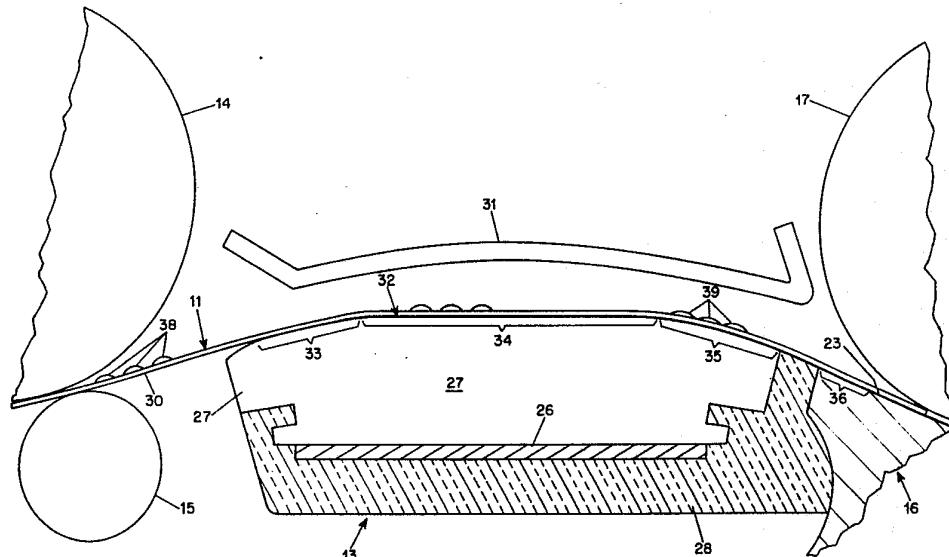




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(54) Title: TREATMENT OF HOT MELT INK IMAGES



(57) Abstract

In the embodiment described in the specification, a hot melt ink image on a substrate (11) is treated in a continuous manner by moving it along a platen (27) having a heating zone to melt drops (38) of hot melt ink and cause them to spread on the substrate. The platen has a flat central portion (34) and curved portions (33, 35) at each end with curvatures sufficient to prevent formation of cockle. At the output end of the heating zone, the substrate (11) is moved continuously into a quenching zone (36) where a cooling platen (16) cools the substrate (11) by thermal contact at a rapid rate to prevent crystallization or frosting of the hot melt ink image. After the quenching zone, the substrate is moved along a surface having a reverse curvature with respect to the curved portions (33, 35) of the heating platen (27) to eliminate residual curvature of the substrate resulting from the curved portions of the heating platen.

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DescriptionTreatment of Hot Melt Ink ImagesTechnical Field

This invention relates to treatment of hot melt ink images and, more particularly, to a system for treating hot melt ink images so as to enhance the quality of the images and, at the same time, prevent cockling and inhibit curling of the substrate which may occur in the processing of the hot melt ink images.

Background Art

In the preparation of hot melt ink images, improved quality can be obtained by maintaining the temperature of the ink on a substrate above its melting point for a selected time. For example, as described in the Fulton et al. Patent No. 4,873,134, heating of a hot melt ink transparency prepared by ink jet printing to a temperature above the melting point of the hot melt ink followed by rapid quenching produces improved transparency projection characteristics. For optimum image quality, the time during which the ink is maintained above its melting point, and the rate of quenching thereafter, should be uniform throughout the image. Moreover, during this process the transparency substrate, which may be made of a sheet of polyester material such as Mylar, for example, may be heated to a temperature that is above the glass transition temperature of the substrate material.

Similarly, as described in the Hoisington et al. Application Serial No. 07/272,005, filed November 15, 1988, the quality of hot melt ink images on porous substrates may be improved by maintaining the sub-

strate at a temperature above its melting point for a selected time.

As described in the Spehrley Jr. et al. Patent No. 4,751,528, however, when a substrate material 5 passes between a high-temperature region and a low-temperature region, differential thermal expansion of the substrate tends to produce cockle in the substrate. Because of the rapid and extreme temperature changes to which a substrate may be subjected during 10 processing of the type described in the above-mentioned Fulton et al. patent and the Hoisington et al. application, there is a strong tendency for the substrate to cockle. Such cockling causes separation of portions of the substrate from the heating and/or 15 cooling surface, causing nonuniform heating and/or cooling of the ink drops on the substrate with an accompanying loss of quality of the image. To prevent such cockle, the substrate may be supported on a curved platen.

20 The response to heating of substrate materials such as transparency substrate polyesters and paper substrates differs and the cockle effect is caused in those substrates in differing ways. When a web or sheet of paper substrate passes from ambient temperature 25 into a heated zone, it expands so that the width of the web increases but, after the paper has been heated for a period of time (typically 5 to 10 seconds), it loses moisture and shrinks, making the web or sheet narrower. On the other hand, the width of a 30 polyester substrate remains larger after it passes into a heated zone so that the cockling effect resulting from such passage must be counteracted or prevented in a different way. During rapid processing of the type described herein, however, the moisture loss 35 from a paper substrate is not significant so that, in general, the same procedures can be used to prevent cockle in both types of substrates during the processing described herein.

When a polyester substrate is kept at a temperature above its glass transition temperature, the substrate loses its flatness memory and tends to conform to the shape in which it is maintained when heated.

5 Thus, where a curved platen surface is provided to prevent cockle, hot melt ink transparencies which have been heated while on the curved surface are formed with a curl which prevents them from lying flat on a projection surface, causing the projected image to be
10 unsatisfactory. Paper substrates may also be curled by such processing.

Disclosure of Invention

Accordingly, it is an object of the present invention to provide a new and improved system for
15 treating hot melt ink images which overcomes the above-mentioned disadvantages of the prior art.

A further object of the invention is to provide a system for treating hot melt ink transparencies to provide improved projection quality of color images.

20 An additional object is to provide a continuous process and apparatus for treating hot melt ink images in which the images are heated rapidly and uniformly for a predetermined time period and cooled rapidly at the end of the predetermined period.

25 Another object of the invention is to provide a system for reducing curl in hot melt ink transparencies to a level which does not cause deterioration of a projected image.

These and other objects of the invention are
30 attained by moving a hot melt ink image on a substrate in a controlled manner into a heating zone across a surface which has sufficient curvature to prevent cockle, maintaining the image within the heating zone for a time long enough to permit hot melt ink drops to
35 melt and spread on the substrate, and moving the image in a controlled manner out of the heating zone along a surface which has sufficient curvature to prevent

formation of cockle in the substrate. Preferably, the substrate is supported at a reduced curvature or held substantially flat in the region of the heating zone between the curved surfaces, and for this purpose, it 5 may be held against the surface of a heated platen.

To avoid crystallization or frosting during cooling of the hot melt ink in the image formed on the substrate, the image is moved from the heating zone to a quenching zone where the temperature is reduced at a 10 rapid rate, such as at least 50°C/sec. and, preferably, at least 500°C/sec. Preferably, quenching is effected by moving the substrate into heat-transfer contact with a relatively cold platen. In addition, to reduce or eliminate curl which may interfere with 15 the quality of projected transparency images, the substrate is preferably moved along a surface having a reverse curvature after quenching. To assure uniform treatment of the hot melt ink image, the substrate is moved continuously through the heating and quenching 20 zones at a uniform rate.

One form of apparatus for treating hot melt ink images includes a heated platen having a substantially flat center surface and curved surfaces at the inlet and outlet ends, along with a substrate-conveying 25 mechanism for conveying an image-containing substrate across the platen surface at a uniform rate and holding it against the curved and flat portions of the surface as it is moved across the surface. To provide quenching, a cooling platen has a quenching zone positioned adjacent to the outlet end of the heated platen 30 and, to assure good heat transfer, the surface of the cooling platen in the quenching zone is preferably curved. In addition, to remove curl in the substrate, the cooling platen has a reversely curved surface to 35 receive the substrate after it has passed through the quenching zone.

Brief Description of Drawings

Further objects and advantages of the invention will be apparent from a reading of the following description in conjunction with the accompanying drawings in which:

Fig. 1 is a schematic sectional view illustrating a representative arrangement for treating hot melt ink images in accordance with the invention; and

Fig. 2 is an enlarged fragmentary view of the arrangement shown in Fig. 1 illustrating the platen arrangement in greater detail.

Best Mode for Carrying Out the Invention

The typical embodiment of the invention shown in the drawings comprises an apparatus 10 having a heating zone for heating a hot melt ink print 11 to melt the ink for a selected time period and a quenching zone for quenching the hot melt ink image at the end of the selected time period to produce a print 12 in which the hot melt ink has spread so as to provide improved image quality without objectionable curl.

The heating zone is formed by a substrate heating platen 13, described in greater detail hereinafter, to which the print 11 is supplied by an input drive roll 14 and a cooperating pinch roll 15. A cooling platen 16, also described hereinafter, has a cooperating drive roll 17 to receive the print 11 from the heating platen 13 and quench the hot melt ink image thereon while moving the print away from the heating zone.

As illustrated in Fig. 1, the cooling platen 16 has two arrays of cooling fins 18 and 19 and the entire hot melt ink image treatment arrangement is enclosed in a housing 20. A spring device 21 supported by the interior surface of the housing 20 has a spring arm 22 which urges the surface 23 of the cooling platen 16 against the output drive roll 17, the cooling platen being pivotally supported by a shaft 24 near the end of an arm 25 adjacent to the pinch roll

15. The housing is arranged to permit circulation of air either by convection or by a fan (not shown) past the arrays of fins 18 and 19 to remove heat from the cooling platen and maintain the temperature of that
5 platen within a desired range, such as below 55°C, to assure rapid cooling of the hot melt ink in the image on the substrate after it leaves the heating zone. Alternatively, if desired, the cooling platen may be cooled by liquid circulation or by a thermoelectric
10 cooling device.

The heating platen 13 includes an electric heater 26 mounted at the rear surface of a platen body 27 and covered by a layer of insulation 28 which also fills the gap between the heating and cooling platens to
15 inhibit direct heating of the adjacent portion of the cooling platen 16. Alternatively, if desired, an air gap may be provided between the adjacent ends of the heating and cooling platens. In order to provide improved quality hot melt ink images by spreading of
20 hot melt ink drops deposited on a substrate 30 by an ink jet printer as described in the above-mentioned Fulton et al. Patent No. 4,873,134 and the Hoisington et al. Application Serial No. 07/272,005, the substrate 30 should be heated in the heating zone to a
25 controlled temperature above the melting point of the ink, such as, for example, 95°C, for a period of, for example, 0.5 to 10 sec. and, preferably, 1 to 5 sec., preferably by contact heat transfer.

A guide member 31, spaced from a substrate-
30 engaging surface 32 of the heated platen body 27, is positioned to enclose the heating zone and to guide the leading and trailing edges of the substrate 30 as it is driven by the input rolls 14 and 15 through the heating zone and into the nip between the cooling
35 platen 16 and the output drive roll 17. Accordingly, the temperature of the platen body 27 is maintained at a desired level above the melting point of the ink and the drive rolls 14 and 17 are arranged as described

hereinafter to maintain each portion of the transparency 11 in the heating zone for the desired length of time.

Since the substrate is heated by heat transfer
5 contact with a temperature-controlled platen, the temperature of the substrate will approach the temperature of the platen at a rate with a thermal time constant, *i.e.*, the time in which the temperature difference is reduced by 63%, of approximately 0.05
10 sec. to 0.10 sec. As a result, if the platen temperature is sufficiently above the melting point of the ink, the desired substrate and ink temperatures can be achieved within the first 0.1 sec. to 0.4 sec., and thereafter it is only thermally necessary to prevent
15 the substrate from cooling before leaving the heating zone.

As best seen in Fig. 2, the heated substrate-engaging surface 32 of the platen 27 has a curved surface section 33 at the input end, a substantially
20 flat central section 34, and another curved section 35 at the output end of the heating zone. Cockle of the substrate not only detracts from the appearance of the print but, more importantly, causes portions of the substrate to be held out of contact with the heating
25 and cooling platens. Where thermal contact heat transfer is required, as in the described platen arrangement, separation of the substrate from the platen surface by more than about 1 or 2 mils (0.025 or
0.05mm) can increase the heat transfer time constant
30 by a factor of two or more so that the desired heating and cooling rates may not be achieved.

The curved surfaces 33 and 35 are arranged to have a curvature which is sufficient to prevent cockle of the substrate 11 as it moves between room temperature at the input end and the high-temperature heating zone and between the heating zone and the low-temperature cooling platen. For example, these curved surfaces may have a radius of less than 8 cm.

and preferably 3 cm. to 5 cm. The central section 34 of the heating platen is preferably flat but, if desired, it may be slightly curved, so long as the curvature imparted to a transparency substrate during 5 its passage along the heating platen is not great enough to prevent it from being overcome by the subsequent decurling action of the cooling platen. Preferably, the radius of curvature of the central section 34 is at least 5 cm.

10 The optimum curvatures of the input and output surfaces 33 and 35, and of the center section 34, if curved, depend upon the ambient temperature, the processing temperature, which is related to the melting temperature of the ink, and the glass transition temperature of the substrate. Of course, if the glass 15 transition temperature of the substrate is above the processing temperature, the curvatures will not cause the substrate to curl and, as long as the radius is small enough to prevent cockle, the values of the 20 curvatures are not important. The radius of curvature required to prevent cockle is given by the equation:

$$R \leq \frac{E \cdot t \cdot k}{\Delta T \cdot \alpha}$$

25 where E is Young's Modulus of the substrate material at the processing temperature, t is the thickness of the substrate, k is a constant, ΔT is the difference between the processing temperature and the lower of the inlet temperature and the quenching temperature, 30 and α is the thermal expansion coefficient of the substrate material. Since Mylar has a high Young's Modulus and a low thermal expansion coefficient, it is a preferred material for use as a transparency substrate.

35 In addition, the angular length of each of the input and output curved surfaces, i.e., the portion 33 and the portion 35 together with the adjacent insulation and cooling platen surfaces, should be great enough to provide good mechanical stability of the

curved substrate. For a 4 mil (0.1 mm) Mylar thick substrate, which is the size and type most readily available, and for most paper substrates, the angular length of those surfaces is preferably at least 10° and desirably 15°.

In order to transport the substrate 30 through the heating zone at a controlled rate, the output drive roll 17 is arranged to drive the substrate at a rate faster than it is driven by the input drive roll 14, and the input drive roll has a one-way clutch arranged to permit the substrate to turn it while causing sufficient drag to hold the substrate against the surface 32 of the platen 27. The slower speed of the input drive roll 14 is selected to permit the leading edge of the substrate 11 to be retained in the heating zone for a slightly longer period to compensate for any lack of close contact with the surface 32 before the substrate is engaged between the drive roll 17 and the surface 23 of the quench platen 16.

For example, the input drive roll 14 may be arranged to advance the substrate 11 at a rate of about 0.5 cm/sec, whereas the output drive roll 17 is arranged to drive the substrate at a rate of about 1 cm/sec. With a total length of the heated platen surface 32 of about 2.5 cm, this arrangement provides a residence time in the heating zone of about 5 sec. for the leading edge of the substrate which is not held tightly against the surface 32, since it has not been engaged by the output drive roll 17, and a residence time of about 2.5 sec. for the rest of the substrate 11, which, except for the trailing end, is held tightly against the heated surface 32 of the platen after the leading edge has been engaged by the output drive roll 17. Since the substrate has been substantially heated by the time the trailing end leaves the input drive roll 16, it is not necessary to hold that end in intimate contact with the platen surface. Preferably, the substrate drive speed provided by the

drive roll 17 is in the range from about 0.25 to 5 cm/sec. and, desirably, the drive speed is in the range from 0.5 to 2 cm/sec.

In the illustrated embodiment, the angular length 5 of the input curved surface section 33 may be about 10°, providing a linear curved surface length of about 0.6 cm, and the angular length of the output curved surface section 35 may be about 5°, providing a curved surface length of about 0.3 cm so that, at a drive 10 speed of 1 cm/sec., the residence time of the portion of the substrate in contact with the output curved surface is only about 0.3 sec. On the other hand, the substrate is held close to or against the flat portion 34 of the platen for about 1.6 secs. As a result of 15 the beam strength of the substrate material, the substrate will not necessarily be held in complete contact with the platen surface 32 along the entire length of the center section 34.

Because the polyester material of a substrate 20 such as Mylar is thus held against the flat or substantially flat surface portion 34 during a large portion of its passage through the heating zone and for a time which is long enough to permit the substrate material to relax, it retains less of the 25 curvature resulting from its passage along the curved surface portions of the platen surface 32.

The cooling platen 16 has a quenching zone 36 adjacent to the output end of the heating zone which receives the substrate 30 as it passes out of the 30 heating zone and quenches the ink image thereon at a rapid rate to avoid crystallization and frosting. For this purpose, the cooling platen temperature in the quenching zone 36 should be low enough to cool the ink at a rate of at least 50°C/sec. and, preferably, at 35 least 500°C/sec. Cooling by contact heat transfer to a metal or other heat-conductive surface is adequate. for this purpose, as long as the quench surface is maintained adequately below the melting temperature of

the ink. Preferably, the cooling platen temperature in the quenching zone is at least 10°C below the melting point of the ink and, desirably, it is at least 30°C below the melting point.

5 With a quenching zone temperature 30°C below the ink melting point and a substrate moving at a rate of about 1 cm/sec., molten ink on the substrate will solidify in substantially less than one second and, preferably, less than one-half second, corresponding
10 to a distance of less than 1 cm. so that a quenching zone 36 having a length of 1 cm. should be sufficient. Therefore, if the drive roll 17 engages the surface of the substrate 30 containing the ink drops at least 1 cm. beyond the beginning of the quenching zone, the
15 ink will be solidified before the drive roll engages the surface, thereby preventing any flattening or other deformation of the ink drops which might degrade the projected image quality of the transparency. This also avoids any offsetting of soft ink onto the drive
20 roll which could produce image defects in a subsequent portion of the same print or other prints.

Since there are compressive cockle-inducing stresses in the substrate until the substrate is cooled, it is important to continue the curvature at
25 the output end of the heating zone into the quenching zone 36. For this purpose, the surface of the insulating layer 28 between the heating platen and the cooling platen and the surface 23 of the cooling platen in the quenching zone have the same curvature
30 as that of the region 35 of the heating platen surface 32. This not only prevents cockle, but also assures good contact of the substrate with the surface 23 of the cooling platen in the quenching zone to provide
35 good heat transfer so that any molten ink drops on the substrate are solidified before they reach the output drive roll. For example, if the quenching time is 150 milliseconds and the substrate is driven at 1 cm/sec.,

a quenching zone length of a few millimeters is sufficient.

After the substrate has passed the quenching zone 36 and is engaged by the output drive roll 17, it is 5 held against and driven around a curved cooling platen surface 37 which has a reverse curvature with respect to the surface portions 33 and 35. Even though a transparency substrate has already been cooled below the glass transition point of the substrate material 10 when it reaches the drive roll 17, it has been found surprisingly that the curl produced in the substrate by the curved surfaces of the heated platen can be reduced or eliminated by passing it along the reverse-curvature cooling platen surface 37 promptly 15 after leaving the quenching zone. The radius of curvature of the reverse curved surface 36 should be less than that of the surfaces 33 and 35 and, desirably, the radius of curvature is less than half that of the surfaces 33 and 35. In a preferred arrangement, the 20 radius of the surface 37 is about one-quarter of that of the surfaces 33 and 35, i.e., about one cm. The effect on decurling is surprising because the stress in a 4-mil (0.1mm) Mylar substrate in the 1 cm. radius curvature section 36 is only about 2,500 psi, which is 25 less than 25% of the yield strength of the material at a cooling platen temperature of about 45°C.

In a typical example, a print 11 having solid hot melt ink drops 38 which were deposited on the surface of the substrate 30 during ink jet printing is passed 30 through a heating zone having a platen temperature of about 95°C at a rate of 1 cm/sec. In the heating zone, the solid ink drops, which have a melting point of about 80°C, are melted and permitted to spread on the surface of the substrate to produce drops 39 having 35 a larger area and an increased radius of curvature, resulting in improved image quality as described in the above-mentioned Fulton et al. patent and the Hoisington et al. application. In the drawings, the

drops 38 and 39, which may, for example, be about 0.1-0.2 mm. in diameter, are illustrated in exaggerated size to show the change of surface shape which results from the processing.

5 As the substrate 11 passes from the heating zone, it moves into thermal contact with the surface 23 of the cooling platen 16 in the quenching zone 36 which, in this example, is maintained at about 45°C. With good thermal contact between the substrate and the

10 surface 23 because of the curved surface in the quenching zone, the thermal transfer time constant is about 0.1 sec., causing the temperature of the substrate and its ink image to be reduced by about 32°C (63% of the difference between 95°C and 45°C) to about

15 63°C in about 0.1 sec. or about 1 mm. of substrate motion into the quenching zone. The average rate of cooling during this time period is 320°C/sec., but the initial cooling rate during the time in which the temperature is reduced to a level below the 80°C melting point is higher since the cooling rate is a negative exponential. During the next 0.1 sec., the temperature falls to about 52°C and the ink temperature continues to approach 45°C as the substrate moves along the cooling platen.

20 25 Such rapid cooling prevents significant crystallization and frosting of the ink image and assures that the ink drops 39 are solidified before they are engaged by the drive roll 17. Thereafter, the substrate 11 is driven around the reverse-curvature surface 37 of the platen, which results in substantial elimination of any curvature caused by passage of the substrate 30 along the curved surfaces 33 and 35 while at an elevated temperature.

30 35 40 Although the invention has been described herein with reference to specific embodiments, many modifications and variations therein will readily occur to those skilled in the art. For example, the curved surfaces 33, 35, 36 and 37 are described herein with

reference to curvatures of fixed radius. It will be apparent, however, that those surfaces may have a varying radius of curvature. Accordingly, all such variations and modifications are included within the 5 intended scope of the invention.

Claims

1. Apparatus for treating hot melt ink images comprising heating means providing a heating zone for heating solid hot melt ink on a substrate to a selected temperature above the melting point of the hot melt ink, quenching means providing a quenching zone adjacent to the heating zone to cool molten ink on the substrate rapidly, and drive means for moving a substrate at a controlled rate through the heating zone and the quenching zone in succession so as to heat hot melt ink on a substrate to a temperature above its melting point for a time period in the range from 0.5 to 10 seconds and immediately thereafter cool the ink to a temperature below its melting point within one second.
2. Apparatus according to Claim 1 wherein the drive means moves the substrate at a controlled rate within the range from 0.25 cm/sec. to 5 cm/sec.
- 20 3. Apparatus according to Claim 1 wherein the drive means moves the substrate at a controlled rate within the range from 0.5 cm/sec. to 2 cm/sec.
4. Apparatus according to Claim 1 wherein the hot melt ink is maintained at a temperature above its melting point for a time period in the range from 1 to 5 secs.
- 25 5. Apparatus according to Claim 1 wherein the hot melt ink is cooled to a temperature below its melting point within 0.5 sec.
- 30 6. Apparatus according to Claim 1 wherein the heating means comprises a heating platen arranged to

provide thermal contact heat transfer between the heating platen and the substrate.

7. Apparatus according to Claim 1 wherein the cooling means comprises a cooling platen arranged to provide thermal contact heat transfer between the cooling platen and the substrate.
8. Apparatus for treating hot melt ink images comprising heating means providing a heating zone for heating a substrate to a temperature which is above the melting point of the ink, cooling means providing a cooling zone adjacent to the heating zone for cooling the substrate after heating, drive means for moving a substrate continuously through the heating zone and the cooling zone, input means having a curved surface for supporting the substrate as it moves into the heating zone to prevent cockle, and output means having a curved surface for supporting the substrate as it moves from the heating zone into the cooling zone to prevent cockle.
9. Apparatus according to Claim 8 wherein the radius of curvature of each of the curved surfaces is less than about 8 cm.
10. Apparatus according to Claim 8 wherein the radius of curvature of each of the curved surfaces is less than about 5 cm.
11. Apparatus according to Claim 8 wherein the angular length of each of the curved surfaces is at least about 5°.
- 30 12. Apparatus according to Claim 8 wherein the angular length of each of the curved surfaces is at least about 10°.

13. Apparatus according to Claim 8 including means for supporting the substrate within the heating zone while maintaining a radius of curvature of the substrate which is greater than that of the curved surfaces.
5
14. Apparatus according to Claim 13 wherein the means for supporting the substrate within the heating zone maintains a radius of curvature which is at least 5 cm.
- 10 15. Apparatus according to Claim 13 wherein the means for supporting the substrate within the heating zone maintains the substrate substantially flat.
16. Apparatus according to Claim 8 including guide means for guiding the substrate in the cooling zone having a surface which is curved in the opposite direction with respect to the curved surfaces of the input and output means.
15
17. Apparatus according to Claim 16 wherein the radius of curvature of the curved surface in the cooling zone guide means is less than that of either of the curved surfaces of the input means and the output means.
20
18. Apparatus according to Claim 16 wherein the radius of curvature of the curved surface in the cooling zone guide means is less than about half that of either of the curved surfaces of the input means and the output means.
25
19. Apparatus according to Claim 16 wherein the radius of curvature of the curved surface in the cooling zone guide means is no more than about 1 cm.
30

20. Apparatus according to Claim 8 wherein the drive means includes input drive means for moving a substrate into the heating zone and output drive means for moving the substrate through the cooling zone.
5
21. Apparatus according to Claim 20 wherein the output drive means moves the substrate at a faster rate than the input drive means.
22. Apparatus according to Claim 20 including one-way
10 clutch means associated with the input drive means.
23. A method for treating a hot melt ink images comprising moving a substrate containing a solid hot melt ink image along a curved surface into a heating zone, heating the substrate in the heating zone to a temperature above the melting point of the hot melt ink, moving the substrate out of the heating zone into a cooling zone along a curved surface, cooling the hot melt ink in the
15 cooling zone and moving the substrate in the cooling zone along a surface having a reverse curvature with respect to the curvature of the curved surfaces.
20
24. A method according to Claim 23 including maintaining the substrate in the heating zone in a condition in which it has a radius of curvature greater than that of the curved surfaces.
25
25. A method according to Claim 23 including moving the lead edge of a substrate into the heating zone at a selected rate by a first transport device at the input end of the heating zone, and moving the substrate through the heating zone at a rate greater than the selected rate by a second
30

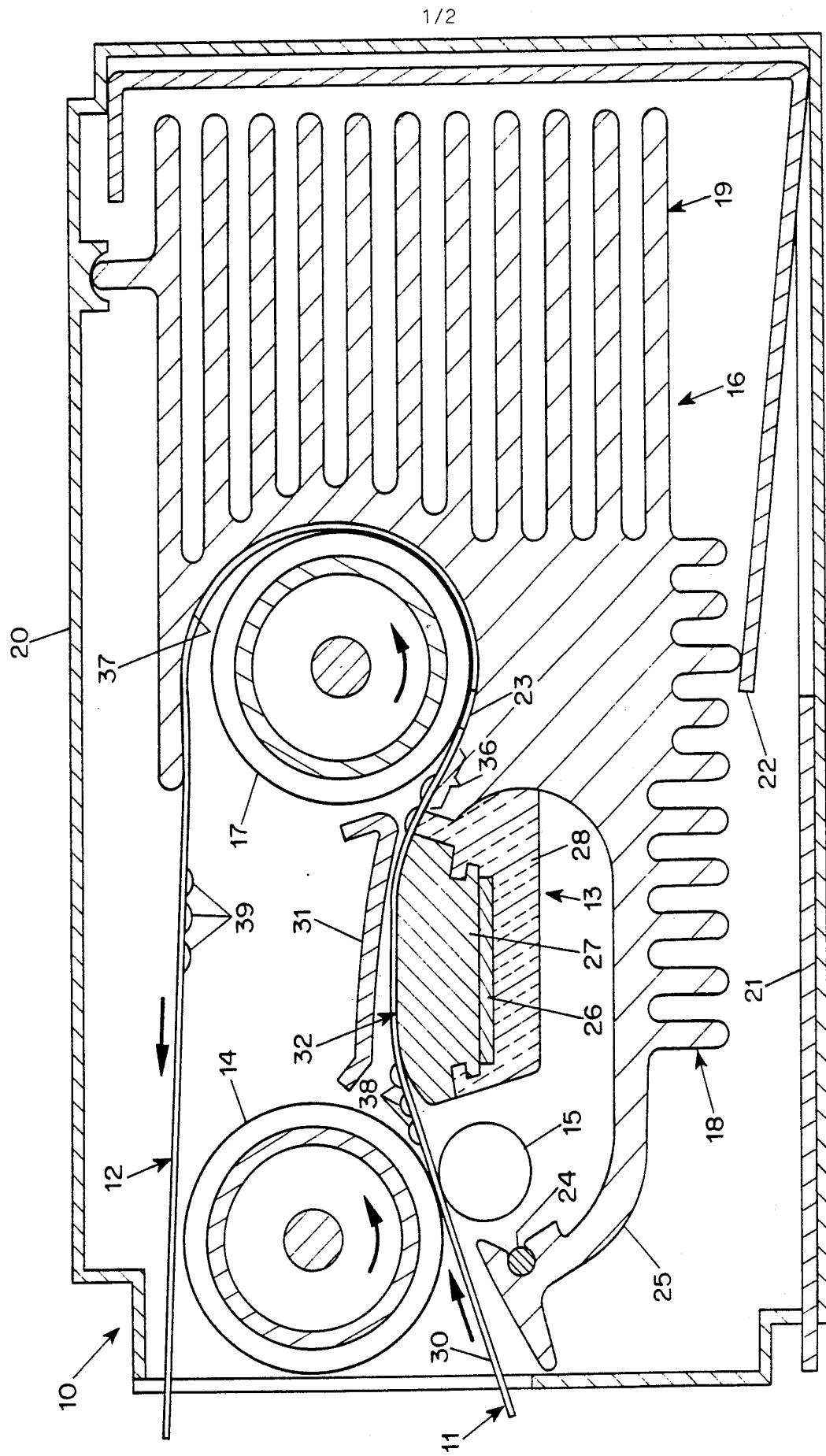
transport device adjacent to the output end of the heating zone while maintaining the substrate in contact with a heated surface.

26. A method according to Claim 25 including applying tension to the substrate between the input and output transport devices to hold the substrate in thermal contact with the heated surface.
27. Apparatus for treating hot melt ink images comprising heating platen means having a first curved surface at an input end, a second curved surface at an output end, and a surface between the two curved surfaces which has less curvature than the curved surfaces, first drive means for directing a substrate to the input end of the heating platen means, and second drive means for withdrawing a substrate from the output end of the heated platen means.
28. Apparatus according to Claim 27 wherein the second drive means is arranged to move the substrate at a higher rate than the first drive means.
29. Apparatus according to Claim 28 wherein the first drive means includes one-way clutch means for imposing a drag on the substrate when it is driven by the second drive means.
30. Apparatus according to Claim 27 including decurling means comprising a platen having a surface with a concave portion and wherein the second drive means comprises a drive roll cooperating with the surface of the platen to engage and drive a substrate along the concave surface, and means for urging one of the second drive means and the surface of the platen toward the other.

31. Apparatus according to Claim 27 including quenching platen means adjacent to the output end of the heating platen means for cooling a hot melt ink image on a substrate at a rapid rate.
- 5 32. Apparatus according to Claim 27 wherein the quenching platen means has a curved surface to provide good heat transfer contact between the platen and the substrate.
- 10 33. Apparatus according to Claim 31 wherein the quenching platen means comprises a plurality of cooling fins arranged to maintain a platen at a temperature less than the melting point of hot melt ink in a hot melt ink image being treated by the apparatus.
- 15 34. Apparatus according to Claim 27 wherein the heating platen means includes heating means for maintaining the heating platen at a temperature above the melting point of hot melt ink in a hot melt ink image being treated by the apparatus.
- 20 35. A method for preparing a transparency comprising applying hot melt ink to the surface of a transparent substrate to form a three-dimensional ink pattern having an upper surface containing a curved configuration, and maintaining the ink in the pattern at a temperature above the melting point of the ink during a time interval of at least 0.5 sec. to change the configuration of the upper surface.
- 25 36. A method according to Claim 35 wherein the ink is maintained at a temperature above its melting point for about 0.5 to 10 sec.

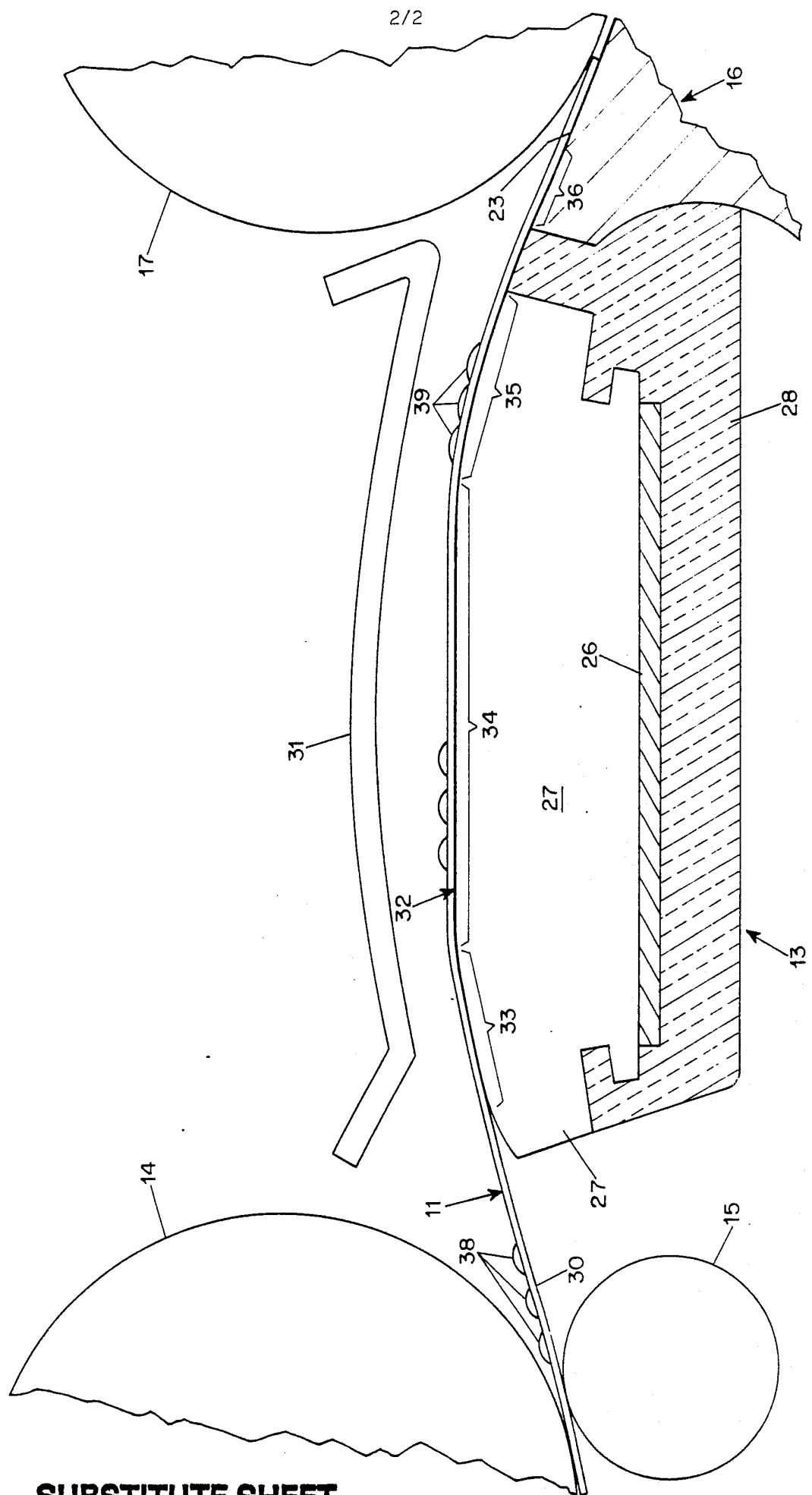
37. A method according to Claim 35 wherein the ink is maintained at a temperature above its melting point for about 1 to 5 sec.
38. A method according to Claim 35 wherein the temperature is maintained within the range from about 5°C to about 40°C above the melting point of the ink.
39. A method according to Claim 35 wherein the temperature is maintained within the range from about 10°C to about 30°C above the melting point of the ink.
40. A method according to Claim 35 including the step of cooling the ink rapidly after the time interval to reduce crystallization or frosting of the ink.
41. A method according to Claim 40 wherein the ink is cooled at a rate of at least 50°C per second.
42. A method according to Claim 41 wherein the ink is cooled at a rate of at least 100°C per second.
43. A method according to Claim 41 wherein the ink is cooled at a rate of about 500°C to 1000°C per second.
44. A method according to Claim 35 wherein the ink is maintained at a temperature above its melting point immediately after it is applied to the transparent substrate.
45. A method according to Claim 35 wherein the ink is solidified after being applied to the transparent substrate and the solidified ink is thereafter

heated and maintained at a temperature above its melting point.



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FIG.

SUBSTITUTE SHEET

**SUBSTITUTE SHEET****FIG. 2**

INTERNATIONAL SEARCH REPORT

International Application No

PCT/US90/04997

I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) ^{1,4}

According to International Patent Classification (IPC) or to both National Classification and IPC

IPC(5): B05D 3/00, 5/00, 5/06; B05C 11/02

US CL.: 427/164,172,256,271,188,324.5,398.2,444; 118/59,67,69; 346/1.1,140R

II. FIELDS SEARCHED

Minimum Documentation Searched ⁴

Classification System ¹	Classification Symbols
US	427/164,172,256,264,271,288,374.5,398.2,444; 118/59,67,69; 346/1.1, 25, 135.1, 140R

Documentation Searched other than Minimum Documentation
to the Extent that such Documents are Included in the Fields Searched ⁵

III. DOCUMENTS CONSIDERED TO BE RELEVANT ^{1,4}

Category ⁶	Citation of Document, ^{1,6} with indication, where appropriate, of the relevant passages ^{1,7}	Relevant to Claim No. ^{1,8}
X	US, A, 4,751,528 (SPEHRLEY, JR. et al.) 14 June 1988, See the entire document.	1-12,35-39 44
X	US, A, 4,853,706 (VAN BRIMER et al.) 01 August 1989 See the entire document.	35-39,45
X,P	US, A, 4,873,134 (FULTON et al.) 10 October 1989 See the entire document.	1-7,35-45
X,E	US, A, 4,971,408 (HOISINGTON et al.) 20 November 1990 See the entire document.	35-39,45
A,P	US, A, 4,889,761 (TITTERINGTON et al.) 26 December 1989 See the entire document.	

* Special categories of cited documents: ^{1,9}

"A" document defining the general state of the art which is not considered to be of particular relevance

"E" earlier document but published on or after the international filing date

"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

"&" document member of the same patent family

IV. CERTIFICATION

Date of the Actual Completion of the International Search ²

18 DECEMBER 1990

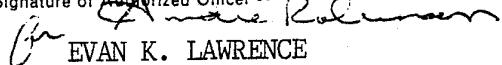
International Searching Authority ¹

ISA/US

Date of Mailing of this International Search Report ²

04 FEB 1991

Signature of Authorized Officer ²⁰


EVAN K. LAWRENCE