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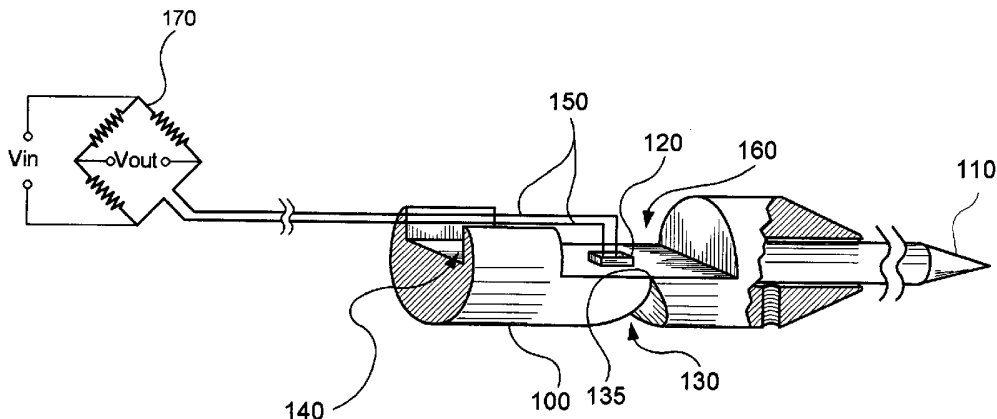
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(54) Title: STRAIN DETECTION FOR AUTOMATED NANO-MANIPULATION



(57) Abstract: We disclose a strain detector for in-situ lift-out, comprising a nano-manipulator probe shaft; a strain gauge mounted on the probe shaft; and a first cut-out on the probe shaft. The first cut-out has a rectangular cross-section. There is a second cut-out on the probe shaft; the second cut-out having a semicircular cross-section. The second cut-out is positioned on the shaft opposite from the first cut-out; the first and second cut-outs, thus defining a thinned region in the probe. The strain gauge is mounted on the probe shaft at the location of the thinned region. There is detecting circuitry for detecting, amplifying and conditioning the output of the strain gauge; and, wires electrically connecting the strain gauge to the detection circuitry. The wires are preferably located in a trench in the probe shaft. Other embodiments are disclosed with multiple strain gauges and detectors, as well as methods of use.



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**Strain Detection for Automated Nano-Manipulation**

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**Patent Application of**

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**Thomas M. Moore**

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**Claim for Priority**

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This application claims the priority of United States provisional application  
16 serial no. 60/592,3322, filed July 28, 2004 and having the title of "Strain detection for  
17 automated nano-manipulation."

18

**Technical Field**

19

This disclosure relates to the removal of specimens inside focused ion-beam  
20 (FIB) microscopes and the preparation of specimens for later analysis in the  
21 transmission electron microscope (TEM), and apparatus to facilitate these activities.  
22 This disclosure also relates to the mechanical testing of materials and tiny structures  
23 outside a FIB.

**Background**

25

The use of In-Situ Lift-Out (INLO) for TEM sample preparation in the FIB has  
26 become a popular and widely accepted technique. INLO enables the preparation of  
27 multiple site-specific TEM samples, at different angles of inspection, and with the  
28 imaging resolution of a Scanning Electron Microscope (SEM), without the need for an  
29 expensive wet lab for conventional sawing, polishing and grinding, and without the need  
30 to sacrifice the wafer being inspected. The ability to perform process control on 300  
31 mm diameter wafers without sacrificing wafers for the inspection is very important  
32 because of the value of these wafers.

1           However, accurate process control requires high throughput TEM sample  
2 preparation. Automation of the sample preparation process will significantly and  
3 favorably impact the analytical throughput of this process and its repeatability.

4           A key apparatus for INLO is an in-situ nano-manipulator that enables full wafer  
5 analysis, such as the AutoProbe 200™ manufactured by Omniprobe, Inc. This nano-  
6 manipulator can be used to lift-out a tiny wedge-shaped portion (typically 5 x 5 x 10  
7 μm) of the sample and to transfer it to a TEM sample holder that is also present in the  
8 FIB vacuum chamber.

9           Ion or electron-beam assisted deposition of metal or other materials from  
10 appropriate source gases injected near the surface in the FIB can be used to attach the  
11 nano-manipulator probe tip to the excised lift-out sample. The same beam-assisted gas  
12 chemistry can be used to attach the lift-out sample to the TEM sample holder. Later, the  
13 ion beam in the FIB can be used to detach the probe tip from the lift-out sample,  
14 completing the in-situ transfer of the lift-out sample to the TEM sample holder. This  
15 lift-out sample can then be thinned to an appropriate thickness for TEM inspection  
16 (<100 nm).

17           Surface contact detection is a critical element of the automation of such a nano-  
18 manipulator-based operation. One of the methods that can be used to determine that the  
19 contact between the nano-manipulator probe tip and the sample surface has been made  
20 is electrical continuity detection. This method is impractical for automation due to  
21 several reasons. If the sample surface is non-conductive, the detection of the steady-  
22 state electrical continuity between the probe tip and the sample surface will not be  
23 successful. Even if the sample surface is electrically conductive, it may not be  
24 electrically connected to the sample holder, or there may be a tough native oxide on the  
25 conductive surface making continuity detection difficult. Without an electrical  
26 connection to the sample holder, continuity detection between the probe tip and sample  
27 surface will be difficult in the FIB environment. Detection of a transient electrical  
28 response due to the connection of the charged sample surface with the probe tip is also  
29 impractical for repetitive automated procedures because this effect is time and material  
30 dependent and also depends on the behavior of the charged particle beams impinging the  
31 surface.

32           A metal layer that covers the surface of the sample and electrically connects the  
33 surface and the sample stage may be deposited using an appropriate gas source and

1 electron or ion beam assisted deposition in the FIB. Such a deposition operation is time  
2 consuming in the FIB, however, and may render the wafer useless for further processing.  
3 In addition, the ion beam may locally remove the metal layer at the place where the  
4 probe tip makes contact with a sample surface and hence defeat the purpose of the  
5 inspection.

6 What is needed is a safe and reliable method of detecting contact between the  
7 sample and the probe of the nano-manipulator, whether inside or outside of a FIB.

#### 8 **Summary**

9 We disclose a strain detector for in-situ lift-out, comprising a nano-manipulator  
10 probe shaft; a strain gauge mounted on the probe shaft; and a first cut-out on the probe  
11 shaft. The first cut-out has a rectangular cross-section. There is a second cut-out on the  
12 probe shaft; the second cut-out having a semicircular cross-section. The second cut-out  
13 is positioned on the shaft opposite from the first cut-out; the first and second cut-outs  
14 thus defining a thinned region in the probe. The strain gauge is mounted on the probe  
15 shaft at the location of the thinned region. There is detecting circuitry for detecting,  
16 amplifying and conditioning the output of the strain gauge; and, wires electrically  
17 connecting the strain gauge to the detection circuitry. The wires are preferably located  
18 in a trench in the probe shaft.

#### 19 **Drawings**

20 Figure 1 shows a perspective view of the preferred embodiment, depicting a  
21 modified probe shaft with a strain gauge attached to it.

22 Figure 2 shows another embodiment, depicting multiple strain gauges.

#### 23 **Description**

24 A sensitive strain gauge mounted in the probe shaft of the nano-manipulator can  
25 function as an efficient surface contact detector in the FIB. Such a detection method  
26 based on mechanical strain in the probe shaft is independent of electrical continuity  
27 effects and will function efficiently on any type of sample surface. The sensitivity of  
28 such a method depends on the type of strain gauge used, the detection circuitry, the  
29 position of the strain gauge on the shaft, and the mechanical design of the probe shaft.  
30 In the preferred embodiment, a tiny (<1 mm<sup>2</sup>) electrical resistance-based silicon strain  
31 gauge is effectively used to measure the level of strain necessary for reliable automation  
32 of surface contact detection. Other types of strain gauges may also be used, such as  
33 resistive foil gauges, or semiconductor strain gauges manufactured by using

1 photolithography masking and solid-state diffusion, instead of adhesive bonding. In the  
2 latter type of strain gauge, the electrical leads are attached directly to the strain-gauge  
3 pattern.

4 Figure 1 shows a three-dimensional view of a modified probe shaft (100) with a  
5 strain gauge (120) attached to it. There are two cut-outs on a probe shaft surface, one is  
6 of rectangular cross-section (160), and another one is of triangular or semi-circular  
7 (arched) cross-section (130), and they are located on the opposite sides of the probe  
8 shaft (100) directly opposite each other creating a very thin section (135) of the probe  
9 shaft. There is also a trench (140) in the probe shaft, which continues along the length  
10 of the probe shaft (100) from the border of the rectangular cut-out (160) to the external  
11 end of the probe shaft (100).

12 In the preferred embodiment, the strain gauge (120) is located at the median of  
13 the rectangular probe shaft cut-out (160), exactly on the very thin section of the probe  
14 shaft (100), created by the intersection of two cut-outs (130 and 160). The triangular or  
15 semi-circular cut-out (130), which serves as the "sensitivity cut-out", reduces the  
16 absolute stiffness of the probe shaft (100) and concentrates the strain at the strain gauge  
17 (120) location. The strain gauge (120) can be attached to a probe shaft surface with a  
18 high elastic modulus adhesive, such as epoxy. Electrical connection between the strain  
19 gauge (120) and the detection circuitry (170) can be made using wires (150) that follow  
20 the trench (140) running along the axis of the probe shaft (100). The wires (150) are  
21 connected to detection circuitry (170) for detecting, amplifying and conditioning the  
22 output of the strain gauge (120). For a resistance-based strain gauge, a conventional  
23 Wheatstone bridge can be used to detect subtle changes in the strain gauge resistance  
24 which can be fed back to the computer control system to indicate load on the probe tip  
25 (110). In the figures, a conventional Wheatstone bridge represents the detector circuitry  
26 (170), but the reader should understand this as an example. In practice, the detector  
27 circuitry (170) would include amplification and signal conditioning elements, as is  
28 known in the art.

29 The modified probe shaft (100) can be manufactured using several methods,  
30 such as machining, which is difficult with such a small object. Preferable alternatives  
31 are laser machining and electrical discharge machining methods.

32 The single strain-gauge system described above can detect strain in one  
33 dimension of deflection of the probe tip. In another embodiment, an additional strain

- 5 -

1 gauge (125) can be mounted at the same or different location along the probe shaft and  
2 perpendicular to the first strain(120) gauge. This additional strain gauge (125) requires  
3 a similar mechanical design of the probe shaft (100), including a local reduction in the  
4 probe shaft diameter (sensitivity cut-out).

5       In general, the apparatus just described may be used as follows: First, the target  
6 location for the touch-down of the probe (100) is defined by moving the nano-  
7 manipulator to a position above the target location. The output of the detector (170) is  
8 monitored while the nano-manipulator is moving towards the target location. When the  
9 output of the detector (170) is a touch-down signal, that is, strain signifying contact, the  
10 nano-manipulator is stopped.

11       I claim:

- 1 1. A strain detector for in-situ lift-out, comprising:  
2 a probe shaft;  
3 a strain gauge;  
4 a first cut-out on the probe shaft;  
5 a second cut-out on the probe shaft, the second cut-out opposite from the first  
6 cut-out; the first and second cut-outs defining a thinned region in the probe shaft;  
7 and,  
8 the strain gauge mounted on the probe shaft at the location of the thinned region.  
9
- 10 2. The strain detector of claim 1, where the strain gauge is a resistance-based strain  
11 gauge.  
12
- 13 3. The strain detector of claim 1, where the strain gauge is a silicon strain gauge.  
14
- 15 4. The strain detector of claim 1 where the strain gauge is a semiconductor strain  
16 gauge.  
17
- 18 5. The strain detector of claim 1, further comprising:  
19 the probe shaft having a trench; the trench connecting to the first cut-out.  
20
- 21 6. The strain detector of claim 1, further comprising:  
22 detecting circuitry for detecting, amplifying and conditioning the output of the  
23 strain gauge;  
24 wires electrically connecting the strain gauge to the detection circuitry.  
25
- 26 7. The strain detector of claim 6 where the detection circuitry comprises a  
27 Wheatstone bridge.  
28
- 29 8. The strain detector of claim 2 where the electrical resistance-based strain gauge  
30 is smaller in cross-sectional area than one square millimeter.  
31
- 32 9. The strain detector of claim 1,

1 where the surface of the first cut-out comprises an adhesive for mounting the strain  
2 gauge to the probe shaft.

3

4 10. The strain detector of claim 9, where the adhesive is epoxy.

5

6 11. The strain detector of claim 1, where the first cut-out has a rectangular cross-  
7 section.

8

9 12. The strain detector of claim 1, where the second cut-out has a triangular cross-  
10 section.

11

12 13. The strain detector of claim 1, where the second cut-out has a semi-circular  
13 cross-section.

14

15 14. A strain detector for in-situ lift-out, comprising:

16 a probe shaft;

17 a first cut-out on the probe shaft;

18 a second cut-out on the probe shaft, the second cut-out opposite from the first  
19 cut-out; the first and second cut-outs defining a first thinned region in the probe  
20 shaft;

21 a first strain gauge mounted on the probe shaft at the location of the first thinned  
22 region;

23 a third cut-out on the probe shaft;

24 a fourth cut-out on the probe shaft, the fourth cut-out opposite from the third cut-  
25 out; the third and fourth cut-outs defining a second thinned region in the probe  
26 shaft;

27 a second strain gauge mounted on the probe shaft at the location of the second  
28 thinned region;

29 where the second strain gauge is located substantially perpendicular to the first  
30 strain gauge.

31

32 15. The strain detector of claim 14, where the first and second strain gauges are  
33 resistance-based strain gauges.



1

2 16. The strain detector of claim 15, where the first and second strain gauges are  
3 silicon strain gauges.

4

5 17. The strain detector of claim 14, further comprising:  
6 the probe shaft having a trench; the trench connecting to the first and third cut-  
7 outs.

8

9 18. The strain detector of claim 16, further comprising:  
10 detecting circuitry for detecting, amplifying and conditioning the output of the  
11 strain gauge;  
12 wires electrically connecting the strain gauge to the detection circuitry; the wires  
13 located in the trench.

14

15 19. The strain detector of claim 18 where the detection circuitry comprises at least  
16 one Wheatstone bridge.

17

18 20. The strain detector of claim 15 where the resistance-based strain gauges are each  
19 smaller in cross-sectional area than one square millimeter.

20

21 21. The strain detector of claim 15,  
22 where the surface of the first cut-out and the third cut-out comprise an adhesive  
23 for mounting the first and second strain gauges respectively to the probe shaft.

24

25 22. The strain detector of claim 21, where the adhesive is epoxy.

26

27 23. The strain detector of claim 14, where the first and third cut-outs have a  
28 rectangular cross-section.

29

30 24. The strain detector of claim 14, where the second and fourth cut-outs have a  
31 triangular cross-section.

32

1 25. The strain detector of claim 14, where the second and fourth cut-outs have a  
2 semi-circular cross-section.

3

4 26. A strain detector for in-situ lift-out, comprising:

5 a probe shaft;

6 a strain gauge;

7 a first cut-out on the probe shaft; the first cut-out having a rectangular cross-  
8 section;

9 a second cut-out on the probe shaft; the second cut-out having a semicircular  
10 cross-section; the second cut-out opposite from the first cut-out; the first and  
11 second cut-outs defining a thinned region in the probe;

12 the strain gauge mounted on the probe shaft at the location of the thinned region;

13 a trench connecting to the first cut-out;

14 detecting circuitry for detecting, amplifying and conditioning the output of the  
15 strain gauge; and,

16 wires electrically connecting the strain gauge to the detection circuitry; the wires  
17 located in the trench.

18

19 27. A method of using an apparatus for detecting contact of a nano-manipulator  
20 probe; the probe comprising a probe shaft; at least one strain gauge; at least a first cut-  
21 out on the probe shaft; at least a second cut-out on the probe shaft, the second cut-out  
22 opposite from the first cut-out; the first and second cut-outs defining a thinned region in  
23 the probe shaft; the number of strain gauges corresponding to the number of thinned  
24 regions; the strain gauge mounted on the probe shaft at the location of the thinned  
25 region; and, the strain gauge connected to a detector; the detector capable of emitting a  
26 touch-down signal; the method comprising:

27 moving the nano-manipulator probe to a position above the target location;

28 monitoring the output of the detector while the nano-manipulator is moving  
29 towards the target location; and,

30 stopping movement of the nano-manipulator when the output of the detector  
31 shows a touch-down signal.

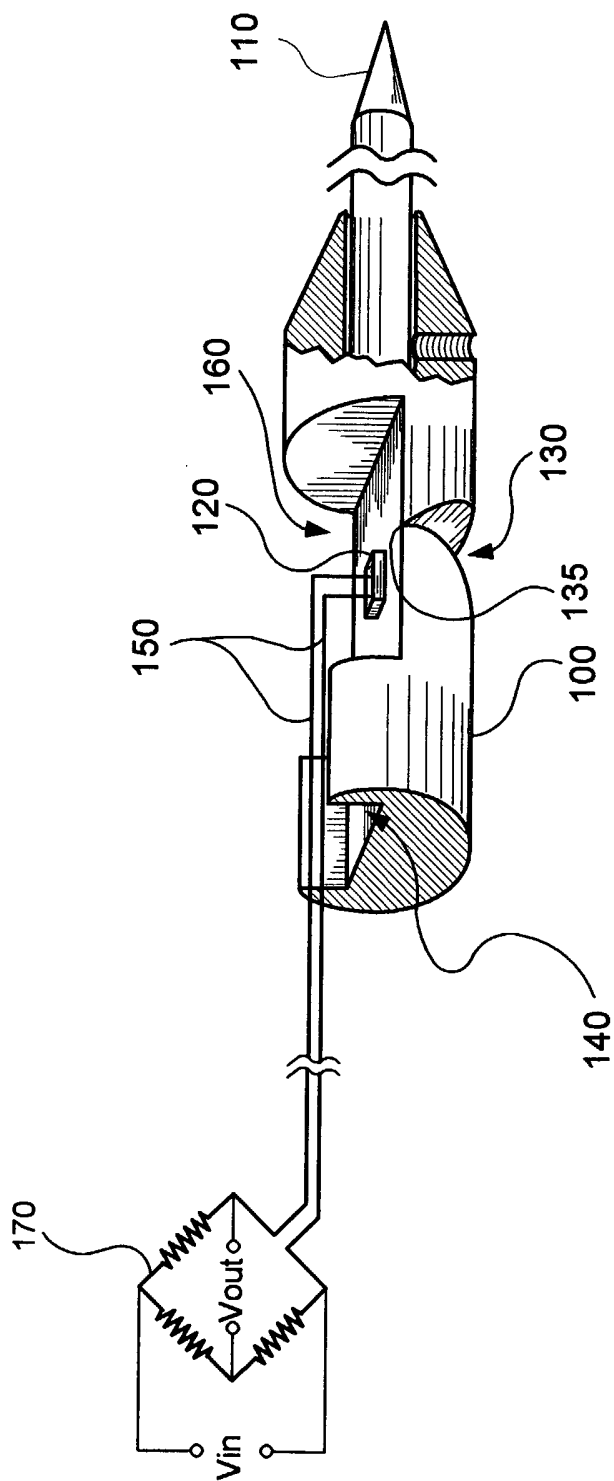


Fig. 1

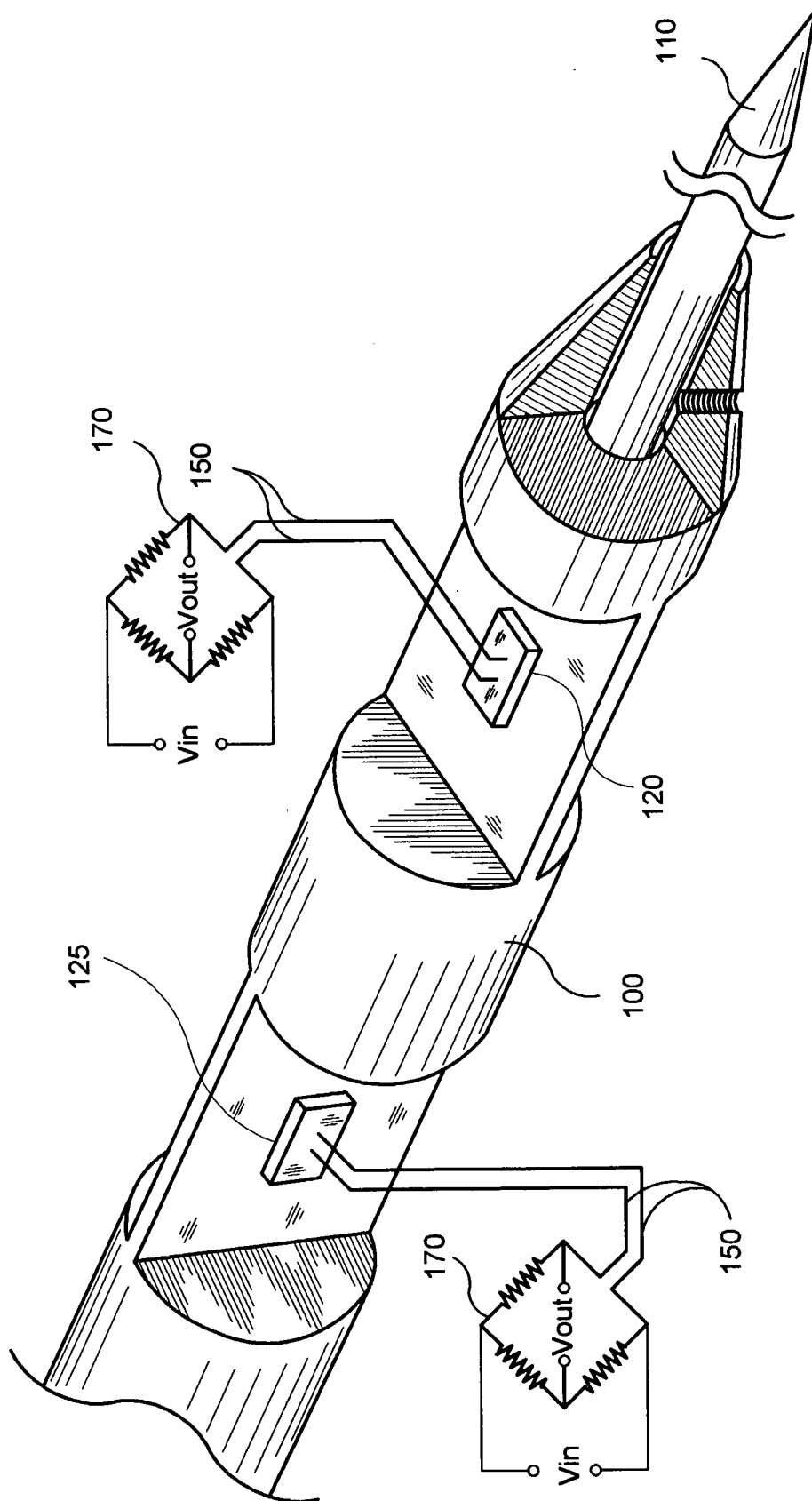


Fig. 2