 5 straight chain perfluoroalkyl radical end groups. Examples of such perfluoropolyethers can have the formula of $C_{r'}F_{(2r'+1)}-A-C_{r'}F_{(2r'+1)}$ in which each r' is independently 3 to 6; A can be $O-(CF(CF_3)CF_2-O)_{w'}$, $O-(CF_2-O)_{x'}(CF_2CF_2-O)_{y'}$, $O-(C_2F_4-O)_{w'}$, $O-(C_2F_4-O)_{x'}(C_3F_6-O)_{y'}$, $O-(CF(CF_3)CF_2-O)_{x'}(CF_2-O)_{y'}$, $O-(CF_2CF_2CF_2-O)_{w'}$,
- 10 $O-(CF(CF_3)CF_2-O)_{x'}(CF_2CF_2-O)_{y'}-(CF_2-O)_{z'}$, or combinations of two or more thereof; preferably A is $O-(CF(CF_3)CF_2-O)_{w'}$, $O-(C_2F_4-O)_{w'}$, $O-(C_2F_4-O)_{x'}(C_3F_6-O)_{y'}$, $O-(CF_2CF_2CF_2-O)_{w'}$, or combinations of two or more thereof; w' is 4 to 100; x' and y' are each independently 1 to 100. Specific examples include, but are not limited to,
- 15 $F(CF(CF_3)-CF_2-O)_9-CF_2CF_3$, $F(CF(CF_3)-CF_2-O)_9-CF(CF_3)_2$, and combinations thereof. In such PFPEs, up to 30% of the halogen atoms can be halogens other than fluorine, such as, for example, chlorine atoms.

- In other embodiments, the two end groups of the perfluoropolyether, independently, may be functionalized by the same or
- 20 different groups. A functionalized PFPE is a PFPE wherein at least one of the two end groups of the perfluoropolyether has at least one of its halogen atoms substituted by a group selected from esters, hydroxyls, amines, amides, cyanos, carboxylic acids, sulfonic acids or combinations thereof.

- 25 In some embodiments, representative ester end groups include $-COOCH_3$, $-COOCH_2CH_3$, $-CF_2COOCH_3$, $-CF_2COOCH_2CH_3$, $-CF_2CF_2COOCH_3$, $-CF_2CF_2COOCH_2CH_3$, $-CF_2CH_2COOCH_3$, $-CF_2CF_2CH_2COOCH_3$, $-CF_2CH_2CH_2COOCH_3$, $-CF_2CF_2CH_2CH_2COOCH_3$.

- In some embodiments, representative hydroxyl end groups include
- 30 $-CF_2OH$, $-CF_2CF_2OH$, $-CF_2CH_2OH$, $-CF_2CF_2CH_2OH$, $-CF_2CH_2CH_2OH$, $-CF_2CF_2CH_2CH_2OH$.

In some embodiments, representative amine end groups include $-CF_2NR^1R^2$, $-CF_2CF_2NR^1R^2$, $-CF_2CH_2NR^1R^2$, $-CF_2CF_2CH_2NR^1R^2$,

$-\text{CF}_2\text{CH}_2\text{CH}_2\text{NR}^1\text{R}^2$, $-\text{CF}_2\text{CF}_2\text{CH}_2\text{CH}_2\text{NR}^1\text{R}^2$, wherein R^1 and R^2 are independently H, CH_3 , or CH_2CH_3 .

In some embodiments, representative amide end groups include $-\text{CF}_2\text{C}(\text{O})\text{NR}^1\text{R}^2$, $-\text{CF}_2\text{CF}_2\text{C}(\text{O})\text{NR}^1\text{R}^2$, $-\text{CF}_2\text{CH}_2\text{C}(\text{O})\text{NR}^1\text{R}^2$,

- 5 $-\text{CF}_2\text{CF}_2\text{CH}_2\text{C}(\text{O})\text{NR}^1\text{R}^2$, $-\text{CF}_2\text{CH}_2\text{CH}_2\text{C}(\text{O})\text{NR}^1\text{R}^2$,
 $-\text{CF}_2\text{CF}_2\text{CH}_2\text{CH}_2\text{C}(\text{O})\text{NR}^1\text{R}^2$, wherein R^1 and R^2 are independently H, CH_3 , or CH_2CH_3 .

In some embodiments, representative cyano end groups include

- $-\text{CF}_2\text{CN}$, $-\text{CF}_2\text{CF}_2\text{CN}$, $-\text{CF}_2\text{CH}_2\text{CN}$, $-\text{CF}_2\text{CF}_2\text{CH}_2\text{CN}$, $-\text{CF}_2\text{CH}_2\text{CH}_2\text{CN}$,
 10 $-\text{CF}_2\text{CF}_2\text{CH}_2\text{CH}_2\text{CN}$.

In some embodiments, representative carboxylic acid end groups include $-\text{CF}_2\text{COOH}$, $-\text{CF}_2\text{CF}_2\text{COOH}$, $-\text{CF}_2\text{CH}_2\text{COOH}$, $-\text{CF}_2\text{CF}_2\text{CH}_2\text{COOH}$, $-\text{CF}_2\text{CH}_2\text{CH}_2\text{COOH}$, $-\text{CF}_2\text{CF}_2\text{CH}_2\text{CH}_2\text{COOH}$.

- In some embodiments, the sulfonic acid end groups is selected
 15 from the group consisting of $-\text{S}(\text{O})(\text{O})\text{OR}^3$, $-\text{S}(\text{O})(\text{O})\text{R}^4$, $-\text{CF}_2\text{OS}(\text{O})(\text{O})\text{OR}^3$, $-\text{CF}_2\text{CF}_2\text{OS}(\text{O})(\text{O})\text{OR}^3$, $-\text{CF}_2\text{CH}_2\text{OS}(\text{O})(\text{O})\text{OR}^3$,
 $-\text{CF}_2\text{CF}_2\text{CH}_2\text{OS}(\text{O})(\text{O})\text{OR}^3$, $-\text{CF}_2\text{CH}_2\text{CH}_2\text{OS}(\text{O})(\text{O})\text{OR}^3$,
 $-\text{CF}_2\text{CF}_2\text{CH}_2\text{CH}_2\text{OS}(\text{O})(\text{O})\text{OR}^3$, $-\text{CF}_2\text{S}(\text{O})(\text{O})\text{OR}^3$, $-\text{CF}_2\text{CF}_2\text{S}(\text{O})(\text{O})\text{OR}^3$,
 $-\text{CF}_2\text{CH}_2\text{S}(\text{O})(\text{O})\text{OR}^3$, $-\text{CF}_2\text{CF}_2\text{CH}_2\text{S}(\text{O})(\text{O})\text{OR}^3$,
 20 $-\text{CF}_2\text{CH}_2\text{CH}_2\text{S}(\text{O})(\text{O})\text{OR}^3$, $-\text{CF}_2\text{CF}_2\text{CH}_2\text{CH}_2\text{S}(\text{O})(\text{O})\text{OR}^3$, $-\text{CF}_2\text{OS}(\text{O})(\text{O})\text{R}^4$,
 $-\text{CF}_2\text{CF}_2\text{OS}(\text{O})(\text{O})\text{R}^4$, $-\text{CF}_2\text{CH}_2\text{OS}(\text{O})(\text{O})\text{R}^4$, $-\text{CF}_2\text{CF}_2\text{CH}_2\text{OS}(\text{O})(\text{O})\text{R}^4$,
 $-\text{CF}_2\text{CH}_2\text{CH}_2\text{OS}(\text{O})(\text{O})\text{R}^4$, $-\text{CF}_2\text{CF}_2\text{CH}_2\text{CH}_2\text{OS}(\text{O})(\text{O})\text{R}^4$, wherein R^3 is H, CH_3 , CH_2CH_3 , CH_2CF_3 , CF_3 , or CF_2CF_3 , R^4 is CH_3 , CH_2CH_3 , CH_2CF_3 , CF_3 , or CF_2CF_3 .

- 25 The additives may be members of the triaryl phosphate family of EP (extreme pressure) lubricity additives, such as butylated triphenyl phosphates (BTPP), or other alkylated triaryl phosphate esters, such as those sold under the trademark Syn-0-Ad[®] 8478 from Akzo Chemicals, tricresyl phosphates and related compounds. Additionally, the metal
 30 dialkyl dithiophosphates (e.g., zinc dialkyl dithiophosphate (or ZDDP), including the commercially available Lubrizol 1375 and other members of this family of chemicals is used in compositions of the disclosed compositions. Other antiwear additives include natural product oils and

asymmetrical polyhydroxyl lubrication additives, such as the commercially available Synergol TMS (International Lubricants).

In some embodiments, stabilizers such as antioxidants, free radical scavengers, and water scavengers and mixtures thereof are included.

- 5 Such additives in this category can include, but are not limited to, butylated hydroxy toluene (BHT), epoxides, and mixtures thereof. Corrosion inhibitors include dodecyl succinic acid (DDSA), amine phosphate (AP), oleoyl sarcosine, imidazone derivatives and substituted sulfonates.

- 10 In one embodiment, the compositions disclosed herein may be prepared by any convenient method to combine the desired amounts of the individual components. A preferred method is to weigh the desired component amounts and thereafter combine the components in an appropriate vessel. Agitation may be used, if desired.

- 15 In another embodiment, the compositions disclosed herein may be prepared by a method comprising (i) reclaiming a volume of one or more components of a refrigerant composition from at least one refrigerant container, (ii) removing impurities sufficiently to enable reuse of said one or more of the reclaimed components, (iii) and optionally, combining all or
20 part of said reclaimed volume of components with at least one additional refrigerant composition or component.

- A refrigerant container may be any container in which is stored a refrigerant blend composition that has been used in a refrigeration apparatus, air-conditioning apparatus or heat pump apparatus. Said
25 refrigerant container may be the refrigeration apparatus, air-conditioning apparatus or heat pump apparatus in which the refrigerant blend was used. Additionally, the refrigerant container may be a storage container for collecting reclaimed refrigerant blend components, including but not limited to pressurized gas cylinders.

- 30 Residual refrigerant means any amount of refrigerant blend or refrigerant blend component that may be moved out of the refrigerant container by any method known for transferring refrigerant blends or refrigerant blend components.

Impurities may be any component that is in the refrigerant blend or refrigerant blend component due to its use in a refrigeration apparatus, air-conditioning apparatus or heat pump apparatus. Such impurities include but are not limited to refrigeration lubricants, being those described earlier
5 herein, particulates including but not limited to metal, metal salt or elastomer particles, that may have come out of the refrigeration apparatus, air-conditioning apparatus or heat pump apparatus, and any other contaminants that may adversely effect the performance of the refrigerant blend composition.

10 Such impurities may be removed sufficiently to allow reuse of the refrigerant blend or refrigerant blend component without adversely effecting the performance or equipment within which the refrigerant blend or refrigerant blend component will be used.

It may be necessary to provide additional refrigerant blend or
15 refrigerant blend component to the residual refrigerant blend or refrigerant blend component in order to produce a composition that meets the specifications required for a given product. For instance, if a refrigerant blend has 3 components in a particular weight percentage range, it may be necessary to add one or more of the components in a given amount in
20 order to restore the composition to within the specification limits.

Compositions of the present invention have zero ozone depletion potential and low global warming potential (GWP). Additionally, the compositions of the present invention will have global warming potentials that are less than many hydrofluorocarbon refrigerants currently in use.
25 One aspect of the present invention is to provide a refrigerant with a global warming potential of less than 1000, less than 700, less than 500, less than 400, less than 300, less than 150, less than 100, or less than 50.

Methods of use

30 The compositions disclosed herein are useful as heat transfer compositions, aerosol propellants, foaming agents, blowing agents, solvents, cleaning agents, carrier fluids, displacement drying agents, buffing abrasion agents, polymerization media, expansion agents for polyolefins and polyurethane, gaseous dielectrics, fire extinguishing

agents, fire suppression agents and power cycle working fluids.

Additionally, in liquid or gaseous form, the disclosed compositions may act as working fluids used to carry heat from a heat source to a heat sink.

Such heat transfer compositions may also be useful as refrigerants in a cycle wherein the fluid undergoes phase changes; that is, from a liquid to a gas and back or vice versa.

The compositions disclosed herein may be useful as low GWP (global warming potential) replacements for currently used refrigerants, including but not limited to R410A (ASHRAE designation for a blend of 50 weight percent R125 and 50 weight percent R32) or R404A (ASHRAE designation for a blend of 44 weight percent R125, 52 weight percent R143a (1,1,1-trifluoroethane), and 4.0 weight percent R134a).

Often replacement refrigerants are most useful if capable of being used in the original refrigeration equipment designed for a different refrigerant. Additionally, the compositions as disclosed herein may be useful as replacements for R410A or R404A in equipment designed for R410A or R404A with some system modifications. Further, the compositions as disclosed herein comprising HFO-1234yf and HFC-32 may be useful for replacing R404A or R410A in equipment specifically modified for or produced entirely for these new compositions comprising HFO-1234yf and HFC-32.

In many applications, some embodiments of the disclosed compositions are useful as refrigerants and provide at least comparable cooling performance (meaning cooling capacity and energy efficiency) as the refrigerant for which a replacement is being sought.

In some embodiments, the compositions disclosed herein are useful for any positive displacement compressor system designed for any number of heat transfer compositions. Additionally, many of the compositions disclosed are useful in new equipment utilizing positive displacement compressors to provide similar performance to the aforementioned refrigerants.

In one embodiment, disclosed herein is a process to produce cooling comprising condensing a composition as disclosed herein and

thereafter evaporating said composition in the vicinity of a body to be cooled.

In another embodiment, disclosed herein is a process to produce heat comprising condensing a composition as disclosed herein in the vicinity of a body to be heated and thereafter evaporating said composition.

In some embodiments, the use of the above disclosed compositions includes using the composition as a heat transfer composition in a process for producing cooling, wherein the composition is first cooled and stored under pressure and when exposed to a warmer environment, the composition absorbs some of the ambient heat, expands, and the warmer environment is thusly cooled.

In some embodiments, the compositions as disclosed herein may be useful in particular in air conditioning applications including but not limited to chillers, high temperature heat pumps, residential, commercial or industrial air conditioning systems (including residential heat pumps), and including window, ductless, ducted, packaged terminal, chillers, and those exterior but connected to the building such as rooftop systems.

In another embodiment the compositions as disclosed herein are useful in automotive heat pumps. Of particular note are compositions having about 21.5 weight percent HFC-32 and about 78.5 weight percent HFC-1234yf that have been found to provide improved heating capacity versus HFC-134a and has a GWP less than 150.

In some embodiments, the compositions as disclosed herein may be useful in particular in refrigeration applications including high, medium or low temperature refrigeration. High temperature refrigeration systems include those for supermarket produce sections among others. Medium temperature refrigeration systems includes supermarket and convenience store refrigerated cases for beverages, dairy and other items requiring refrigeration. Low temperature refrigeration systems include supermarket and convenience store freezer cabinets and displays, ice machines and frozen food transport. Other specific uses such as in commercial, industrial or residential refrigerators and freezers, ice machines, self-contained coolers and freezers, supermarket rack and distributed systems, flooded

evaporator chillers, direct expansion chillers, walk-in and reach-in coolers and freezers, and combination systems.

Additionally, in some embodiments, the disclosed compositions may function as primary refrigerants in secondary loop systems that
5 provide cooling to remote locations by use of a secondary heat transfer fluid, which may comprise water, a glycol or carbon dioxide.

In another embodiment is provided a method for recharging a heat transfer system that contains a refrigerant to be replaced and a lubricant, said method comprising removing the refrigerant to be replaced from the
10 heat transfer system while retaining a substantial portion of the lubricant in said system and introducing one of the compositions herein disclosed to the heat transfer system.

In another embodiment, a heat exchange system comprising a composition disclosed herein is provided, wherein said system is selected
15 from the group consisting of air conditioners, freezers, refrigerators, water chillers, flooded evaporator chillers, direct expansion chillers, walk-in coolers, heat pumps, mobile refrigerators, mobile air conditioning units, and systems having combinations thereof.

Vapor-compression refrigeration, air-conditioning, or heat pump
20 systems include an evaporator, a compressor, a condenser, and an expansion device. A vapor-compression cycle re-uses refrigerant in multiple steps producing a cooling effect in one step and a heating effect in a different step. The cycle can be described simply as follows. Liquid refrigerant enters an evaporator through an expansion device, and the
25 liquid refrigerant boils in the evaporator, by withdrawing heat from the environment, at a low temperature to form a gas and produce cooling. The low-pressure gas enters a compressor where the gas is compressed to raise its pressure and temperature. The higher-pressure (compressed) gaseous refrigerant then enters the condenser in which the refrigerant
30 condenses and discharges its heat to the environment. The refrigerant returns to the expansion device through which the liquid expands from the higher-pressure level in the condenser to the low-pressure level in the evaporator, thus repeating the cycle.

In one embodiment, there is provided a heat transfer system containing a composition as disclosed herein. In another embodiment is disclosed a refrigeration, air-conditioning, or heat pump apparatus containing a composition as disclosed herein. In another embodiment, is
5 disclosed a stationary refrigeration, air-conditioning, or heat pump apparatus containing a composition as disclosed herein. In a particular embodiment, is disclosed a medium temperature refrigeration apparatus containing the composition of the present invention. In another particular embodiment, is disclosed a low temperature refrigeration apparatus
10 containing the composition of the present invention.

In yet another embodiment is disclosed a mobile refrigeration or air conditioning apparatus containing a composition as disclosed herein.

The compositions as disclosed herein may also be useful as power cycle working fluids in heat recovery processes, such as organic Rankine
15 cycles. In relation to this embodiment is disclosed a process for recovering heat which comprises: (a) passing a working fluid through a first heat exchanger in communication with a process which produces heat; (b) removing said working fluid from said first heat exchanger; (c) passing said working fluid to a device that produces mechanical energy;
20 and (d) passing said working fluid to a second heat exchanger.

The power cycle working fluids for the above described method may be any of the compositions as disclosed herein. In the first heat exchanger heat is absorbed by the working fluid causing it to be evaporated. The heat source may comprise any source of available heat
25 including waste heat. Such heat sources include fuel cells, internal combustion engines (exhaust gas), internal compression engines, external combustion engines, operations at oil refineries, petrochemical plants, oil and gas pipelines, chemical industry, commercial buildings, hotels, shopping malls supermarkets, bakeries, food processing industries,
30 restaurants, paint curing ovens, furniture making, plastics molders, cement kilns, lumber kilns (drying), calcining operations, steel industry, glass industry, foundries, smelting, air conditioning, refrigeration, and central heating.

The device for producing mechanical energy may be an expander or a turbine thus producing shaft power that can do any kind of mechanical work by employing conventional arrangements of belts, pulleys, gears, transmissions or similar devices depending on the desired speed and torque required. The shaft can be connected to an electric power-generating device such as an induction generator. The electricity produced can be used locally or delivered to the grid.

At the second heat exchanger, the working fluid is condensed and then returned to the first heat exchanger thus completing the cycle. A compressor or pump may be included in the cycle between the second heat exchanger and the first heat exchanger to elevate the pressure of the working fluid.

EXAMPLES

The concepts disclosed herein will be further described in the following examples, which do not limit the scope of the invention described in the claims.

EXAMPLE 1

Cooling performance

Cooling performance for a composition containing HFO-1234yf and HFC-32 is determined and displayed in Table 1 as compared to R410A (ASHRAE designation for a refrigerant blend containing 50 wt% HFC-32 and 50 wt% HFC-125). The pressures, discharge temperatures, COP (energy efficiency) and cooling capacity (cap) are calculated from physical property measurements for the following specific conditions (as typical for air conditioning):

	Evaporator temperature	45 °F (7.2 °C)
	Condenser temperature	110 °F (43.3 °C)
30	Subcool amount	5 °F (2.8 °C)
	Return gas temperature	65 °F (18.3 °C)
	Compressor efficiency is	70%

Note that the superheat is included in cooling capacity.

TABLE 1

Composition	Pres evap, kPa	Pres cond, kPa	Disch Temp, ° C	COP	COP rel. to R410A (%)	Cap (kJ/m ³)	Cap rel. to R410A (%)	Temp Glide, °C (Cond/Evap)
R410A	991	2589	82.8	4.12		5830		0.17/0.1
HFO-1234yf	398	1104	60.5	4.44	108	2642	45.3	0
HFC-32	1016	2692	102.8	4.19	102	6438	110.4	0
HFO- 1234yf/HFC- 32 (80/20 wt%)	596	1650	67.3	4.295	104	3758	64.5	7.1/6.0
HFO- 1234yf/HFC- 32 (70/30 wt%)	685	1868	73.4	4.25	103	4251	72.9	6.7/6.0
HFO- 1234yf/HFC- 32 (55/45 wt%)	801	2145	79.4	4.20	102	4886	83.8	4.7/4.4
HFO- 1234yf/HFC- 32 (45/55 wt%)	867	2299	83.2	4.19	102	5269	90.4	3.3/3.0
HFO- 1234yf/HFC- 32 (35/65 wt%)	922	2427	87.2	4.19	102	5615	96.3	2.0/1.7
HFO- 1234yf/HFC- 32 (30/70 wt%)	945	2482	89.2	4.19	102	5771	99.0	1.5/1.2
HFO- 1234yf/HFC- 32 (25/75 wt%)	964	2531	91.3	4.19	102	5913	101	1.1/0.8
HFO- 1234yf/HFC-	980	2574	93.4	4.19	102	6042	104	0.7/0.5

32 (20/80 wt%)								
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These data indicate that certain compositions of the present invention would serve as good replacements for R410A and even provide improvements over pure HFC-32. Of note are compositions ranging from 20 weight percent to 55 weight percent HFO-1234yf and 80 weight percent to 45 weight percent HFC-32 that provide cooling capacity with $\pm 20\%$ of that for R410a, improved energy efficiency (COP) compared to R410A and low temperature glide. When compared to pure HFC-32, certain of these compositions provide a better match to R410a, for example, in cooling capacity and lower discharge temperatures (thus increasing compressor life). In particular, the compositions ranging from 25 weight percent to 30 weight percent HFO-1234yf provide between 99-101% capacity relative to R410A, 102% COP relative to R410A and a lower compressor discharge temperature than R-32.

15

EXAMPLE 2

Heating Performance

Table 2 shows the performance of some exemplary compositions as compared to HFC-134a, HFO-1234yf, and R410A at typical heat pump conditions. In Table 2, Evap Pres is evaporator pressure, Cond Pres is condenser pressure, Comp Disch T is compressor discharge temperature, COP is coefficient of performance (analogous to energy efficiency), and CAP is capacity. The calculated data are based on physical property measurements and the following specific conditions.

25 Evaporator temperature 32 °F (0 °C)
 Condenser temperature 113 °F (45 °C)
 Subcool amount 21.6 °F (12 K)
 Return gas superheat 5.4 °F (3 K)
 Compressor efficiency is 70%

TABLE 2

Composition	Evap Press (kPa)	Cond Press (kPa)	Compr Disch Temp (° C)	COP	COP relative to R410A (%)	CAP (kJ/m ³)	CAP relative to R410A (%)	Temp Glide, ° C (cond/ evap)
HFC-134a	293	1160	64.6	4.724	106	2795	43	0
HFO-1234yf	314	1151	54	4.621	103.7	2681	41.3	0
R410A	794	2695	83	4.547	100	6470	100	0.17/0.1
HFO-1234yf/HFC-32 78.5 / 21.5 wt %	490	1766	70	4.563	102.4	4161	64	7.2 / 6.5
HFO-1234yf/HFC-32 57.5 / 42.5 wt %	632	2206	80	4.496	100.9	5273	81	5.0 / 4.9
HFO-1234yf/HFC-32 27.5 / 72.5 wt %	770	2623	93	4.485	100.6	6506	100	1.2 / 0.9
HFO-1234yf/HFC-32 42.5 / 57.5 wt %	712	2445	86	4.607	100.6	5947	91.5	2.8 / 2.6

These data indicates that these compositions may serve as replacements for R410A in heat pump applications. In particular,

5 compositions ranging from about 25 weight percent to about 60 weight percent HFO-1234yf and about 75 weight percent to about 40 weight percent HFC-32 are demonstrated as having heating capacity within \pm 20% of that for R410A, slightly improved energy efficiency (COP) and average temperature glide of less than about 5 °C. Additionally, the

10 composition having 78.5 weight percent HFO-1234yf and 21.5 weight percent HFC-32 provides significantly improved heating capacity versus HFC-134a, such that it could serve as a low GWP replacement for HFC-134a in, for example, automotive heat pumps.

15

EXAMPLE 3 **Flammability**

Flammable compounds may be identified by testing under ASTM (American Society of Testing and Materials) E681-2004, with an electronic ignition source. Such tests of flammability were conducted on

20 compositions of the present disclosure at 101 kPa (14.7 psia), 50 percent

relative humidity, and 23 °C and 100 °C at various concentrations in air in order to determine the lower flammability limit (LFL). The results are given in Table 3.

TABLE 3

Composition (weight percent)	LFL (vol % in air)	
	23 °C	100 °C
HFO-1234yf/HFC-32 (45/55 wt%)	11.0	10.0
HFO-1234yf/HFC-32 (55/45 wt%)	10.0	9.0
HFO-1234yf/HFC-32 (70/30 wt%)	8.5	7.5

5

These data demonstrate that the compositions comprising HFO-1234yf and HFC-32 with less than 45 weight percent HFO-1234yf may be classified as non-flammable in Japan due to LFL of greater than 10 volume percent.

10

EXAMPLE 4

Global Warming Potentials

Values for global warming potential (GWP) for some of the disclosed compositions are listed in Table 4 as compared to GWP values for HCFC-22, HFC-134a, R404A, and R410A. The GWP for the pure components are listed for reference. The GWP values for compositions containing more than one component are calculated as weighted averages of the individual component GWP values. The values for the HFCs are taken from the "Climate Change 2007 – IPCC (Intergovernmental Panel on Climate Change) Fourth Assessment Report on Climate Change", from the section entitled "Working Group 1 Report: "The Physical Science Basis", Chapter 2, pp. 212-213, Table 2.14. The value for HFO-1234yf was published in Papadimitriou et al., *Physical Chemistry Chemical Physics*, 2007, vol. 9, pp. 1-13. Specifically, the 100 year time horizon GWP values are used.

25

TABLE 4

Component or composition	GWP
HCFC-22	1810
HFC-134a	1430
HFC-32	675
HFO-1234yf	4
R404A	3922
R507	3985
R410A	2088
HFO-1234yf/HFC-32 (90/10 wt %)	71
HFO-1234yf/HFC-32 (80/20 wt %)	138
HFO-1234yf/HFC-32 (78.5/21.5 wt %)	148
HFO-1234yf/HFC-32 (70/30 wt %)	205
HFO-1234yf/HFC-32 (57.5/42.5 wt %)	289
HFO-1234yf/HFC-32 (55/45 wt %)	306
HFO-1234yf/HFC-32 (50/50 wt %)	340
HFO-1234yf/HFC-32 (45/55 wt %)	373
HFO-1234yf/HFC-32 (35/65 wt %)	440
HFO-1234yf/HFC-32 (30/70 wt %)	474
HFO-1234yf/HFC-32 (27.5/72.5 wt %)	490
HFO-1234yf/HFC-32 (20/80wt %)	541

- Many compositions as disclosed herein provide lower GWP alternatives to HCFC-22, R404A, and/or R410A etc. Additionally, the addition of HFO-1234yf to HFC-32 can provide significantly lower GWP refrigerants than HFC-32 alone.

EXAMPLE 5

Refrigeration Performance

- Table 5 shows the performance of some exemplary compositions as compared to HFO-1234yf, HFC-32, and R404A. In Table 5, Evap Pres is evaporator pressure, Cond Pres is condenser pressure, Comp Disch T is compressor discharge temperature, COP is coefficient of performance (analogous to energy efficiency), and CAP is cooling capacity. The data are based on the following conditions.

Evaporator temperature 14 °F (-10 °C)
 Condenser temperature 104 °F (40 °C)
 Subcool amount 2.8 °F (6 K)
 Return gas temperature 65 °F (18°C)

5 Compressor efficiency is 70%

Note that the evaporator superheat enthalpy is included in cooling capacity and energy efficiency determinations.

TABLE 5

Composition	Evap Press (kPa)	Cond Press (kPa)	Compr Disch Temp (°C)	COP	COP relative to R404A (%)	CAP (kJ/m ³)	CAP relative to R404A (%)	Temp Glide, °C (avg)
R404A	436	1833	84.9	2.836		2602		0.37
HFO-1234yf	221	1016	76.5	3.024	107	1490	57.2	0
HFC-32	581	2485	144	2.756	97.2	3777	145	0
HFO-1234yf/HFC-32 (35/65 wt %)	530	2243	119	2.800	98.7	3337	128	1.8
HFO-1234yf/HFC-32 (45/55 wt %)	497	2124	112	2.809	99.0	3127	120.2	3.1
HFO-1234yf/HFC-32 (55/45 wt %)	457	1982	106	2.827	99.7	2892	111	4.6
HFO-1234yf/HFC-32 (70/30 wt %)	387	1726	97.2	2.873	101	2498	96.0	6.3
HFO-1234yf/HFC-32 (78.5/21.5wt %)	343	1556	91.8	2.912	103	2247	86.4	6.6
HFO-1234yf/HFC-32 (80/20 wt %)	335	1524	90.9	2.917	103	2199	84.5	6.5
HFO-1234yf/HFC-32 (90/10 wt %)	279	1291	84.3	2.968	105	1869	71.8	4.9

10 The data in Table 5 demonstrates that compositions from about 45 weight percent to about 80 weight percent HFO-1234yf have capacity

±20% that of R404A and would therefore perform as replacements for R404A in low temperature refrigeration applications. Also, for the compositions in Table 5, the energy efficiency (displayed above as COP) falls within just a few percent of or even improves over energy efficiency for R404A. They also have significantly lower compressor discharge temperatures than HFC-32 which can increase compressor life.

EXAMPLE 6

Refrigeration Performance

Table 6 shows the performance of some exemplary compositions as compared to HFO-1234yf, HFC-32, and R404A. In Table 6, Evap Pres is evaporator pressure, Cond Pres is condenser pressure, Comp Disch T is compressor discharge temperature, COP is coefficient of performance (analogous to energy efficiency), and CAP is cooling capacity. The data are based on the following conditions.

Evaporator temperature	14 °F (-35 °C)
Condenser temperature	104 °F (40 °C)
Subcool amount	2.8 °F (6 K)
Return gas temperature	65 °F (18°C)

Compressor efficiency is 70%

Note that the evaporator superheat enthalpy is included in cooling capacity and energy efficiency determinations.

TABLE 6

Composition	Evap Press (kPa)	Cond Press (kPa)	Compr Disch Temp (°C)	CAP (kJ/m ³)	CAP relative to R404A (%)	COP	COP relative to R404A (%)	Temp Glide, °C (avg)
R404A	167	1833	126	974.4		1.573		0.37
HFO-1234yf	78.3	1016	114	519.4	53.3	1.682	107	0
HFC-32	221	2485	229	1404	144	1.478	94.0	0
HFO-1234yf/HFC-32 (35/65 wt %)	203	2243	184	1246	128	1.522	96.8	1.6
HFO-1234yf/HFC-32 (45/55 wt %)	188	2124	174	1156	119	1.531	97.3	2.8
HFO-1234yf/HFC-32 (55/45 wt %)	171	1982	163	1058	109	1.545	98.2	4.3
HFO-1234yf/HFC-32 (70/30 wt %)	142	1726	147	897	92.1	1.579	100	6.4
HFO-1234yf/HFC-32 (78.5/21.5 wt %)	124	1556	139	796	81.7	1.602	102	6.1
HFO-1234yf/HFC-32 (80/20 wt %)	121	1524	137	777	79.7	1.606	102	6.0
HFO-1234yf/HFC-32 (90/10 wt %)	99.7	1291	126	654	67.1	1.643	104.5	4.7

The data demonstrates that compositions from about 45 weight percent to about 80 weight percent HFO-1234yf have capacity $\pm 20\%$ that of R404A and would therefore perform as replacements for R404A in low temperature refrigeration applications. Also, for the compositions in Table 6, the energy efficiency (displayed above as COP) falls within just a few percent of or even improves over energy efficiency for R404A. They also have significantly lower compressor discharge temperatures than HFC-32 which can increase compressor life.

CLAIMS

What is claimed is:

1. A composition comprising about 1 weight percent to about 80
5 weight percent 2,3,3,3-tetrafluoropropene and about 99 weight
percent to about 20 weight percent difluoromethane.
2. The composition of claim 1 comprising about 30 weight percent to
about 80 weight percent 2,3,3,3-tetrafluoropropene and about 70
10 weight percent to about 20 weight percent difluoromethane.
3. The composition of claim 1 comprising about 45 weight percent to
about 80 weight percent 2,3,3,3-tetrafluoropropene and about 55
weight percent to about 20 weight percent difluoromethane.
15
4. The composition of claim 1 comprising about 55 weight percent to
about 80 weight percent 2,3,3,3-tetrafluoropropene and about 45
weight percent to about 20 weight percent difluoromethane.
- 20 5. The composition of claim 1 comprising about 45 weight percent to
about 55 weight percent 2,3,3,3-tetrafluoropropene and about 55
weight percent to about 45 weight percent difluoromethane.
6. The composition of claim 1 further comprising at least one lubricant
25 selected from the group consisting of mineral oils, alkylbenzenes,
synthetic paraffins, synthetic naphthenes, poly alpha olefins,
polyalkylene glycols, dibasic acid esters, polyesters, neopentyl
esters, polyvinyl ethers, silicones, silicate esters, fluorinated
compounds, phosphate esters and mixtures thereof.
- 30 7. The composition of claim 1 further comprising at least one additive
selected from the group consisting of lubricants, dyes (including UV
dyes), solubilizing agents, compatibilizers, stabilizers, tracers,
perfluoropolyethers, anti wear agents, extreme pressure agents,

corrosion and oxidation inhibitors, metal surface energy reducers, metal surface deactivators, free radical scavengers, foam control agents, viscosity index improvers, pour point depressants, detergents, viscosity adjusters, and mixtures thereof.

5

8. A process to produce cooling comprising condensing the composition of claim 1 and thereafter evaporating said composition in the vicinity of a body to be cooled.

10 9. A process to produce heat comprising condensing the composition of claim 1 in the vicinity of a body to be heated and thereafter evaporating said composition.

15 10. A method for replacing R410A in a system designed to use R410A, wherein said method comprises providing the composition of claim 1 to said system.

20 11. A method for replacing R404A in a system designed to use R404A, wherein said method comprises providing the composition of claim 3 to said system.

12. A refrigeration, air-conditioning or heat pump apparatus containing the composition of claim 1.

25 13. A stationary air conditioning apparatus containing the composition of claim 1.

14. A stationary refrigeration system containing the composition of claim 3.

30

15. Use of the compositions of any of claims 1 through 7 as a power cycle working fluid.

16. An automotive air conditioner or heat pump containing the composition of claim 1.

INTERNATIONAL SEARCH REPORT

International application No
PCT/US2010/061611

A. CLASSIFICATION OF SUBJECT MATTER
INV. C09K5/04
ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
C09K

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EP0-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 2006/243944 A1 (MINOR BARBARA H [US] ET AL) 2 November 2006 (2006-11-02) paragraphs [0001], [0006]; table 9 claims 3,14-16,46,47,55-59 -----	1-16
X	WO 2009/116282 A1 (DAIKIN IND LTD [JP]; MATSUURA HIDEKI [JP]; TANAKA MASARU [JP]; HARA HI) 24 September 2009 (2009-09-24) the whole document	1-4,6-9, 12-14,16
E	-& EP 2 267 311 A1 (DAIKIN IND LTD [JP]) 29 December 2010 (2010-12-29) paragraph [0109]; claims ----- -/--	1-4,6-9, 12-14,16



Further documents are listed in the continuation of Box C.



See patent family annex.

* Special categories of cited documents :

"A" document defining the general state of the art which is not considered to be of particular relevance

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"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

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Date of the actual completion of the international search

17 March 2011

Date of mailing of the international search report

23/03/2011

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