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(54) **Title:** A CONTROL SYSTEM FOR A WIND TURBINE GENERATOR

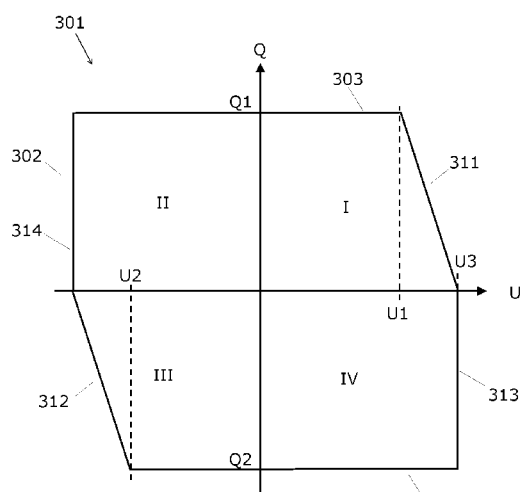


Fig. 3A

(57) **Abstract:** The invention relates to a control system for a wind turbine generator, WTG. The control system defines reactive limits for a reactive power reference for the WTG. The reactive limits are defined as a function of a physical parameter, e.g. the output voltage of the WTG. In case the reactive power reference exceeds the predefined limits, the reactive power reference is limited. By limiting the reactive power reference output voltages which exceed certain output voltage limits may be avoided and, thereby, a disconnection of the WTG from the grid may be avoided.



## A CONTROL SYSTEM FOR A WIND TURBINE GENERATOR

### FIELD OF THE INVENTION

The present invention relates to a control system for wind turbine generator, in particular to a control system configured to control generation of reactive power. Further, the invention relates to a wind turbine generator comprising the control system.

### BACKGROUND OF THE INVENTION

Due to different conditions the voltage at the output terminals of the wind turbine generator (WTG) may become unacceptable low or high. Such unacceptable output voltages may be harmful for components of the wind turbine generator.

In case that the output voltage becomes too high or low the wind turbine generator may be disconnected from the grid connection to avoid damaging components of the wind turbine generator.

US 8 710 689 discloses a wind energy installation including a rotor, a generator driven by the rotor, and a converter for generating electrical power which is output into a power supply system via a transformer. The installation also includes an open-loop control system having an open-loop converter control unit. The open-loop control system supplies an actuating signal for a reactive component to the converter. The installation further includes a voltage measurement device arranged on the transformer. The voltage signal of the voltage measurement device is applied to an input of a state-dependent setpoint value shifter, whose output signal is applied to a limitation module for the reactive component acting on the converter. With this configuration, the installation can be better protected and the transformer can be better utilized.

### SUMMARY OF THE INVENTION

It is an object of the present invention to improve the control of a wind turbine generator.

It is a further object to provide an improved control system for a wind turbine generator, in particular an improved control system configured to control generation of reactive power.

- 5 In particular, it may be seen as an object of the present invention to provide a control system that solves the above mentioned problems caused by unacceptable output voltages at the output terminals of the wind turbine generator, and/or to provide a control system that avoids disconnecting of wind turbine generators from the grid.

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In a first aspect of the invention there is provided a control system for a wind turbine generator, the wind turbine generator comprising a reactive power controller, the control system comprising

- a QV limit module configured to define predetermined reactive limits dependent on an output voltage of the wind turbine generator, wherein the QV limit module is configured to receive a reactive reference from an external source, and wherein the QV limit module is configured to output the reactive reference as an output reactive reference  $Q_{refQV}$  and, in case the reactive reference ( $Q_{ref}$ ) exceeds one of the predetermined reactive limits (302), the QV limit module is configured to determine the output reactive reference  $Q_{refQV}$  by limiting the reactive reference  $Q_{ref}$  to the exceeded predetermined reactive limit, and wherein the reactive power controller is configured to control generation of reactive power from a power generator system of the wind turbine generator dependent on the output reactive reference  $Q_{refQV}$  or other reactive reference being dependent on the output reactive reference  $Q_{refQV}$ , and
- an update module configured to supply the predetermined reactive limit for an actual output voltage back to the external source.

Advantageously, the possible limitation of the reactive reference dependent on the output voltage of the wind turbine generator may provide better control of the output voltage so that disconnection of the wind turbine generator from the grid may be avoided. The feedback of the reactive limit to the provider of the reactive reference, i.e. the external source, may enable adaption of the reactive reference  $Q_{ref}$  based on the predetermined reactive limits for the actual output voltage.

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In an embodiment the QV limit module is configured so that the predetermined reactive limits define capacitive limits setting limits for the reactive references being capacitive references and inductive limits setting limits for the reactive references being inductive references within a predefined range of the output  
5 voltage.

In an embodiment the QV limit module is configured so that the capacitive limits decreases, i.e. decreases with decreasing capacitive limit values, for increasing output voltages above a first threshold voltage.  
10

In an embodiment the QV limit module is configured so that the inductive limits decreases, i.e. decreases with decreasing inductive limit values, for decreasing output voltages below a second threshold voltage.

15 In an embodiment the QV limit module is configured so that the capacitive limits comprise extended capacitive limits defining inductive values which increase for increasing output voltages above a third threshold voltage being greater than the first threshold voltage, and wherein the QV limit module is configured to set the capacitive reference  $Q_{refcap}$  to an inductive value according to the extended  
20 capacitive limits in case the output voltage exceeds the third threshold voltage.

In an embodiment the QV limit module is configured so that the inductive limits comprise extended inductive limits defining capacitive values which increase for increasing output voltages below a fourth threshold voltage being smaller than the  
25 second threshold voltage, and wherein the QV limit module is configured to set the inductive reference to a capacitive value according to the extended inductive limits in case the output voltage is smaller than the third threshold voltage.

In an embodiment the QV limit module is configured so that the inductive limits  
30 increase above a nominal limit  $Q_2$  for increasing output voltages above a fifth threshold voltage being greater than the third threshold voltage, and wherein the QV limit module is configured to set the inductive reference, and optionally also the capacitive reference, to one of the inductive limits above the nominal limit  $Q_2$  in case the output voltage exceeds the fifth threshold voltage.

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In an embodiment the QV limit module is configured so that the capacitive limits increase above a nominal limit  $Q_1$  for decreasing output voltages below a sixth threshold voltage being smaller than the fourth threshold voltage, and wherein the QV limit module is configured to set the capacitive reference, and optionally  
5 also the inductive reference, to one of the the capacitive limits above the nominal limit  $Q_1$  in case the output voltage is smaller than the sixth threshold voltage.

In an embodiment the control system further comprises a QP limit module configured to define predetermined reactive limits dependent on an active  
10 reference (active power or current reference), wherein the QP limit module is configured to limit the output reactive reference in case the output reactive reference exceeds the predetermined reactive limits of the QP limit module.

Advantageously, the series connection of the QV and QP limit modules may  
15 ensure that the reactive references is limited according to the most restrictive reactive limit dependent on the actual output voltage and the actual active power reference.

In an embodiment the update module is configured to compare the predetermined  
20 reactive limit for an actual output voltage of the QV limit module with the predetermined reactive limit of the QP limit module so as to determine the most restrictive reactive limit, and configured to supply the determined most restrictive reactive limit back to the external source.

25 Advantageously, the feedback of the most restrictive reactive limit to the provider of the reactive reference, i.e. the external source, may enable adaption of the reactive reference  $Q_{ref}$  based on the most restrictive predetermined reactive limit for the actual output voltage and actual active power reference.

30 In an embodiment the control system comprise one or more other limit modules connected in series with the QV limit module, wherein the other limit modules define predetermined reactive limits dependent on other physical parameters. The other limit modules may be configured to limit the output reactive reference  $Q_{refQV}$  from the QV limit module in case the output reactive reference exceeds  
35 the predetermined reactive limits of the other limit modules.

Advantageously, the series connection of the QV and other limit modules may ensure that the reactive references is limited according to the most restrictive reactive limit dependent on the actual output voltage and other physical  
5 parameters, e.g. temperature.

In an embodiment the update module is configured to compare the predetermined reactive limit for an actual output voltage of the QV limit module with the predetermined reactive limit(s) of the one or more other limit modules so as to  
10 determine the most restrictive reactive limit, and configured to supply the determined most restrictive reactive limit back to the external source.

Advantageously, the feedback of the most restrictive reactive limit to the provider of the reactive reference, i.e. the external source, may enable adaption of the  
15 reactive reference  $Q_{ref}$  based on the most restrictive predetermined reactive limit for the actual output voltage and other actual physical parameters, e.g. temperature.

A second aspect of the invention relates to a wind turbine generator comprising  
20 the control system according to the first aspect.

A third aspect of the invention relates to a method for controlling a wind turbine generator, comprising the steps of  
- receiving a reactive reference  $Q_{ref}$  from an external source,  
25 - outputting the reactive reference  $Q_{ref}$  as an output reactive reference  $Q_{refQV}$ , wherein, in case the reactive reference  $Q_{ref}$  exceeds one of a plurality of predetermined reactive limits (302), the output reactive reference  $Q_{refQV}$  is determined by limiting the reactive reference  $Q_{ref}$  to the exceeded predetermined reactive limit, and wherein the predetermined reactive limits are dependent on an  
30 output voltage  $U_{WTG}$  of the wind turbine generator,  
- controlling generation of reactive power from a power generator system of the wind turbine generator dependent on the output reactive reference  $Q_{refQV}$  or other reactive reference  $Q_{refQP}$  being dependent on the output reactive reference  $Q_{refQV}$ ,

- supplying the predetermined reactive limit for an actual output voltage back to the external source.

A fourth aspect of the invention relates to at least one computer program product  
5 directly loadable into the internal memory of at least one digital computer,  
comprising software code portions for performing the steps of the method  
according to the third aspect when said at least one product is/are run on said at  
least one computer.

10 In general the various aspects of the invention may be combined and coupled in  
any way possible within the scope of the invention. These and other aspects,  
features and/or advantages of the invention will be apparent from and elucidated  
with reference to the embodiments described hereinafter.

#### 15 BRIEF DESCRIPTION OF THE DRAWINGS

Embodiments of the invention will be described, by way of example only, with  
reference to the drawings, in which

Fig. 1 illustrates a power generator system of a wind turbine generator,  
20 Fig. 2 illustrates a control system for a wind turbine generator,  
Figs. 3A-B show examples of QV limit modules 301,  
Fig. 4 illustrates an embodiment of the control system configured with one or  
more other limit modules,  
Fig. 5 illustrates an alternative control system for a wind turbine generator, and  
25 Fig. 6 illustrates a method of an embodiment of the invention.

#### DETAILED DESCRIPTION OF EMBODIMENTS

Fig. 1 illustrates a power generator system 101 of a wind turbine generator 100  
connected to the grid 103. The power generator system 101 may comprise a  
30 generator driven by the rotor of the wind turbine generator and a power converter  
configured to adjust the voltage amplitude and frequency of the generator AC  
voltage into a converter output AC voltage. The power generator system 101 is  
capable of adjusting the phase between the converter output AC voltage and the  
converter output AC current and, thereby, the amount of reactive and active  
35 power supplied to the grid 103.

The power generator system 101 may be connected to the grid 103 via a transformer. The reactance of the transformer, as well as the reactance of other components is included in the reactance 102. The reactive current supplied by the power generator system 101 generates a voltage drop  $\Delta U$  across the reactance 102.

A resistance of the transformer and other components between the generator system 101 and the grid 103 is also present but not included in Fig. 1, i.e. is not included in the component 102 which is considered a pure reactive component. Normally, the resistive voltage drop due to the active current is smaller than the reactive voltage drop so that it can be neglected.

The voltage  $U_{PCC}$  at the point of common connection PCC can be considered to deviate only a few percentages from a nominal voltage.

The voltage at the output of the wind turbine generator, e.g. the voltage at the output of the power generator system 101 can therefore be described and simplified to  $U_{WTG} = \Delta U + U_{PCC}$ . Since  $U_{PCC}$  is substantially constant (is typically only allowed to vary a few percent from a nominal value  $\pm 10\%$ ), the voltage  $U_{WTG}$  depends mainly on the voltage drop  $\Delta U$  and, thereby, on the amplitude of the reactive current supplied by the output of the wind turbine generator.

In case the reactive current or power supplied by the wind turbine generator is inductive the sign of  $\Delta U$  will be negative, i.e.  $U_{WTG}$  will be lower than  $U_{PCC}$ .

In case the reactive current or power supplied by the wind turbine generator is capacitive the sign of  $\Delta U$  will be positive, i.e.  $U_{WTG}$  will be higher than  $U_{PCC}$ .

30

In order to protect electrical components of a wind turbine generator against over or under voltages, i.e. against situations wherein  $U_{WTG}$  becomes too high or too low, the wind turbine generator may be configured to shut down or disconnect from the grid connection when the output voltage  $U_{WTG}$  becomes too high or too low.

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An under voltage may cause an increased generation of current from the WTG in order to maintain a required power output. The increased current may cause thermal problems. An over voltage may cause excessive loads of electrical components since internal voltages may exceed nominal design limits.

As described above, an over voltage can be induced by the WTG by injecting too much capacitive power or because the electrical grid causes a too high capacitive current flow through the reactance 102 or simply due to a transient in the system due to load operation or generator malfunction. Similarly, an under voltage can be induced by the WTG by injecting too much inductive power or because the electrical grid causes a too high inductive current flow through the reactance 102 or simply due to a transient in the system due to load operation or generator malfunction.

15

Fig. 2 shows a control system 200 for a wind turbine generator. The control system 200 comprises a QV limit module 201 defining predetermined reactive limits dependent on an output voltage  $U_{WTG}$  measured at an output of the wind turbine generator, e.g. at the output of the power generator system 101.

20

The QV limit module 201 is configured to receive a reactive reference  $Q_{ref}$  from a power plant controller 220. In case the reactive reference  $Q_{ref}$  does not exceed the predetermined reactive limits, the reactive reference  $Q_{ref}$  is outputted unmodified as an output reactive reference  $Q_{refQV}$ , e.g. by setting  $Q_{refQV}$  equal to  $Q_{ref}$ . In case the reactive reference  $Q_{ref}$  does exceed the predetermined reactive limits, the output reactive reference  $Q_{refQV}$  is determined by limiting the reactive reference  $Q_{ref}$  to the exceeded predetermined reactive limit.

The predetermined reactive limits may be configured to define both capacitive limits and inductive limits within a predefined range of the output voltage  $U_{WTG}$ . Thus, predetermined capacitive and inductive limits may be defined for over- and/or under voltages of the output voltage  $U_{WTG}$ .

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Thus, predetermined reactive limits define capacitive limits setting limits for capacitive reactive references  $Q_{ref}$  and inductive limits setting limits for inductive reactive references  $Q_{ref}$  within the predefined range of the output voltage.

5 The predetermined reactive limits may be defined by a plurality of numerical values defined as a function the output voltage  $U_{WTG}$  and the reactive reference  $Q_{ref}$ , e.g. dependent on the sign of the reactive reference  $Q_{ref}$  indicating whether the reactive reference is capacitive or inductive. The predetermined reactive limits may be predetermined in the sense that the plurality of numerical values of the  
10 predetermined reactive limits are stored, e.g. as a look up table in a memory of a computer. A single predetermined reactive limit may refer to a single numerical value, e.g. a value associated with a given output voltage  $U_{WTG}$  (e.g. an actual output voltage) and a given reactive reference  $Q_{ref}$ .

The reactive limits may be reactive power limits, reactive current limits or other  
15 limits corresponding to reactive power or current limits. It is understood that a reactive quantity may be an inductive or capacitive quantity. Accordingly, the QV limit module 201 and other reactive limit modules 202, 401 defines predetermined reactive limits dependent on the output voltage  $U_{WTG}$  or dependent on other physical parameters where the reactive limits may be limits in terms of reactive  
20 power, reactive current or other parameter derivable from reactive power or reactive current. Thus, a QV limit module may be referred to as a reactive limit module.

The output reactive reference  $Q_{refQV}$ , which may be limited or unaffected by the  
25 QV limit module, may be supplied directly to a reactive power controller 203 configured to control generation of reactive power or reactive current from the power generator system 101 of the wind turbine generator dependent on the output reactive reference  $Q_{refQV}$  or dependent on other reactive reference which depends on the output reactive reference  $Q_{refQV}$ .

30

Thus, the output reactive reference  $Q_{refQV}$  could be supplied directly to the serially connected reactive power controller 203 or it could be supplied to another limit module such as a QP limit module 202 which defines predetermined reactive limits dependent on active power or active current, e.g. dependent on an active  
35 reference (power or current reference) or a measured active power or current

generated by the power generator system 101 and wherein the QP limit module is configured to limit the output reactive reference  $Q_{refQV}$  in case the output reactive reference exceeds one of the predetermined reactive limits of the QP limit module. Accordingly, the QP limit module 202 generates an output reactive  
5 reference  $Q_{refQP}$  which depends on the output reactive reference  $Q_{refQV}$ , i.e. which is unmodified or limited depending on the value of  $Q_{refQV}$ . The active reference input or active power or current measurement input is not shown in Fig. 2.

10 In general the reactive power controller 203 may be configured to control generation of reactive power or reactive current dependent, at least partially, on an input reactive reference  $Q_{refin}$ . The control system may be configured so that the input reactive reference  $Q_{refin}$  is based on the output reactive reference  $Q_{refQV}$ , e.g.  $Q_{refin}$  may be set equal to  $Q_{refQV}$ , or  $Q_{refin}$  may be based on other  
15 reactive reference, e.g.  $Q_{refQP}$ , which depends on the output reactive reference  $Q_{refQV}$ , or a reactive reference  $Q_{refXX}$  from other limit modules 401.

The power plant controller 220 may be a central controller configured to control power generation from a plurality of wind turbine generators dependent on  
20 measured electrical quantities at the point of common coupling PCC, e.g. measured voltage  $U_{PCC}$ , measured reactive power  $Q_{PCC}$  or measured active power  $P_{PCC}$  and corresponding references (e.g.  $U_{refPCC}$ ,  $Q_{refPCC}$  and  $P_{refPCC}$ ) supplied e.g. by a grid operator system. Accordingly, the power plant controller may generate a reactive reference  $Q_{ref}$  to the wind turbine generator in order to  
25 control one of the measured electrical quantities at the PCC.

Generally, the QV limit module may be configured so that in case of an over voltage, a reactive reference  $Q_{ref}$  which is capacitive, i.e. a capacitive reference  $Q_{capref}$  from the power plant controller, is limited in order to avoid further  
30 voltage increases in the output voltage.

Similarly, the QV limit module may be configured so that in case of an under voltage, a reactive reference  $Q_{ref}$  which is inductive, i.e. an inductive reference  $Q_{indref}$  from the power plant controller, is limited in order to avoid further voltage  
35 decreases in the under voltage.

The control system 200 may further comprise an update module 210 for supplying one of the predetermined reactive limits  $Q_{\text{limit}}$  for an actual output voltage outputted by one or more of the limit modules 201, 202, 401 back to the power plant controller. Accordingly, the predefined capacitive limit  $Q_{\text{limit}}$  and/or the inductive limit  $Q_{\text{limit}}$  for an actual output voltage  $U_{\text{WTG}}$  may be forwarded to the power plant controller 220 which may be configured to determine future reactive references  $Q_{\text{ref}}$  dependent on the limits forwarded by the update module 210. Accordingly, the limit modules 201, 202, 401, e.g. the QV limit module 201, may be configured to determine one of the predetermined reactive limits  $Q_{\text{limit}}$  for an actual output voltage, e.g. by using a recently measured output voltage  $U_{\text{WTG}}$  as the actual output voltage and determining the predetermined reactive limit  $Q_{\text{limit}}$  associated with that voltage. The predetermined reactive limit  $Q_{\text{limit}}$  may include either the capacitive or inductive limit, or both the capacity and inductive limits associated with a given output voltage.

The update module 210 may be configured to determine the most restrictive reactive limit  $Q_{\text{restrict}}$  from a plurality of limit modules including the QV module 201 and one or more other limit modules such as the QP limit module 202. Accordingly, the update module 210 may be configured to determine the smallest (here the absolute values are considered) capacitive and inductive limits among the reactive limits supplied by the limit modules 201, 202 and to forward the determined smallest reactive limits to the power plant controller 220 or external source 520. For example, the update module 210 may be configured to compare the predetermined reactive limit for an actual output voltage of the QV limit module 201 with the predetermined reactive limit(s), e.g.  $Q_{\text{limit\_QP}}$ , of one or more other limit modules, including the QP limit module 202, so as to determine the most restrictive reactive limit, and configured to supply the determined reactive limit to the power plant controller 220. The most restrictive reactive limit may include either the capacitive or inductive limit, or both the capacity and inductive limits associated with a given output voltage.

Figs. 3A-B show examples of QV limit modules 301. The horizontal axis defines voltage values  $U$  and the vertical axis defines reactive values  $Q$ . The origin of the coordinate system defines a voltage value of one pu corresponding the nominal

output voltage, and a reactive value of zero. Accordingly, values of the horizontal axis are positive, values of the vertical axis in the first and second quadrants (I, II) are positive, values of the vertical axis in the third and fourth quadrants (III,IV) are negative. Reactive values in the first and second quadrants are  
5 defined as capacitive values. Reactive values in the third and fourth quadrants are defined as inductive values. Voltages in the first and fourth quadrants are defined as over voltages since they are larger than the nominal voltage (1 pu). Voltages in the second and third quadrants are defined as under voltages since they are smaller than the nominal voltage (1 pu).

10

In order to avoid limitation to a specific coordinate system definition, reactive values of the coordinate system of the QV limit module, e.g. capacitive and reactive limits are considered as absolute values. I.e. inductive values in the third and fourth quadrants, which according to the coordinate system are negative,  
15 may be referred to as positive values.

The reactive values in the coordinate system may be reactive power values, reactive current values or other reactive values related to reactive power.

20 The predetermined reactive limits 302 comprise capacitive limits 303 in the first and second quadrants setting limits for reactive references  $Q_{ref}$  being capacitive references  $Q_{refcap}$  and inductive limits 304 in the third and fourth quadrants setting limits for reactive references  $Q_{ref}$  being inductive references  $Q_{refind}$  within a predefined range of the output voltage  $U_{WTG}$  along the horizontal axis.

25

The reactive references  $Q_{ref}$ ,  $Q_{refcap}$ ,  $Q_{refind}$  as well as any other reactive reference described herein may be a reference for reactive current or power. Accordingly, the predetermined reactive limits 302 may define reactive (inductive or capacitive) power or current limits for reactive (inductive or capacitive) power  
30 or current references  $Q_{ref}$ .

The reactive limits 302 define capacitive and inductive limits 303, 304 corresponding to nominal capacitive and inductive limits  $Q_1$ ,  $Q_2$  between a first upper threshold voltage  $U_1$  and a second lower threshold voltage  $U_2$ . The nominal  
35 capacitive and inductive limits define the standard maximum reactive limits of the

wind turbine generator, e.g. the standard maximum reactive powers that can be produced by the wind turbine generator.

The QV limit modules in Figs. 3A-B comprises decreasing capacitive limits 311  
5 which decrease for increasing output voltages  $U_{WTG}$  above the first threshold voltage  $U_1$ . The decreasing capacitive limits 311 define decreasing capacitive values, e.g. power values. The first threshold voltage is larger than the nominal voltage  $U_{WTG}$ . For example, the first threshold voltage may be equal to 1.1 times the nominal voltage. The capacitive limits may decrease linearly from the  
10 nominal capacitive limit value down to zero as shown in Figs. 3A-B. Accordingly, a capacitive reference  $Q_{ref}$  ( $Q_{refcap}$ ) may be limited by the decreasing capacitive limits 311 in order to avoid that the over voltage increases further.

Similarly, the QV limit modules in Figs. 3A-B comprises decreasing inductive limits  
15 312 which decrease (i.e. the absolute value decreases) for decreasing output voltages  $U_{WTG}$  below the second threshold voltage  $U_2$ . The decreasing inductive limits 312 define decreasing inductive values, e.g. power values. The second threshold voltage is smaller than the nominal voltage  $U_{WTG}$ . For example, the second threshold voltage may be equal to 0.9 times the nominal voltage. The  
20 inductive limits may decrease linearly from the nominal capacitive limit value down to zero as shown in Figs. 3A-B. Accordingly, an inductive reference  $Q_{ref}$  ( $Q_{refind}$ ) may be limited by the decreasing inductive limits 312 in order to avoid that the under voltage decreases further.

25 In case of an over voltage an inductive reference  $Q_{refind}$  may be limited only by the nominal inductive limits 304, e.g. up to an upper third threshold voltage  $U_3$ . According to the example in Fig. 3A, for voltages above the third threshold voltage  $U_3$ , the inductive reference  $Q_{ref}$  is limited to zero according to inductive limits  
313.

30

The QV limit module in Fig. 3B differs from the QV limit module in Fig. 3A in that it comprises extended capacitive limits 321 defining inductive values which increase for increasing output voltages  $U_{WTG}$  above the third threshold voltage  $U_3$ . The third threshold voltage is greater than the first threshold voltage  $U_1$  and may as  
35 an example be equal to 1.13, possibly 1.2 times, the nominal voltage. The

capacitive limits 321 may increase linearly from zero up to the nominal inductive limit value  $Q_2$ . Accordingly, for voltages above  $U_3$ , a capacitive reference  $Q_{refcap}$  may be limited by the extended capacitive limits 321 so that a capacitive reference is turned into an inductive reference. Accordingly, the limit module 201  
5 may be configured to set the capacitive reference  $Q_{refcap}$  to an inductive value according to the extended capacitive limits 321 in case the output voltage exceeds the third threshold voltage.

Since the effect of an inductive reference  $Q_{ref}$  is that the output voltage  $U_{WTG}$  is  
10 decreased, the extended capacitive limits 321 may help bringing the overvoltage below  $U_3$ . For example, a capacitive reference at point 331 may be turned into an inductive reference at point 332. An inductive reference  $Q_{ref}$  at an output voltage above  $U_3$  is still limited to the upper nominal inductive reference  $Q_2$ .

15 Similarly, the QV limit module in Fig. 3B differs from the QV limit module in Fig. 3A in that it comprises extended inductive limits 322 defining capacitive values which increase for increasing output voltages  $U_{WTG}$  below the fourth threshold voltage  $U_4$ . The fourth threshold voltage is smaller than the second threshold voltage  $U_2$  and may as an example be equal to 0.87, possibly equal to 0.8, times  
20 the nominal voltage. The inductive limits may increase linearly from zero up to the nominal capacitive limit value  $Q_1$ . Accordingly, for voltages below  $U_4$ , an inductive reference  $Q_{refind}$  may be limited by the extended inductive limits 322 so that an inductive reference is turned into a capacitive reference. Accordingly, the limit module 201 may be configured to set the inductive reference  $Q_{refind}$  to a  
25 capacitive value according to the extended inductive limits 322 in case the output voltage exceeds the third threshold voltage.

Since the effect of a capacitive reference  $Q_{ref}$  is that the output voltage  $U_{WTG}$  is increased, the increasing inductive limits 322 may help bringing the under voltage  
30 above  $U_4$ . For example, an inductive reference at point 333 may be turned into a capacitive reference at point 334. A capacitive reference  $Q_{ref}$  at an output voltage below  $U_4$  is still limited to the upper nominal capacitive reference  $Q_1$ .

The QV limit module in Fig. 3B further may further comprise inductive limits 341  
35 (increasing or non-increasing) which increase or remain equal to the nominal

value  $Q_2$  for increasing output voltages  $U_{WTG}$  above the fifth threshold voltage  $U_5$ . For example, the fifth threshold voltage may be equal to 1.2, possibly equal to 1.3, times the nominal voltage. The inductive limits may increase linearly from the nominal inductive limit  $Q_2$  possibly up to a given maximum value (not shown). Accordingly, for voltages above  $U_5$ , an inductive reference  $Q_{refind}$  (optionally also a capacitive reference  $Q_{refcap}$ ) may be limited by the inductive limits 341 defined above the nominal value  $Q_2$ . Optionally, in case the reactive reference  $Q_{ref}$  is capacitive, the capacitive reference is turned into an inductive reference according to the limit function 341. Since the effect of an inductive reference  $Q_{ref}$  is that the output voltage  $U_{WTG}$  is decreased, the inductive limits 341 may cause injection of even higher inductive power for bringing the over voltage below  $U_5$ . In case the limits 341 constitutes a linear function, the slope of the inductive limit 341 may be selected within the range from zero and upwards, e.g. up to a slope of one as shown in Fig. 3B. For a zero slope, the inductive limits 341 are equal to the nominal inductive limit  $Q_2$  for increasing output voltages  $U_{WTG}$ .

Accordingly, QV limit module 201 may be is configured so that the inductive limits 304 increase above a nominal limit value  $Q_2$  (or is extended with a limit equal to  $Q_2$ ) for increasing output voltages above the fifth threshold voltage.

The QV limit module in Fig. 3B may further comprise capacitive limits 342 (increasing or non-increasing) which increase or remain equal to the nominal value  $Q_1$  for decreasing output voltages  $U_{WTG}$  below the sixth threshold voltage  $U_6$ . For example, the third threshold voltage may be equal to 0.83, possibly equal to 0.7, times the nominal voltage. The inductive limits may increase linearly from the nominal inductive limit  $Q_1$  possibly up to a given maximum value (not shown). Accordingly, for voltages below  $U_6$ , a capacitive reference  $Q_{ref}$  (optionally also an inductive reference  $Q_{ref}$ ) may be limited by the capacitive limits 342 defined above the nominal value  $Q_1$ . In the optional case where the reactive reference  $Q_{ref}$  is inductive, the inductive reference is turned into a capacitive reference according to the limit function 342. Since the effect of a capacitive reference  $Q_{ref}$  is that the output voltage  $U_{WTG}$  is increased, the capacitive limits 342 may cause injection of even higher capacitive power for bringing the under

voltage above  $U_6$ . Similar to limit 341, the slope of the limits 342, i.e. the linear function defined by the limits, may be zero or greater than zero.

Accordingly, QV limit module 201 may be is configured so that the capacitive  
5 limits 303 increase above a nominal limit value  $Q_1$  (or is extended with a limit equal to  $Q_1$ ) for decreasing output voltages below the sixth threshold voltage.

The QV reactive limits shown in Figs. 3A-B are examples and it is understood that the predetermined reactive limits 302 may be configured in different ways.

10

Fig. 4 shows an embodiment of the control system 200 configured with one or more other limit modules 401, optionally the QP limit module 202, connected in series with the QV limit module. The order of the limit modules may be different than shown in Fig. 4. The other limit modules 401 define predetermined reactive  
15 limits dependent on other physical parameters such as the temperature of a WTG component (e.g. generator) and distortion in output voltage  $U_{WTG}$ . The other limit modules 401 are configured to limit the output reactive reference  $Q_{refQV}$  in case the output reactive reference exceeds the predetermined reactive limit.

Accordingly, a limit module may receive  $Q_{refQV}$  from the QV limit model 201 or  
20 an output reactive reference from another limit model can generate an output reactive reference  $Q_{refXX}$  dependent on the predefined reactive limits and the received input. The predetermined reactive limits of e.g. a QT limit module 401 which define reactive limits dependent on temperature of a WTG component may have the same capacitive and inductive limit curves as the limit curves 303, 304  
25 in Fig. 3, but with voltage  $U$  replaced with temperature. As noted previously, the update module 210 may be configured to determine the most restrictive reactive limits from one or more of a plurality of limit modules including the QV module 201, one or more other limit module 401 and the QP limit module 202.

30 In the example in Fig. 2, the QV limit module receives the reactive reference  $Q_{ref}$  from the power plant controller 220 and the update module 210 supplies the reactive limits to the power plant controller 220.

Fig. 5 shows a general configuration of the control system 500 being functionally  
35 equivalent with the control system 200, but where the QV limit module receives

the reactive reference  $Q_{ref}$  from an external source 520 and the update module 210 supplies the most restrictive reactive limits to the external source 520 as a feedback signal.

- 5 Accordingly, the external source 520 may be a power plant controller 220, a grid operator or other source which is able to generate a reactive reference  $Q_{ref}$ , and possibly modify the reactive reference dependent on a feedback from the update module 210. The external source 520 is a source which normally is external to the wind turbine generator 100, i.e. which is located outside the wind turbine
- 10 generator (e.g. outside the nacelle) and which supplies the reactive reference  $Q_{ref}$  to the wind turbine generator via a wired or wireless connection between the external source and the wind turbine generator.

The QV limit module 201 as well as one or more of the other limit modules 401

15 and the update module 210 may be comprised by the wind turbine generator 100. More generally, any one or more of the QV limit module 201, the other limit modules 401 and the update module 210 may be located externally from the wind turbine generator, e.g. they may be comprised by the external source 520, while the remaining limit modules 201, 401 may be comprised by the wind turbine

20 generator.

Accordingly, control system 200 may be part of a wind turbine generator, an external source 520, a power plant controller 220 or the control system 200 may be distributed over different units.

25

Fig. 5 shows an example, where the control system 200 is distributed over the wind turbine generator and the external source 520 so that the QV limit module is comprised by the external source 520 and so that the QP limit module 202 and the update module 210 is comprised by the wind turbine generator. Accordingly,

30 the output voltage  $U_{WTG}$  from the WTG is supplied to the externally located QV limit module 201. The reactive reference  $Q_{ref}$ , which may be provided by the external source 520 or other external source, is also supplied as an input to the QV limit module 201. The reactive limits for an actual output voltage  $Q_{limits}$  from the QV and QP limit modules 201, 202 are supplied to the update module 210

which determines the most restrictive reactive limits  $Q_{restrict}$  and supplies these limits to the external source 520.

Fig. 6 illustrates a method of an embodiment of the invention comprising the 5 steps:

- 601: receiving a reactive reference  $Q_{ref}$  from an external source 520, 220,
- 602: outputting the reactive reference  $Q_{ref}$  as an output reactive reference  $Q_{refQV}$ , wherein the output reactive reference  $Q_{refQV}$  is determined by limiting the reactive reference  $Q_{ref}$  to a predetermined reactive limit 302 in case the 10 reactive reference  $Q_{ref}$  exceeds the predetermined reactive limit 302, and wherein the predetermined reactive limit 302 is dependent on an output voltage  $U_{WTG}$  of the wind turbine generator,
- 603: controlling generation of reactive power from a power generator system 101 of the wind turbine generator dependent on the output reactive reference 15  $Q_{refQV}$  or other reactive reference, e.g.  $Q_{refQP}$ , being dependent on the output reactive reference  $Q_{refQV}$ ,
- 604: supplying the reactive limits for an actual output voltage back to the external source.

20 In summary the invention relates to a control system for a wind turbine generator (WTG). The control system defines reactive limits for a reactive power reference for the WTG. The reactive limits are defined as a function of a physical parameter, e.g. the output voltage of the WTG. In case the reactive power reference exceeds the predefined limits, the reactive power reference is limited. By limiting the 25 reactive power reference output voltages which exceed certain output voltage limits may be avoided and, thereby, a disconnection of the WTG from the grid may be avoided.

Embodiments of invention can be implemented by means of electronic hardware, 30 software, firmware or any combination of these. Software implemented embodiments or features thereof may be arranged to run on one or more data processors and/or digital signal processors. Software is understood as a computer program which may be stored/distributed on a suitable computer-readable medium, such as an optical storage medium or a solid-state medium supplied 35 together with or as part of other hardware, but may also be distributed in other

forms, such as via the Internet or other wired or wireless telecommunication systems. Accordingly, the computer-readable medium may be a non-transitory medium.

- 5 The individual elements of an embodiment of the invention may be physically, functionally and logically implemented in any suitable way such as in a single unit, in a plurality of units or as part of separate functional units. The invention may be implemented in a single unit, or be both physically and functionally distributed between different units and processors. A unit may constitute a control system or  
10 subunits thereof.

Although the present invention has been described in connection with the specified embodiments, it should not be construed as being in any way limited to the presented examples. The scope of the present invention is to be interpreted in  
15 the light of the accompanying claim set. In the context of the claims, the terms "comprising" or "comprises" do not exclude other possible elements or steps. Also, the mentioning of references such as "a" or "an" etc. should not be construed as excluding a plurality. The use of reference signs in the claims with respect to elements indicated in the figures shall also not be construed as limiting the scope  
20 of the invention. Furthermore, individual features mentioned in different claims, may possibly be advantageously combined, and the mentioning of these features in different claims does not exclude that a combination of features is not possible and advantageous.

## CLAIMS

1. A control system (200) for a wind turbine generator (100), the wind turbine generator comprising a reactive power controller (203), the control system comprising
  - 5 - a QV limit module (201) configured to define predetermined reactive limits (302) dependent on an output voltage ( $U_{WTG}$ ) of the wind turbine generator, wherein the QV limit module is configured to receive a reactive reference ( $Q_{ref}$ ) from an external source (520, 220), and wherein the QV limit module is configured to output the reactive reference as an output reactive reference ( $Q_{refQV}$ ) and, in
    - 10 case the reactive reference ( $Q_{ref}$ ) exceeds one of the predetermined reactive limits (302), the QV limit module is configured to determine the output reactive reference ( $Q_{refQV}$ ) by limiting the reactive reference ( $Q_{ref}$ ) to the exceeded predetermined reactive limit (302), and wherein the reactive power controller (203) is configured to control generation of reactive power from a power
      - 15 generator system (101) of the wind turbine generator (100) dependent on the output reactive reference ( $Q_{refQV}$ ) or other reactive reference ( $Q_{refQP}$ ,  $Q_{refXX}$ ) being dependent on the output reactive reference ( $Q_{refQV}$ ), and
      - an update module (210) configured to supply the predetermined reactive limit ( $Q_{limitQV}$ ) for an actual output voltage back to the external source (520).
- 20  
2. A control system according to claim 1, wherein the QV limit module (201) is configured so that the predetermined reactive limits define capacitive limits (303) setting limits for the reactive references ( $Q_{ref}$ ) being capacitive references ( $Q_{refcap}$ ) and inductive limits (304) setting limits for the reactive references
  - 25 ( $Q_{ref}$ ) being inductive references ( $Q_{refind}$ ) within a predefined range of the output voltage ( $U_{WTG}$ ).
3. A control system according to claim 2, wherein the QV limit module (201) is configured so that the capacitive limits decreases for increasing output voltages
  - 30 above a first threshold voltage ( $U_1$ ).
4. A control system according to any of claims 2-3, wherein QV limit module (201) is configured so that the inductive limits decreases for decreasing output voltages below a second threshold voltage ( $U_2$ ).

5. A control system according to claim 3, wherein the QV limit module (201) is configured so that the capacitive limits comprise extended capacitive limits (321) defining inductive values which increase for increasing output voltages above a third threshold voltage (U3) being greater than the first threshold voltage (U1),  
5 and wherein the QV limit module is configured to set the capacitive reference (Qrefcap) to an inductive value according to the extended capacitive limits (321) in case the output voltage exceeds the third threshold voltage.
6. A control system according to claim 4, wherein the QV limit module (201) is  
10 configured so that the inductive limits comprise extended inductive limits (322) defining capacitive values which increase for increasing output voltages below a fourth threshold voltage (U4) being smaller than the second threshold voltage (U2), and wherein the QV limit module is configured to set the inductive reference (Qrefind) to a capacitive value according to the extended inductive limits (322) in  
15 case the output voltage is smaller than the third threshold voltage.
7. A control system according to any of claims 2-6, wherein the QV limit module (201) is configured so that the inductive limits increase above a nominal limit (Q2) for increasing output voltages above a fifth threshold voltage (U5) being  
20 greater than the third threshold voltage (U3), and wherein the QV limit module is configured to set the inductive reference (Qrefind) to one of the inductive limits above the nominal limit (Q2) in case the output voltage exceeds the fifth threshold voltage.
- 25 8. A control system according to any of claims 2-7, wherein the QV limit module (201) is configured so that the capacitive limits (303) increase above a nominal limit (Q1) for decreasing output voltages below a sixth threshold voltage (U6) being smaller than the fourth threshold voltage (U4), and wherein the QV limit module is configured to set the capacitive reference (Qrefcap) to the one of the  
30 capacitive limits above the nominal limit (Q1) in case the output voltage is smaller than the sixth threshold voltage.
9. A control system according to any of the preceding claims, wherein the control system (200) further comprises a QP limit module (202) configured to define  
35 predetermined reactive limits dependent on an active reference, wherein the QP

limit module is configured to limit the output reactive reference (QrefQV) in case the output reactive reference (QrefQV) exceeds the predetermined reactive limits of the QP limit module.

5 10. A control system according to claim 9, wherein the update module (210) is configured to compare the predetermined reactive limit (QlimitQV) for an actual output voltage of the QV limit module (201) with the predetermined reactive limit of the QP limit module (202) so as to determine the most restrictive reactive limit, and configured to supply the determined most restrictive reactive limit back to the  
10 external source (520).

11. A control system according to any of the preceding claims, wherein the control system comprise one or more other limit modules (202, 401) connected in series with the QV limit module (201), and wherein the other limit modules define  
15 predetermined reactive limits dependent on other physical parameters.

12. A control system according to claim 11, wherein the update module (210) is configured to compare the predetermined reactive limit (QlimitQV) for an actual output voltage of the QV limit module (201) with the predetermined reactive  
20 limit(s) of the one or more other limit modules (202, 401) so as to determine the most restrictive reactive limit, and configured to supply the determined most restrictive reactive limit back to the external source (520).

13. A wind turbine generator (100) comprising the control system according to claim 1.

25

14. A method for controlling a wind turbine generator (100), comprising  
- receiving a reactive reference (Qref) from an external source (520, 220),  
- outputting the reactive reference (Qref) as an output reactive reference (QrefQV), wherein, in case the reactive reference (Qref) exceeds one of a plurality  
30 of predetermined reactive limits (302), the output reactive reference (QrefQV) is determined by limiting the reactive reference (Qref) to the exceeded predetermined reactive limit (302), and wherein the predetermined reactive limits (302) are dependent on an output voltage (U\_WTG) of the wind turbine generator,

- controlling generation of reactive power from a power generator system (101) of the wind turbine generator dependent on the output reactive reference ( $Q_{refQV}$ ) or other reactive reference ( $Q_{refQP}$ ) being dependent on the output reactive reference ( $Q_{refQV}$ ), and
- 5 - supplying the predetermined reactive limit ( $Q_{limitQV}$ ) for an actual output voltage back to the external source (520).

15. At least one computer program product directly loadable into the internal memory of at least one digital computer, comprising software code portions for  
10 performing the steps of the method according to claim 14 when said at least one product is/are run on said at least one computer.

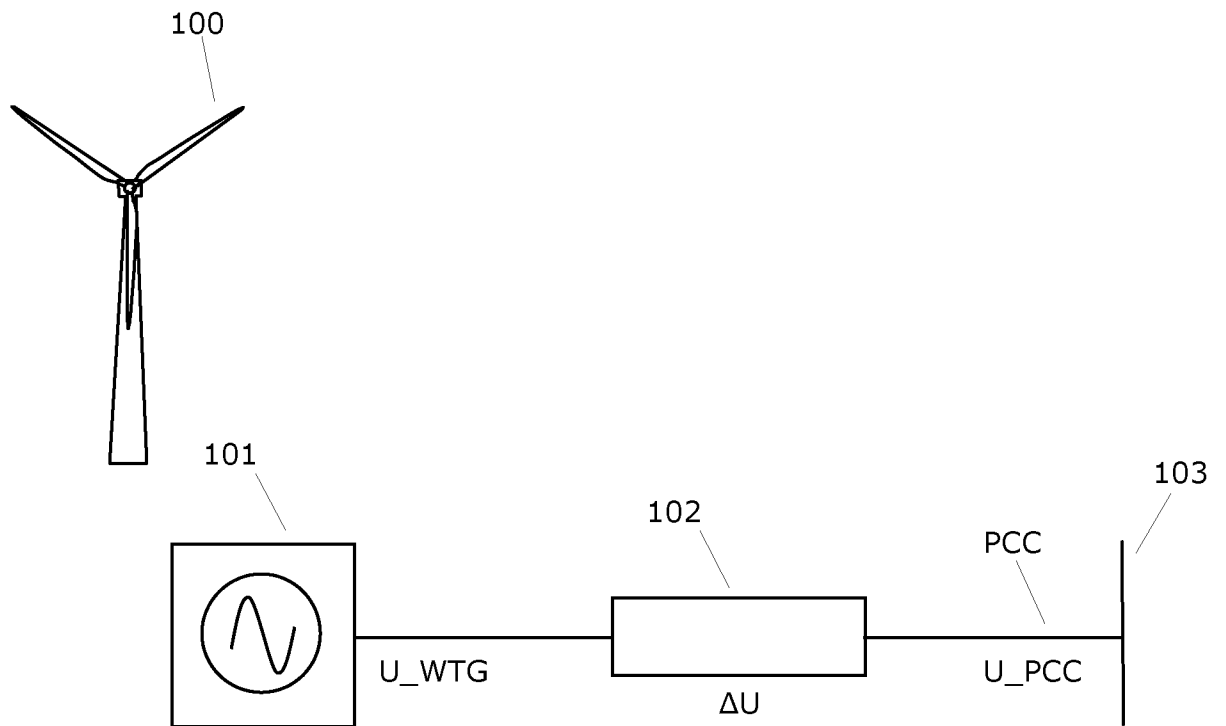


Fig. 1

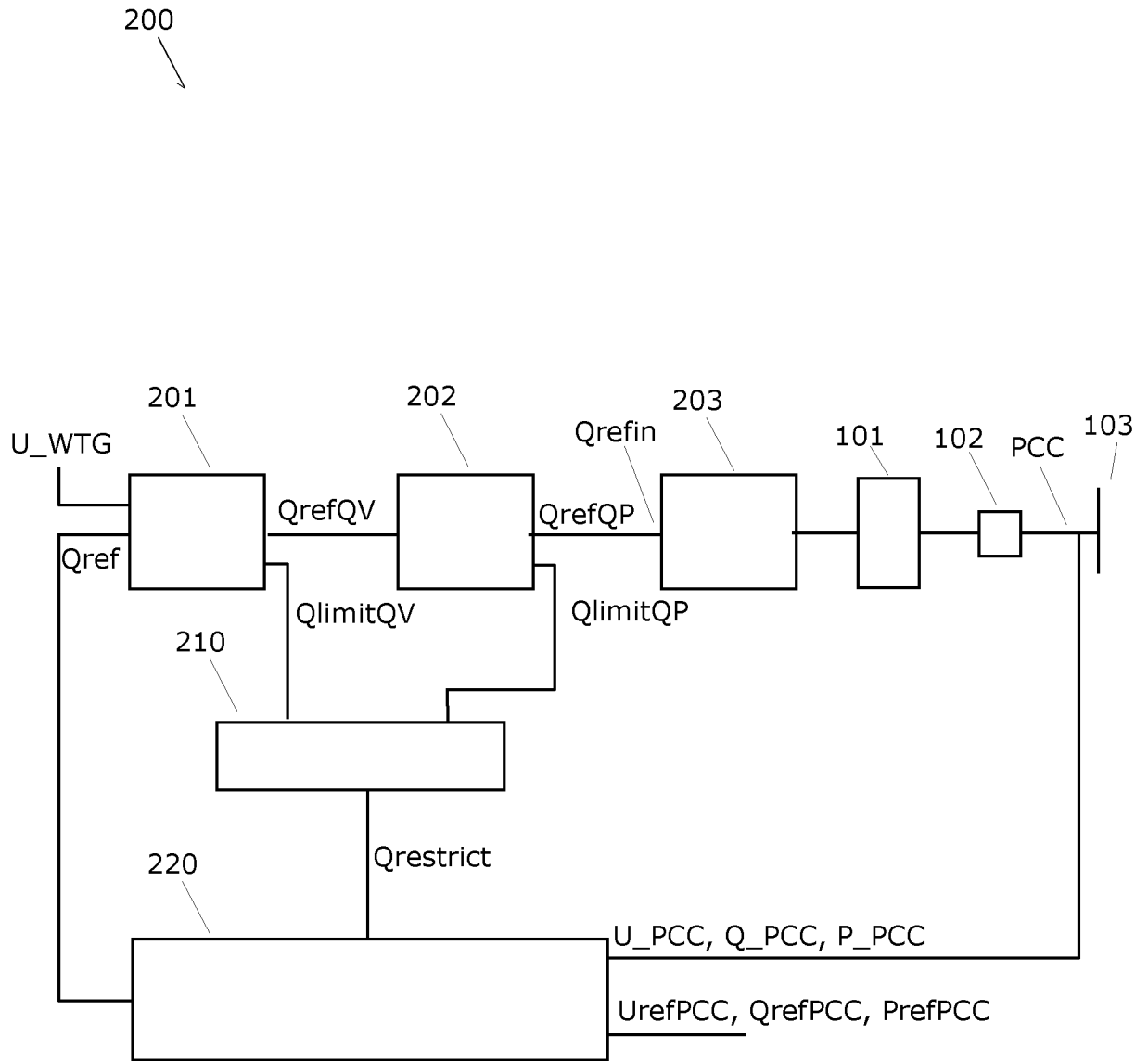


Fig. 2

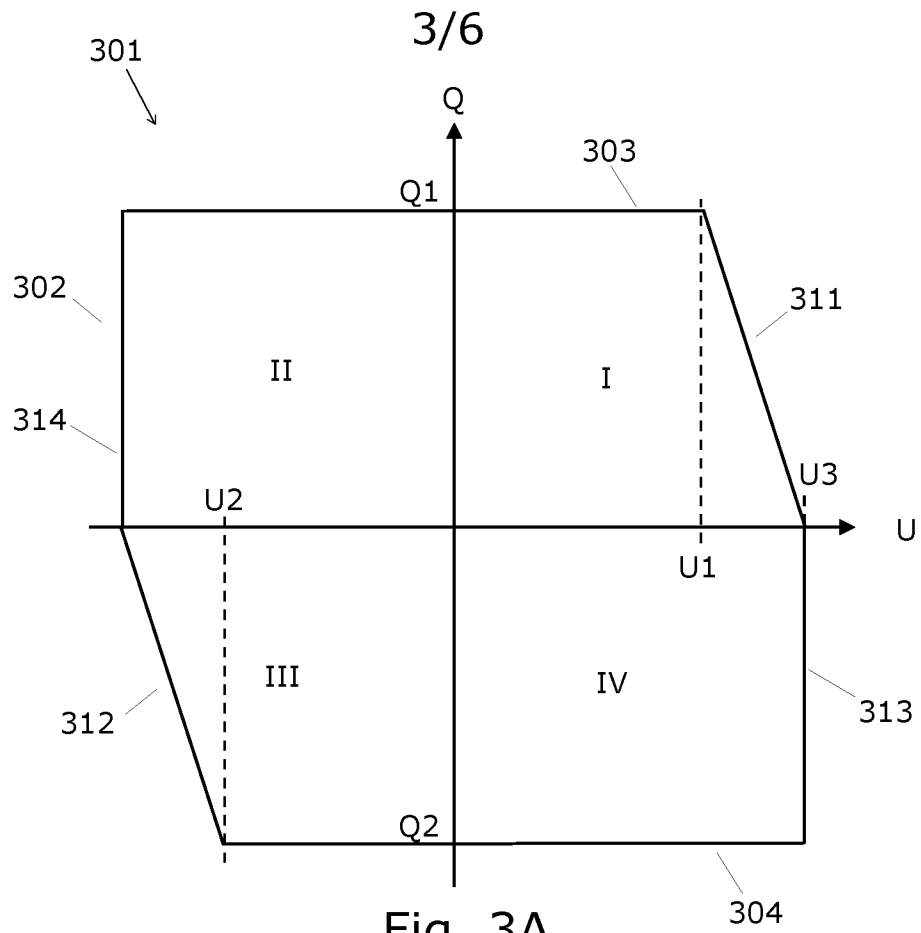


Fig. 3A

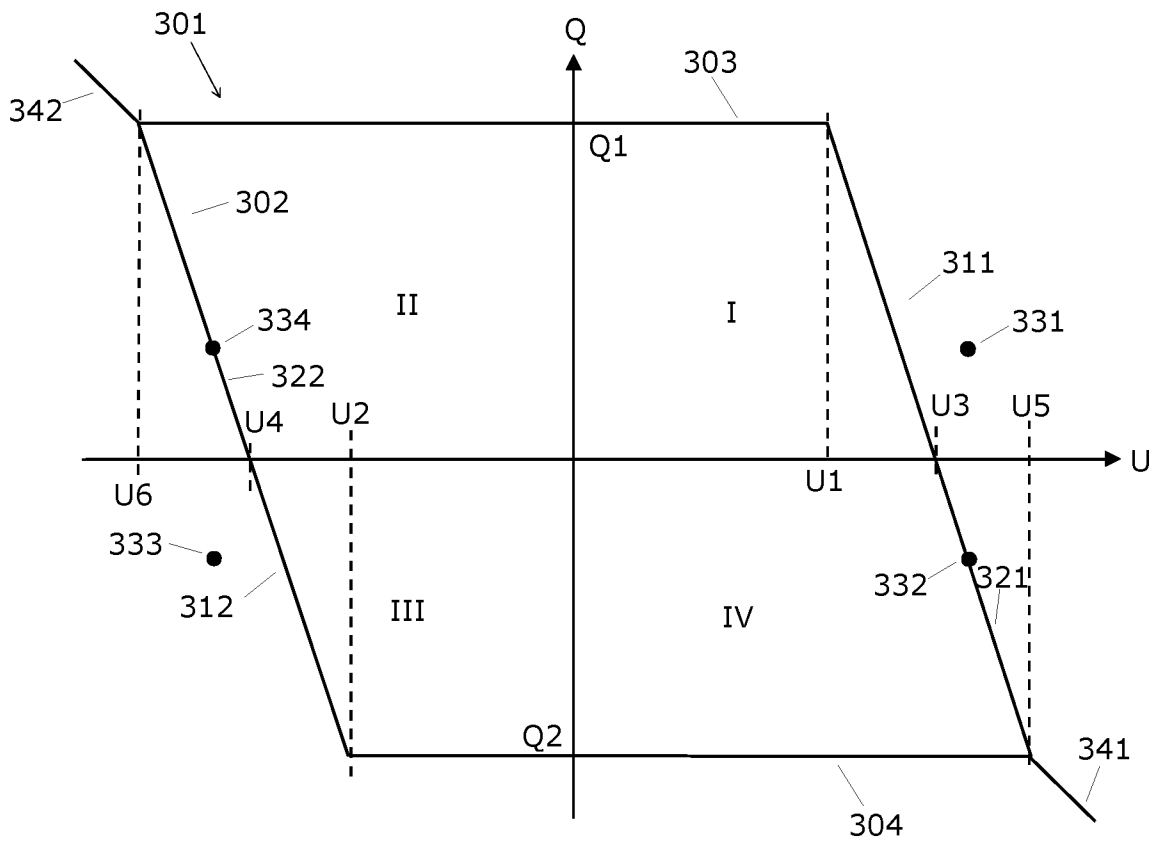


Fig. 3B

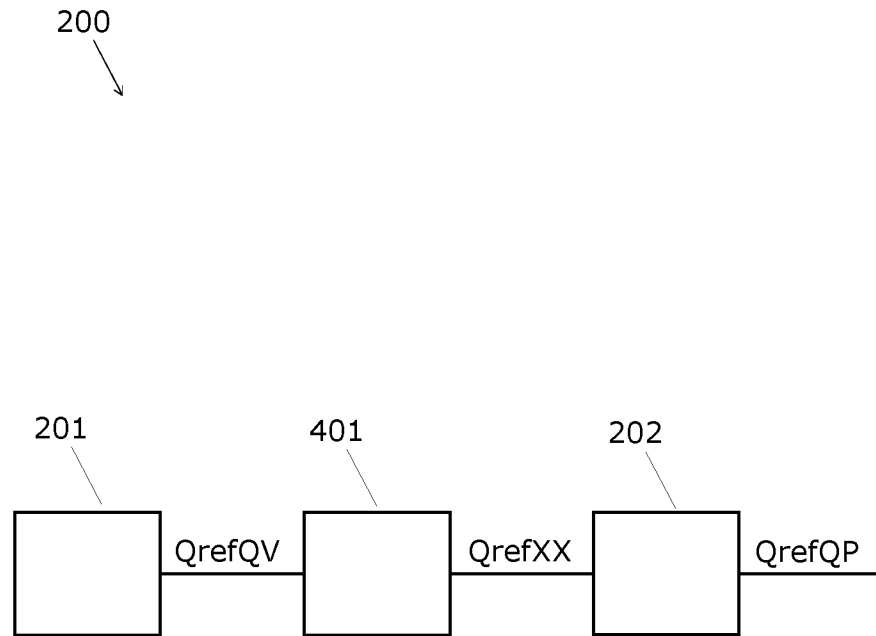


Fig. 4

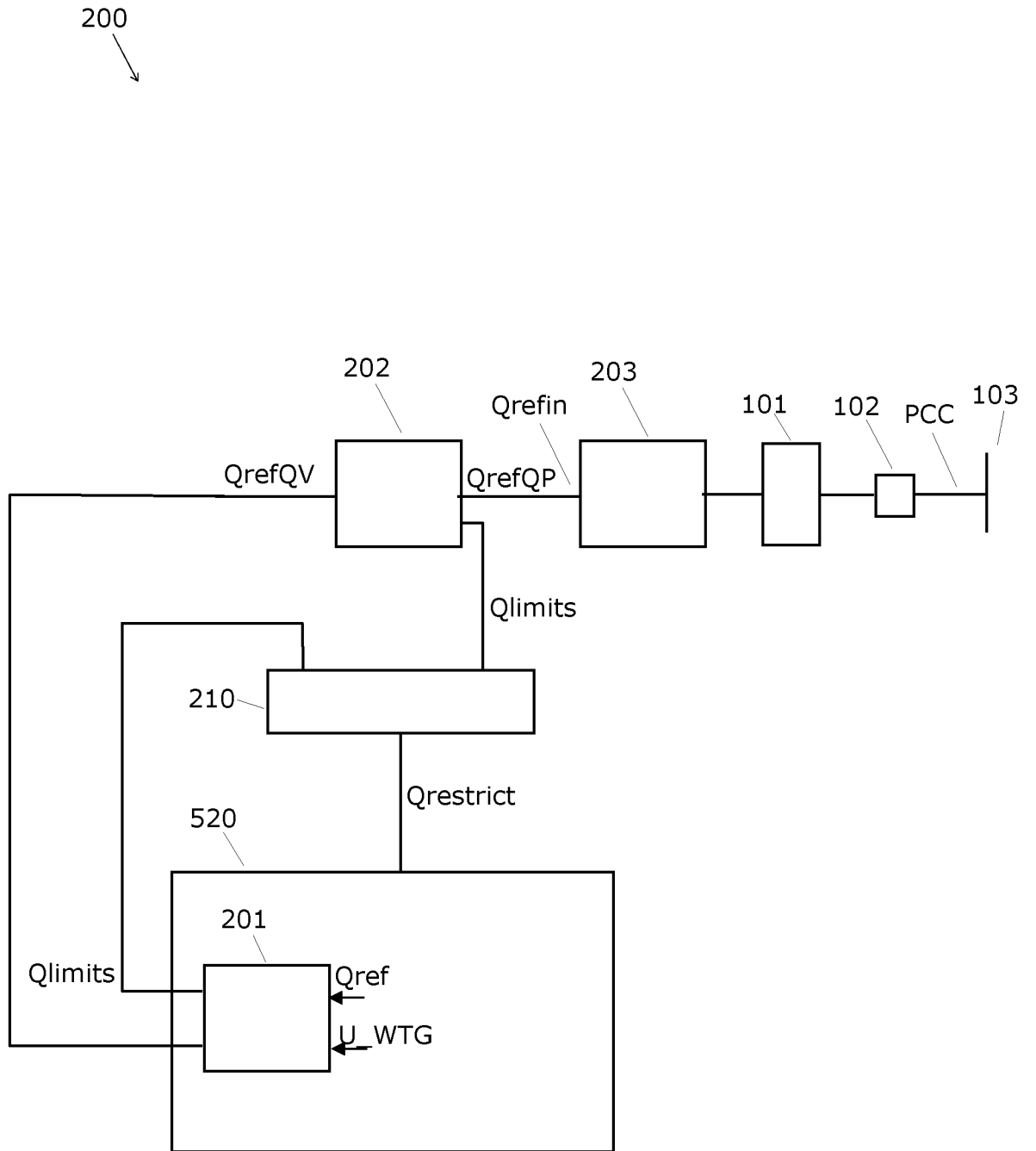


Fig. 5

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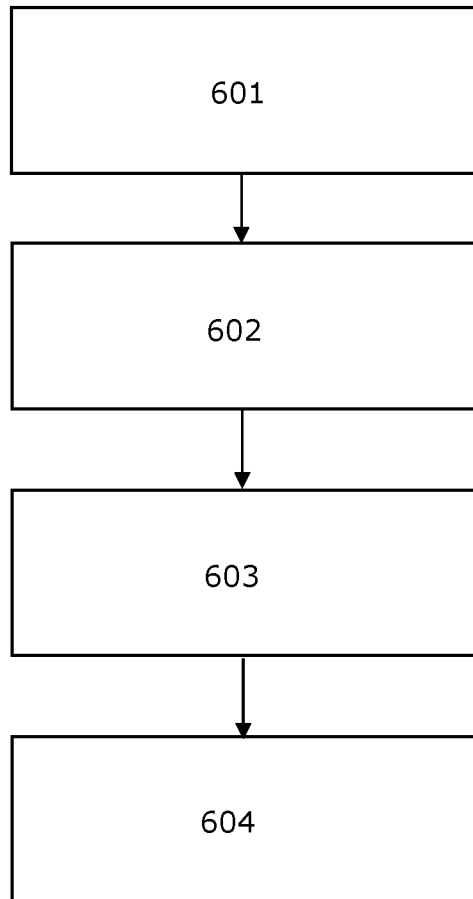


Fig. 6

**INTERNATIONAL SEARCH REPORT**

International application No PCT/DK2015/050225
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**A. CLASSIFICATION OF SUBJECT MATTER**  
 INV. H02J3/16 H02J3/38 F03D7/04 H02P9/00  
 ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**  
 Minimum documentation searched (classification system followed by classification symbols)  
 H02J F03D H02P

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)  
 EPO-Internal, WPI Data

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X Y	US 2011/156389 A1 (ARLABAN GABEIRAS TERESA [ES] ET AL) 30 June 2011 (2011-06-30) abstract paragraphs [0028], [0061] - [0067]; claim 1; figures 1,2,3,7	1,2,4, 9-14 3,5-8
X	----- VALVERDE GUSTAVO ET AL: "Reactive power limits in distributed generators from generic capability curves", 2014 IEEE PES GENERAL MEETING   CONFERENCE & EXPOSITION, IEEE, 27 July 2014 (2014-07-27), pages 1-5, XP032670411, DOI: 10.1109/PESGM.2014.6939359 [retrieved on 2014-10-29]	1-15
Y	page 1, left-hand column page 3, left-hand column; figure 3; table III -----	3,5-8

Further documents are listed in the continuation of Box C.       See patent family annex.

\* Special categories of cited documents :

"A" document defining the general state of the art which is not considered to be of particular relevance	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"E" earlier application or patent but published on or after the international filing date	"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"O" document referring to an oral disclosure, use, exhibition or other means	"&" document member of the same patent family
"P" document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search  8 October 2015	Date of mailing of the international search report  16/10/2015
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Name and mailing address of the ISA/ European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Fax: (+31-70) 340-3016	Authorized officer  Jäschke, Holger
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# INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/DK2015/050225

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 2011156389 A1	30-06-2011	EP 2317135 A1	04-05-2011
		ES 2333393 A1	19-02-2010
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		WO 2009147274 A1	10-12-2009
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